

# Alexa: MPI+X Shock Hydrodynamics on Dynamically Adaptive Tetrahedral Meshes

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N. Roberts and T. Voth MULTIMAT 2017

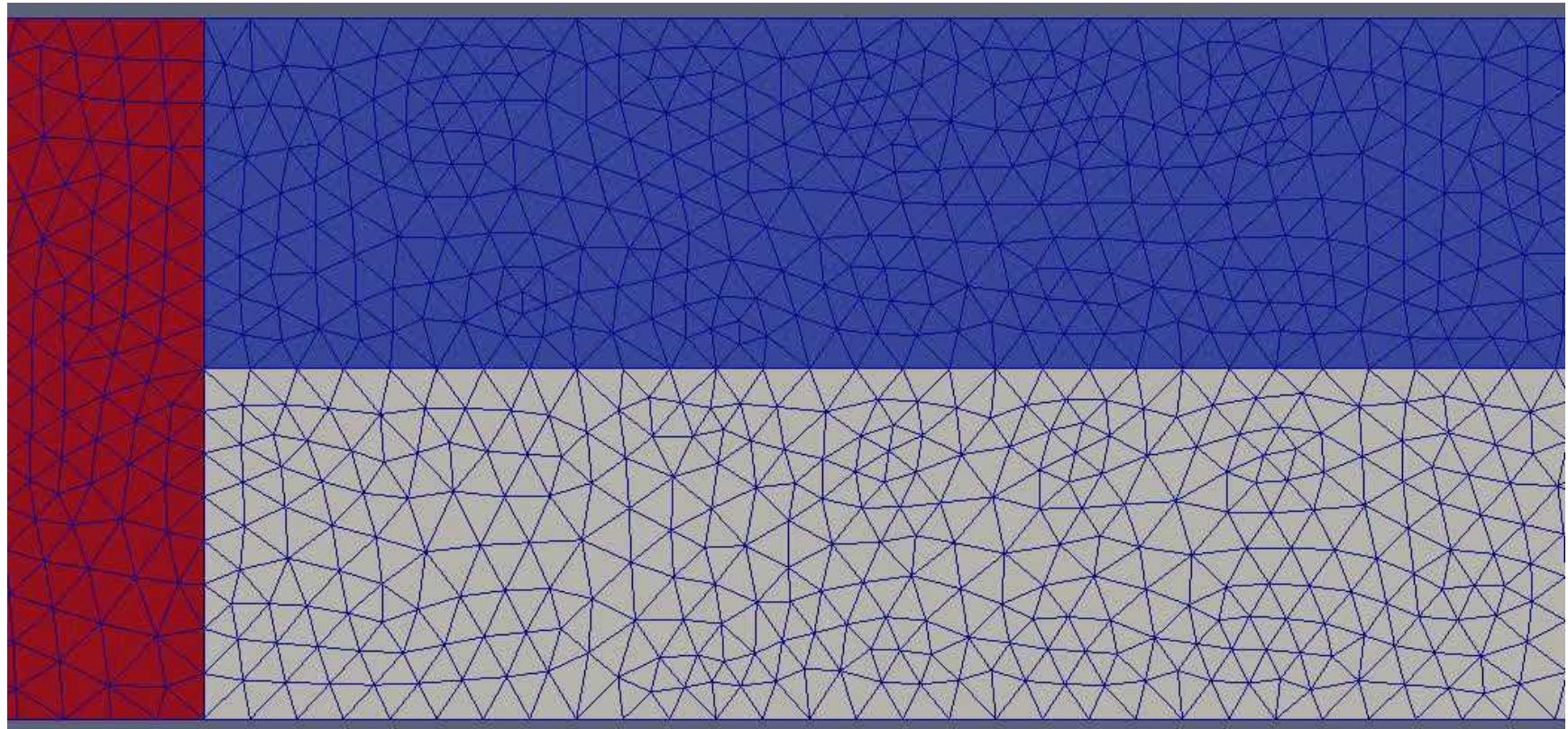


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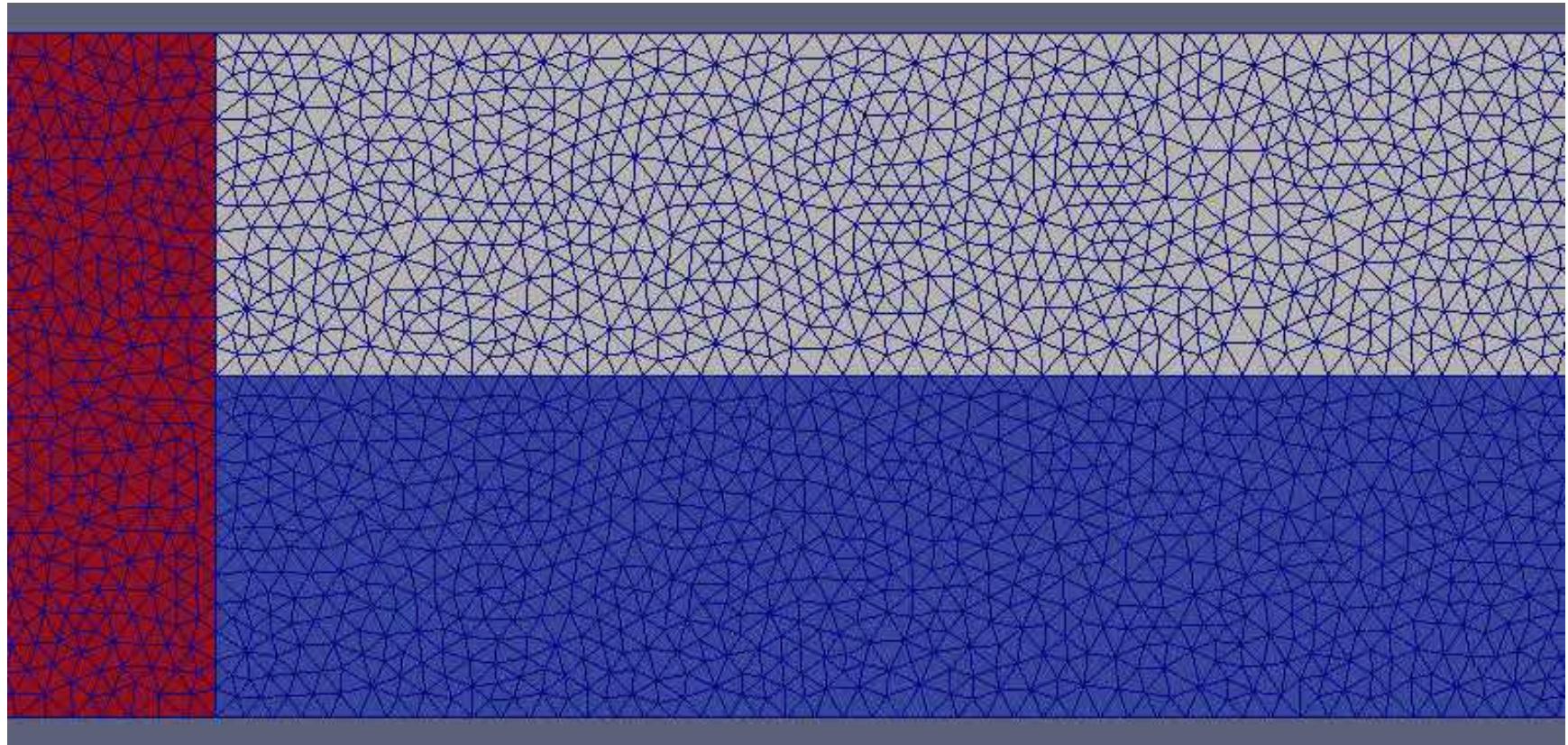
# Alexa

- Portably Performant: runs efficiently on most modern hardware, especially NVIDIA GPUs
- Adaptive Lagrangian: Like ALE (Arbitrary Lagrangian-Eulerian) except no Eulerian component, does adaptation (remeshing) by local modification, maintains single-material elements
- Shock Hydrodynamics: Compressible gases, elastic and plastic solids, and more material models combined to form true multi-material simulations
- All in 3D!

# Pure Lagrangian Triple-Point



# Adaptive Lagrangian Triple-Point



# Lagrangian continuum equations

- Conservation of linear momentum:

$$\langle \delta\varphi, \rho\dot{\mathbf{v}} \rangle + \langle \text{grad}[\delta\varphi], \boldsymbol{\sigma} \rangle = 0 \quad \forall \varphi$$

- Balance of internal energy:

$$\langle \delta\theta, \rho\dot{\varepsilon} \rangle - \langle \delta\theta, \text{grad}[\mathbf{v}] \bullet \boldsymbol{\sigma} \rangle = 0 \quad \forall \delta\theta$$

- Kinematics:

$$\dot{\mathbf{x}} - \mathbf{v} = \mathbf{0}$$

$$\mathbf{F} := \text{GRAD}[\mathbf{x}] \quad J := \det(\mathbf{F})$$

- Conservation of mass:

$$\rho = J^{-1}\rho_0$$

- Constitutive model:

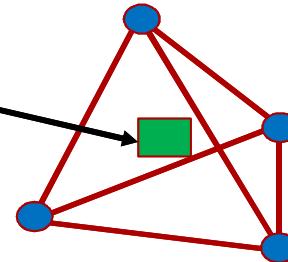
$$\boldsymbol{\sigma} := -\hat{p}(\rho, \epsilon)\mathbf{I} + \boldsymbol{\sigma}_{\text{dev}} + \boldsymbol{\sigma}_{\text{art}}$$

# Implementational details

- Use *VMS four-node tetrahedral elements* (for now).

Cell-Centered:

- Density
- Internal Energy
- Deformation Gradient
- Pressure



Nodal:

- Displacement
- Velocity
- Pressure

- Use *second order explicit predictor-corrector* time integration.
- *Tensor shock-capturing artificial viscosity*.
- Limited number of material models:
  - Ideal gas
  - Mie-Gruneisen
  - Neo-hookean thermo-elastic
  - Mechanical multiplicative J-2 plasticity

# VMS Formulation

- Conservation of linear momentum:

$$\langle \delta\varphi^h, \rho\dot{\mathbf{v}}^h \rangle + \langle \text{grad}[\delta\varphi^h], -p^h \rangle + \langle \text{grad}\delta\varphi^h, \text{dev}\boldsymbol{\sigma} \rangle + \langle \text{grad}\delta\varphi^h, -p' \rangle = 0 \quad \forall \varphi^h$$

- Balance of internal energy:

$$\langle \delta\theta^h, \rho\dot{\varepsilon} \rangle - \langle \delta\theta^h, \text{grad}[\mathbf{v}] \bullet (-p^h\mathbf{I} + \text{dev}\boldsymbol{\sigma} - p'\mathbf{I}) \rangle = 0 \quad \forall \delta\theta^h$$

- Pressure projection:

$$\langle \eta^h, p^h \rangle - \langle n^h, p \rangle + \langle \text{grad}\eta^h, -\mathbf{u}' \rangle = 0 \quad \forall \eta^h$$

Multi-scale fields:

$$p' = -\tau(\dot{p}^h + \rho c^2 \text{div } \mathbf{v}^h)$$

$$\mathbf{v}' = -\frac{\tau}{\rho} (\rho\dot{\mathbf{v}}^h + \text{grad}p^h - \text{div}(\text{dev}\boldsymbol{\sigma})) \quad \mathbf{u}' = \int_0^t \rho c^2 \mathbf{v}'(t) dt$$

# VMS Formulation

- The pressure-prime term is designed to stabilize zero-energy volume modes for materials without deviatoric response.
- The displacement-prime term is designed to stabilize the inf-sup condition for continuous nodal pressure element formulations.
- The goal is for this element to be applicable for both compressible gas dynamics (no zero-energy modes) and nearly incompressible elasticity simulations (no locking).
- Yes, that is a lot to ask of a single element formulation! Maybe too much...

# Time integration

for(int  $i = 0; i < 2; ++i\{$

Define  $\boldsymbol{\sigma} := -p^h \mathbf{I} - \mathbf{p}' + \boldsymbol{\sigma}_{\text{dev}}$

1. Update nodal velocity:

$$\left\langle \delta\boldsymbol{\varphi}^h, \rho(\mathbf{v}_{n+1}^{(i+1)} - \mathbf{v}_n) \right\rangle + \Delta t \left\langle \text{grad}[\delta\boldsymbol{\varphi}^h], \boldsymbol{\sigma}_{n+\frac{1}{2}}^{(i)} \right\rangle = 0$$

2. Update element-centered internal energy:

$$\left\langle \delta\theta^h, \rho(\varepsilon_{n+1}^{(i+1)} - \varepsilon_n) \right\rangle - \Delta t \left\langle \delta\theta^h, \text{grad}[\mathbf{v}_{n+\frac{1}{2}}^{(i+1)}] \bullet \boldsymbol{\sigma}_{n+\frac{1}{2}}^{(i)} \right\rangle = 0$$

3. Update nodal coordinates:

$$\mathbf{x}_{n+1}^{(i+1)} - \mathbf{x}_n - \Delta t \cdot \mathbf{v}_{n+\frac{1}{2}}^{(i+1)} = \mathbf{0}$$

4. Update deformation gradient, volume element, and spatial density.
5. Update element-centered material models.

# Time Integration (continued)

6. Update nodal pressure field:

$$\left\langle \eta^h, p_{n+1}^{h(i+1)} \right\rangle - \left\langle \eta^h, p_{n+1}^{i+1} \right\rangle + \left\langle \text{grad} \eta^h, -\mathbf{u}'_{n+\frac{1}{2}}^{(i+1)} \right\rangle = 0$$

7. Update element-centered fine scale fields:

$$\mathbf{v}' := -\frac{\tau}{\rho_{n+\frac{1}{2}}^{(i+1)}} \left[ \rho_{n+\frac{1}{2}}^{(i+1)} \left( \mathbf{v}_{n+1}^{(i+1)} - \mathbf{v}_n \right) \Delta t^{-1} + \text{grad } p_{n+\frac{1}{2}}^{h(i+1)} \right]$$

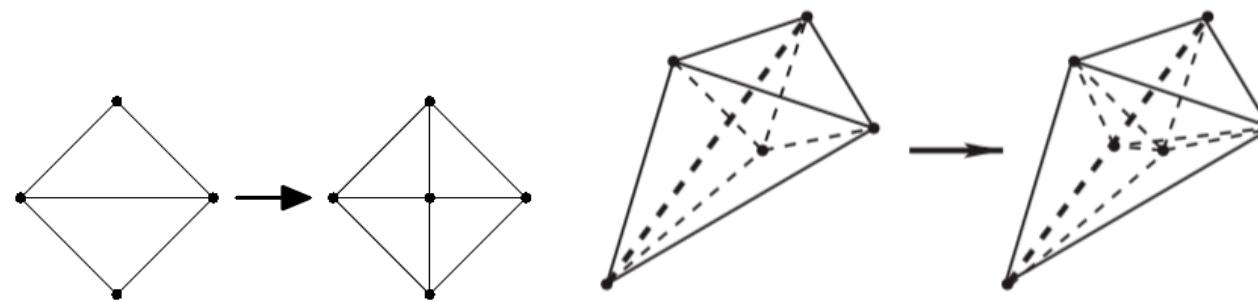
$$\mathbf{u}'_{n+1}^{(i+1)} = \mathbf{u}'_n + \left[ \rho_{n+\frac{1}{2}}^{(i+1)} c_{n+\frac{1}{2}}^{(i+1)2} \right] (\mathbf{v}' \Delta t)$$

}

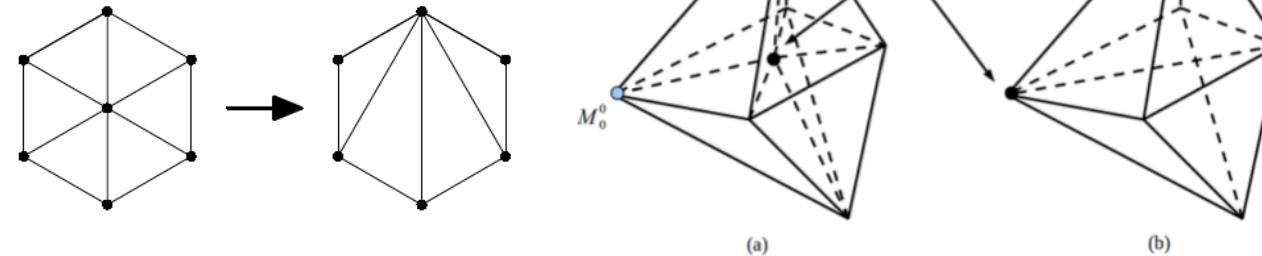
The sequence of steps here is explicitly designed to discretely conserve total energy.

# Local Cavity Modifications

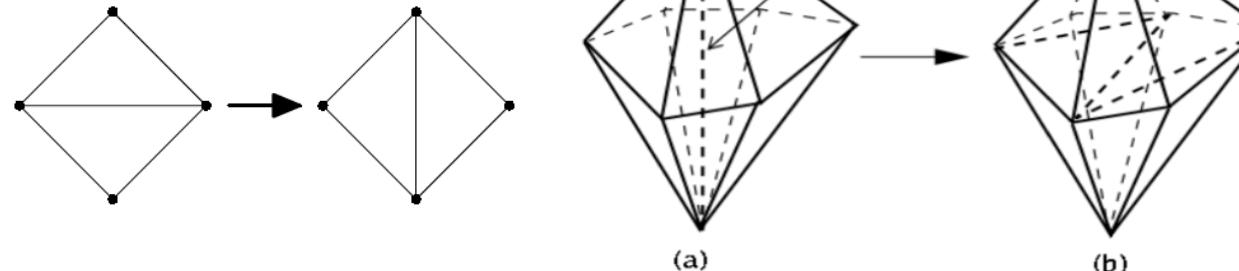
- Split



- Collapse



- Swap



# Metric Tensor Field

- Symmetric Positive Definite tensor

$$\mathcal{M} = R^T \Lambda R, \quad R^T R = I, \quad \Lambda = \text{diag}(\lambda_1, \dots, \lambda_d), \quad \forall i \in [1, d] : \lambda_i > 0$$

- Exist linear transform(s) from real space to “metric space”

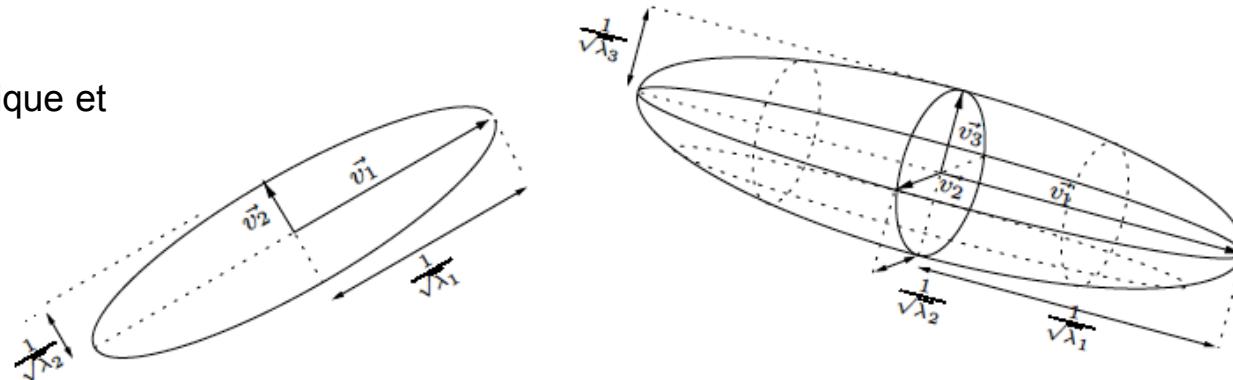
$$Q = \Lambda^{\frac{1}{2}} R, \quad \Lambda^{\frac{1}{2}} = \text{diag}(\sqrt{\lambda_1}, \dots, \sqrt{\lambda_d})$$

- Defines an inner product, transform-then-dot

$$\mathbf{u}^T \mathcal{M} \mathbf{v} = \mathbf{u}^T R^T \Lambda R \mathbf{v} = \mathbf{u}^T R^T \Lambda^{\frac{1}{2}} \Lambda^{\frac{1}{2}} R \mathbf{v} = \mathbf{u}^T Q^T Q \mathbf{v} = (Qu)^T (Qv) = \tilde{\mathbf{u}}^T \tilde{\mathbf{v}}$$

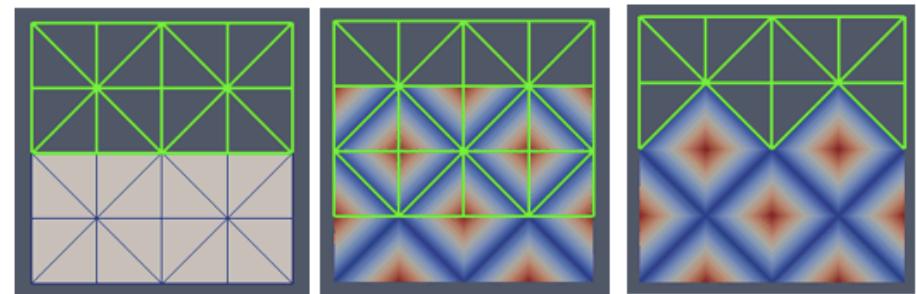
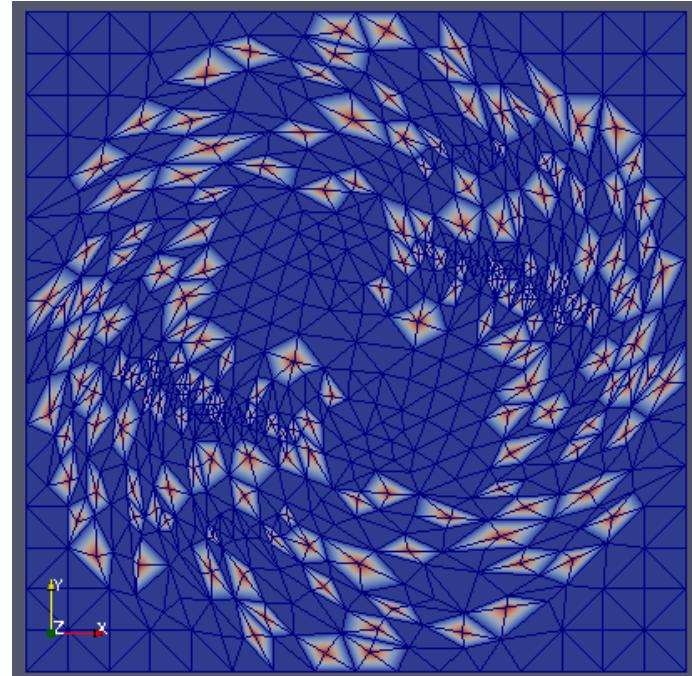
- Defines an ellipsoid of desired resolution in each direction

F. Alauzet and P. Frey  
 Estimateur d'erreur géométrique et  
 métriques anisotropes pour  
 l'adaptation de maillage.  
 Partie I : aspects théoriques



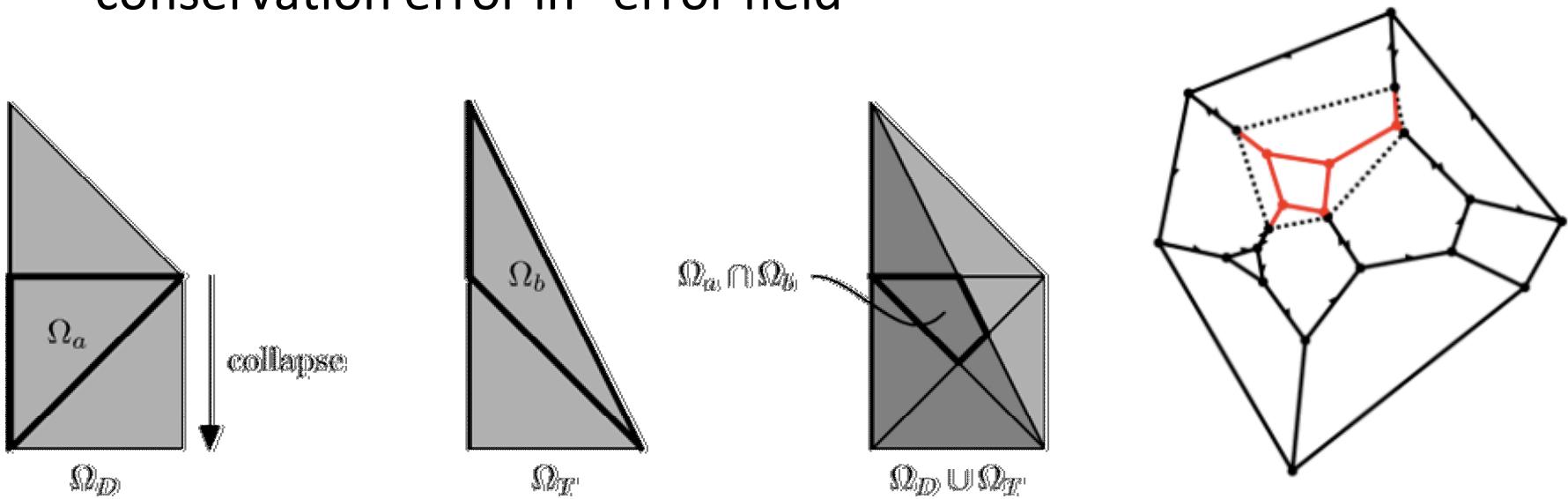
# One Round of Changes

- All of the same kind
- Non-overlapping (independent set)
- Runs in parallel with minimal and scalable communication
- Construct new mesh from old mesh
- Selection and modification are fully deterministic
- Serial-parallel consistent!



# Conserved cell-average quantities

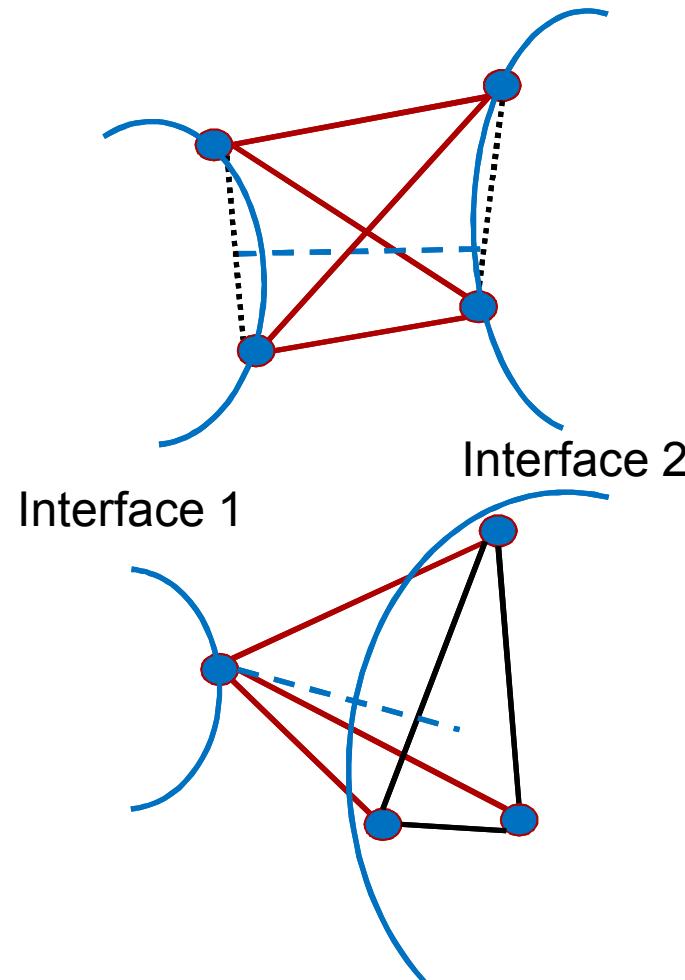
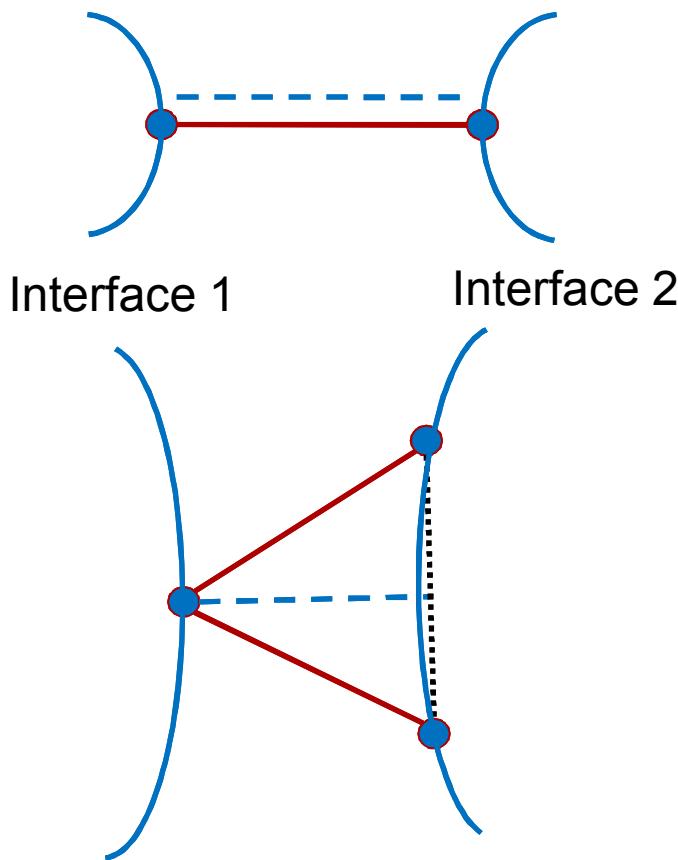
- For refinement, simply divide by two, assign to child cells
- Use R3D-based intersection remap on interior cavities
  - Conservative and bounds-preserving
- For curved boundary collapses, keep same density, record conservation error in “error field”



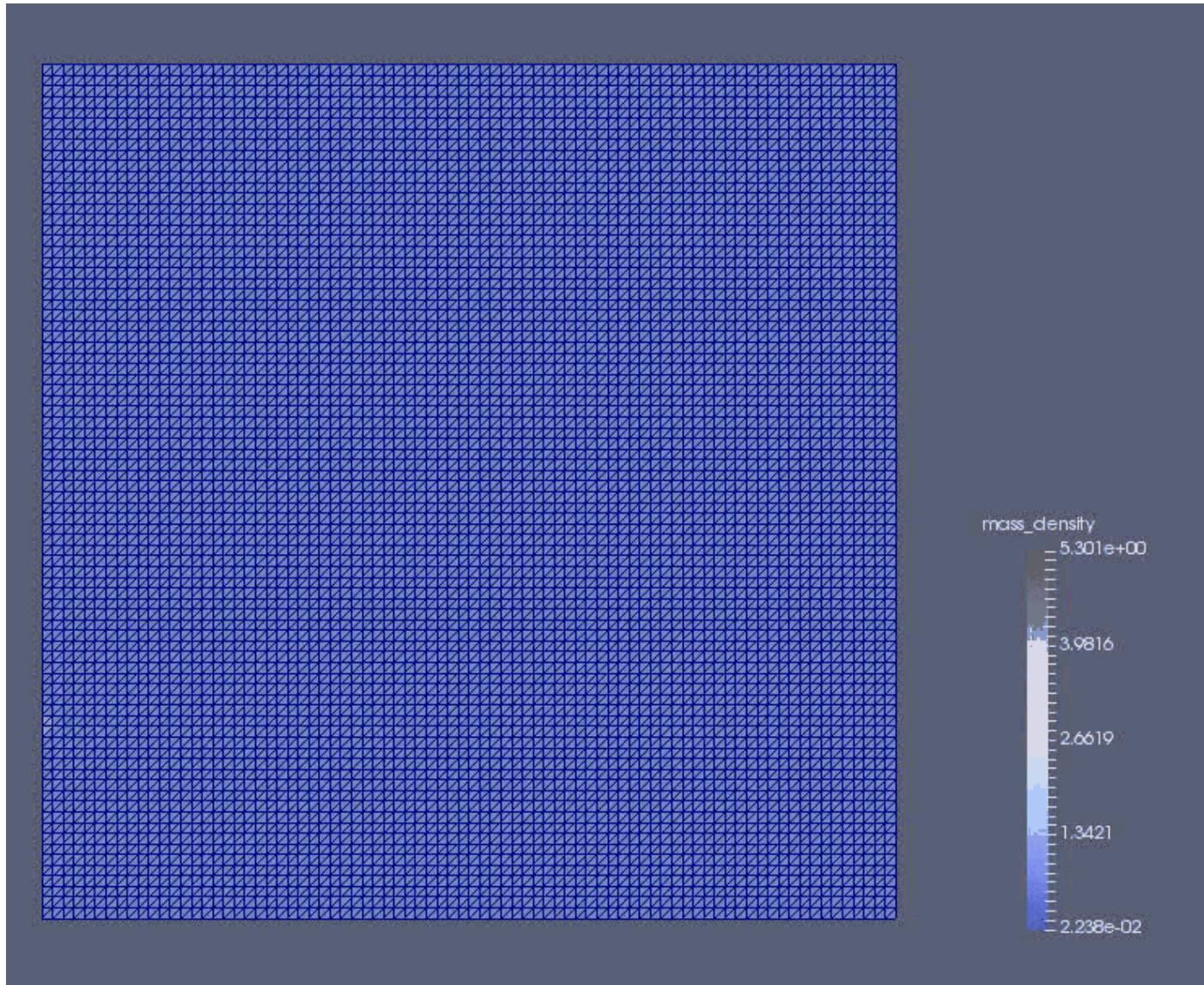
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# Two-Interface Proximity Detection

- Measure shortest distance across single elements

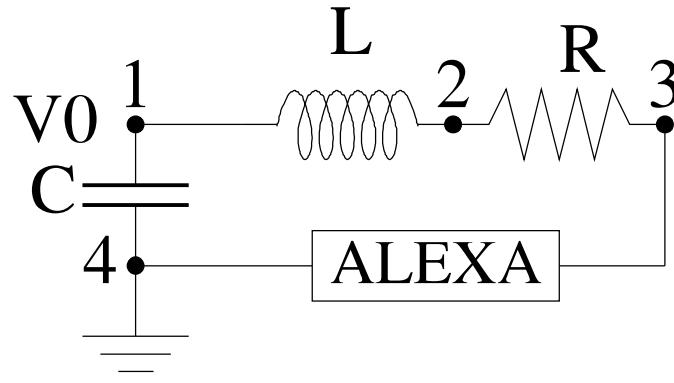


# Airblast



# Low-Rm MHD (Joule Heating)

- We model a circuit with Joule heating connected to our mesh.
- We allow an RLC circuit, and a scalar conductivity  $\sigma$ .



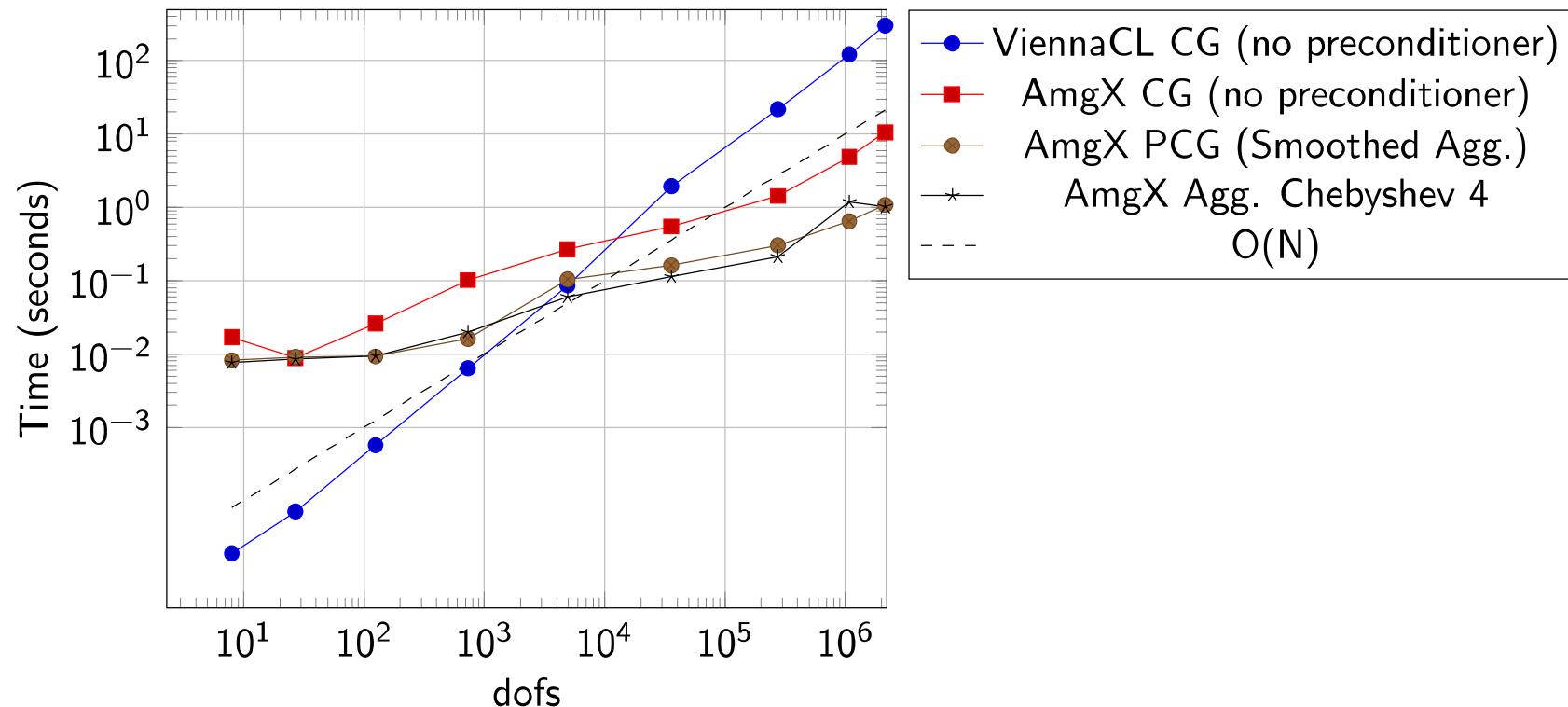
- Computationally intensive part of this is the Poisson solve:

$$(\nabla \phi, \sigma \nabla v)_{\Omega} = (f, v)_{\Omega} \quad \forall v$$

To gauge performance on a problem that approximates the physics of interest, we use a high-contrast  $\sigma = (10^6 - 1)x^2 + 1$  and solve on  $\Omega = [0, 1]^3$ . We use GPU-accelerated solvers a single NVIDIA P100.

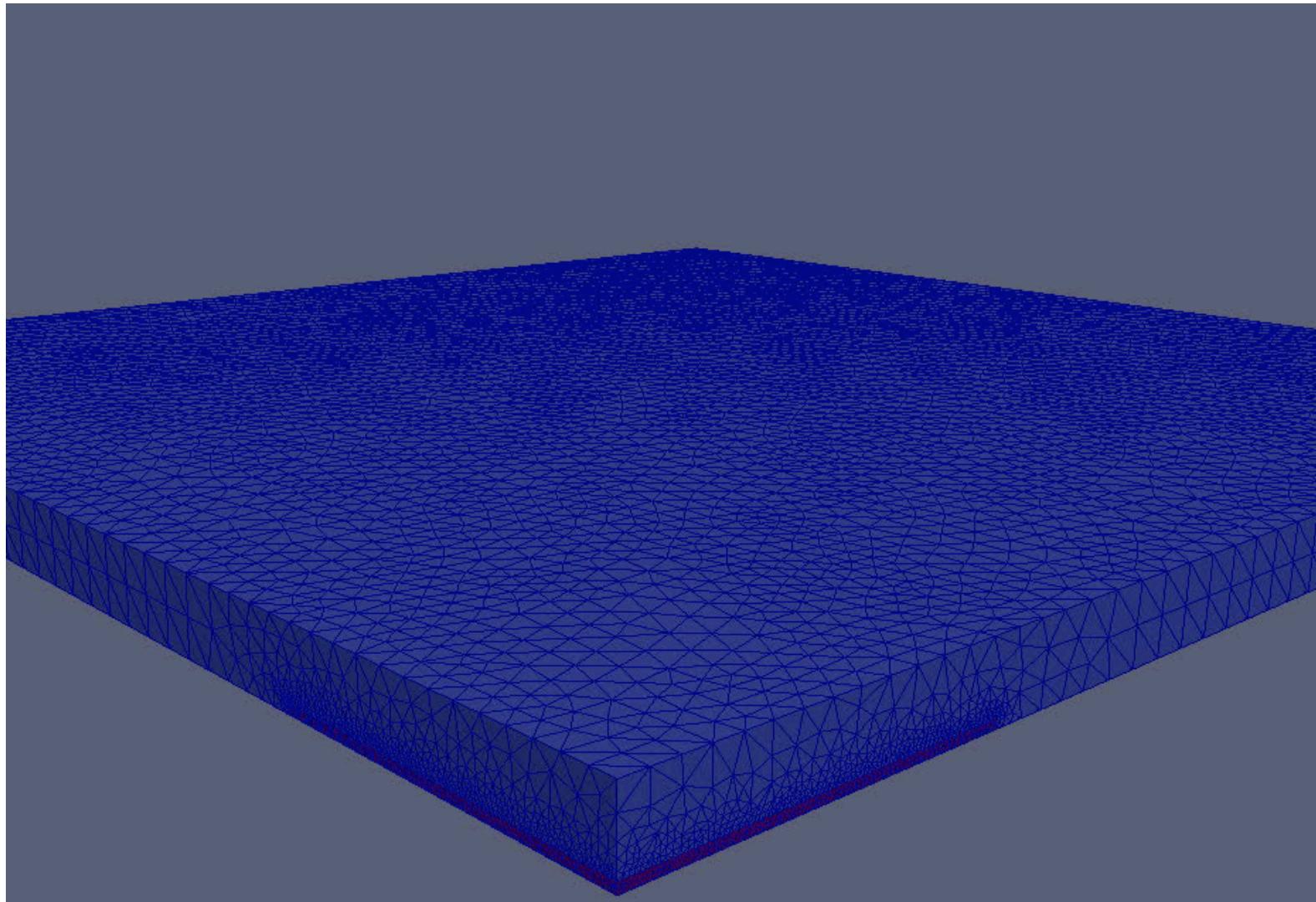
# Higher-Contrast Poisson: Timings

White P100 3D FEM (higher-contrast Poisson), performance comparison



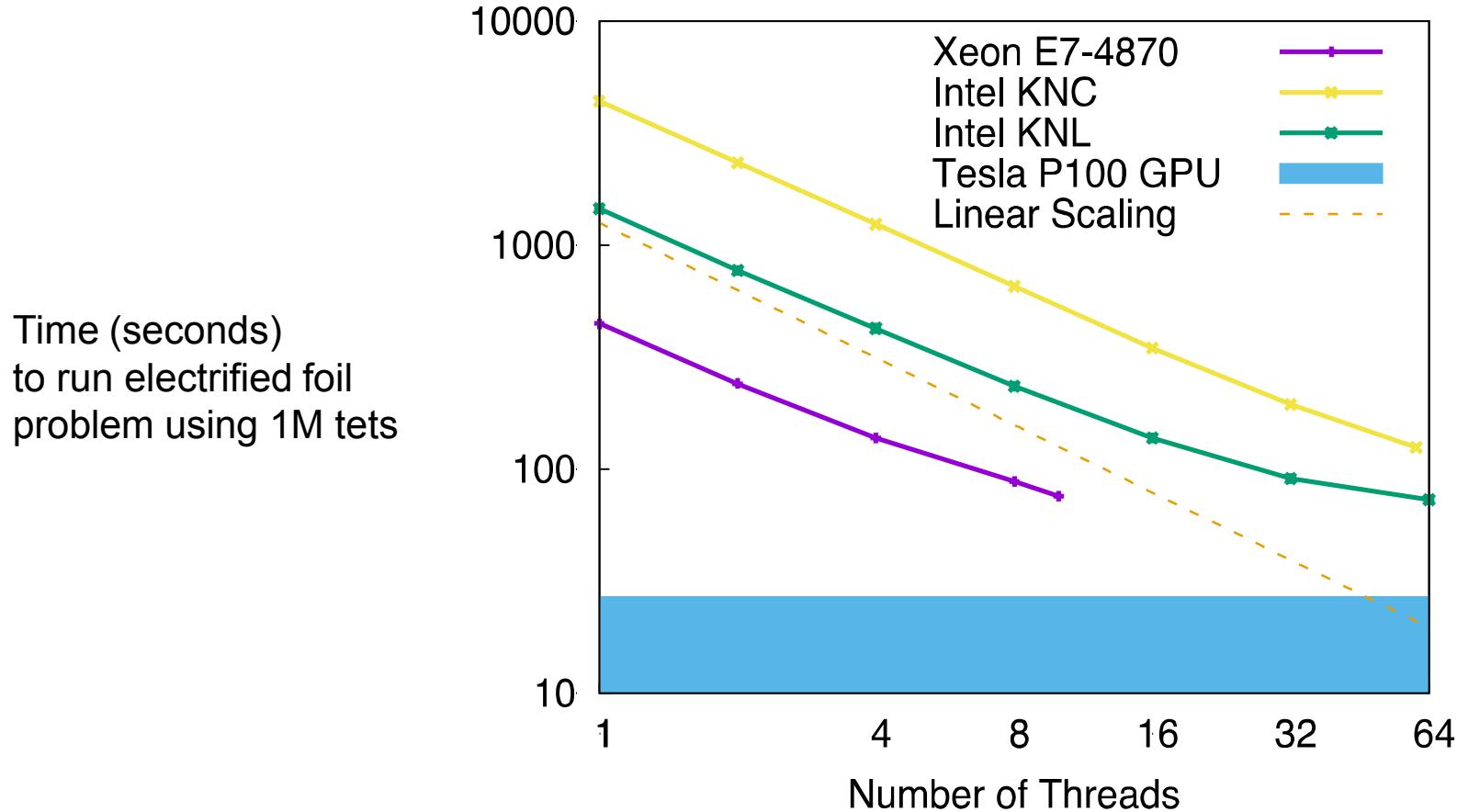
Convergence criterion: reduce residual by factor of  $10^{-10}$ .

# Electrified Foil



# Performance Portability

- Kokkos is used for on-node parallelism
- Good performance across Intel Xeon Phi and NVIDIA cards



# Thank You

... Questions ?

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