

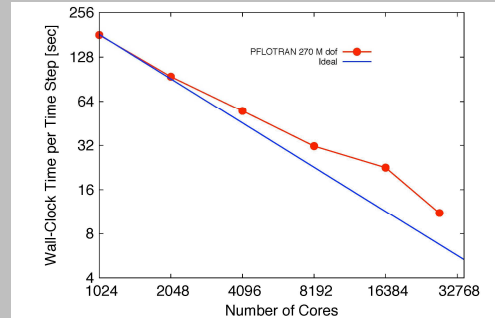
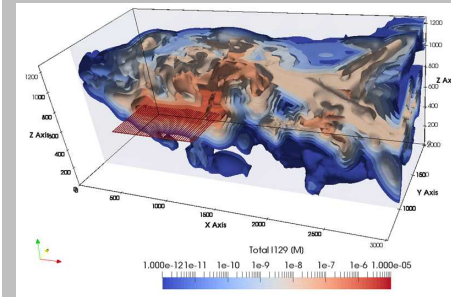
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$$\frac{\partial m_a}{\partial t} = -\nabla \cdot (\rho_l X_a^l \mathbf{q}_l + \rho_g X_a^g \mathbf{q}_g + \mathbf{J}_a^l + \mathbf{J}_a^g) + q_a^G,$$

$$\frac{\partial m_w}{\partial t} = -\nabla \cdot (\rho_l X_w^l \mathbf{q}_l + \rho_g X_w^g \mathbf{q}_g + \mathbf{J}_w^l + \mathbf{J}_w^g) + q_w^G,$$

$$\frac{\partial e}{\partial t} = -\nabla \cdot (\rho_l H_l \mathbf{q}_l + \rho_g H_g \mathbf{q}_g - \kappa_{\text{eff}} \nabla T) + q_e^G,$$



# PFLOTRAN Overview

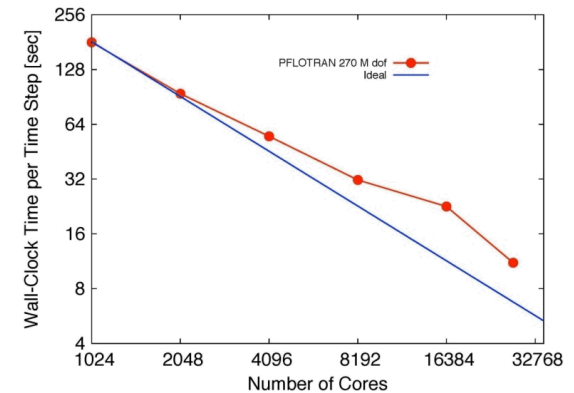
for the French National Radioactive Waste Management Agency

Glenn E. Hammond

September 19, 2017

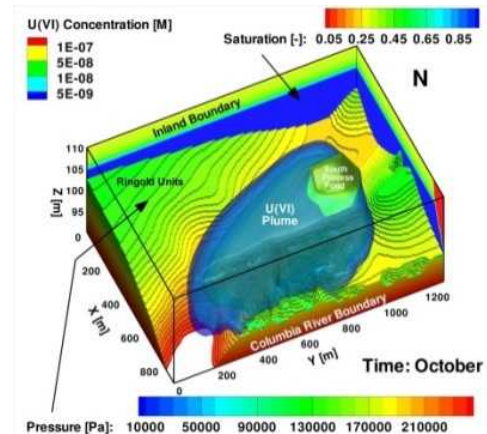
# PFLOTRAN

- **Petascale** reactive multiphase flow and transport code
- **Open source** license (GNU LGPL 2.0)
- **Object-oriented** Fortran 2003/2008
  - Pointers to procedures
  - Classes (extendable derived types with member procedures)
- Founded upon well-known (**supported**) open source libraries
  - MPI, PETSc, HDF5, METIS/ParMETIS/CMAKE
- Demonstrated performance
  - Maximum # processes: 262,144 (Jaguar supercomputer)
  - Maximum problem size: 3.34 billion degrees of freedom
  - **Scales well to over 10K cores**



# Application of PFLOTRAN

- Nuclear waste disposal
  - Waste Isolation Pilot Plant (WIPP) in Carlsbad, NM
  - DOE Used Fuel Disposition Program
  - SKB Forsmark Spent Fuel Nuclear Waste Repository (Sweden, Amphos<sup>21</sup>)
- Climate: coupled overland/groundwater flow; CLM
  - Next Generation Ecosystem Experiments (NGEE) Arctic
  - DOE Earth System Modeling (ESM) Program
- Biogeochemical transport modeling
  - U(VI) fate and transport at Hanford 300 Area
  - Hyporheic zone biogeochemical cycling
    - Columbia River, WA, USA
    - East River, CO, USA
- CO<sub>2</sub> sequestration
- Enhanced geothermal energy
- Radioisotope tracers
- Colloid-facilitated transport



Hammond and Lichtner, WRR, 2010

# Discretization and Numerical Methods

- Spatial discretization
  - Finite volume (2-point flux default)
  - Structured and unstructured grids
- Time discretization: fully-implicit backward Euler
- Nonlinear solver
  - Newton-Raphson
  - Line search/damping with custom convergence criteria
- Linear solver: direct (LU) or iterative (BiCGStab)
- Multi-physics coupling
  - Flow and transport/reaction: sequential
  - Transport and reaction: global implicit
  - Geomechanics and flow/transport: sequential
  - Geophysics and flow/transport: sequential

Deep Borehole  
Waste Disposal

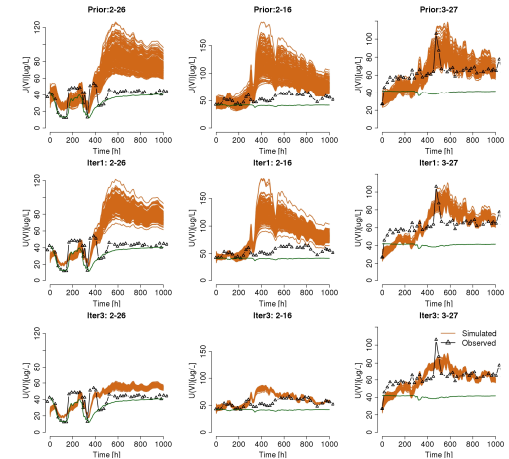


Emily Stein, SNL, 2015

# PFLOTRAN Computing Capability

- High-Performance Computing (HPC)
  - Increasingly mechanistic process models
  - Highly-refined 3D discretizations
  - Massive probabilistic runs
- Open Source Collaboration
  - Leverages a diverse scientific community
  - Sharing among subject matter experts and stakeholders from labs/universities
- Modern Fortran (2003/2008)
  - Domain scientists remain engaged
  - Modular framework for customization
- Leverages Existing Capabilities
  - Meshing, visualization, HPC solvers, etc.
  - Configuration management, testing, and QA

## Data Assimilation



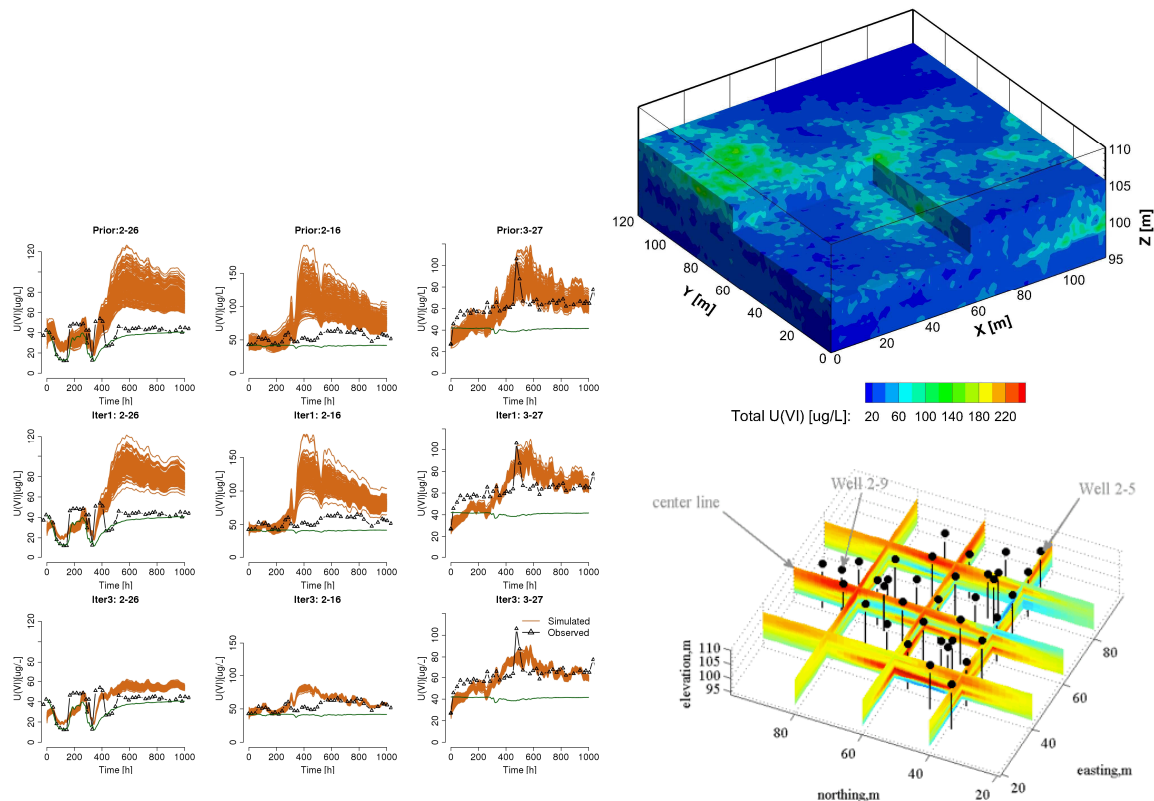
Xingyuan Chen, PNNL, 2011



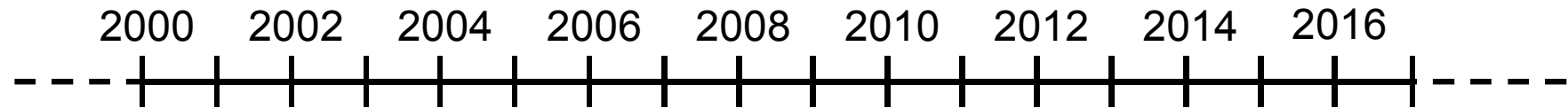
# Benefits of Massively Parallel HPC

## Data Assimilation at the Hanford 300 Area (Xingyuan Chen, 2011)

- Problem domain:
  - $120 \times 120 \times 15\text{m}$
  - $\Delta x, \Delta y, \Delta z = 1, 1, 0.5\text{ m}$
  - 432K grid cells
  - 15 chemical species
  - 6.48M dofs total
- 1-2 month simulation:
  - $\Delta t = 1\text{ hour}$
- Computing, e.g.
  - 128 cores  
(single realization)
  - 64,000 cores  
(500 realizations)
  - 1 hour wallclock runtime
  - ~7 cpu years



# PFLOTRAN Development Timeline



Peter Lichtner

Glenn Hammond

Richard Mills

Chuan Lu

Jitu Kumar

Gautam Bisht

Satish Karra

Ben Andre

Nate Collier

Heeho Park

Paolo Orsini

Jennifer Frederick

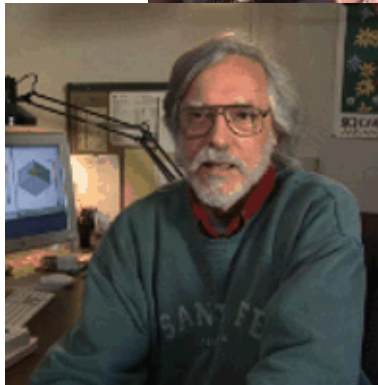
Ramesh Sarathi

*First release*

*SciDAC-funded rewrite*

*Process model refactor*

# PFLOTRAN Developers

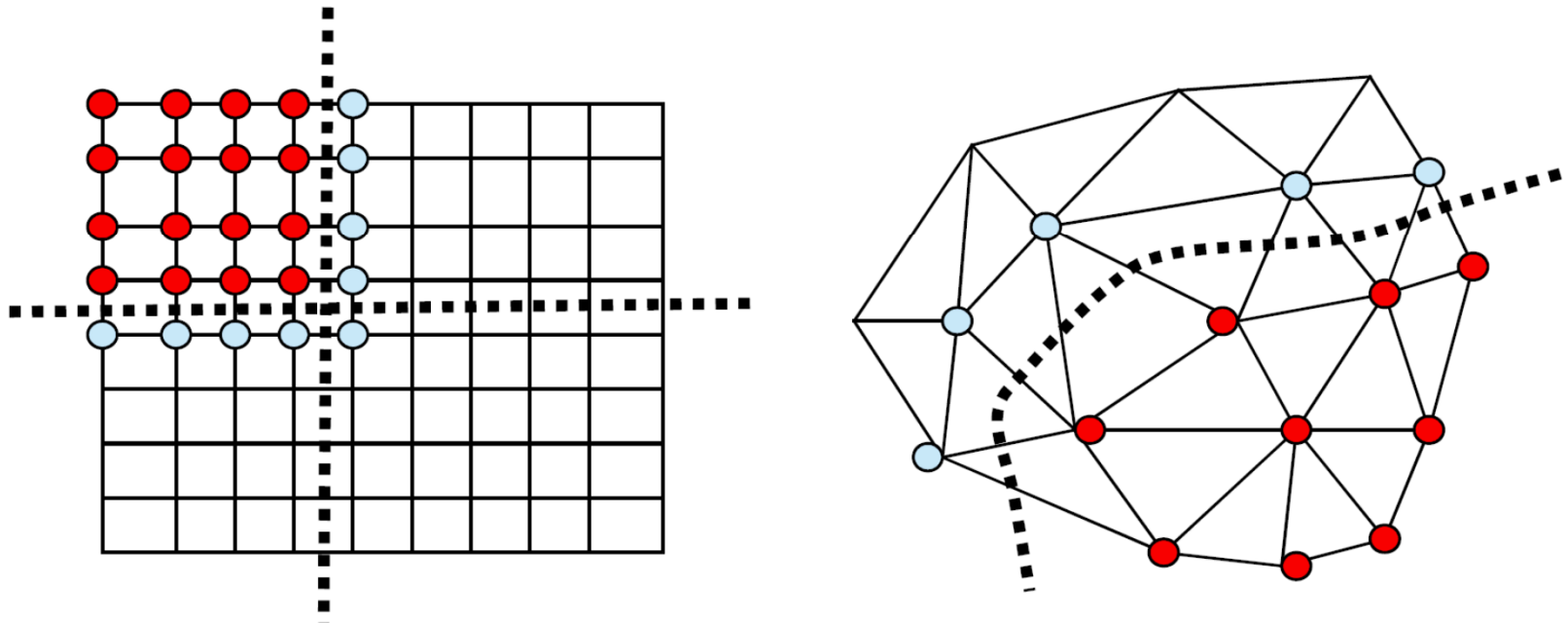


# Approach to Parallelization

## Domain Decomposition

● Local node

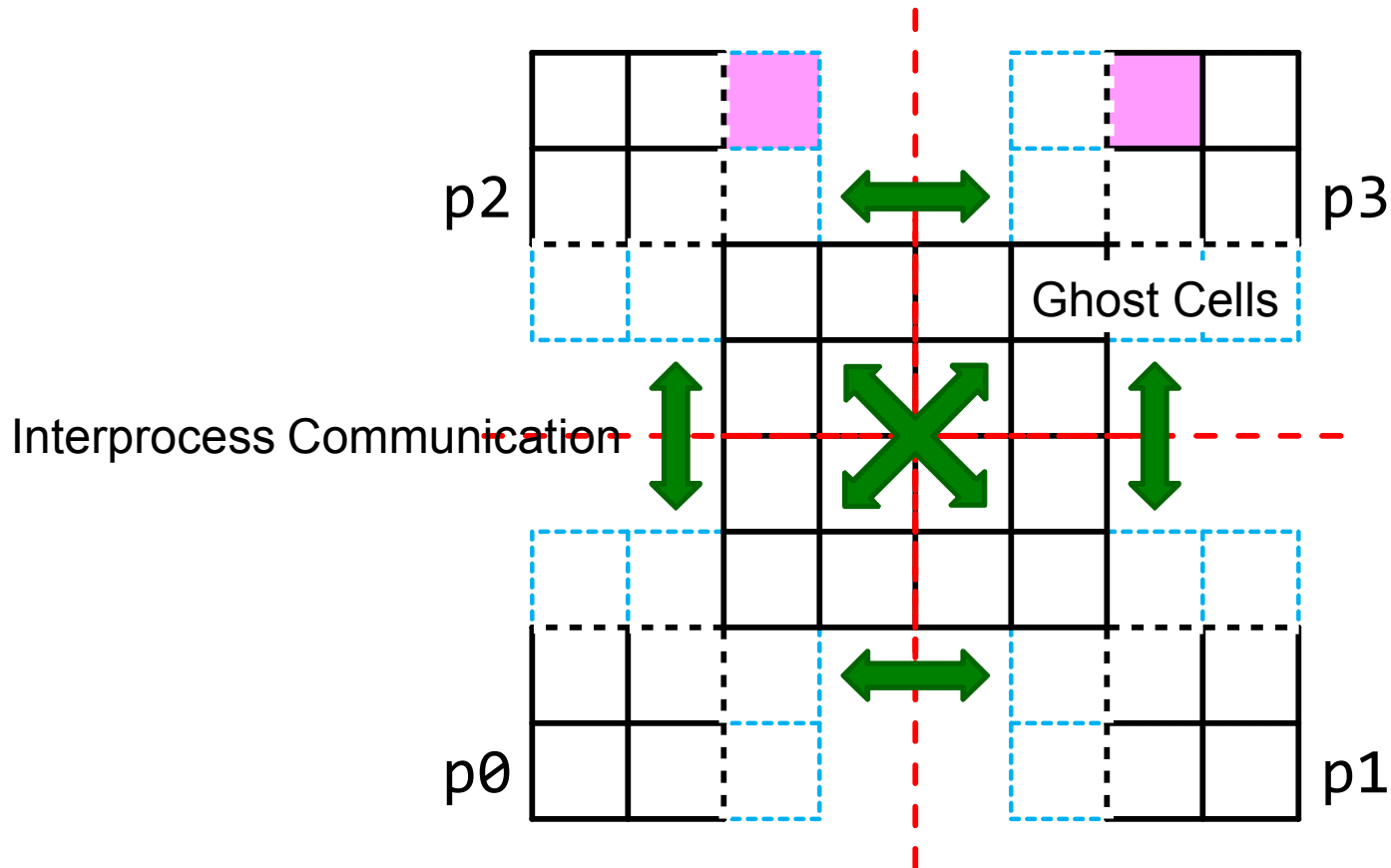
○ Ghost node



Ghost node information used only in flux calculations.

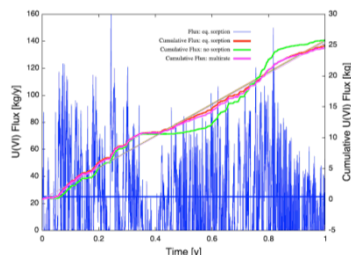
# Domain Decomposition

## Structured Grid Example

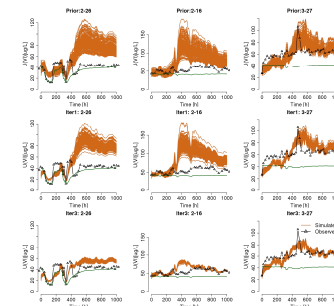


# PFLOTRAN Output Formats

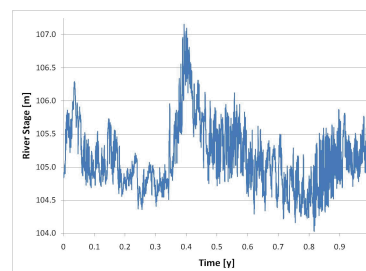
- Excel: \*.tec [POINT]
- gnuplot: \*.tec [POINT]
- MATLAB: \*.tec [POINT], \*.h5
- Matplotlib: \*.tec [POINT]
- Tecplot : \*.tec [POINT, BLOCK, FEBRICK]
- ParaView: \*.h5, \*.xmf, \*.vtk
- R \*.tec [POINT], \*.h5
- VisIt \*.h5, \*.xmf, \*.vtk



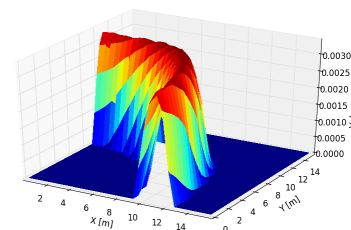
gnuplot



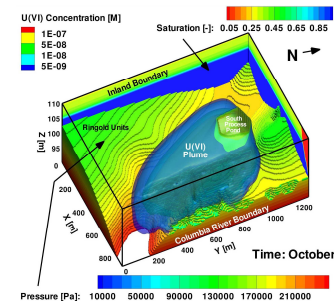
R



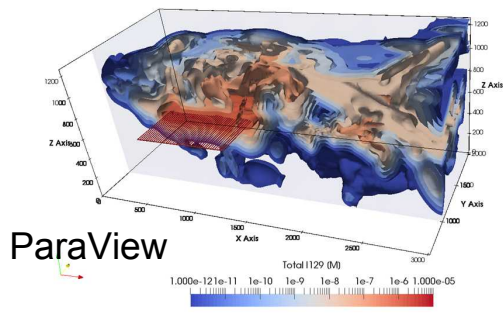
Excel



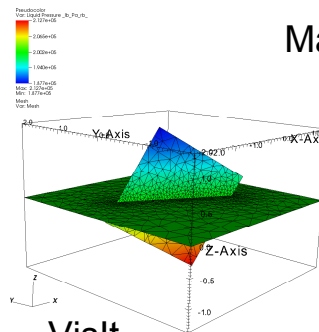
Matplotlib



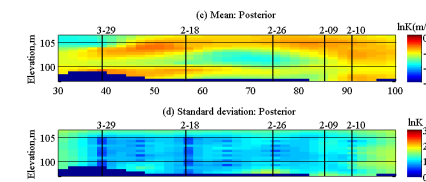
Tecplot



ParaView



VisIt

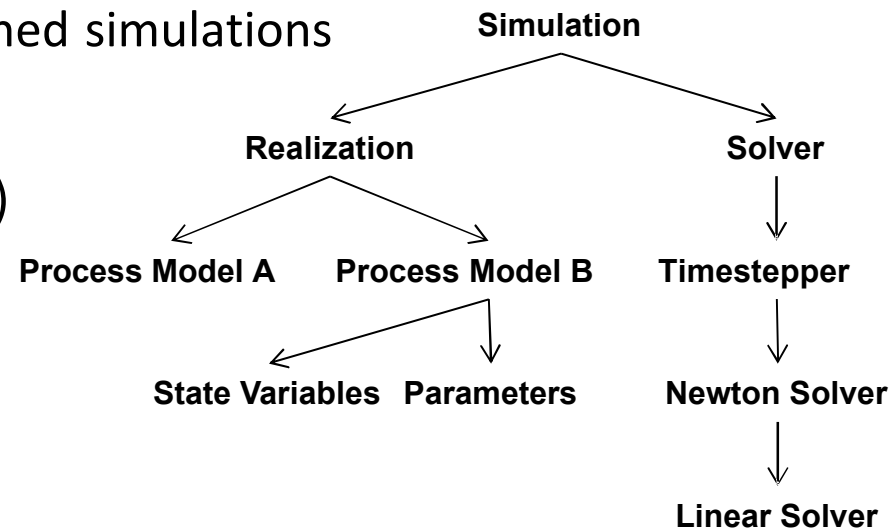


MATLAB

# Why Object-Oriented Fortran 2003/2008?

- Why Fortran?
  - Experienced domain scientists remain engaged
  - Commonality among all domain scientists
- Why object-oriented?
  - Modular data structures
    - Eases code development and debugging – data locality
    - Nesting of processes and data
  - Tree structure enables self-contained simulations

- Why Fortran 2003/2008?
  - Classes (extendable derived types)
    - Member functions
    - Inheritance
  - Pointers to procedures
    - E.g. swapping equations of state



# Object Oriented Fortran

## Fortran 77

```
subroutine X(a,b,c,d,e,f,...)
```

```
...
```

```
common/array/a(ncomp,ncell)
```

```
do icell = 1, ncell  
  do icomp = 1, ncomp  
    a(icomp,icell) = ...  
  enddo  
enddo
```

## OO Fortran 90

```
subroutine X(realization)
```

```
...
```

```
grid => realization%patch%grid  
reaction => realization%reaction  
cells => realization%patch...%cells
```

```
do icell = 1, grid%ncell  
  do icomp = 1, reaction%ncomp  
    cells(icell)%conc(icomp) = ...  
  enddo  
enddo
```

# Fortran 2003/2008

## Fortran 90

```
select case(eos_type)
  case(WATER)
    call EvaluateWater(p,t)
  case(AIR)
    call EvaluateAir(p,t)
  case(CO2)
    call EvaluateCO2(p,t)
  case(CH4)
    call EvaluateCH4(p,t)
end select
```

## Fortran 2003/2008

```
type, extends(eos_base) :: eos_C02
  ...
contains
  procedure :: Evaluate => EvaluateC02
end type eos_C02

class(eos_C02) :: eos

call eos%Evaluate(p,t)
```

eos = equation of state

# PFLOTRAN Support Infrastructure

- [www.pflotran.org](http://www.pflotran.org): documentation and overview
- Git: distributed source control management tool
- Bitbucket: online PFLOTRAN repository
  - git clone <https://bitbucket.org/pflotran/pflotran>
  - Source tree
  - Commit logs
  - Pull requests
  - Issue tracker
  - Wiki
    - Link to [documentation.pflotran.org](http://documentation.pflotran.org)
      - Developer/Theory/User guides
      - FAQ (entries motivated by questions on mailing list)
- Travis CI: automated building and testing (regression and unit)
- Google Groups: pflotran-users and pflotran-dev mailing lists
- Google Analytics: tracks behavior on Bitbucket

# PFLOTRAN Flow Modes

- Covered in shortcourse
  - RICHARDS: variably-saturated water
  - TH: variably-saturated water-energy
  - GENERAL: multiphase air-water-energy
  - WIPP\_FLOW: immiscible air-water
  - MPHASE: supercritical CO<sub>2</sub>-water-energy
  - FLASH2: supercritical CO<sub>2</sub>-water-energy (experimental)
  - IMMIS: air-water (experimental)
  - MISCIBLE: X-water-energy (experimental)
  - TOIL\_IMS: oil-water-energy (experimental)

# Flow Governing Equations

## General Mode (air-water-energy)

Water Mass 
$$\frac{\partial \phi (s_l \rho_l X_w^l + s_g \rho_g X_w^g)}{\partial t} = -\nabla \cdot (\rho_l X_w^l \mathbf{q}_l + \rho_g X_w^g \mathbf{q}_g + \mathbf{J}_w^l + \mathbf{J}_w^g) + q_w$$

Air Mass 
$$\frac{\partial \phi (s_l \rho_l X_a^l + s_g \rho_g X_a^g)}{\partial t} = -\nabla \cdot (\rho_l X_a^l \mathbf{q}_l + \rho_g X_a^g \mathbf{q}_g + \mathbf{J}_a^l + \mathbf{J}_a^g) + q_a$$

Energy 
$$\frac{\partial \phi (s_l \rho_l U_l + s_g \rho_g U_g) + (1 - \phi) C_p^{\text{rock}} \rho_{\text{rock}} T}{\partial t} = -\nabla \cdot (\rho_l H_l \mathbf{q}_l + \rho_g H_g \mathbf{q}_g - \kappa_{\text{eff}} \nabla T) + q_e$$

$\phi$  = effective porosity [-]

$s_l$  = liquid saturation [-]

$s_g$  = gas saturation [-]

$\rho_l$  = liquid phase density [kmol/m<sup>3</sup>]

$\rho_g$  = gas phase density [kmol/m<sup>3</sup>]

$X_w^l$  = mole fraction of water in the liquid phase [-]

$X_w^g$  = mole fraction of water in gas phase [-]

$X_a^l$  = mole fraction of air in the liquid phase [-]

$X_a^g$  = mole fraction of air in gas phase [-]

$\mathbf{q}_l$  = liquid phase Darcy flux [m/sec]

$\mathbf{q}_g$  = gas phase Darcy flux [m/sec]

$\mathbf{J}_w^l$  = water diffusive flux in liquid phase [kmol/m<sup>2</sup>/sec]

$\mathbf{J}_a^l$  = air diffusive flux in liquid phase [kmol/m<sup>2</sup>/sec]

$\mathbf{J}_w^g$  = water vapor diffusive flux in gas phase [kmol/m<sup>2</sup>/sec]

$\mathbf{J}_a^g$  = air diffusive flux in gas phase [kmol/m<sup>2</sup>/sec]

$q_w$  = water source/sink [kmol/sec]

$q_a$  = air source/sink [kmol/sec]

$q_e$  = energy source/sink [MJ/sec]

$U_l$  = liquid phase internal energy [MJ/kmol]

$U_g$  = gas phase internal energy [MJ/kmol]

$H_l$  = liquid phase enthalpy [MJ/kmol]

$H_g$  = gas phase enthalpy [MJ/kmol]

$C_p^{\text{rock}}$  = rock heat capacity [MJ/kg rock-K]

$\rho_{\text{rock}}$  = rock particle density [kg/m<sup>3</sup> rock]

$T$  = temperature [C]

$\kappa_{\text{eff}}$  = effective thermal conductivity [W/K-m]

# Flow Governing Equations

Darcy Flux

$$\mathbf{q}_\alpha = -\frac{k k_\alpha}{\mu_\alpha} \nabla (p_\alpha - \gamma_\alpha g z), \quad (\alpha = l, g)$$

Air Diffusion in Liquid Phase

$$\mathbf{J}_a^l = -\tau \phi S_l D_l \rho_l \nabla X_a^l$$

Air Diffusion in Gas Phase

$$\mathbf{J}_a^g = -\tau \phi S_g D_g^0 \left( \frac{T}{T_K} \right)^\theta \frac{p_0}{p_g} \rho_g \nabla X_a^g$$

$\mathbf{q}_\alpha$  = Darcy flux for phase  $\alpha$  [m/s]

$k$  = intrinsic permeability [m<sup>2</sup>]

$k_\alpha$  = relative permeability for phase  $\alpha$  [-]

$\mu_\alpha$  = viscosity for phase  $\alpha$  [Pa-s]

$p_\alpha$  = pressure for phase  $\alpha$  [Pa]

$\gamma_\alpha$  = density for phase  $\alpha$  [kg/m<sup>3</sup>]

$g$  = gravity [m/s<sup>2</sup>]

$z$  = elevation [m]

$\mathbf{J}_a^l$  = diffusive flux of air in liquid phase [kmol/m<sup>2</sup>-s]

$\tau$  = tortuosity [-]

$D_l$  = aqueous diffusivity [m<sup>2</sup>/s]

$\mathbf{J}_a^g$  = diffusive flux of air in gas phase [kmol/m<sup>2</sup>-s]

$D_g^0$  = gas diffusivity [m<sup>2</sup>/s]

$p_0$  = reference pressure [Pa]

# Flow Primary Variables

General Mode

Thermodynamic State of Fluid	Primary Variables		
	$X_1$	$X_2$	$X_3$
Two-Phase	$p_g$	$s_g$	$T$
	$p_g$	$s_g$	$p_a$
Liquid	$p_l$	$X_a^l$	$T$
Gas	$p_g$	$p_a$	$T$

# Flow Governing Equations

## TH Mode (water-energy)

Water Mass

$$\frac{\partial \phi (s_l \rho_l)}{\partial t} = -\nabla \cdot (\rho_l \mathbf{q}_l) + q_w$$

Energy

$$\frac{\partial \phi (s_l \rho_l U_l) + (1 - \phi) C_p^{\text{rock}} \rho_{\text{rock}} T}{\partial t} = -\nabla \cdot (\rho_l H_l \mathbf{q}_l - \kappa_{\text{eff}} \nabla T) + q_e$$

# Flow Governing Equations

## RICHARDS Mode (water)

Water Mass

$$\frac{\partial \phi(s_l \rho_l)}{\partial t} = -\nabla \cdot (\rho_l \mathbf{q}_l) + q_w$$

# Constitutive Relations

- Characteristic curves
  - Capillary pressure / saturation functions
    - E.g. Brooks Corey, van Genutchen
  - Relative permeability functions
    - E.g. Burdine, Mualem
  - One may add custom characteristic curves by extending the base classes

# Saturation Function Classes

```
type :: sat_func_base_type
  type(polynomial_type), pointer :: sat_poly
  type(polynomial_type), pointer :: pres_poly
  PetscReal :: Sr
  PetscReal :: pcmax
  PetscBool :: analytical_derivative_available
contains
  procedure, public :: Init => SFBaseInit
  procedure, public :: Verify => SFBaseVerify
  procedure, public :: Test => SFBaseTest
  procedure, public :: SetupPolynomials => SFBaseSetupPolynomials
  procedure, public :: CapillaryPressure => SFBaseCapillaryPressure
  procedure, public :: Saturation => SFBaseSaturation
end type sat_func_base_type

type, public, extends(sat_func_base_type) :: sat_func_VG_type
  PetscReal :: alpha
  PetscReal :: m
contains
  procedure, public :: Init => SF_VG_Init
  procedure, public :: Verify => SF_VG_Verify
  procedure, public :: CapillaryPressure => SF_VG_CapillaryPressure
  procedure, public :: Saturation => SF_VG_Saturation
end type sat_func_VG_type
```

# Constitutive Relations (cont.)

- Equations of state
  - Water
    - Density (Constant, Exponential, Planar (lookup table), **IFC67**, Batzle and Wang,, etc.)
    - Enthalpy (Constant, Planar, **IFC67**, etc.)
    - Viscosity (Constant, **Default**, Batzle and Wang, Grabowski)
  - Steam
    - Density (Constant, Planar, **IFC67**)
    - Enthalpy (Constant, Planar, **IFC67**)
  - Gas
    - Density (Constant, **Ideal**, RKS)
    - Enthalpy (Constant, **Ideal**)
    - Viscosity (Constant, **TOUGH2** mixture)
  - Custom EOSs can be added through the use of Fortran procedure pointers

# Constitutive Relations (cont.)

- Solubility of gas component in liquid phase
  - Function of gas pressure through the Henry's law constant
- Water saturation pressure
  - IFC67

# Transport

- Multicomponent
- Mobile/immobile primary species
- Advection
  - First order upwinding
- Hydrodynamic dispersion
  - Temperature-dependent molecular diffusion
  - Species-dependent molecular diffusion (charge balance issues)
  - Material-specific mechanical dispersion

# Biogeochemical Reaction

- Aqueous speciation
  - Ion activity models
    - Debye-Huckel B-dot
- Mineral precipitation-dissolution
  - Kinetic
    - Transition state theory
    - Temperature dependent
      - Arrhenius-based
    - Prefactors
    - Attenuation
    - Rate limiters
    - Thresholds
  - Equilibrium – initial/boundary conditions only
- General ( $A + B \leftrightarrow C$ )
  - $N^{\text{th}}$  order kinetics
  - Reversible
- Microbiological
  - Michaelis–Menten kinetics
  - Biomass
  - Inhibition
- Radioactive decay with daughter products
  - Limited to aqueous and sorbed phases

# Biogeochemical Reaction (cont.)

- Sorption
  - Isotherm-based
    - Linear
    - Langmuir
    - Freundlich
  - Ion exchange
    - Equilibrium
  - Surface complexation
    - Equilibrium
    - Kinetic
    - Multirate kinetic
- Reaction Sandbox
  - Framework for implementing custom kinetic (rate-limited) reactions

# Reactive Transport Governing Equations

$$\frac{\partial}{\partial t} (\phi s \Psi_j + \Psi_{S,j}) + \nabla \cdot (\mathbf{q} - \phi s \mathbf{D} \nabla) \Psi_j = Q_j - \sum_r \nu_{jr} I_r$$

$$\Psi_j = C_j + \sum_{i=1}^{N_X} \nu_{ji} \frac{K_i}{\gamma_i} \prod_{j'=1}^{N_c} (\gamma_{j'} C_{j'})^{\nu_{j'i}}$$

$\phi$  = porosity [-]

$s$  = liquid saturation [-]

$\Psi_j$  = total component concentration of species  $j$  [mol/L]

$\Psi_{S,j}$  = total sorbed concentration of species  $j$  [mol/m<sup>3</sup>]

$\mathbf{q}$  = liquid Darcy velocity [m/s]

$\mathbf{D}$  = hydrodynamic dispersion coefficient [m<sup>2</sup>/s]

$Q_j$  = source/sink for species  $j$  [mol/s]

$\nu_{jr}$  = stoichiometry of species  $j$  in kinetic reaction  $r$  [-]

$I_r$  = kinetic rate for reaction  $r$  [mol/s]

$C_j$  = free ion concentration for species  $j$  [mol/kg water]

$N_X$  = # aqueous complexes [-]

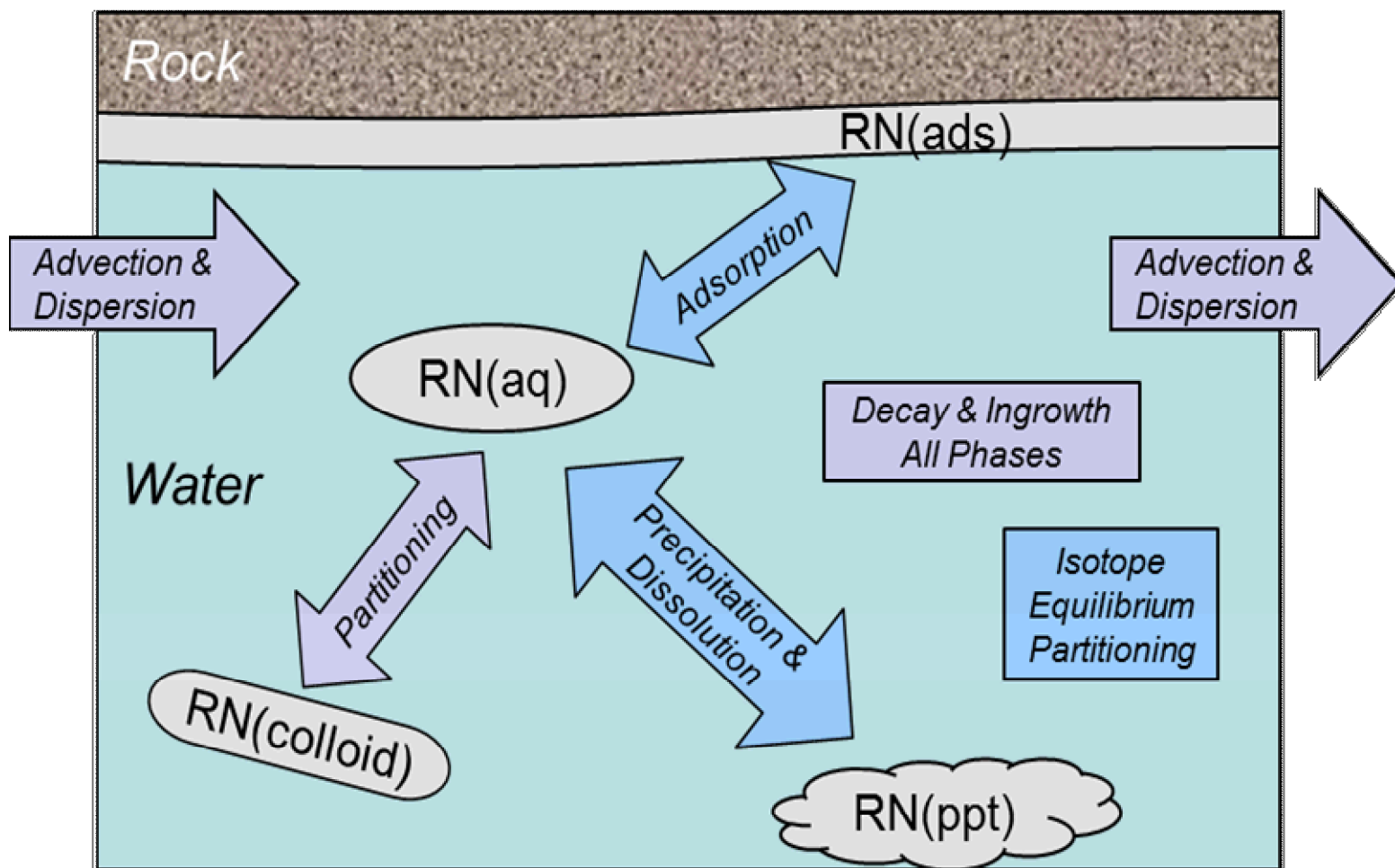
$\nu_{ji}$  = stoichiometry of species  $j$  in complex  $i$  [-]

$K_i$  = equilibrium constant for complex  $i$

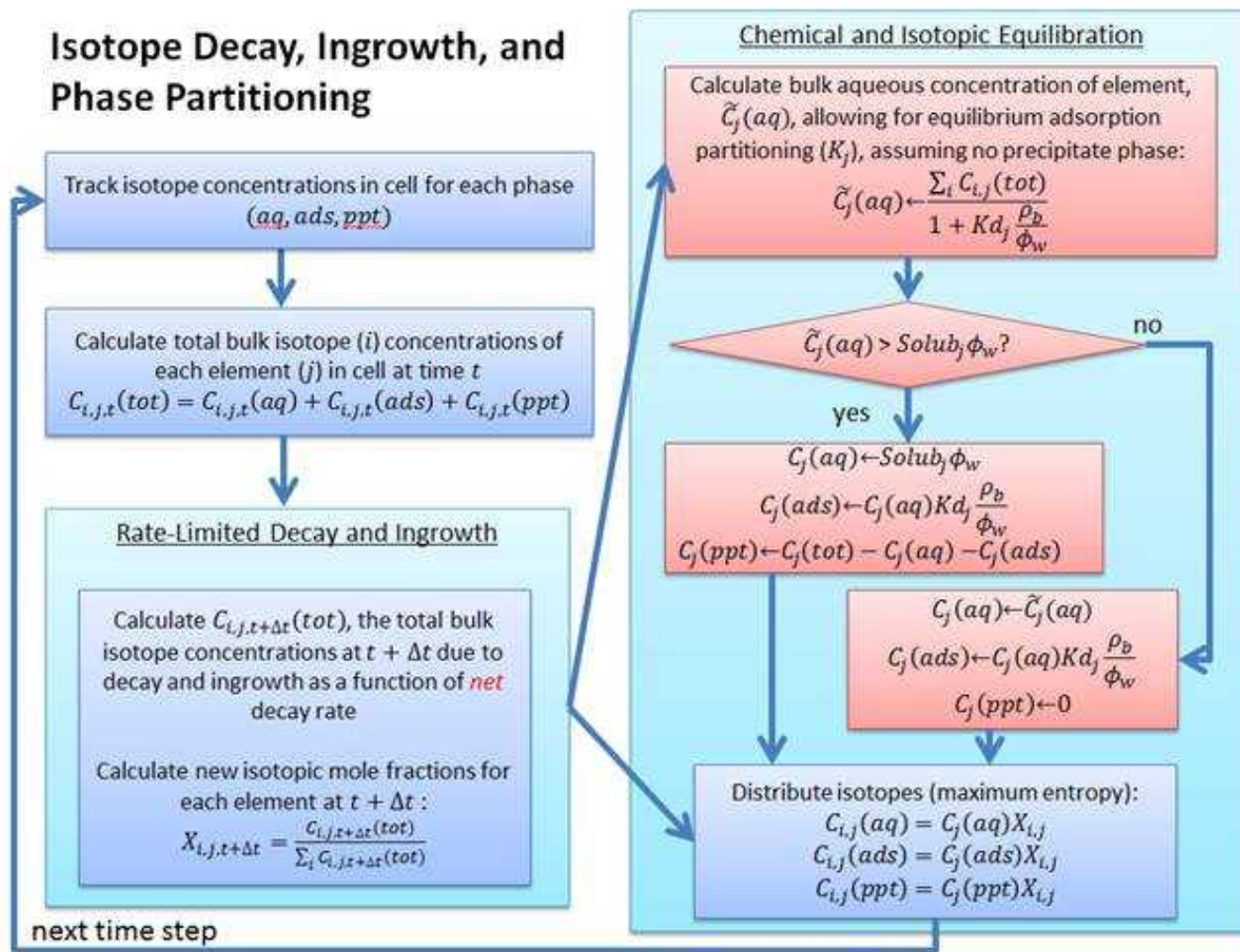
$\gamma_i$  = activity coefficient for complex  $i$  [-]

$N_c$  = # primary aqueous species [-]

# Isotope Decay, Ingrowth and Partitioning



# Isotope Decay, Ingrowth and Partitioning



# Reaction Sandbox

Reaction Sandbox Class (to be modified by the user)

```
type, public, extends(reaction_sandbox_base_type) :: &
    reaction_sandbox_xxx_type
    ! Add class parameters here
    class(reaction_sandbox_base_type), pointer :: next
contains
    ! Map procedures here
    procedure, public :: ReadInput => XXXRead
    procedure, public :: Setup => XXXSetup
    procedure, public :: Evaluate => XXXReact
    procedure, public :: Destroy => XXXDestroy
end type reaction_sandbox_base_type
```

Reaction Sandbox Linked List (not modified by the user)

```
cur_reaction => rxn_sandbox_list
do
    if (.not.associated(cur_reaction)) exit
    call cur_reaction%Evaluate(Residual, Jacobian, &
        state_variables)
    cur_reaction => cur_reaction%next
enddo
```

# Simple Reaction Sandbox

## Available Species:

Aqueous: Aaq, Baq, Caq, Daq, Eaq, Faq

Immobilized: Xim, Yim

## Example Rate Expressions:

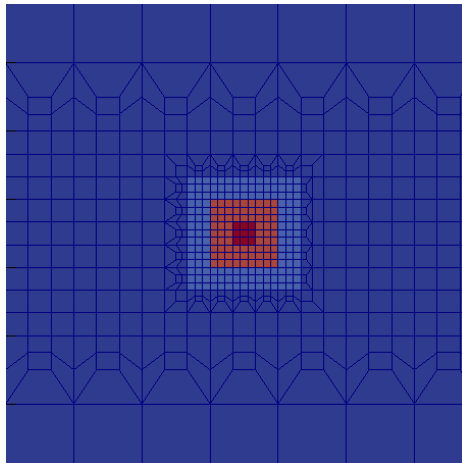
## Units of Rate Constant k

Rate = k * L_water	! [mol/L-sec]	0 <sup>th</sup> Order
Rate = k * Aaq * L_water	! [1/sec]	1 <sup>st</sup> Order
Rate = k * Aaq * Baq * L_water	! [L/mol-sec]	2 <sup>nd</sup> Order
Rate = k * Aaq / (K_Aaq + Aaq) * L_water	! [mol/L-sec]	
Rate = k * Xim * L_water * & Aaq / (K_Aaq + Aaq) * & Baq / (K_Baq + Baq)	! [mol-m <sup>3</sup> bulk / L-mol_biomass-sec]	
Rate = (k * Aaq - kr * Caq) * L_water	! [1/sec]	

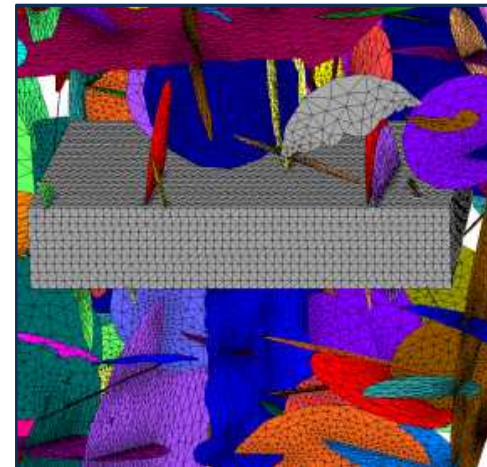
Assumed Units: Aqueous species [mol/L water], Immobilized species [mol/m<sup>3</sup> bulk volume], Rate constant k [reaction-dependent], Rate [mol/sec], K\_Xxx [mol/L water], L\_water [L water]

# Gridding

- Structured
  - Uniform or variable grid spacing
- Unstructured Implicit
  - Finite element format (elements and vertices)
- Unstructured Explicit
  - Polyhedral format (define cells and connectivity)



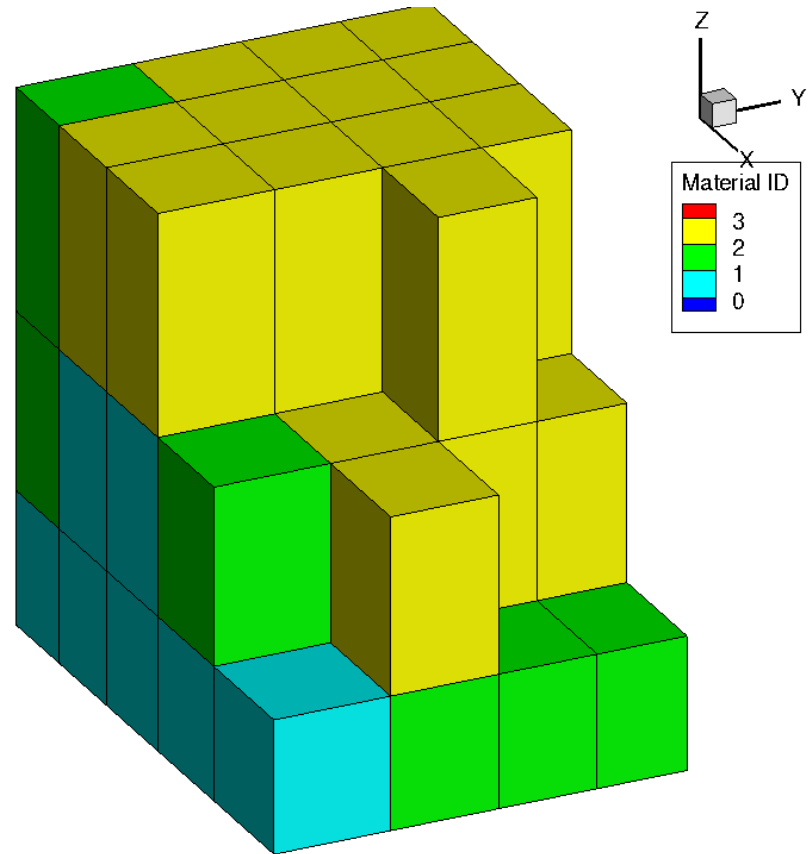
Emily Stein  
Sandia National Laboratories



Satish Karra  
Los Alamos National Laboratory

# Structured Grid

```
GRID
  TYPE structured
  ORIGIN 0.d0 0.d0 0.d0
  NXYZ 5 4 3
  DXYZ
    10. 11. 12. 13. 14.
    13. 12. 11. 10.
    15. 20. 25.
  /
END
```



# Unstructured Implicit Grid

GRID

TYPE unstructured ./mixed.h5

END

15 24

P 4 5 6 2 1

T 4 3 5 1

H 19 9 5 12 17 7 6 16

T 5 13 14 15

P 13 5 12 22 15

H 20 10 9 19 18 8 7 17

...

5.000000e+00 5.000000e+00 5.000000e+00

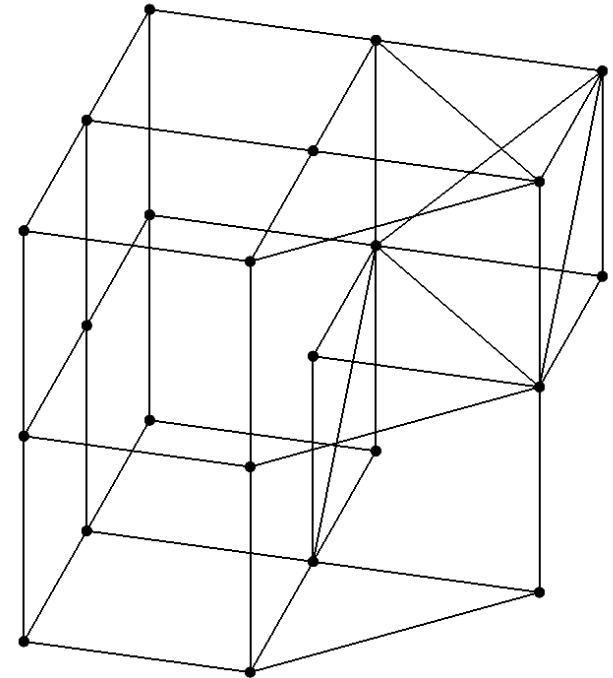
5.000000e+00 2.500000e+00 5.000000e+00

5.000000e+00 5.000000e+00 2.500000e+00

5.000000e+00 2.500000e+00 2.500000e+00

...

0.000000e+00 2.500000e+00 0.000000e+00



# Unstructured Explicit Grid

GRID

TYPE unstructured\_explicit ./mixed.uge

END

CELLS 15

1 4.0625 4.0625 4.0625 5.20833

2 4.375 4.375 3.125 2.60417

3 3.3333 3.3333 3.75 7.8125

4 3.3333 1.6667 3.75 7.8125

5 3.3333 1.6667 1.25 7.8125

...

15 1.25 3.75 0.3125 2.60417

CONNECTIONS 24

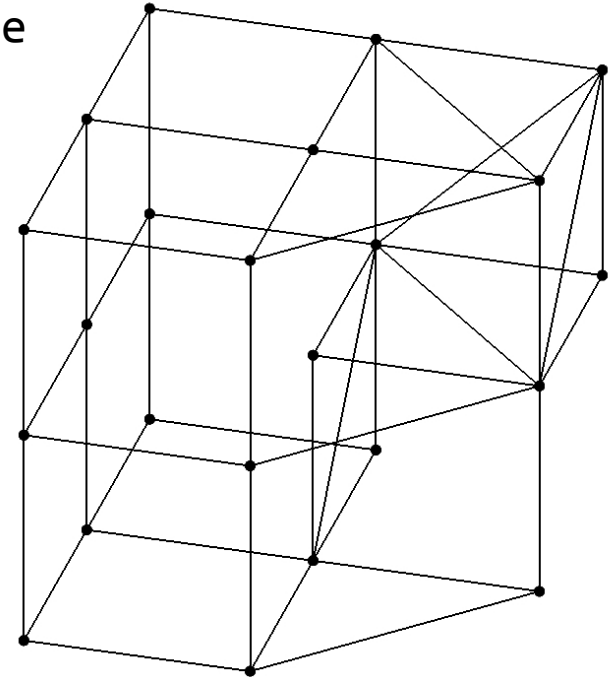
1 2 4.16667 4.16667 3.3333 6.25

1 3 3.75 3.75 3.75 8.8388

3 4 3.75 2.5 3.75 6.25

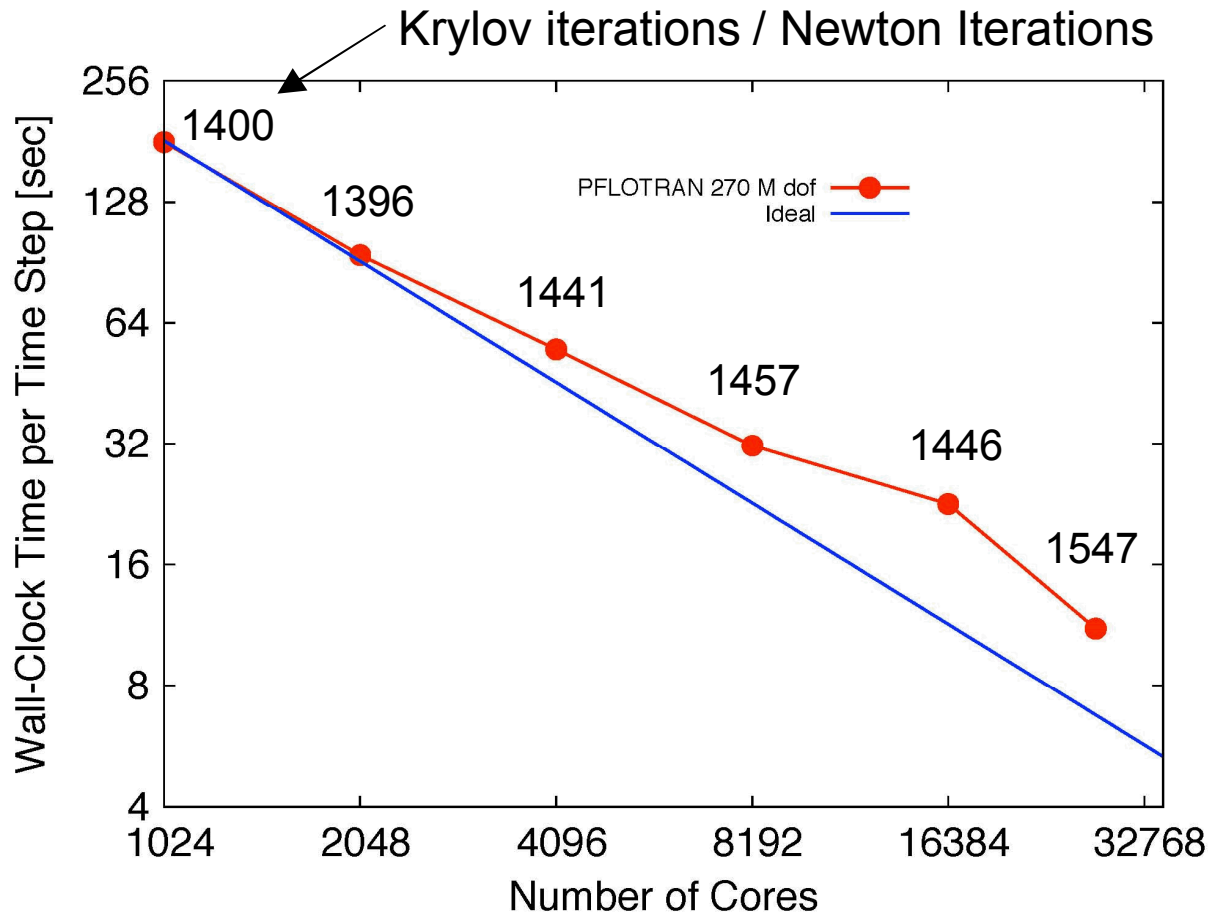
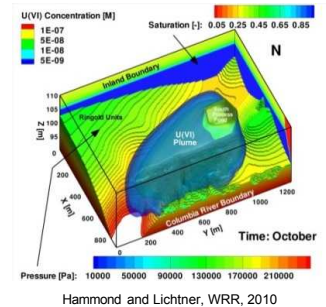
...

14 15 0.41667 3.75 0.41667 2.2097



# PFLOTRAN Parallel Performance

Hanford 300 Area



Overall 60% efficient  
Science

(1-2% of overall time)

- 75% efficient (wall clock)

Solvers

(96% of overall time)

- 90% efficient (iteration count)
- 64% efficient (wall clock)

# ANDRA QUESTIONS

# ANDRA Questions

## ■ Multiphase Flow

- Solvers employed (in particular, for variably saturated transport)?
  - Nonlinear solver
    - Newton's method
      - » Analytical and/or numerical derivatives
  - Linear solver
    - Direct
    - Iterative Krylov
    - Constrained Pressure Residual (CPR) being investigated for oil flow modes
- How is multiphase state transition handled?
  - Swapping of primary dependent variables when thresholds are exceeded
  - Thresholds
    - Liquid → 2 Phase          vapor pressure < saturation pressure
    - Gas → 2 Phase             vapor pressure > saturation pressure
    - 2 Phase → Liquid         gas saturation < 0
    - 2 Phase → Gas             gas saturation > 1

# ANDRA Questions

- Multiphase Flow
  - How are molecular diffusion terms defined? By phase, species, material, zone?
    - Multiphase flow
      - Molecular diffusion: by phase
    - Reactive transport
      - Molecular diffusion: by species and phase
      - Mechanical dispersion: by material
  - How is dissolution of gas component in liquid phase handled? Henry's law?
    - Henry's law
  - How are thermal dynamic properties of water handled?
    - Through equations of state for each phase

# ANDRA Questions

- Reactive Transport
  - Kinetic precipitation-dissolution?
    - Yes, through kinetic mineral precipitation-dissolution
  - Ion exchange and surface complexation?
    - Yes
  - Is it possible to simulate reactive transport in variably saturated media?
    - Yes, saturation state has no impact on biogeochemical reaction
  - What phenomena are currently coupled to chemistry?
    - Multiphase flow
    - Multicomponent transport
    - Density dependent flow (e.g. salinity)
    - Feedbacks to flow/transport through porosity and tortuosity

# ANDRA Questions

- Heterogeneous material properties (how assigned)?

# How are initial and boundary conditions and material properties assigned?

- Create definition blocks
  - Material properties
  - Flow conditions
  - Transport conditions
  - Regions
- Create couplers
  - Initial condition
  - Boundary condition
  - Source sink
  - Strata

# How are material properties assigned?

- Define a material property blocks

```
MATERIAL_PROPERTY sand
  ID 1
  POROSITY DATASET Porosity
  TORTUOSITY 1.d0
  CHARACTERISTIC_CURVES sf1
  PERMEABILITY
    PERM_X 1.d-12
    PERM_Y 1.d-12
    PERM_Z 1.d-13
  /
END
```

```
MATERIAL_PROPERTY clay
  ID 2
  POROSITY 0.55d0
  TORTUOSITY DATASET Tortuosity
  CHARACTERISTIC_CURVES sf2
  PERMEABILITY
    DATASET Permeability
  /
END
```

# How are material properties assigned?

- Define region blocks

```
REGION all
  COORDINATES
    0.d0 0.d0 0.d0
    60.d0 46.d0 60.d0
  /
END
```

```
REGION east
  FACE EAST
  COORDINATES
    60.d0 0.d0 0.d0
    60.d0 46.d0 60.d0
  /
END
```

```
REGION well
  BLOCK 4 4 2 3 3 3
END
```

```
REGION observation_point
  COORDINATE 35.d0 22.d0 15.d0
END
```

# How are material properties assigned?


- Couple them through strata blocks

```
STRATA  
  REGION all  
  MATERIAL clay  
END
```

```
STRATA  
  REGION well  
  MATERIAL sand  
END
```

```
STRATA  
  MATERIAL materials_ids.h5  
END
```

Material IDs  
defined on a cell  
by cell basis



# How are initial and boundary conditions assigned?

- Define flow condition blocks

```
FLOW_CONDITION east
  TYPE
    PRESSURE hydrostatic
  /
  INTERPOLATION LINEAR
  DATUM LIST
    TIME_UNITS d
    0.d0 0.d0 0.d0 34.d0
    10.d0 0.d0 0.d0 39.d0
    50.d0 0.d0 0.d0 33.d0
    100.d0 0.d0 0.d0 34.d0
  /
  PRESSURE 101325 ! Pa
END
```

```
FLOW_CONDITION injection_well
  TYPE
    RATE scaled_volumetric_rate neighbor_perm
  /
  RATE 1 m^3/hr
END
```

# How are initial and boundary conditions assigned?

- Define transport condition blocks

```
TRANSPORT_CONDITION columbia_river
  TYPE dirichlet_zero_gradient
  CONSTRAINT_LIST
    0.d0 river_water
  /
END
```

```
TRANSPORT_CONDITION initial_groundwater
  TYPE dirichlet_zero_gradient
  CONSTRAINT_LIST
    0.d0 initial_groundwater
  /
END
```

```
TRANSPORT_CONDITION tracer_pulse
  TYPE dirichlet
  TIME_UNITS d
  CONSTRAINT_LIST
    0.d0 well_tracer
    10.d0 groundwater
  /
END
```

# How are initial and boundary conditions assigned?

- Define constraint blocks for use within transport conditions

```
CONSTRAINT initial_groundwater
```

```
CONCENTRATIONS
```

```
H+          1.d-7          M Calcite
Ca++        1.20644e-3     T
Cu++        1.e-8         T
Mg++        5.09772e-4     T
UO2++       2.4830E-11     T DATASET initial_U
K+          1.54789e-4     T
Na+         1.03498e-3     Z
HCO3-       2.57305e-3     T
Cl-         6.97741e-4     T
F-          2.09491e-5     T
HPO4--      1.e-8         M Fluorapatite
NO3-        4.69979e-4     T
SO4--       6.37961e-4     T
```

```
/
```

```
MINERALS
```

```
Calcite     DATASET initial_Calcite_vol_frac DATASET initial_Calcite_area
Metatorbernite 0.    1. cm^2/cm^3
```

```
/
```

```
END
```

# How are initial and boundary conditions assigned?

- Couple them through boundary and initial condition blocks

```
INITIAL_CONDITION
  FLOW_CONDITION initial
  TRANSPORT_CONDITION initial_groundwater
  REGION all
END
```

```
BOUNDARY_CONDITION east
  FLOW_CONDITION east
  TRANSPORT_CONDITION columbia_river
  REGION east
END
```

```
SOURCE_SINK well
  FLOW_CONDITION injection_well
  TRANSPORT_CONDITION tracer_pulse
  REGION well
END
```

# ANDRA Questions

- Heterogeneous material properties (how assigned)?

```
CONSTRAINT initial_groundwater
CONCENTRATIONS
```

```
  H+          1.d-7          M Calcite
  Ca++        1.20644e-3     T
  Cu++        1.e-8         T
  Mg++        5.09772e-4     T
  UO2++       2.4830E-11     T DATASET initial_U
  K+          1.54789e-4     T
  Na+         1.03498e-3     Z
  HCO3-       2.57305e-3     T
  Cl-         6.97741e-4     T
  F-          2.09491e-5     T
  HPO4--      1.e-8         M Fluorapatite
  NO3-        4.69979e-4     T
  SO4--       6.37961e-4     T
```

```
/
```

```
MINERALS
```

```
  Calcite     DATASET initial_Calcite_vol_frac DATASET initial_Calcite_area
  Metatorbernite 0.    1. cm^2/cm^3
```

```
/
```

```
END
```

# ANDRA Questions

- Decay chains (with and without branching)?
  - For aqueous and sorbed phases, use standard reactive transport
  - For aqueous, sorbed and mineral phases, use Isotope Decay, Ingrowth and Partitioning process model
- Sorption (isotherms supported)
  - Linear, Langmuir and Freundlich
- Precipitation-dissolution (handling of radioactive decay in solid phase)
  - Isotope Decay, Ingrowth and Partitioning process model

# ANDRA Questions

- Boundary and initial conditions (variable in time and space)?
  - Boundary conditions:
    - Variable in time: yes
    - Variable in space: yes
      - By region
      - Interpolated
  - Initial conditions: variable in space
    - Variable in space: yes
      - By region
      - Cell by cell
      - Interpolated
- Gridding (irregular Cartesian allowed?)
  - Yes
    - Structured with variable spacing
    - Unstructured explicit

# ANDRA Questions

- General
  - Is it possible to calculate a flux across an internal surface?
    - Currently restricted to Cartesian grid
    - Plans to implement unstructured
  - Is full tensor hydraulic conductivity supported?
    - No, nor full tensor dispersion either
  - Are some of these points scheduled for a future version of PFLOTRAN?
    - Fluxes across internal surfaces for unstructured grids (fall 2017)

# ANDRA Questions

- Roadmap for future development
  - Fluxes across internal surfaces for unstructured grids (fall 2017)
  - Colloids - kinetic rate limited (2018)
  - Input file interface for species dependent diffusion coefficients (2018)

# Questions?