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An Overview of Magnetic Materials R&D at Sandia National Labs

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Sandia National Laboratories develops advanced technology needed to ensure global peace. Focused R&D is a requirement.

Albuquerque, New Mexico



Livermore, California



SNL is an FFRDC: Federally funded Research and Development Center

SNL is GOCO: Government owned, contractor operated

SNL GOCO Management:

AT&T: 1949–1993

Martin Marietta: 1993–1995

Lockheed Martin: 1995–2017

Honeywell and Northrop Grumman (NTESS): 2017 - present

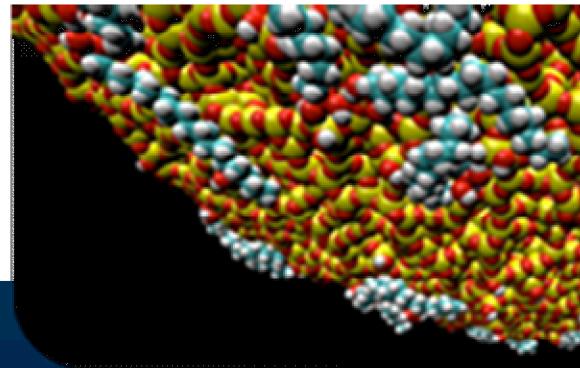
SNL's Science and Engineering Foundations



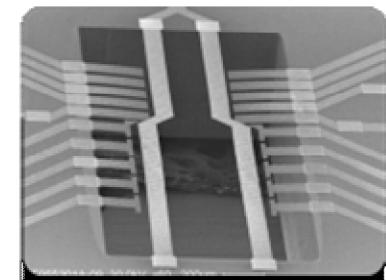
Computing and information science



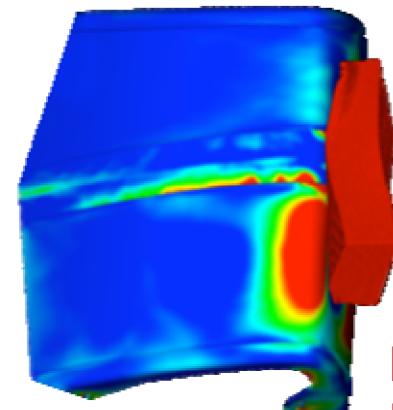
Materials science



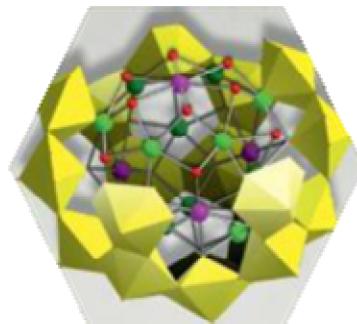
Nanodevices and microsystems



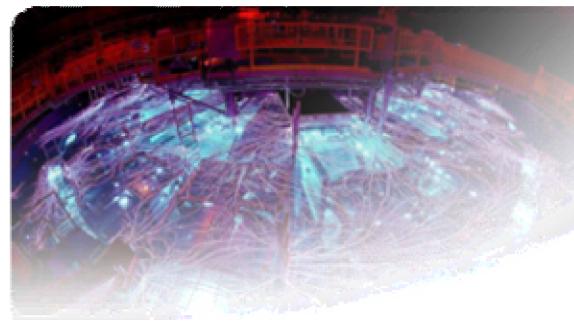
Engineering sciences



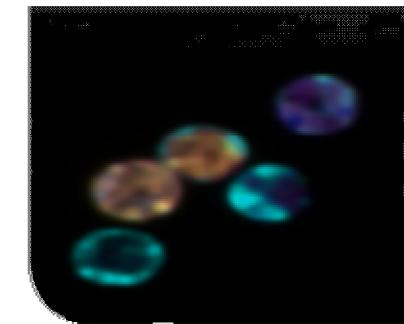
Geoscience



Radiation effects and high-energy density science

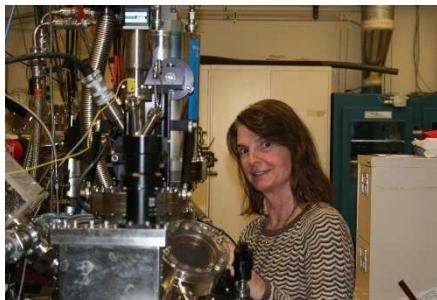
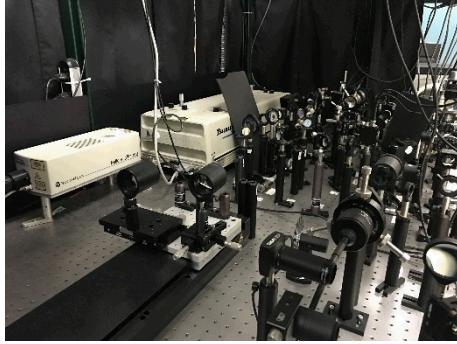


Bioscience



Missions: NW, Defense/Intelligence/Homeland Security, Energy/Climate

SNL Nanoscale Sciences Department R&D Activities

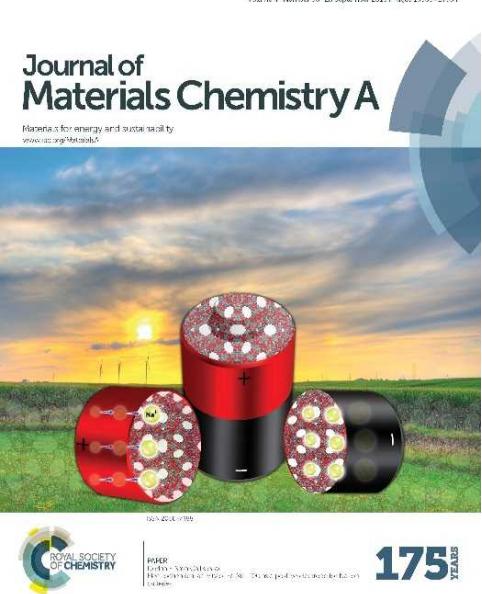
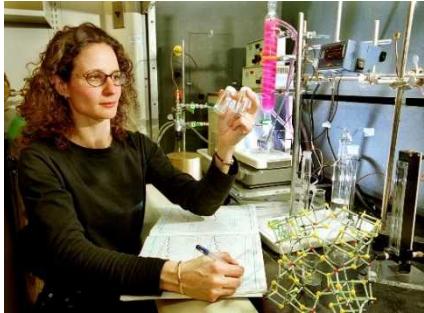
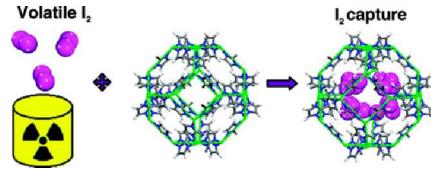


Thermal Imaging, Characterization & Spectroscopy

J|A|C|S
JOURNAL OF THE AMERICAN CHEMICAL SOCIETY

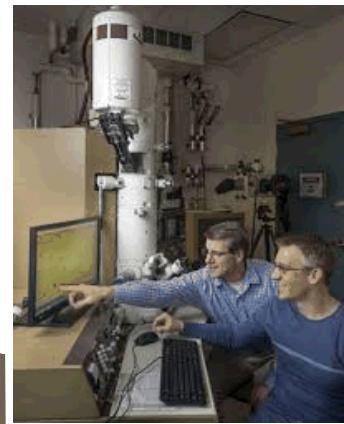
Capture of Volatile Iodine, a Gaseous Fission Product, by Zeolitic Imidazolate Framework-8

Dorina F. Sasu,¹ Mark A. Rodriguez,² Karen W. Chapman,¹ Peter J. Chupas,¹ Jeffery A. Greenhouse,³ Paul S. Crozier,⁴ and Tina M. Nelson^{1,5}

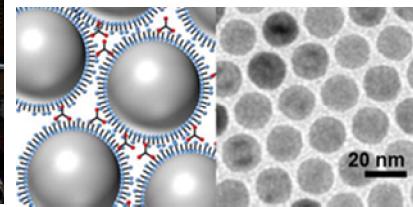


Materials and Electro Chemistry Synthesis and Characterization

Thin Film and Nanotemplate Materials



Electron & Scanning Probe Microscopy



Magnetic Materials and Characterization

Magnetic Device Materials impact many National Security Needs



Applications:

- Permanent Magnet based Actuators
- Passive Components for Power Electronics (i.e., inductors)
- Advanced Electronics (including Beyond Moore and Quantum Computing)
- Magnetic Sensors and Tags
- RF Applications

Typical Performance Needs:

- High frequency (into GHz)
- Reduced losses during operation (i.e., due to eddy currents)
- Small form factor (i.e., high saturation magnetization materials)
- Environmental stability in demanding environments
- Manufacturable

Key Challenge: Technology Readiness Level (TRL) Maturation, need academic and other partners

Power Electronics (and Therefore Inductive Elements) are Ubiquitous

Satellites



Electric ships



UAVs



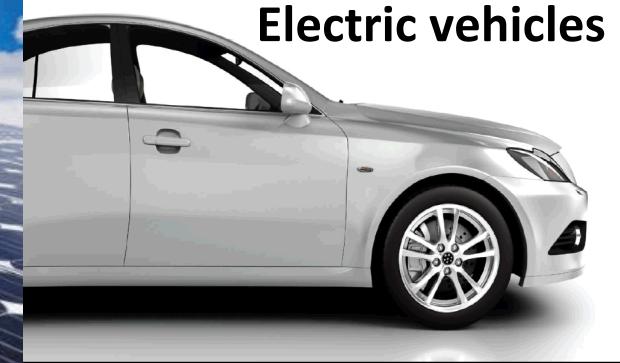
Transmission



Photovoltaics



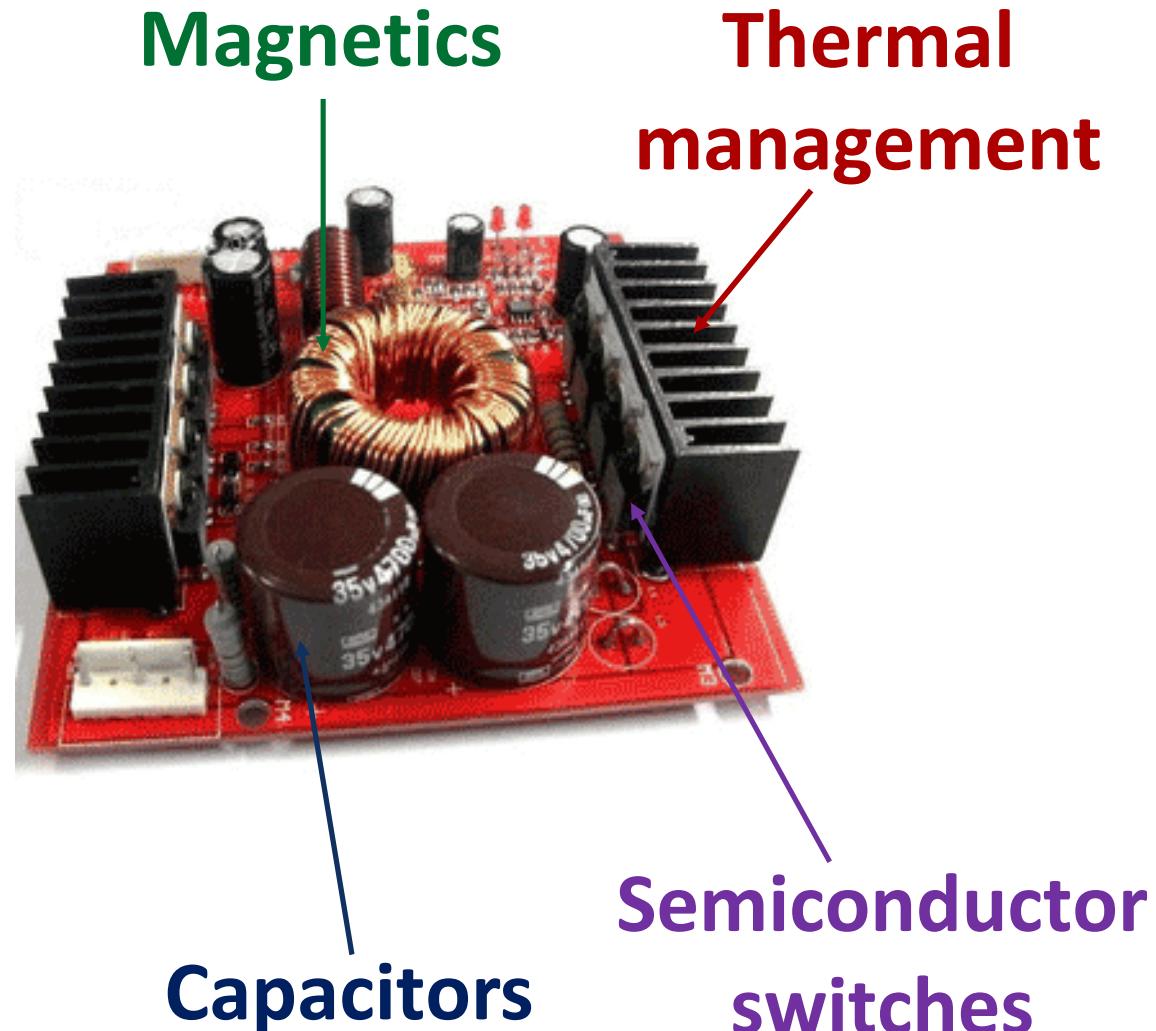
Electric vehicles



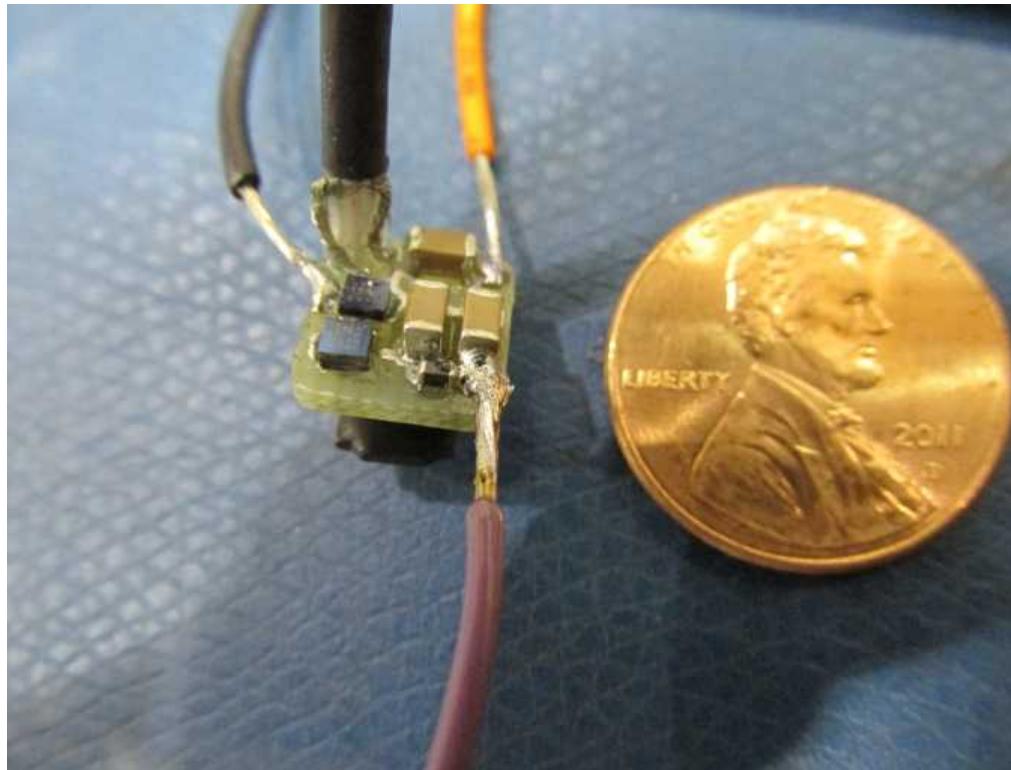
Soft Magnetic Devices Impact Power System Volume and Weight

Passive elements and thermal management comprise the bulk of the volume and mass of a power converter

WBG/UWBG materials enable higher switching frequency and better thermal management



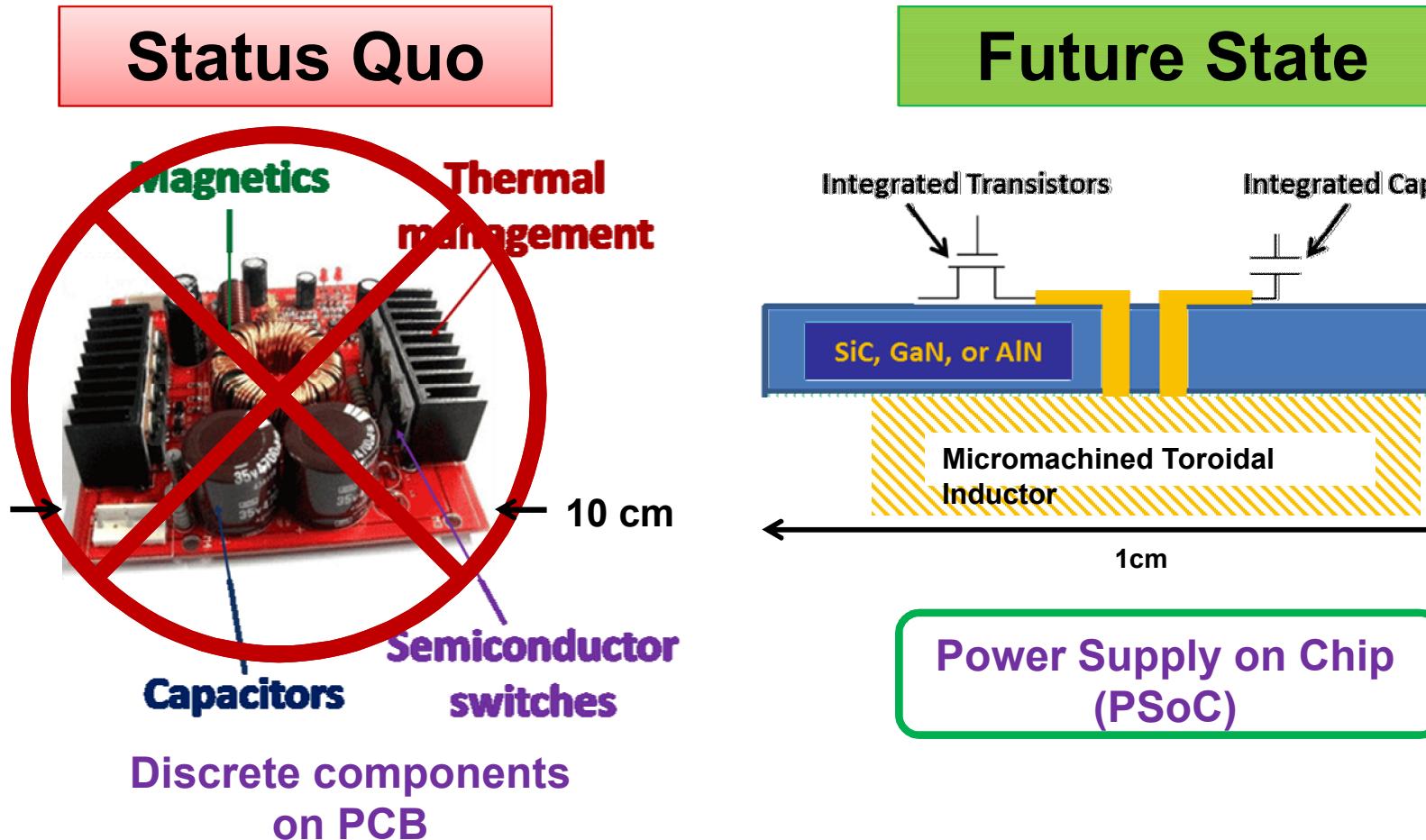
Concept: Miniaturized power electronics



Courtesy of Jack Flicker

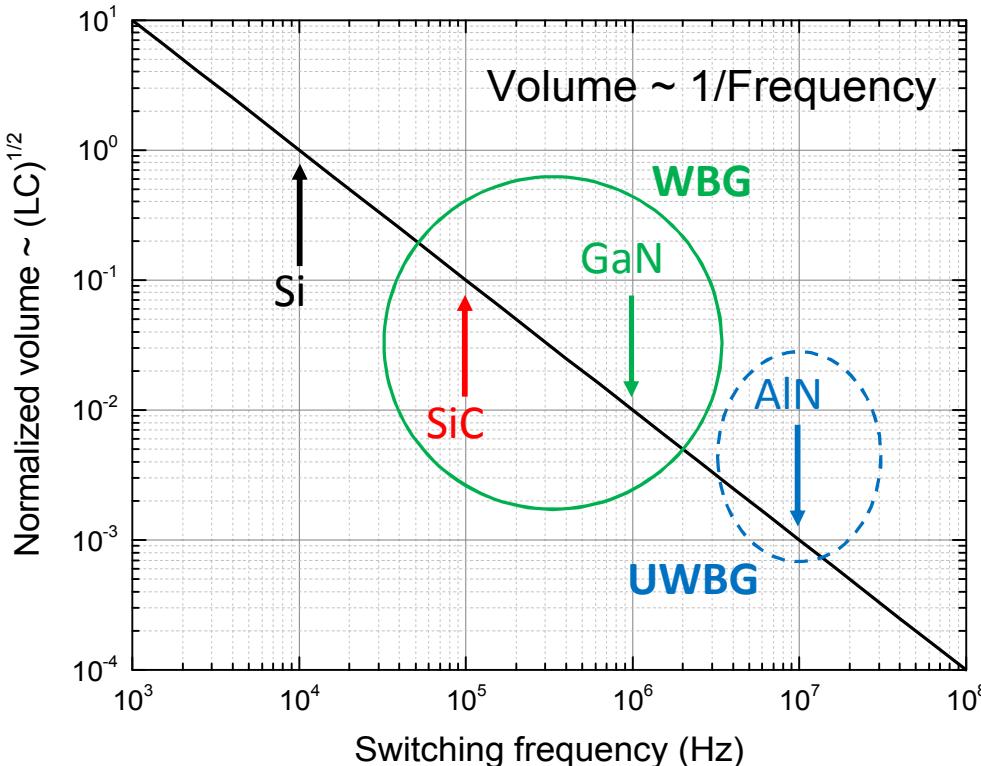
- Achieved: GaN \Rightarrow 215 W/in³
- 92 V, ~92 mA \Rightarrow 8.5 W, 215 W/in³, 1 MHz

Status Quo and Future State



#1 figure of merit: reduced form factor!

Higher Frequencies Decrease Inductance Requirements, However...



- Higher switching frequency is enabled by scaling properties of WBG/UWBG materials
- Ideal $1/f$ SWaP dependence (true dependence likely weaker $1/f^n$ with $n < 1$ due to nonidealities)
- Other benefits exist, e.g. higher voltage without series stacking of devices, and higher temperature operation
- *UWBGs may be required for specialized applications such as pulsed power*

Inductive core materials have essentially been an afterthought and new magnetic materials are needed

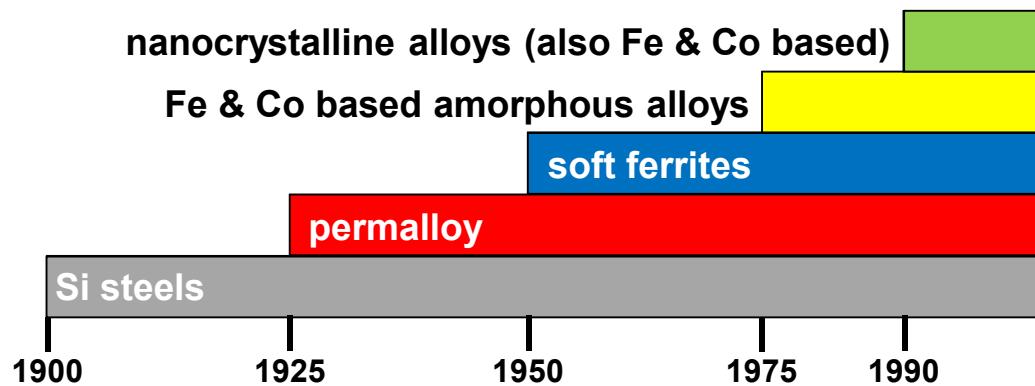
Transformer EMP Vulnerability



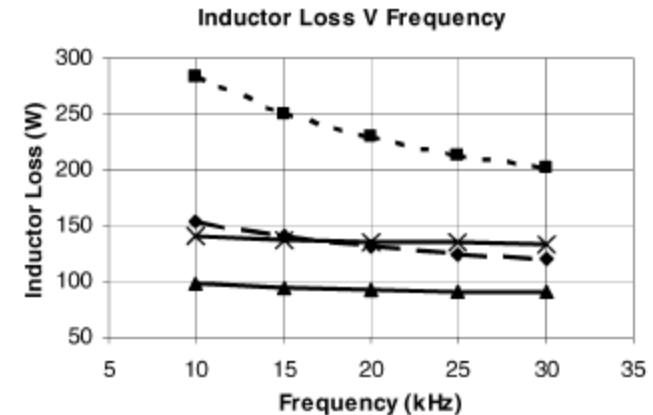
- **Geomagnetic storms couple very efficiently to long transmission lines**
- **Transformer can be driven to saturation, creating harmonics and reactive power**
- **Enough heat generated to melt copper windings**
- **Transformers the grid component that is hardest to replace**

Permanent damage to the Salem New Jersey Nuclear Plant GSU Transformer caused by the March 13, 1989 geomagnetic storm. Photos courtesy of PSE&G.

Soft Magnetic Material Development



Adapted from: L.A. Dobrzański, M. Drak, B. Ziębowicz, Materials with specific magnetic properties, Journal of Achievements in Materials and Manufacturing Eng., 17, 37 (2006).

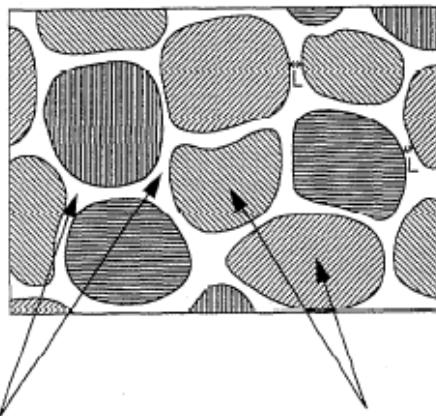


B.J. Lyons, J.G. Hayes, M.G. Egan, Magnetic Material Comparisons for High-Current Inductors in Low-Medium Frequency DC-DC Converters, IEEE, 71 (2007).



Magnetic Material	J_s (T)	$\rho(\mu\Omega\cdot m)$	Cost
VITROPERM (Vacuumschmelze)	1.20	1.15	High
Metglas 2605SC	1.60	1.37	High
Ferrite (Fexxocube)	0.52	5×10^6	Low
Si steel	1.87	0.05	Low
γ' -Fe ₄ N	1.89	~200	Low

Nanocrystalline Alloys & Manufacturing



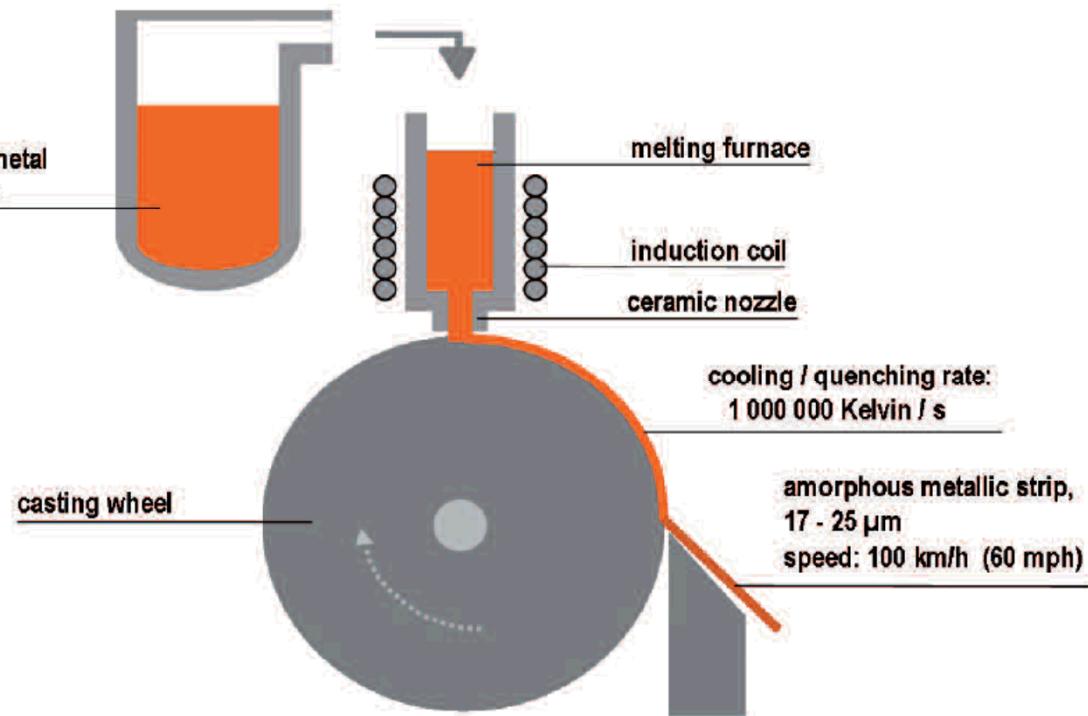
Intergranular amorphous phase with high T_c and high thermal stability due to large amounts of M and B elements.

Nano-scale α -Fe grains with small λ due to small amounts of M and B elements.

“NANOPERM”

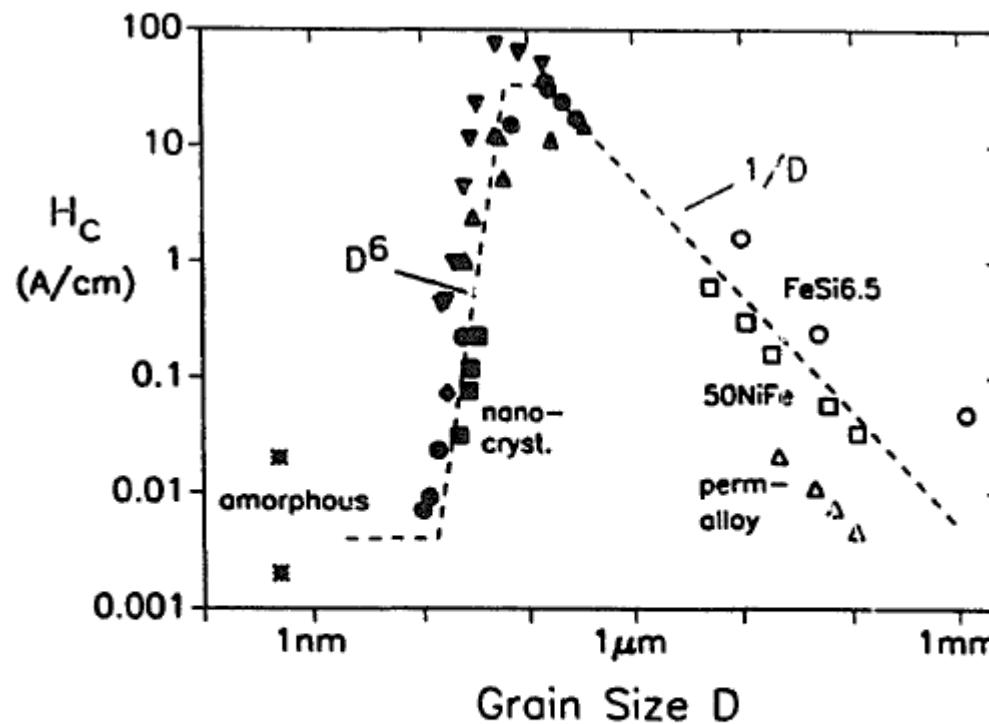
A. Makino, et. al., Nanocrystalline Soft Magnetic Fe-M-B (M = Zr, Hf, Nb) alloys and their applications, Mat. Sci. and Eng., A226-228, 594 (1997).

- Complex stoichiometries including Fe, Co, and other inactive elements such as B, Zr, Hf, Nb, Cu, Mo, Si, C
- Time consuming and high temperature processing → costly!
- Substantial inactive material to form a low loss nanocrystalline structure
- Material produced in tapes and often combined with plastic laminations



VITROPERM (Vacuumschmelze)

Coercivity as a Function of Particle Size

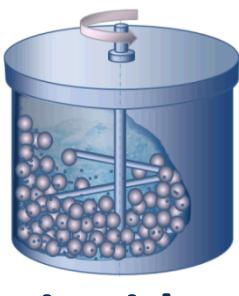


γ' -Fe₄N Synthesis and Processing

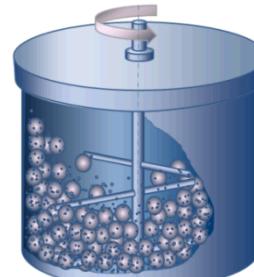
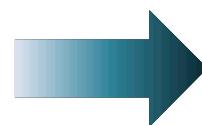


U.S. Patent Filed January 2015 (#62/105,918)

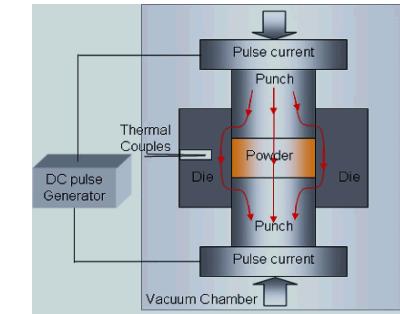
Synthesis of dense nanocrystalline iron nitrides using a two-step reactive milling and high pressure spark plasma sintering (SPS).



Liquid N₂



NH₃



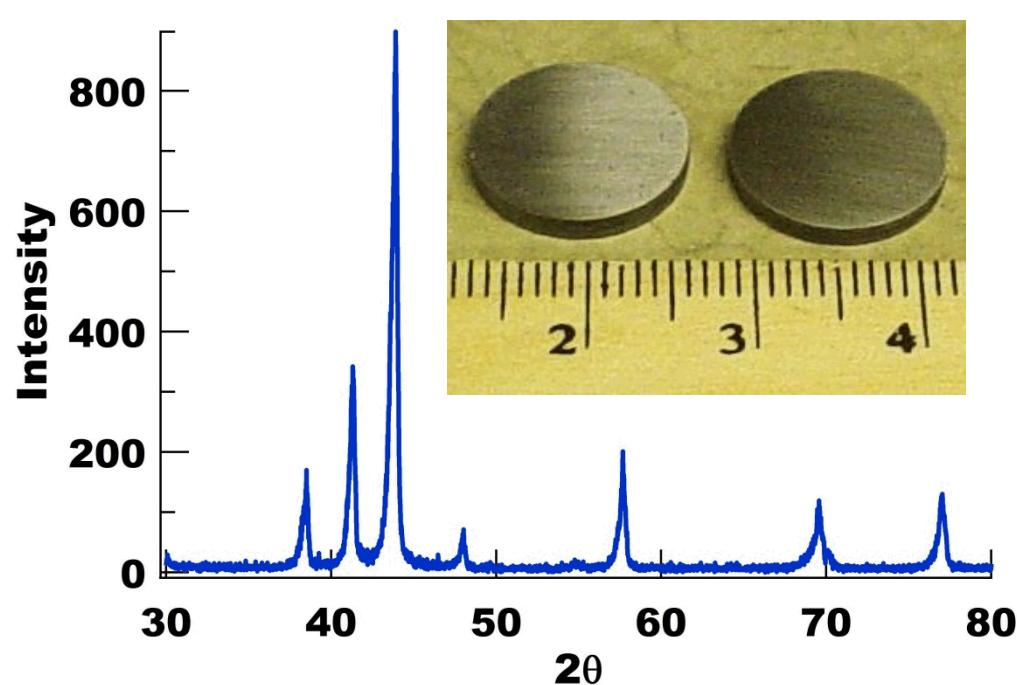
Spark Plasma
Sintering (SPS)

- Cryomilling creates nanocrystalline Fe powder with large amounts of vacancies, grain boundaries, and dislocations
- Defects serve as fast diffusion pathways for nitrogen atoms from NH₃
- SPS quickly consolidates raw powders with a low sintering temperature
 - Excellent control over grain growth
 - Result: Improved magnetic properties



SPS consolidated Iron Nitride

First ever bulk γ' - Fe_4N !

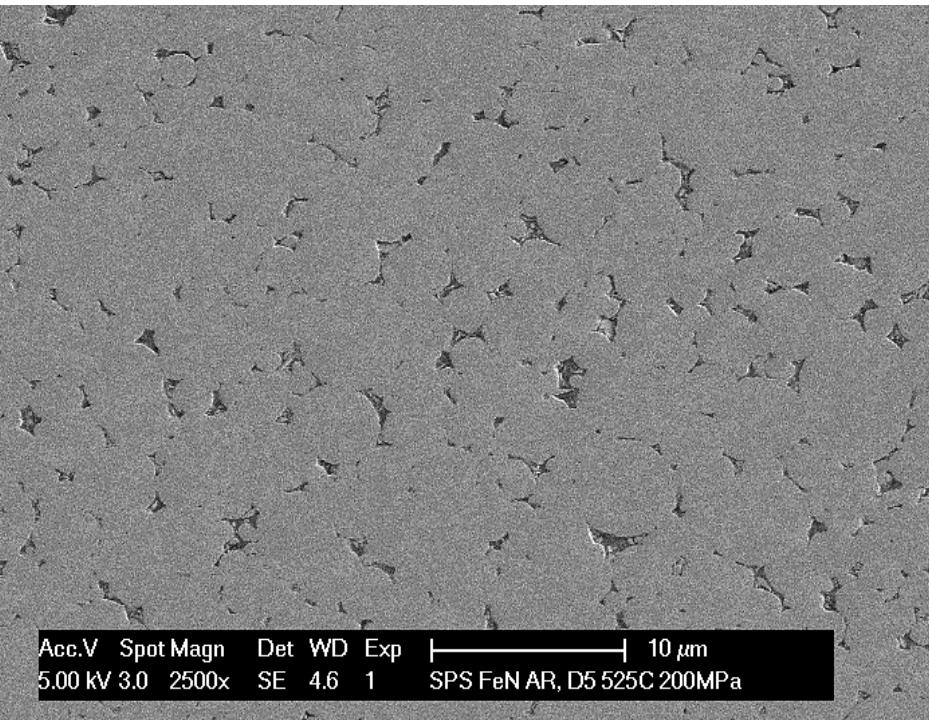


- Fe nitride powders well consolidated with little porosity
- Grain sizes 200 nm – 1 μm \rightarrow fine grain size = low loss
- γ' - Fe_4N primary phase
- Fe_3N secondary phase from mixed phase starting material

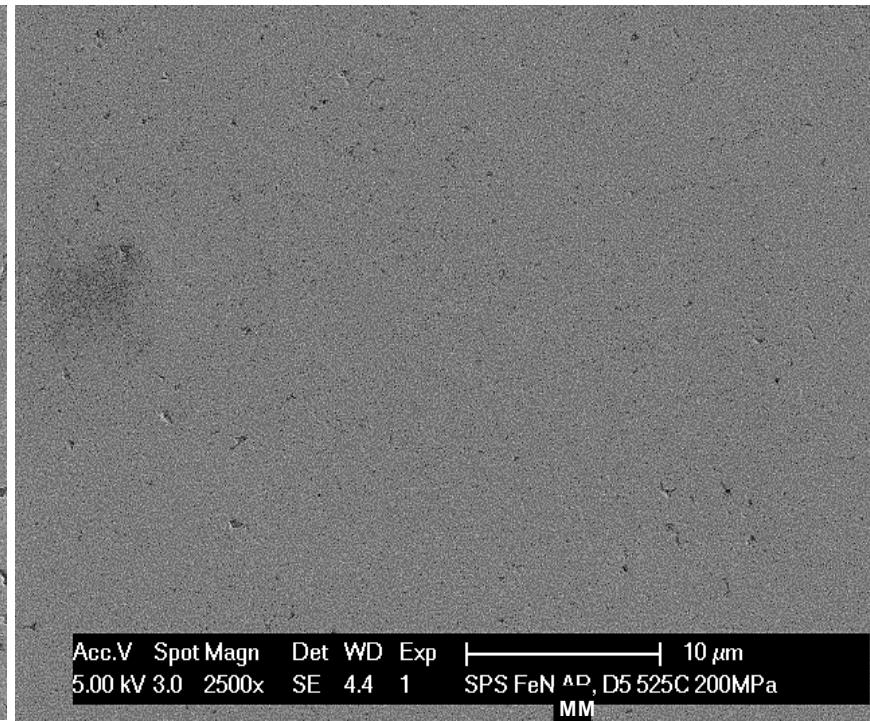
SEM of SPSed FeN samples, (Ø5mm, 525°C, 200MPa)



W/ as-received FeN powder

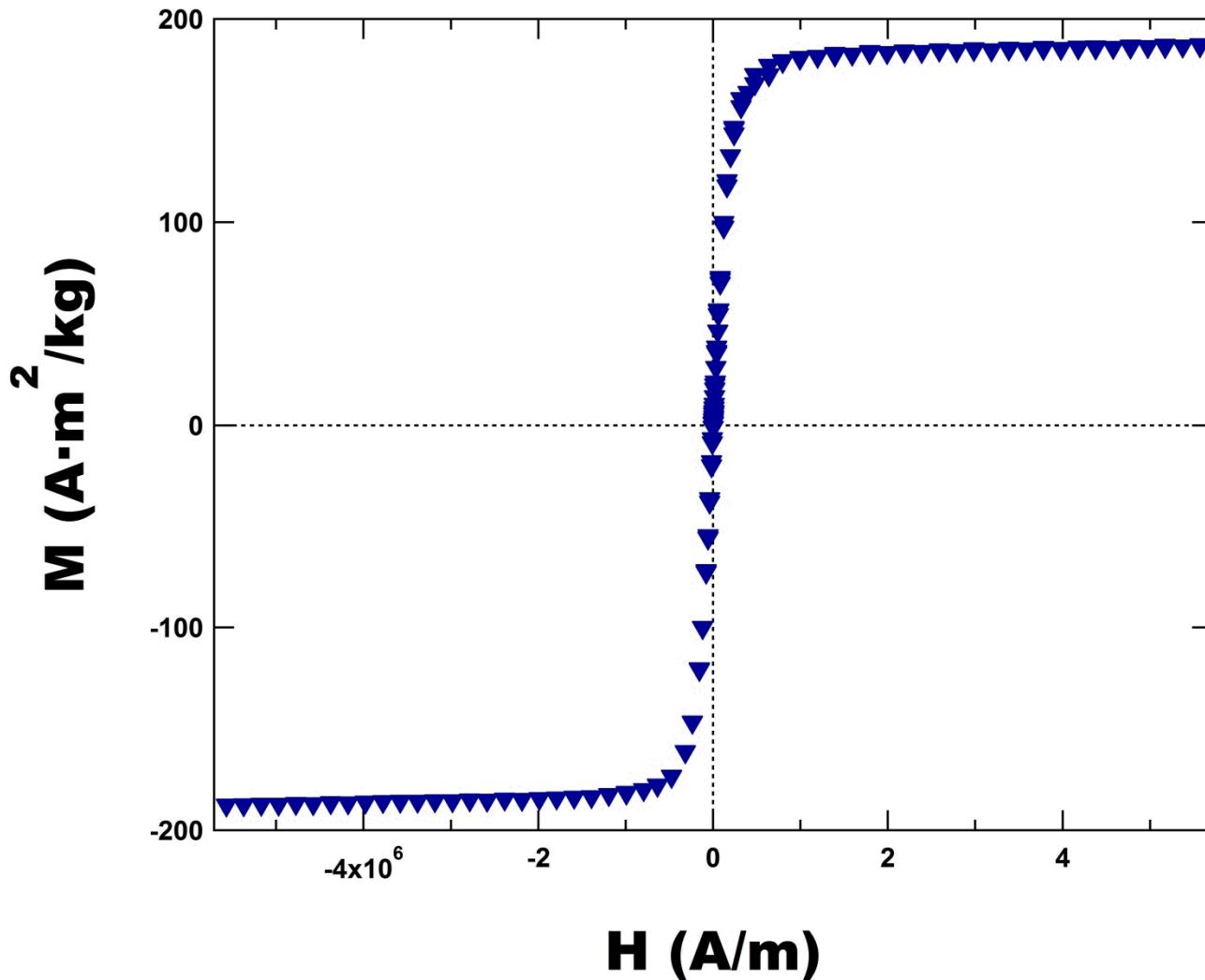


W/ milled FeN powder



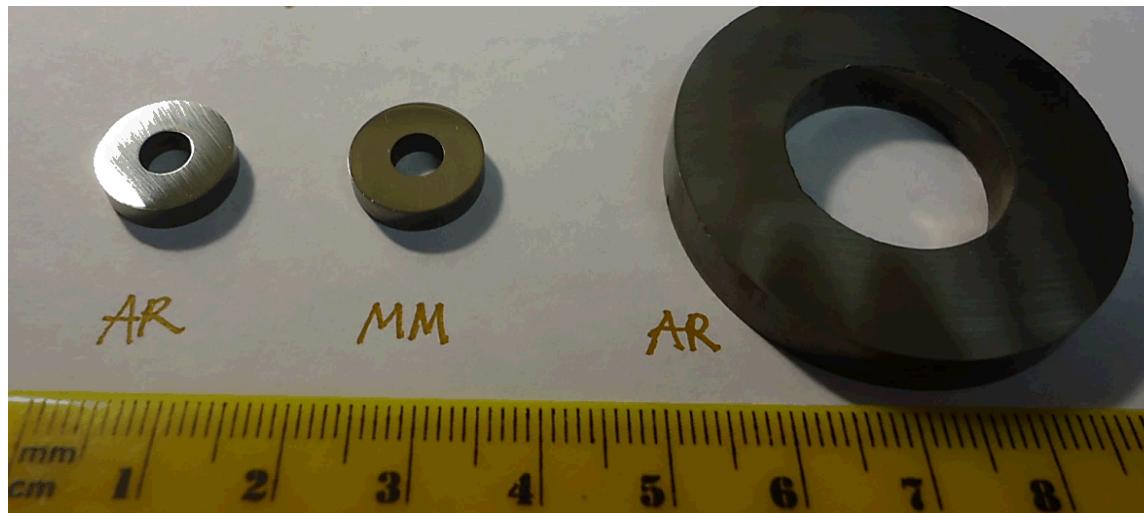
- **Milled FeN powder produces more uniform and dense SPSed billets**
 - Higher packing density with smaller particle size
 - Increased diffusion ability with smaller grain size of milled powder

Magnetic Characterization



- Fe_4N SPSed at 550°C and 100 MPa achieved an M_{sat} of $188 \text{ A}\cdot\text{m}^2/\text{kg}$.
- Predicted M_{sat} of bulk γ' - Fe_4N is $209 \text{ A}\cdot\text{m}^2/\text{kg}$ (Fe is $217 \text{ A}\cdot\text{m}^2/\text{kg}$)
- Negligible coercivity

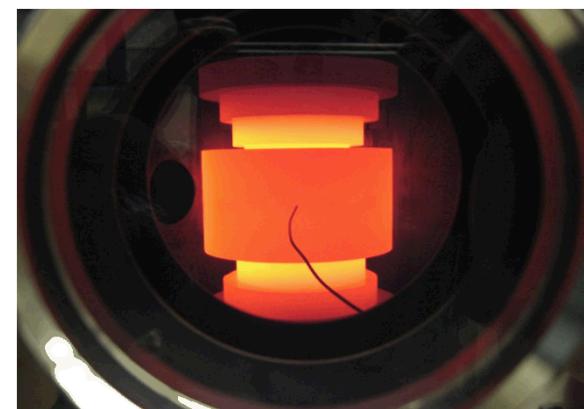
Net-Shaping of Transformer Cores



- Can sinter toroids and other shapes directly (net-shaping)
- Eliminates the need for machining
- Toroids being wound and tested

γ' -Fe₄N Conclusions

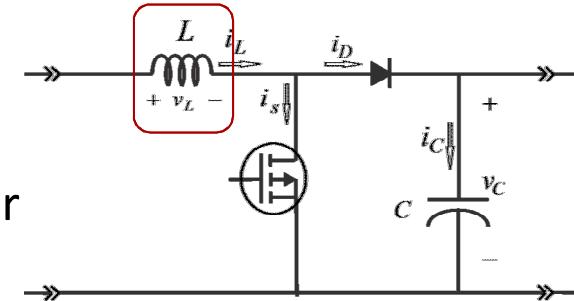
- γ' -Fe₄N has the potential to serve as a new low cost, high performance transformer core material
 - $M_{sat} > \text{Si steel}$
 - Increased current and field (and therefore power) carrying capability
 - Resistivity 200X greater than nanocrystalline and amorphous alloys
 - Only requires low cost and abundant elements (Fe & N)
 - High temperature (T) operation complementing Sandia development of high T capacitors and WBG semiconductors
- The fabrication of bulk γ' -Fe₄N using SPS has been demonstrated
 - SPS can consolidate iron nitrides without material decomposition
 - Parts can be fabricated directly using net-shaping



Another interesting approach for soft magnetic composites

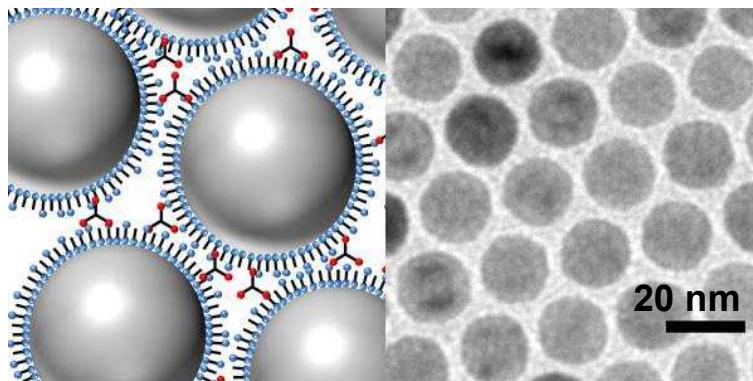
Develop new inductor materials made from superparamagnetic nanoparticle composites

- Eliminates main loss mechanisms: hysteresis and eddy cur
- Inductors can be “tailor made” (i.e. 3D printed)
- Achieve $B_{\max} > 1.0$ T at 10 MHz



The S&T Challenges

- Magnetic nanoparticle size will need to be tightly controlled to eliminate hysteresis
- Material will need to be optimized for flux density/rad-hardness



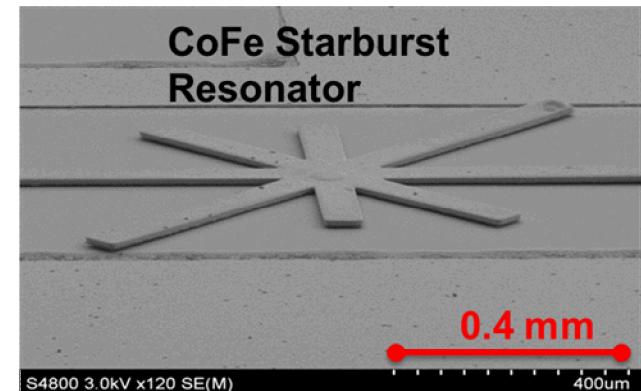
All particles magnetize at the same rate, allowing maximization of magnetic saturation with zero magnetic hysteresis.

- New Synthesis and Characterization tools offer a fresh perspective towards generating new magnetic device materials for a wide variety of emerging needs
- R&D and Technological Maturation needs create an opportunity for creative partnerships between National Labs like SNL with academic, government lab and industry partnerships

Future:

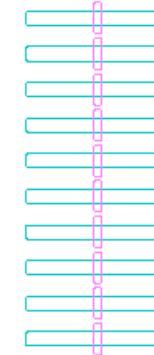
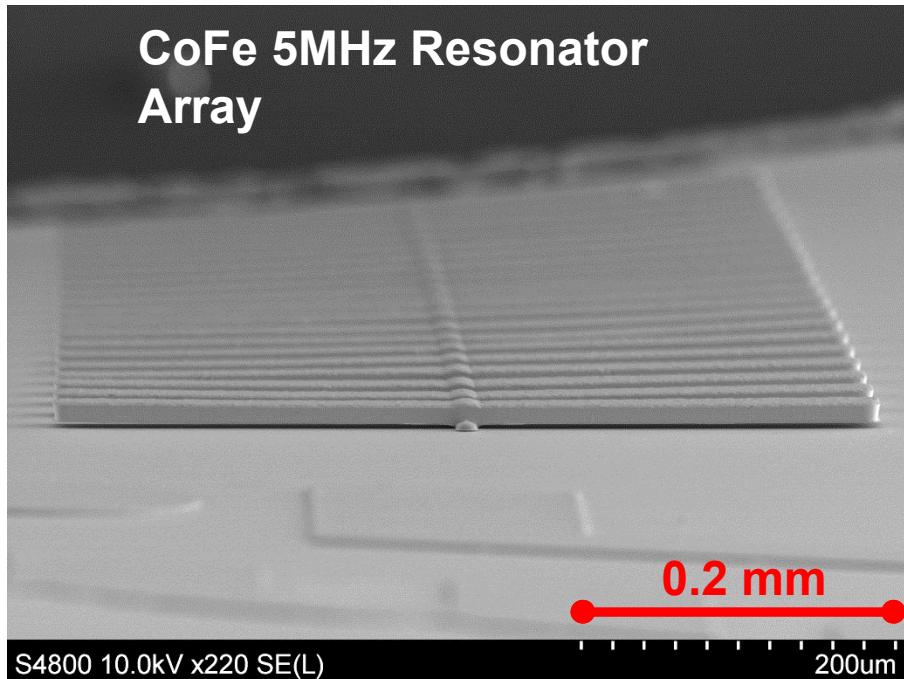
- Advances in Electrodeposited Magnetic Materials for Compact MEMS Magnetoelastic Resonators and Magnetostrictive Sensors
- Magnetic Josephson Junction Device Materials for enabling superconducting electronics (for Beyond Moore's Law)

2.4 mm long freestanding resonator



**Multi-Frequency Micro Resonator,
"Starburst Pattern"**

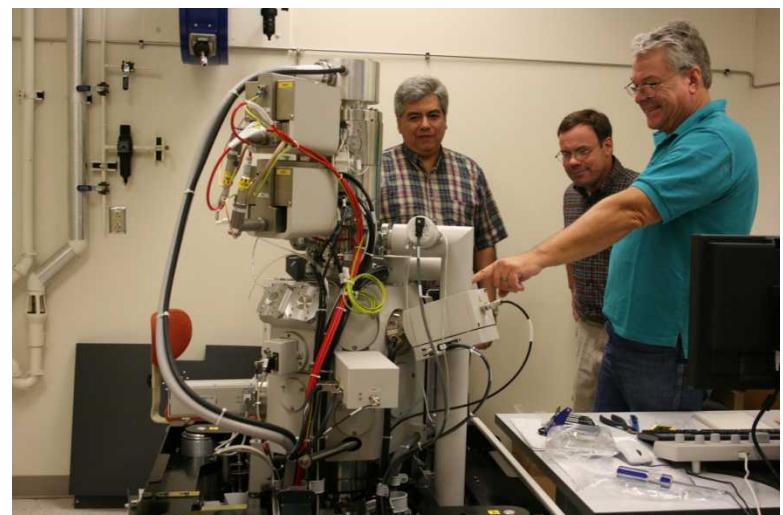
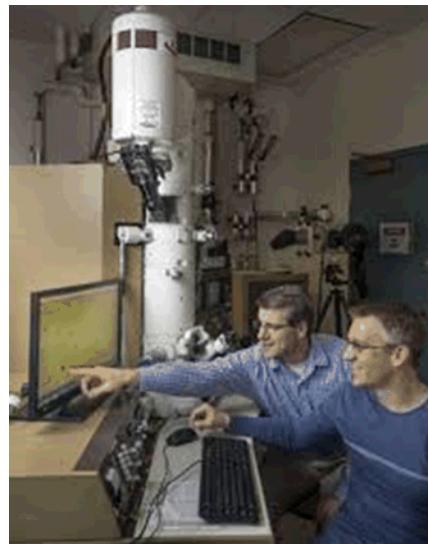
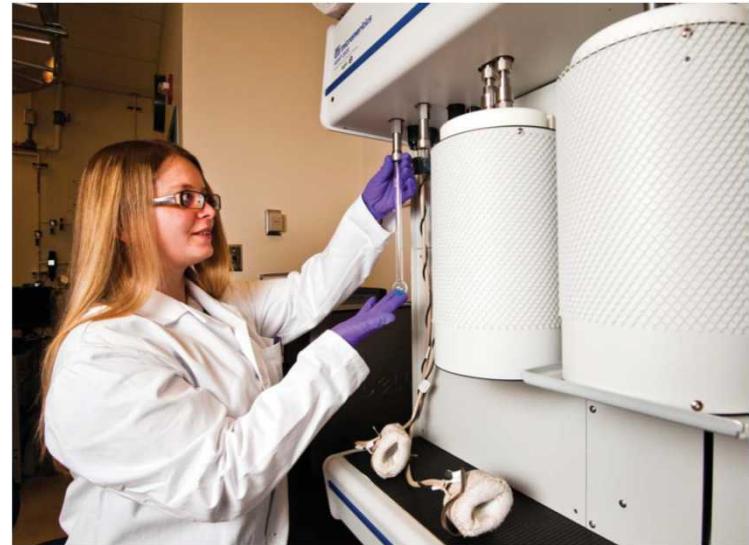
First ever electroplated CoFe micro-resonators



$L=0.5\text{mm}$: $PL=25\mu\text{m}$

- Resonator arrays increase device signal amplitude
- Via proper design resonators can measure a host of environmental parameters
- Temperature, pressure, current, gases, stress/strain, angular position, and many more!

Questions?



Back Up Slides

Sandia's Governance History & Structure



GOCO: Government owned, contractor operated



Sandia Corporation

- AT&T: 1949–1993
- Martin Marietta: 1993–1995
- Lockheed Martin: 1995–2017
- NTESS (Honeywell): 2017–present



research and development center

Sandia's Mission Has Evolved



1950s

Production
engineering &
manufacturing
engineering

1960s

Development
engineering

1970s

Multiprogram
laboratory

1980s

Research,
development and
production

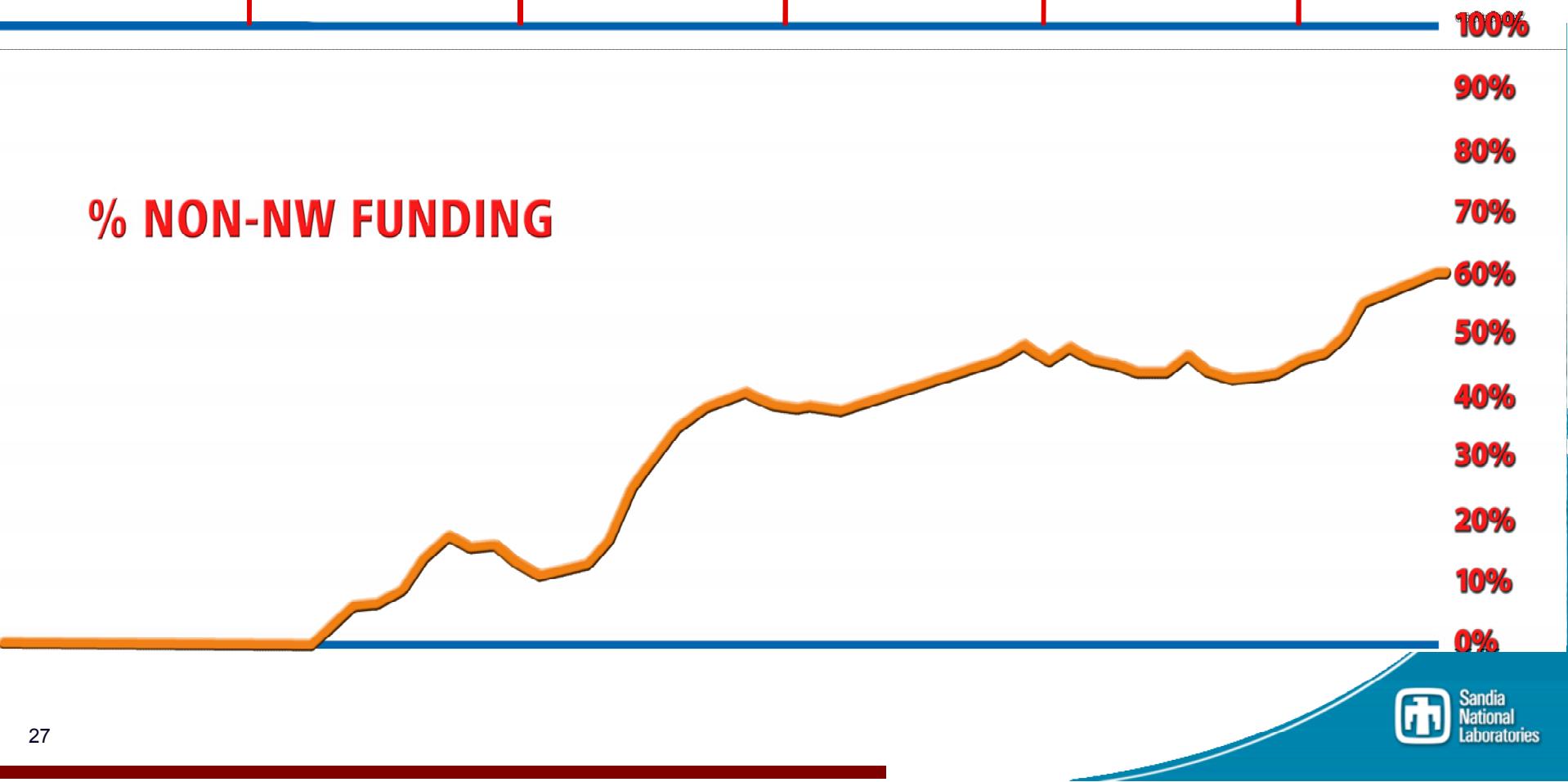
1990s

Post-Cold War
transition

2000s

Broader national
security challenges

% NON-NW FUNDING



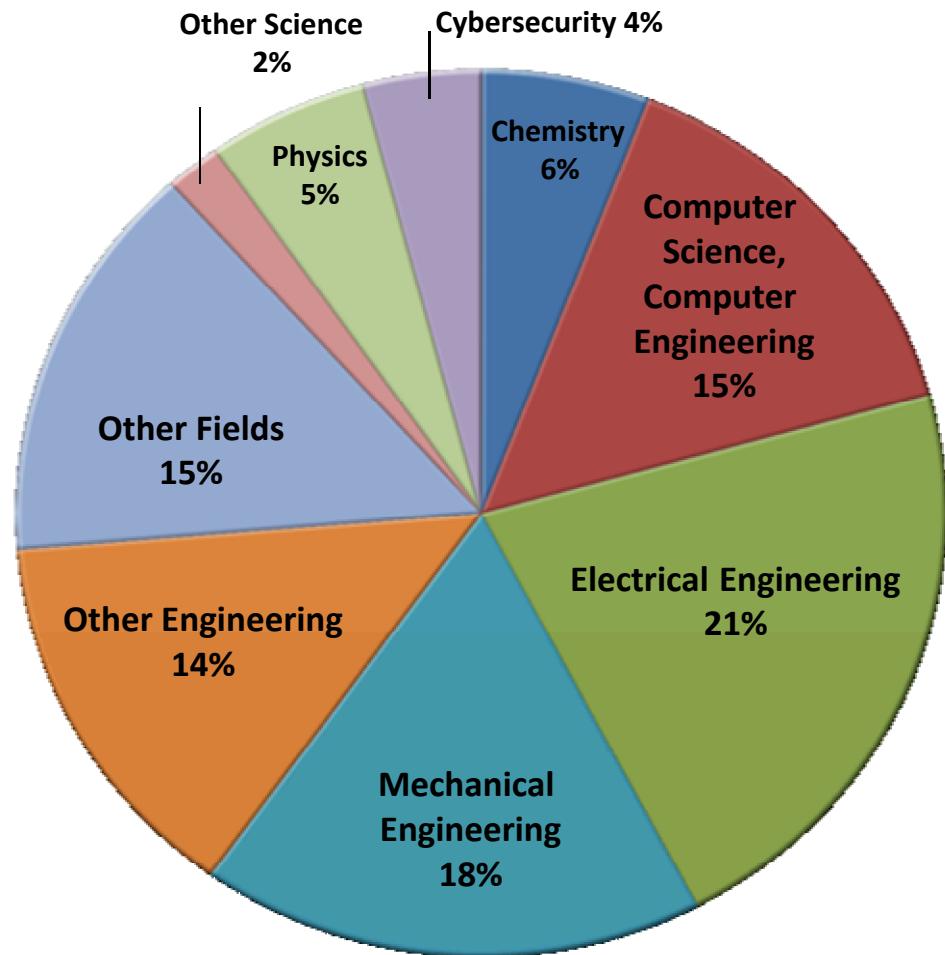
Sandia's Workforce

- On-site workforce: 11,711
- Regular employees: 9,494
- Advanced degrees: 5,330

Data as of April 22, 2014



R&D staff (5,000) by discipline



General SNL Career Categories Engaged in Science and Engineering



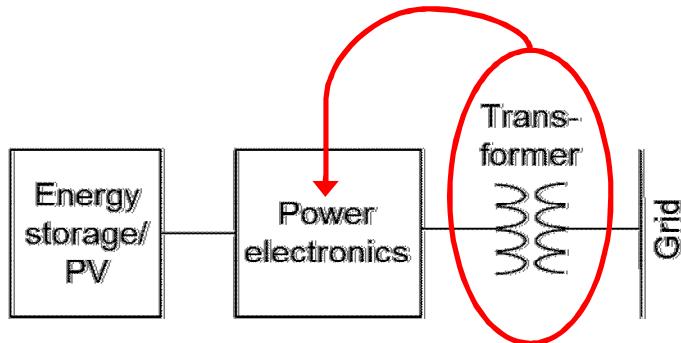
Researchers:

- Technical Staff – generally PhD (sometimes MS in mission application areas) Scientists and Engineers who take leadership roles in defining R&D
- Technologists – HS, associates degree, bachelors degrees and masters degree educated people in technical areas who support Technical Staff
- Postdocs – temporary (2-3 years), sometimes are not US citizens
- Undergraduate and Graduate Student Interns (summer and year round, US citizens)
- Visiting Faculty

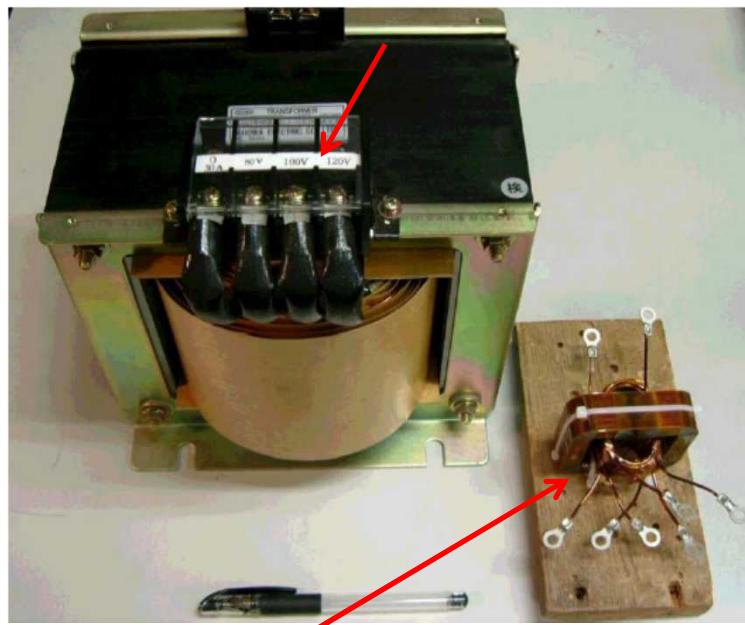
Research Managers – usually PhD educated, often promoted from experienced technical staff; responsible for enabling the technical staff and setting coherent “big picture” research directions

Sandia targets the “best and the brightest” for technical staff, i.e. the top 10% of all college graduates. GPA’s must be $\geq 3.0/4.0$. Scientific leadership and initiative is desired as much as teamwork and good human interaction skills.

Benefits of a High Frequency Transformer



Line frequency (50 Hz) transformer



High frequency (20 kHz) transformer

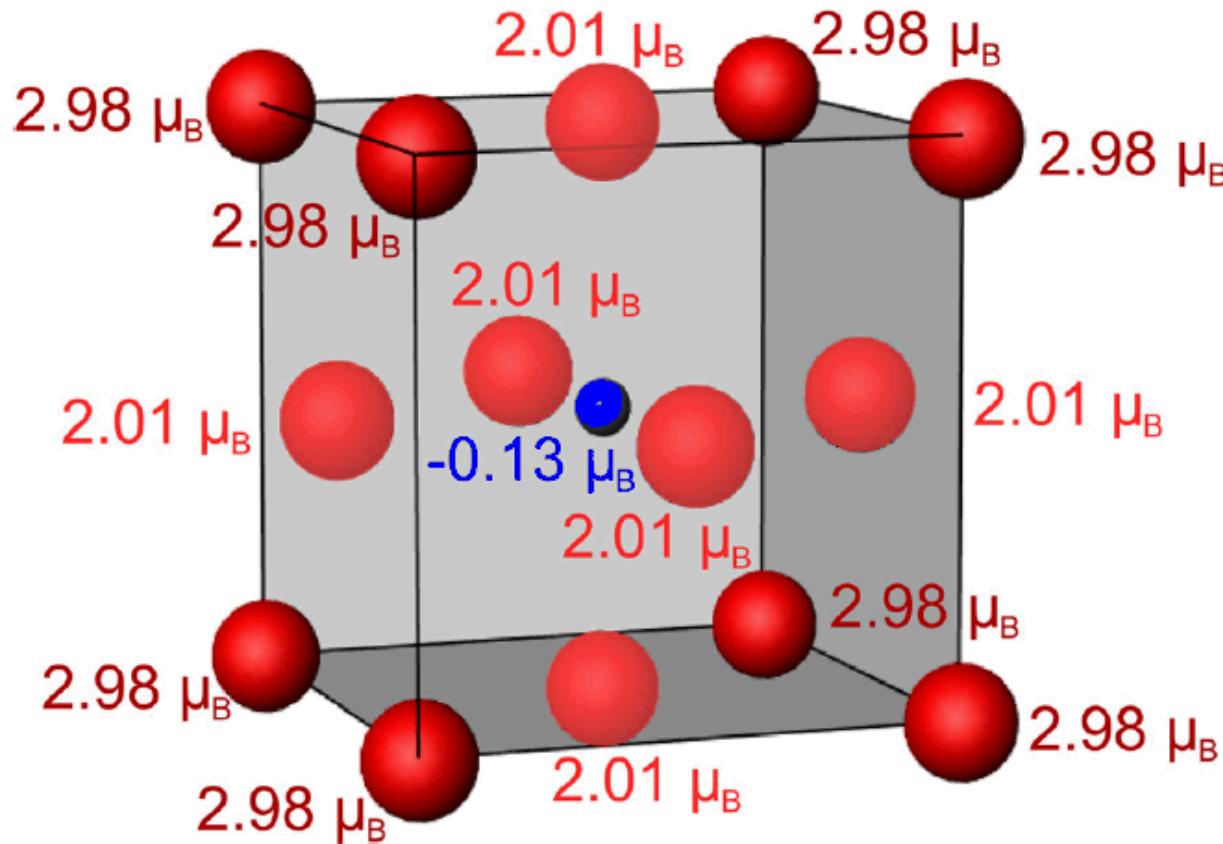
- Integrate output transformer within power conversion electronics
- Leverage high switching speed, voltage, and temperature performance of WBG semiconductors
- Transformer core materials for high frequency transformers have been an afterthought (no current material meets all needs)

Material requirements:

- Low loss in 10-200 kHz frequency range
- High permeability (low coercivity)
- High saturation magnetizations
- Low magnetostriction
- High temperature performance

Scalable & affordable

γ' -Fe₄N Unit Cell



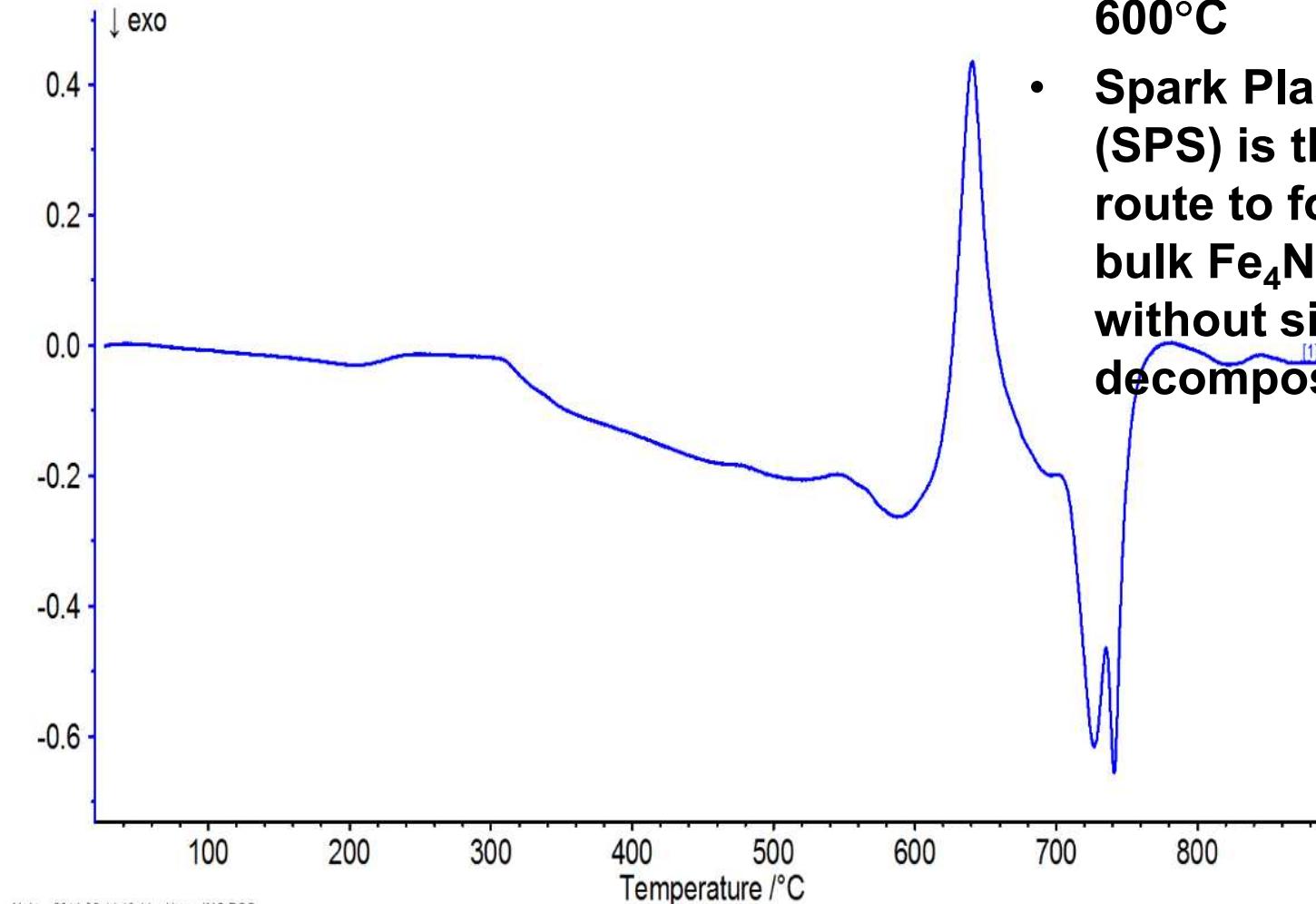
fcc γ Fe structure stabilized by interstitial nitrogen in the body center

G. Scheunert, et al., A review of high magnetic moment thin films for microscale and nanotechnology Applications, *Appl. Phys. Rev.*, 3, 011301 (2016).

J.M.D. Coey, *Magnetism and Magnetic Materials* (Cambridge University Press, Cambridge, UK, 2012).

Differential Scanning Calorimetry (DSC) of Fe_4N

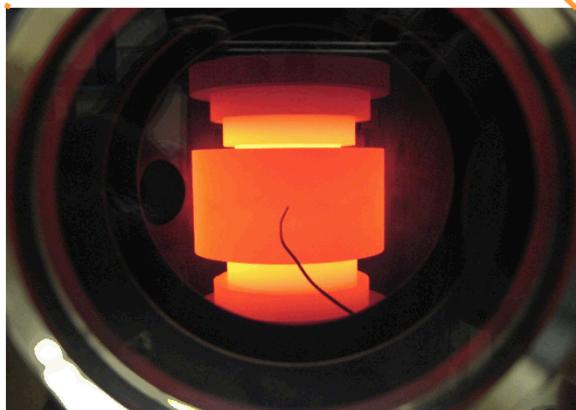
DSC /(mW/mg)



- Decomposition of sintered FeN begins $\approx 600^\circ\text{C}$
- Spark Plasma Sintering (SPS) is the only viable route to form fully dense bulk Fe_4N samples without simultaneous decomposition

Spark Plasma Sintering (SPS)

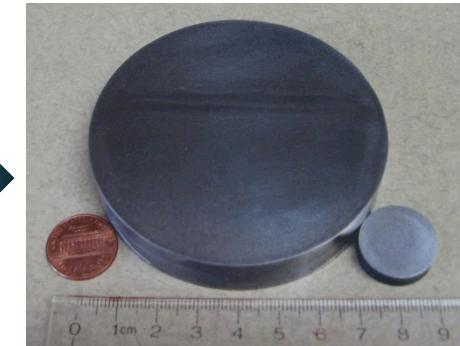
SPS Model: SPS-825S Dr. Sinter® at UC Irvine



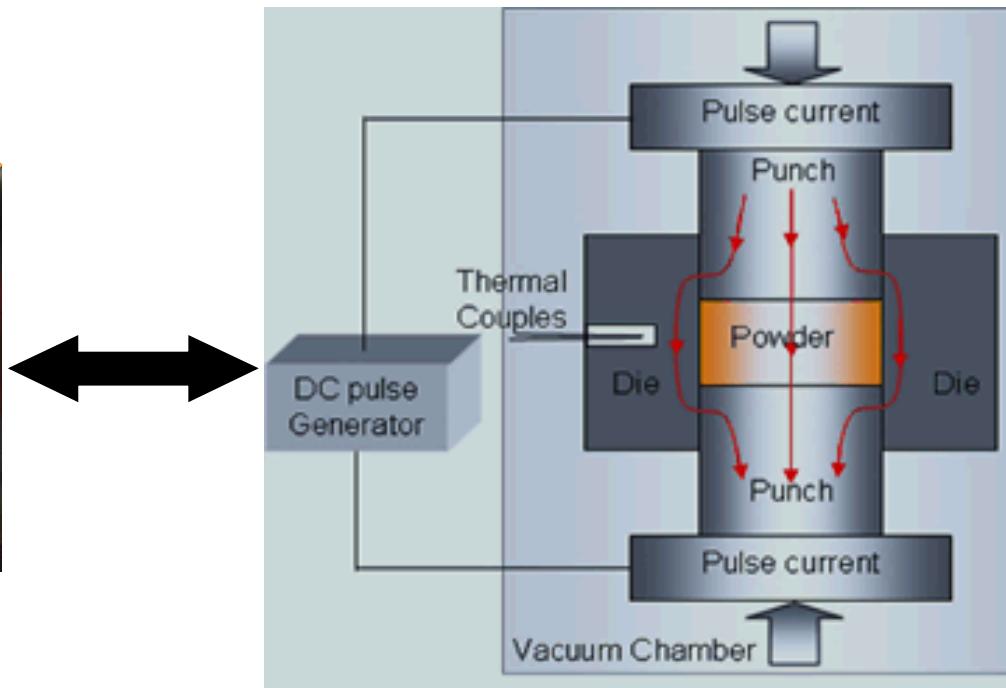
SPS
Chamber



Starting Powder in Die

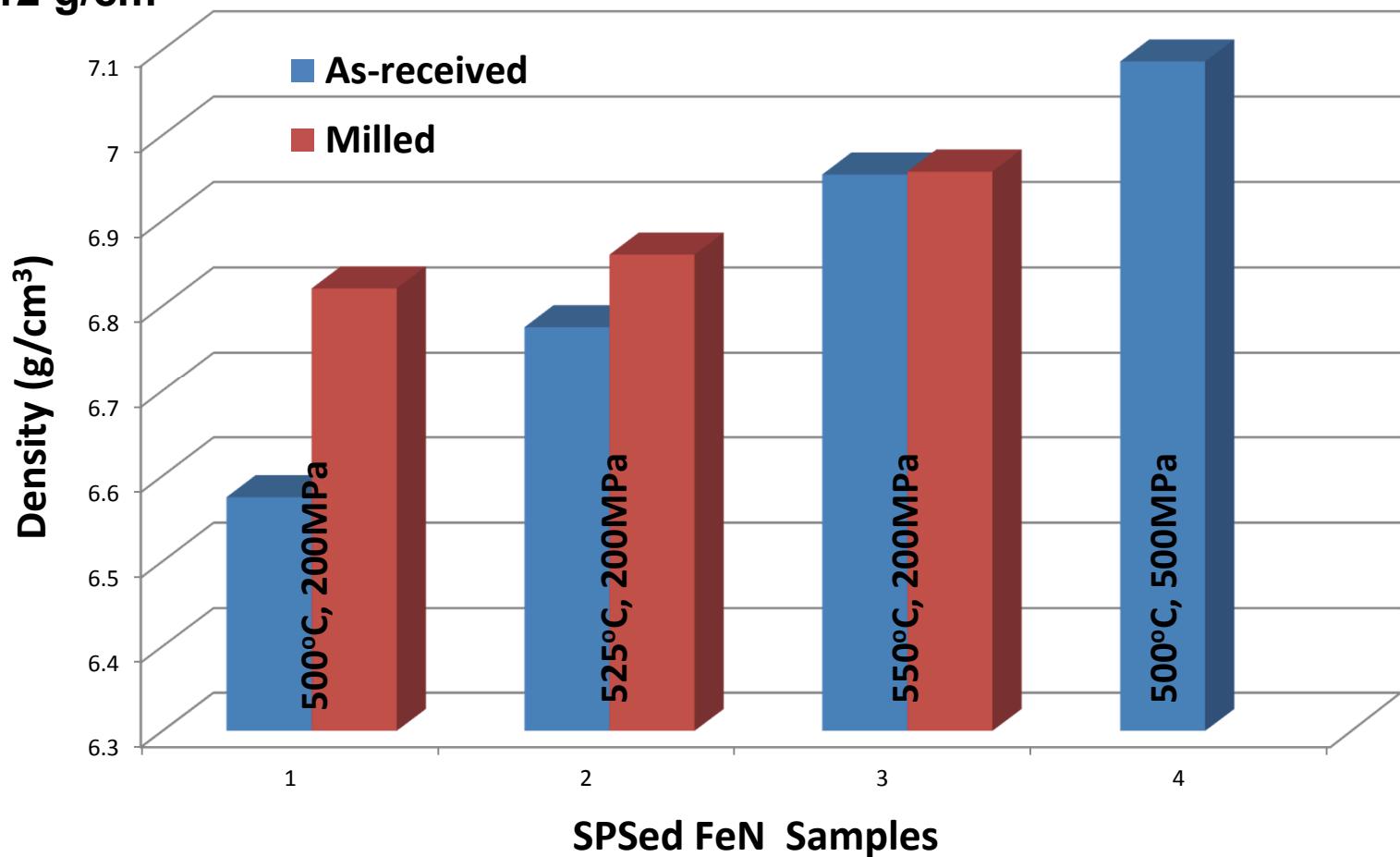


End Product



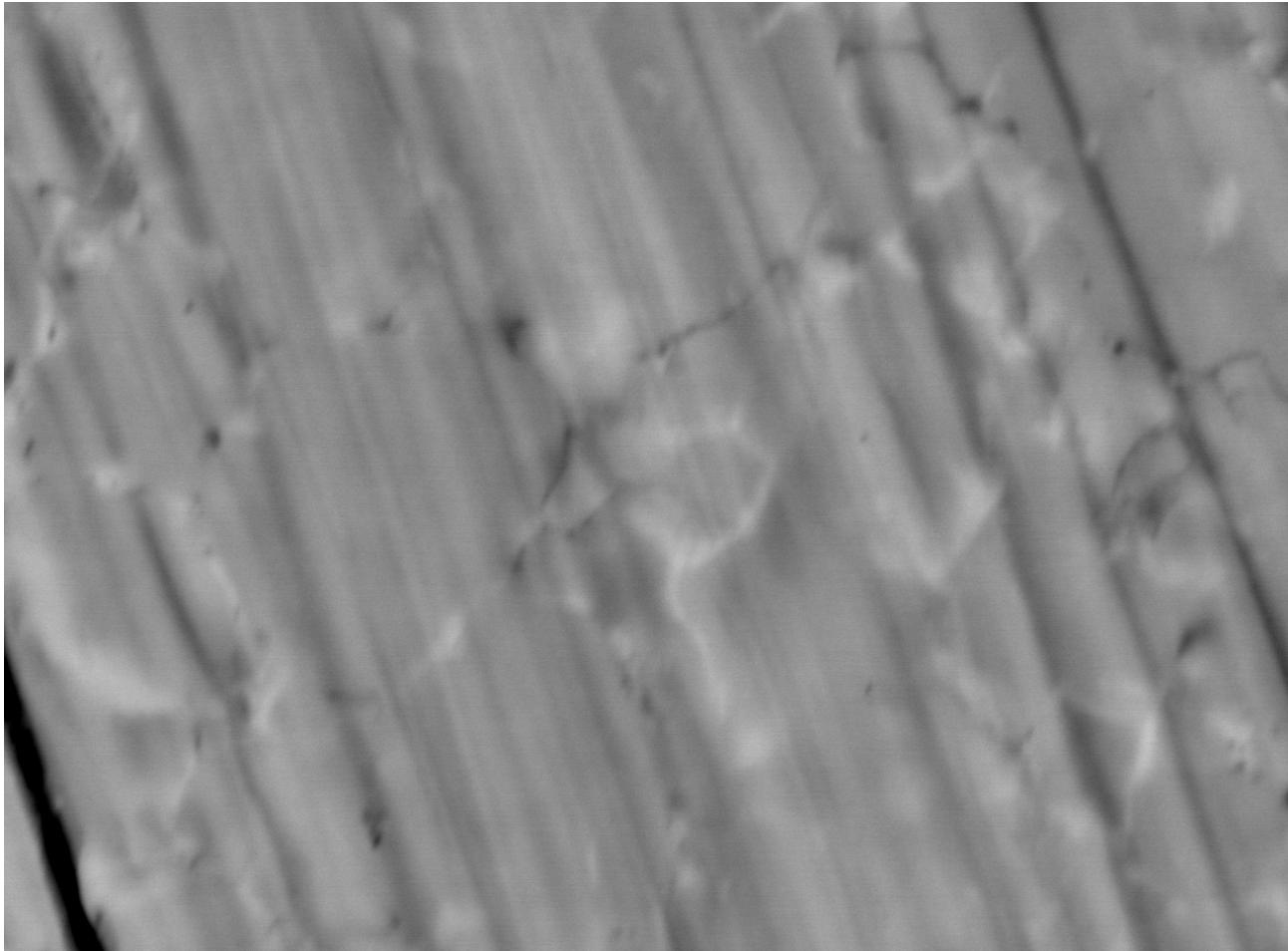
Density of SPSed Fe_4N samples

$$\rho_{\text{theory}} = 7.212 \text{ g/cm}^3$$



- Density increases with increasing SPS temperature and pressure
- Higher degree of variation in SPSed samples using as-received powder
- Milling improves density and uniformity

Toroid Surface SEM and EDS



x 10,000

20.0kV COMPO

1
NOR

JEC
WIL

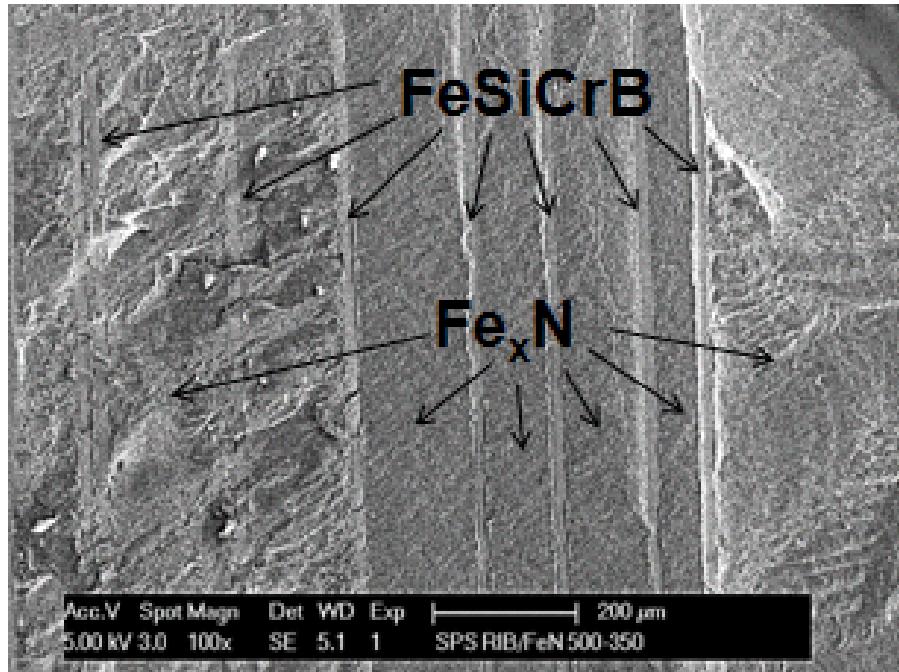
11/10/2014
11.0mm 11:08:26

- Small variation in composition between grain boundary and center
- Grain center stoichiometry \approx Fe_4N
- Grain boundary is \approx 3 Atomic% richer in iron

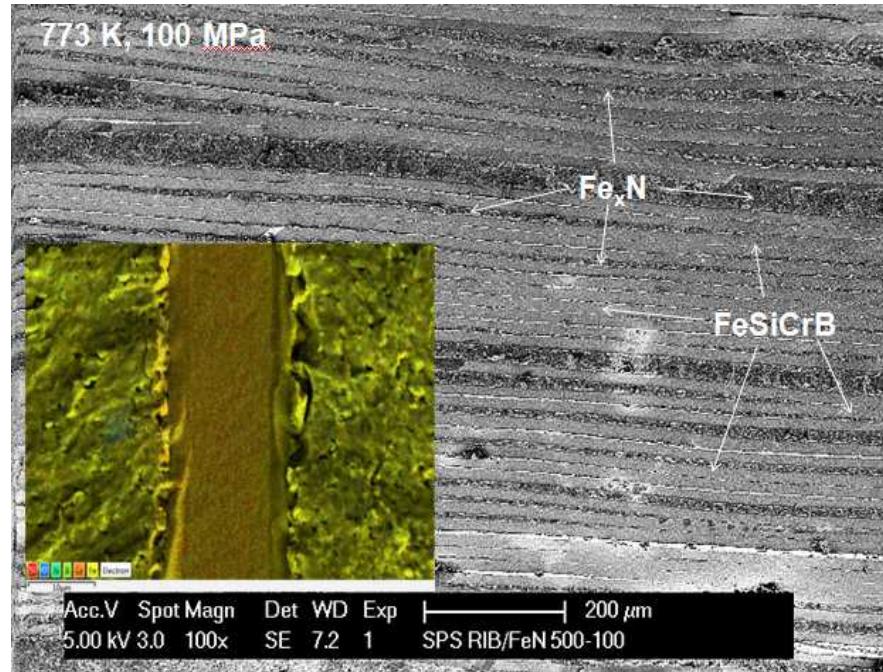
*SEM/EDS analysis
completed by Dick
Grant (SNL)

Location	Fe (Atomic %)	N (Atomic %)
Grain center	81.3	18.7
Grain boundary	84.2	15.8

SEMs of FeSiCrB and Fe_xN composites

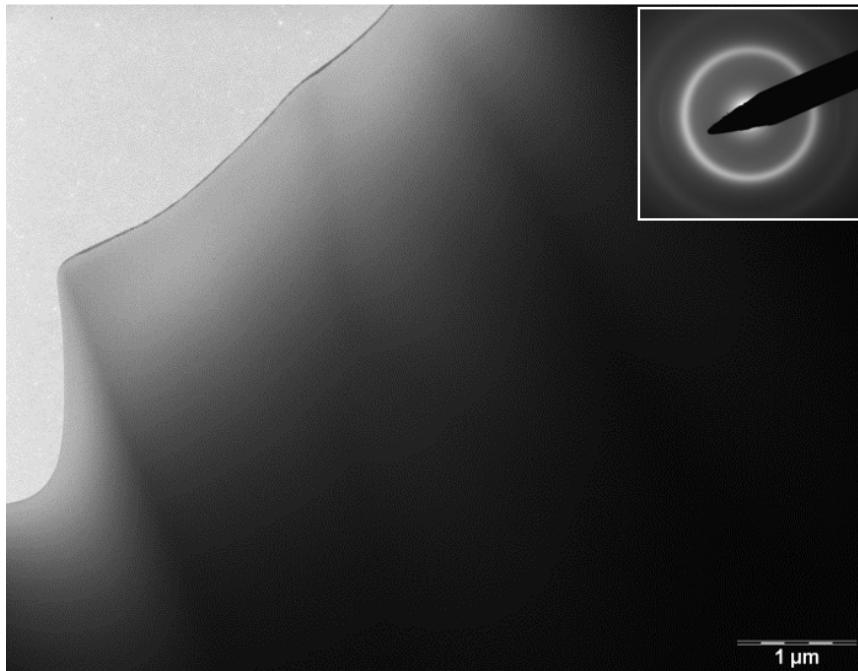


10 vol% FeSiCrB ribbon

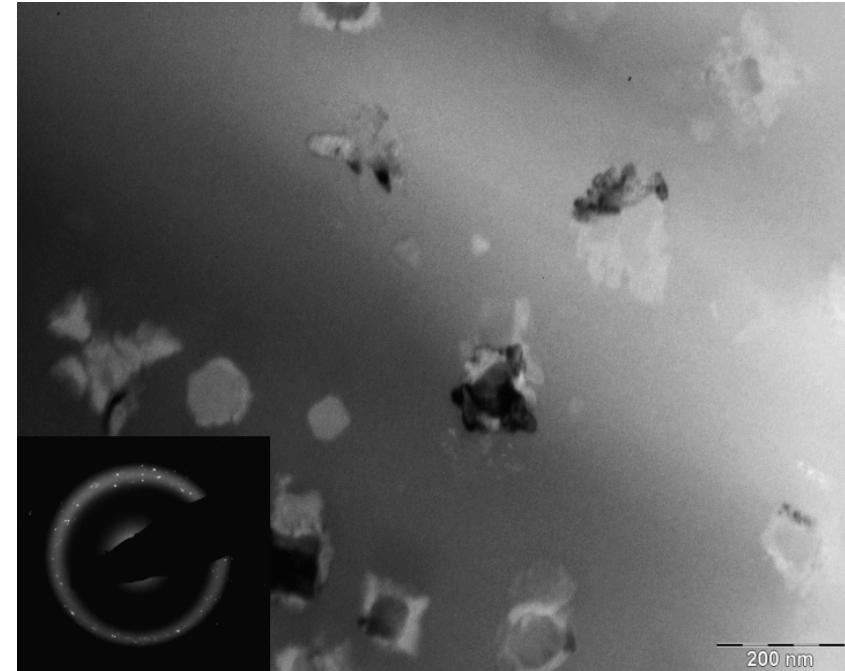


90 vol% FeSiCrB ribbon plus
EDS mapping (inset)

TEMs of FeSiCrB before and after sintering

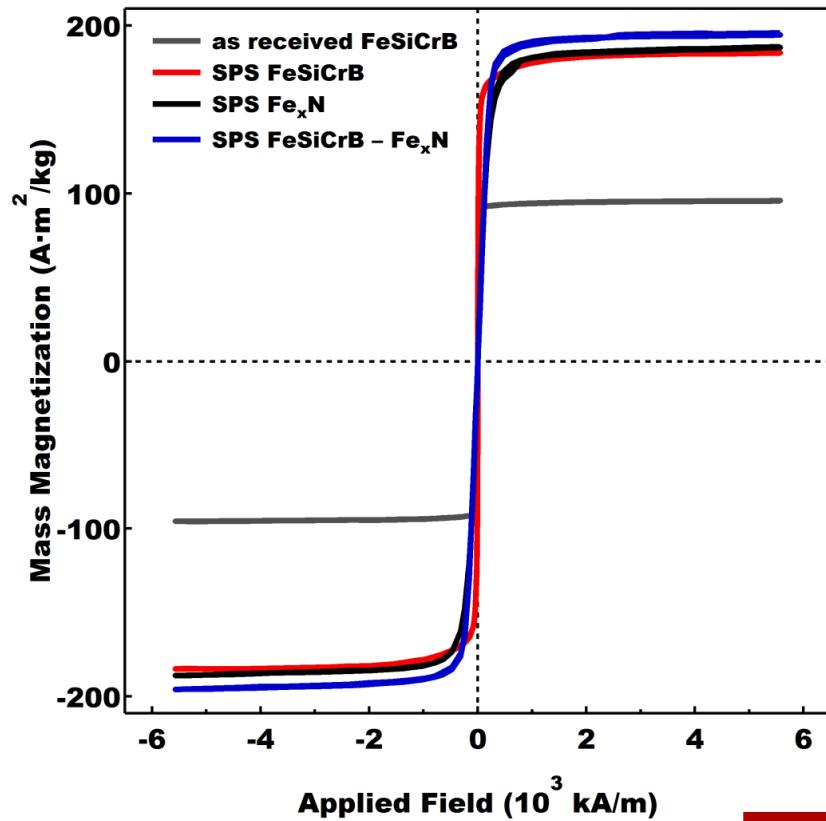


Before SPS



After SPS

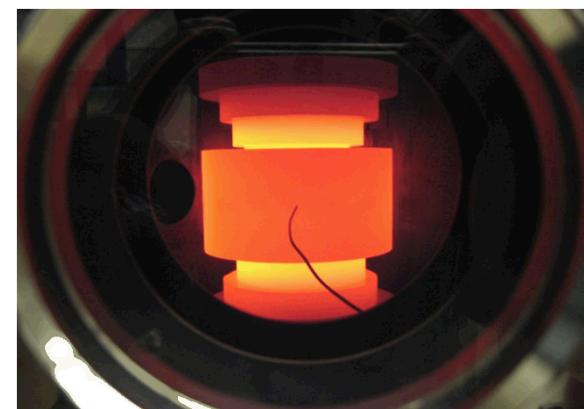
Composite DC Magnetic Response



Sample	M_{sat} ($\text{A}\cdot\text{m}^2/\text{kg}$)
As received FeSiCrB ribbon	96.0
SPSed FeSiCrB ribbon	185.3
SPSed Fe_xN	188.0
SPSed FeSiCrB- Fe_xN	196.5

γ' -Fe₄N Conclusions

- γ' -Fe₄N has the potential to serve as a new low cost, high performance transformer core material
 - $M_{sat} > \text{Si steel}$
 - Increased current and field (and therefore power) carrying capability
 - Resistivity 200X greater than nanocrystalline and amorphous alloys
 - Only requires low cost and abundant elements (Fe & N)
 - High temperature (T) operation complementing Sandia development of high T capacitors and WBG semiconductors
- The fabrication of bulk γ' -Fe₄N using SPS has been demonstrated
 - SPS can consolidate iron nitrides without material decomposition
 - Parts can be fabricated directly using net-shaping



2017 Spring MRS Symposium

Outline

- **Synthesis of bulk γ' -Fe₄N soft magnetic materials**
 - Why soft magnetic materials are important
 - History of soft magnetic materials & current state of the art
 - γ' -Fe₄N R&D
- **Highly magnetostrictive electrodeposited CoFe materials and devices**
 - New electrodeposition chemistry
 - “Dumb” vs. smart tags and sensors
 - First ever electroplated CoFe micro-resonators

Magnetostriuctive materials: Current state of the art & limitations



- Terfenol-D, terbium, iron, and dysprosium
 - Highest known magnetostriction at about 2000 microstrains ($\lambda_s = 2000\text{ppm}$)
 - Difficult manufacturing process and expensive due to rare earth materials
 - Poor piezomagnetic coefficient – high bias and AC field needed
- Galfenol, gallium alloyed with iron ($\lambda_s \sim 400\text{ppm}$)
 - Difficult to electrodeposit and large intrinsic stress
 - Gallium salts for electrodeposition expensive
 - $\text{Ga}_2(\text{SO}_4)_3$ at \$138 for 5g
- Cobalt and iron (CoFe) can be formed into a magnetostrictive alloy with common stoichiometries of 50% cobalt with 50% iron and 70 to 75% cobalt and 25 to 30% iron
 - Theoretical saturation magnetostriction of $\lambda_s \approx 1000 \text{ ppm}$
 - CoSO_4 at \$2.10 for 5g
- Metglas
 - Only commercially available material and therefore used in a lot of current device work
 - Three alloys: 2826MB, 2605SA1
 - $\lambda_s = 12 - 27 \text{ ppm}$

New method to electrodeposit CoFe

Improvements over existing electrodeposition methods

- New Fe cation source
- Oxygen scavengers
- Grain refiners, levelers
- Surfactant
- Pulsed plating

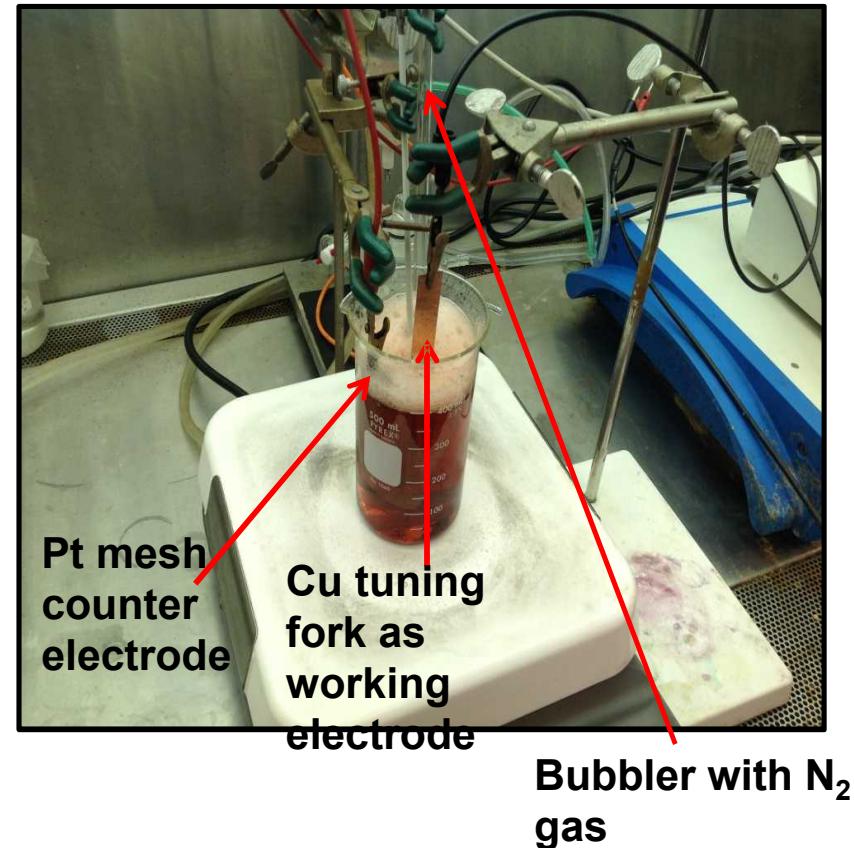
Example of previous work:

Osaka, T.; Yokoshima, T.; Shiga, D.; Imai, K.; Takashima, K.
Electrochim Solid St 2003, 6, (4), C53-C55.

Our work:

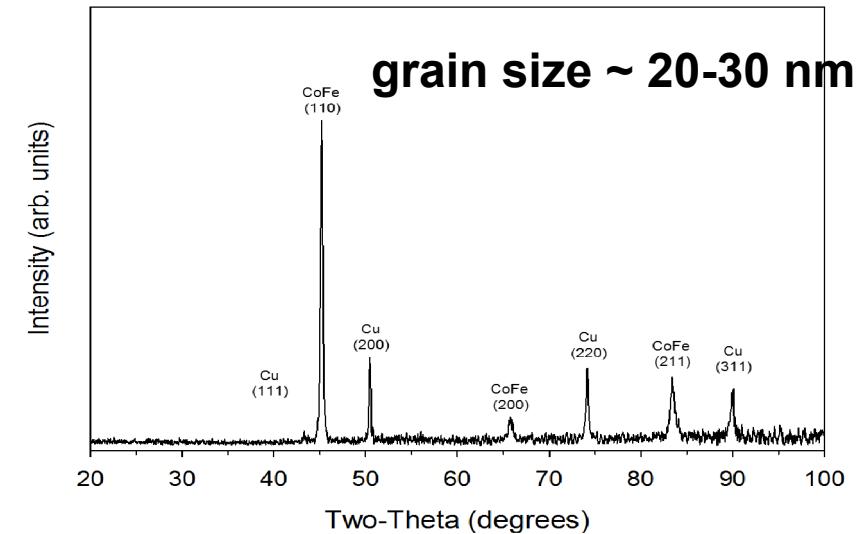
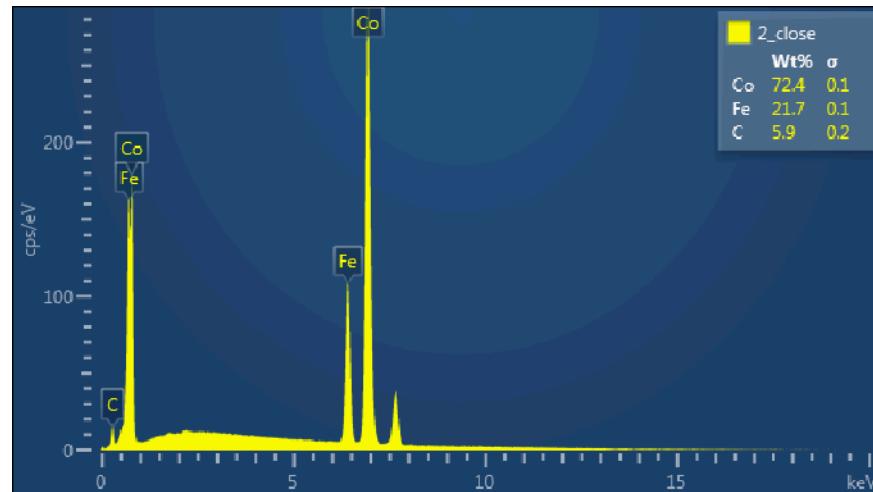
Jamin Pillars, Eric Langlois, Christian Arrington, Todd Monson, Andrew Hollowell, Mark Rodriguez, "Electrodeposition of a High Magnetostriction CoFe Film," to be submitted to *Electrochimica Acta*

Jamin Pillars, Eric Langlois, Christian Arrington, Todd Monson, "Electrodeposition Processes for Magnetostrictive Resonators," U.S. Patent Application #14876652, October, 2015.



High quality, low oxide (< 8 at%) CoFe films

- Achieving $\text{Co}_{0.7}\text{Fe}_{0.3}$ ratio reported to have “giant magnetostriction” by Hunter et al.*
 - As-sputtered films $\lambda_s = 84 \pm 5$ ppm
 - 800°C anneal and slow cool, $\lambda_s = 156 \pm 7$ ppm
 - 800°C anneal and quench, $\lambda_s = 260 \pm 10$ ppm
 - Anneal produced fcc (111) β -Co peak
 - (fcc+ bcc)/bcc phase boundary
- Note on limitations of sputtering
 - Line-of-sight deposition
 - Limited thickness (<2 micron) and high intrinsic stress
 - High temperature anneal would degrade CMOS devices
 - High cost and wasteful
 - Lack of anisotropic etch



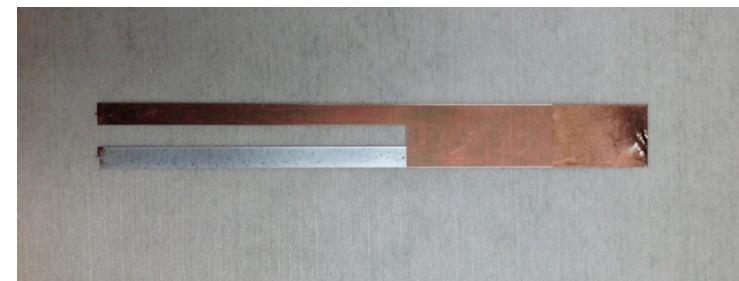
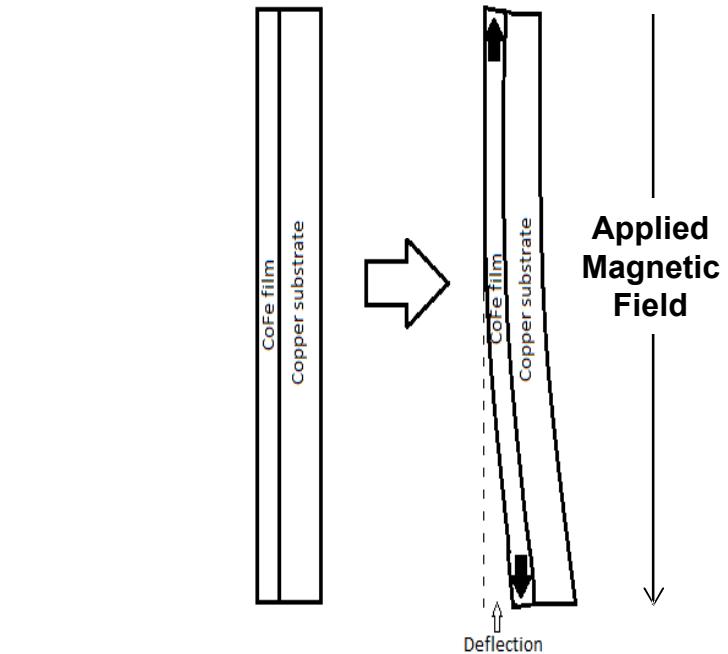
* Hunter, D., et al., *Giant magnetostriction in annealed Co(1-x)Fe(x) thin-films*. Nat Commun, 2011. 2: p. 518.

Novel rapid magnetostriction testing

- Klokholm (1976) observed deflection of bimorph when magnetized
- The expression du Tremolet de Lacheisserie and Peuzin is:

$$\lambda_{eff}(D_{sat}) = \frac{2(D_{\parallel} - D_{\perp})E_s t_s^2 (1 + \nu_f)}{9E_f L^2 t_f (1 + \nu_s)}$$

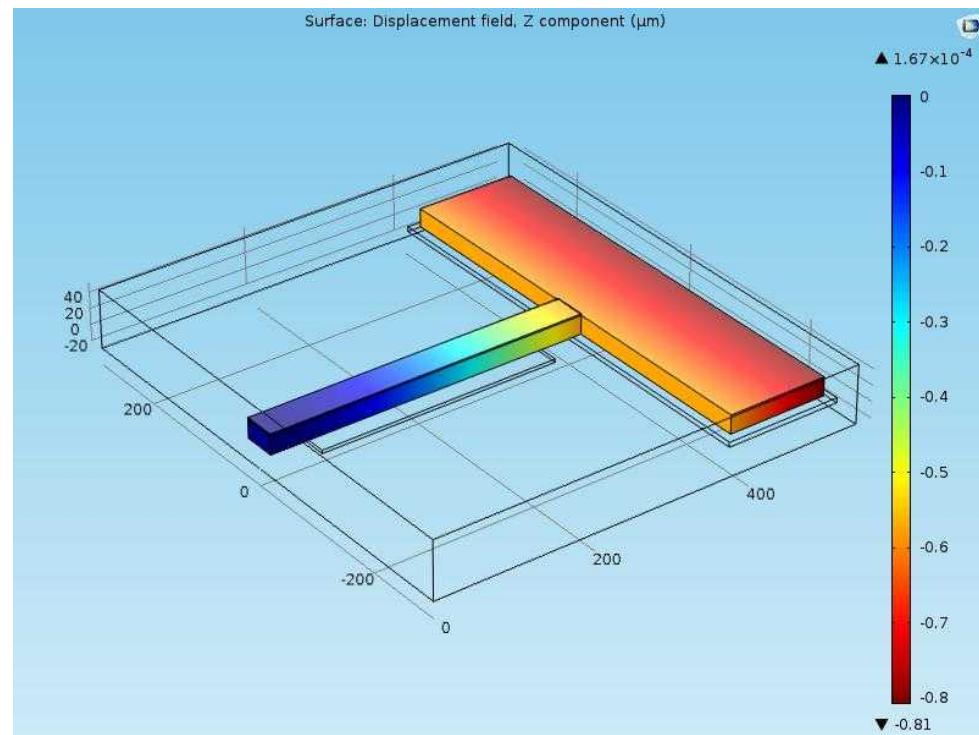
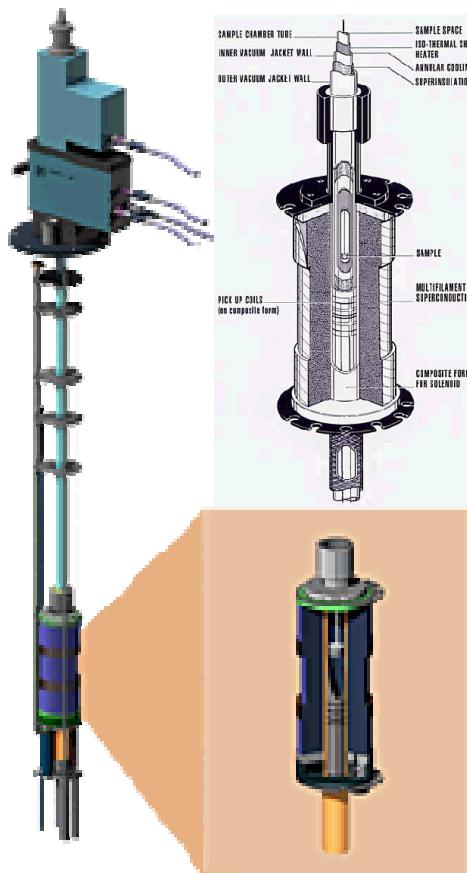
- Solenoid for *in situ* displacement measurements
 - Cu tuning fork substrate
- Calculated magnetostriction for CoFe compared with a Metglas standard



Calibrated solenoid used for testing

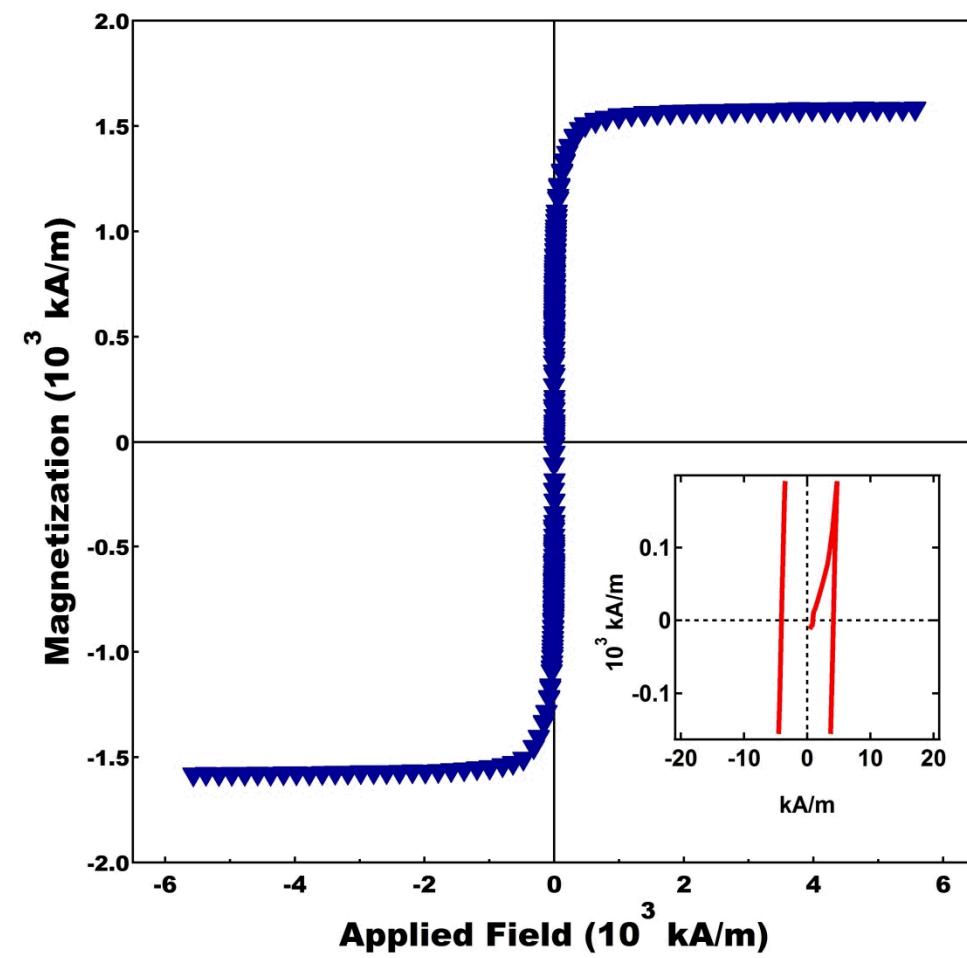
MEMS cantilever capacitors for λ_s measurement, coming soon to our lab

Quantum Design Magnetic Property Measurement System (MPMS) probe assembly



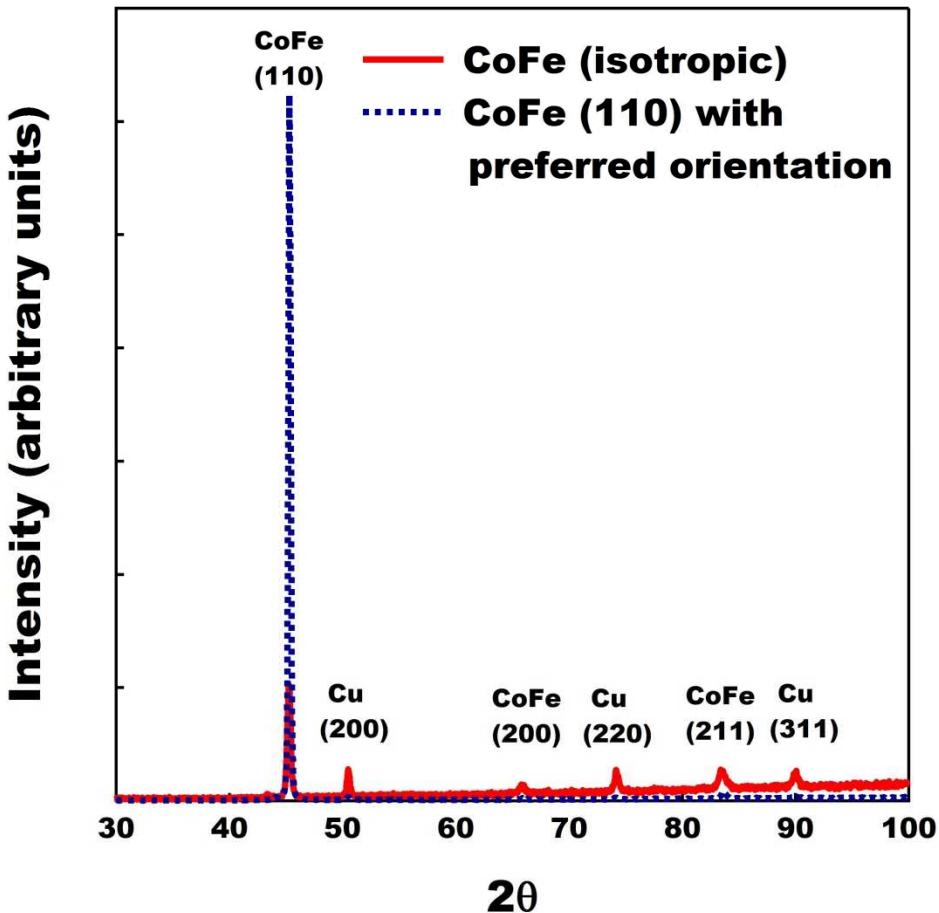
- Will enable more precise λ_s measurements
- Two orthogonal capacitors will allow for measurement of both D_{\parallel} and D_{\perp}

Electrodeposited CoFe magnetic properties



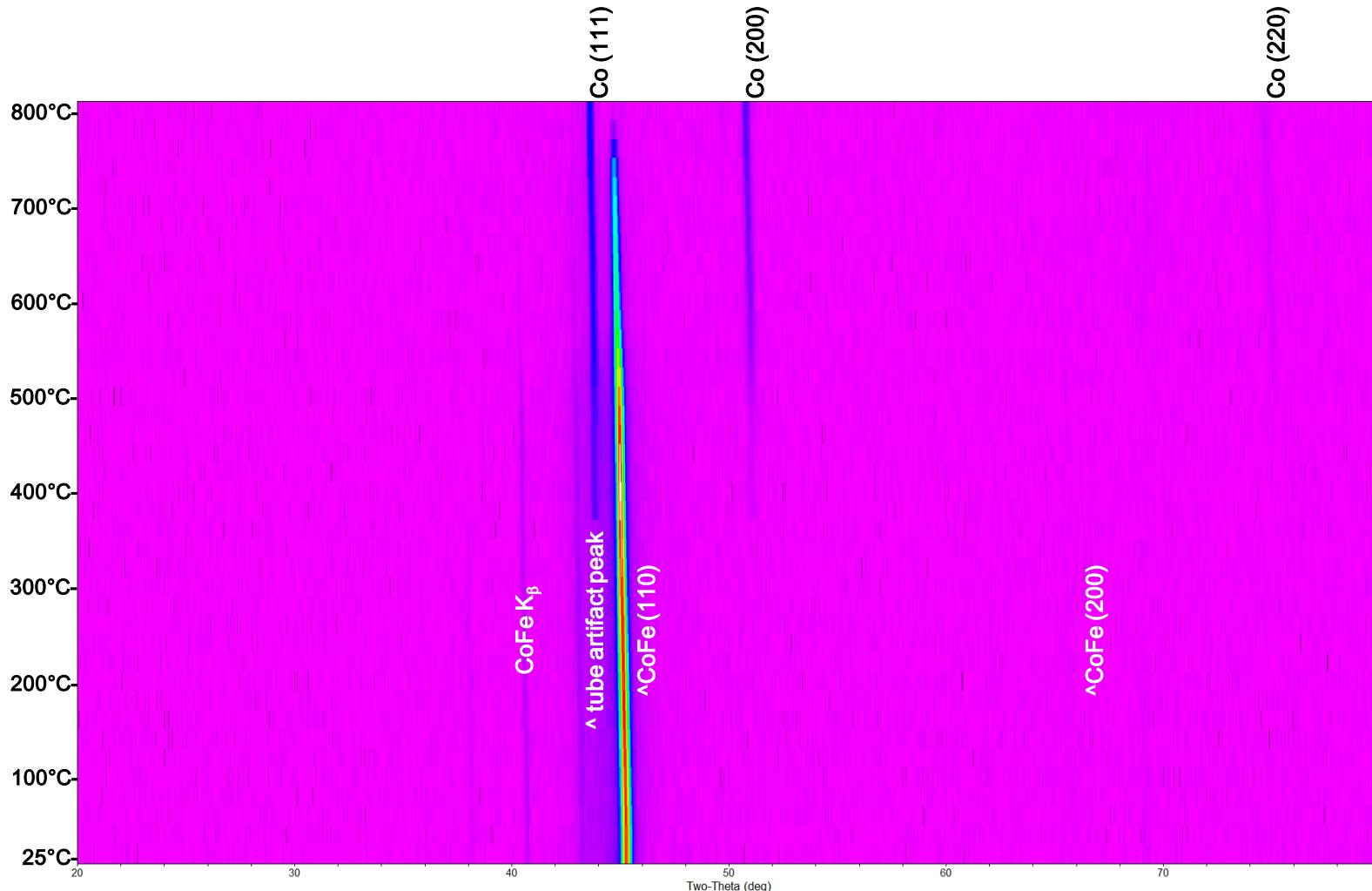
Sample	M_s (A/m)	H_c (A/m)	χ
CoFe	1.58×10^6	4.13×10^3	165.6
Metglas 2605SA1	1.07×10^6	1.16×10^3	140.8
Sample	λ_s (ppm)		
CoFe (isotropic)	172 ± 25		
CoFe (110) preferred orientation	229 ± 32		
Hunter et al. CoFe as-sputtered	84 ± 5		
Hunter et al. CoFe 800°C anneal and quench	260 ± 10		
Metglas 2605SA1	26 ± 4		

(110) preferred orientation



- Sample 1: isotropic CoFe
- Sample 2: CoFe with strong (110) out-of-plane preferred orientation
- Results in enhanced magnetostriiction
 - As reported on previous slide

HT XRD in gHe (ramped at 20° C/min)



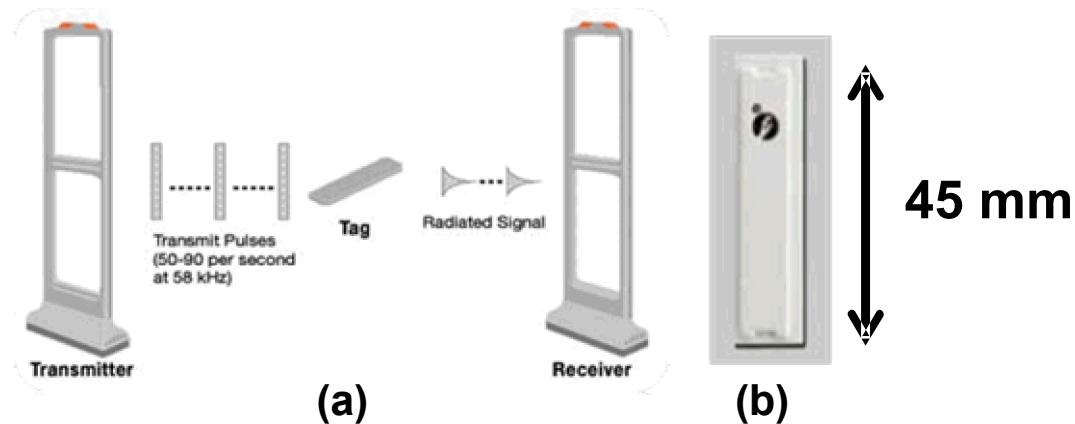
- **Separation of FCC Co > 350 °C**
- **We thank James Griego for collecting this data!**

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 - New electrodeposition chemistry
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 - First ever electroplated CoFe micro-resonators

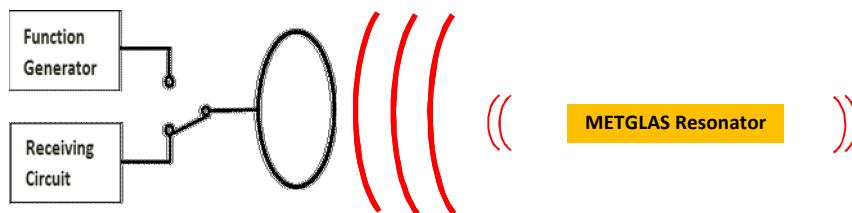
Magnetoelastic sensor overview

“Dumb



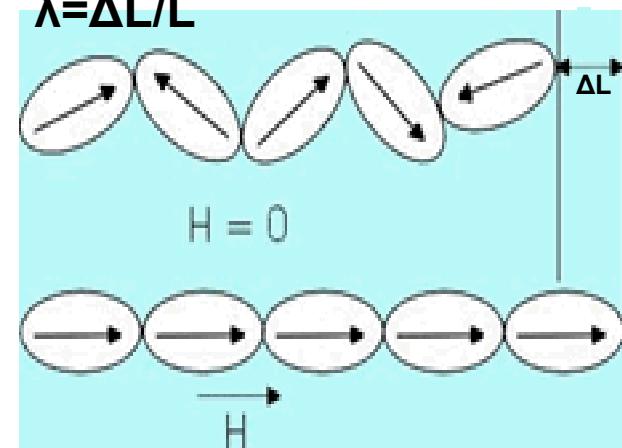
a) magnetic dipole antenna interrogation zone

b) magnetoelastic tag in plastic package



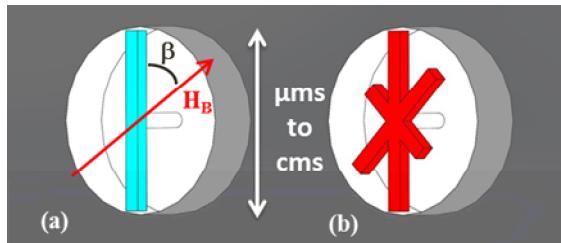
amorphous magnetic material such as METGLAS™ ($\text{Ni}_{40-50}\text{Fe}_{40-50}\text{Mo}_{5-10}\text{B}_{1-5}$)

Magnetostriction,
 $\lambda = \Delta L/L$



Magnetic Smart Tag (MaST)

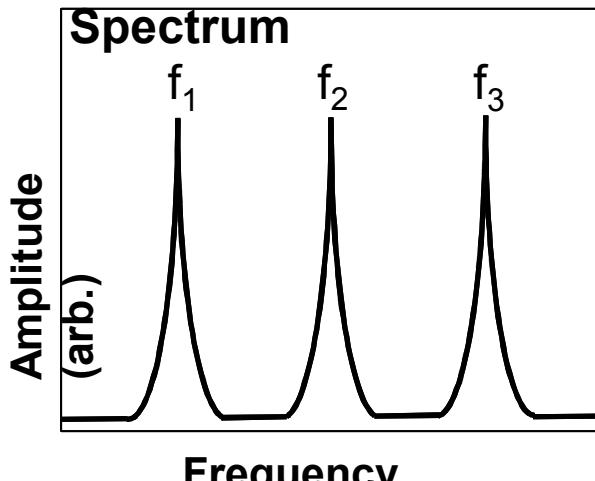
“Smart



- a) Single frequency resonator
- b) Multi-Frequency resonator (3)

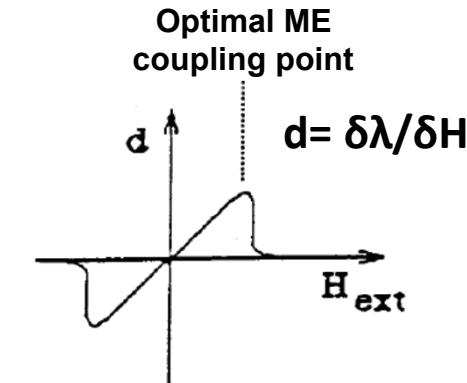
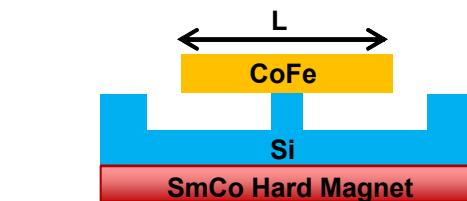
$$f_r = \frac{1}{2L} \left[\sqrt{\frac{\rho}{E_0} + \frac{9\lambda^2 s \rho ((|H_B| \cos(\beta))^2)}{J_s H_A^3}} \right]^{-1}$$

Multi-Frequency Spectrum

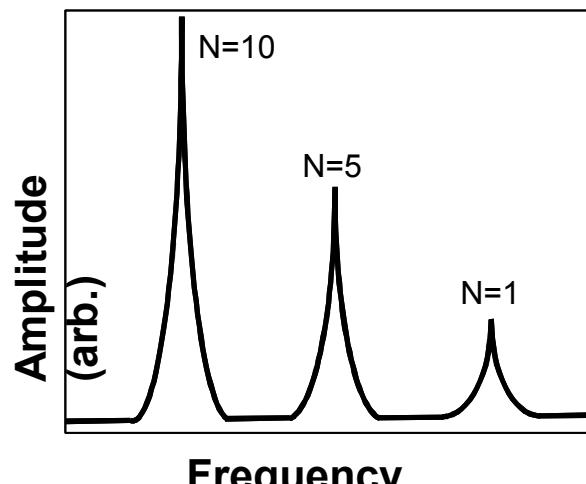


Peak frequency constitutes primary tag identity!

MagSens resonator cross section



Multi-Frequency/Multi-Amplitude Spectrum

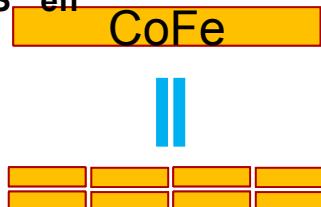


Relative amplitude constitutes secondary tag identity!

Signal strength is related to effective volume:

$$\Delta m = \chi H_{ex} V_{eff} <$$

$$M_s V_{eff}$$

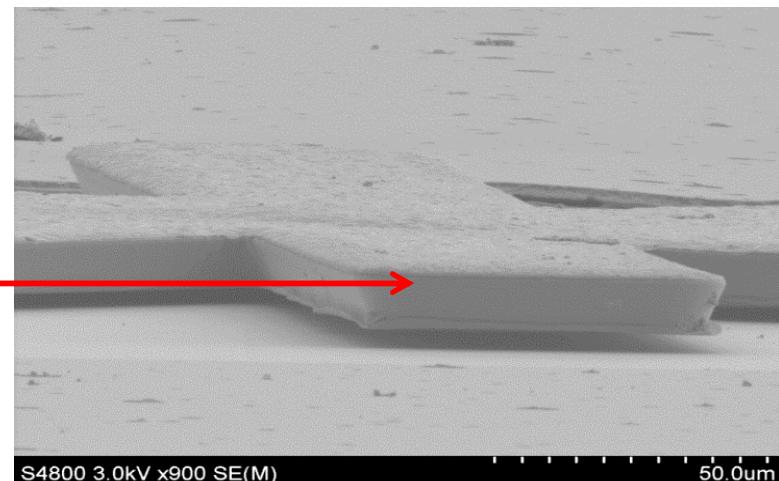
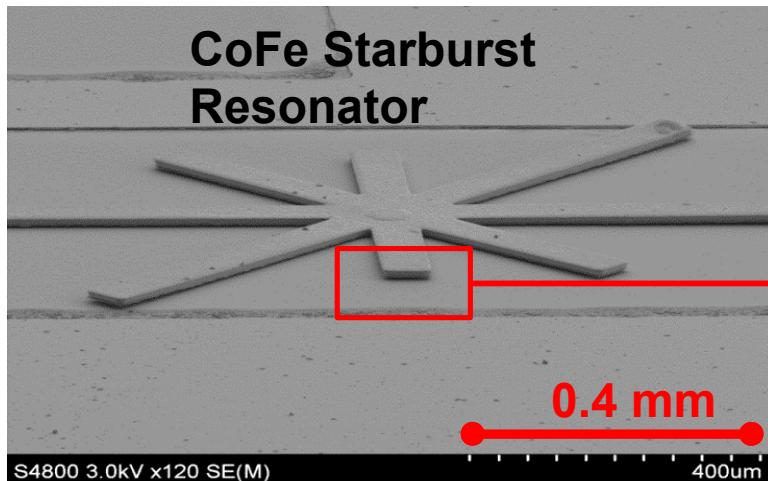


Outline

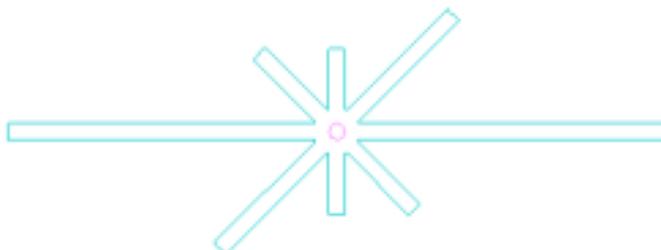
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First ever electroplated CoFe micro-resonators

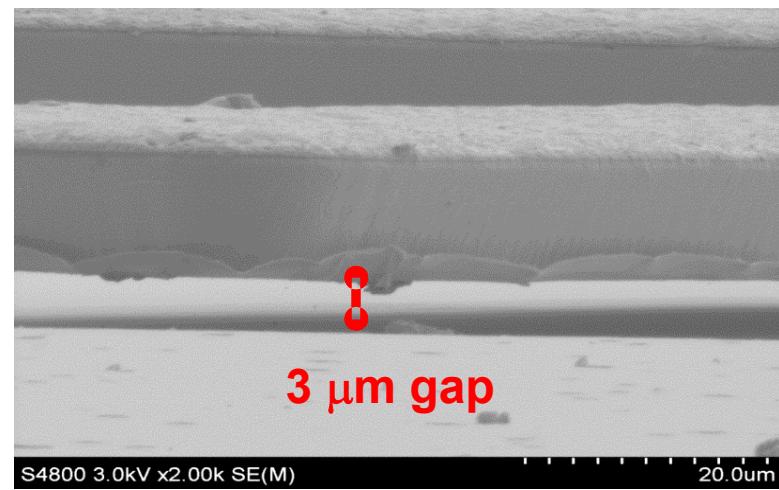
2.4 mm long freestanding resonator



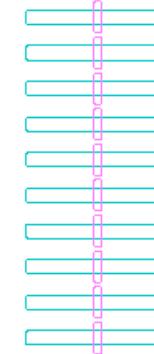
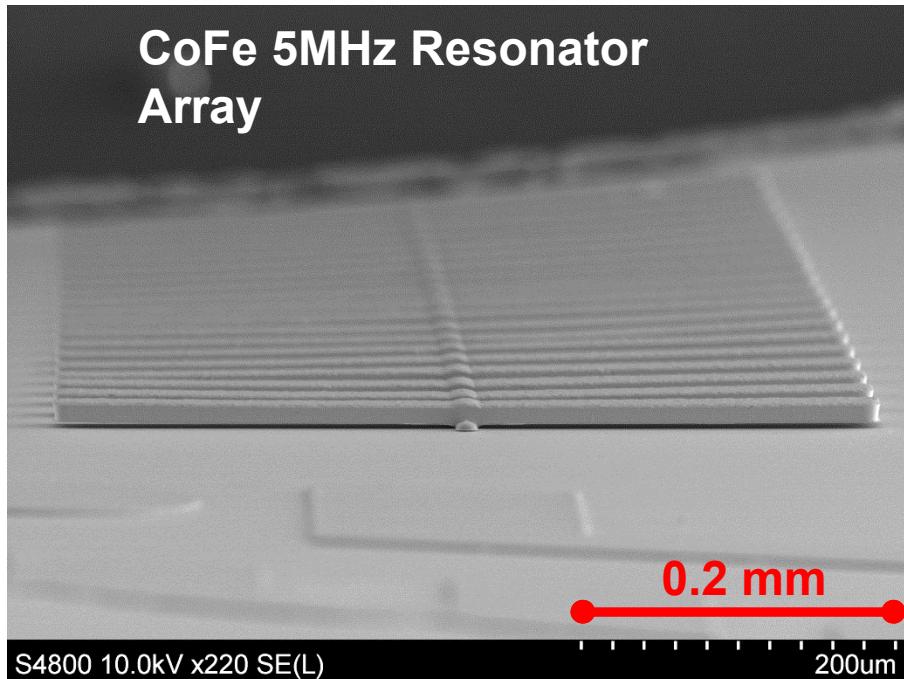
Multi-Frequency Micro Resonator,
"Starburst Pattern"



$L=0.6\text{mm}-2.4\text{mm}$



First ever electroplated CoFe micro-resonators



$L=0.5\text{mm}$: $PL=25\mu\text{m}$

- Arrays of resonators increase signal amplitude
- Via proper design resonators can measure a host of environmental parameters
- Temperature, pressure, current, gases, stress/strain, angular position, and many more!

Electrodeposited CoFe Conclusions

- New method to electrodeposit thick (10+ μm), low oxide (< 8 at%) low stress, highly magnetostrictive CoFe
 - $\lambda_s = 229 \pm 32$ ppm for CoFe with (110) out-of-plane preferred orientation
 - Significantly exceeds λ_s of Metglas 2605SA1 and is comparable to CoFe sputter deposited by Hunter et al.
 - U.S. patent application (#14876652) filed
 - Electrodeposited CoFe bypasses issues associated with sputtering and avoids high cost and manufacturing challenges of Terfenol-D and Galfenol
- First ever free standing CoFe micro-resonators demonstrated
- MEMS CoFe resonators can be used as smart tags and to measure a host of environmental parameters
 - Temperature, pressure, current, gases, stress/strain, angular position, and many more!
- Demonstration of these devices coming soon!

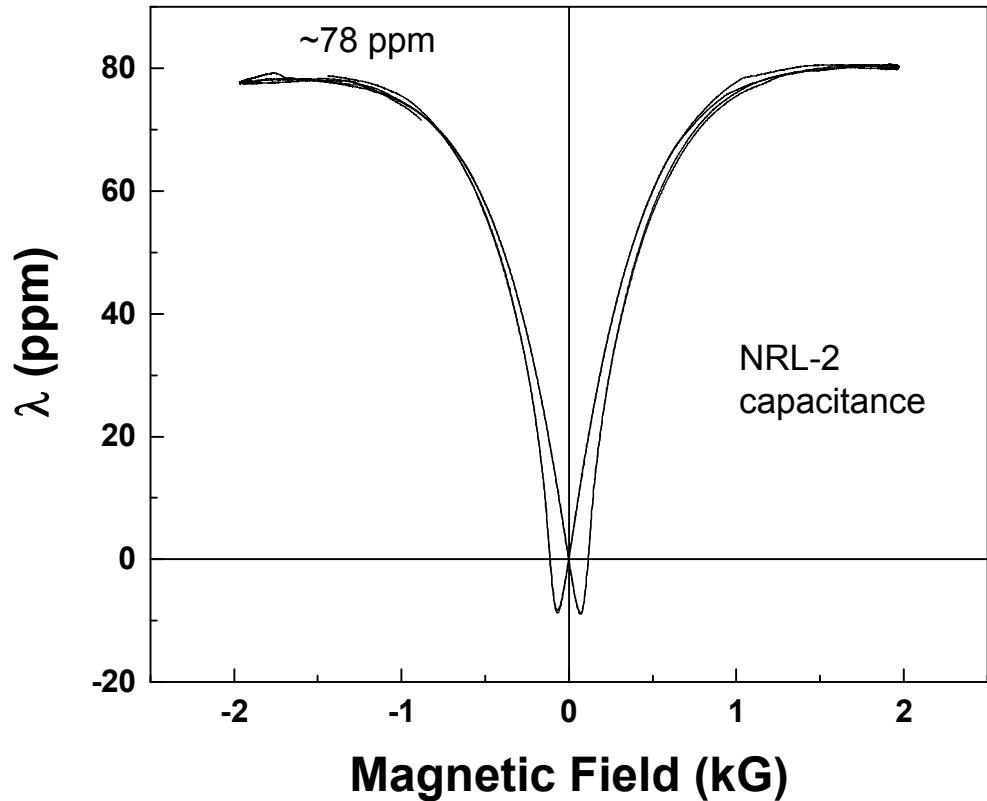
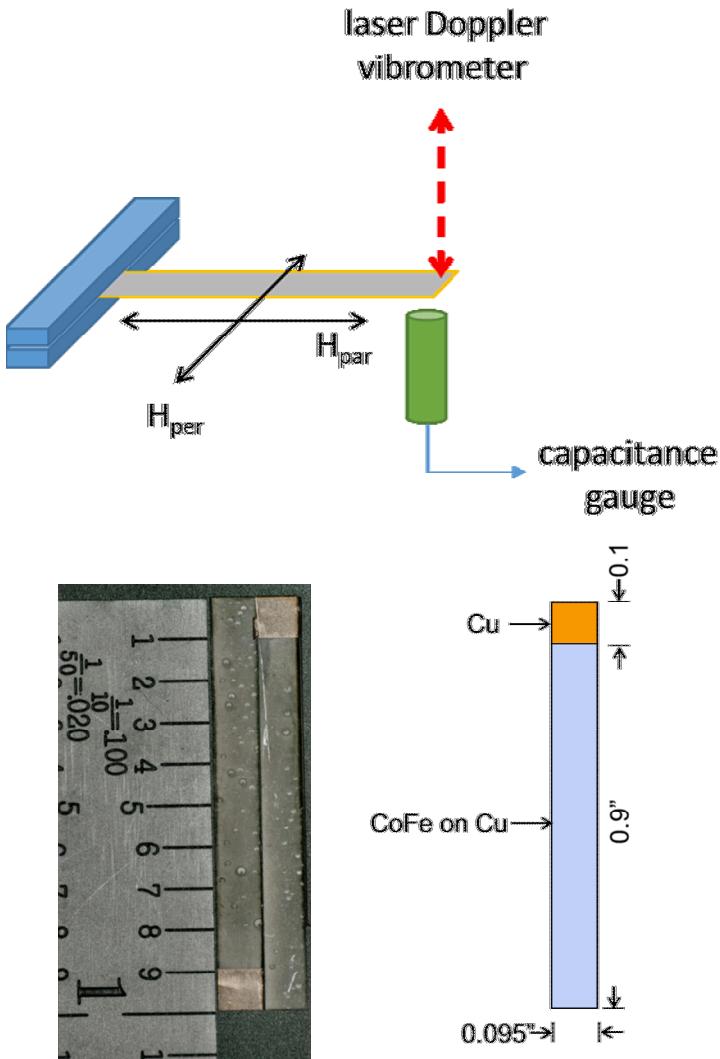
Acknowledgements

- γ' -Fe₄N R&D supported by Dr. Imre Gyuk and the Energy Storage Program in the Office of Electricity Delivery and Energy Reliability at the US Department of Energy
- CoFe material and device R&D supported by Sandia's Laboratory Directed Research and Development (LDRD) program
- We thank Robert Delaney (El Dorado High School) for his assistance with magnetic data fitting and analysis



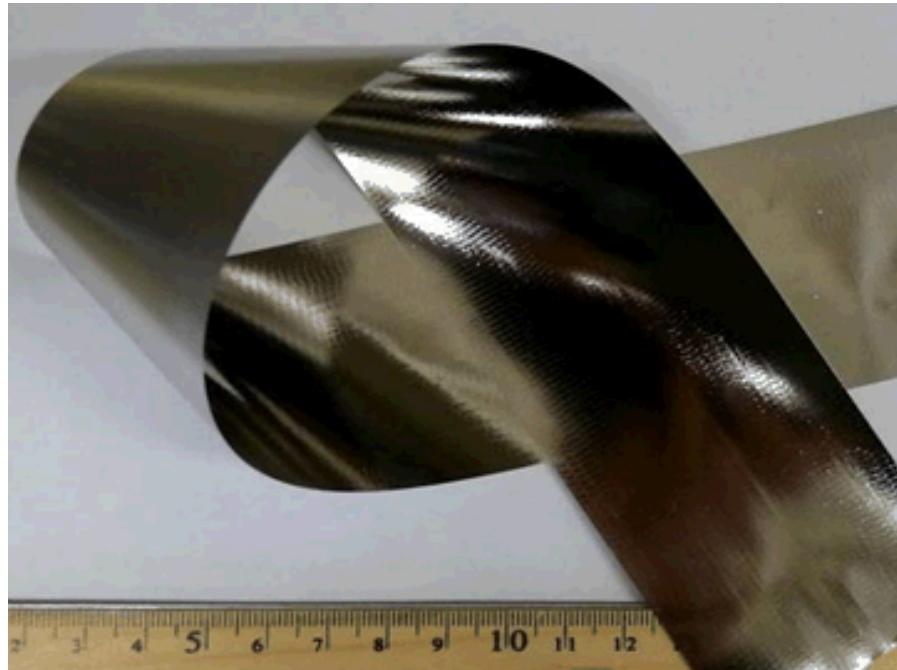
Extra Slides

NRL measurements of CoFe Cantilevers

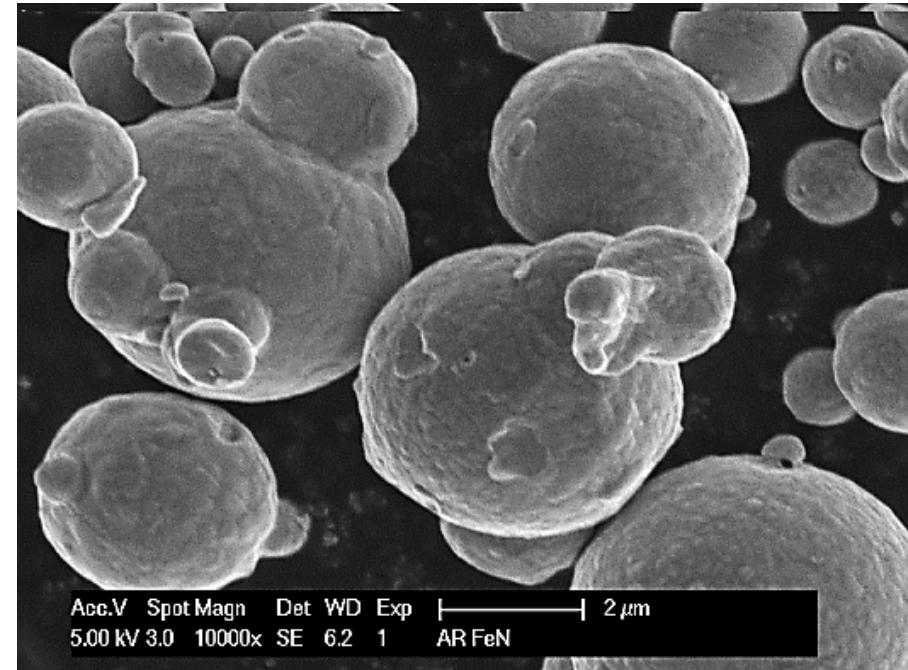


Smaller CoFe coated Cu tine
machined using ns-laser.

FeSiCrB ribbons and Fe_xN powder



FeSiCrB ribbon



Fe_xN powder

Iron nitrides crystalline structure

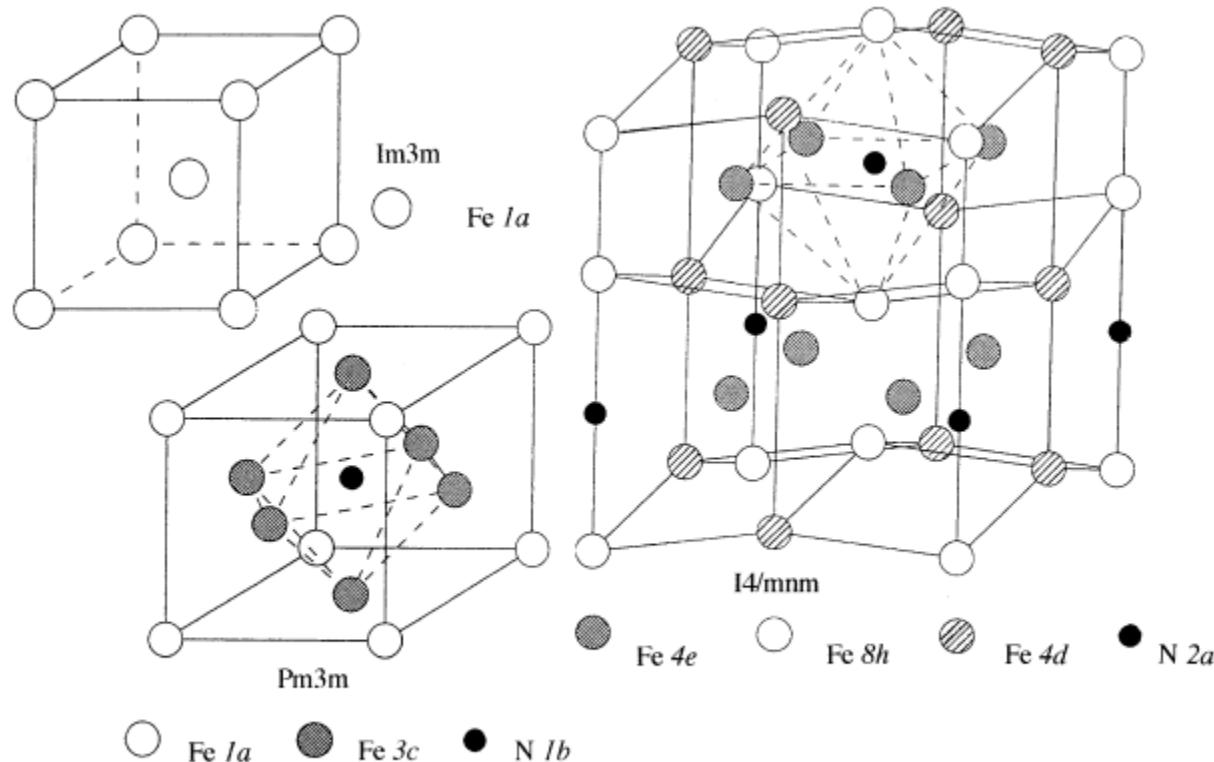


Fig. 1. Crystal structures of α -Fe, γ -Fe₄N and α'' -Fe₁₆N₂, drawn to scale.

J.M.D. Coey, P.A.I. Smith, Magnetic Nitrides, J. Magn. Mag. Mat., 200, 405 (1999).

Soft Magnetic Material Permeability

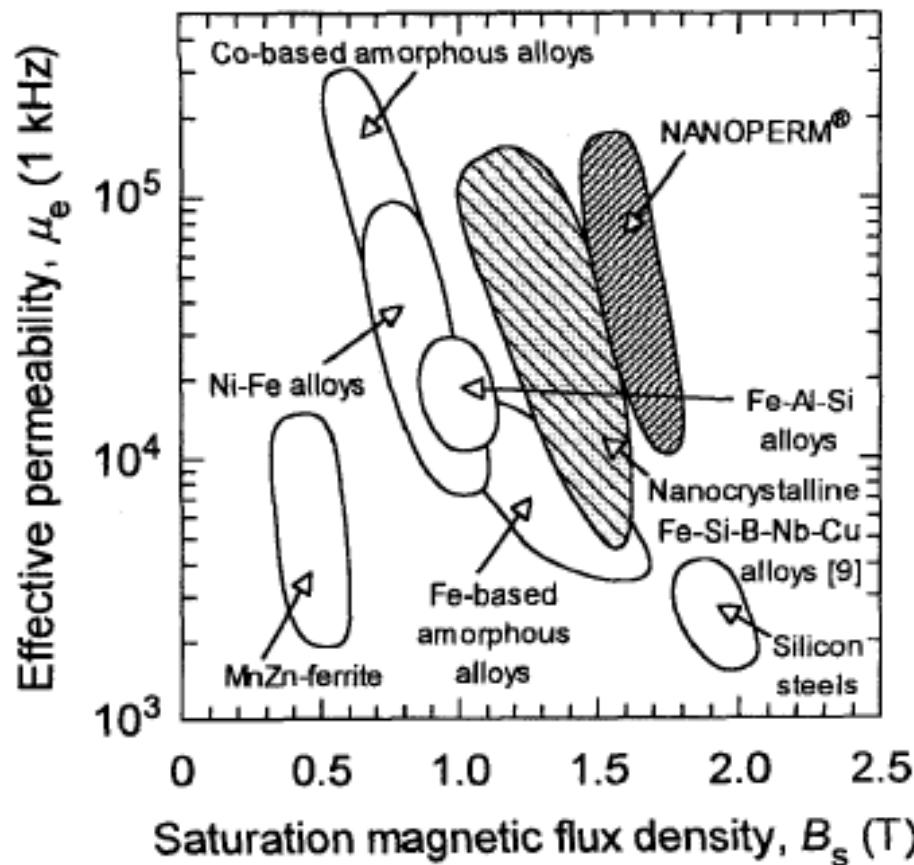


Fig. 2. Relation between B_s and μ_e at 1 kHz for NANOPERM®, the nanocrystalline Fe-Si-B-Nb-Cu alloys [9] and conventional soft magnetic materials

A. Makino, et. al., Applications of Nanocrystalline Soft Magnetic Fe-M-B (M = Zr, Nb) Alloys "NANOPERM", IEEE Trans. Magn., 33, 3793 (1997).

Magnetic Moment Variation with Nitrogen Concentration

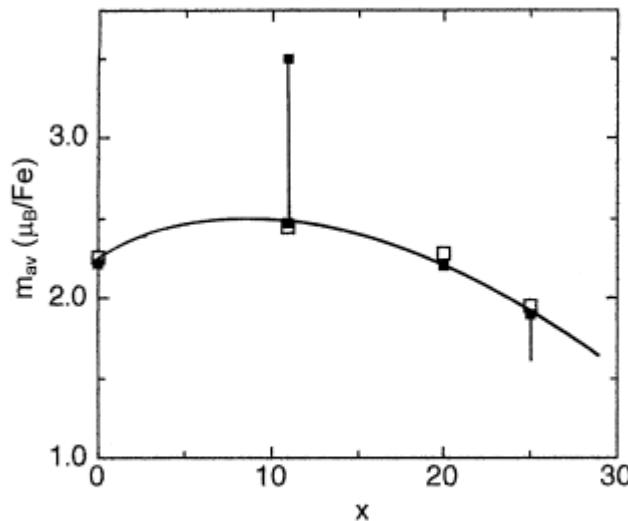
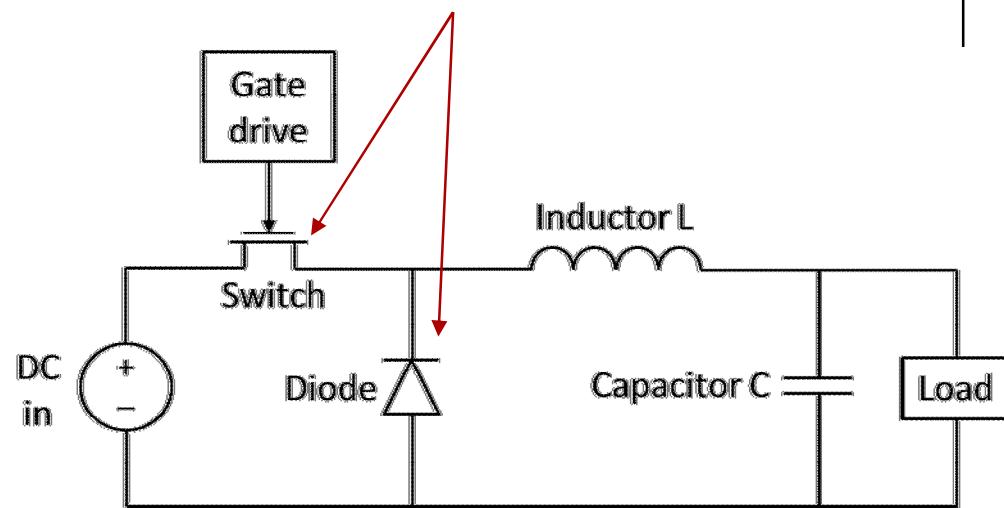


Fig. 3. Calculated (open symbol) and measured (solid symbol) average iron moments in Fe-N compounds.

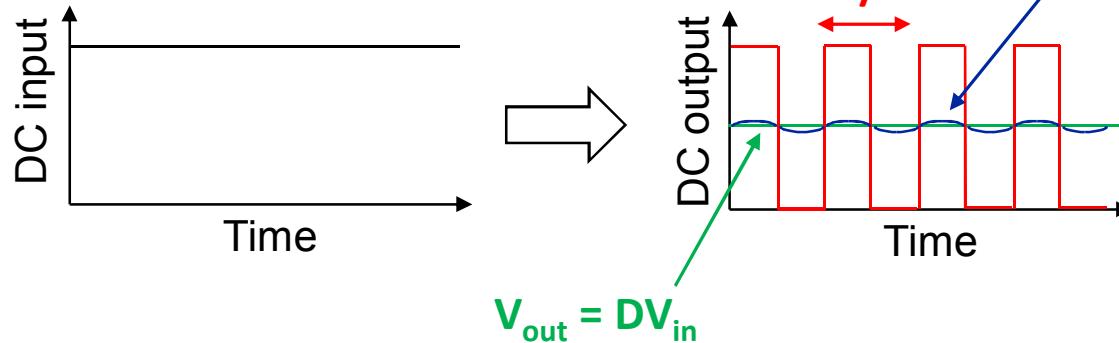
J.M.D. Coey, P.A.I. Smith, Magnetic Nitrides, J. Magn. Mag. Mat., 200, 405 (1999).

Higher Switching Frequency Enables Reduction in Passive Element Volume and Weight

Power semiconductor devices



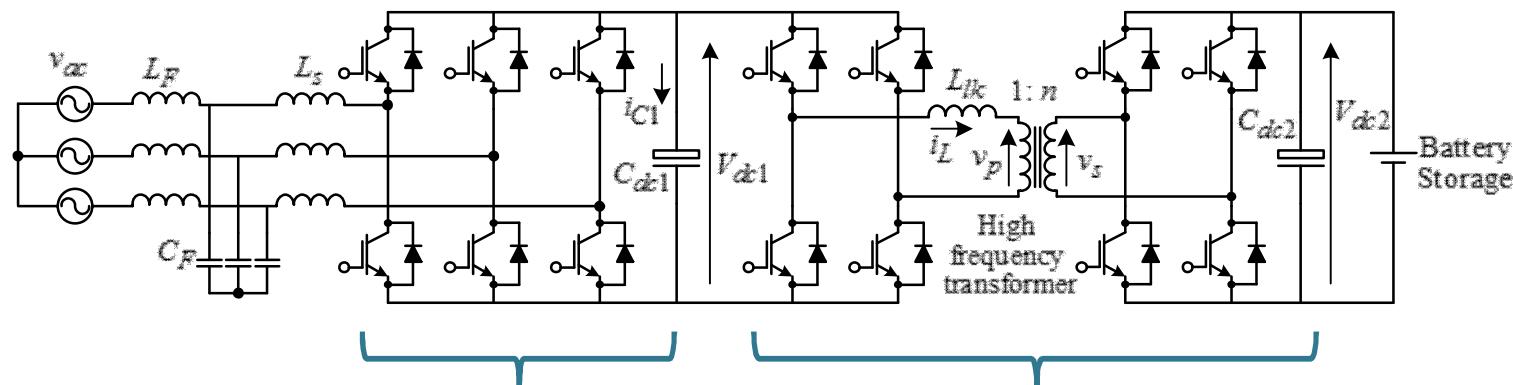
Step-Down (Buck) DC-to-DC Converter



$$\frac{V_{ripple}}{V_{out}} = \frac{1 - D}{8LCf^2}$$

Increasing f allows one to reduce L and C while keeping the ripple constant

High Frequency Link Power Conversion System Configuration

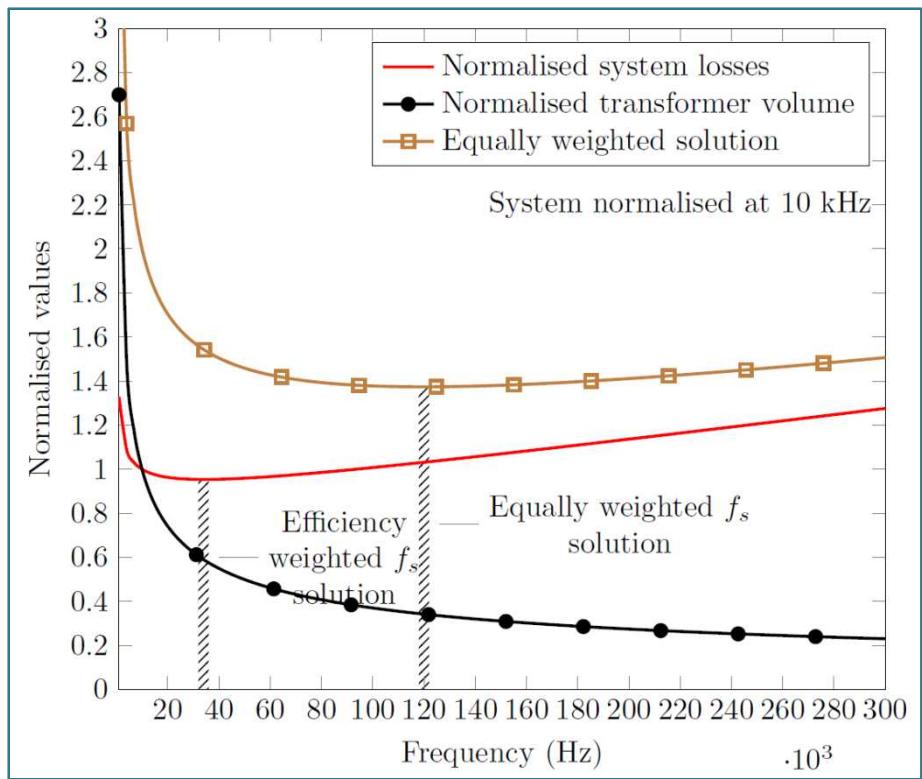


- Optimal switching frequency based on the losses at this stage

Volume occupied by heat sinks and non-magnetic components were not considered !!

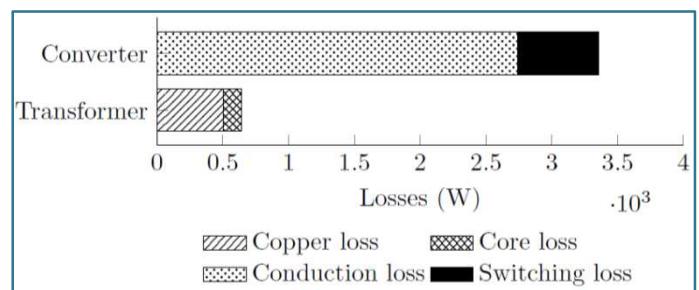
- Optimal switching frequency based on:
 - Switching and conduction losses in the switch
 - Volume of the transformer
 - Losses in the transformer
 - Copper losses in transformer windings
 - Core losses of the transformer

Optimum Frequency with SiC MOSFETs



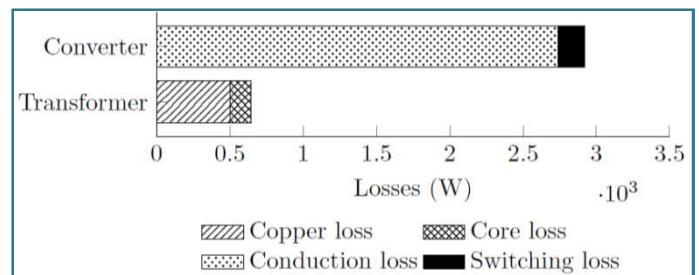
Equally weighted solution:

The converter has optimal solution at a frequency of **120 kHz** with equal weights on volume and losses

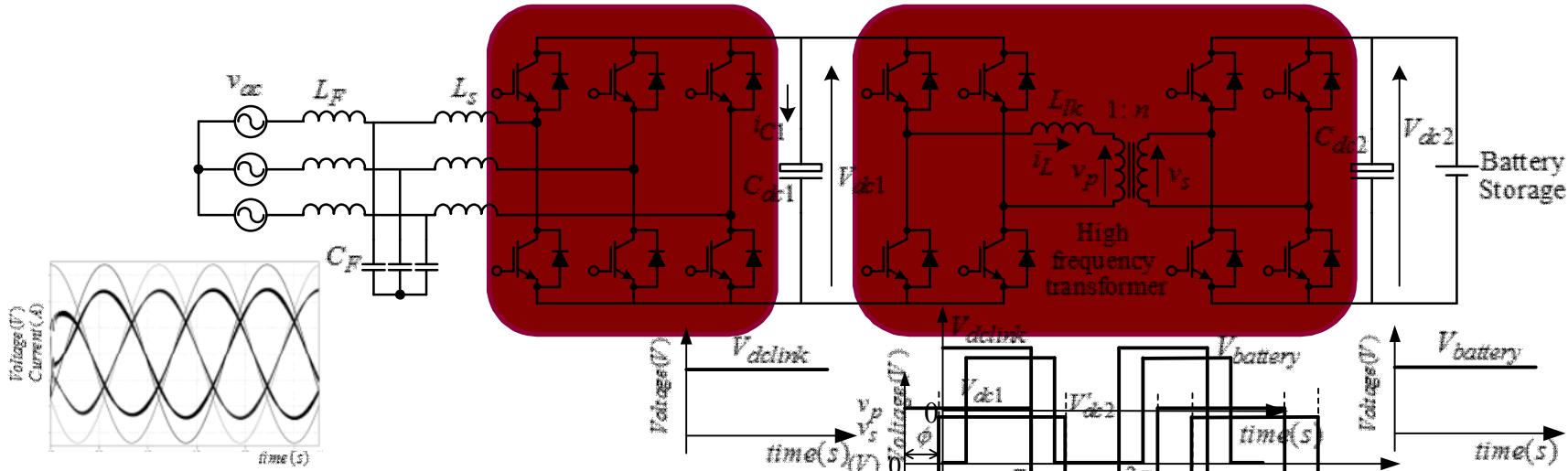


Efficiency driven solution:

The optimal solution for minimum loss condition is **35 kHz**



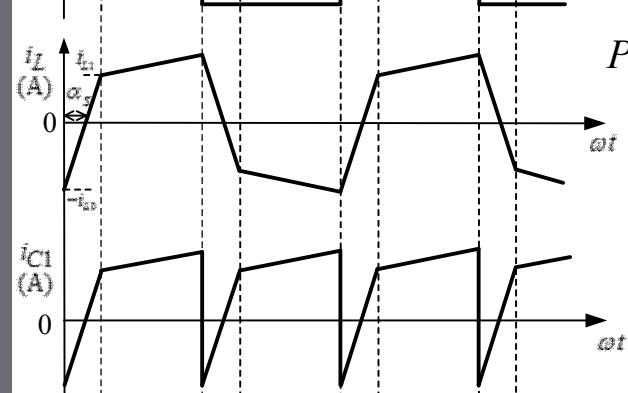
System Configuration



Parameters

Power Level	250 kW
Maximum RMS current	370 A
Maximum voltage	1100 V $\pm 10\%$
Transformer core material	Ferrite
Transformer turns ratio	1:1
Transformer leakage inductance	18 μ F
Snubber capacitance	20 nF
DC Capacitor (Input/ Output)	4.4 mF

Specifications



$$P = \frac{V_{dc1}V_{dc2}}{2\pi fL} \phi \left(1 - \frac{\phi}{\pi} \right)$$

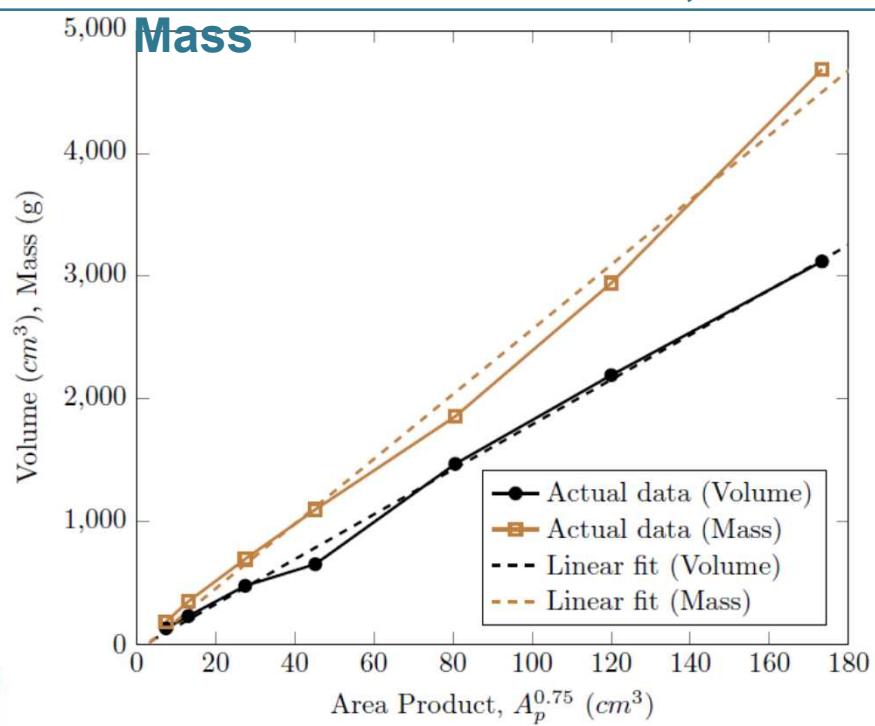
Loss and Volume Estimation

Transformer Volume Estimation:

Power handling capacity of the cores are identified by Area product, A_p

$$(A_p \text{ cm}^4) \frac{S}{k_w J_{max} \Delta B_{max} f}$$

Area Product vs Volume, Mass



A_c = Area of the core

A_w = Window area

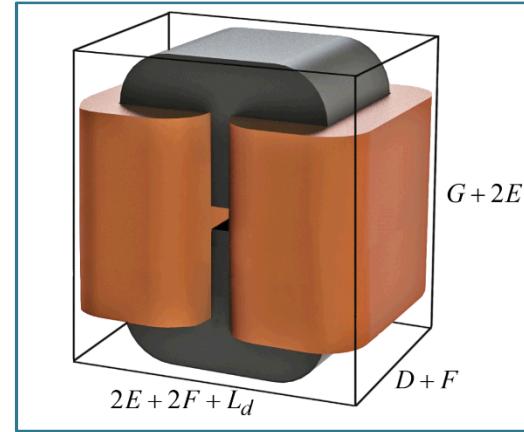
S = Total volt-amp rating of the transformer (VA)

k_w = window utilization factor

J_{max} = Current density (A/cm²)

ΔB_{max} = flux density (T)

f = switching frequency (Hz)



$$\text{Volume} = K_v A_p^{0.75}; K_v = 18.302$$

$$\text{Mass} = K_p A_p^{0.75}; K_p = 26.41$$

$$\text{Volume} = \frac{8.328 \times 10^6}{\Delta B^{0.75} f^{0.75}} \text{ cm}^3$$

Transformer Losses

Transformer copper loss:

$$P_{cu} = 2K_r \frac{N_{pri} \rho l}{A_{cond}} I_{rms}^2$$

$$N_{pri} = \frac{V_{pri}}{\Delta B_{max} A_c f}$$

$$P_{cu} = \frac{288475.68}{\Delta B^{0.75} f^{0.75}} W$$

Mean turns length :

$$l = 2(E + D) + \pi F/2$$

where,

$$N_{pri} = \frac{1703.1}{\Delta B^{0.5} f^{0.5}}; R_{dc} = \frac{1.0536}{\Delta B^{0.75} f^{0.75}}$$

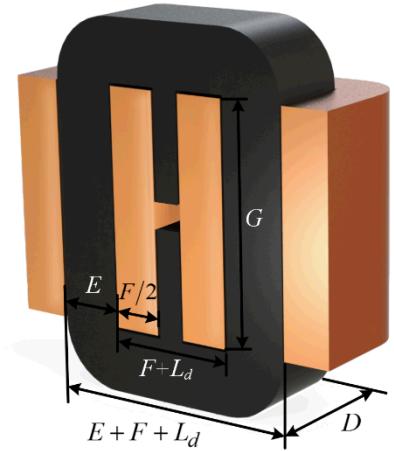
Transformer Iron loss:

$$P_{fe} = \left(k f_{eq}^{\alpha-1} \hat{B}^{\beta} \right) f \quad \leftarrow \text{Modified Steinmetz equation}$$

$$f_{eq} = \frac{2}{\Delta B^2 \pi^2} \int_0^T \left(\frac{dB}{dt} \right)^2 dt$$

The total iron losses in a 3C93 ferrite core is

$$P_{fe} = 4.77 f^{0.6} \Delta B^{2.45}$$



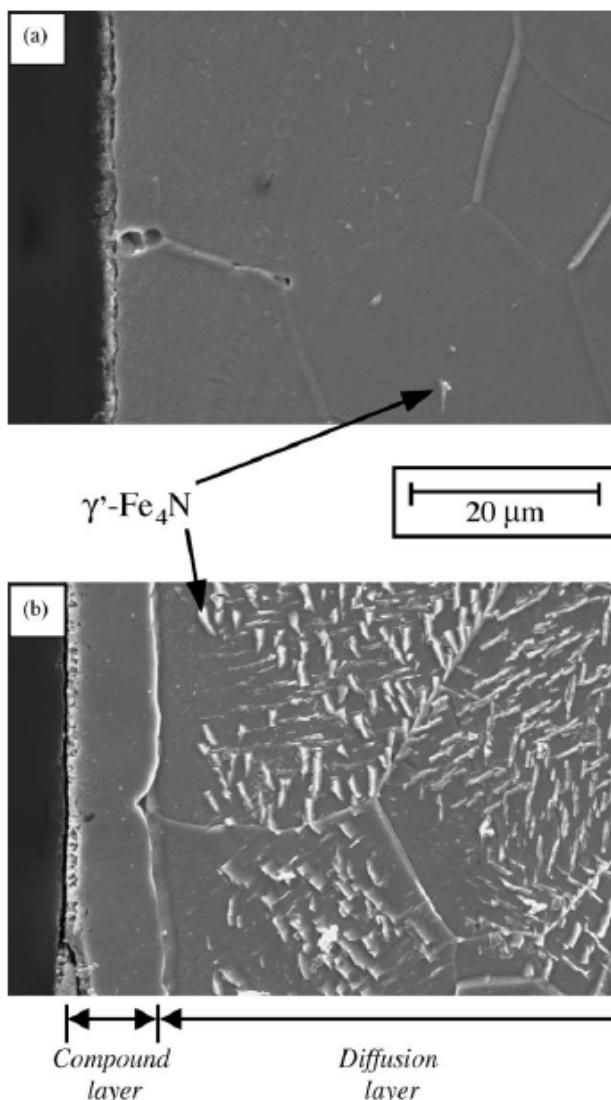
Optimal flux density

$$\begin{aligned} P_T &= P_{cu} + P_{fe} \\ &= \frac{288475.68}{\Delta B^{0.75} f^{0.75}} + 4.77 f^{0.6} \Delta B^{2.45} \end{aligned}$$

$$\frac{dP_T}{dB}(f = \text{const}) = 0$$

$$B_{opt} = \frac{21.557}{f^{0.425}}$$

In House Synthesis of Raw Materials: Electrochemical Nitriding of Iron



- Growth of γ' -Fe₄N demonstrated by Japanese electrochemists
- Formed γ' -Fe₄N at the surface of Fe(0) electrode using Li₃N as nitride source
- Demonstrates electrochemical synthesis of iron nitride possible
- Our goal is to demonstrate autonucleation of iron nitride with flowing N₂

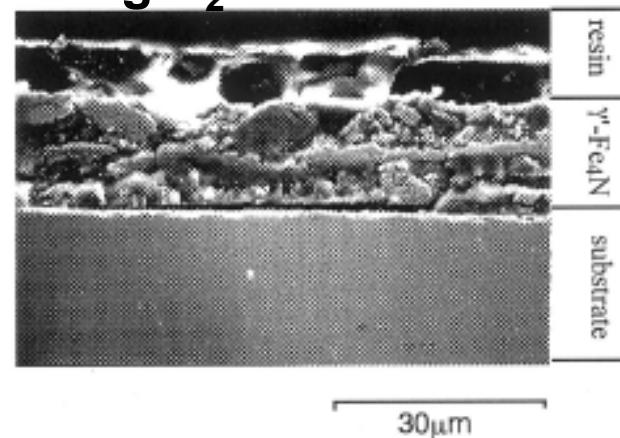
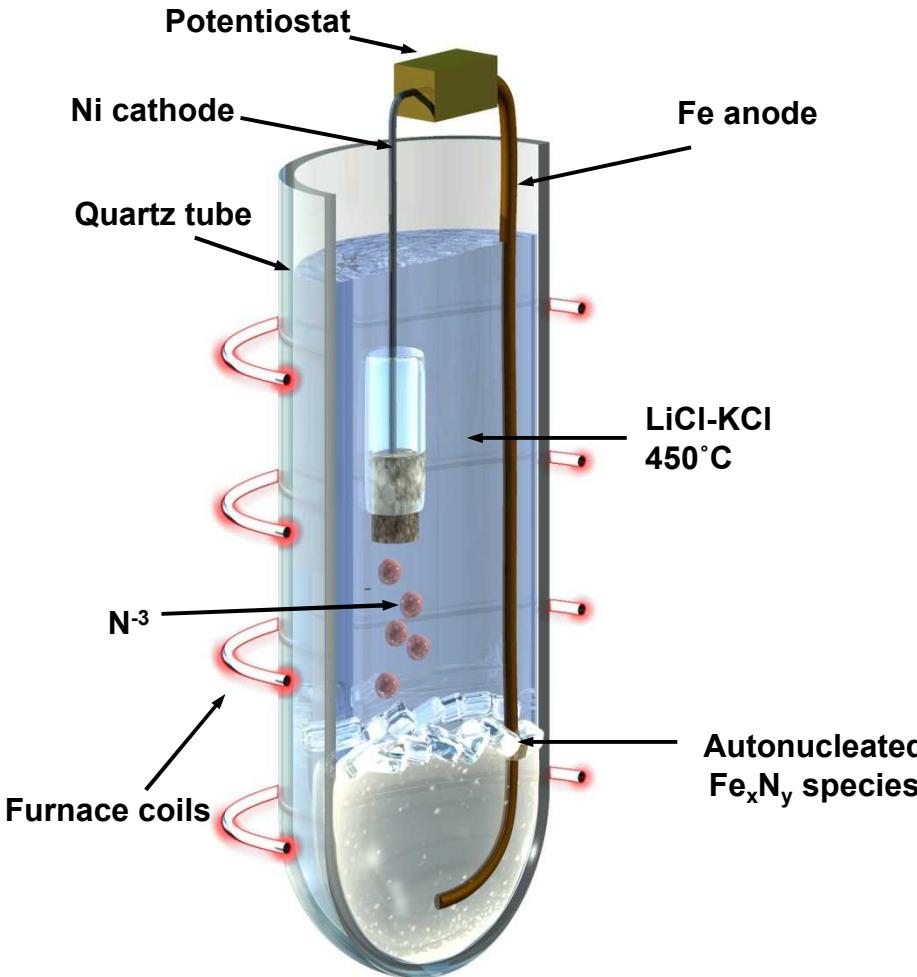


Fig. 10. Cross-sectional SEM image of iron electrode after potential pulse electrolysis for 1 h.

Electrochemical Solution Growth of Magnetic Nitrides



- Not electroplating!!!!
- Molten salt solution growth of GaN developed and patented at Sandia
- Create ionic precursors electrochemically
- Use salt transport to deliver precursors
- Increase growth rate through flux of reactants (increase currents, N₂ flow also has an effect)
- Can control oxidation state of transition metal
- Produces high quality material



Precursors can be replenished as they are consumed
Advantage: Continuous, isothermal or steady-state growth

Other Magnetic Nitrides of Interest

Material	Phase	σ_s (Am ² /kg)	J_s (T), if available	T_c (K)	H_c (A/m)
FeN	rocksalt (fcc or fct)	209			
γ' -Fe ₄ N	antiperovskite-like	209	1.89	769	460
α'' -Fe ₁₆ N ₂	tetragonal	230 - 286	2.3	810	
α'' -Fe ₉₀ N ₁₀		230			
g-C ₄ N ₃	graphitic	62			
MnN	rocksalt	194-308			4000
α -Fe	bcc	217	2.15	1044	70
• Nitrides will have higher resistivities than current transformer core materials and will not require laminations of inactive material to mitigate eddy current losses					

Grid-connected inverter with high-frequency DC link

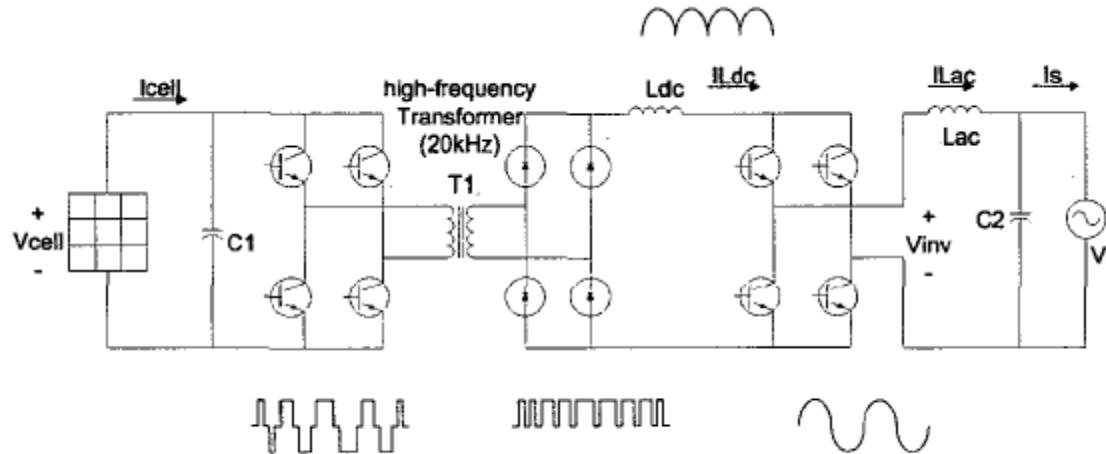


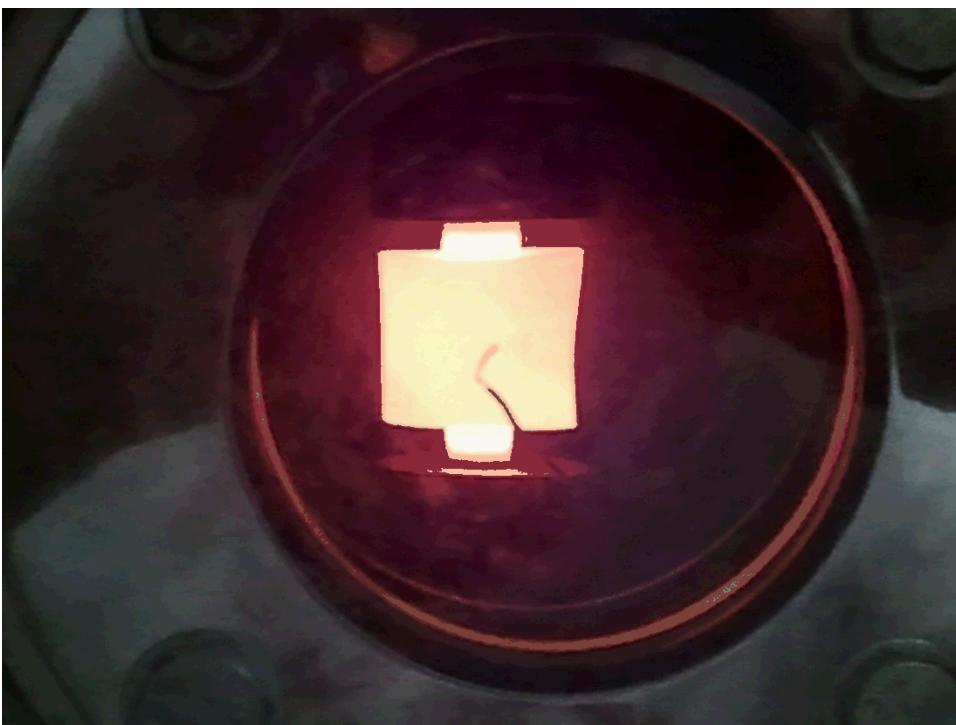
Fig. 1. Grid-connected inverter with high-frequency DC link.

Y. Jung, et. al., High-frequency DC link inverter for grid-connected photovoltaic system, IEEE, 1410 (2002).

Spark Plasma Sintering (SPS)



- DC current
 - ON(1-99 ms)/OFF(1-9 ms) pulse
- Surface activation
 - Electromigration
- Short time
 - 5~30 min
 - Max. heating rate ~ 400 °C/min
- SPS-825S
 - Max. force: 250 kN
 - Max. current: 8000 A
 - Sample dimension: $\Phi 80$ mm
- Offers the ability to fine tune grain size in sintered devices



SPS for Manufacturing Ceramics

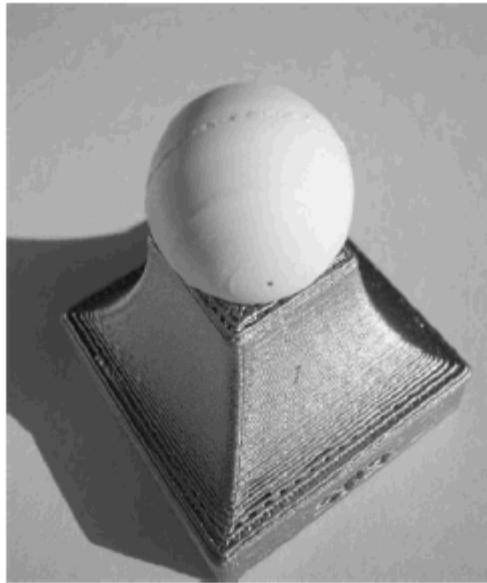


Fig. 9. Al_2O_3 sphere obtained in one single step by SPS.^[63]

J. Galy, Private Communication, 2007.

Hungría et. al., Adv. Eng. Mater. Vol. 11 (2009)
616
DOI: 10.1002/adem.200900052

SPS System Manufacturers:

- Fuji Electronic Industrial Co. (Japan)
- FCT Systeme GmbH (Germany)
 - Can make components up to 500 mm (~20") in diameter
- Thermal Technology LLC (Santa Rosa, CA)

- **Size of equipment increasing to accommodate commercial needs**
- **Technology for continuous SPS under development**
- **A large number of companies have acquired SPS but often request this info to not be made public to maintain a competitive advantage**