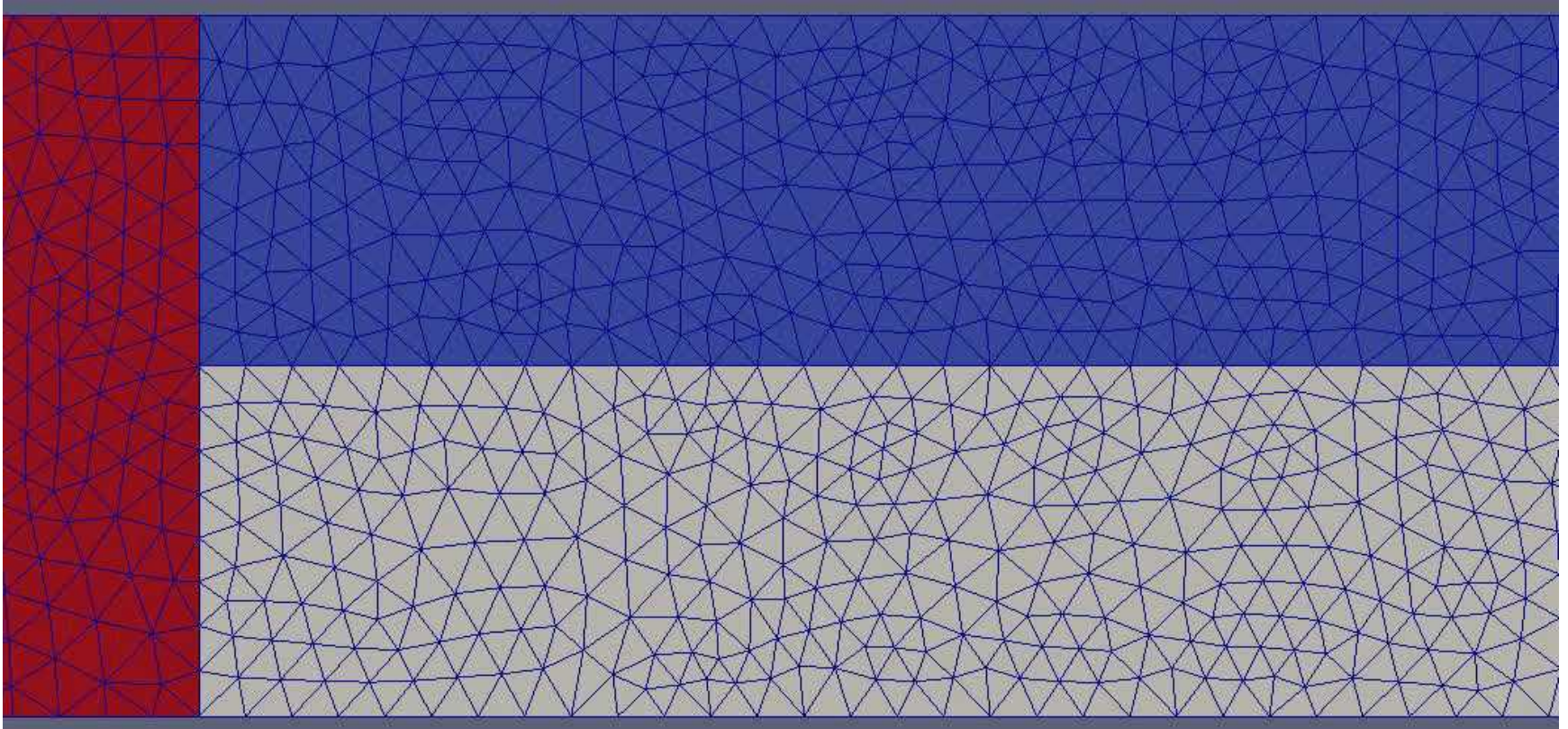


Alexa: MPI+X Shock Hydrodynamics on Dynamically Adaptive Tetrahedral Meshes

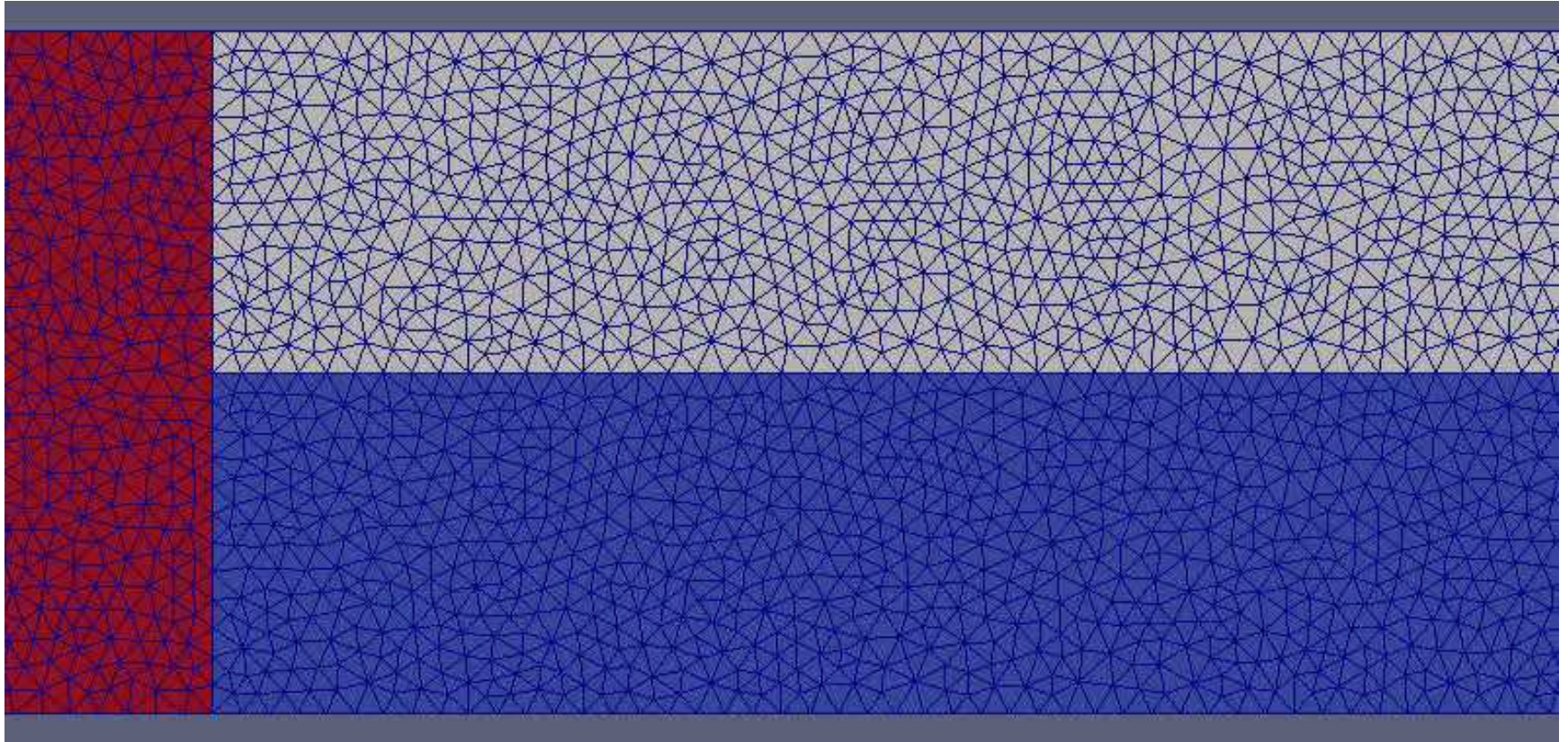
G. Hansen, D. Ibanez, E. Love, J. Overfelt,
N. Roberts and T. Voth MULTIMAT 2017

- Portably Performant: runs efficiently on most modern hardware, especially NVIDIA GPUs
- Adaptive Lagrangian: Like ALE (Arbitrary Lagrangian-Eulerian) except no Eulerian component, does adaptation (remeshing) by local modification, maintains single-material elements
- Shock Hydrodynamics: Compressible gases, elastic and plastic solids, and more material models combined to form true multi-material simulations
- All in 3D!

Pure Lagrangian Triple-Point



Adaptive Lagrangian Triple-Point



Lagrangian continuum equations

- Conservation of linear momentum:

$$\langle \delta \boldsymbol{\varphi}, \rho \dot{\mathbf{v}} \rangle + \langle \text{grad}[\delta \boldsymbol{\varphi}], \boldsymbol{\sigma} \rangle = 0 \quad \forall \boldsymbol{\varphi}$$

- Balance of internal energy:

$$\langle \delta \theta, \rho \dot{\epsilon} \rangle - \langle \delta \theta, \text{grad}[\mathbf{v}] \bullet \boldsymbol{\sigma} \rangle = 0 \quad \forall \delta \theta$$

- Kinematics:

$$\dot{\mathbf{x}} - \mathbf{v} = \mathbf{0}$$

$$\mathbf{F} := \text{GRAD}[\mathbf{x}] \quad J := \det(\mathbf{F})$$

- Conservation of mass:

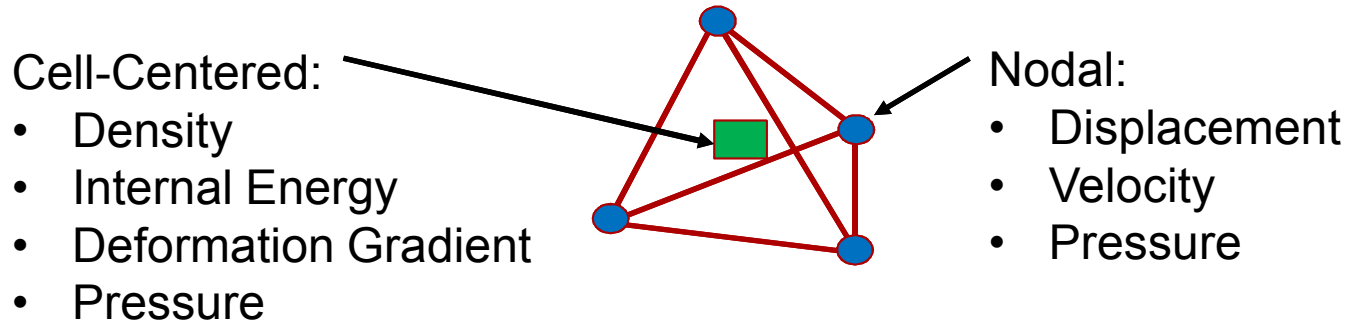
$$\rho = J^{-1} \rho_0$$

- Constitutive model:

$$\boldsymbol{\sigma} := -\hat{p}(\rho, \epsilon) \mathbf{I} + \boldsymbol{\sigma}_{\text{dev}} + \boldsymbol{\sigma}_{\text{art}}$$

Implementational details

- Use *VMS four-node tetrahedral* elements (for now).



- Use *second order explicit predictor-corrector* time integration.
- *Tensor shock-capturing artificial viscosity.*
- Limited number of material models:
 - Ideal gas
 - Mie-Gruneisen
 - Neo-hookean thermo-elastic
 - Mechanical multiplicative J-2 plasticity

VMS Formulation

- Conservation of linear momentum:

$$\langle \delta \boldsymbol{\varphi}^h, \rho \dot{\mathbf{v}}^h \rangle + \langle \text{grad}[\delta \boldsymbol{\varphi}^h], -p^h \rangle + \langle \text{grad} \delta \boldsymbol{\varphi}^h, \text{dev} \boldsymbol{\sigma} \rangle + \langle \text{grad} \delta \boldsymbol{\varphi}^h, -p' \rangle = 0 \quad \forall \boldsymbol{\varphi}^h$$

- Balance of internal energy:

$$\langle \delta \theta^h, \rho \dot{\varepsilon} \rangle - \langle \delta \theta^h, \text{grad}[\mathbf{v}] \bullet (-p^h \mathbf{I} + \text{dev} \boldsymbol{\sigma} - p' \mathbf{I}) \rangle = 0 \quad \forall \delta \theta^h$$

- Pressure projection:

$$\langle \eta^h, p^h \rangle - \langle n^h, p \rangle + \langle \text{grad} \eta^h, -\mathbf{u}' \rangle = 0 \quad \forall \eta^h$$

Multi-scale fields:

$$p' = -\tau(\dot{p}^h + \rho c^2 \text{div} \mathbf{v}^h)$$

$$\mathbf{v}' = -\frac{\tau}{\rho} (\rho \dot{\mathbf{v}}^h + \text{grad} p^h - \text{div}(\text{dev} \boldsymbol{\sigma})) \quad \mathbf{u}' = \int_0^t \rho c^2 \mathbf{v}'(t) dt$$

VMS Formulation

- The pressure-prime term is designed to stabilize zero-energy volume modes for materials without deviatoric response.
- The displacement-prime term is designed to stabilize the inf-sup condition for continuous nodal pressure element formulations.
- The goal is for this element to be applicable for both compressible gas dynamics (no zero-energy modes) and nearly incompressible elasticity simulations (no locking).
- Yes, that is a lot to ask of a single element formulation! Maybe too much...

Time integration

for(int $i = 0; i < 2; ++i$) {

Define $\boldsymbol{\sigma} := -p^h \mathbf{I} - p' + \boldsymbol{\sigma}_{\text{dev}}$

1. Update nodal velocity:

$$\left\langle \delta \varphi^h, \rho(\mathbf{v}_{n+1}^{(i+1)} - \mathbf{v}_n) \right\rangle + \Delta t \left\langle \text{grad}[\delta \varphi^h], \boldsymbol{\sigma}_{n+\frac{1}{2}}^{(i)} \right\rangle = 0$$

2. Update element-centered internal energy:

$$\left\langle \delta \theta^h, \rho(\varepsilon_{n+1}^{(i+1)} - \varepsilon_n) \right\rangle - \Delta t \left\langle \delta \theta^h, \text{grad}[\mathbf{v}_{n+\frac{1}{2}}^{(i+1)}] \bullet \boldsymbol{\sigma}_{n+\frac{1}{2}}^{(i)} \right\rangle = 0$$

3. Update nodal coordinates:

$$\mathbf{x}_{n+1}^{(i+1)} - \mathbf{x}_n - \Delta t \cdot \mathbf{v}_{n+\frac{1}{2}}^{(i+1)} = \mathbf{0}$$

4. Update deformation gradient, volume element, and spatial density.

5. Update element-centered material models.

Time Integration (continued)

6. Update nodal pressure field:

$$\left\langle \eta^h, p_{n+1}^{h(i+1)} \right\rangle - \left\langle \eta^h, p_{n+1}^{i+1} \right\rangle + \left\langle \text{grad} \eta^h, -\mathbf{u}'_{n+\frac{1}{2}}^{(i+1)} \right\rangle = 0$$

7. Update element-centered fine scale fields:

$$\mathbf{v}' := -\frac{\tau}{\rho_{n+\frac{1}{2}}^{(i+1)}} \left[\rho_{n+\frac{1}{2}}^{(i+1)} \left(\mathbf{v}_{n+1}^{(i+1)} - \mathbf{v}_n \right) \Delta t^{-1} + \text{grad} p_{n+\frac{1}{2}}^{h(i+1)} \right]$$

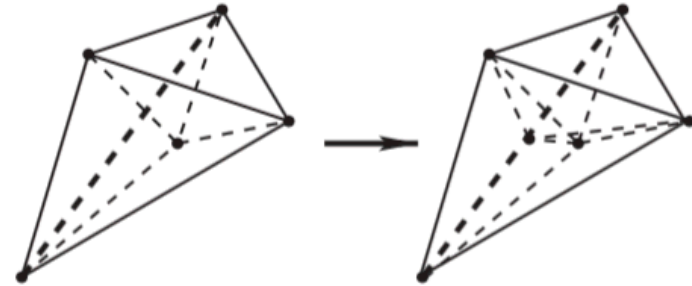
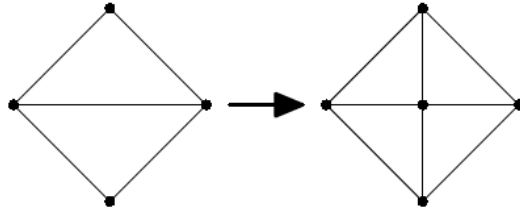
$$\mathbf{u}'_{n+1}{}^{(i+1)} = \mathbf{u}'_n + \left[\rho_{n+\frac{1}{2}}^{(i+1)} c_{n+\frac{1}{2}}^{(i+1)2} \right] (\mathbf{v}' \Delta t)$$

}

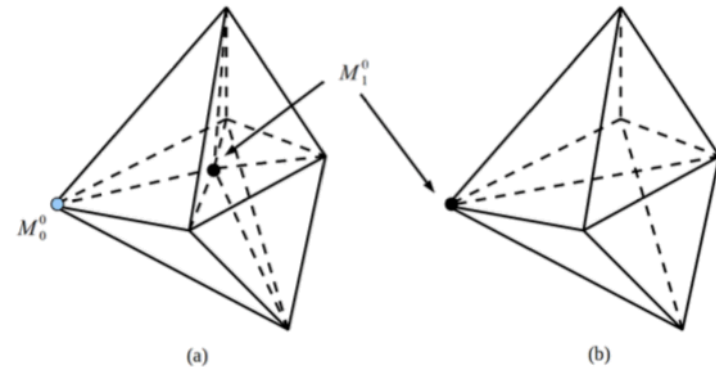
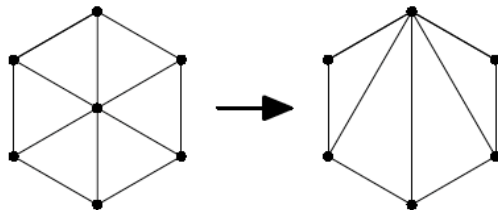
The sequence of steps here is explicitly designed to discretely conserve total energy.

Local Cavity Modifications

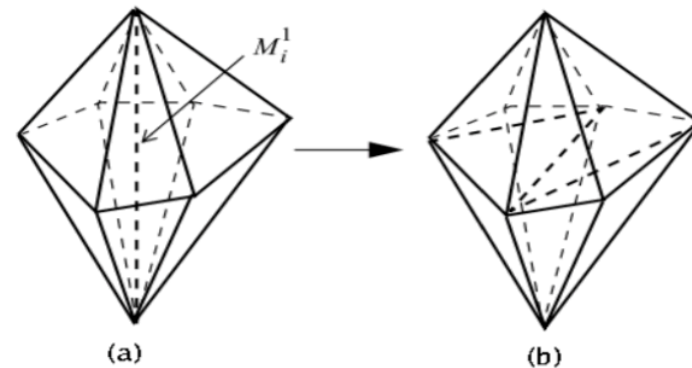
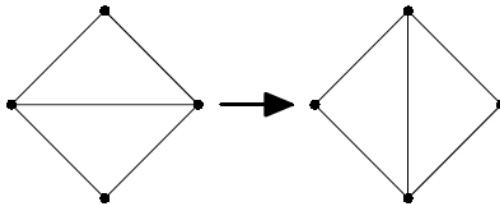
- Split



- Collapse



- Swap



Metric Tensor Field

- Symmetric Positive Definite tensor

$$\mathcal{M} = R^T \Lambda R, R^T R = I, \Lambda = \text{diag}(\lambda_1, \dots, \lambda_d), \forall i \in [1, d] : \lambda_i > 0$$

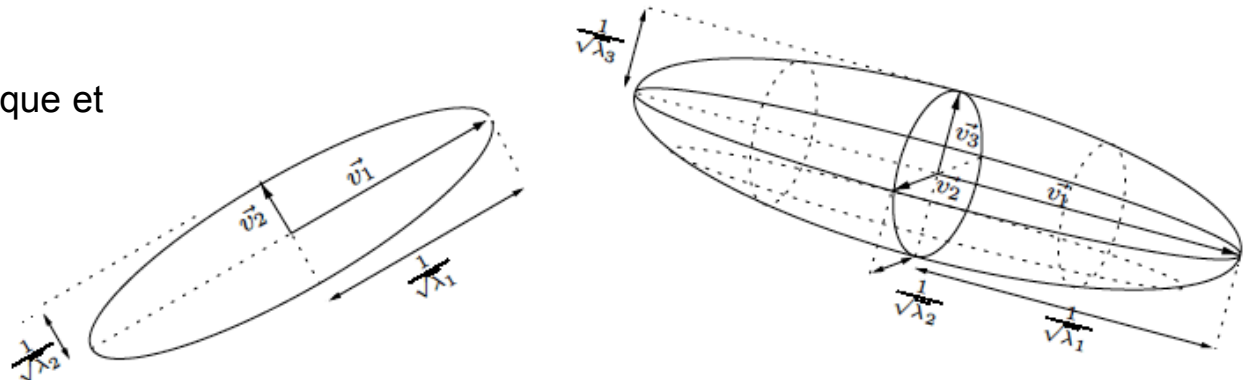
- Exist linear transform(s) from real space to “metric space”

$$Q = \Lambda^{\frac{1}{2}} R, \Lambda^{\frac{1}{2}} = \text{diag}(\sqrt{\lambda_1}, \dots, \sqrt{\lambda_d})$$

- Defines an inner product, transform-then-dot

$$\mathbf{u}^T \mathcal{M} \mathbf{v} = \mathbf{u}^T R^T \Lambda R \mathbf{v} = \mathbf{u}^T R^T \Lambda^{\frac{1}{2}} \Lambda^{\frac{1}{2}} R \mathbf{v} = \mathbf{u}^T Q^T Q \mathbf{v} = (Q \mathbf{u})^T (Q \mathbf{v}) = \tilde{\mathbf{u}}^T \tilde{\mathbf{v}}$$

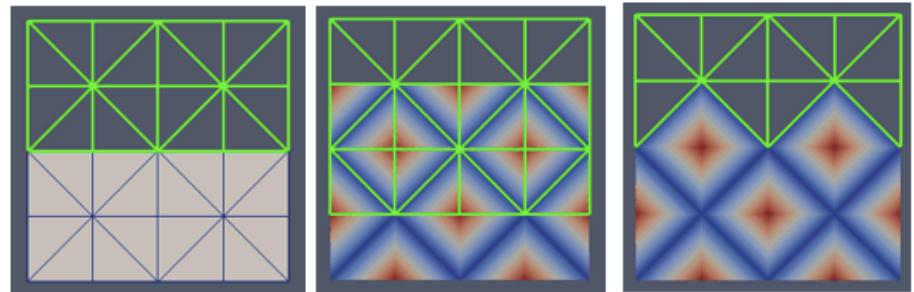
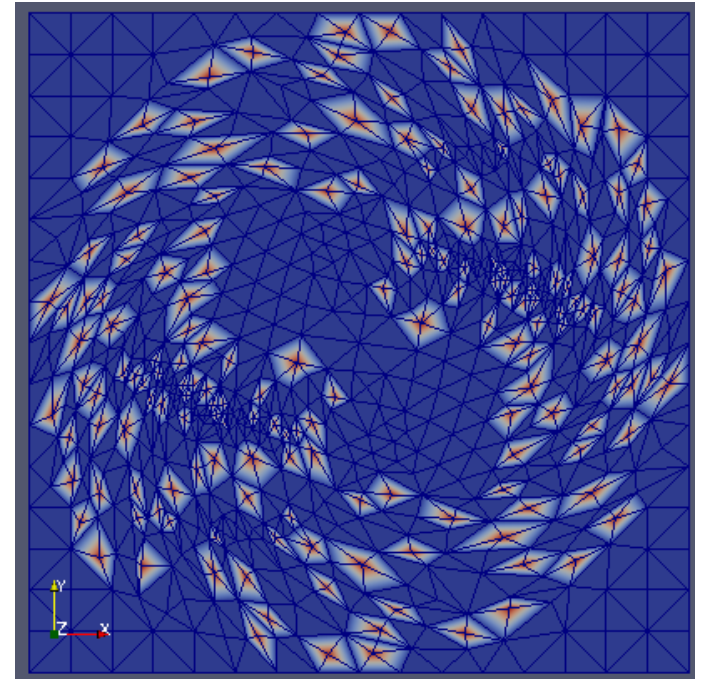
- Defines an ellipsoid of desired resolution in each direction



F. Alauzet and P. Frey
Estimateur d'erreur géométrique et
métriques anisotropes pour
l'adaptation de maillage.
Partie I : aspects théoriques

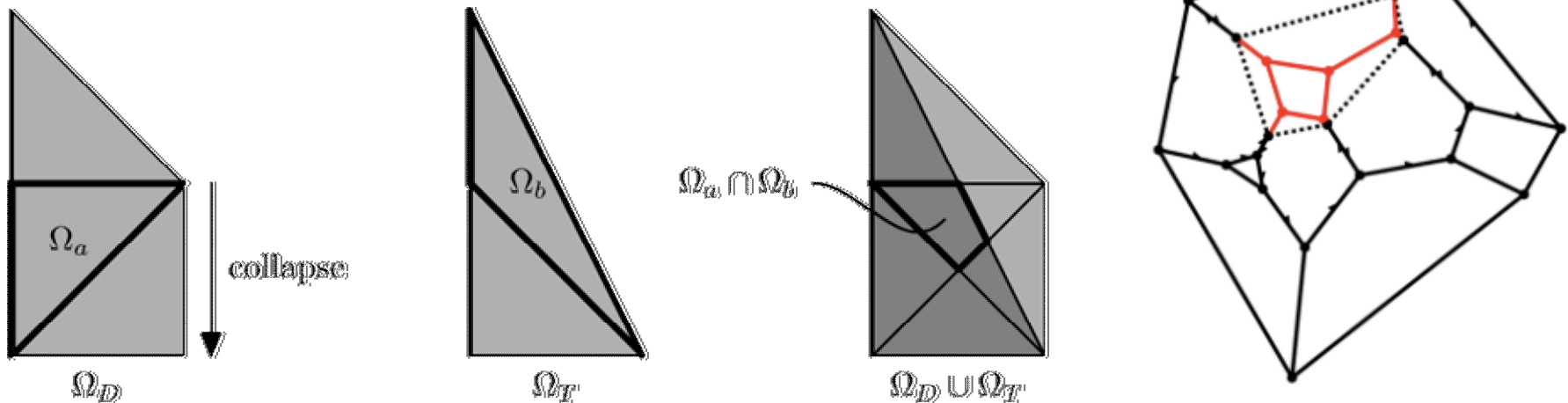
One Round of Changes

- All of the same kind
- Non-overlapping (independent set)
- Runs in parallel with minimal and scalable communication
- Construct new mesh from old mesh
- Selection and modification are fully deterministic
- Serial-parallel consistent!



Conserved cell-average quantities

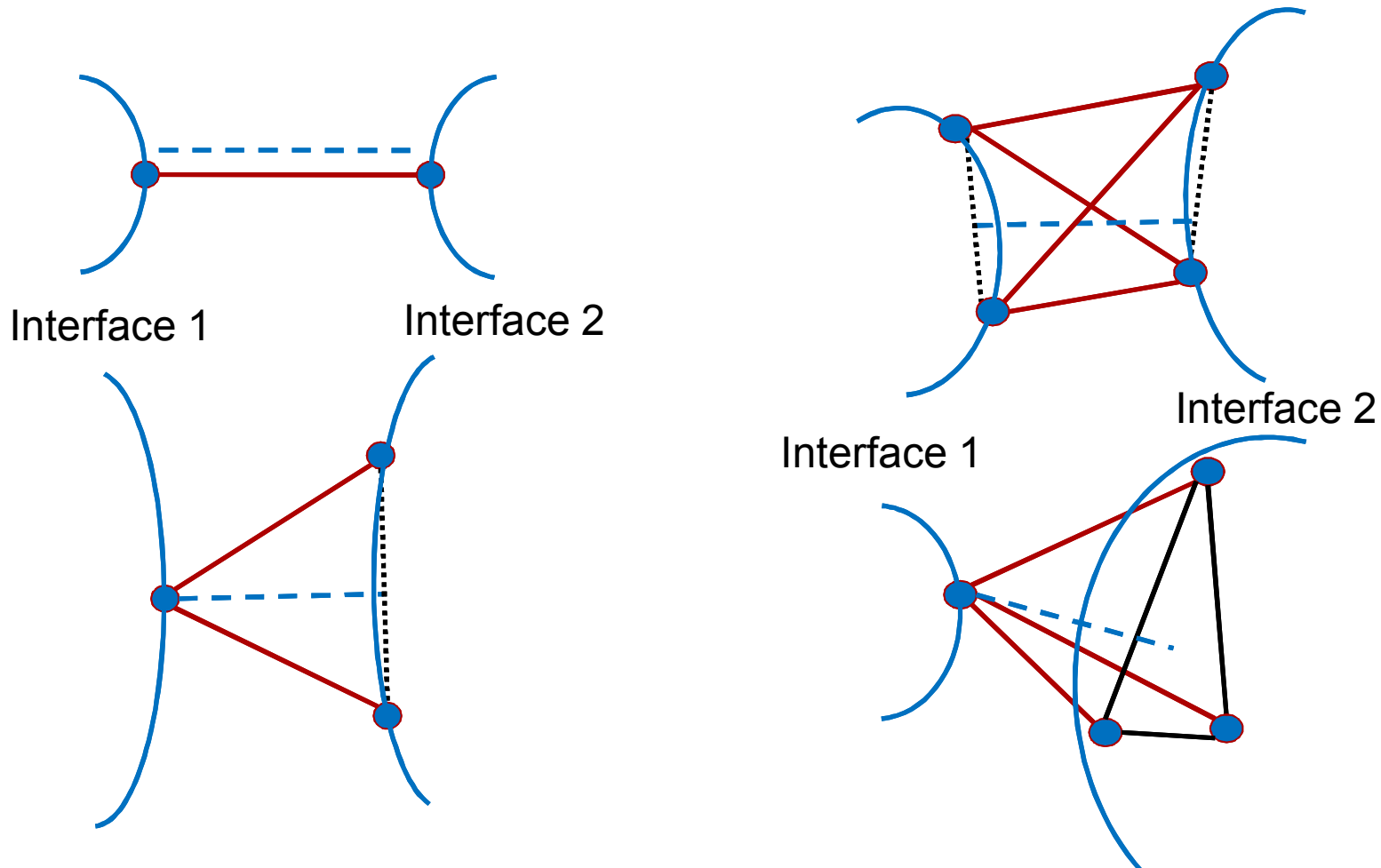
- For refinement, simply divide by two, assign to child cells
- Use R3D-based intersection remap on interior cavities
 - Conservative and bounds-perserving
- For curved boundary collapses, keep same density, record conservation error in “error field”



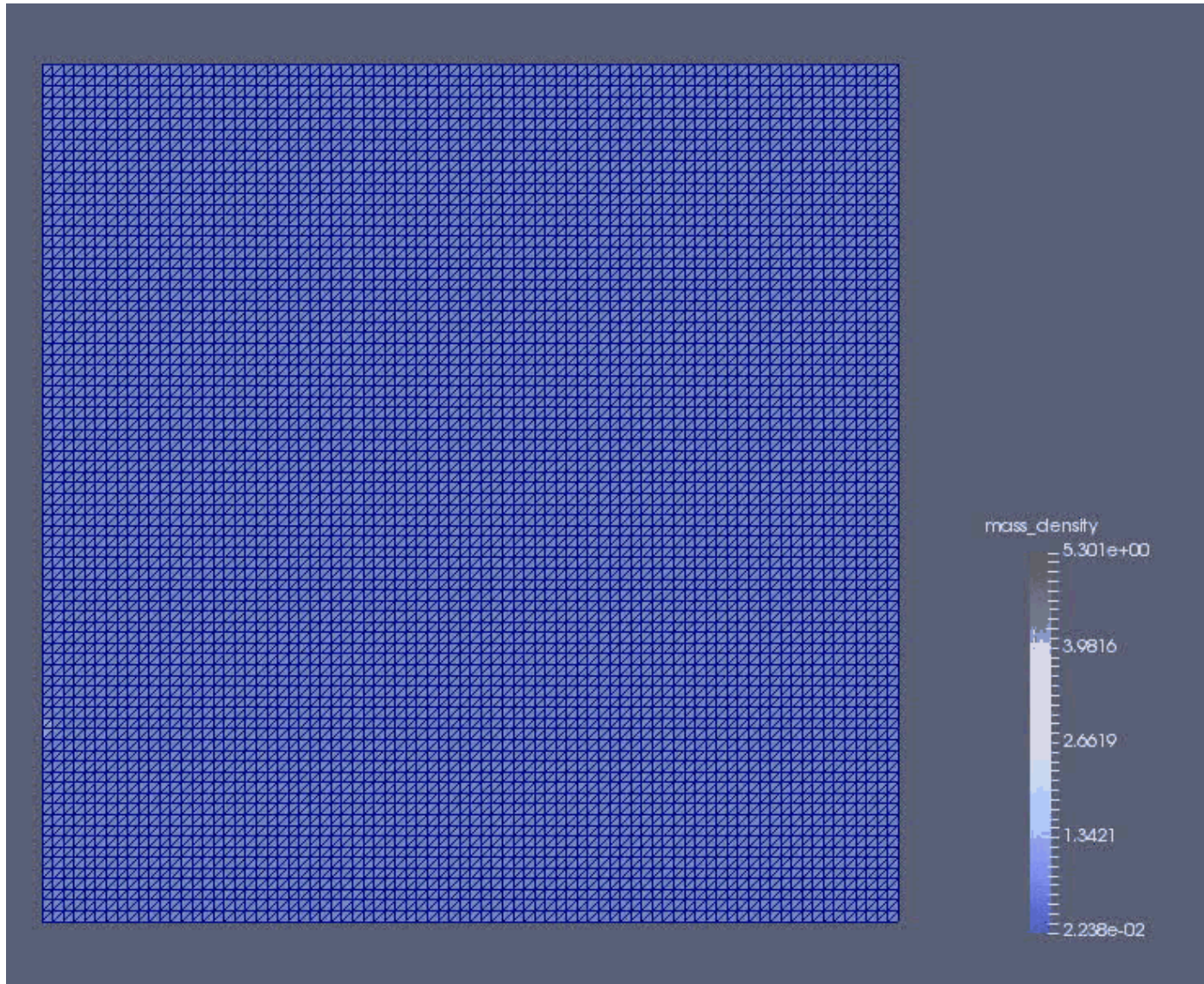
[LA-UR-15-26964](#)

Two-Interface Proximity Detection

- Measure shortest distance across single elements

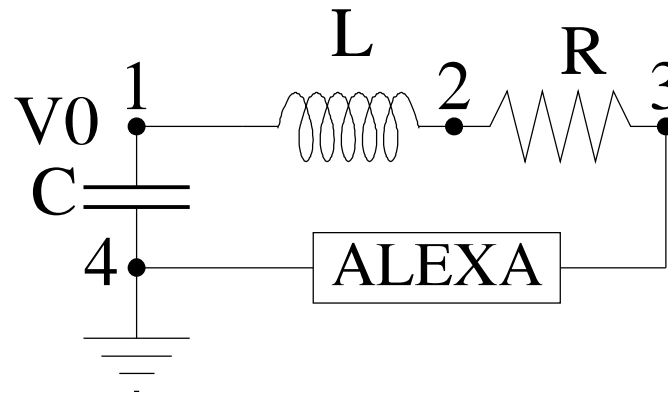


Airblast



Low-Rm MHD (Joule Heating)

- We model a circuit with Joule heating connected to our mesh.
- We allow an RLC circuit, and a scalar conductivity σ .



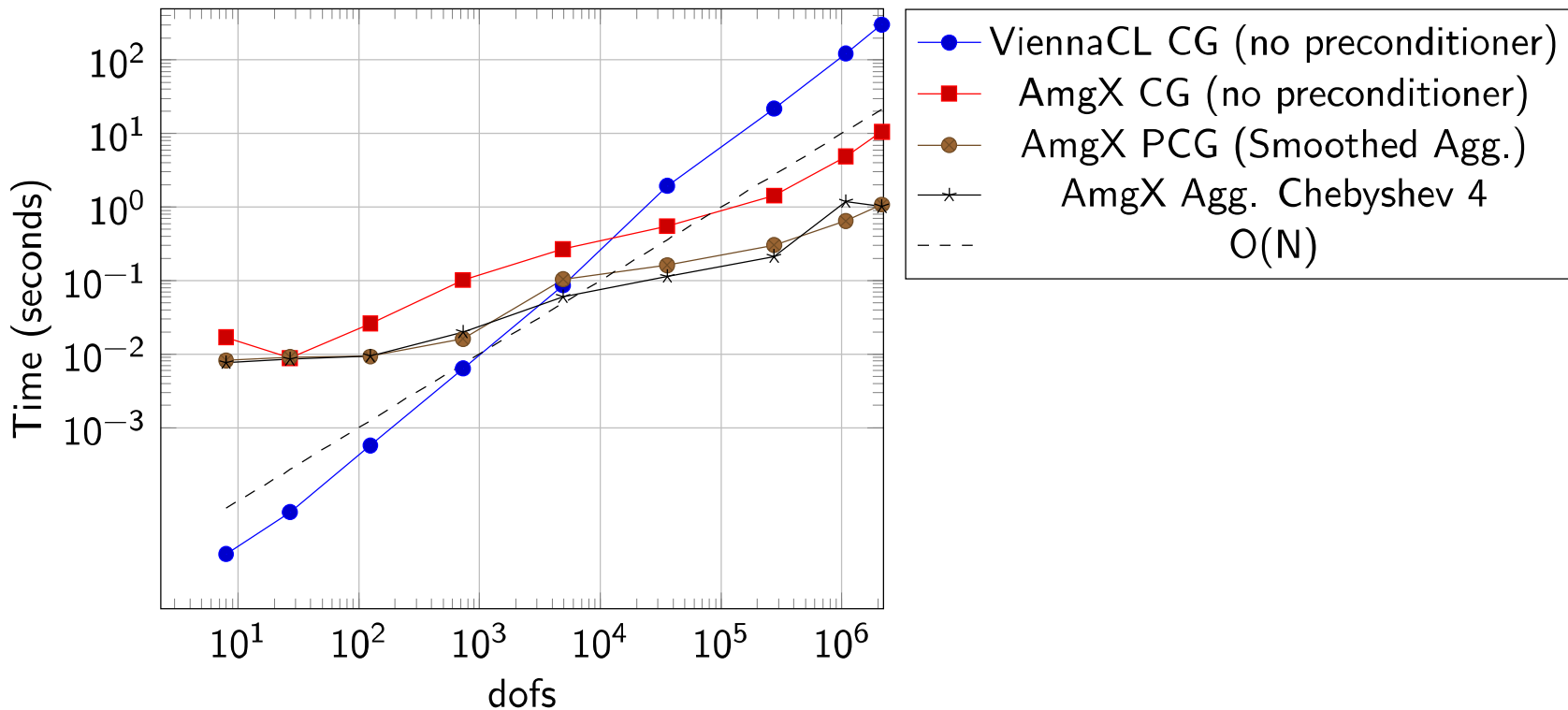
- Computationally intensive part of this is the Poisson solve:

$$(\nabla\phi, \sigma\nabla v)_{\Omega} = (f, v)_{\Omega} \quad \forall v$$

To gauge performance on a problem that approximates the physics of interest, we use a high-contrast $\sigma = (10^6 - 1)x^2 + 1$ and solve on $\Omega = [0, 1]^3$. We use GPU-accelerated solvers a single NVIDIA P100.

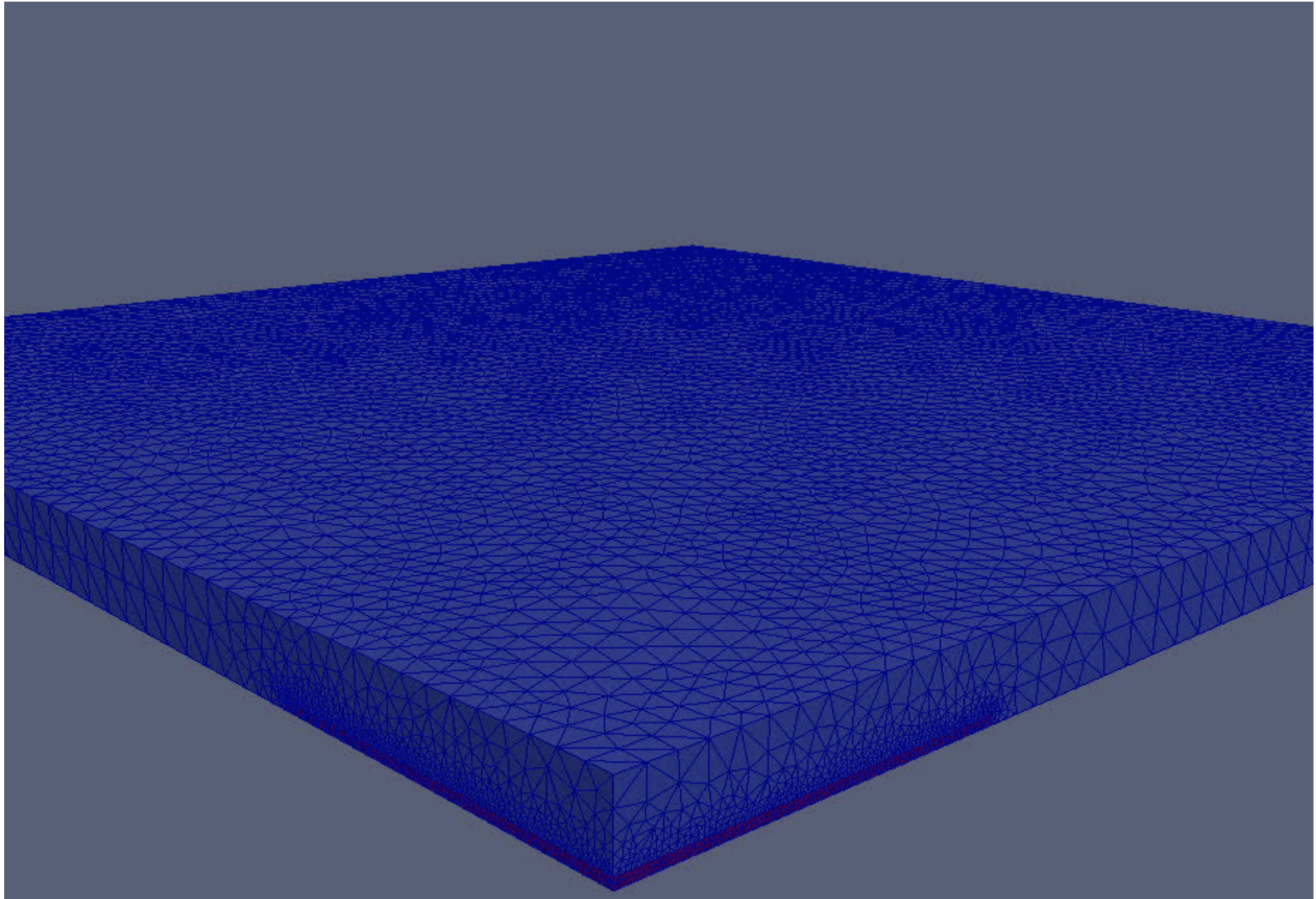
Higher-Contrast Poisson: Timings

White P100 3D FEM (higher-contrast Poisson), performance comparison



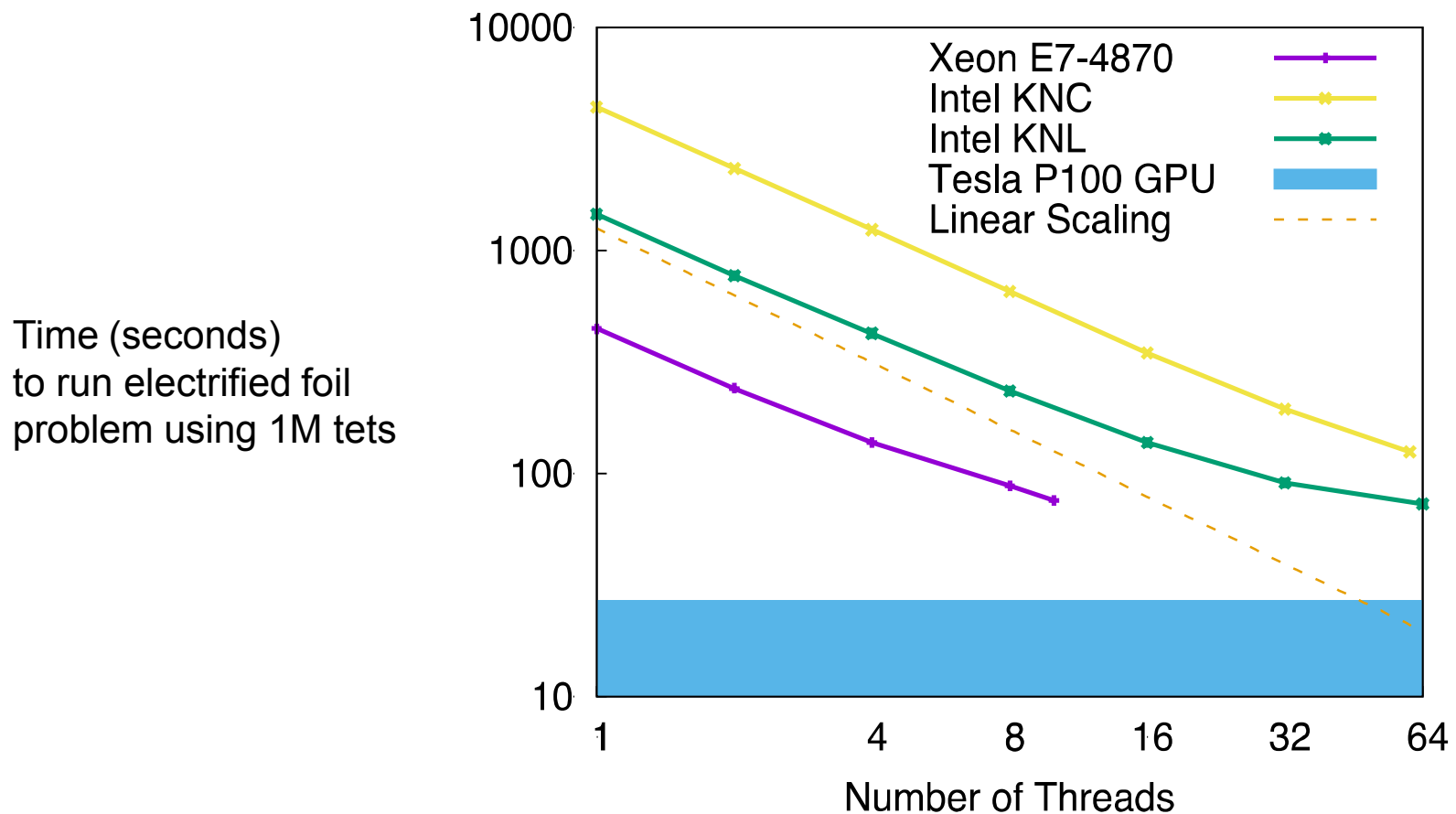
Convergence criterion: reduce residual by factor of 10^{-10} .

Electrified Foil



Performance Portability

- Kokkos is used for on-node parallelism
- Good performance across Intel Xeon Phi and NVIDIA cards



Thank You

... Questions ?

Glen Hansen

Dan Ibanez

Ed Love

James Overfelt,

Nate Roberts

Tom Voth