

Compatibility and Suitability of Existing Steel Pipelines for Transport of Hydrogen-Natural Gas Blends

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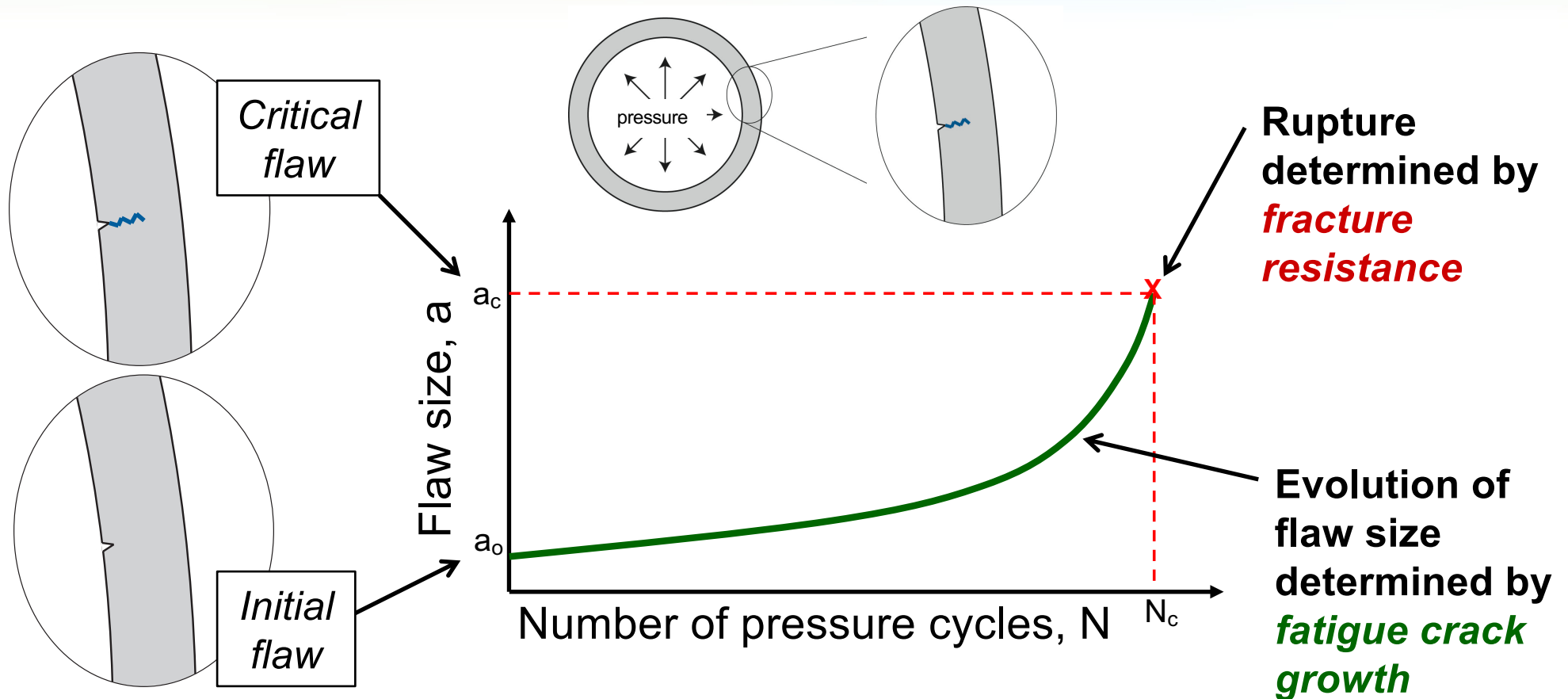
Sandia National Laboratories

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Outline

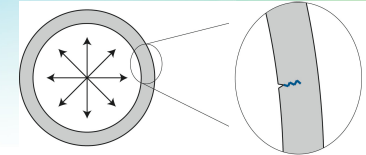
- **Overview of fracture mechanics based assessment**
- **Representative fatigue and fracture data measured in hydrogen**
- **Example life calculations based on idealized cracks**

Fracture mechanics-based assessment of fatigue and fracture hydrogen pipelines

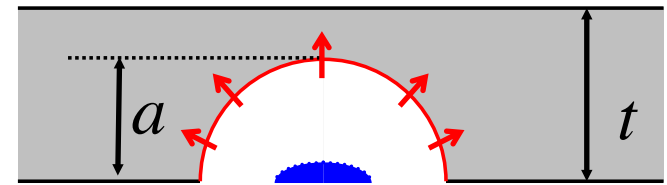


ASME B31.12 describes rules for hydrogen pipelines with reference to ASME BPVC Section VIII, Division 3, Article KD-10

Crack growth through the thickness of the pipeline driven by hoop stress



- Initial flaw grows due to pressure cycle
- Driving force is characterized by ΔK

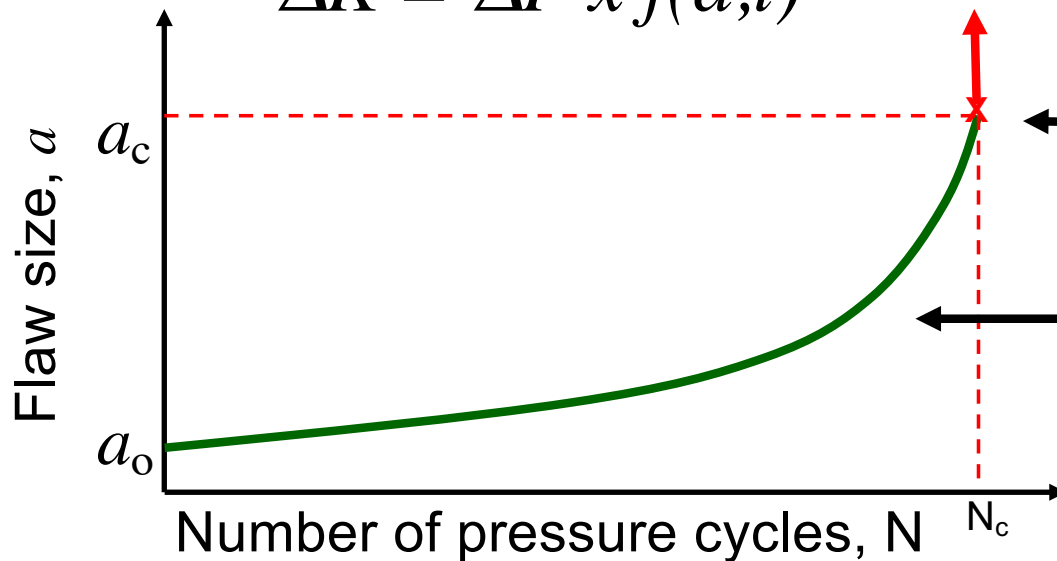


Initial flaw

a = depth of crack

t = wall thickness

$$\Delta K = \Delta P \times f(a,t)$$



$$K_{IH} = P \times f(a_c, t)$$

$$a = a_i + \left(\frac{da}{dN} \right)^{a=a_i} \Delta N$$

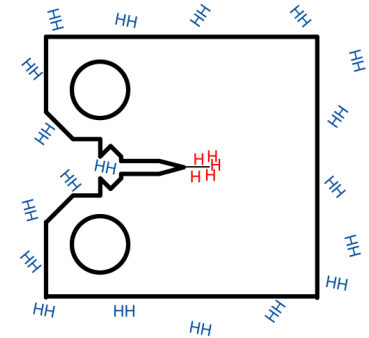
$$\frac{da}{dN} = C \Delta K^m$$

Fracture mechanics parameters must be measured in relevant hydrogen environments

Fatigue crack growth

Characterized by $da/dN = f(\Delta K)$

Typical fatigue crack growth methodology described in ASTM E647



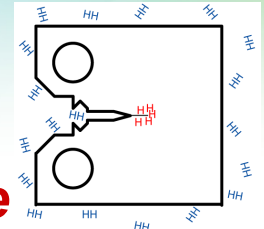
Fracture resistance

Characterized by K_{IC} or in hydrogen K_{IH}

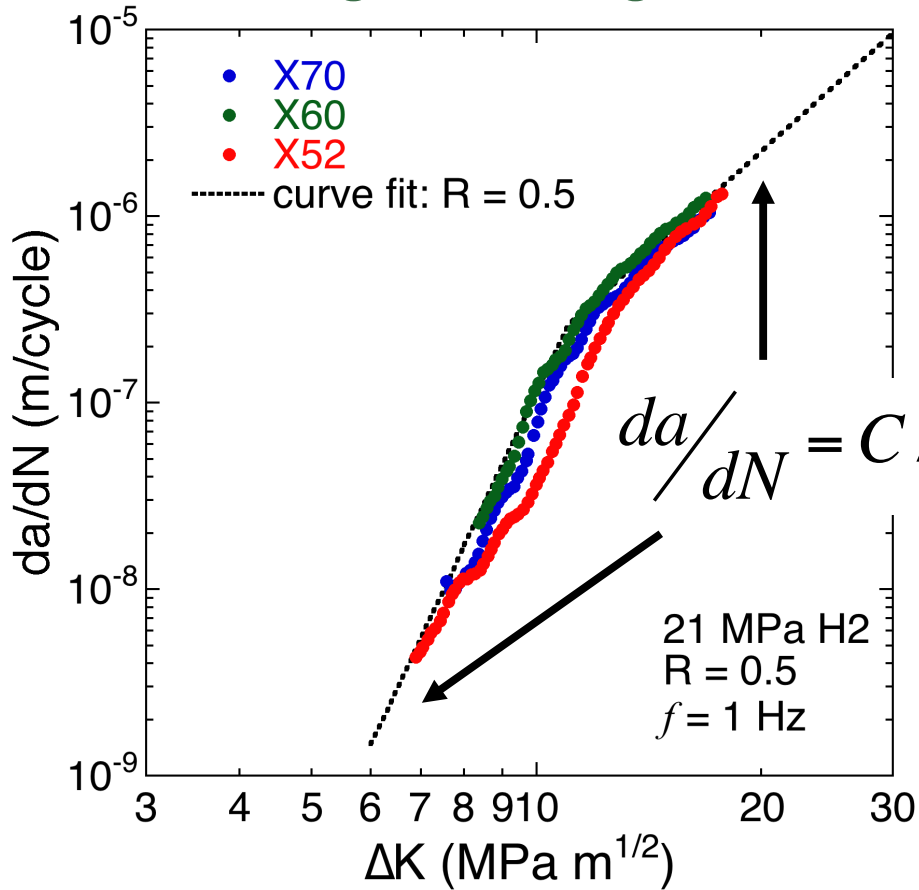
Elastic-plastic methods are generally needed (ASTM E1820), K_{IH} is calculated from these methods

CSA CHMC1 describes requirements for mechanical testing in high-pressure gaseous hydrogen environments, referencing standard fatigue and fracture methods (e.g., ASTM)

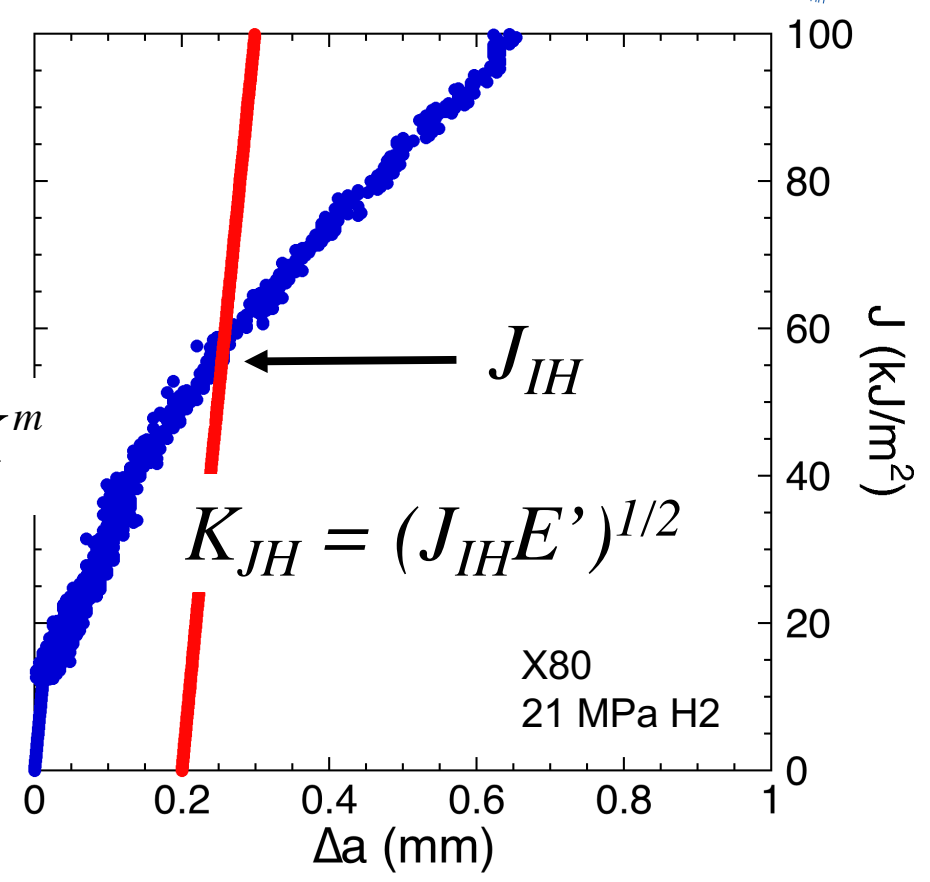
Fracture mechanics measurements can be made in gaseous hydrogen



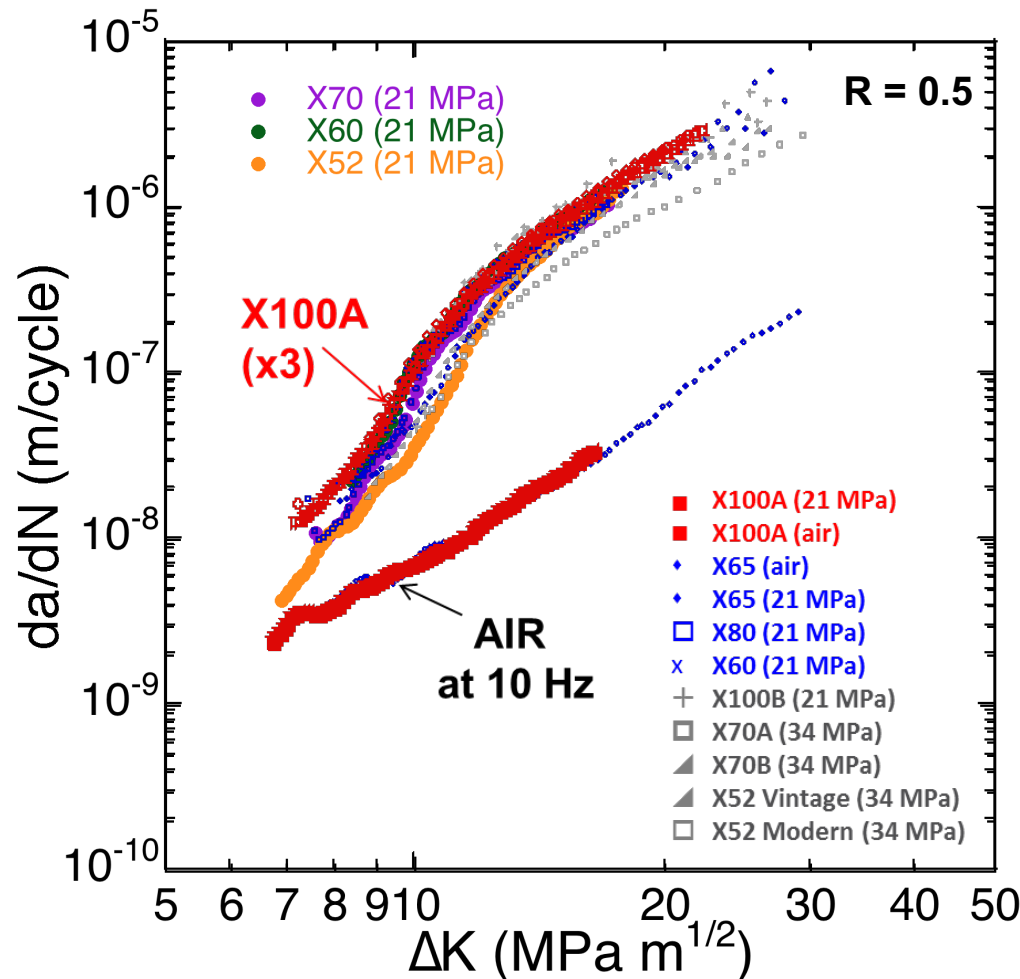
Fatigue crack growth



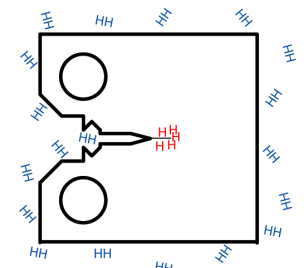
Fracture resistance



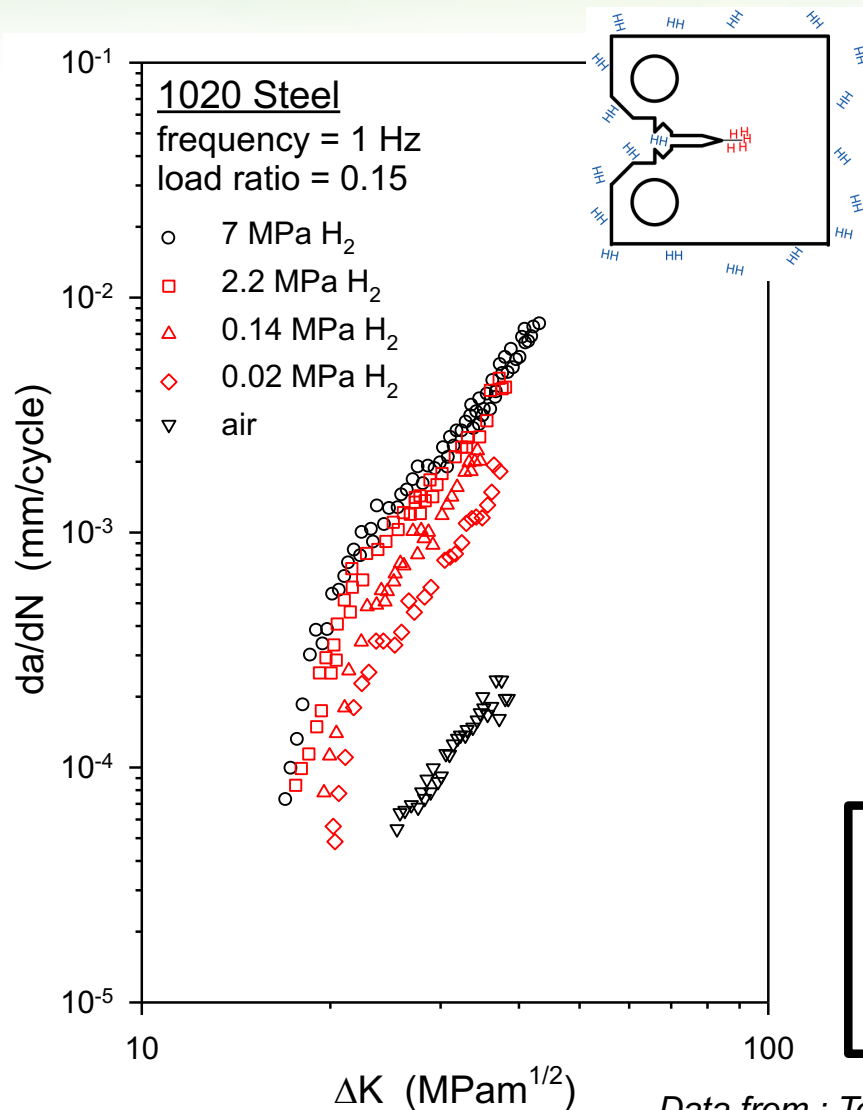
Low strength steels tend to show very similar fatigue crack growth rates in gaseous hydrogen



- A wide variety of pipeline steels display nominally the same fatigue response in high-pressure gaseous hydrogen
- The effect of pressure on fatigue crack growth rates is modest for high-pressure hydrogen



Low pressure hydrogen can have significant effects on fatigue crack growth rates

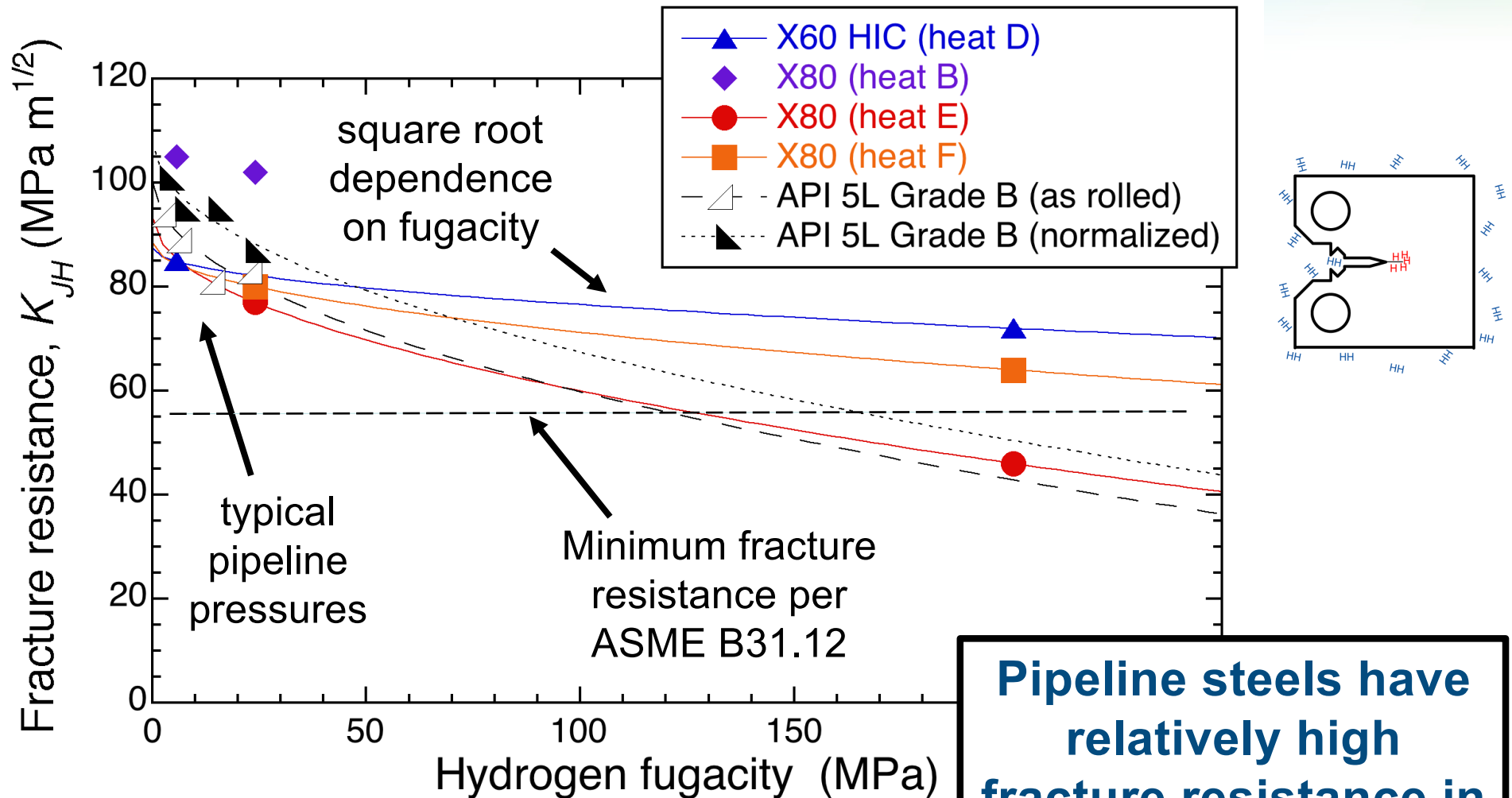


- Sub-atmospheric pressure of hydrogen (<0.1MPa) can have substantial effect on fatigue crack growth rates for carbon steels
- The effect of pressure on fatigue is generally within the scatter for pressure greater than about 2 MPa

Low partial pressure of hydrogen has nominally same effect as pure hydrogen on pipeline steels

Data from : *Technical Reference on Hydrogen Compatibility of Materials*, Sandia, 2008

Fracture resistance in gaseous hydrogen depends on pressure (unlike fatigue)

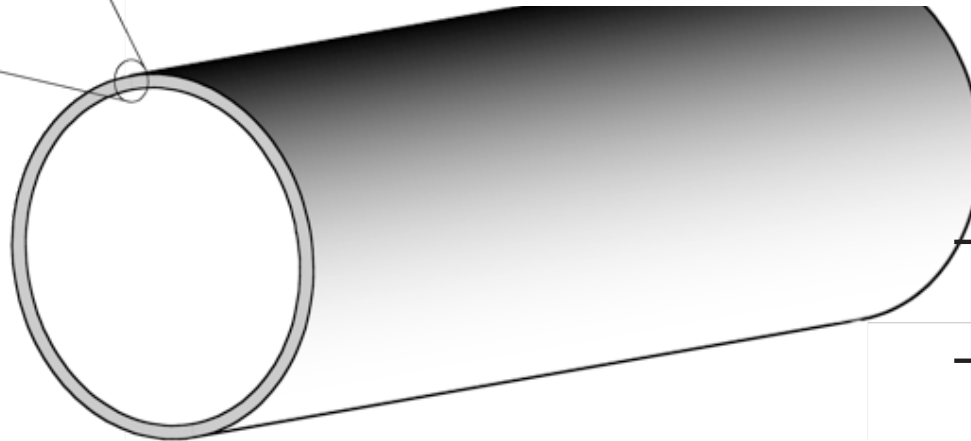
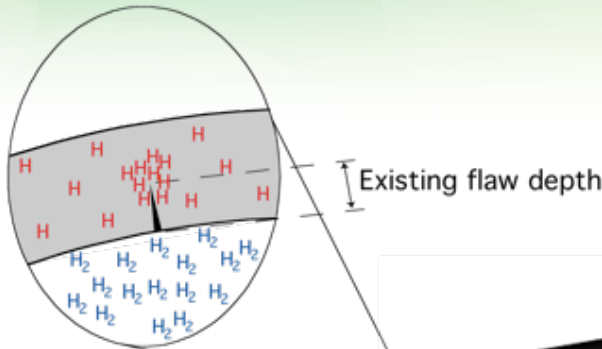


Data from : *Technical Reference on Hydrogen Compatibility of Materials*, Sandia, 2008

Consider a typical “high-pressure” pipeline

Material: X70
 TS = 586 MPa
 YS = 500 MPa

OD = 762 mm
 t = 15.9 mm
 P_{max} = 7 MPa
 P_{min} = 4 MPa



Semi-elliptical crack

thickness (t)

inside surface

$$2c = 3a$$

a

semi-elliptical

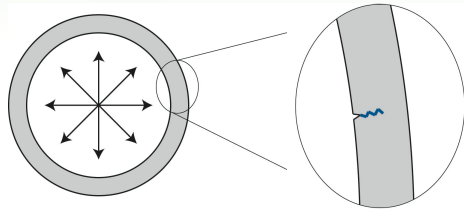
a/t = crack depth

$a/2c$ = depth to length ratio

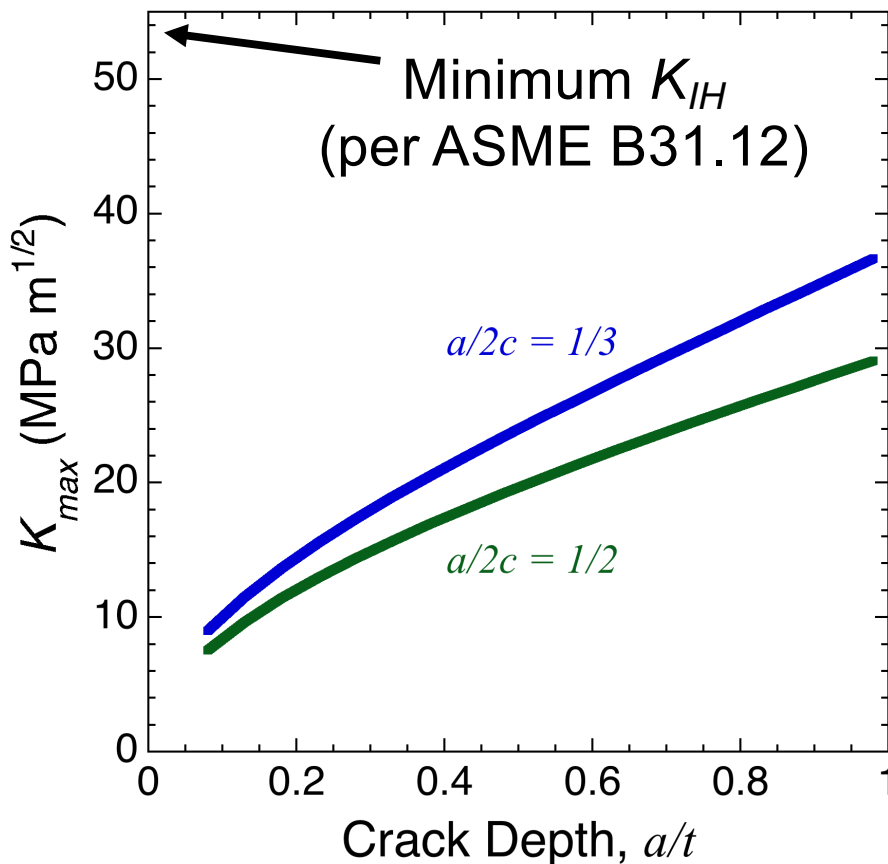
natural crack shape: $a/2c = 1/2$

ASME crack shape: $a/2c = 1/3$

Stress intensity associated with semi-elliptical crack in “high-pressure” pipeline

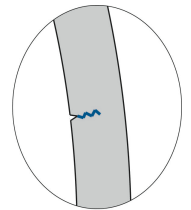


Hoop stress at $P_{max} = 162$ MPa
 stress ratio: hoop/TS = 28%



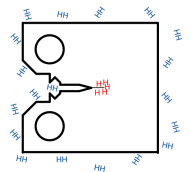
Driving force on semi-elliptical crack:

$$K_{max} < 40 \text{ MPa m}^{1/2}$$



Typical pipeline material fracture resistance:

$$K_{JH} > 75 \text{ MPa m}^{1/2}$$



Fracture resistance of pipeline steels in H₂ is greater than driving force on semi-elliptical cracks

Fatigue crack growth relationships for pipeline materials in gaseous hydrogen

$$P_{max} = 7 \text{ MPa} \ \& \ P_{min} = 4 \text{ MPa}$$

$$R = 0.57$$

For $a/t = 30\%$ & $a/2c = 1/3$

$$\Delta K \sim 7.7 \text{ MPa m}^{1/2}$$

For $a/t = 40\%$ & $a/2c = 1/2$

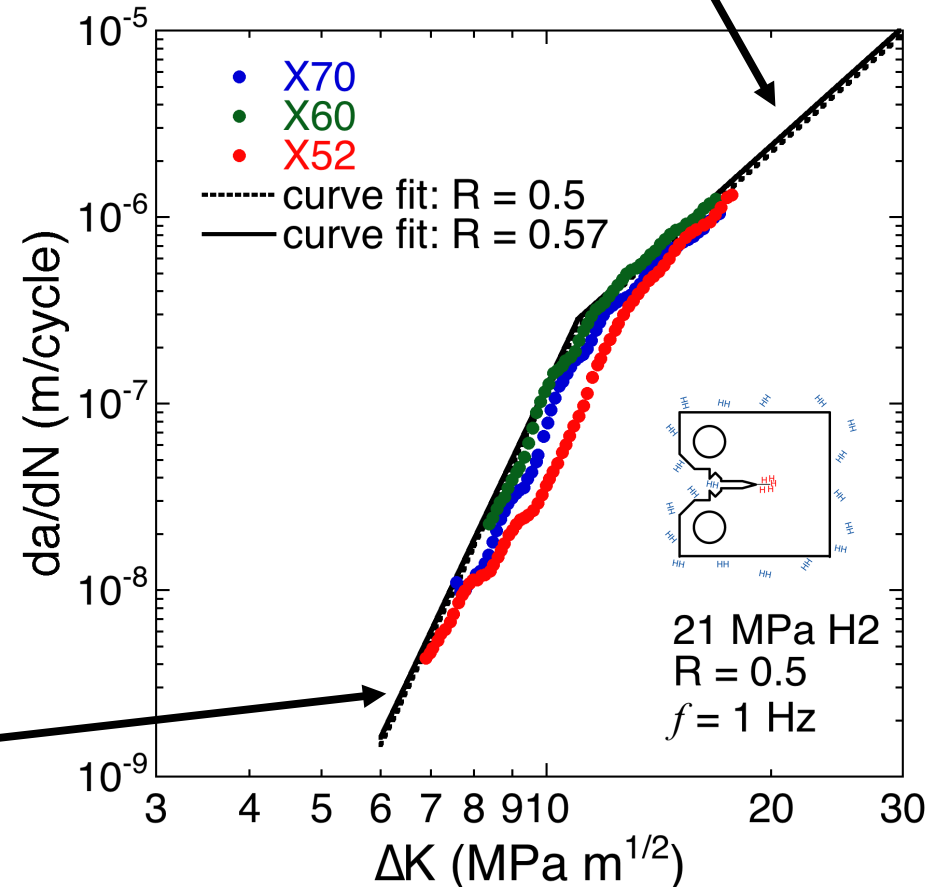
$$\Delta K \sim 7.5 \text{ MPa m}^{1/2}$$

For $6 < \Delta K < 11 \text{ MPa m}^{1/2}$

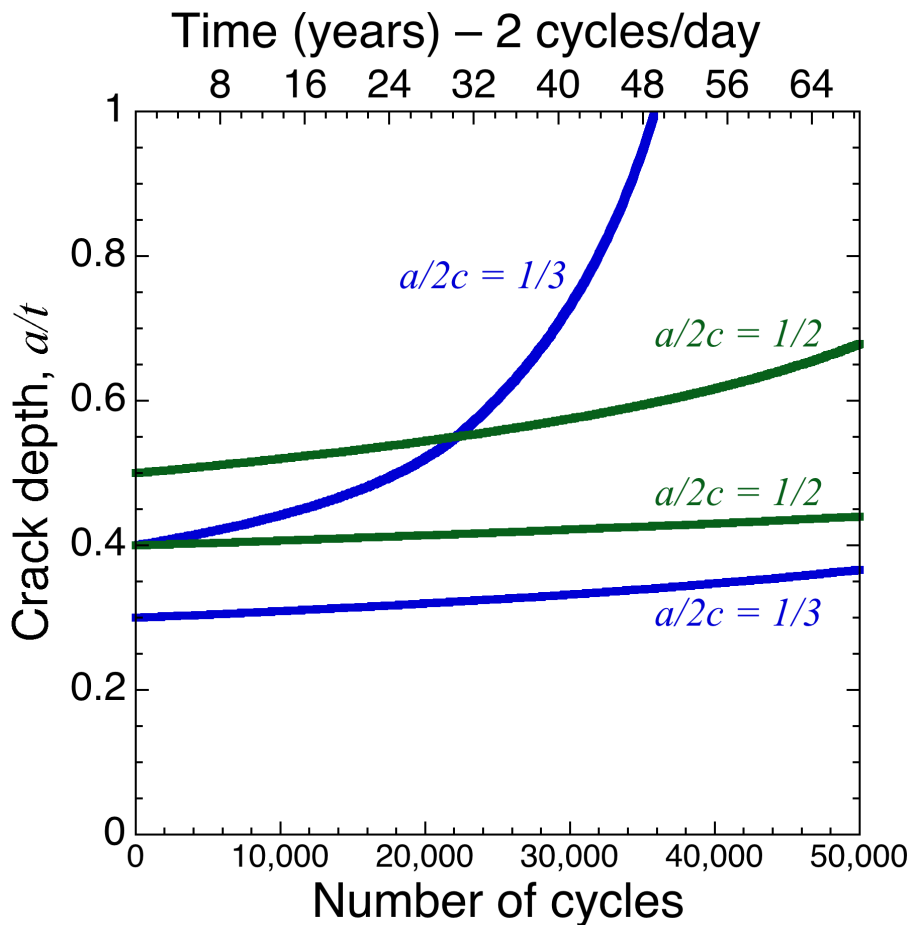
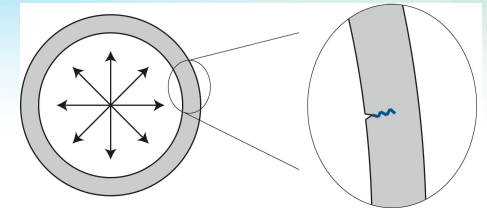
$$da/dN \text{ (m/cycle)} = 3.9 \times 10^{-16} \Delta K^{8.5}$$

For $\Delta K \geq 11 \text{ MPa m}^{1/2}$

$$da/dN \text{ (m/cycle)} = 5 \times 10^{-11} \Delta K^{3.6}$$



Predicted lifetime of pipeline with growing fatigue cracks in hydrogen



Assuming

- Pressure cycles between 4 & 7 MPa
- Constant crack shape ($a/2c$)
- Large initial defects
- Fatigue crack growth rates in pure H₂ (at higher pressure)

Using:
$$a = a_i + \left(\frac{da}{dN} \right)^{a=a_i} \Delta N$$

- 10,000s of cycles are needed to extend the crack significantly
- At 2 cycles per day, decades are needed to advance the crack

Summary

- Fatigue crack rates of pipeline steels are independent of hydrogen partial pressure to first order
 - *H₂-NG mixtures have same effect as pure hydrogen*
- Fracture resistance, on the other hand, is sensitive to pressure – but remains relatively high at high pressure
- For conditions of typical pipeline operating with large daily pressure swings ($P_{\max} = 7$ MPa; $P_{\min} = 4$ MPa):
 - Large defects (30-40% wall thickness) show only modest fatigue-induced extension on time scale of decade
 - Stress intensity factor for through wall cracks can be less than fracture resistance measured in hydrogen
 - *Hydrogen does not induce rupture of pipeline*
 - Details, of course, depend on specifics of geometry

