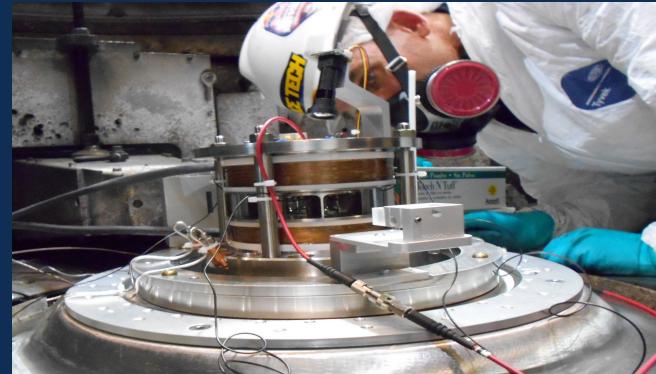
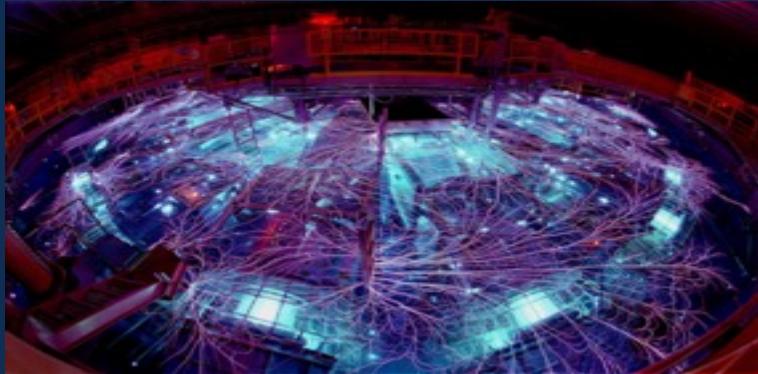


*Exceptional service in the national interest*



# Introduction to Magneto-Inertial Fusion on Z

Kyle Peterson

*Manager, Radiation & Inertial Confinement Fusion Target Design*

**2017 HEDS summer school**



Sandia National Laboratories is a multi-mission laboratory managed and operated by National Technology & Engineering Solutions of Sandia, LLC., a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.

**This work is the collective effort of many exceptional scientists and engineers**



D.J. Ampleford, T.J. Awe, C.J. Bourdon, G.A. Chandler, P.J. Christenson, M.E. Cuneo, M. Geissel, M.R. Gomez, K.D. Hahn, S.B. Hansen, E.C. Harding, A.J. Harvey-Thompson, M.H. Hess, B.T. Hutsel, C.A. Jennings, B. Jones, M.C. Jones, R.J. Kaye, G. Laity, D.C. Lamppa, M.R. Lopez, M.R. Martin, M. K. Matzen, L.A. McPherson, T. Nagayama, J.S. Lash, P.F. Knapp, J.L. Porter, G.A. Rochau, D.C. Rovang, C.L. Ruiz, M.E. Savage, P.F. Schmit, J. Schwarz, D.B. Sinars, S.A. Slutz, I.C. Smith, W.A. Stygar, R.A. Vesey, M.R. Weis, E.P. Yu, *Sandia National Laboratories*

R.R. Paguio, D.G. Schroen, K. Tomlinson, *General Atomics*

B.E. Blue, M.C. Herrmann, *Lawrence Livermore National Laboratories*

R.D. McBride, *University of Michigan*

A.B. Sefkow, *Laboratory for Laser Energetics*

*Irvin R. Lindemuth*

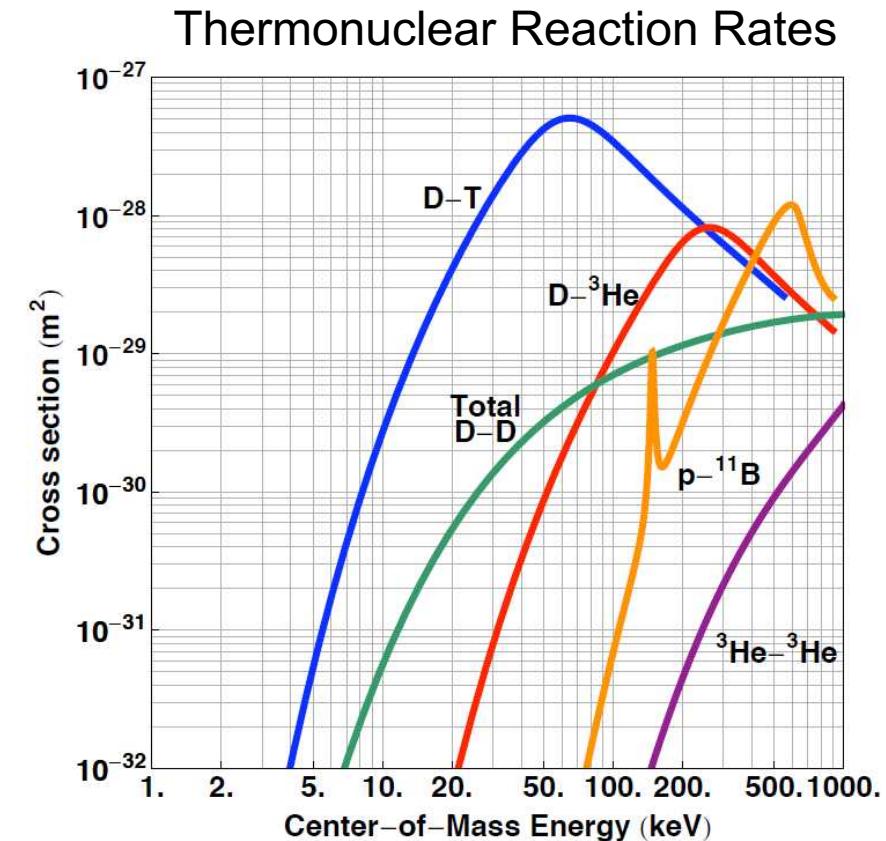
# Thermonuclear fusion powers the galaxy. Can we use it to power earth?

$$Y_{\text{fus}} = Q n_1 n_2 \langle \sigma v \rangle V \tau$$



A galaxy of controlled fusion reactors

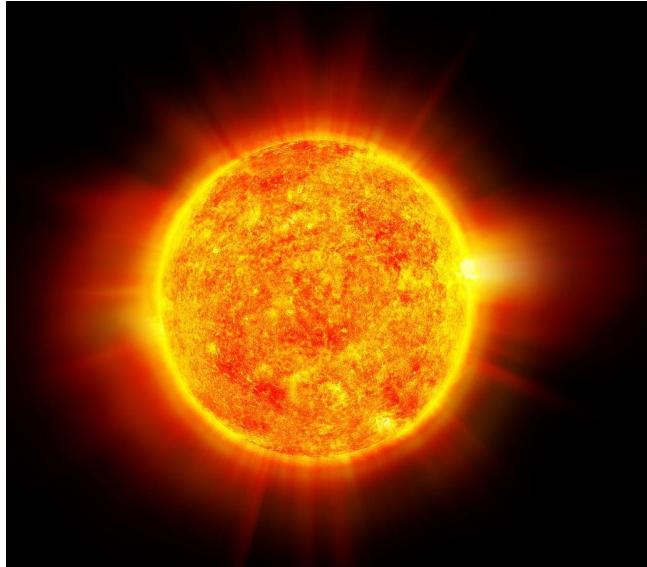
We need high temperatures,  $\sim 4$  keV for D-T



4 keV  $\approx$  40 Million K

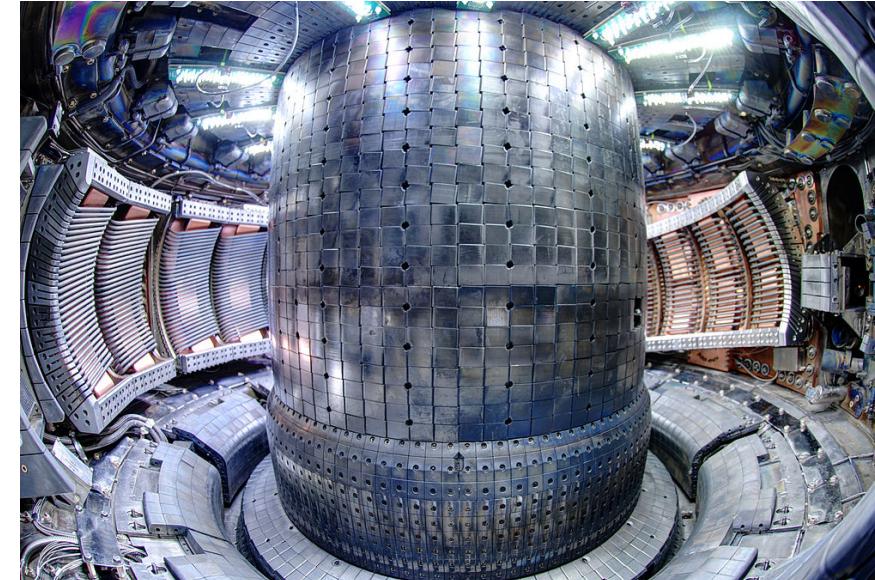
# But there is (at least) one other significant challenge... confinement!

Gravitational

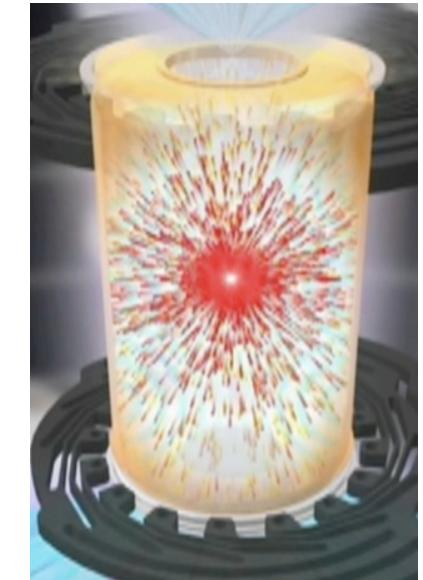


**steady-state  
controlled fusion reactor**  
 $\tau \sim \infty$

Magnetic



Inertial

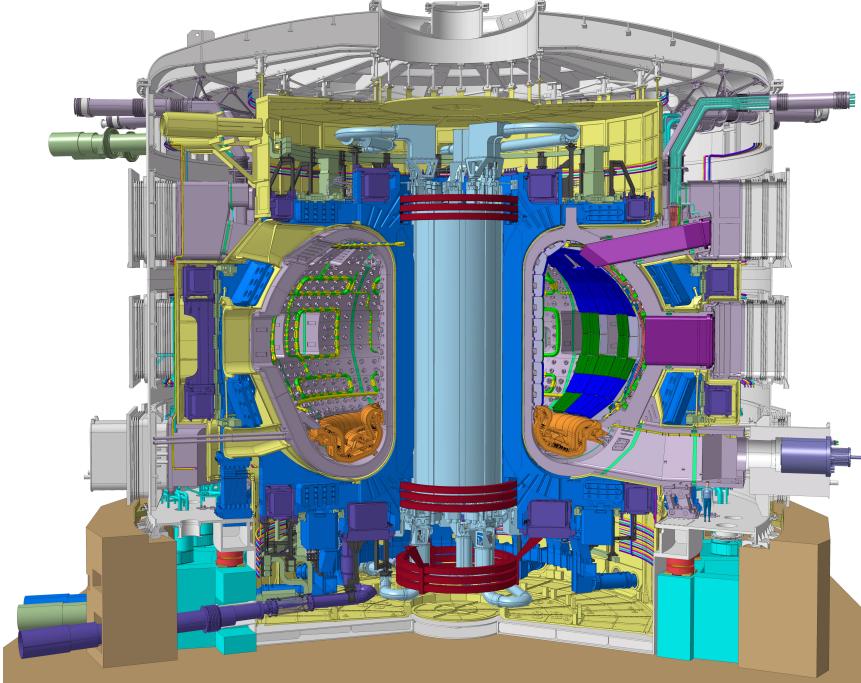


- magnetic confinement studied since 1950s
- Currently, the flagship project is ITER
- Ideally steady-state,  $\tau \sim 300\text{-}500$  s

- studied over 50 years with lasers
- Currently, the flagship is NIF
- Pulsed operation,  $\tau \sim 10$  ps

# Magnetic confinement fusion utilizes magnetic fields hold a plasma while fusion reactions occur

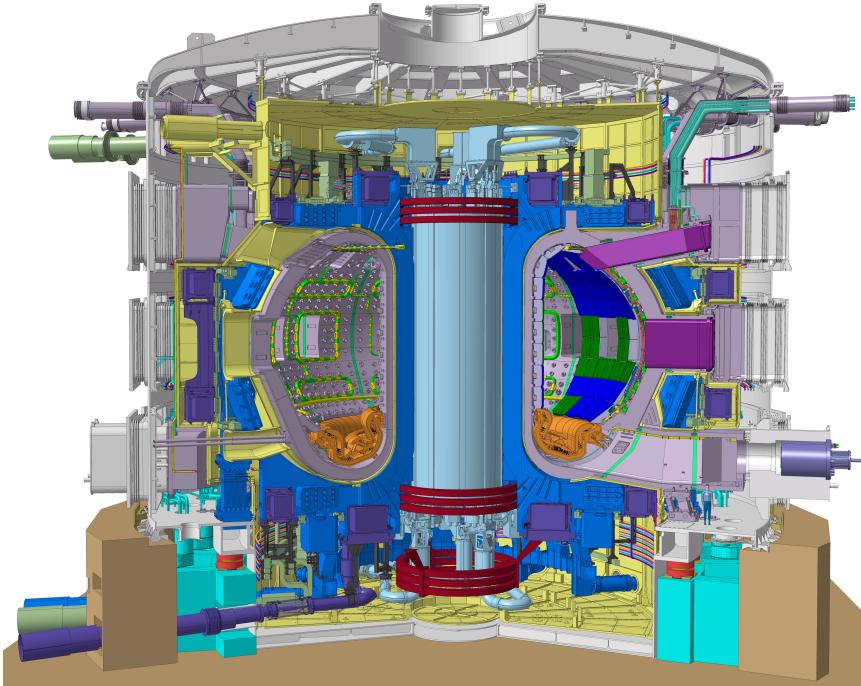
ITER



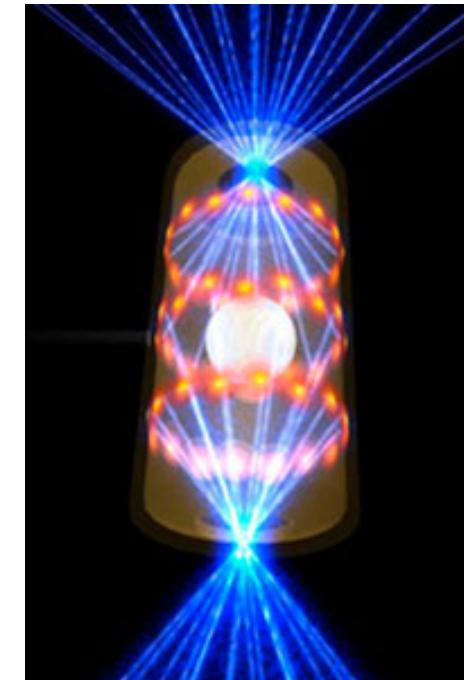
<b>Density</b>	$1 \times 10^{14} \text{ cm}^{-3}$		
<b>Volume</b>	$8 \times 10^8 \text{ cm}^3$		
<b>Duration</b>	300-500 s		
<b>Magnetic field</b>	100 kG		

# Inertial confinement fusion relies on sufficient fusion reactions occurring prior to falling apart

ITER



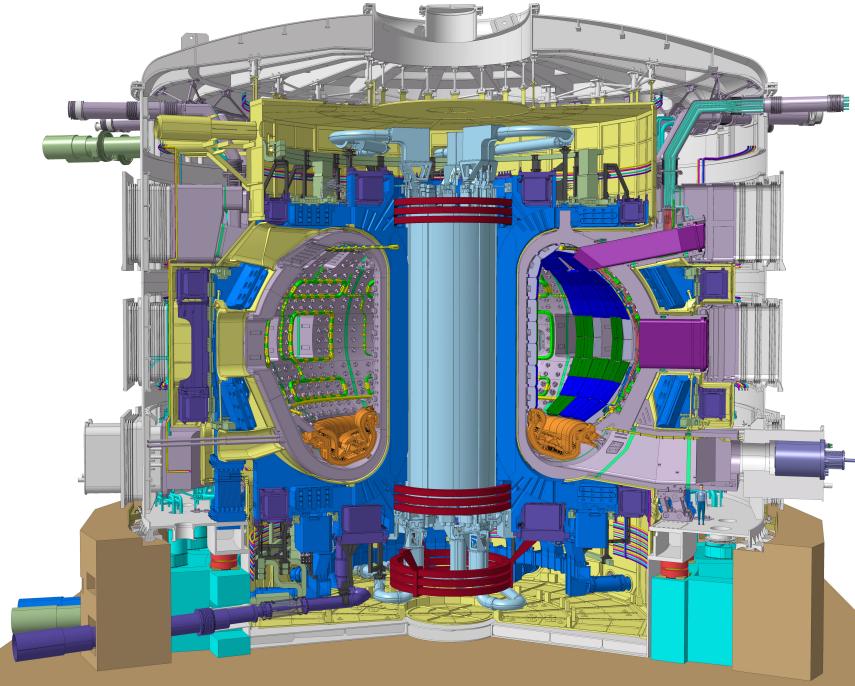
NIF hohlraum



<b>Density</b>	$1 \times 10^{14} \text{ cm}^{-3}$		$2-20 \times 10^{25} \text{ cm}^{-3}$
<b>Volume</b>	$8 \times 10^8 \text{ cm}^3$		$6 \times 10^{-8} \text{ cm}^3$
<b>Duration</b>	300-500 s		$5-10 \times 10^{-11} \text{ s}$
<b>Magnetic field</b>	100 kG		0 kG

# Inertial confinement fusion relies on sufficient fusion reactions occurring prior to falling apart

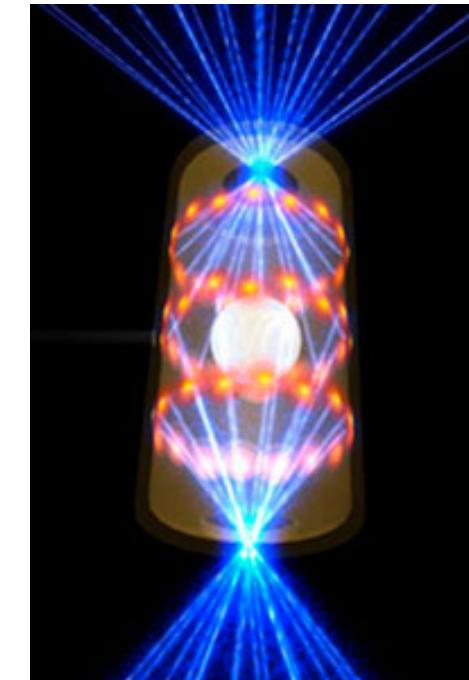
ITER



Both approaches are very expensive!

Is there a confinement approach at intermediate densities? **YES!**

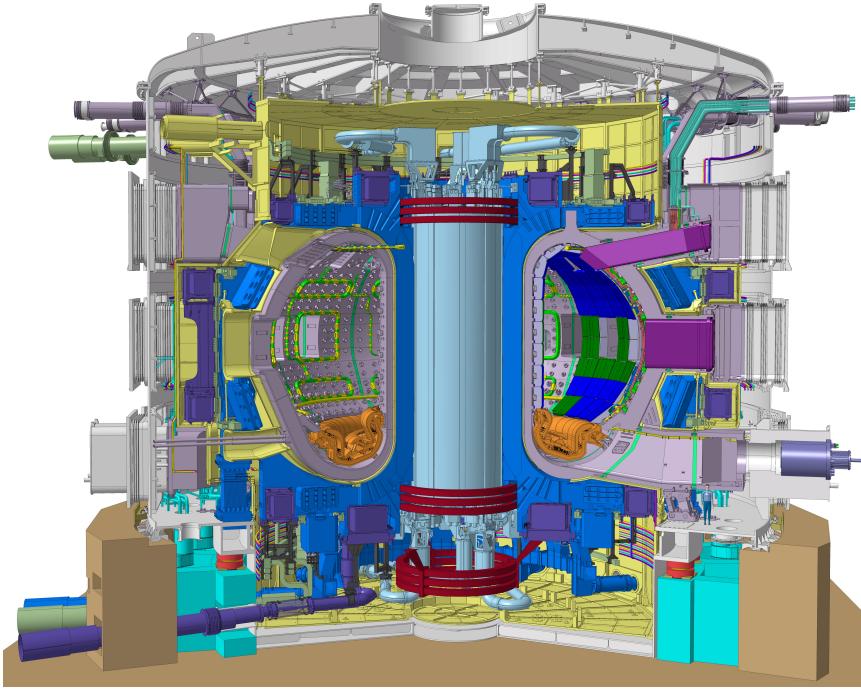
NIF hohlraum



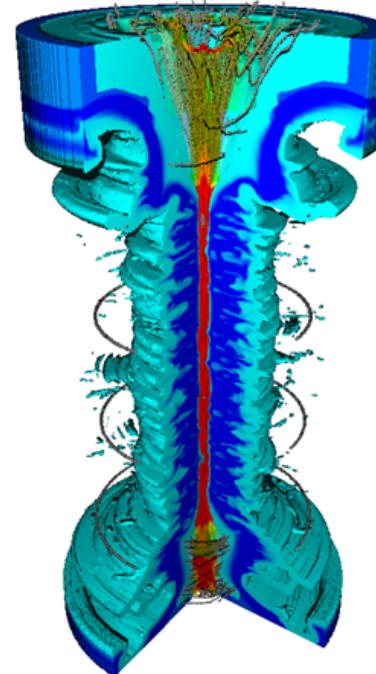
<b>Density</b>	$1 \times 10^{14} \text{ cm}^{-3}$		$2-20 \times 10^{25} \text{ cm}^{-3}$
<b>Volume</b>	$8 \times 10^8 \text{ cm}^3$		$6 \times 10^{-8} \text{ cm}^3$
<b>Duration</b>	300-500 s		$5-10 \times 10^{-11} \text{ s}$
<b>Magnetic field</b>	100 kG		0 kG

# Magneto-inertial fusion sits in the space between magnetic and inertial confinement fusion

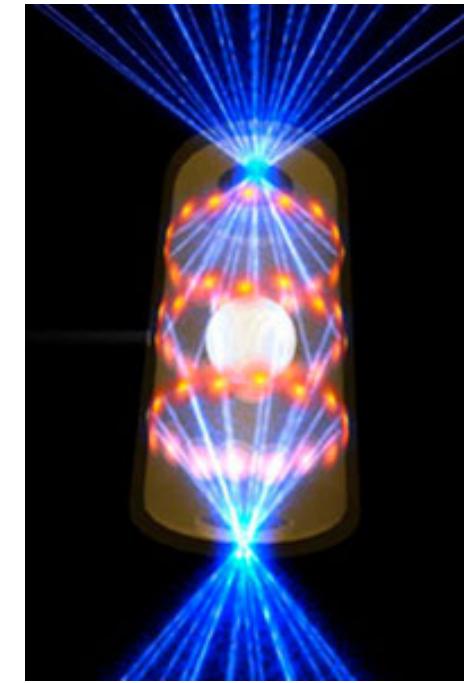
ITER



One example: MagLIF

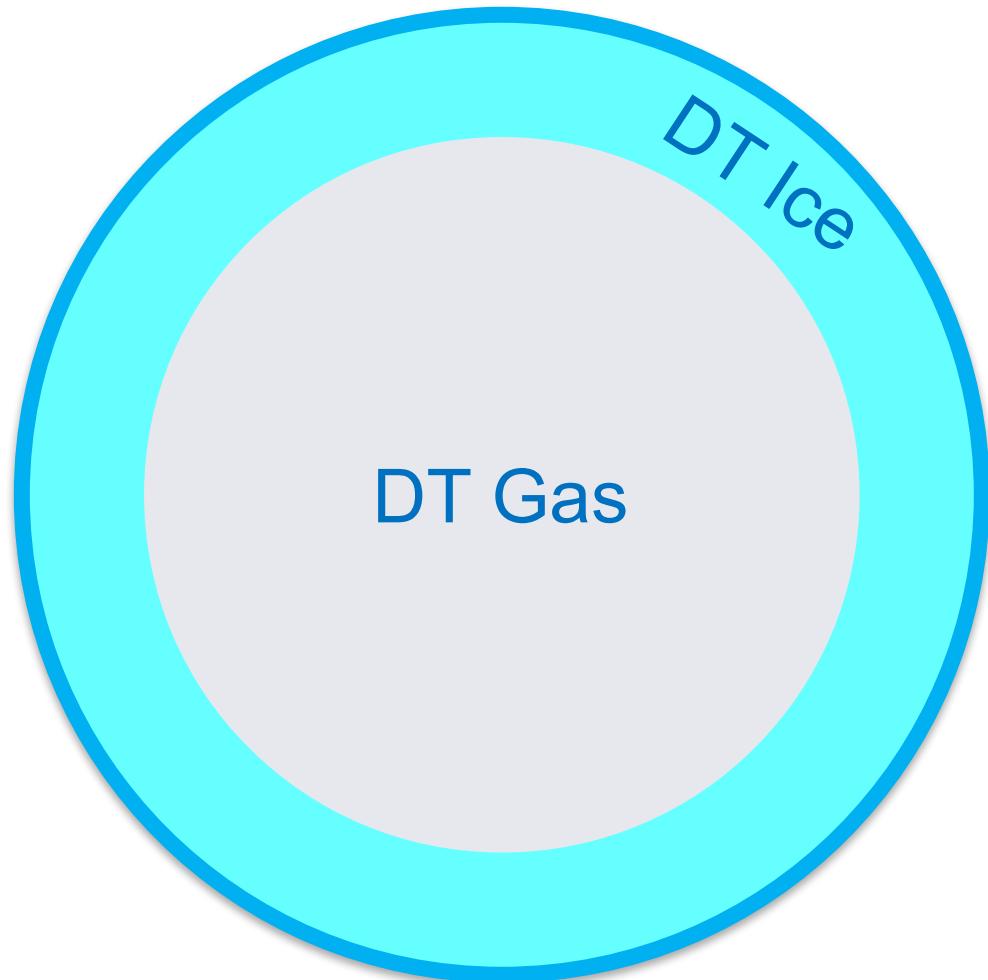


NIF hohlraum



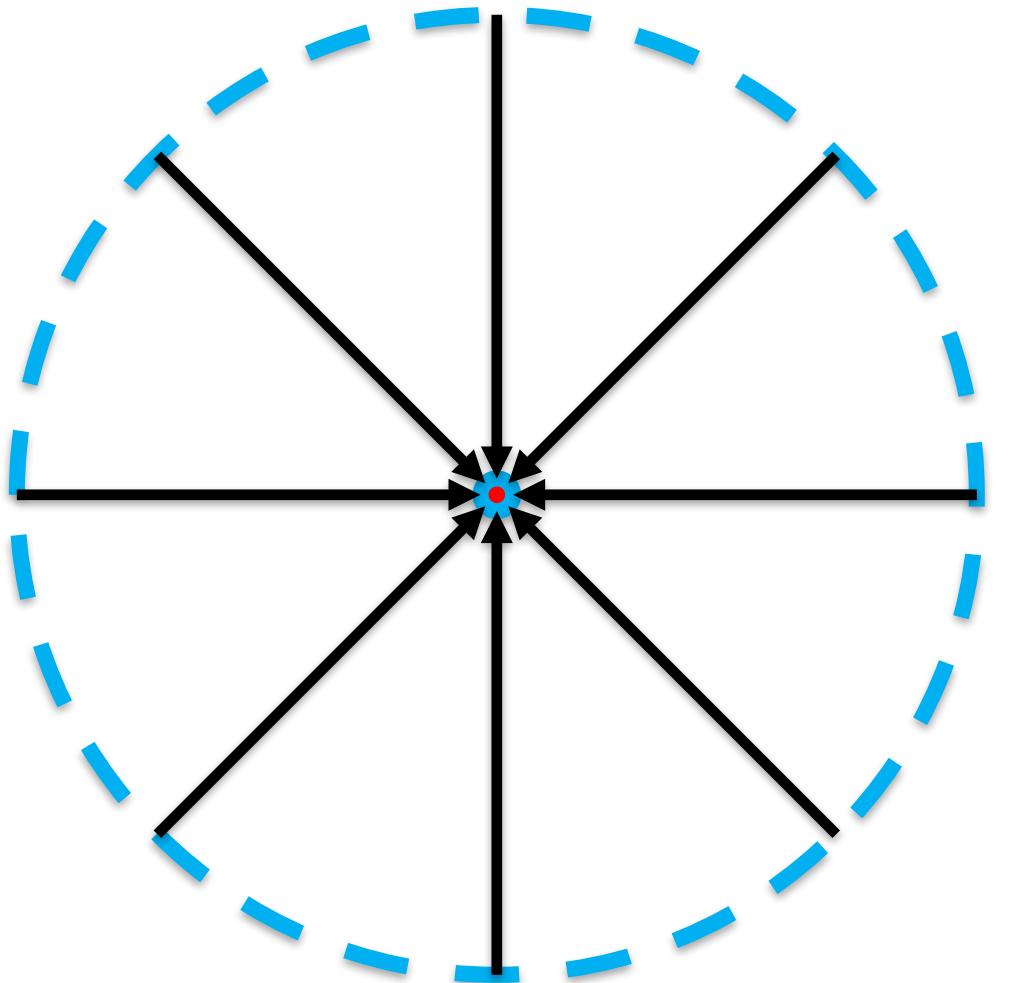
<b>Density</b>	$1 \times 10^{14} \text{ cm}^{-3}$	$1 \times 10^{23} \text{ cm}^{-3}$	$2-20 \times 10^{25} \text{ cm}^{-3}$
<b>Volume</b>	$8 \times 10^8 \text{ cm}^3$	$8 \times 10^{-5} \text{ cm}^3$	$6 \times 10^{-8} \text{ cm}^3$
<b>Duration</b>	300-500 s	$1-2 \times 10^{-9} \text{ s}$	$5-10 \times 10^{-11} \text{ s}$
<b>Magnetic field</b>	100 kG	50-100 MG	0 kG

# A quick review of traditional ICF...



- Start with a sphere containing DT

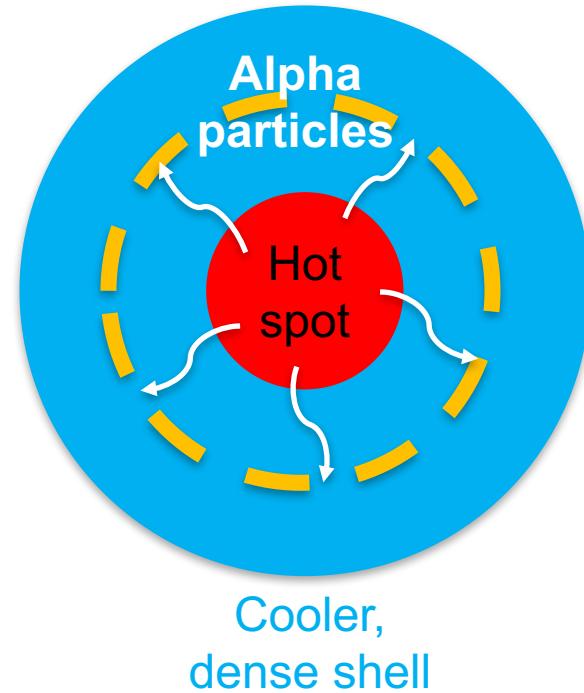
# A quick review of traditional ICF...



- Start with a sphere containing DT
- Implode the sphere
  - Compress radius by 30 (volume by 27,000)
  - Series of shocks heat the center (hot spot)

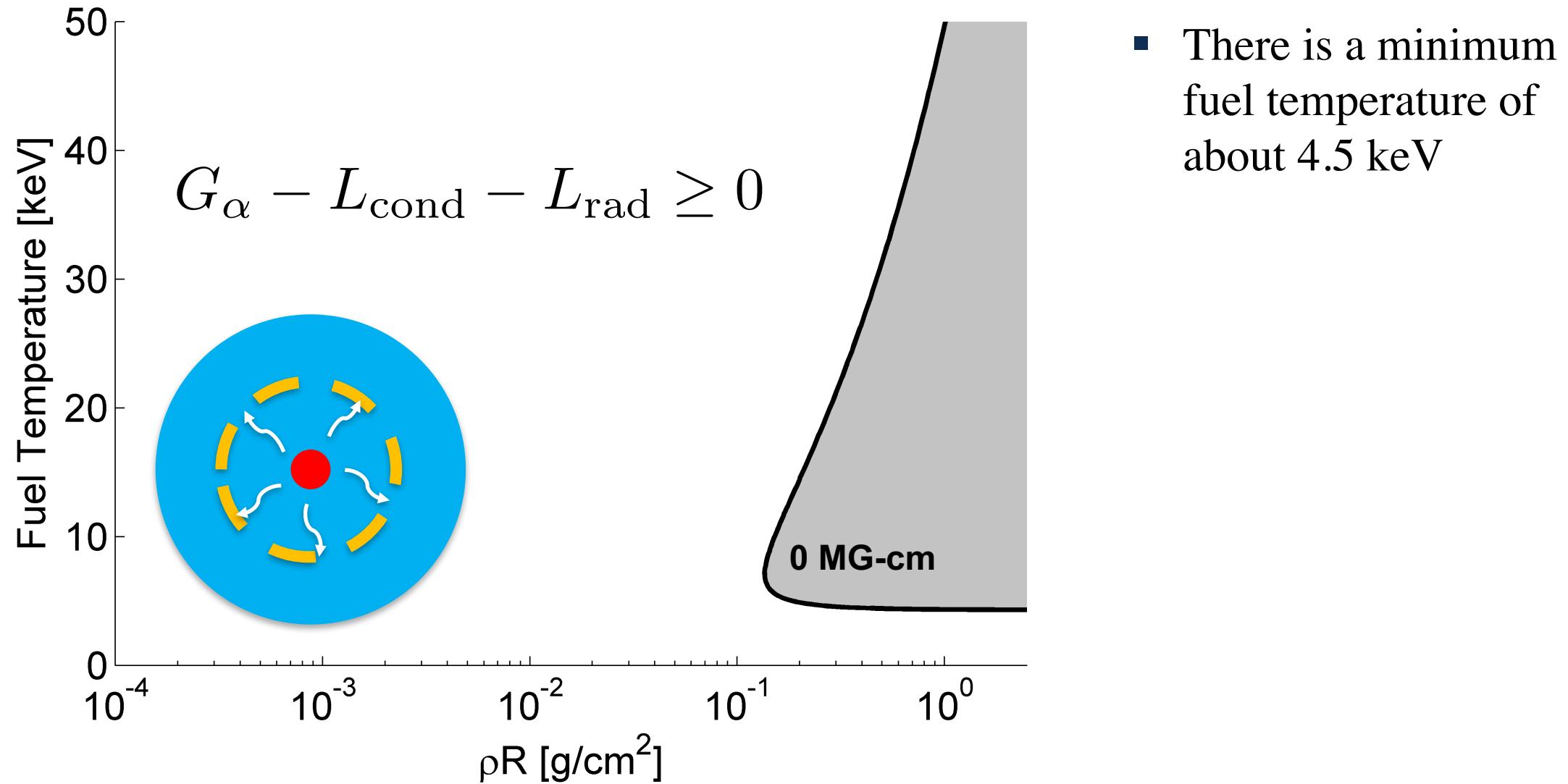
# A quick review of traditional ICF...

## Zooming in

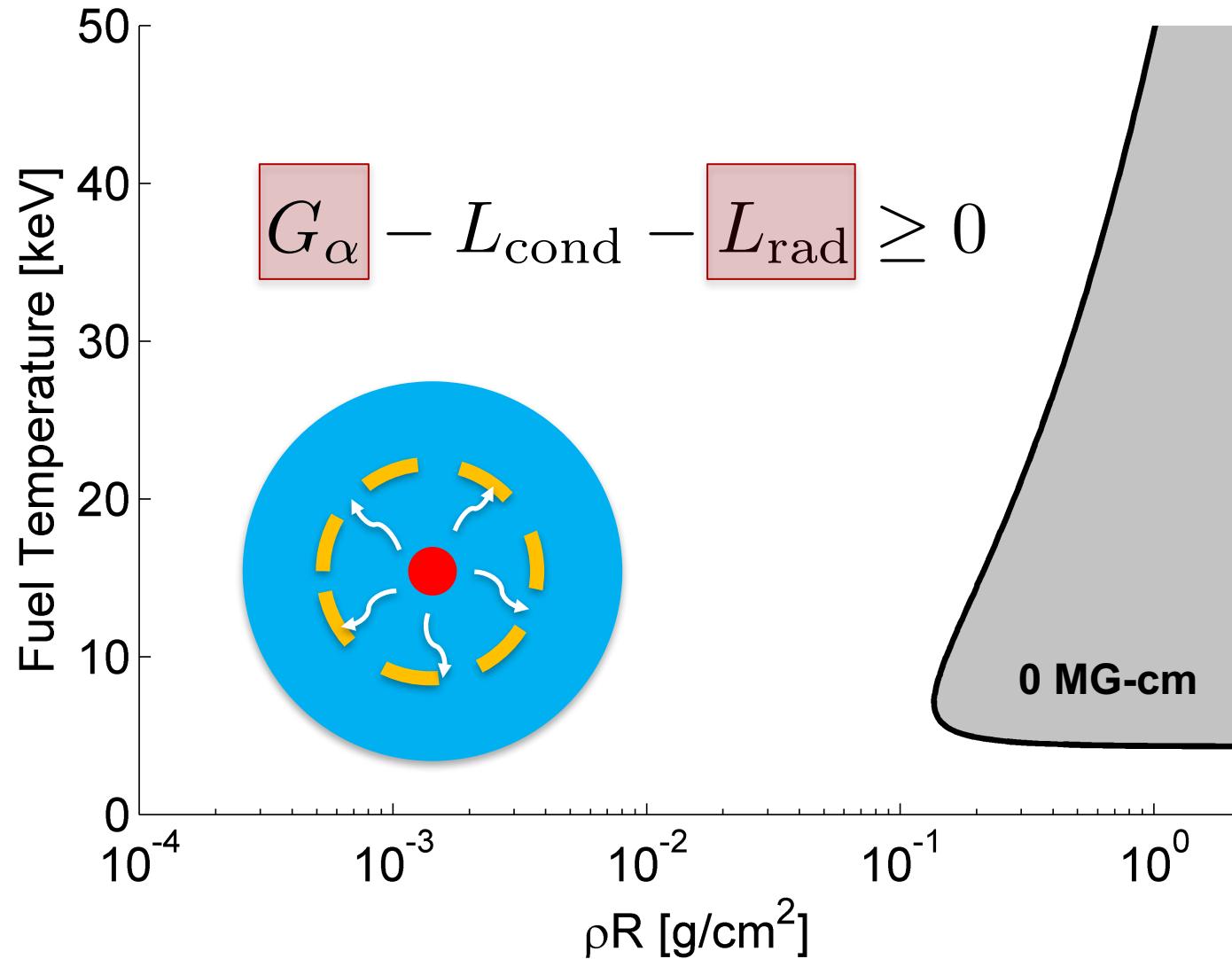


- Start with a sphere containing DT
- Implose the sphere
  - Compress radius by 30 (volume by 27,000)
  - Series of shocks heat the center (hot spot)
- Fuel in hot spot undergoes fusion
  - Fusion products (3.5 MeV a-particles) heat surrounding dense fuel
- With a favorable power balance, a chain reaction occurs
  - For parameters of interest on the NIF, this requires  $P_{HS} > 300$  Gbar and  $\rho_{cold} > 1000$  g/cm<sup>3</sup>

# In order for an ICF to produce fusion gain, both high temperatures and sufficient confinement (areal density) is required

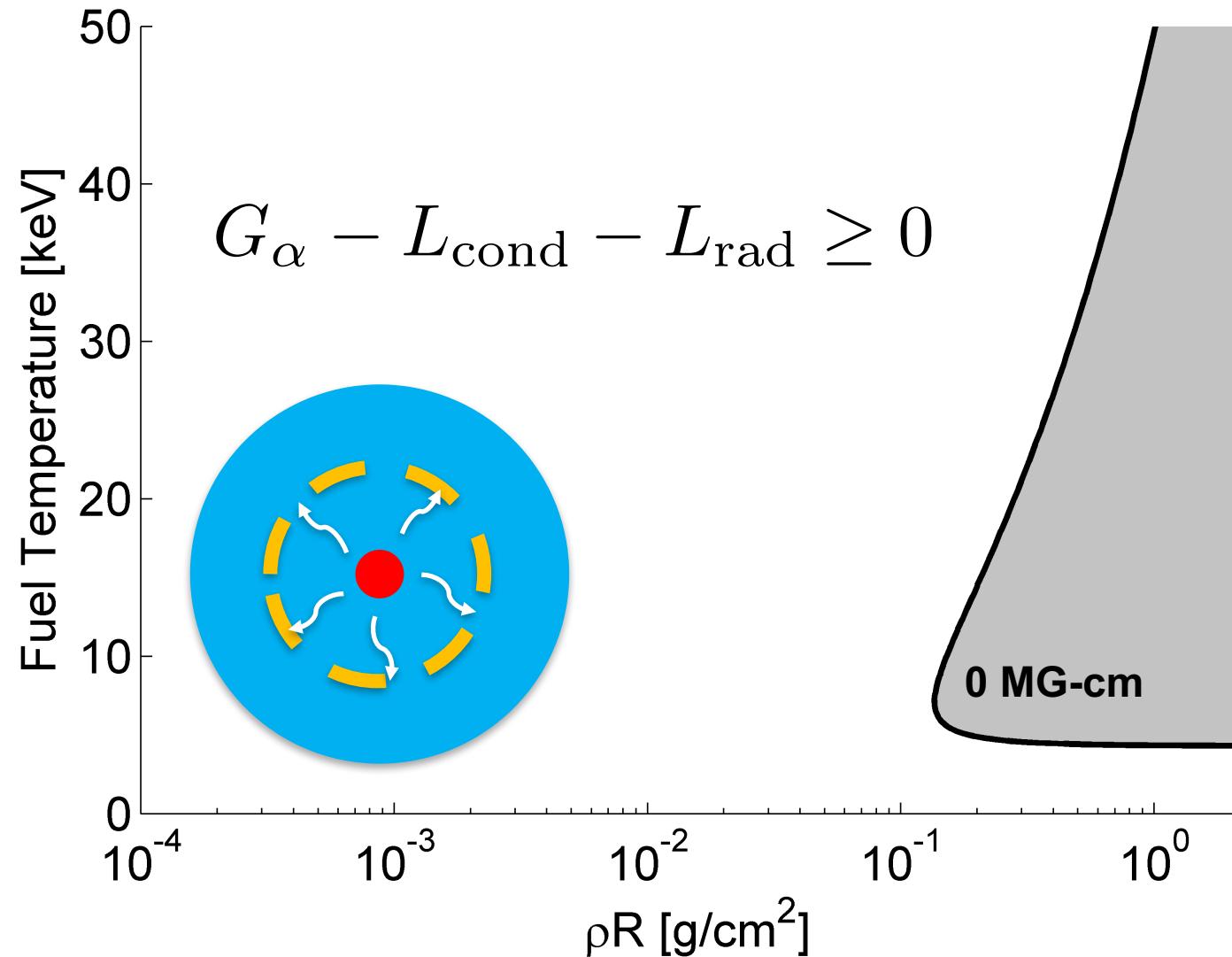


# In order for an ICF to produce fusion gain, both high temperatures and sufficient confinement (areal density) is required



- There is a minimum fuel temperature of about 4.5 keV
  - This is where fusion heating outpaces radiation losses

# In order for an ICF to produce fusion gain, both high temperatures and sufficient confinement (areal density) is required



- There is a minimum fuel temperature of about 4.5 keV
  - This is where fusion heating outpaces radiation losses
- The minimum fuel areal density is around 0.2 g/cm<sup>2</sup>
- Traditional ICF concepts attempt to operate in this minimum

# Ignition conditions necessitate high compression

*Ignition requirements:* 
$$\begin{cases} \rho R > 0.2 - 0.5 \text{ g/cm}^2 \\ T = 5 - 12 \text{ keV} \end{cases}$$

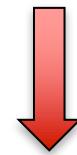


$${}^* M_{\text{fuel}} \sim \mathcal{O}(200 \text{ } \mu\text{g})$$

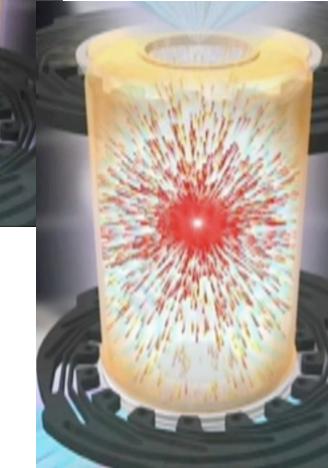


$$Y \propto M_{\text{fuel}} = \frac{4\pi}{3} \frac{(\rho R)^3}{\rho^2}$$

$$\rho = \rho_0 \left( \frac{R_0}{R} \right)^3 \equiv \rho_0 (CR)^3$$



$$\rho R \propto (\rho_0^2 M_{\text{fuel}})^{\frac{1}{3}} (CR)^2 \rightarrow (CR)_{\text{NIF}} \approx 30 - 40$$

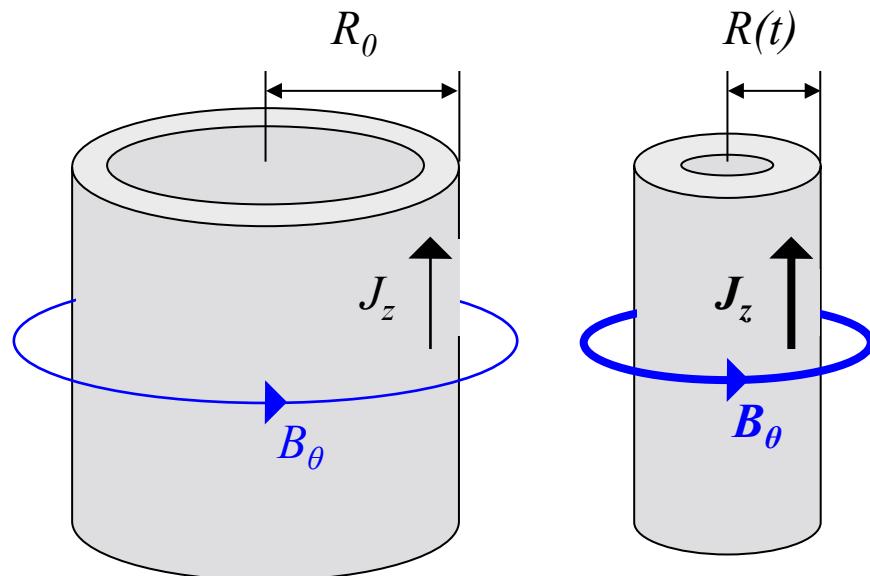


$$\mathcal{O}(10^2 \text{ MJ})$$

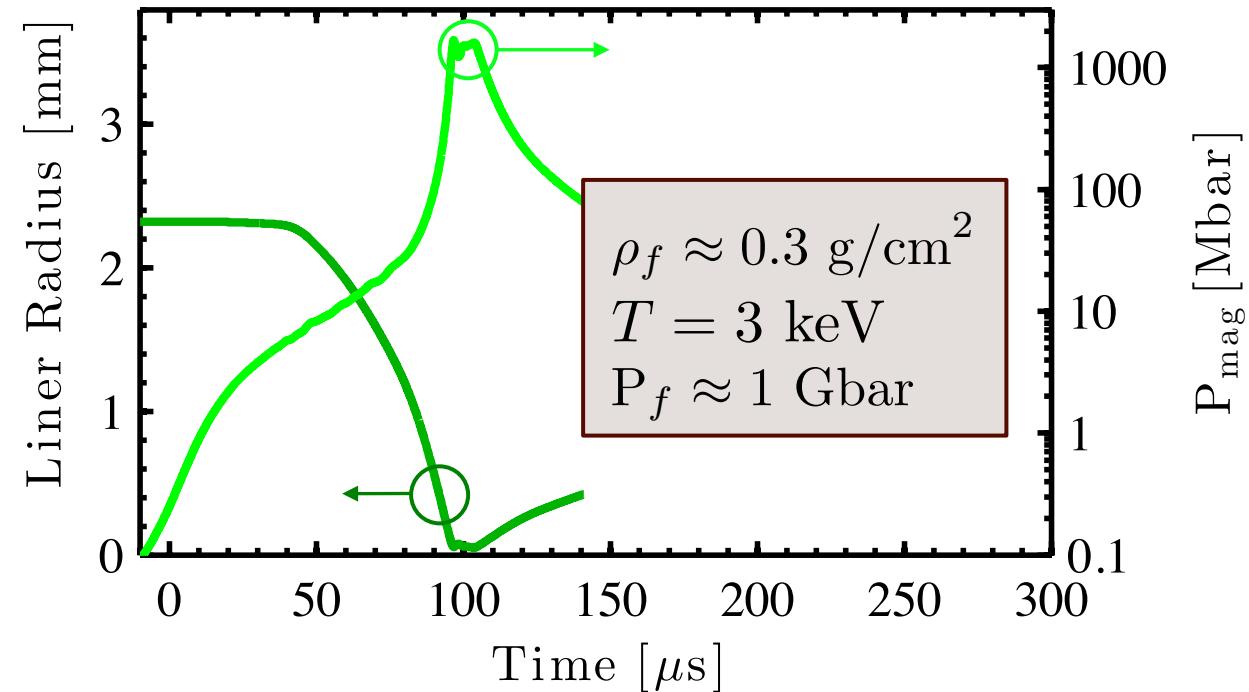
Very small fuel mass requires immense compression to obtain adequate confinement for burn

Laser direct drive or indirect drive is typically used to drive ICF implosions, but magnetically-driven cylindrical implosions are another efficient alternative

$$P = \frac{B^2}{2\mu_0} = 140 \cdot \left( \frac{I_{[\text{MA}]} / 30}{R(t)_{[\text{mm}]} } \right)^2 \text{ [Mbar]}$$



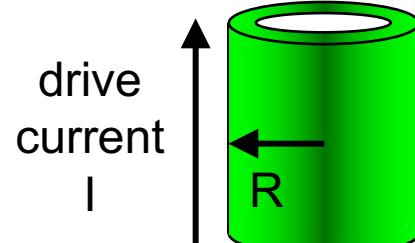
$$\rho \left( \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} \right) = \frac{\mathbf{J} \times \mathbf{B}}{c} - \nabla P$$



# Magnetic drive pressures on Z can be comparable to the drive pressure in radiation driven capsules

## Magnetically-Driven Cylinder

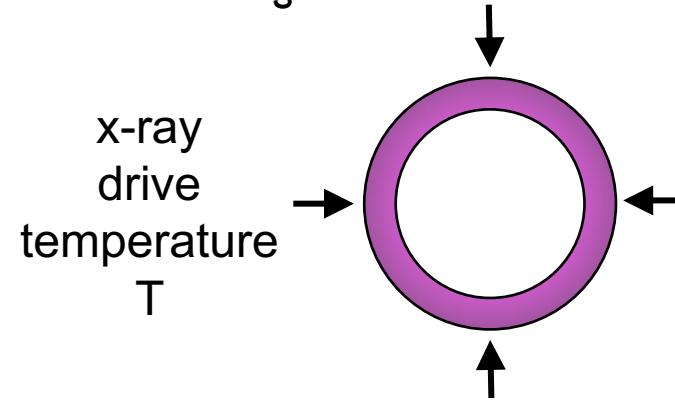
$$P = \frac{B^2}{2\mu_0} = 141 \left( \frac{I_{MA} / 30}{R_{mm}} \right)^2 \text{ MBar}$$



140 MBar at 30 MA and 1 mm

## Radiation-Driven Sphere

$$P = \frac{(2/5)(1-\alpha)\sigma T^4}{C_s} = 3T^{3.5} \text{ MBar}$$



140 MBar at 300 eV

# The Z machine employs relatively efficient pulsed power to create high energy density matter

1–4 kJ Z Beamlet Laser (ZBL)  
for radiography and  
MagLIF fuel preheating

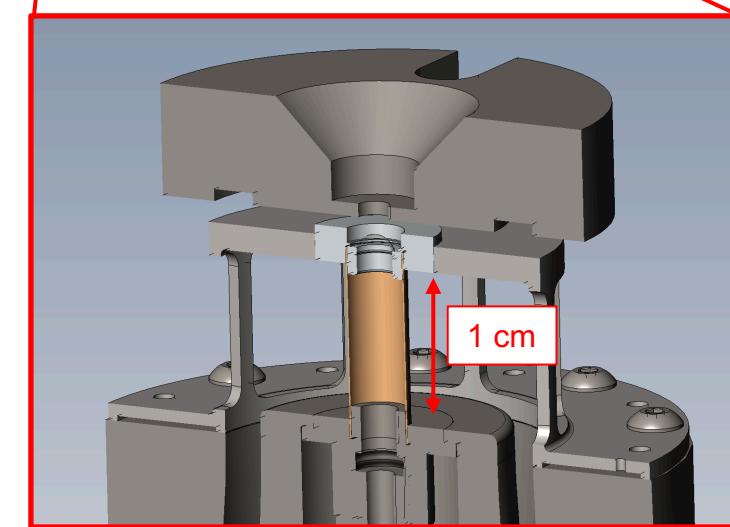
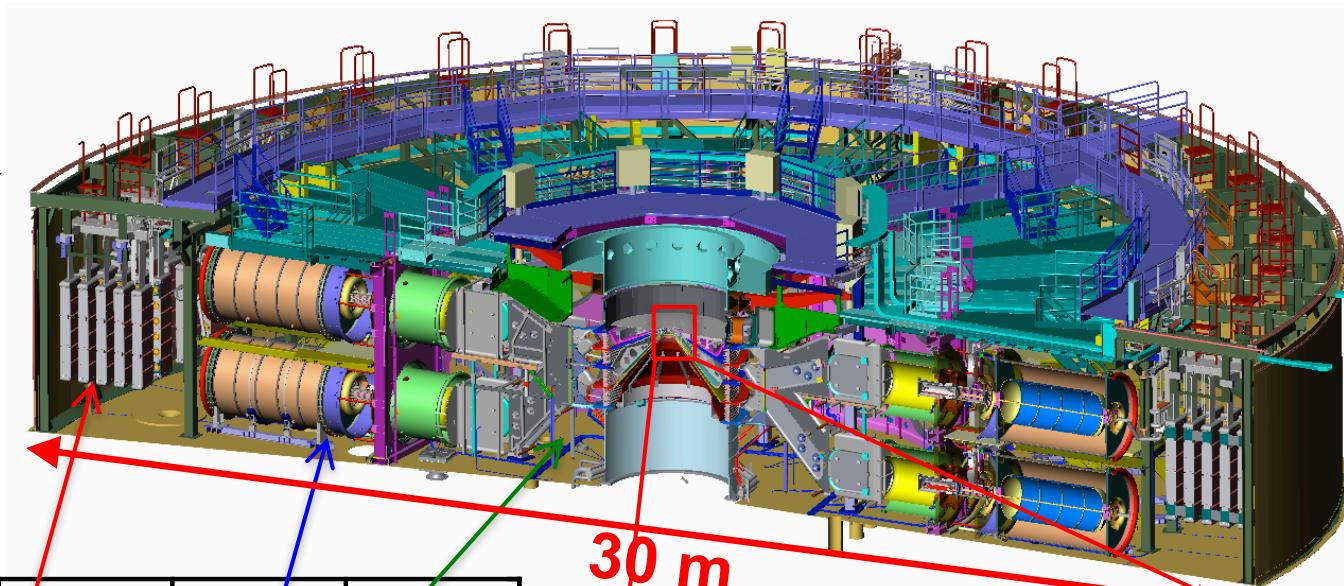
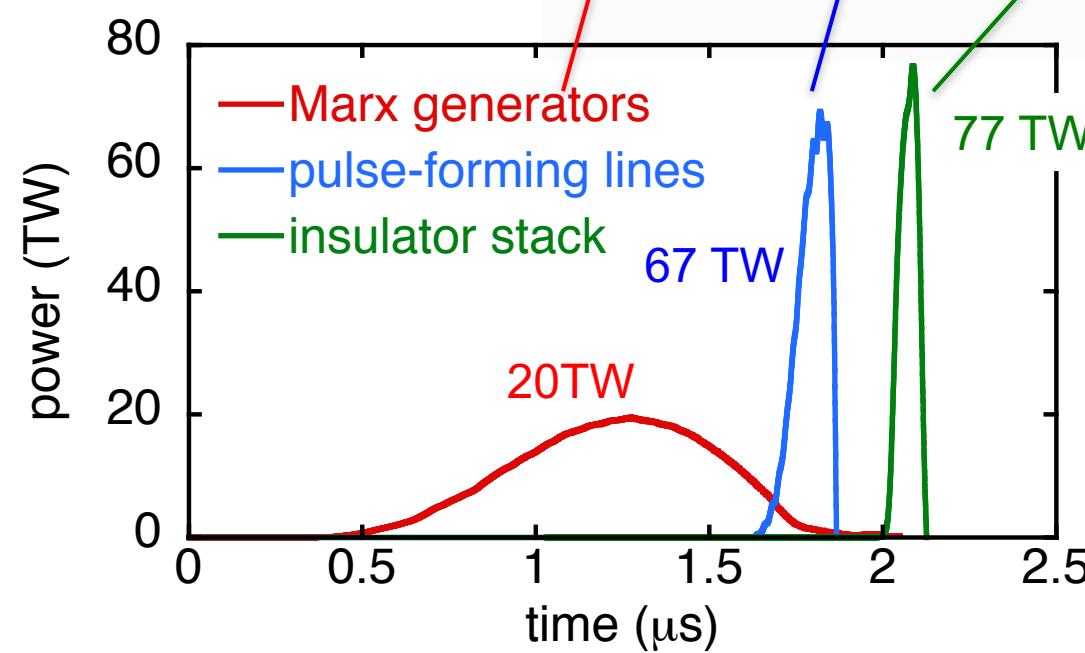
10,000 ft<sup>2</sup>



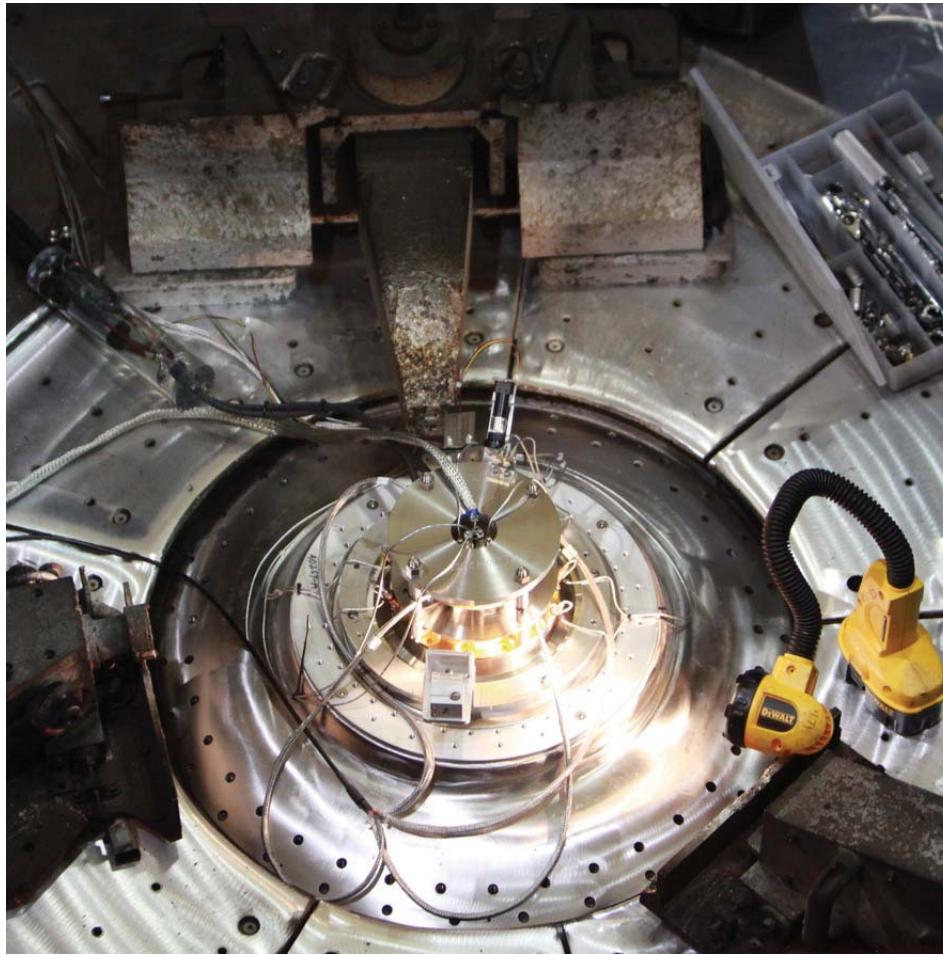
# Pulsed-power is all about energy compression in both space and time

Energy compression achieved by a sequence of storage and switching techniques :

- Voltages are added in series
- Currents are added in parallel



**Debris from MagLIF experiments must be carefully managed (several MJ energy release equivalent to few sticks of dynamite)**

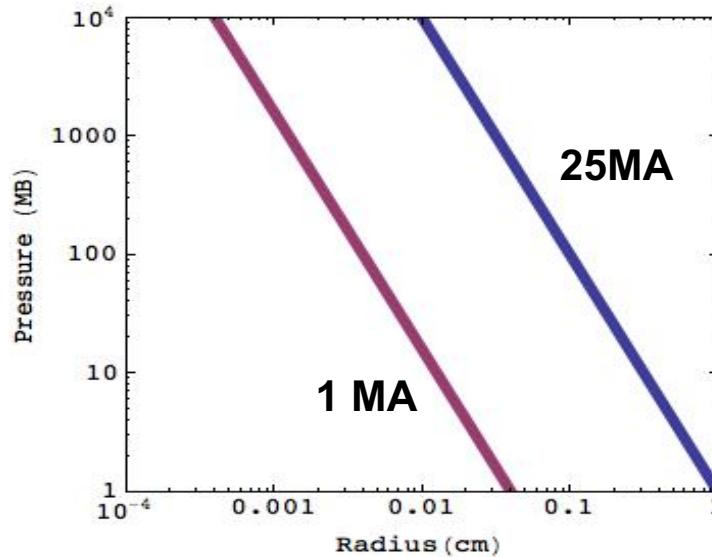


Pre-shot photo of coils & target hardware



Post-shot photo

# Magnetic implosions can efficiently perform work on the fuel while reaching very high pressures, if the current can reach small radius



$$B_\theta(G) \sim \frac{I(A)}{5R(cm)} \quad P \sim \frac{B^2}{8\pi} \sim \frac{I^2}{R^2}$$

A current carrying cylinder is driven more strongly the farther it converges

What limits current delivery to small radius?

- Ideal driver limits ( $dL/dt > 0$  eventually causes  $dI/dt < 0$ )
- Power flow losses
- Asymmetric current delivery (displacement of magnetic center from geometric center)
- 3D current redistribution
- Current shunting in target

A magnetic implosion continues to extract energy as it implodes:

$$E_{kin} \sim I^2 \log\left(\frac{R_0}{R_f}\right)$$

# Instabilities increase with amount of convergence and ultimately limit the achievable pressure

- Key challenge for all ICF concepts
- Rayleigh-Taylor (RT) instabilities occur along accelerating interfaces
- Cylindrical geometry requires higher convergence than spherical

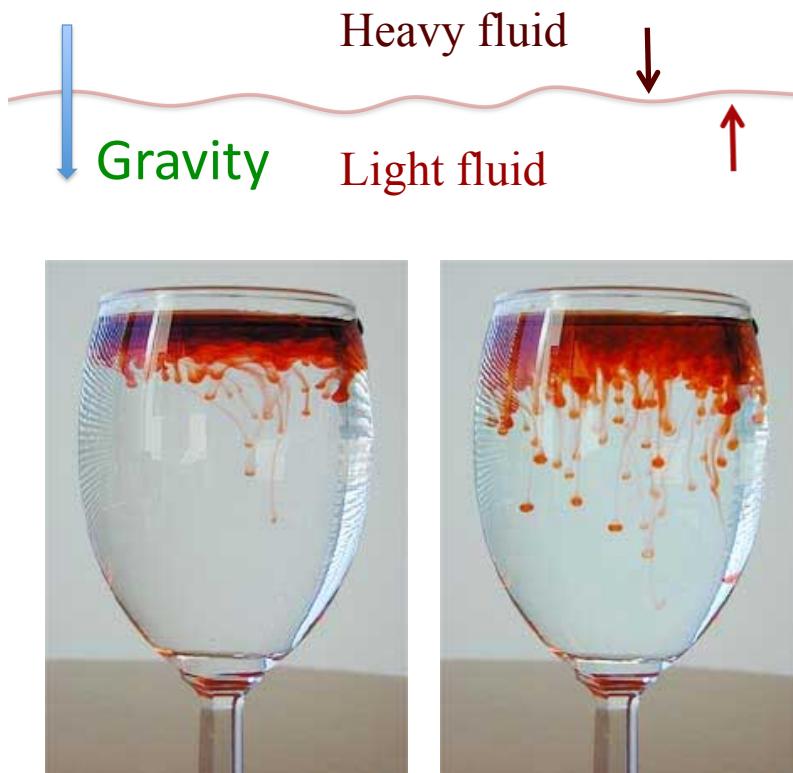


Image sources: physicscentral.com, large.stanford.edu

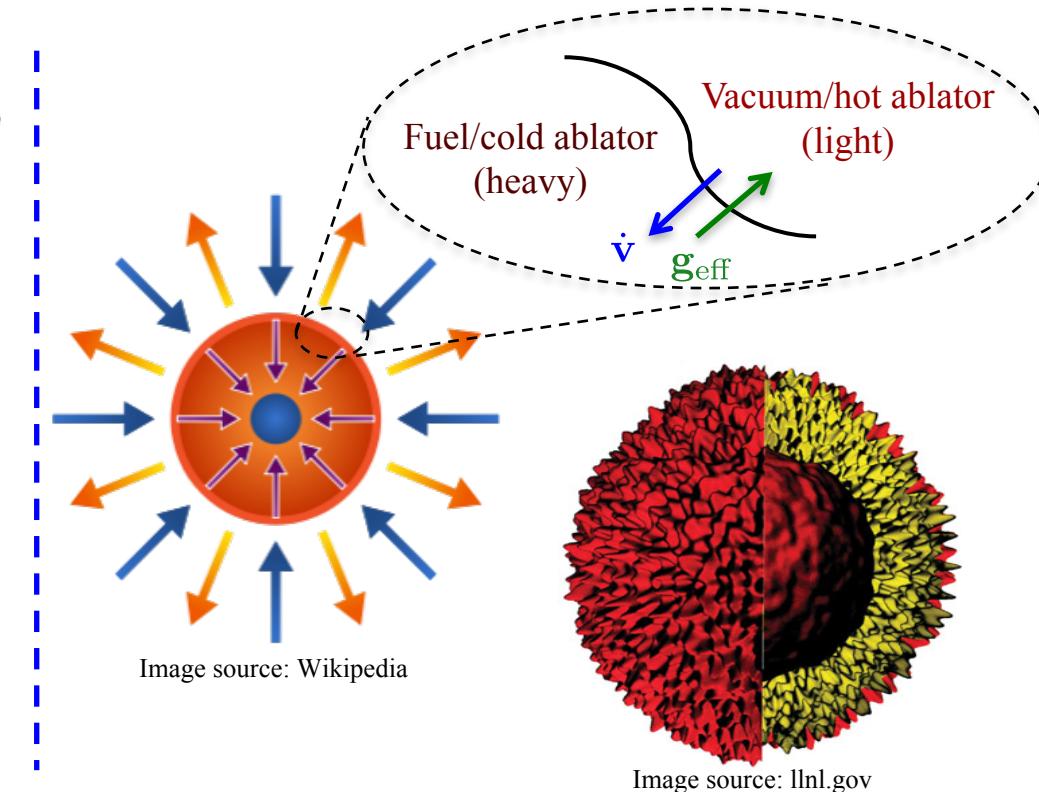
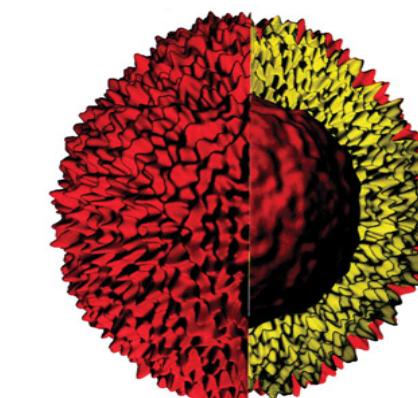


Image source: Wikipedia

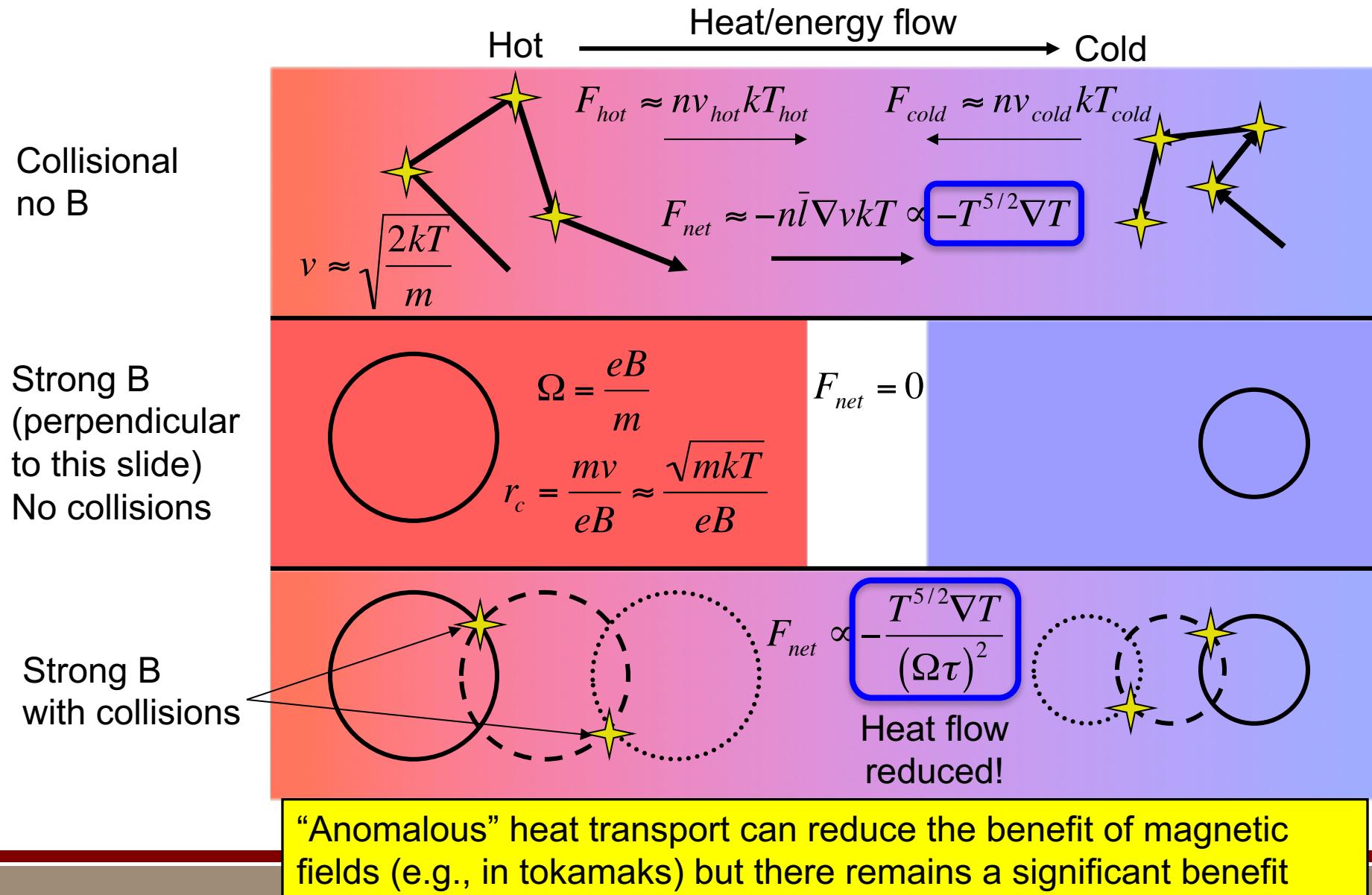


# Magneto-inertial Fusion attempts to operate in an intermediate fuel density space between magnetic confinement fusion and inertial confinement fusion



- Strategy:
  - Reduce fuel density (compared to ICF) to suppress radiation losses
  - Use a magnetic field to suppress the thermal conduction losses during compression (Not confine the plasma!)
  - Reduce required target convergence
- Requirements:
  - Magnetized fuel
  - Pre-heated fuel
  - Compression system
    - Pre-heated and pre-magnetized plasma compressed until fusion is achieved
- The terms **MTF** (Magnetized Target Fusion) and **MIF** (Magneto Inertial Fusion) generally used interchangeably

# Particle transport can be reduced by strong magnetic fields, even in collisional plasmas

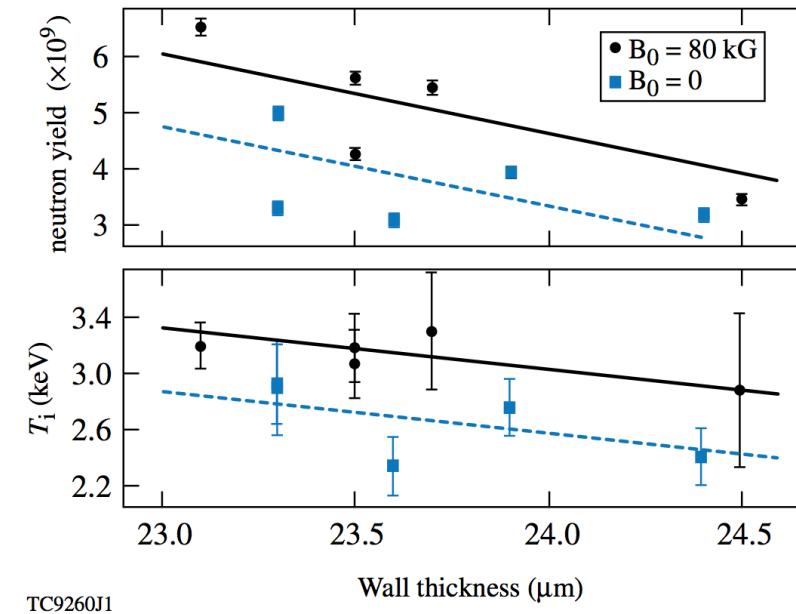
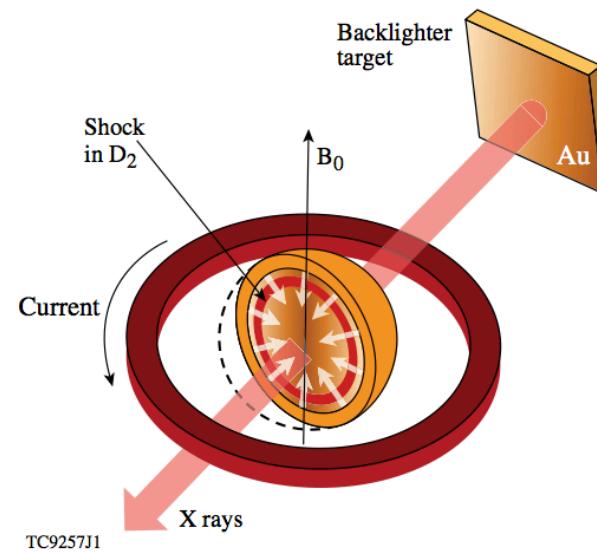


# The potential benefits of strong magnetic fields in fusing plasmas has been known for quite some time

- 1945 - Benefits of magnetized plasmas for fusing plasmas recognized
  - “A possible method of cutting down the conduction to the walls would be the application of a strong magnetic field,  $H$ . This tends to make the electrons go in circles between collisions, so impedes their mobility. Actually, it makes them go in spirals, and does not reduce the conductivity parallel to  $H$  but only to the other two dimensions, so one would probably want to design the container elongated in the direction of  $H$ , or even toroidal...with the lines of force never leaving the deuterium...rather large fields will be required...thus a field in excess of 20,000 gausses would help reduce conduction loss.” - **Enrico Fermi**, "Super Lecture No. 5--Thermal Conduction as Affected by a Magnetic Field," Los Alamos Report 344, Sept. 17, 1945.
- 1949 - R. Landshoff, Phys. Rev. 76, 904

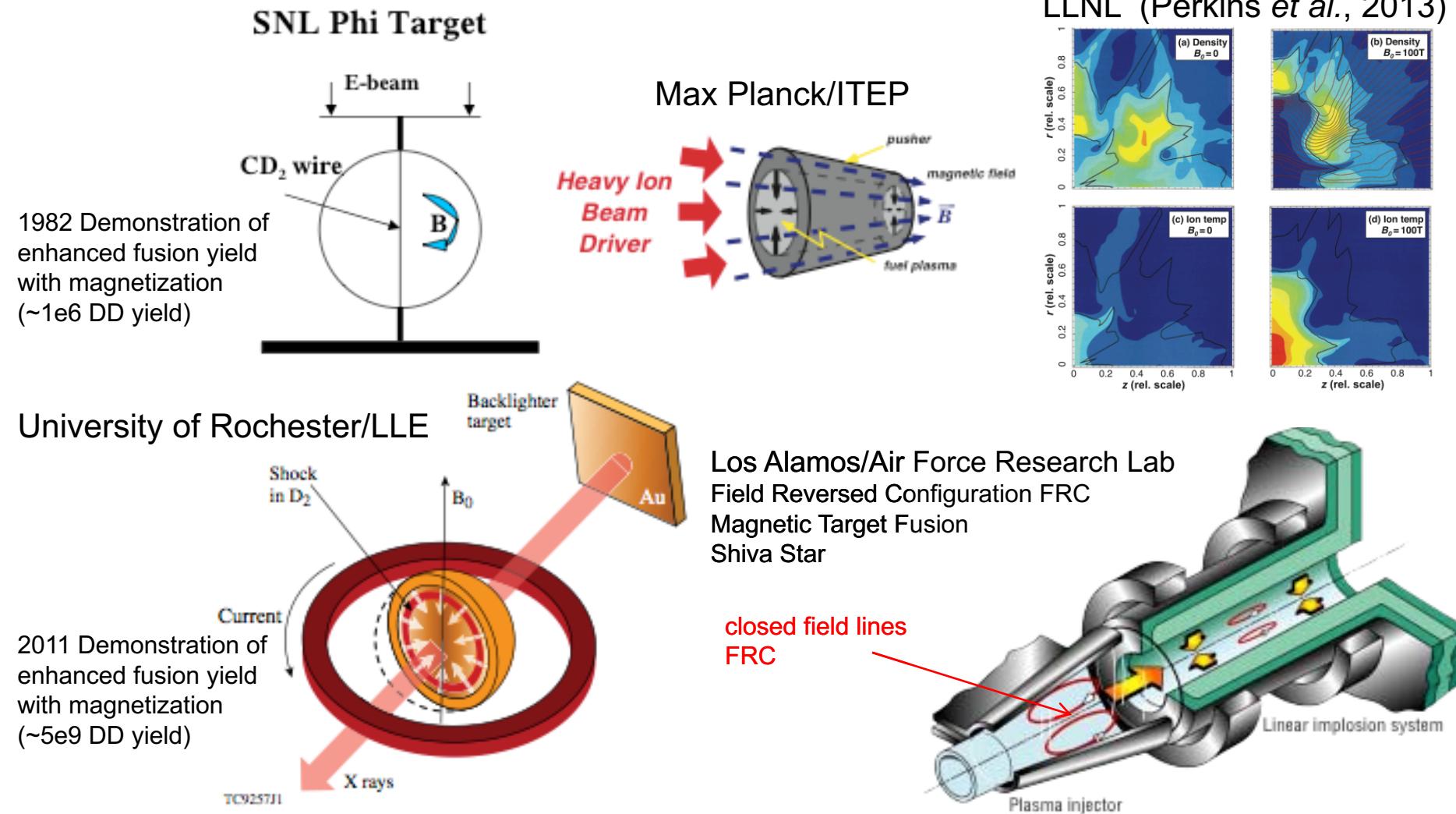


# Laser-driven spherical capsule implosions at the University of Rochester\* showed clear indicators of higher temperatures (and yields) due to fuel magnetization



- Simple axial field used in a spherical implosion geometry
- Field suppressed electron heat conduction losses along one direction
- The resulting 30% increase in temperature and 15% increase in yield is consistent with rough estimates for heat loss suppression

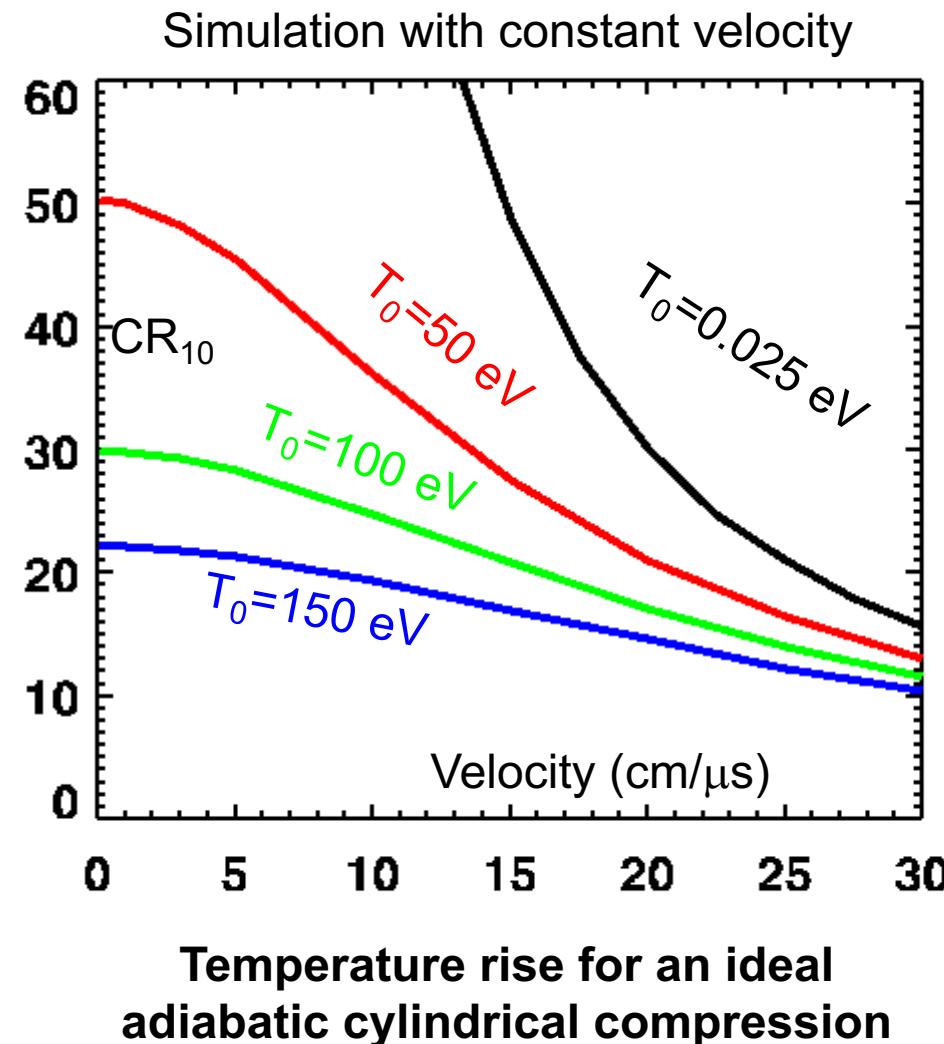
Many groups have proposed using magnetic fields to help with pulsed fusion concepts, however all have been relatively small efforts.



# There is a resurgence of interest in magneto-inertial fusion research in the United States

- **Currently supported ARPA-E MIF projects in the USA (\$30M)**
  - California Institute of Technology & Los Alamos National Laboratory
  - Helion Energy, Inc.
  - Lawrence Berkeley National Laboratory & Cornell University
  - Los Alamos National Laboratory & Hyper V Technologies (~100 ns)
  - Magneto-Inertial Fusion Technologies, Inc.
  - NumerEx, LLC & National High Magnetic Field Laboratory
  - Sandia National Laboratories & University of Rochester (~1-10 ns)
  - Swarthmore College & Bryn Mawr College
  - University of Washington & Lawrence Livermore National Laboratory
- **Other MIF projects are also pursued:**
  - General Fusion
  - Tri-alpha
  - Los Alamos National Laboratory & Air Force Research Laboratory (~10  $\mu$ s)
- **Other countries also interested in MIF (e.g., Russian MAGO concept)**

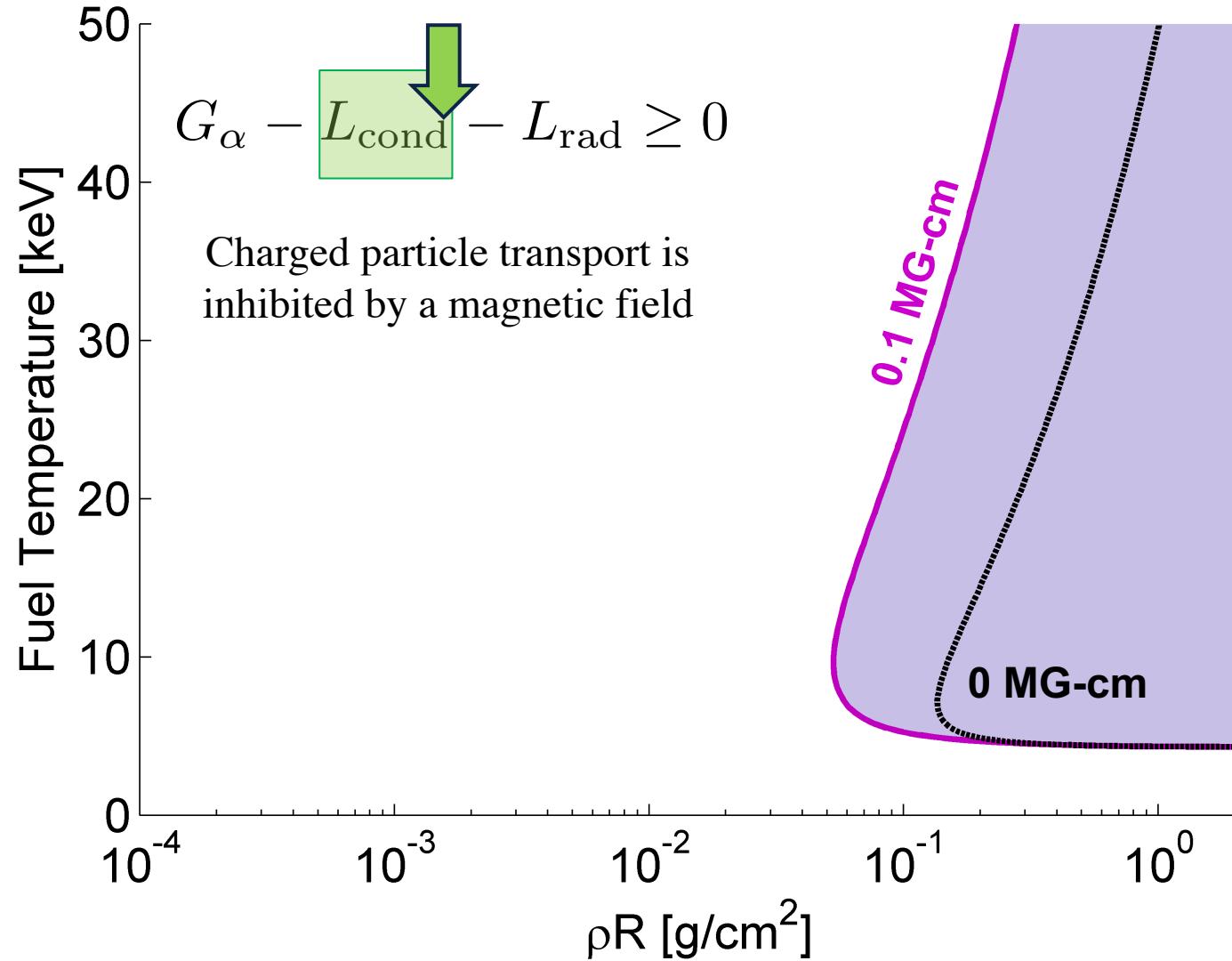
# Preheating the fuel enables fusion temperatures to be achieved with less compression



- CR<sub>10</sub> = Convergence Ratio ( $R_0/R_f$ ) needed to obtain 10 keV (ignition) with no radiation losses or conductivity
- Only possible if electrons are magnetized throughout the implosion!
- Magneto-inertial fusion concepts attempt to adiabatically compress the fuel to ignition

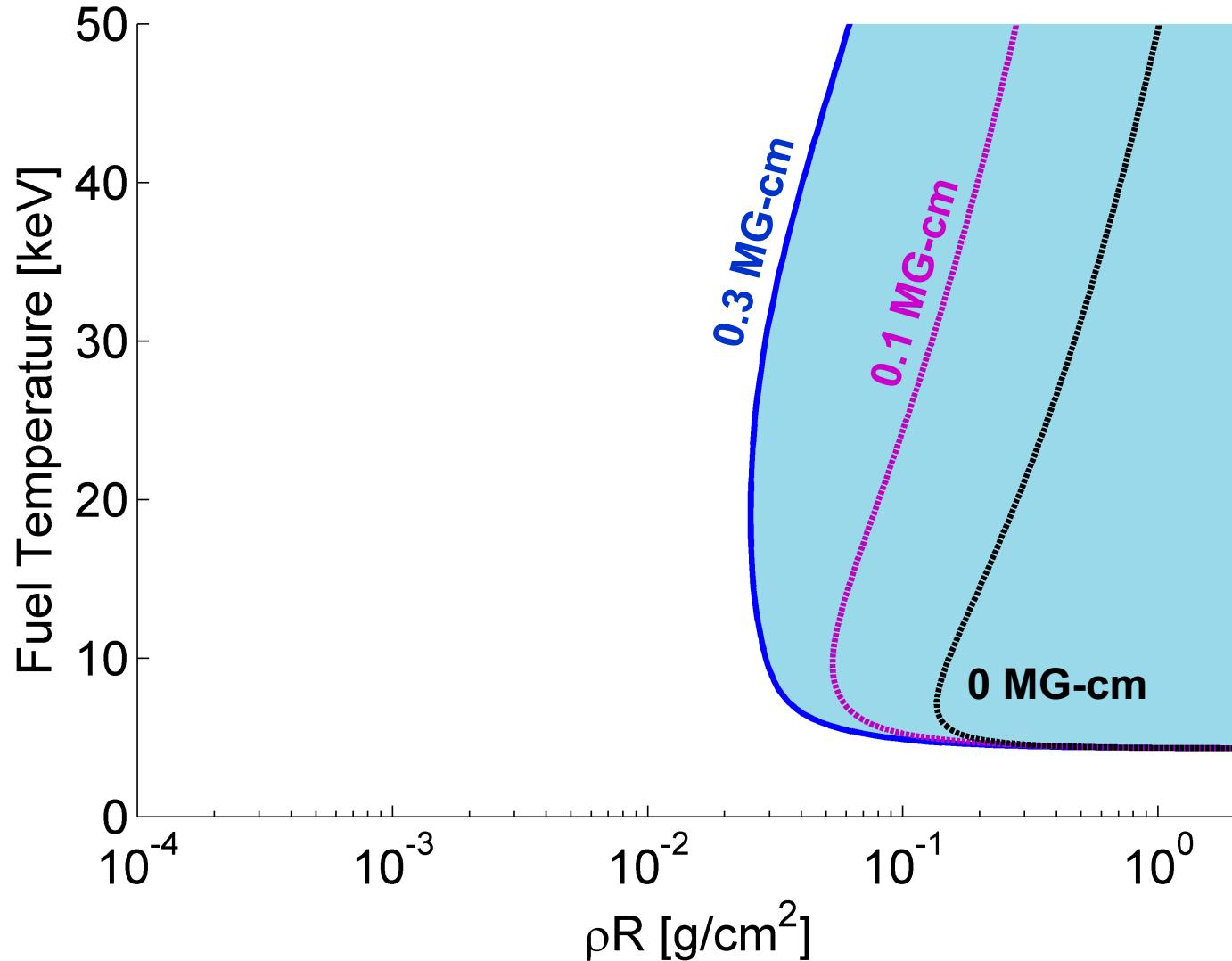
$$T = T_0 (r_0/r_f)^{4/3}$$

# Magneto-inertial fusion (MIF) utilizes magnetic fields to relax the stagnation requirements of ICF



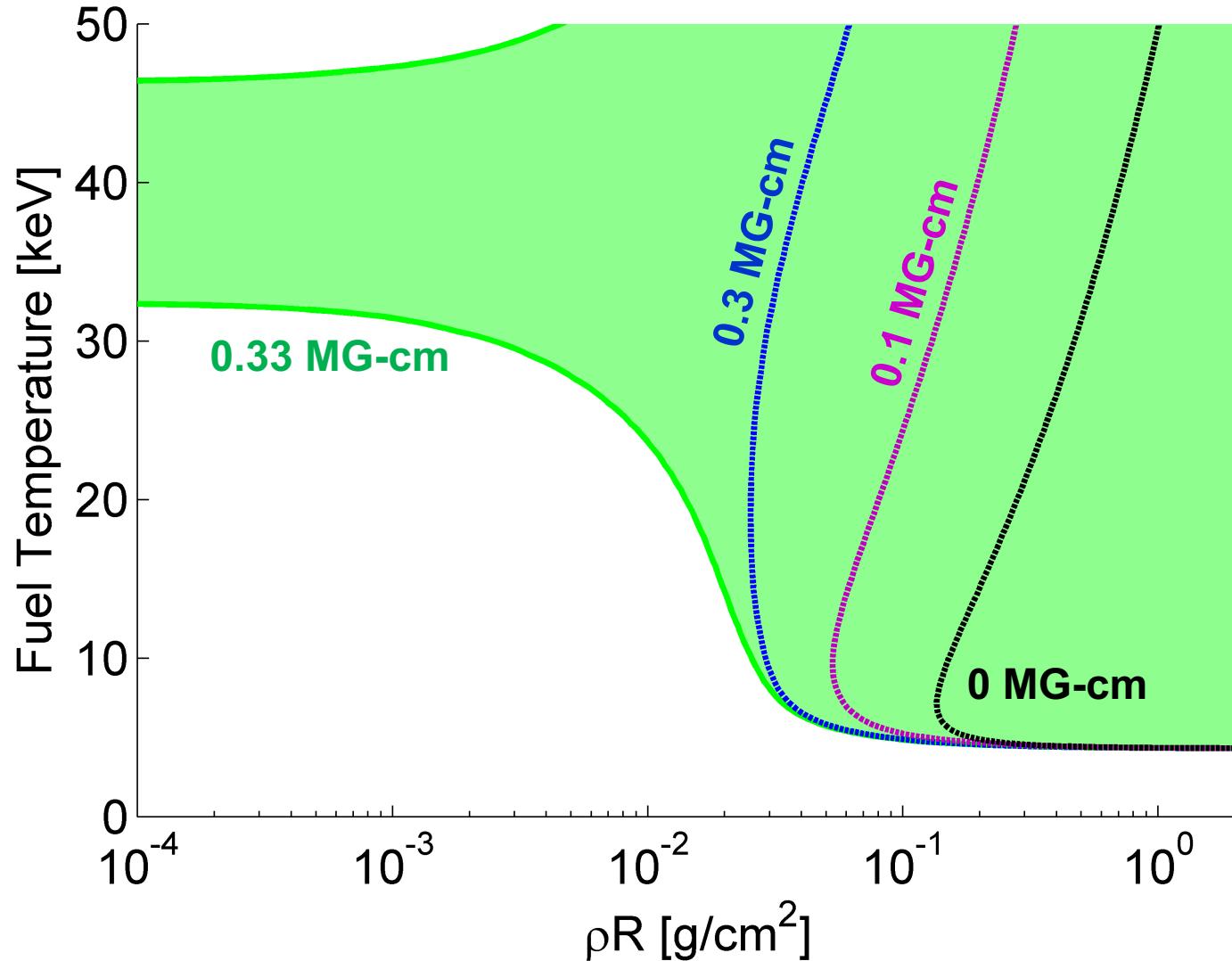
- Applying a magnetic field opens up a larger region of parameter space – confinement time increases
- This is sufficient field to neglect electron thermal conduction loss
- Note: The minimum temperature does not change because it is driven by radiation losses

# Magneto-inertial fusion (MIF) utilizes magnetic fields to relax the stagnation requirements of ICF



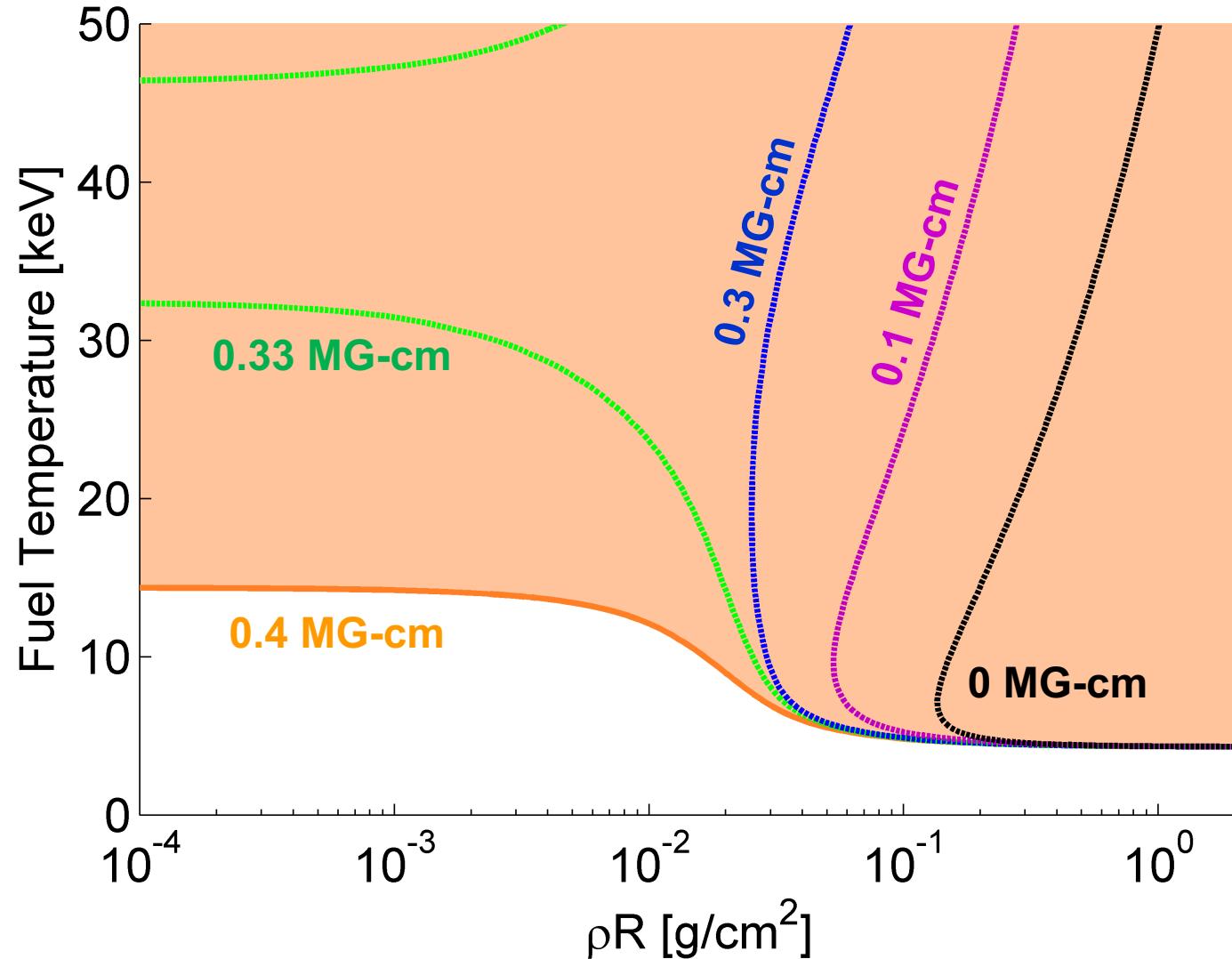
- This is sufficient field to neglect ion thermal conduction losses
- The Larmor radius of fusion alphas is approximately the radius of the fuel

# Magneto-inertial fusion (MIF) utilizes magnetic fields to relax the stagnation requirements of ICF



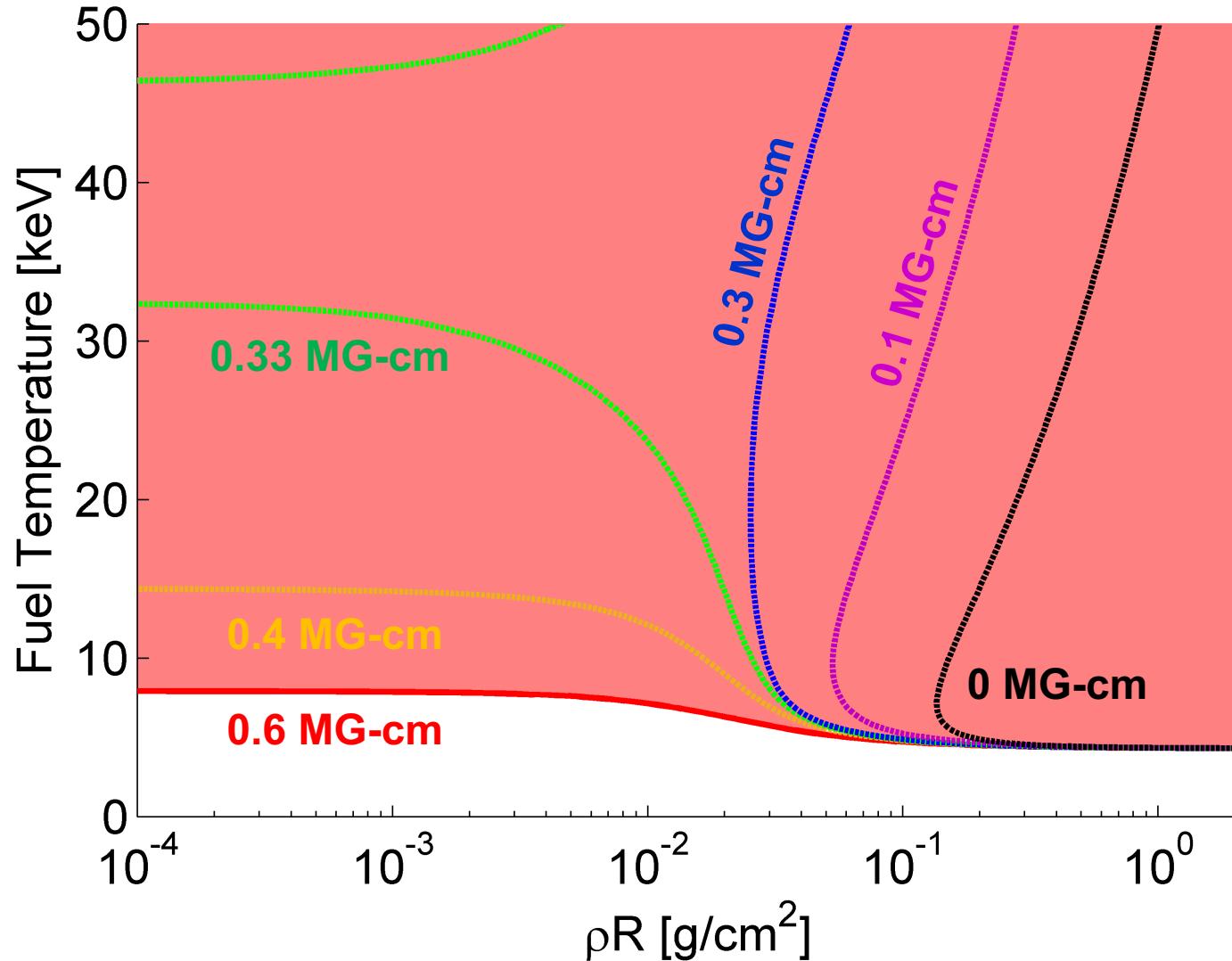
- There are dramatic gains for small changes in the field when the Larmor radius is slightly less than the fuel radius
- Substantial increase in the fusion energy trapped in the fuel

# Magneto-inertial fusion (MIF) utilizes magnetic fields to relax the stagnation requirements of ICF



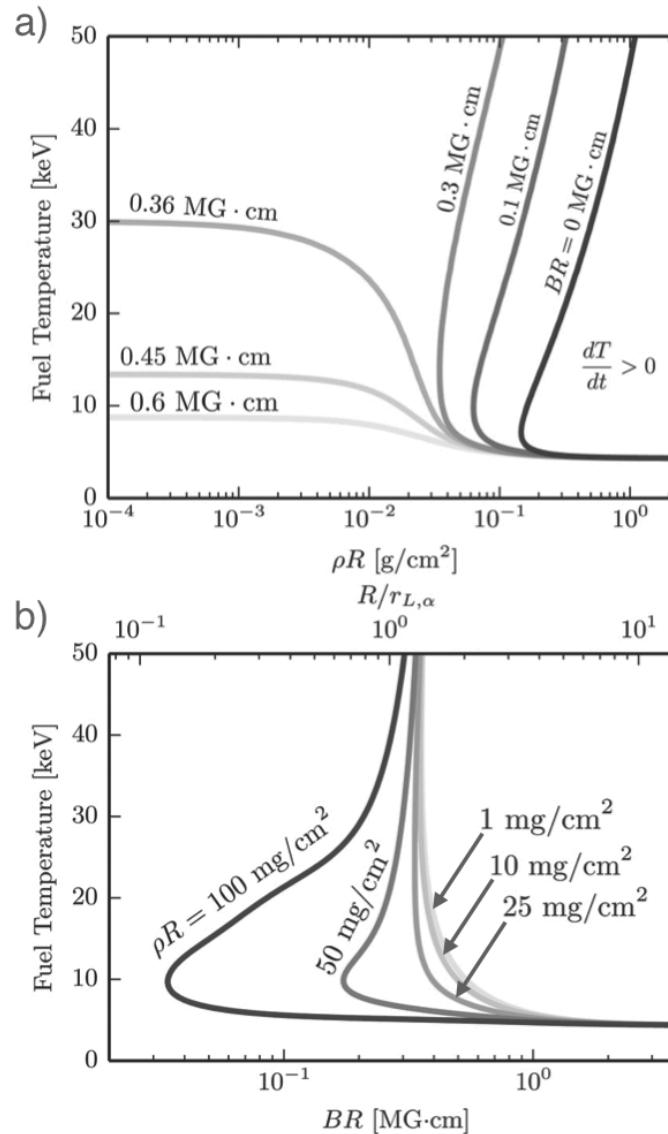
- As field increases, confinement of the charged fusion-products is achieved through the magnetic field rather than the areal density

# Magneto-inertial fusion (MIF) utilizes magnetic fields to relax the stagnation requirements of ICF

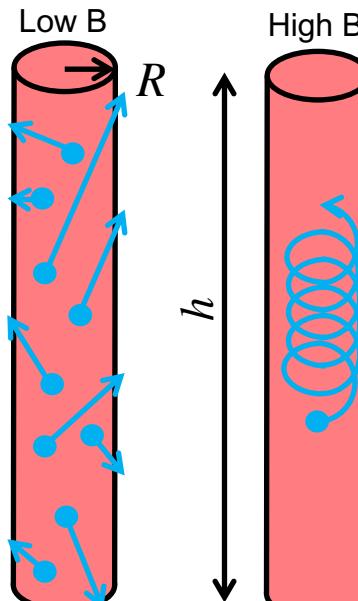


- When the Larmor radius is about half of the fuel radius, the effect begins to saturate
- This means there is an optimal field for a given fuel configuration

# In MIF, charged particle confinement is determined by the magnetization (“BR”) and not the fuel areal density (“ $\rho R$ ”) as in ICF



$$\frac{R}{r_\alpha} = \frac{BR [T \cdot \text{cm}]}{26.5} = \frac{BR [G \cdot \text{cm}]}{2.65e5} \approx 4BR [\text{MG} \cdot \text{cm}]$$

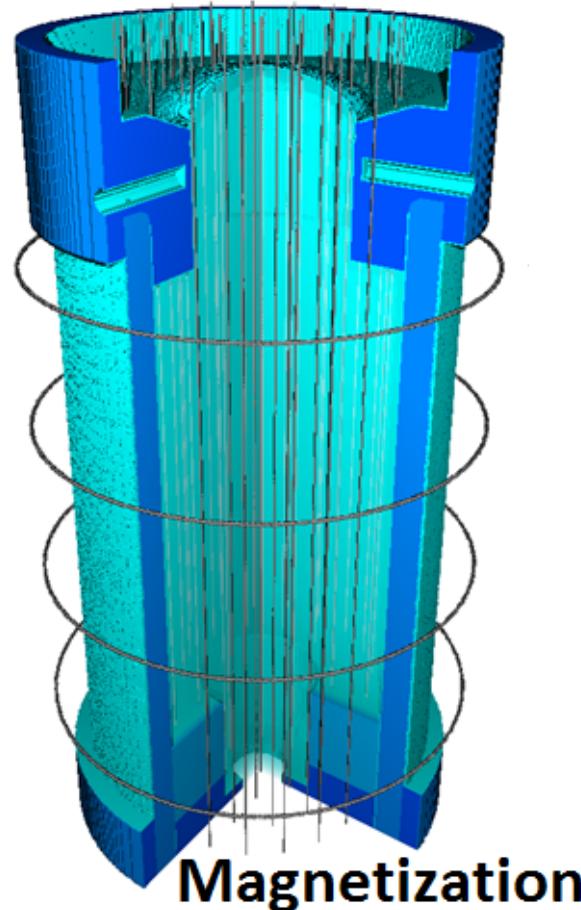


Fraction of trapped  $\alpha$ 's (tritons) is a function of **BR** only

At  $BR > 0.5$  MG-cm the effects saturate (particles are well confined).

However, areal density of the **liner** compressing the fuel is also important to the inertial confinement of the liner/fuel assembly

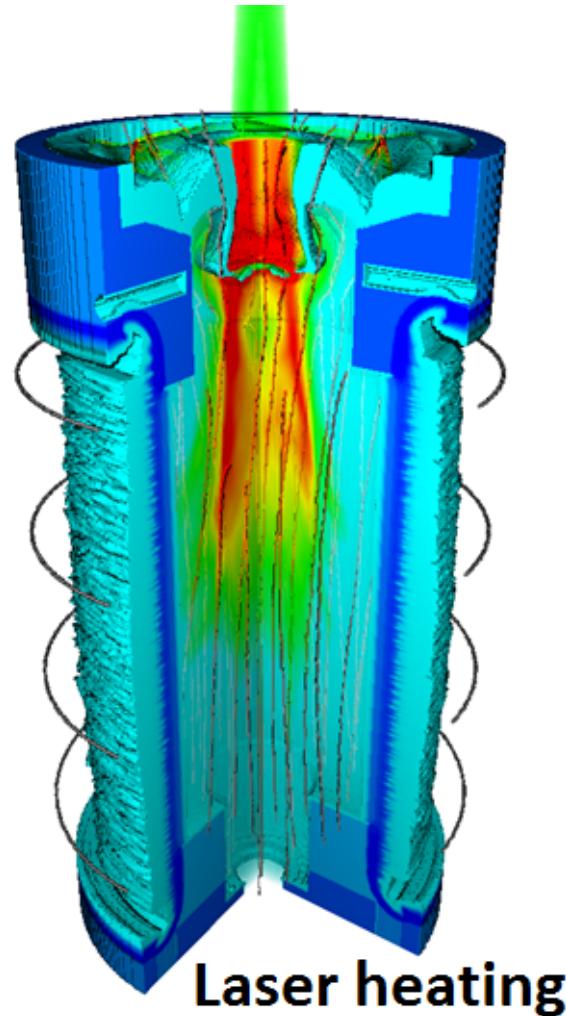
MagLIF<sup>[1,2]</sup> is an MIF concept that relies on three stages to heat, compress and confine fusion fuel



## Stage 1: Magnetization

- Be liner containing fusion fuel
  - $D_2$  gas  $\sim mg/cc$  ( $n_e/n_{crit} < 0.1$ )
- Axial magnetic field is applied to target
  - 100-300 kG
  - $\sim ms$  risetime
- Z current starts creating an azimuthal drive field

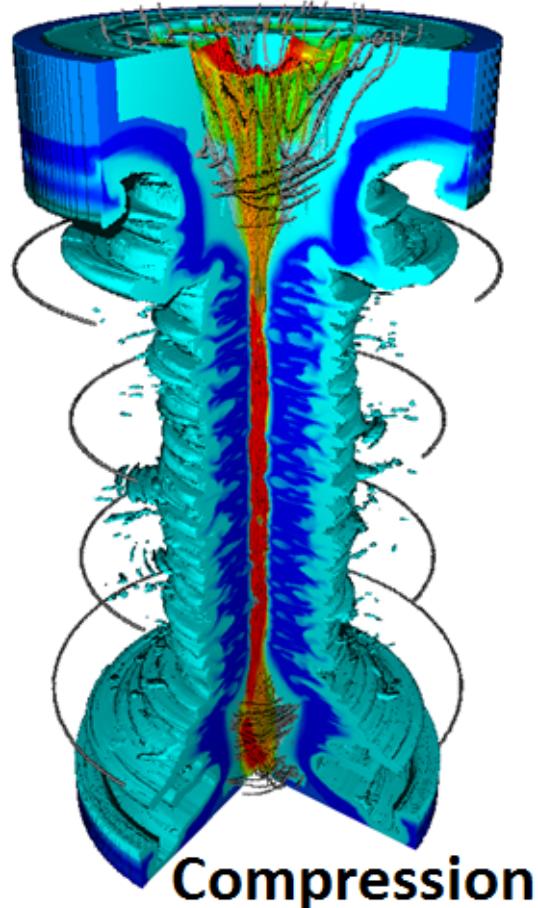
MagLIF<sup>[1,2]</sup> is an MIF concept that relies on three stages to heat, compress and confine fusion fuel



## Stage 2: Laser Heating

- **Liner begins to compress**
  - OD is moving but ID is stationary
- **Laser heats the fuel**
  - $T_e \sim 100s$  of eV
- **Liner ID begins to implode**
- **Simulations indicate that fuel conditions isotropize over the 10s of ns of the implosion**

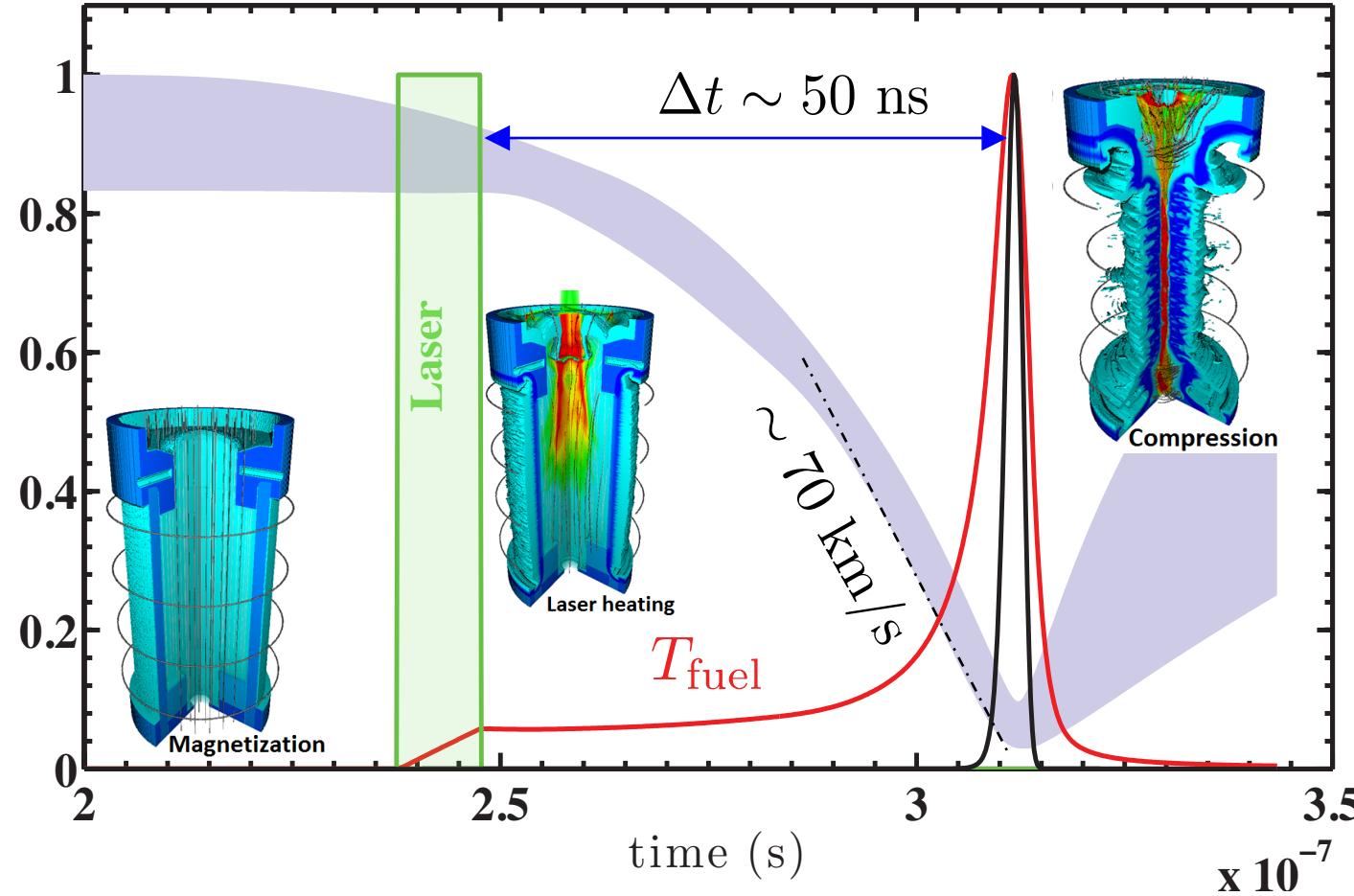
MagLIF<sup>[1,2]</sup> is an MIF concept that relies on three stages to heat, compress and confine fusion fuel



## Stage 3: Compression

- Axial magnetic field insulates fuel from liner throughout implosion
  - Field increases substantially through magnetic flux compression
- Fuel is heated through  $PdV$  work to keV temperatures
- Liner stagnates
  - Plasma pressure exceeds drive pressure

# Magnetization and preheat reduce peak velocity required for ignition compared to traditional ICF

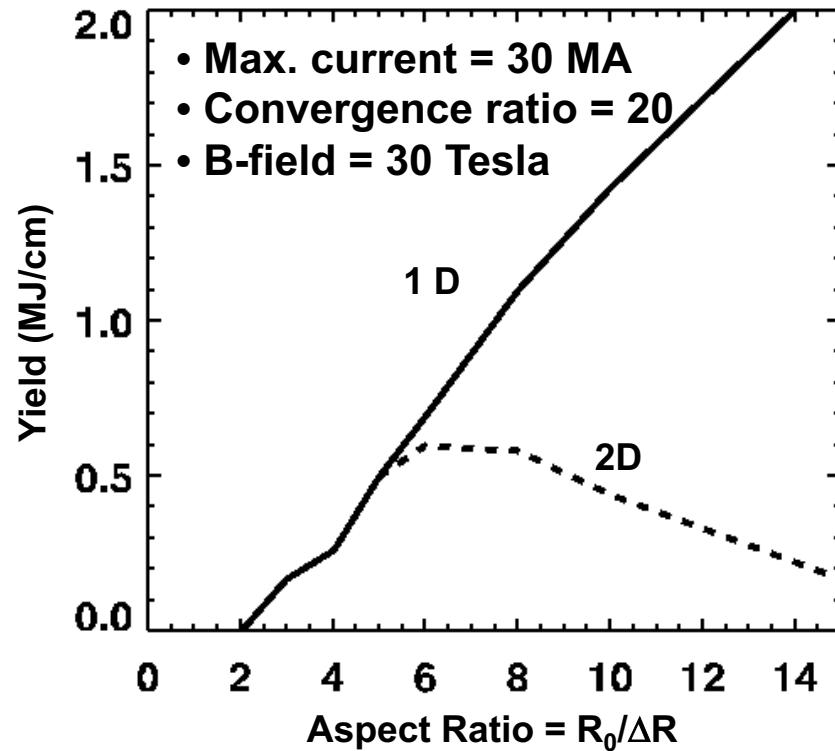


- Magnetization confines 3.5 MeV  $\alpha$ -particles at lower  $\rho R$
- Preheating + magnetization allows ignition temperature to be reached at a lower implosion velocity<sup>[1]</sup>

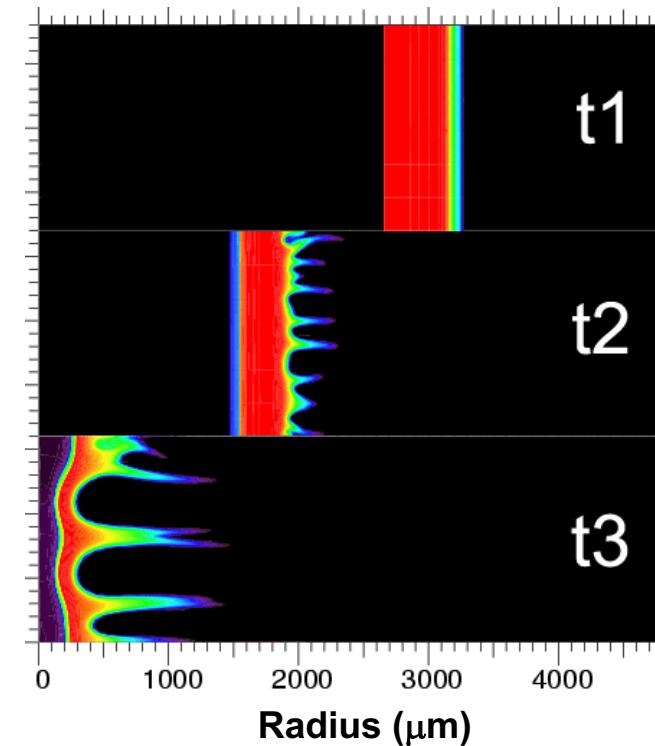
[1] S. A. Slutz, *et al.*, Phys. Plasmas **17** 056303 (2010)

[2] S. A. Slutz, and R.A. Vesey, PRL **108**, 025003 (2012)

# Reducing the implosion velocity requirements through fuel heating and magnetization allows us to use thicker, more massive liners to compress the fuel that are more stable

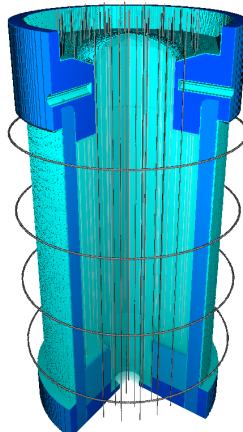


- The Magneto-Rayleigh-Taylor instability degrades the yield as the aspect ratio is increased (due to decreased liner  $\rho R$ )



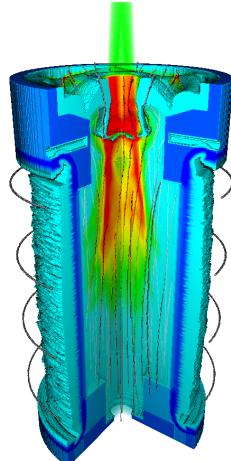
- Simulations of AR=6 Be liner show reasonably uniform fuel compression and sufficient liner  $\rho R$  at stagnation to inertially confine the fuel

# MagLIF experiments are complicated to field and analyze



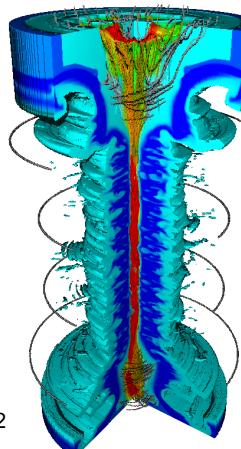
## Magnetization

- 10-30 T axial B-field
- 3 ms risetime
- $\sim 1 \text{ mg/cm}^3$  initial density



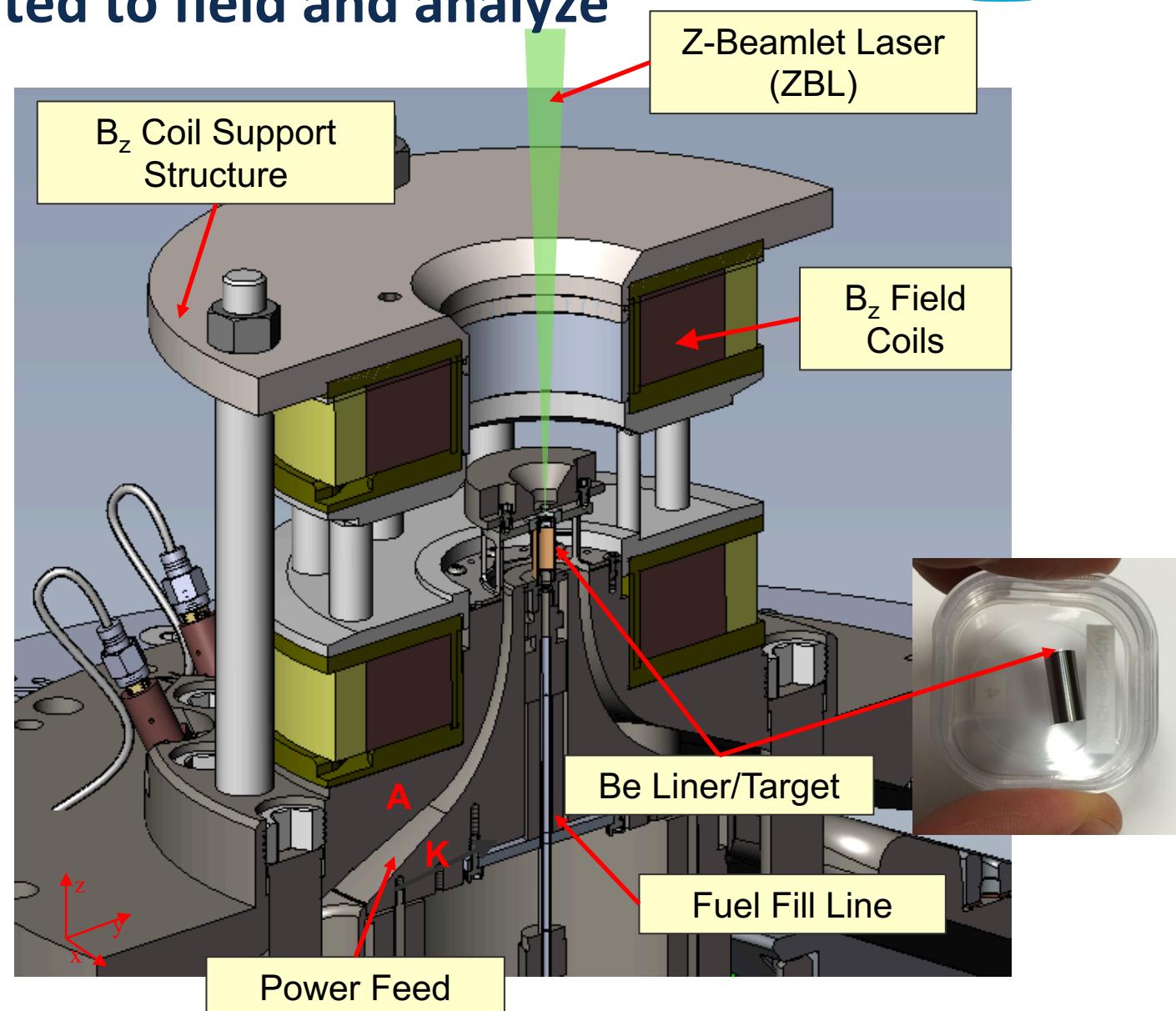
## Laser Heating

- 1-4 kJ, 1-4 ns
- $2\omega$ , f/10 beam
- $\sim 50$  ns from preheat to stagnation

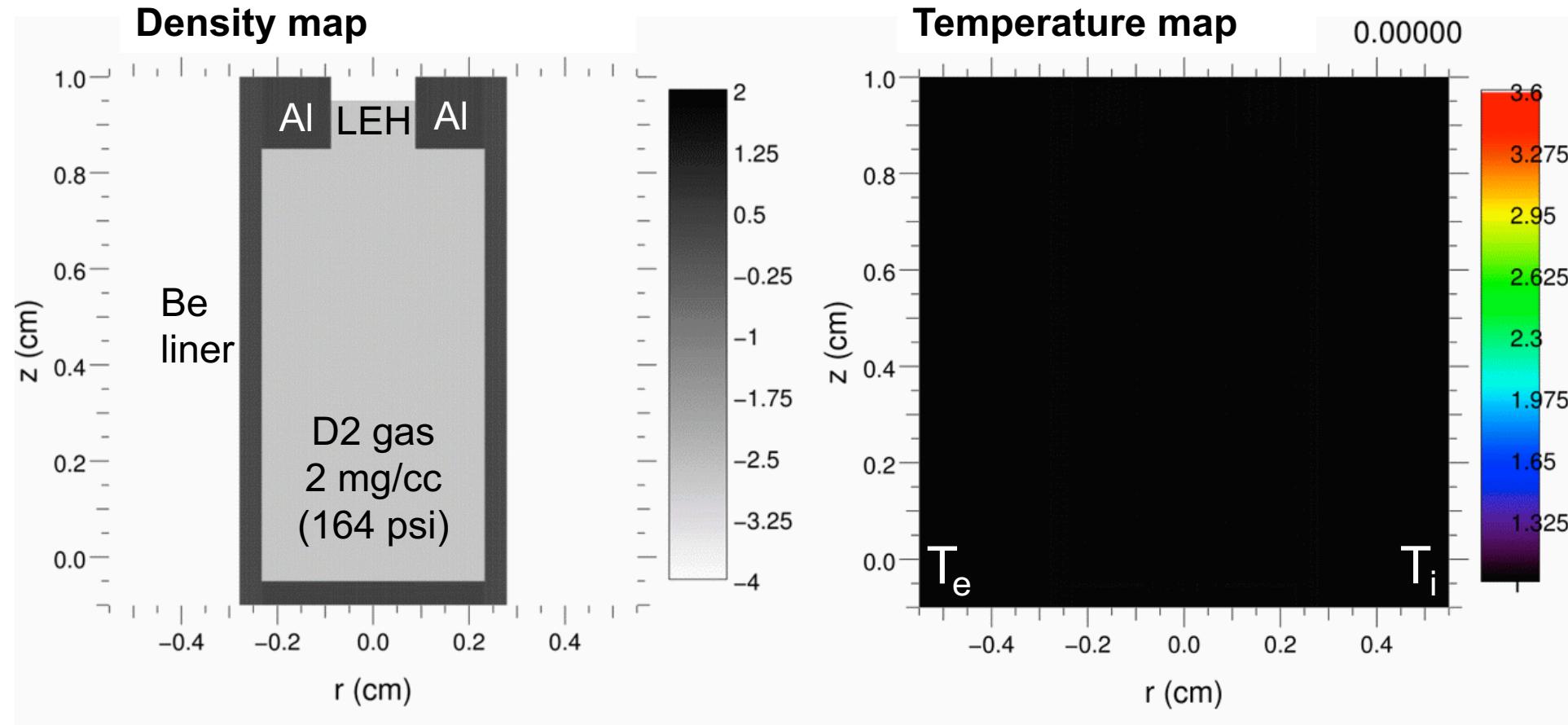


## Implosion and Stagnation

- CR = 25-40
- Burn duration 1-2 ns
- Flux compression  $>> 100x B_0$
- $\rho R_f \sim 0.01 \text{ g/cm}^2$ ,  $\rho L_f \sim 1 \text{ g/cm}^2$

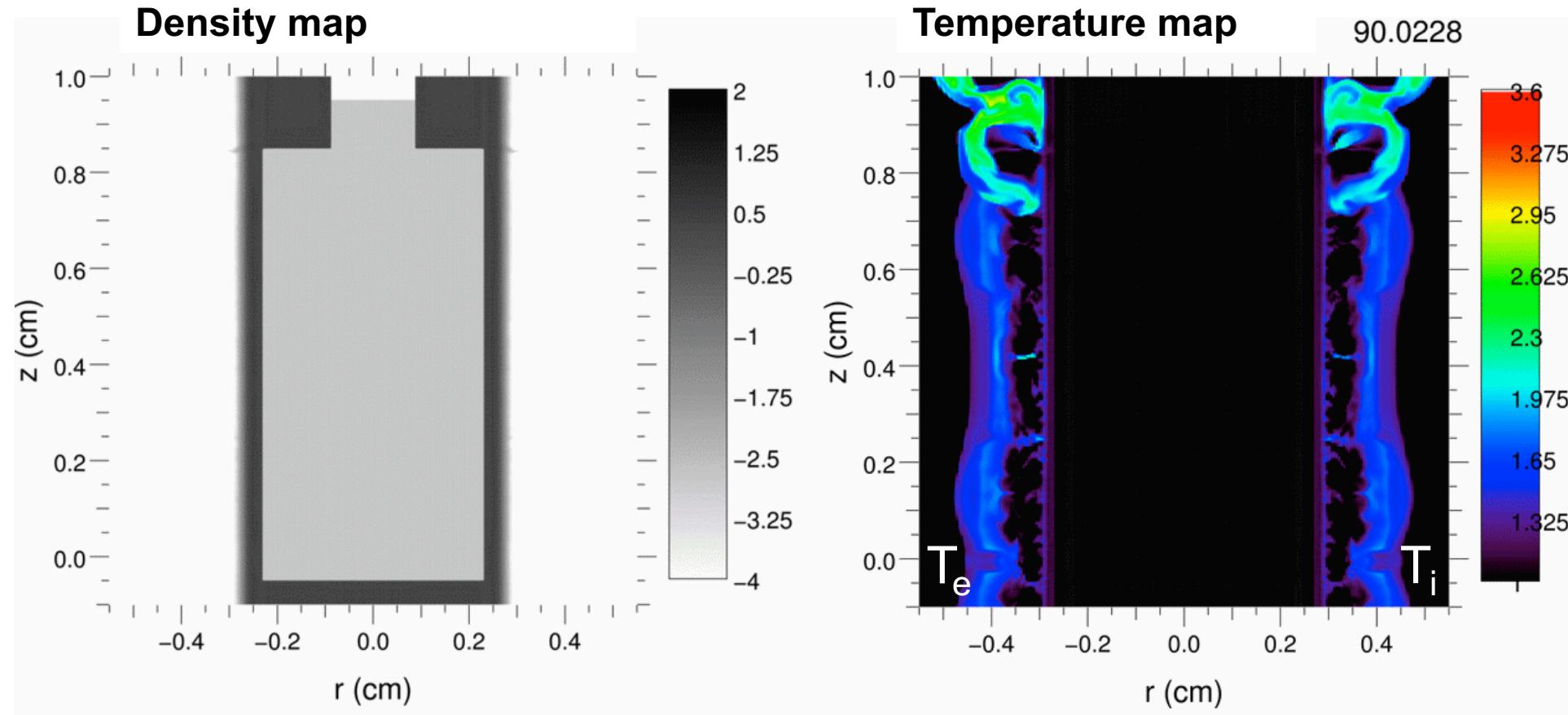


## An example fully integrated 2D HYDRA calculation illustrates the stages of a MagLIF implosion



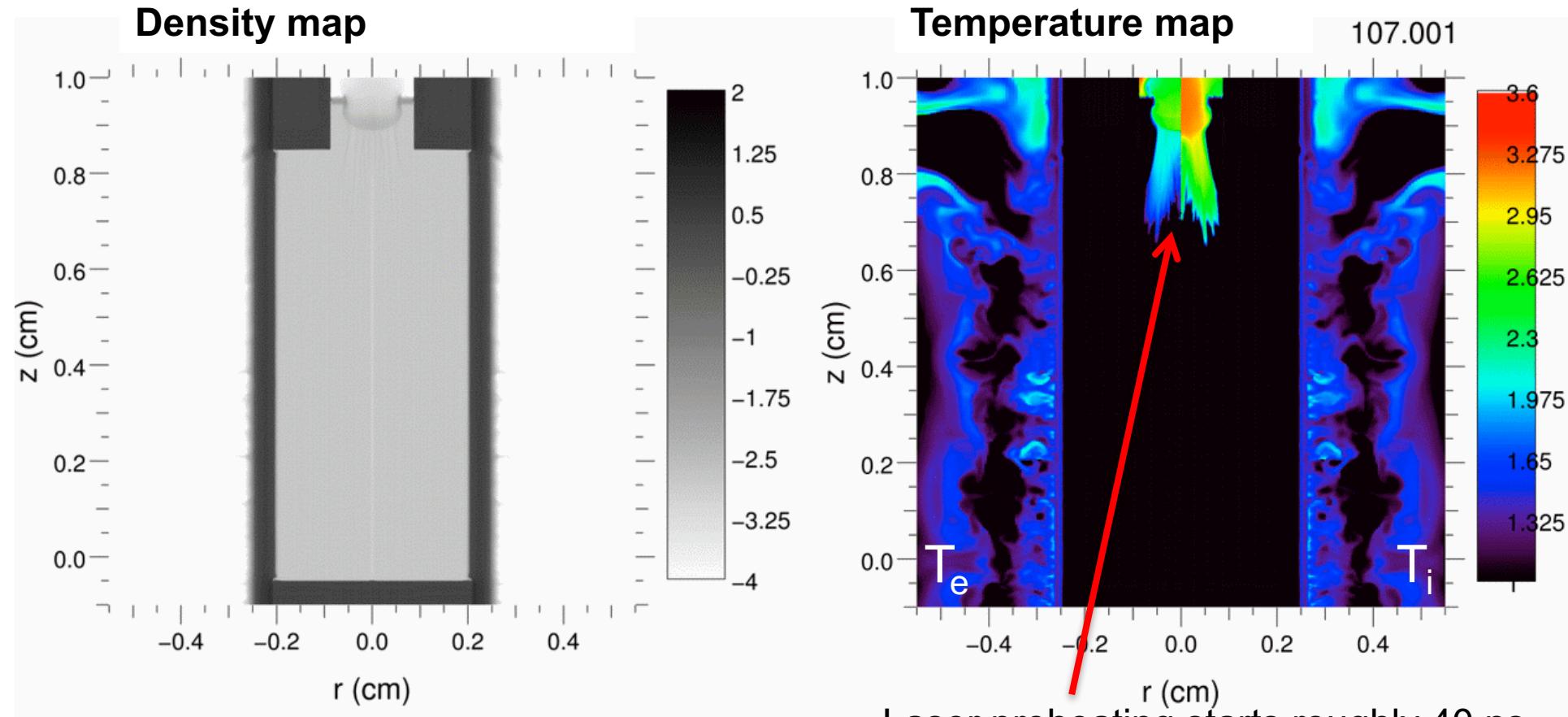
Example calculations by A.B. Sefkow: DD fuel,  $I=18$  MA,  $B_z=10$  T,  $E_{LASER}=2.6$  kJ

# The fusion fuel is preheated using the Z-Beamlet laser after the liner begins to implode



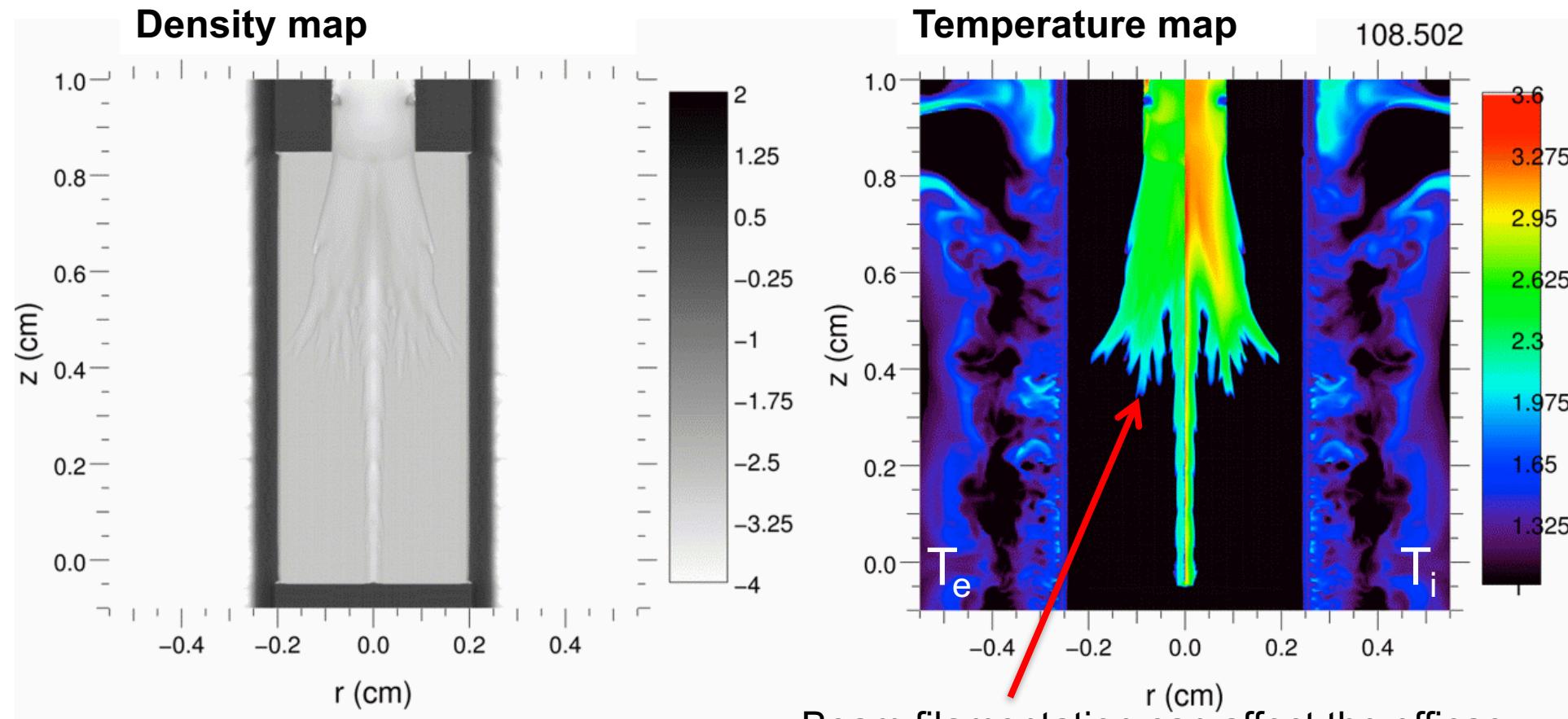
Example calculations by A.B. Sefkow: DD fuel,  $I=18$  MA,  $B_z=10$  T,  $E_{\text{LASER}}=2.6$  kJ

# The fusion fuel is preheated using the Z-Beamlet laser after the liner begins to implode



Example calculations by A.B. Sefkow: DD fuel,  $I=18$  MA,  $B_z=10$  T,  $E_{\text{LASER}}=2.6$  kJ

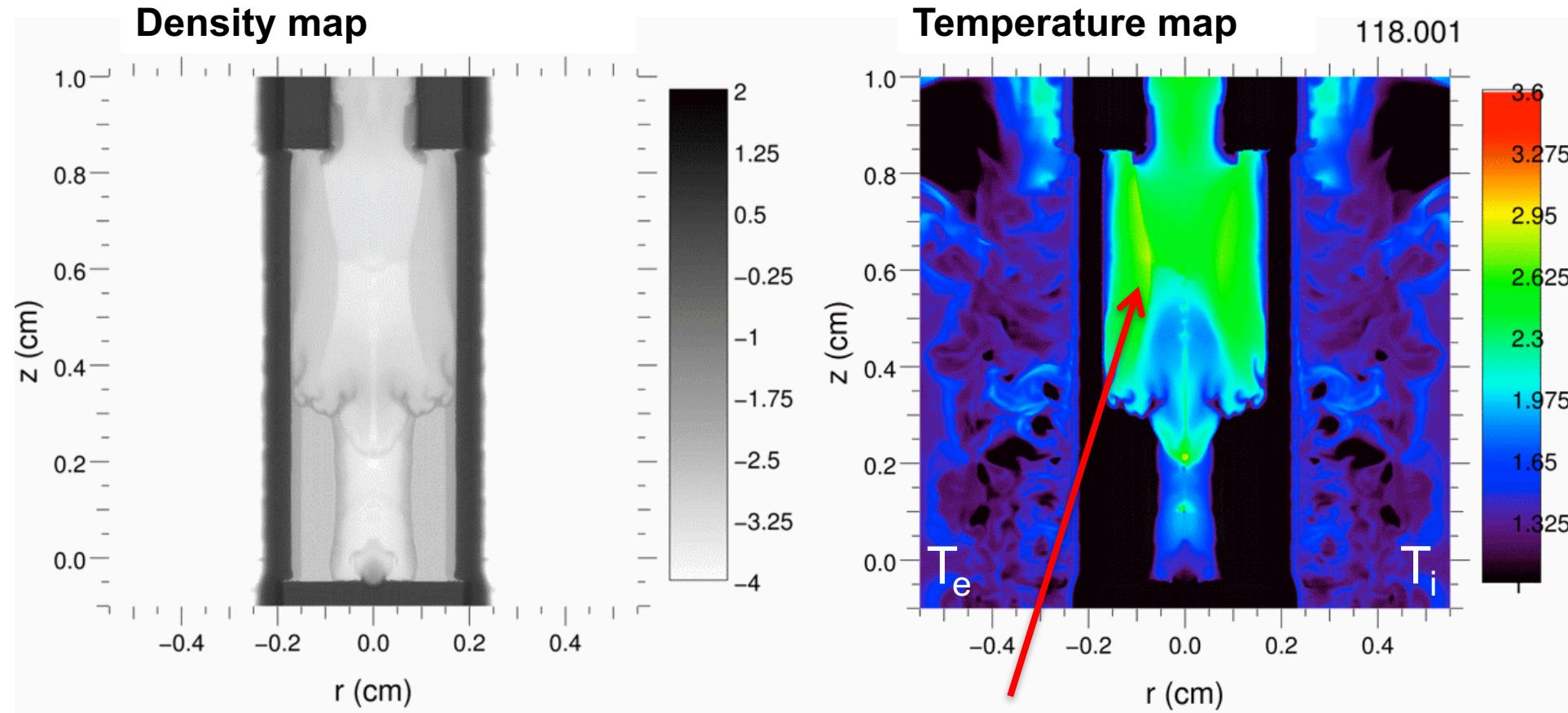
# The fusion fuel is preheated using the Z-Beamlet laser after the liner begins to implode



Beam filamentation can affect the efficacy and depth of laser coupling to the fuel

Example calculations by A.B. Sefkow: DD fuel,  $I=18$  MA,  $B_z=10$  T,  $E_{\text{LASER}}=2.6$  kJ

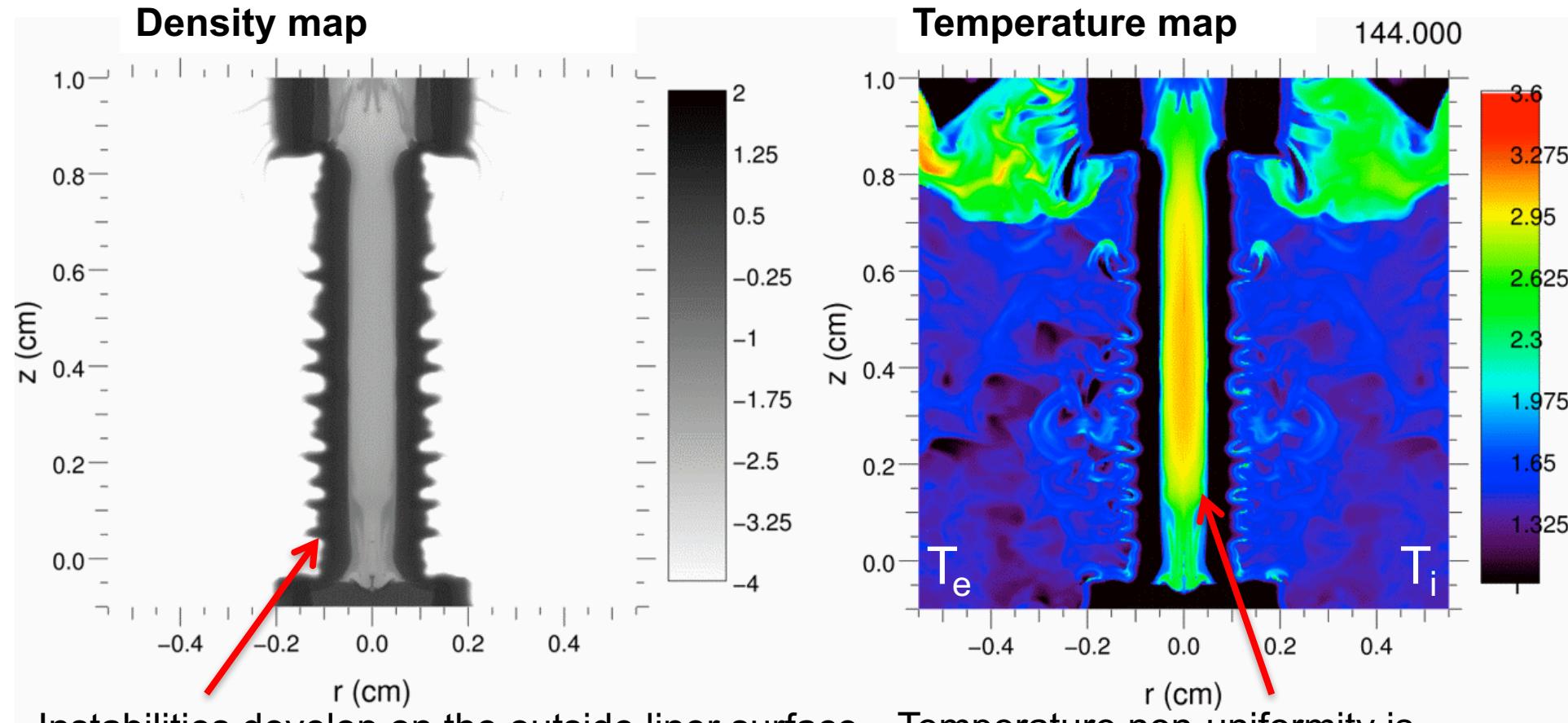
The preheated fuel is then compressed by the imploding liner, reducing the convergence required to reach fusion temperatures



Initially high peak temperatures ( $\sim 1$  keV) relax to  $\sim 300$  eV as the energy diffuses into the fuel

Example calculations by A.B. Sefkow: DD fuel,  $I=18$  MA,  $B_z=10$  T,  $E_{\text{LASER}}=2.6$  kJ

The preheated fuel is then compressed by the imploding liner, reducing the convergence required to reach fusion temperatures

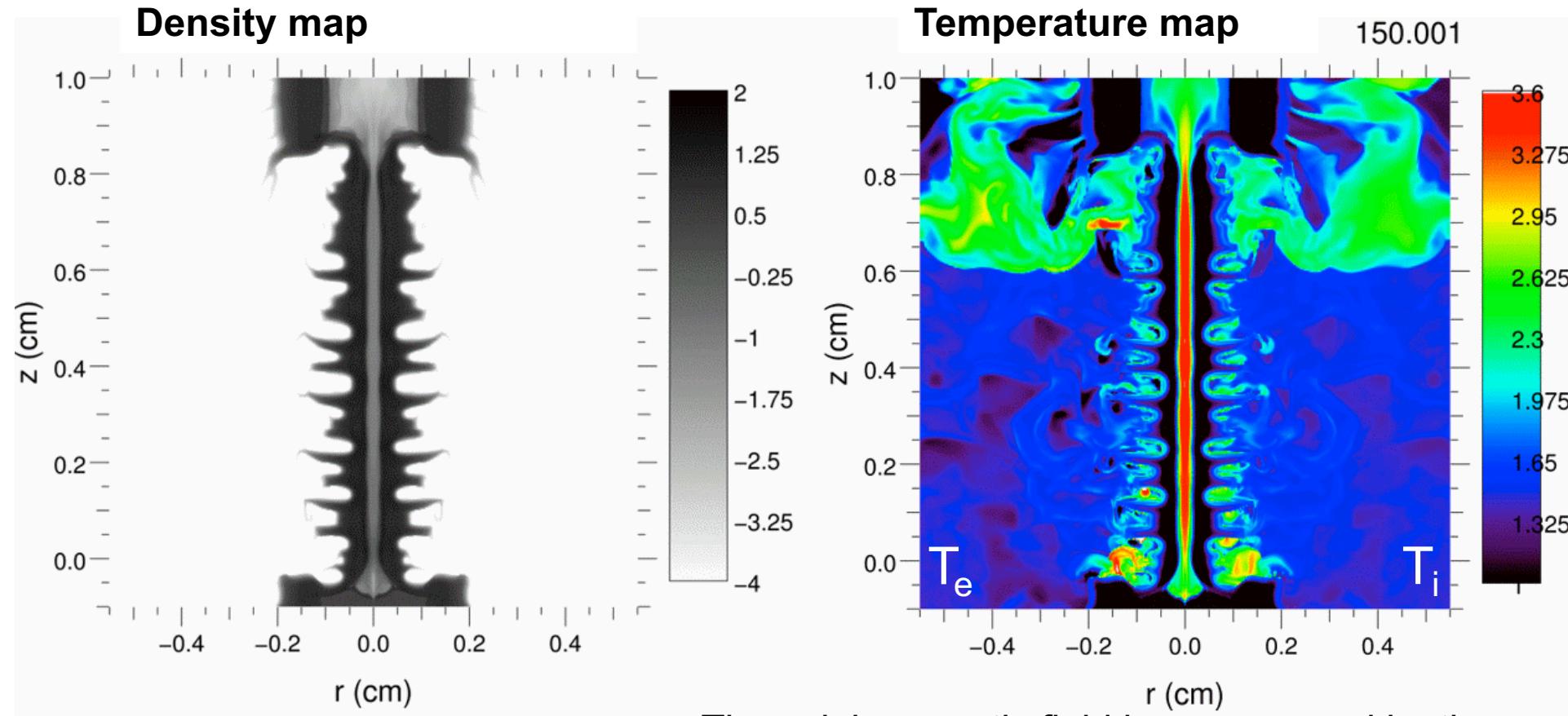


Instabilities develop on the outside liner surface, but impact on fuel mitigated by use of thick liner

Temperature non-uniformity is smoothed out during compression

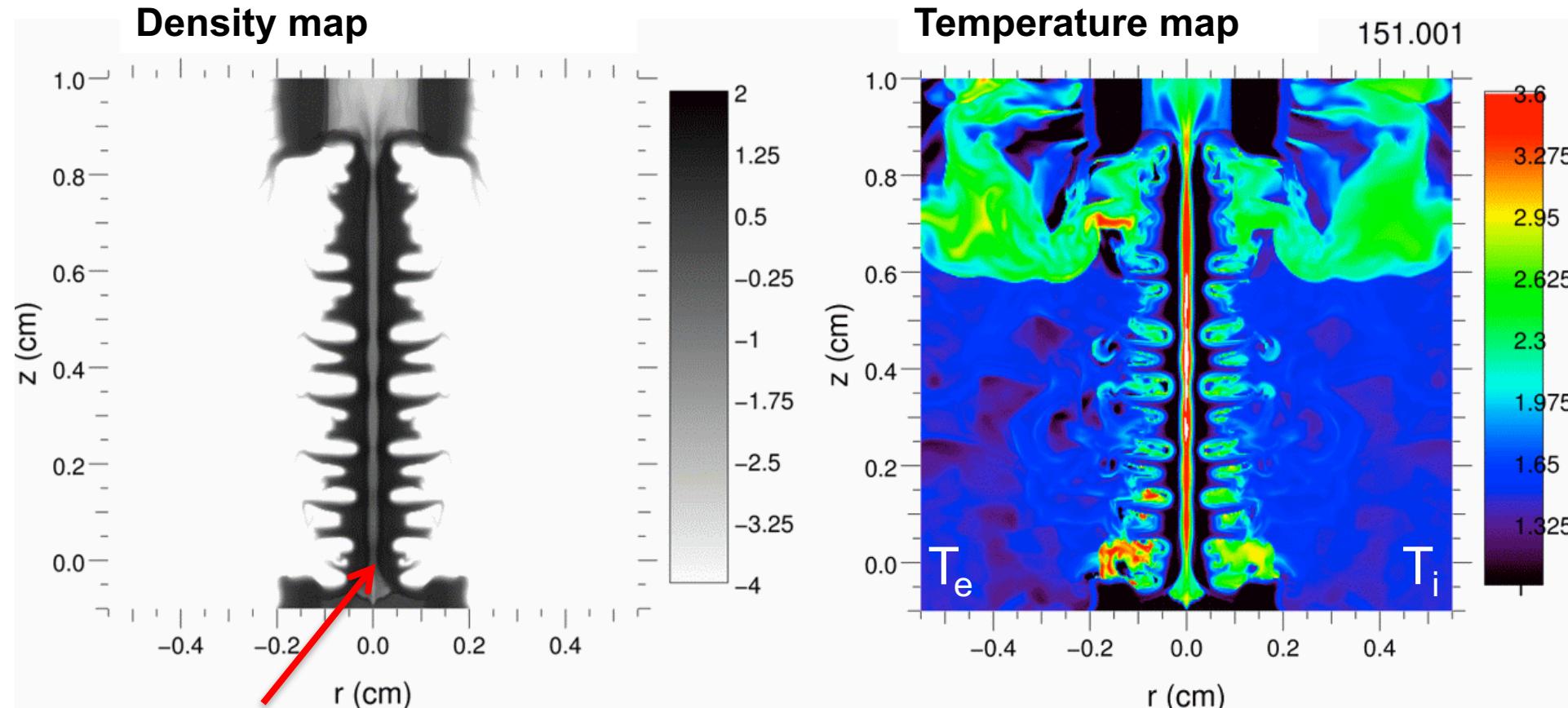
Example calculations by A.B. Sefkow: DD fuel,  $I=18$  MA,  $B_z=10$  T,  $E_{\text{LASER}}=2.6$  kJ

The preheated fuel is then compressed by the imploding liner, reducing the convergence required to reach fusion temperatures



The axial magnetic field is compressed by the liner (some loss due to Nernst) and suppresses heat loss to the relatively cold liner

The preheated fuel is then compressed by the imploding liner, reducing the convergence required to reach fusion temperatures

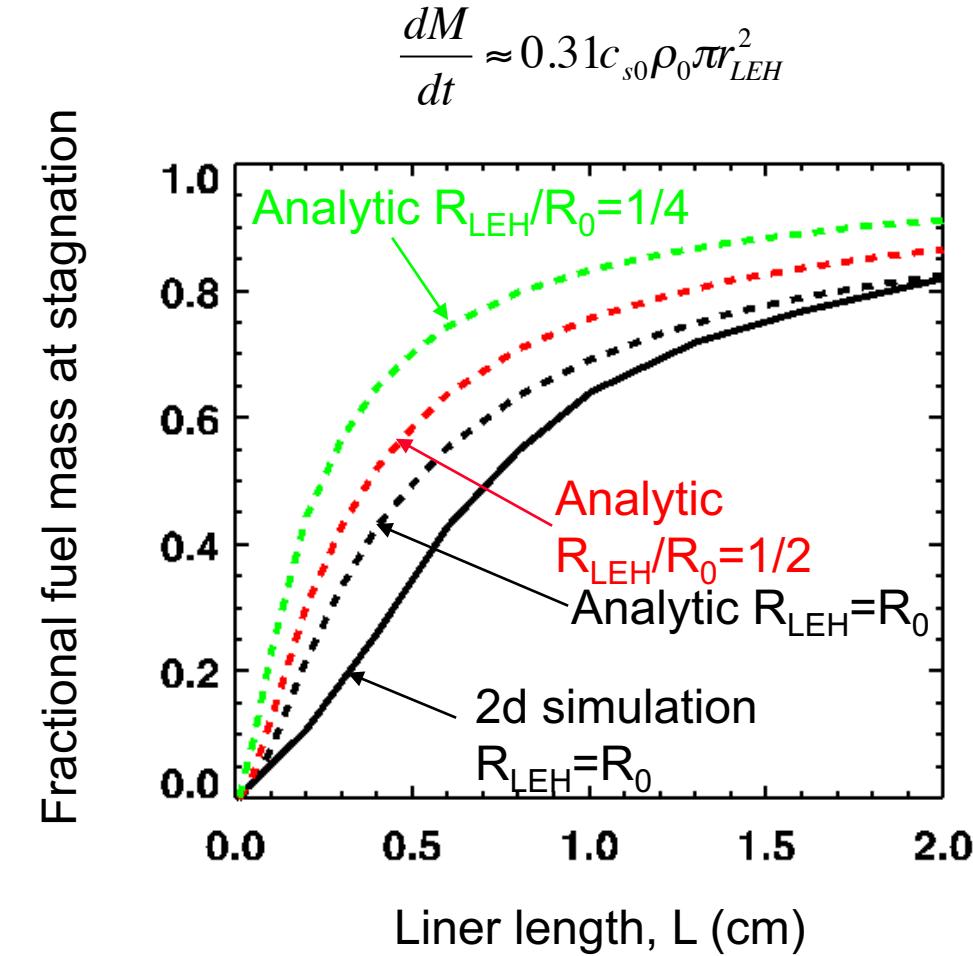
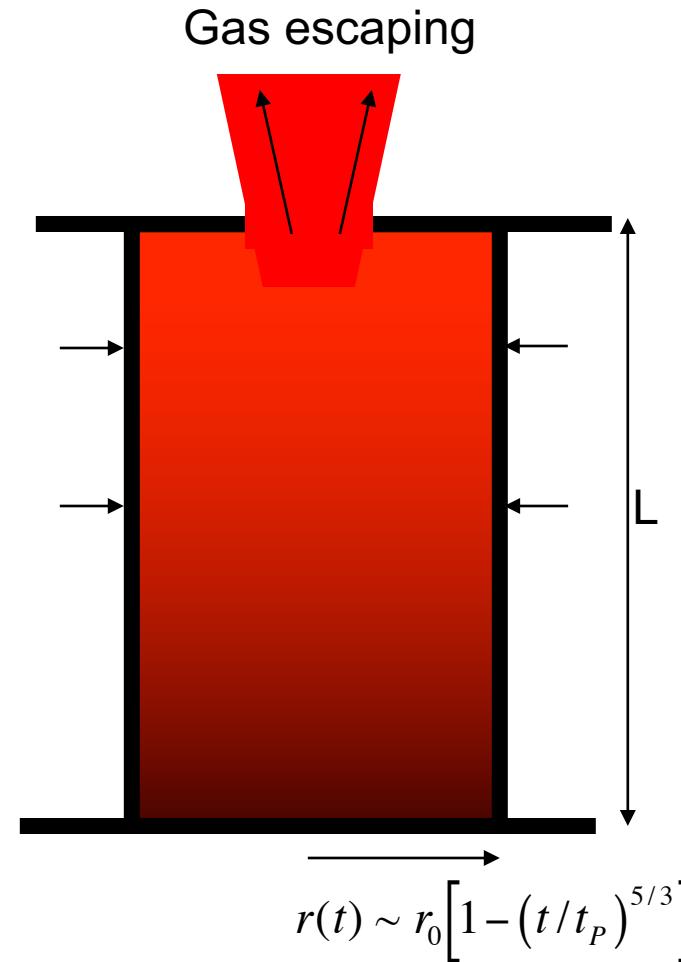


Final temperature  $\sim 8$  keV

Peak Bfield  $>13000$  T, Radial CR $\sim 23$

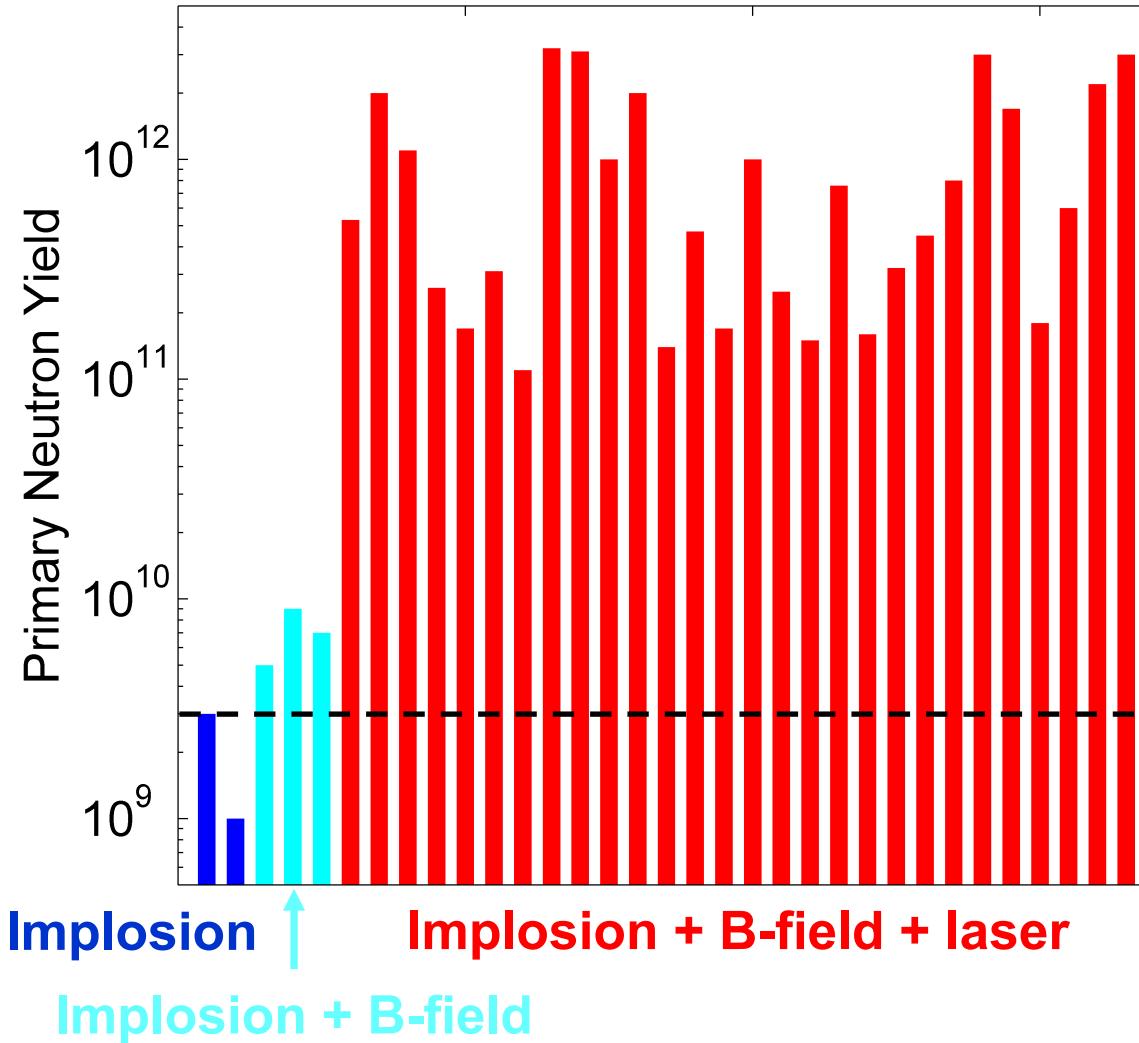
Example calculations by A.B. Sefkow: DD fuel,  $I=18$  MA,  $B_z=10$  T,  $E_{\text{LASER}}=2.6$  kJ

# Analytic estimates and 2D simulations suggest the loss of fuel through the laser entrance hole should be manageable



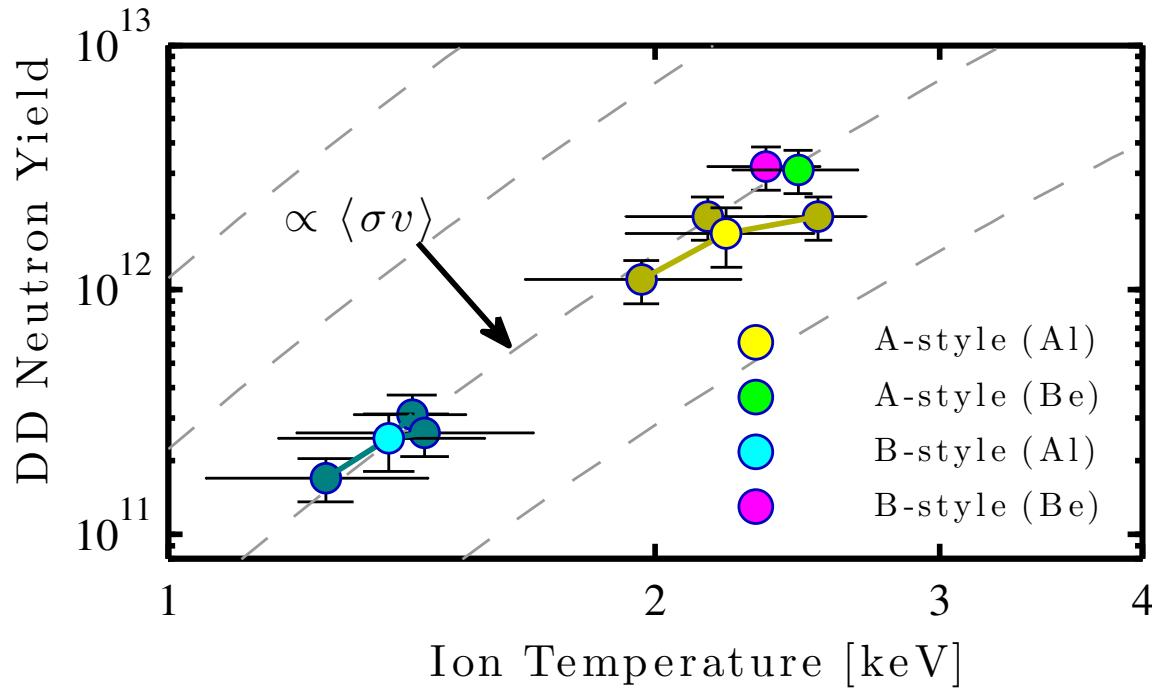
Note: Unlike most MIF approaches which use closed field line geometries, MagLIF has an open geometry

# Primary neutron yields up to $4\text{e}12$ produced only when the B-field and laser heating are included



- Experiments without the magnetic field and laser produce yields at the typical background level
- Adding just the magnetic field had a marginal change in yield
- In experiments where the magnetic field was applied and the laser heated the fuel, the yield increased by about 2 orders of magnitude

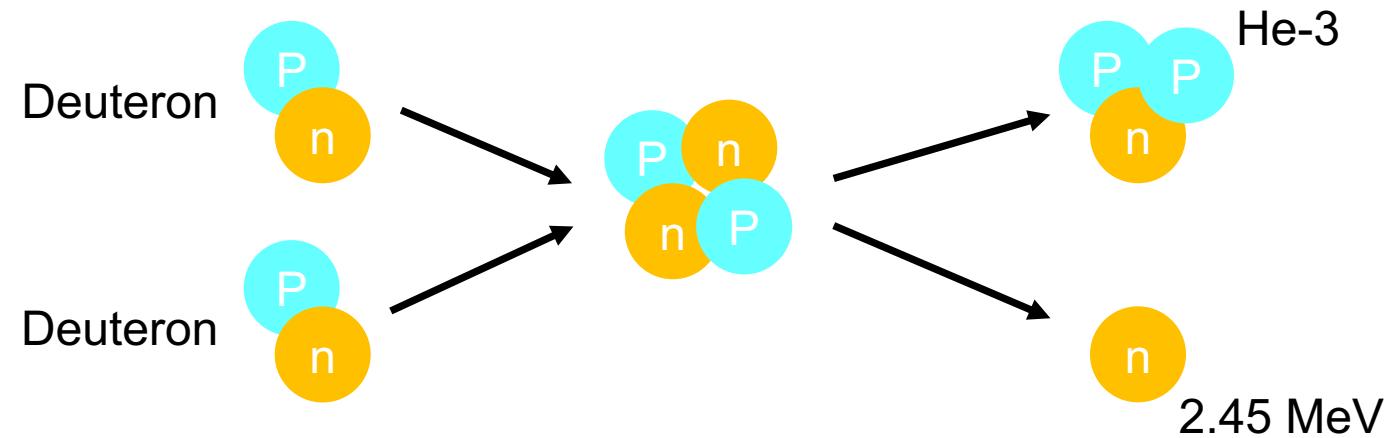
# The primary neutron yield increases as the ion temperature increases



- Yield and ion temperature are related by the fusion reaction rate
- Experimental values roughly follow the trajectory of the fusion reaction rate
- This is expected for a thermonuclear plasma

# The use of D-D fuel in our current MagLIF experiments allows us to measure magnetization

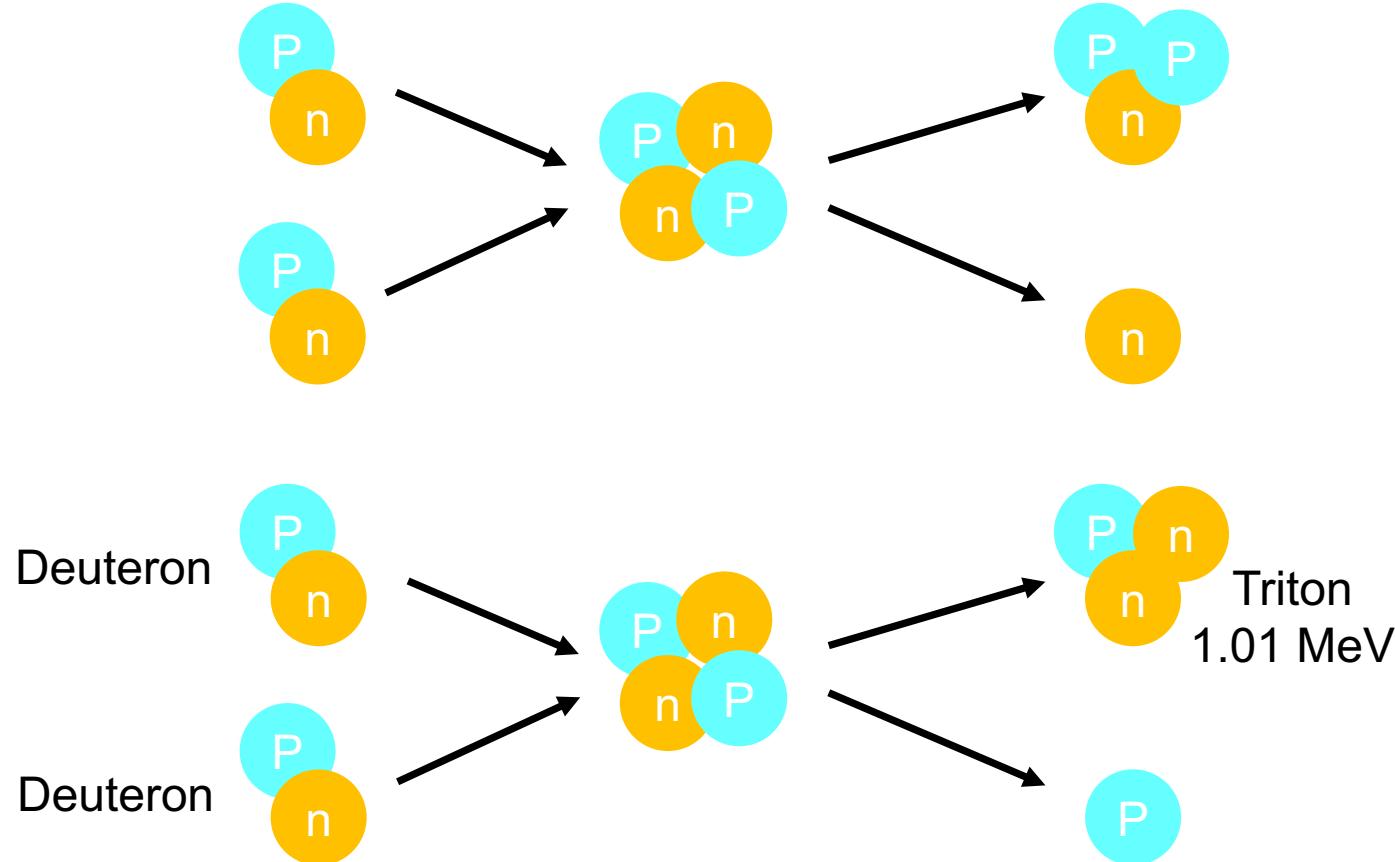
## Primary Reactions



One branch of the D-D reaction produces 2.45 MeV neutrons and an energetic alpha particle...

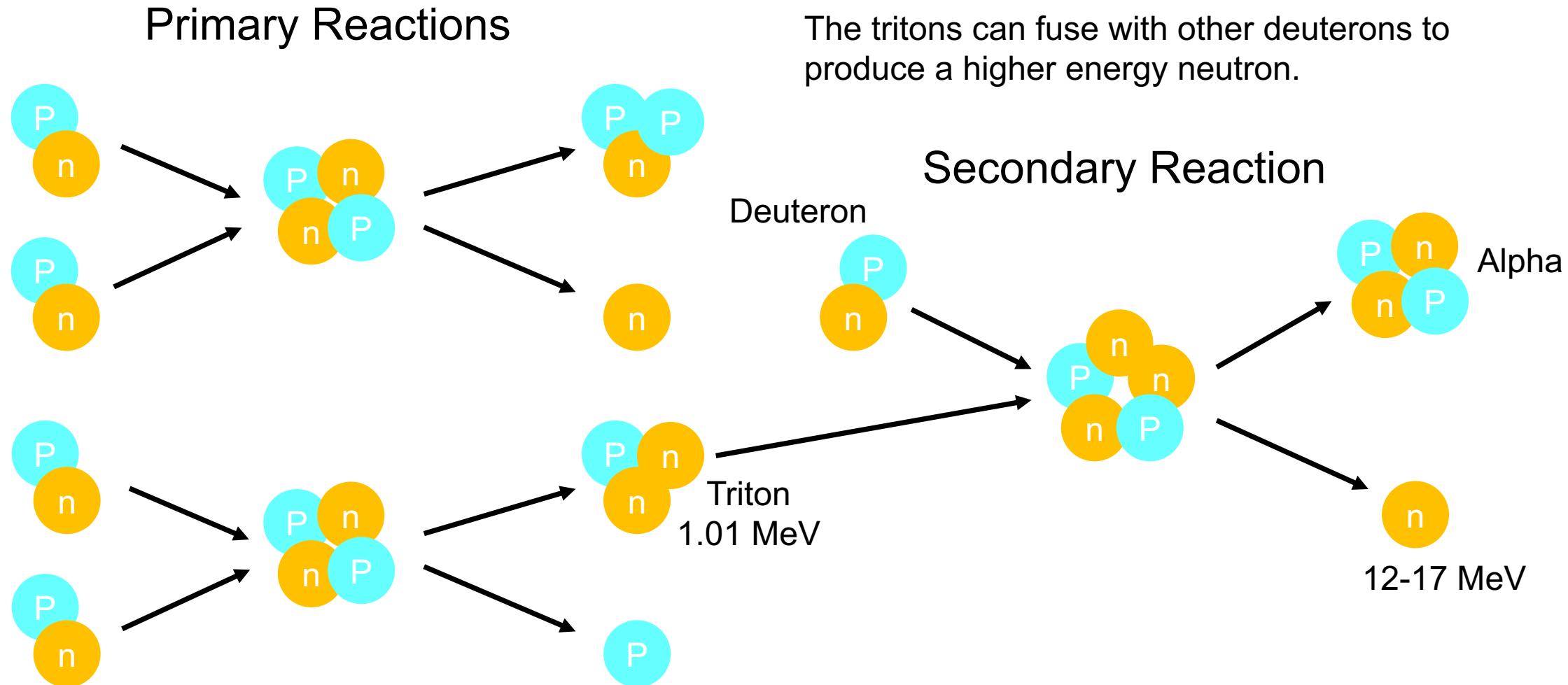
# The use of D-D fuel in our current MagLIF experiments allows us to measure magnetization

## Primary Reactions



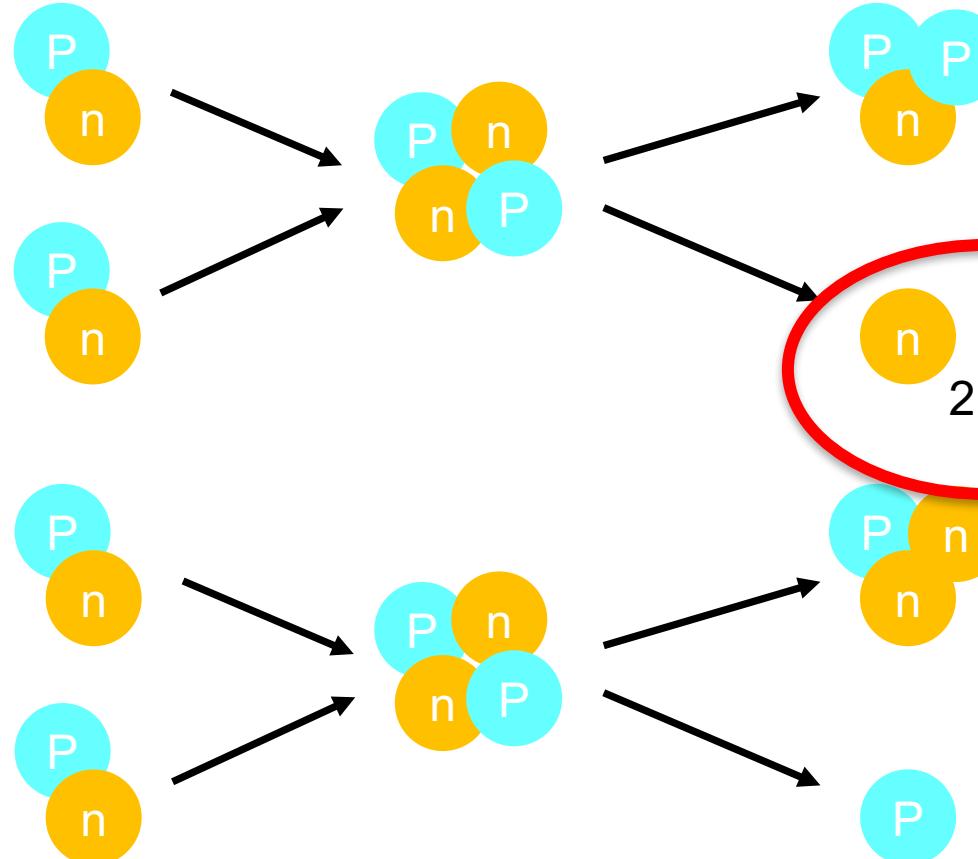
... the other branch produces a 1 MeV triton and energetic proton.

# The use of D-D fuel in our current MagLIF experiments allows us to measure magnetization

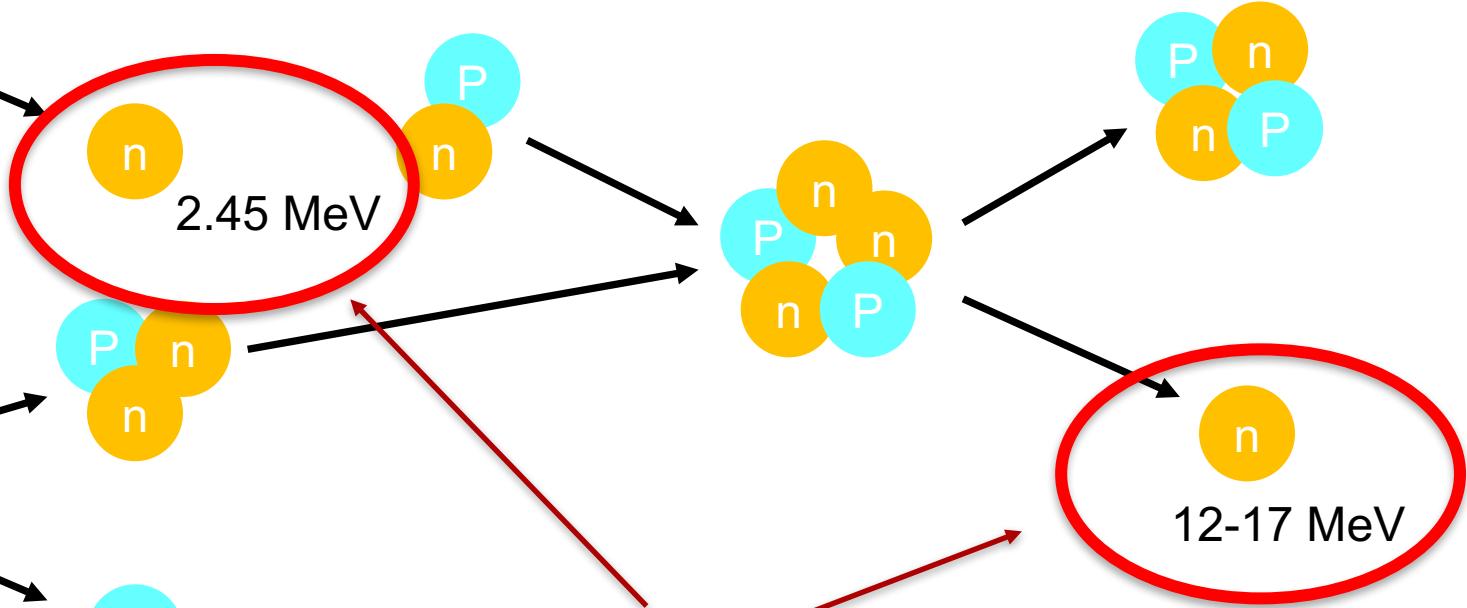


# The use of D-D fuel in our current MagLIF experiments allows us to measure magnetization

## Primary Reactions



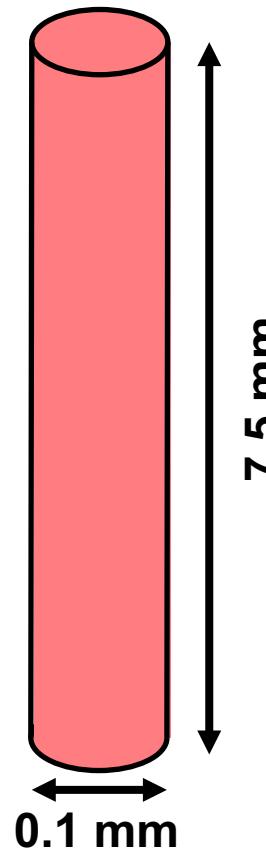
## Secondary Reaction



We measure both of these!

# Secondary neutrons are produced when primary tritons react before exiting the fuel

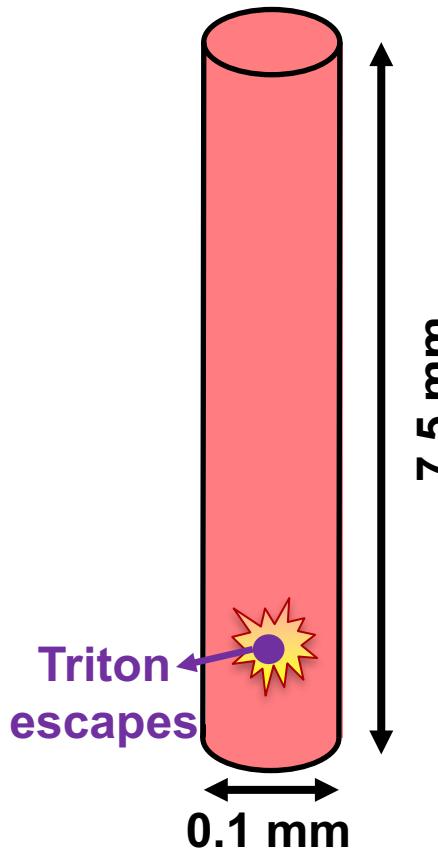
## No B-field



- High aspect ratio stagnation geometry
  - Height  $\gg$  radius

# Secondary neutrons are produced when primary tritons react before exiting the fuel

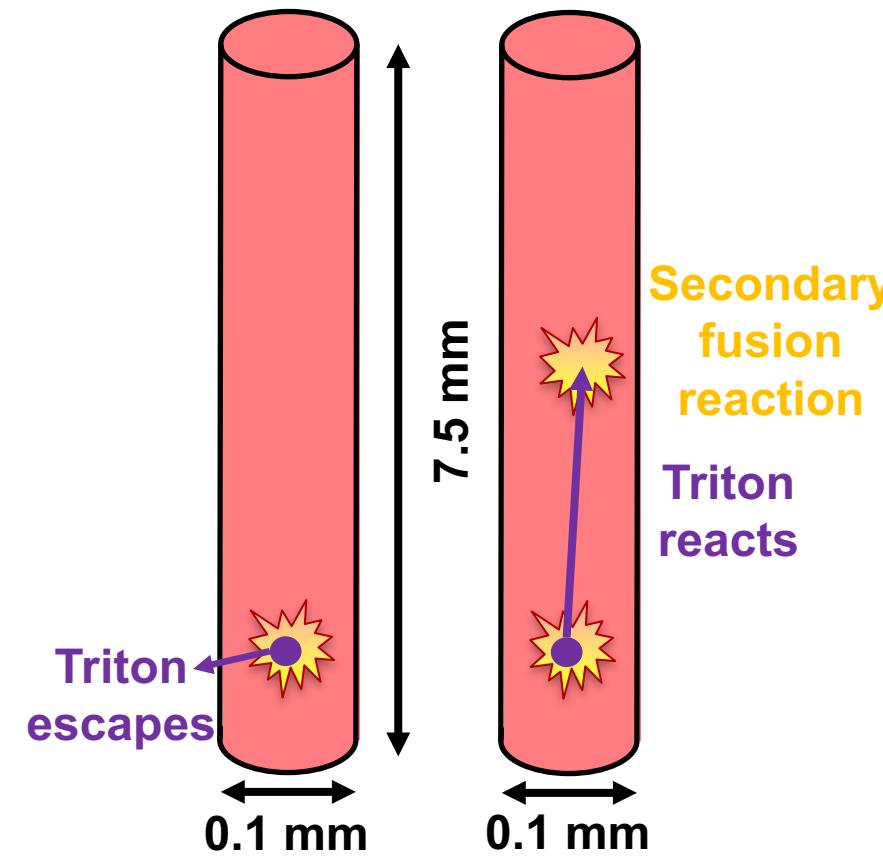
## No B-field



- High aspect ratio stagnation geometry
  - Height  $\gg$  radius
- Consider 2 cases:
  - 1) Triton is created traveling radially
    - Very little probability of interacting prior to escaping

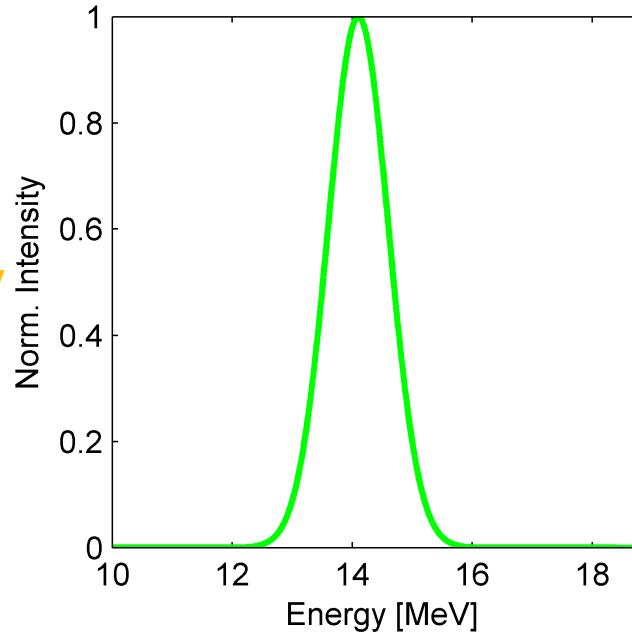
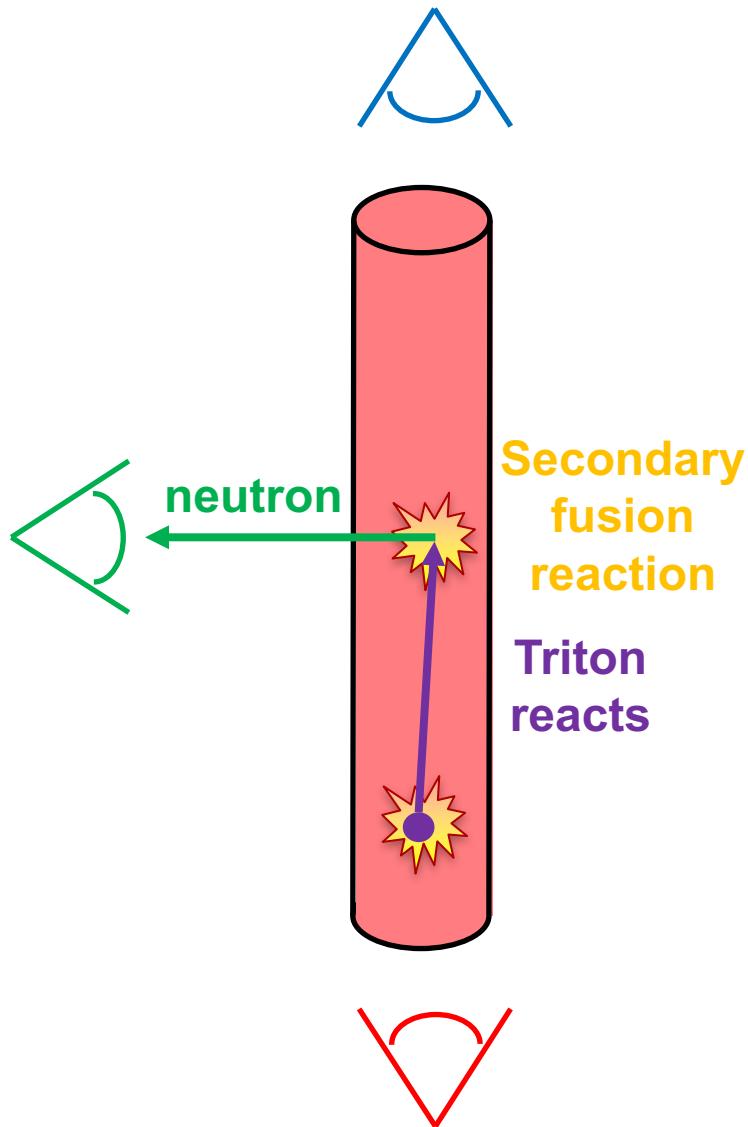
# Secondary neutrons are produced when primary tritons react before exiting the fuel

## No B-field



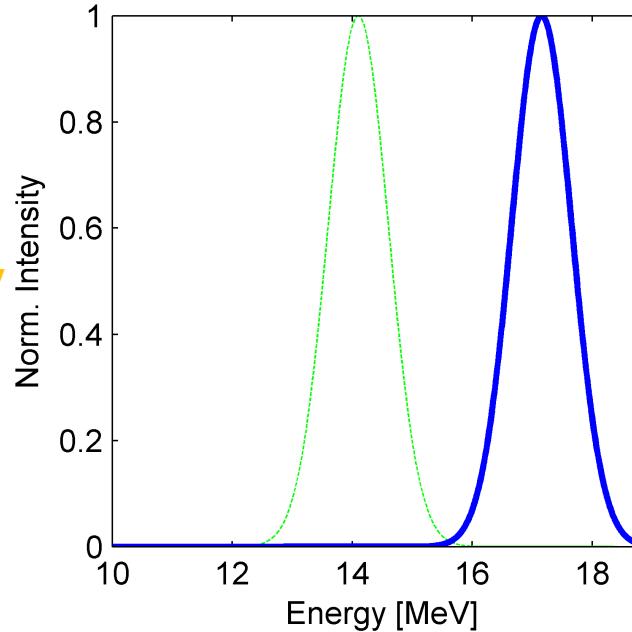
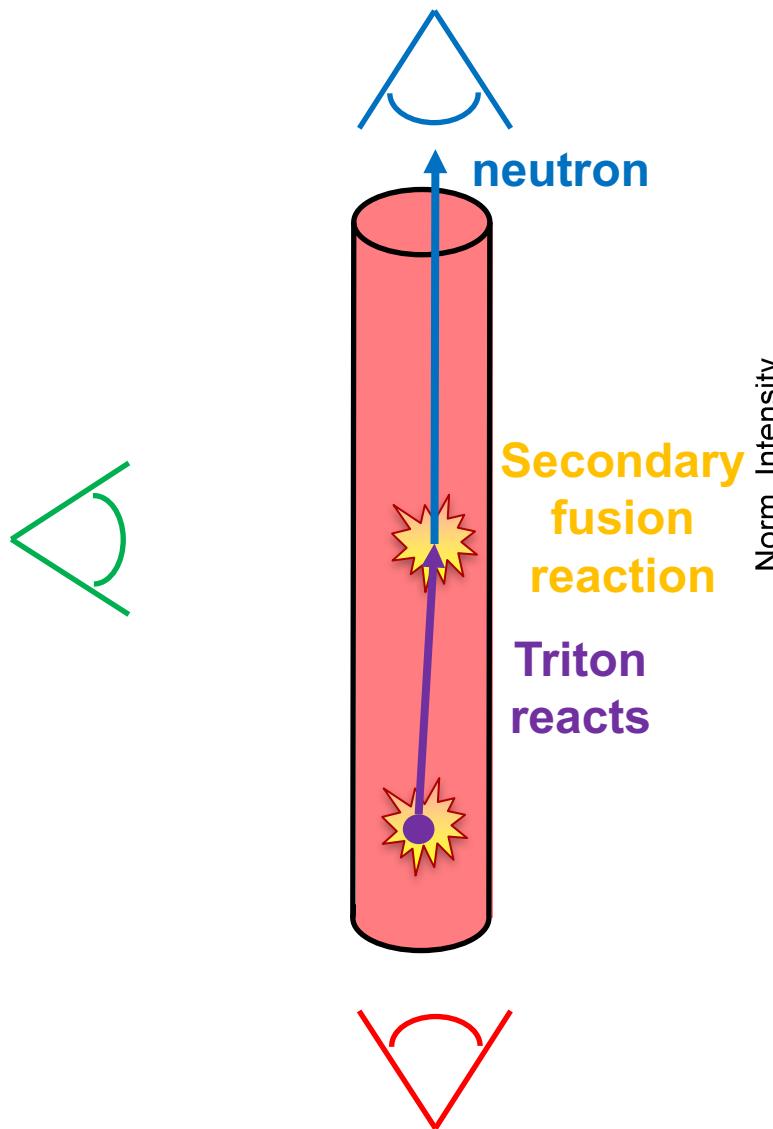
- High aspect ratio stagnation geometry
  - Height  $\gg$  radius
- Consider 2 cases:
  - 1) Triton is created traveling radially
    - Very little probability of interacting prior to escaping
  - 2) Triton is created traveling axially
    - High probability of fusion prior to escaping

# The secondary neutron energy spectra are not expected to be isotropic



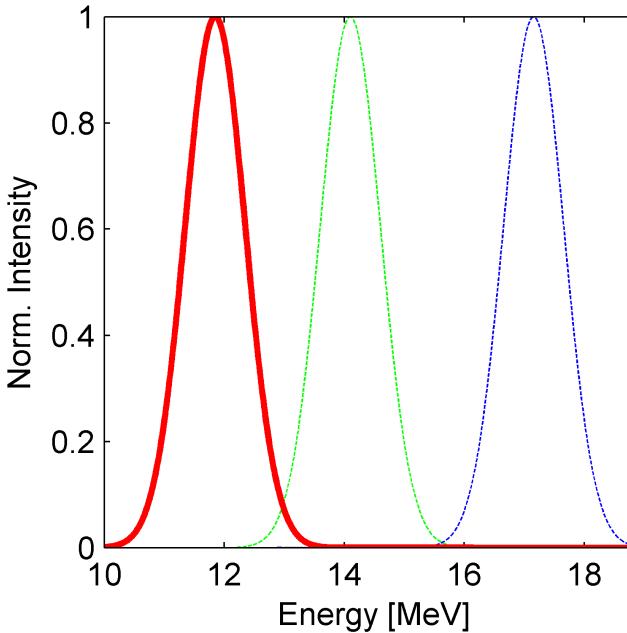
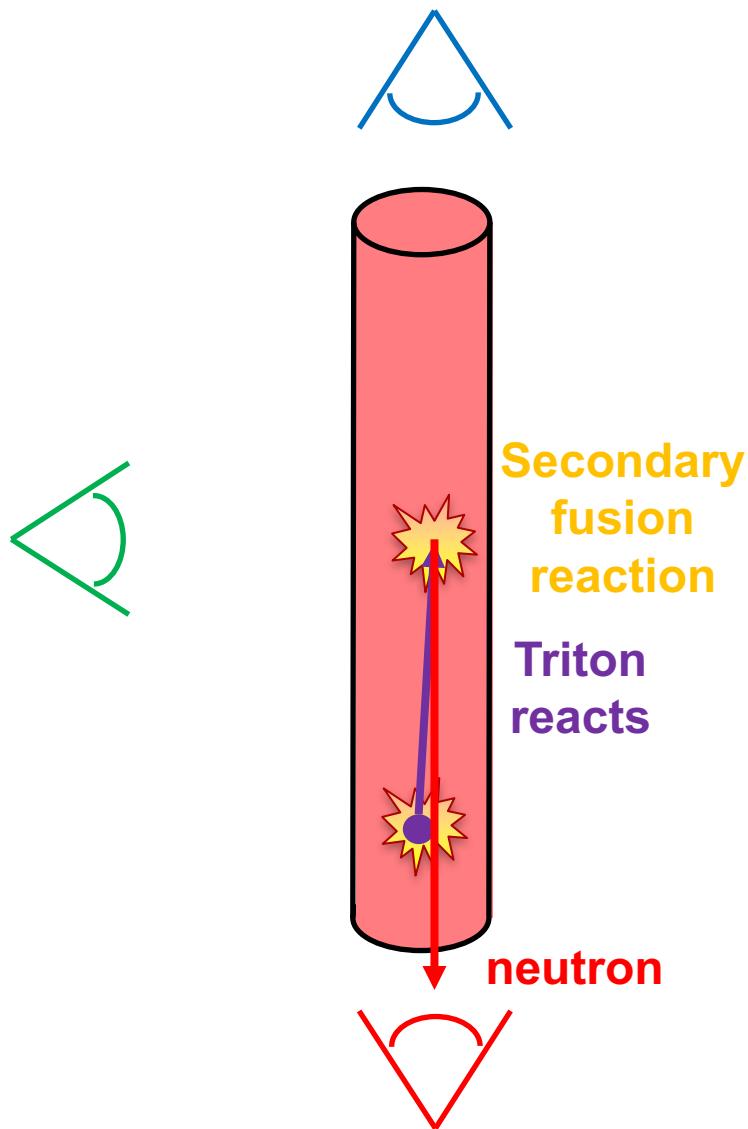
- Consider 3 detector locations:
  - Radial
  - Neutrons at nominal energy

# The secondary neutron energy spectra are not expected to be isotropic



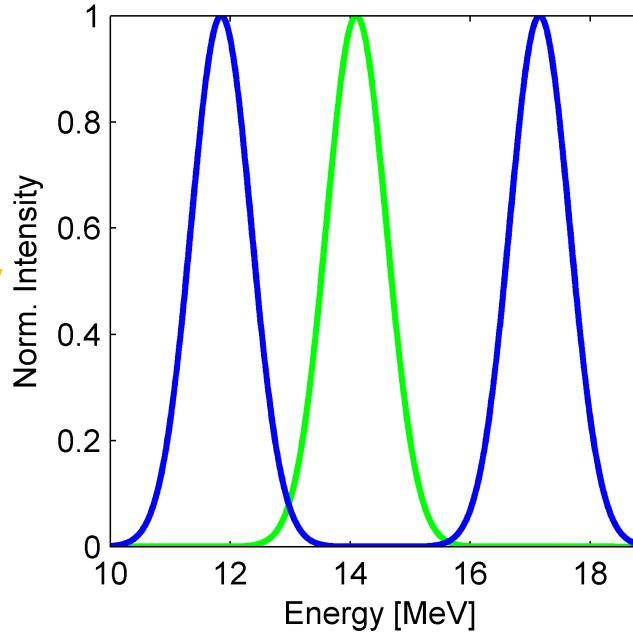
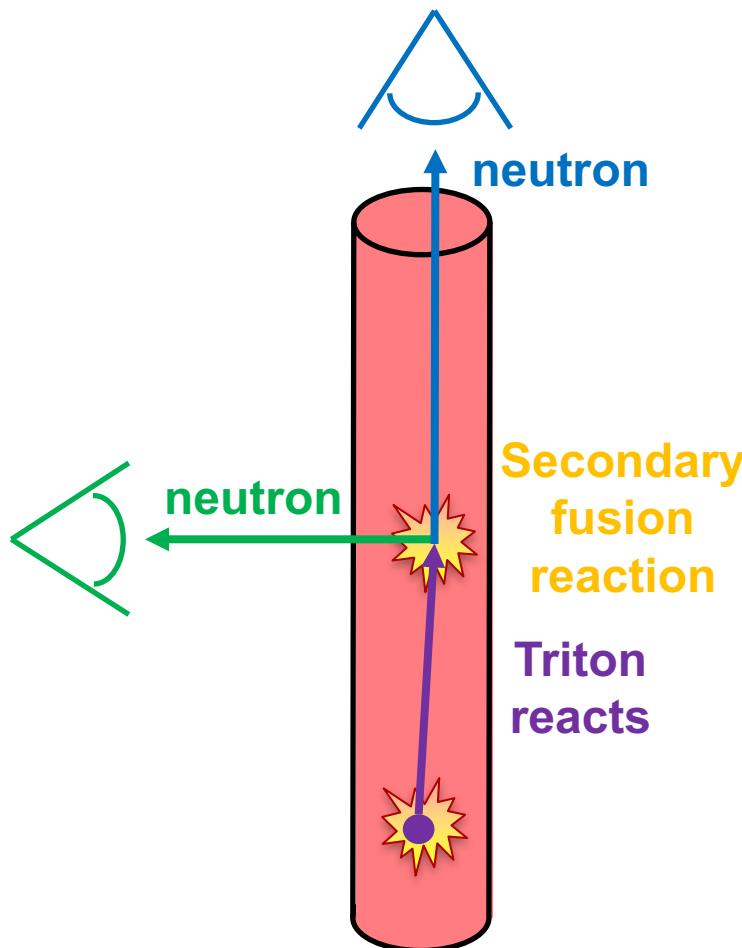
- Consider 3 detector locations:
  - Radial
    - Neutrons at nominal energy
  - Axial (triton moving towards)
    - Neutrons shifted to higher energy

# The secondary neutron energy spectra are not expected to be isotropic



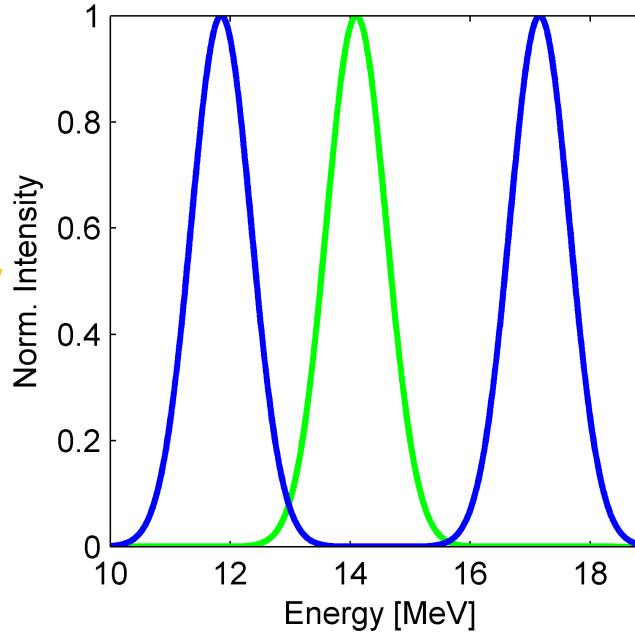
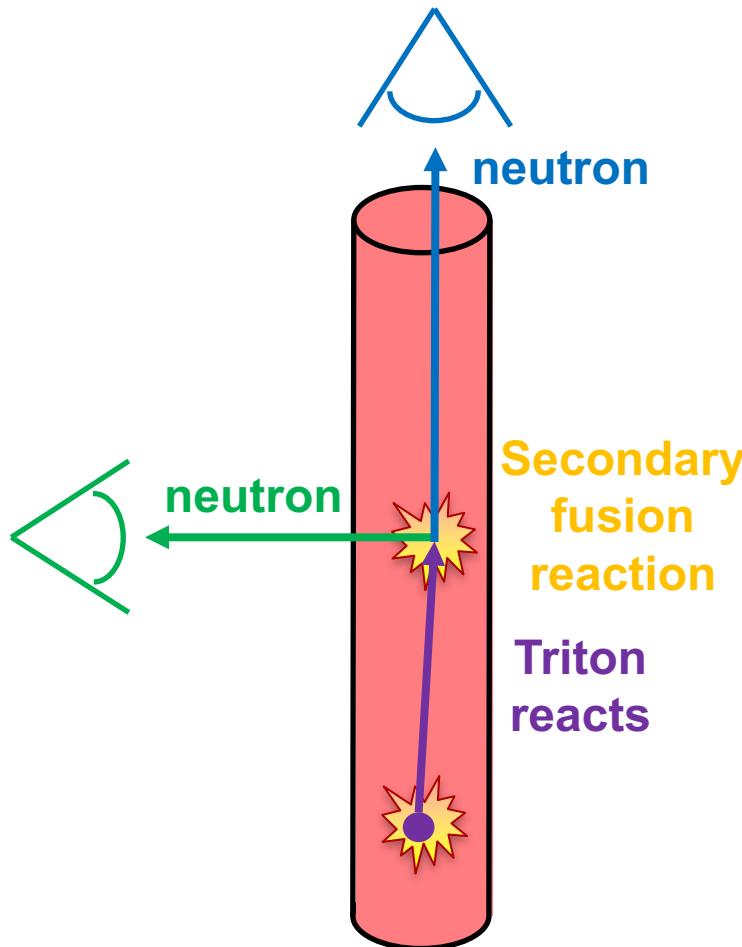
- Consider 3 detector locations:
  - Radial
    - Neutrons at nominal energy
  - Axial (triton moving towards)
    - Neutrons shifted to higher energy
  - Axial (triton moving away)
    - Neutrons shifted to lower energy

# The secondary neutron energy spectra are not expected to be isotropic



- Consider 3 detector locations:
  - Radial
    - Neutrons at nominal energy
  - Axial (triton moving towards)
    - Neutrons shifted to higher energy
  - Axial (triton moving away)
    - Neutrons shifted to lower energy
- Axial detectors will have double peaked structure

# The secondary neutron energy spectra are not expected to be isotropic

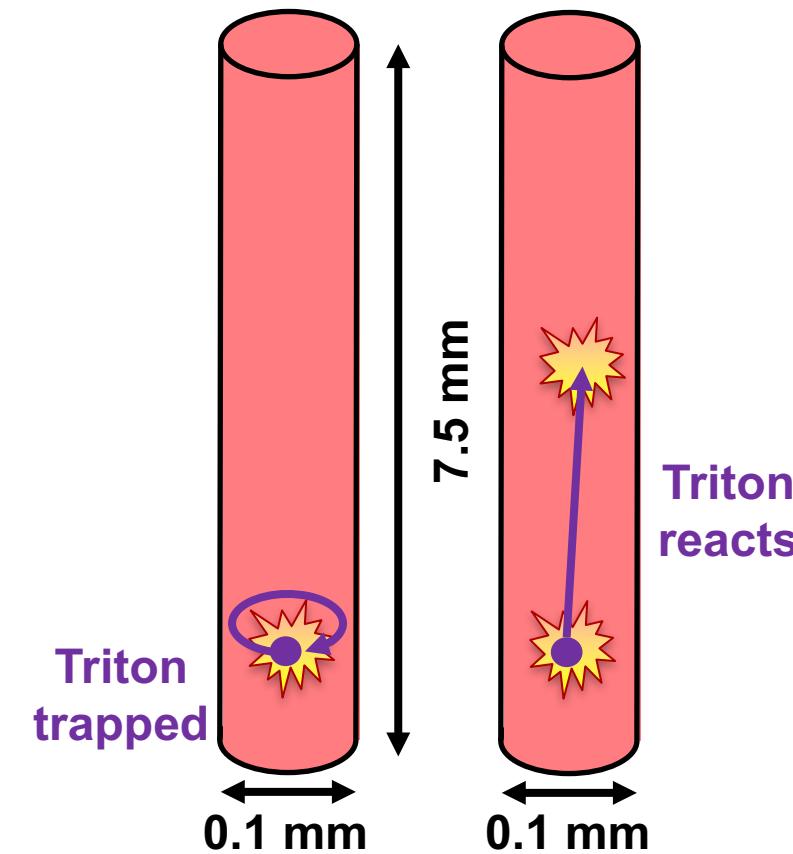


- Consider 3 detector locations:
  - Radial
    - Neutrons at nominal energy
  - Axial (triton moving towards)
    - Neutrons shifted to higher energy
  - Axial (triton moving away)
    - Neutrons shifted to lower energy
- Axial detectors will have double peaked structure

**It is important to note that the vast majority of tritons escape without interacting**

# Adding a strong enough axial magnetic field allows tritons to interact for any initial direction

## High B-field

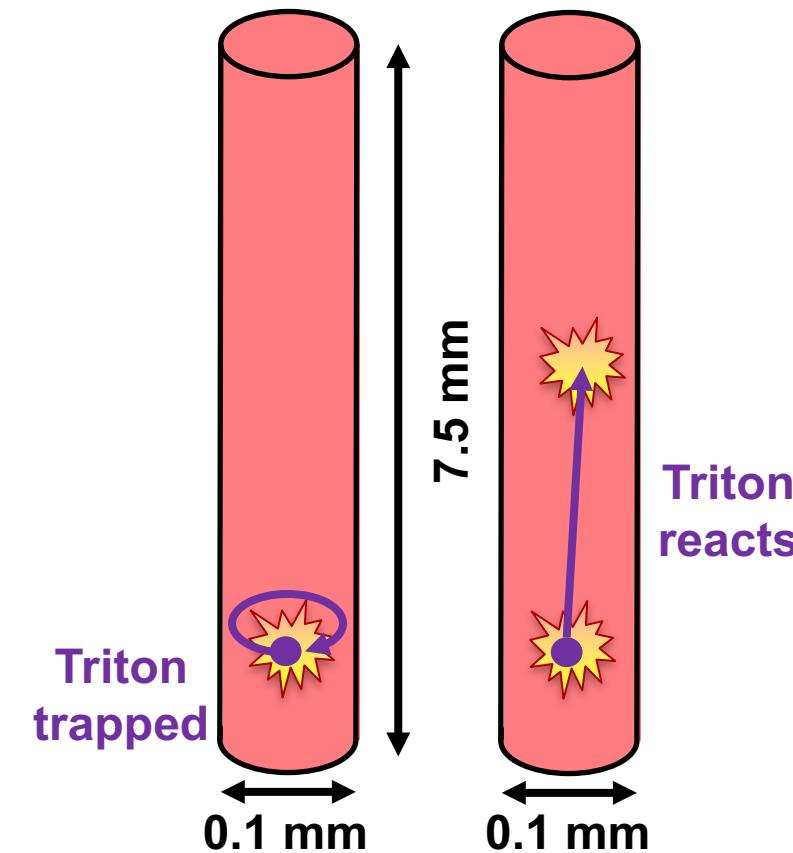


- Consider 2 cases:

- 1) Triton is created traveling axially
  - Axial field has little impact on trajectory
  - Triton has a high probability of fusion
- 2) Triton is created traveling radially
  - Axial magnetic field traps triton within fuel volume
  - Triton has a high probability of fusion

# Adding a strong enough axial magnetic field allows tritons to interact for any initial direction

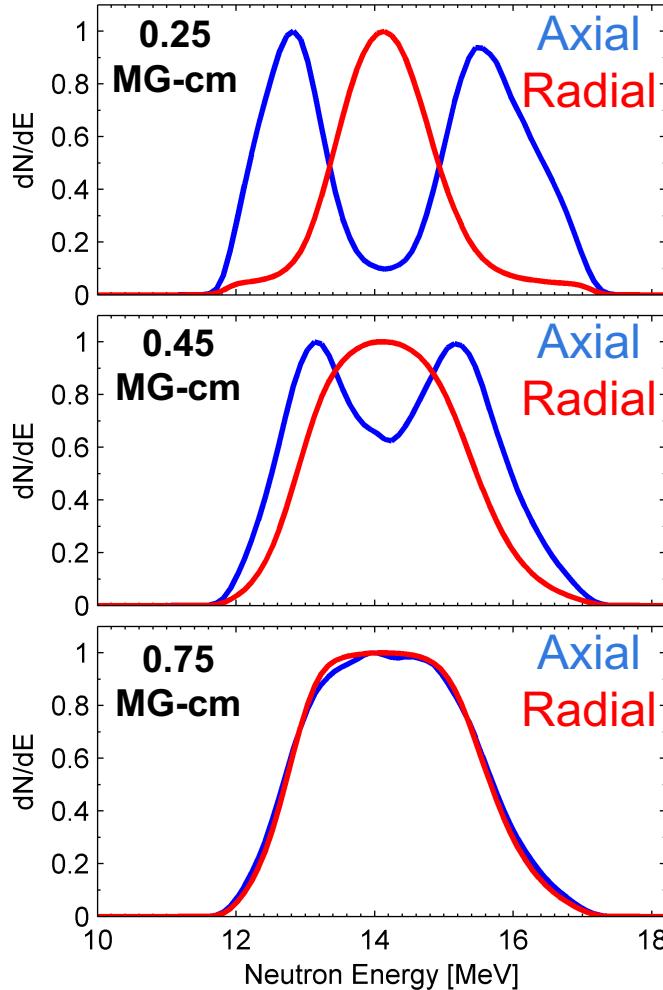
## High B-field



- Consider 2 cases:
  - 1) Triton is created traveling axially
    - Axial field has little impact on trajectory
    - Triton has a high probability of fusion
  - 2) Triton is created traveling radially
    - Axial magnetic field traps triton within fuel volume
    - Triton has a high probability of fusion
- With a high enough magnetic field, all tritons have equal probability of secondary fusion

# Simulations indicate the secondary neutron spectra become isotropic with large B-field

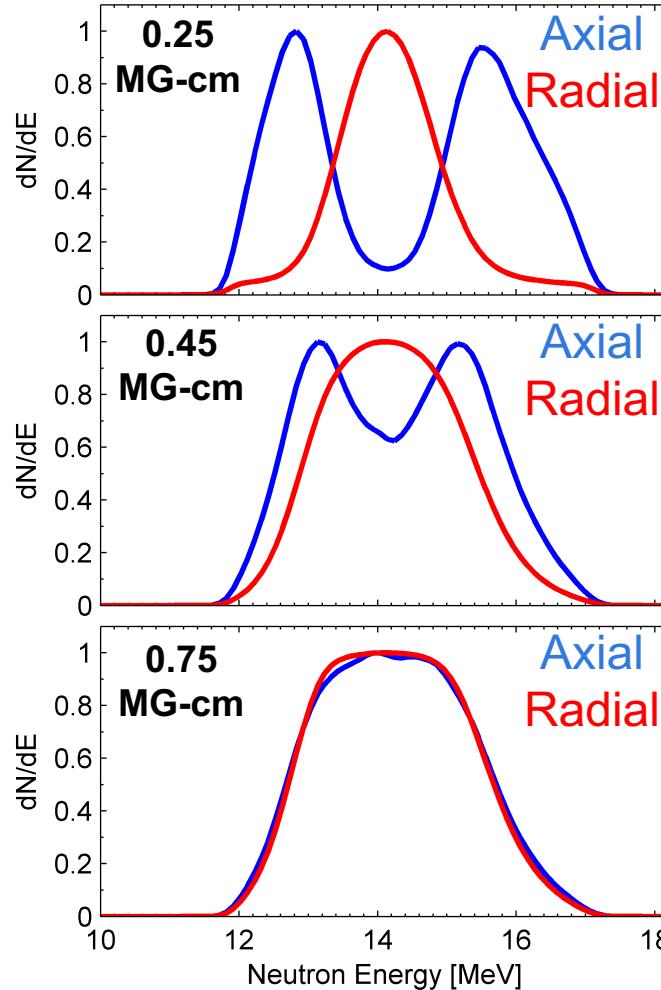
## Simulated Spectra



- As the magnetic field increases, a greater fraction of the radially directed tritons are trapped
- As the distribution of trapped tritons becomes more isotropic, the secondary neutron spectra also become more isotropic

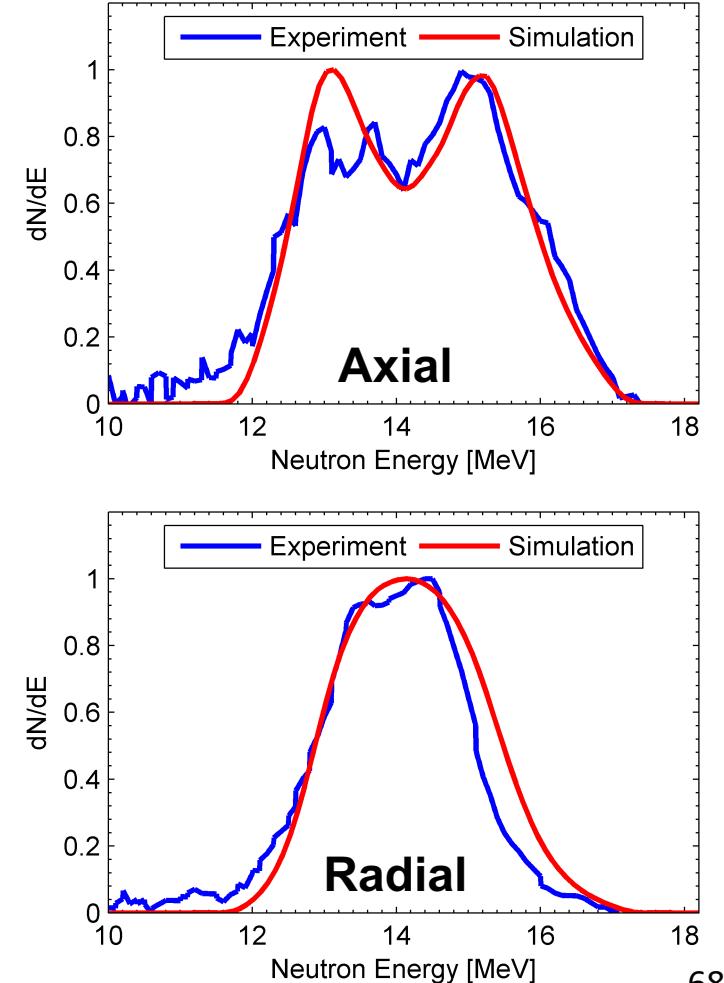
# Simulations indicate the secondary neutron spectra become isotropic with large B-field

## Simulated Spectra

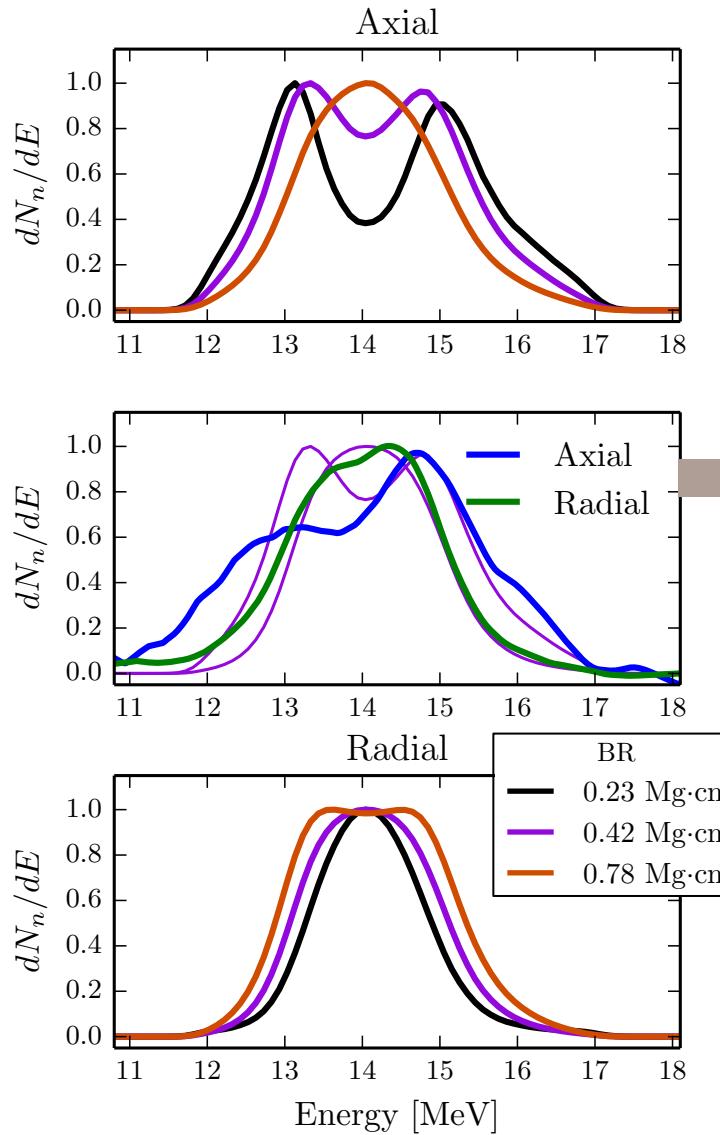


- As the magnetic field increases, a greater fraction of the radially directed tritons are trapped
- As the distribution of trapped tritons becomes more isotropic, the secondary neutron spectra also become more isotropic

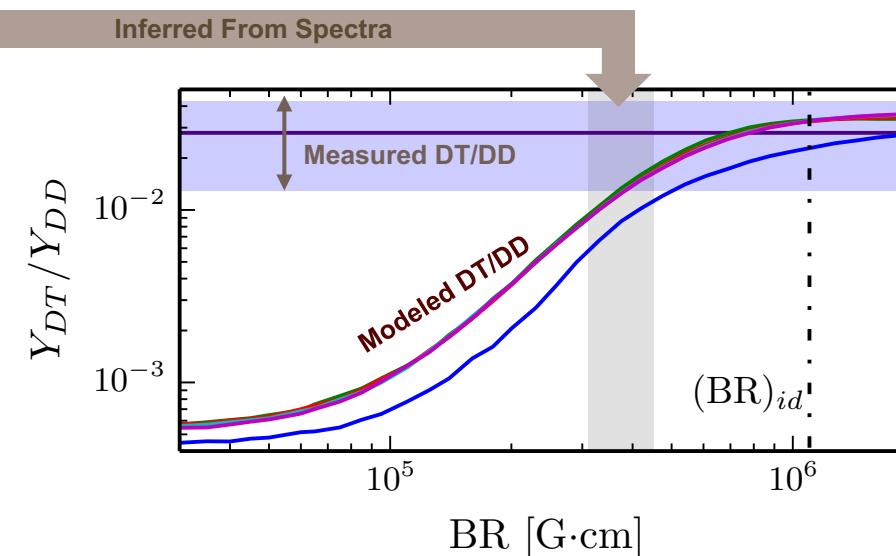
## 0.34 MG-cm



# DT Spectra are used in conjunction with measured DT/DD ratio to constrain the stagnation $BR$



- $T_i \sim T_e = 3.1$  keV
- $\rho = 0.5$  g/cc
- $R = 50\text{--}100 \mu\text{m}$
- $\rho R = 2\text{--}5 \text{ mg/cm}^2$
- $\rho Z \sim 0.3 \text{ g/cm}^2$



$$BR \approx 4(\pm 0.7) \times 10^5 \text{ G} \cdot \text{cm} \sim 17 \times (BR)_o$$

- Not a rigorous fit to the spectra
- Considering only the high energy half of the spectra (scattering)
- In reasonable agreement with integrated 2D simulations<sup>[2]</sup>  
 $(B_z R)_{stag} = 5.3 \times 10^5 \text{ G} \cdot \text{cm}$

$$F_t \approx 55\%$$

Axial nonuniformities and azimuthal field are the biggest missing features that can contribute to the modeled spectra

# Experimentally inferred stagnation $BR$ indicates we are trapping 1 MeV tritons and magnetizing electrons

- Modeling suggests we are depositing >35% of the triton energy
- Scales to >40%  $\alpha$  deposition

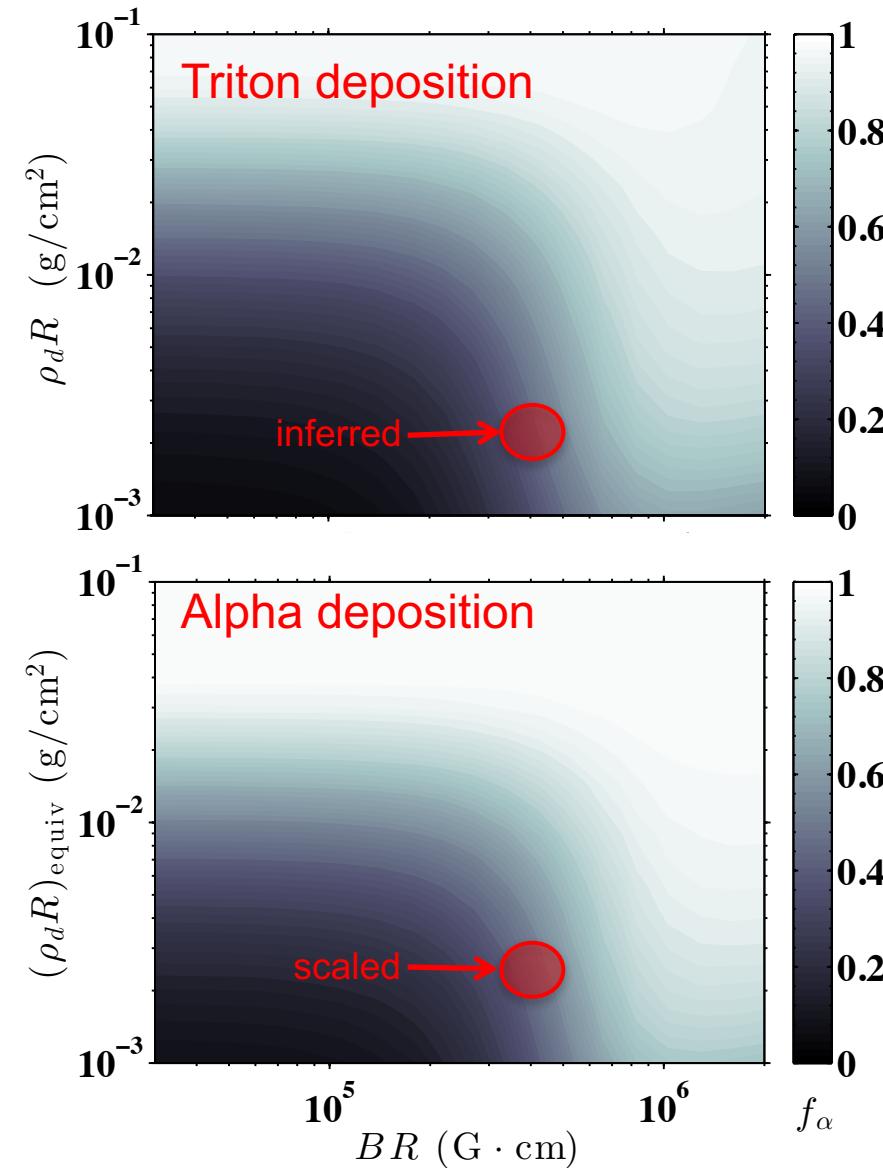
$$BR \sim 4 \times 10^5 G \cdot \text{cm} \rightarrow \frac{R}{r_\alpha} \sim 1.5 - 2$$

$$r_\alpha \approx 1.07 r_t$$

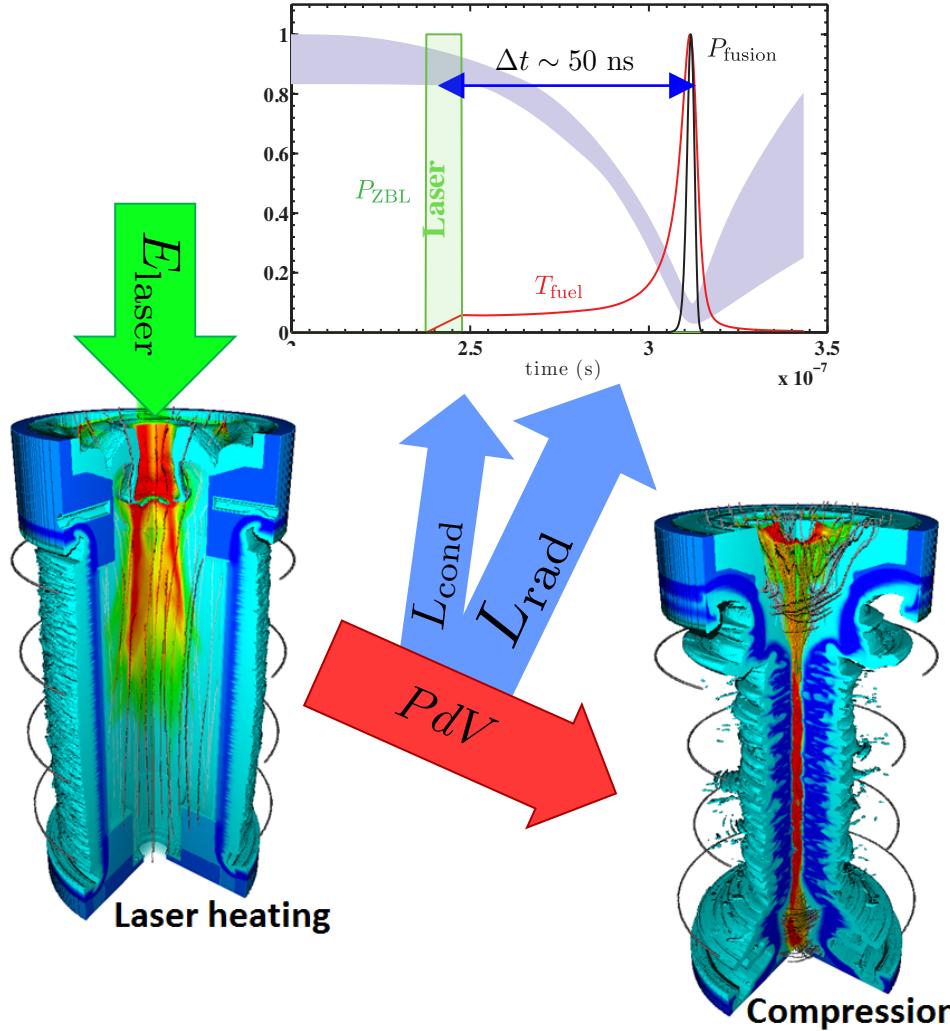
- Magnetizing fast tritons implies electrons are magnetized as well

$$\omega_{ct} \tau_{te} \approx \omega_{ce} \tau_{ee}$$

MagLIF works! We were able to compress flux, preheat the plasma and keep it hot and magnetize the burn products!

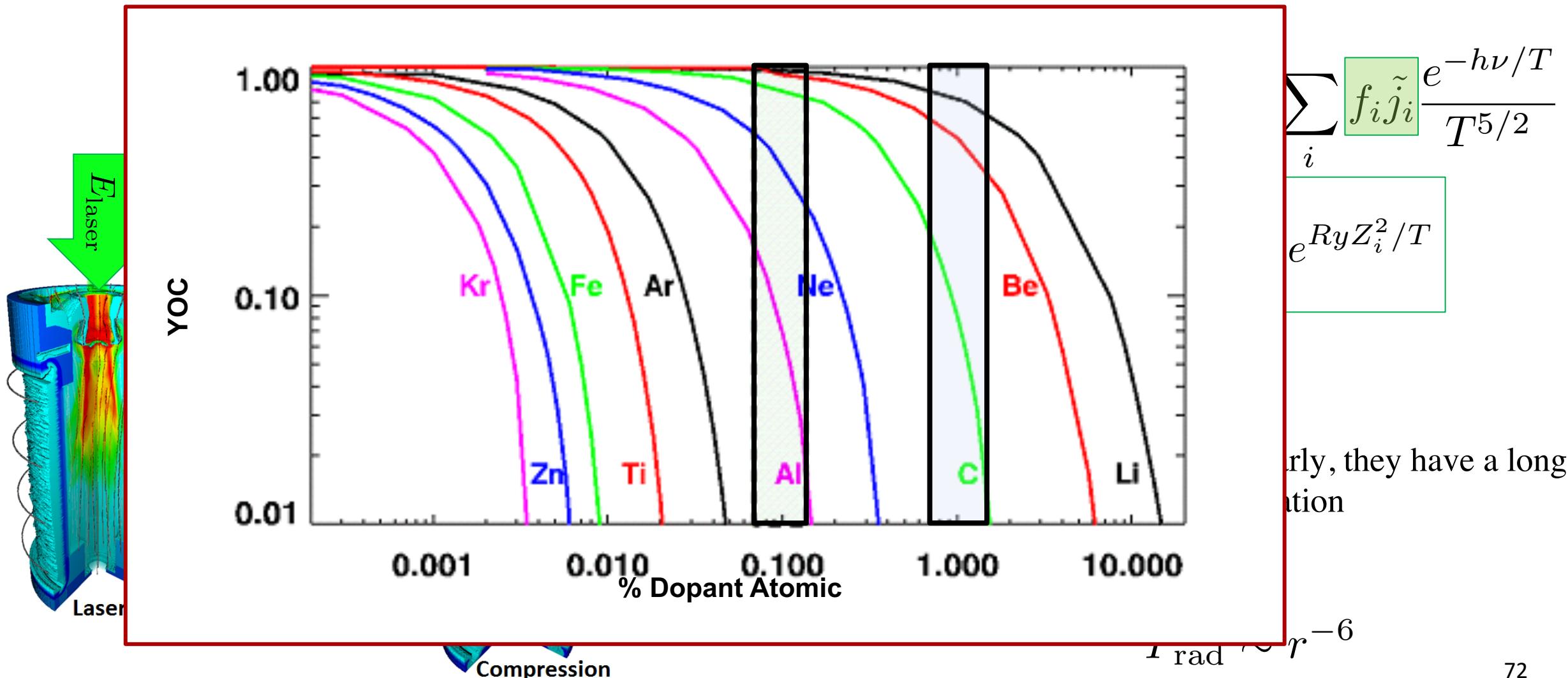


# Mix degrades performance by enhancing losses due to radiation

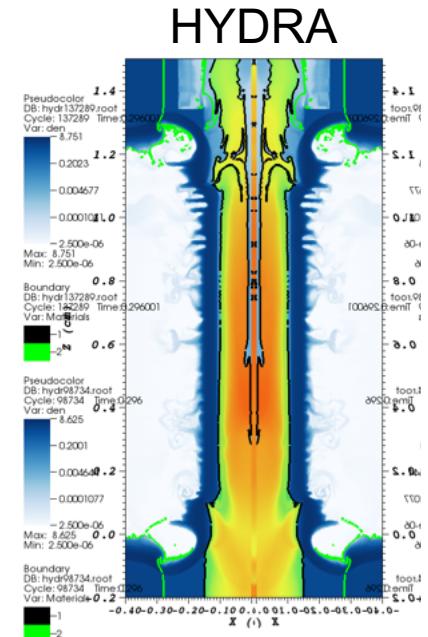
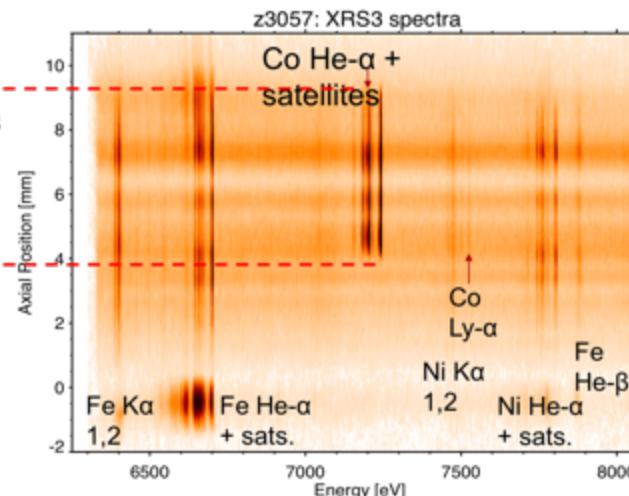
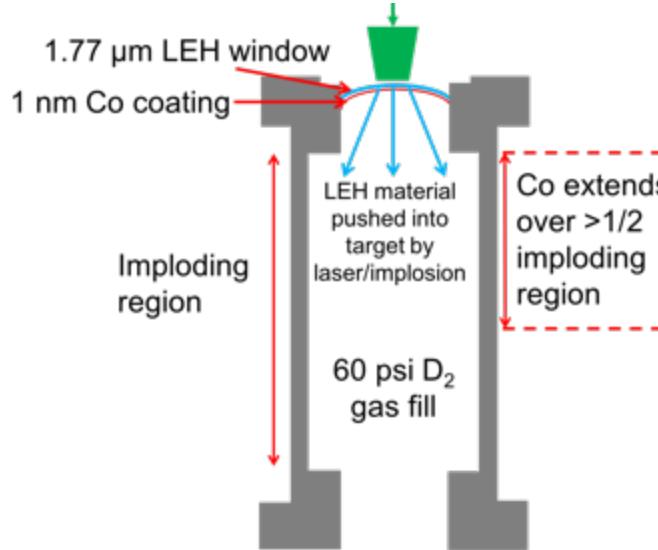


- Approximate bremsstrahlung emission loss:  $P_r \sim Z \rho^2 T^{1/2}$
- Z is the charge of the mix species
- Unlike traditional ICF, if contaminants get into the hot spot early (during laser heating), they have a long time to radiate heat away before stagnation

# Mix degrades performance by enhancing losses due to radiation

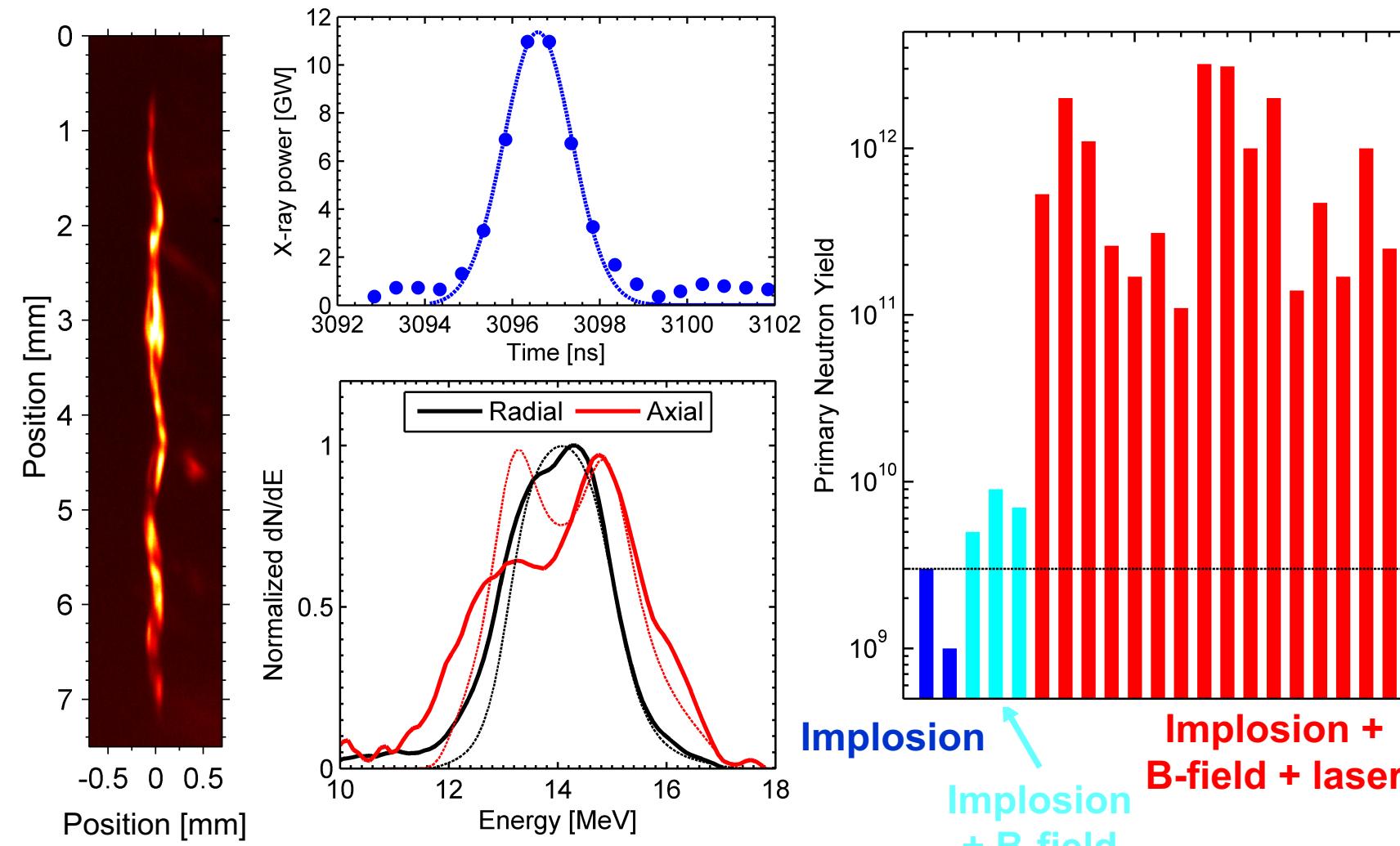


# Over the past year, We have made significant progress in diagnosing and understanding mix in MagLIF implosions on Z using spectroscopy



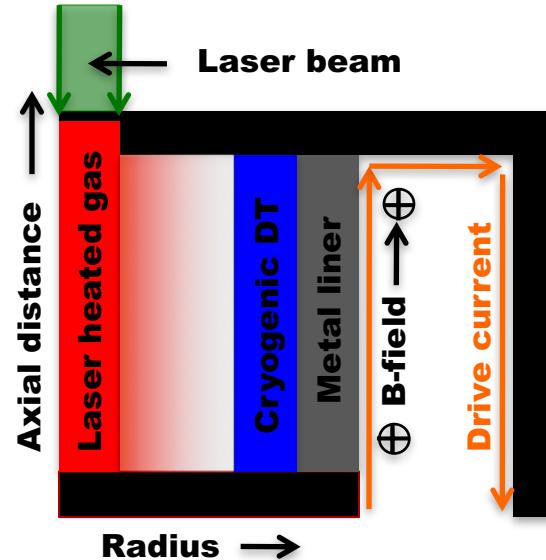
- Both window and upper endcap material has been observed to mix into fuel at stagnation

**We have demonstrated key aspects of magneto-inertial fusion on Sandia's Z facility**

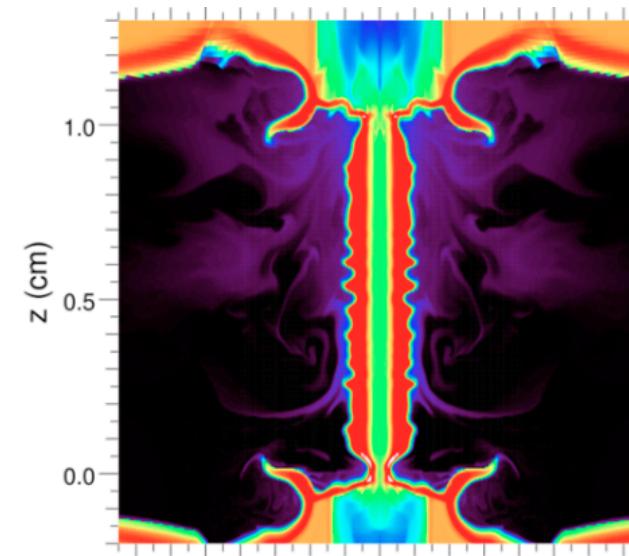
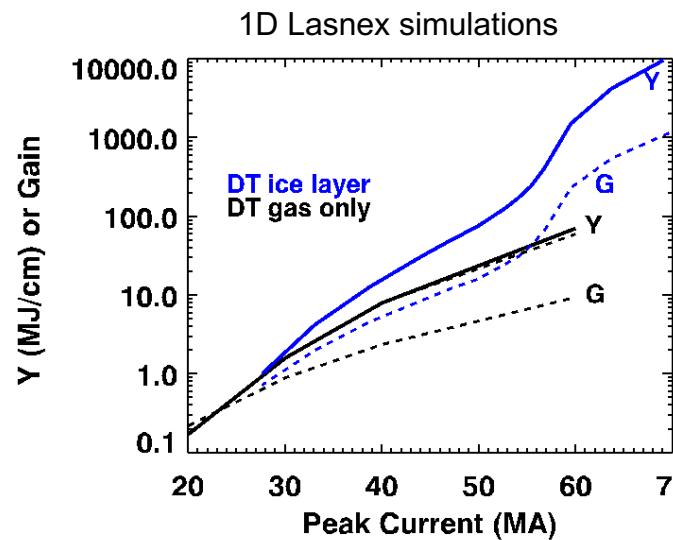


- DT-equivalent yields up to about 1 kJ have been measured
- We are still working on improving our understanding in order to improve performance

# High gain fusion is challenging with MIF targets



- MTF targets are generally designed for volumetric burn with gains  $\sim 1-10$
- Difficult to ignite DT ice layer
  - Magnetization inhibits deposition of alpha particles in ice
  - Low hot spot density and long confinement times limit fusion power
- 2D Simulations have shown that MagLIF could in principle provide high yield and gain<sup>1</sup> on future accelerators
  - Magnetization must not be too high



A 2D integrated Hydra simulation<sup>2</sup> produced  $\sim 6$  GJ  
 $AR_{\text{liner}} = 6$   
 $\rho_{\text{gas}} = 5 \text{ mg cm}^{-3}$   
 $B_z^0 = 8 \text{ T}$   
 $E_{\text{laser}} = 25 \text{ kJ}$   
 Peak drive current = 70 MA

# MagLIF shows promise as a route to high fusion yields in the laboratory, but we have a long road ahead

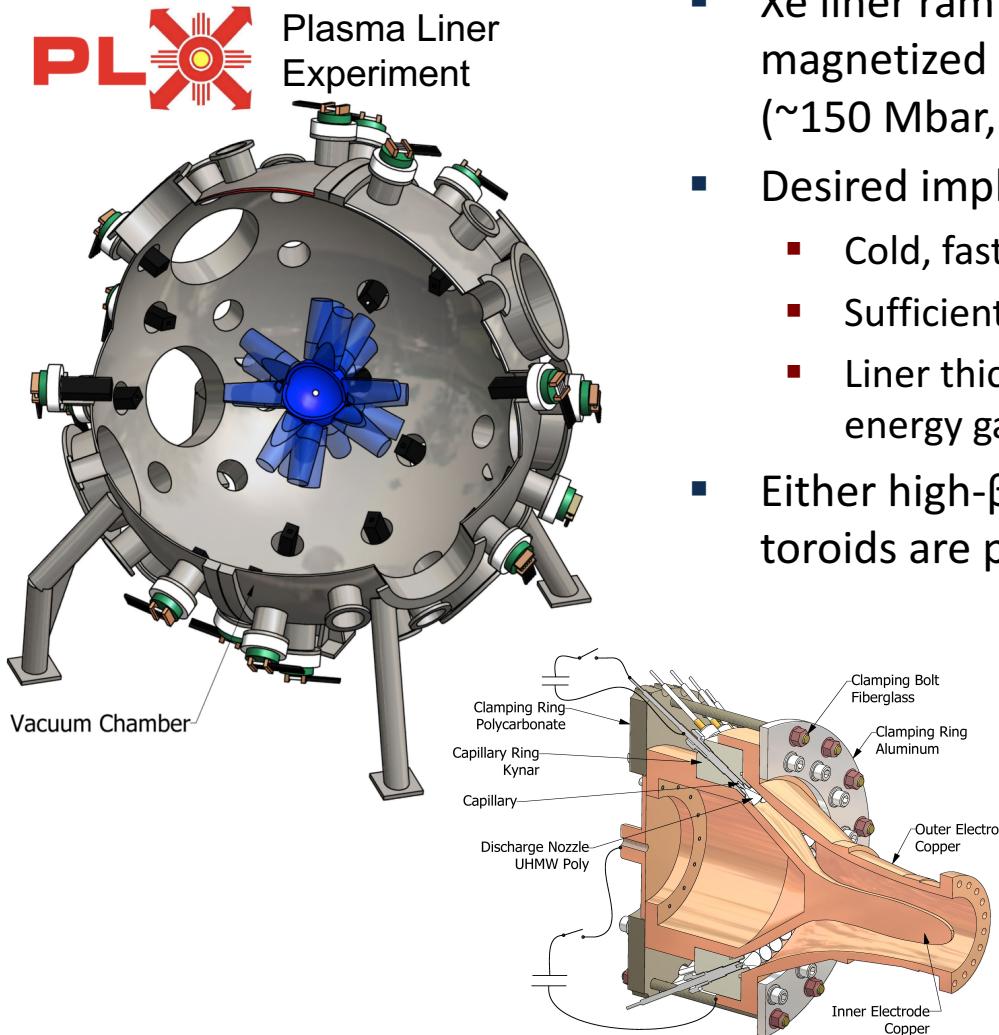
- We have demonstrated the key aspects of the concept:
  - Preheat, compression, magnetic insulation, and trapping of charged fusion products
- Significant challenges remain
  - Sources of fuel contaminants (mix) must be understood and controlled
  - Need to test code predictions of scaling and understanding of critical physics
    - Need higher initial magnetic fields
    - Need to couple more laser energy into the fuel, without generating more mix
    - Need to improve current delivery to target
- High gain may be possible, but large fusion yields can be obtained with relatively low gain

# Summary: MTF is not just ICF the addition of a magnetic field

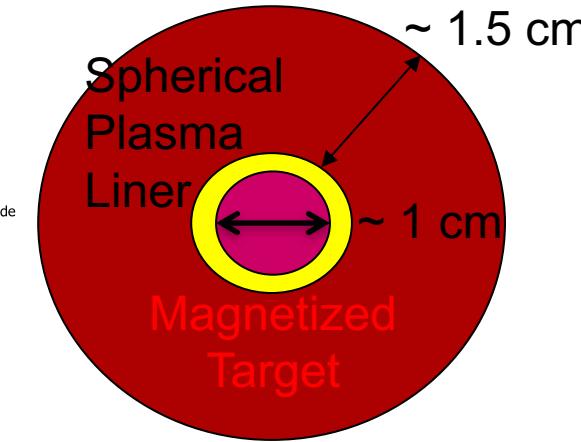
- Lower velocity implosions
  - Less driver power required – less expensive!
  - More massive pushers (liners) leading to longer burn times
  - Lower pressures
- Approximately adiabatic compression (no shocks)
  - ICF targets require exquisite pulse shape control to keep fuel on low adiabat
- Lower density targets
  - reduced radiation rates
  - Bigger targets physically
- Preheat is good!
  - Reduced radial convergence (e.g.,  $< 10$ )
- Alpha deposition characterized by  $rB$ , not  $\rho r$
- Inertial confinement provided by liner (not the fuel)
- Low  $\rho$  with  $B \rightarrow$  new physics regimes

# Other MIF examples

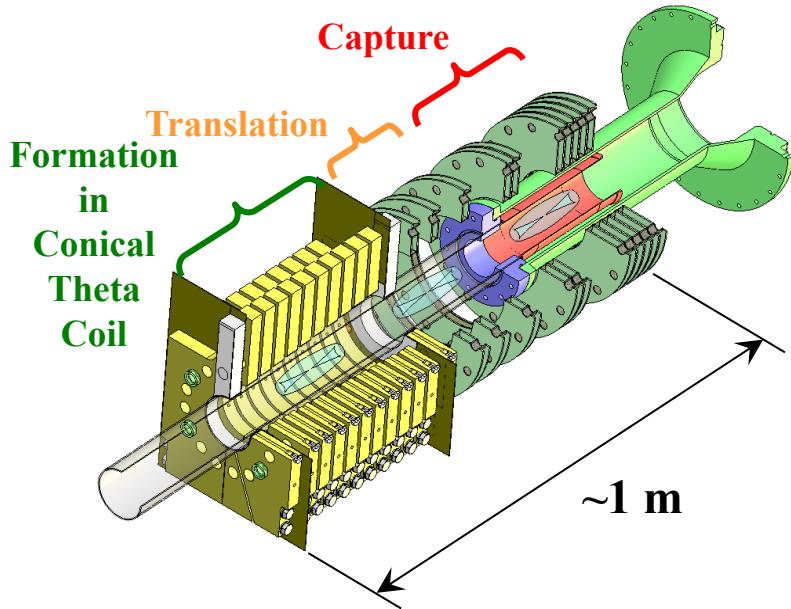
# A team led by Los Alamos will investigate the compression of a magnetized plasma using the merger of supersonic plasma jets (Plasma Jet Driven Magneto-Inertial Fusion)



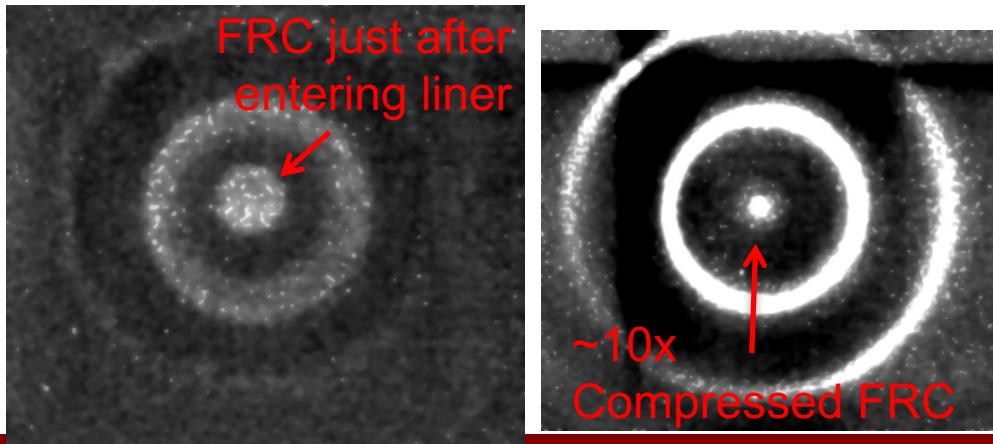
- Xe liner ram pressure ( $\rho v^2$ ) at  $>50$  km/s compresses magnetized target to fusion conditions ( $\sim 150$  Mbar,  $\sim 10$  keV, 300 ns)  $\rightarrow \sim 130$  MJ yield,  $G > 20$
- Desired implosion needs:
  - Cold, fast, highly collisional, high-Z liner, i.e., high Mach #
  - Sufficient uniformity (target convergence ratio  $\sim 10 \times$ )
  - Liner thickness & profiles optimized for dwell (burn) time & energy gain
- Either high- $\beta$  magnetized plasmas or merged compact toroids are potentially suitable targets



# AFRL/LANL led a team that investigated the cylindrical compression of a ~10 cm field-reversed configuration plasma by >10x at >10 microsecond time scales



Formation, translation and capture magnetic coils

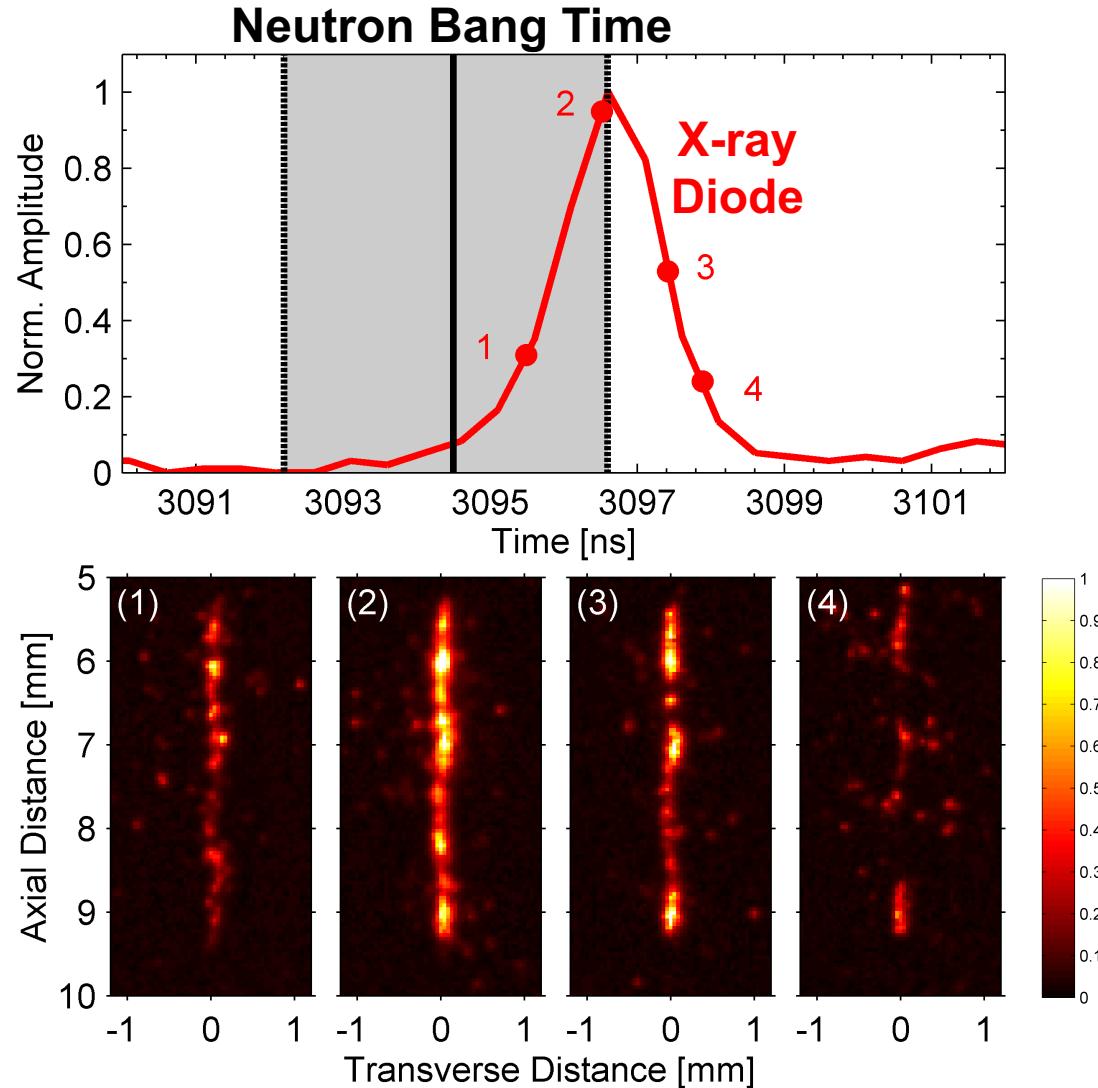


- A compression test was conducted in Oct. 2013.
- Soft x-ray images showed the FRC was compressed to < 0.5 cm diam. (~10x compression), but the plasma was cold (~300 eV based on neutron yield).
- This was the highest density FRC plasma ever created.
- FRC lifetime was too short compared to timescale of compression—stayed cold until the very end of the implosion

J.H. Degnan *et al.* Nuclear Fusion **53**, 093003 (2013).  
C. Grabowski *et al.*, IEEE Trans. Plasma Sci. **42**, pp. 1179-1188 (2014).

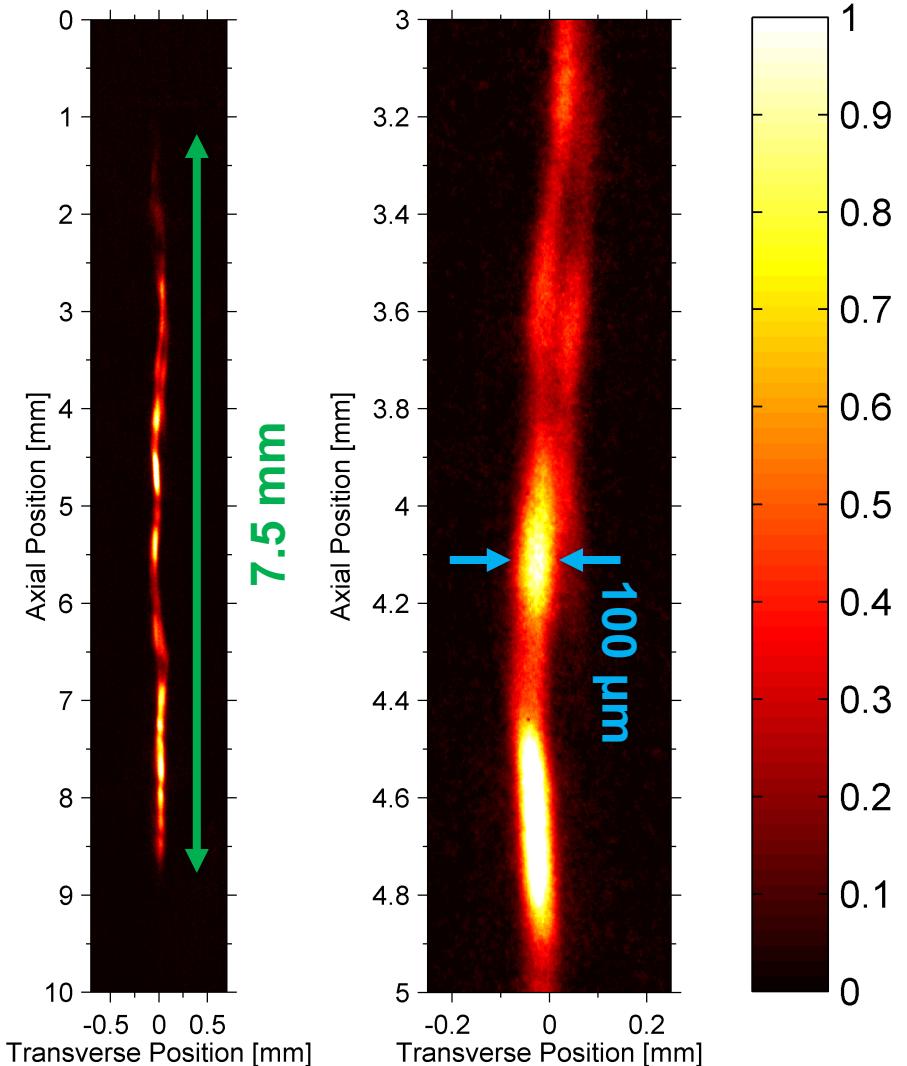
# Backups

# X-ray diodes and time-resolved x-ray pinhole images show the fuel radiating at stagnation



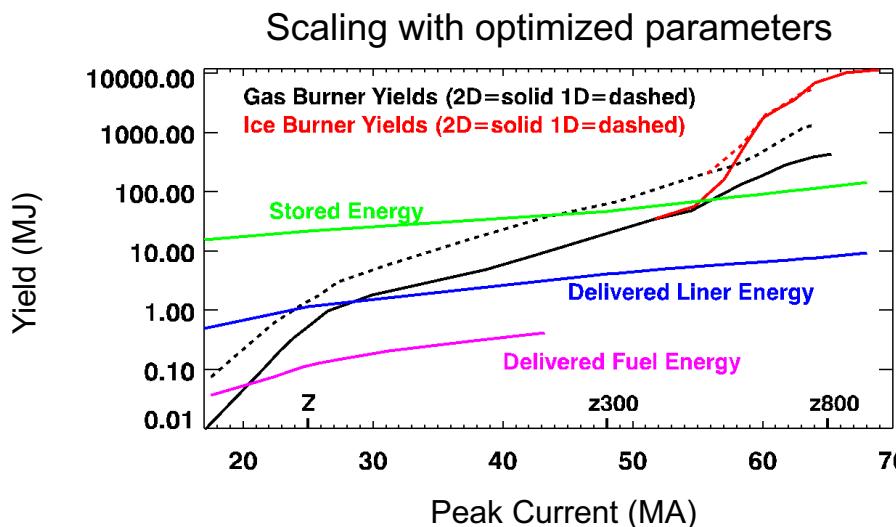
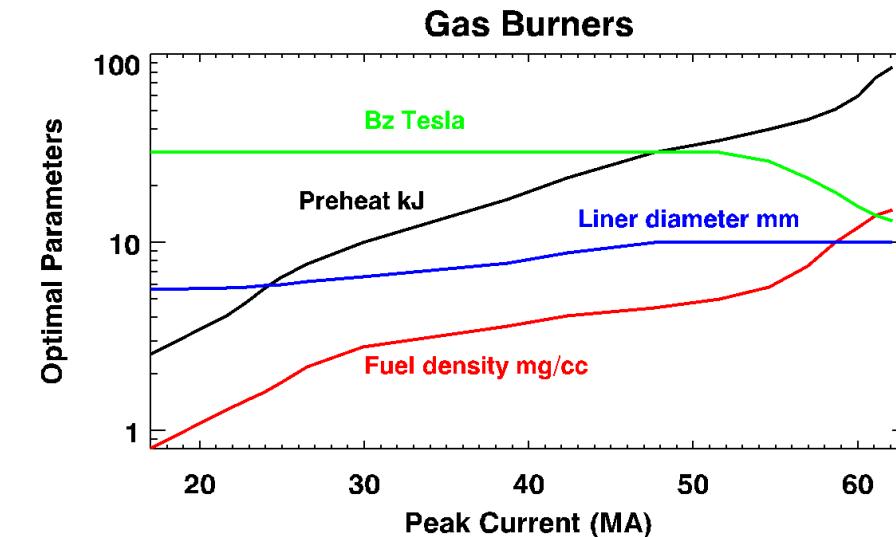
- Heavily-filtered diodes detect a 2 ns FWHM burst of x-rays
- Coincides with the neutron bang time measurement to within timing uncertainties
- Filtered pinhole images during the x-ray burst show a narrow emission column

# Our spherical crystal imaging system was repurposed to record x-ray emission from the fuel



- Hot fuel emission at stagnation gives information about the CR and uniformity of the plasma
- Hot fuel radius is CR  $\sim 45$
- Helical structure to the emission column
- Intensity fluctuations a combination of emission and opacity variations

# Our program plan is to develop platforms that enable testing of optimal configurations for scaling



**Our present experimental configuration is far from optimal**

B-field=10 Tesla (optimum >30 Tesla)

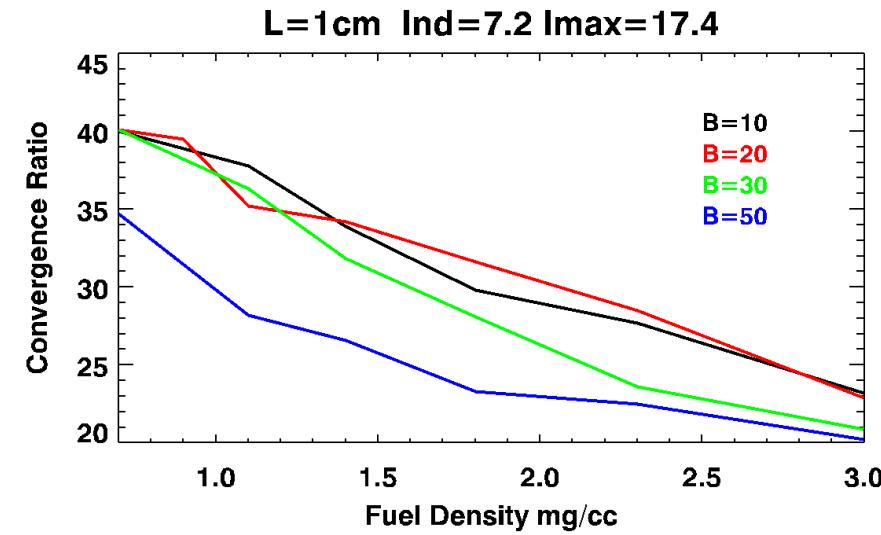
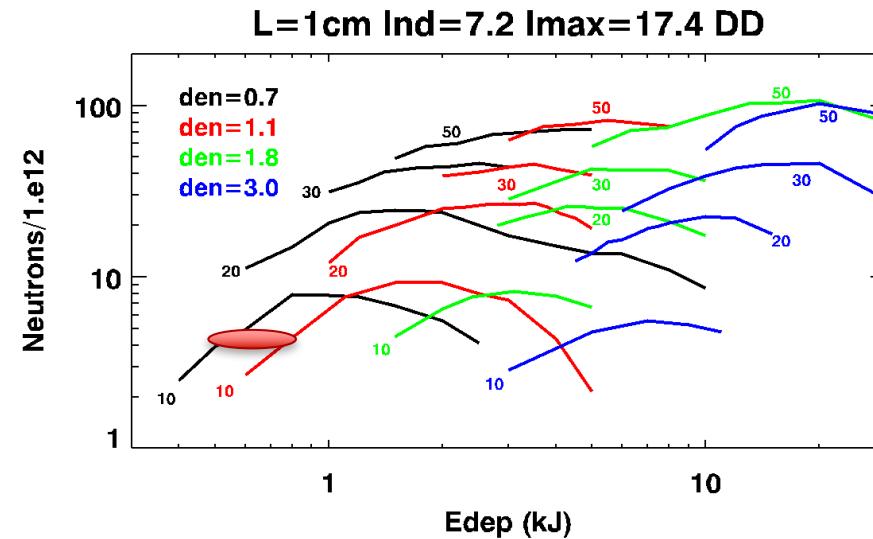
Fuel density=0.7 => **high convergence**

Preheat energy < 1 kJ

Feed inductance 7.2 nH =>  $I_{\max} \sim 17.4$  MA

Simulations predict favorable scaling of yield with drive current<sup>1</sup> when MagLIF parameters are optimized

# Higher initial field is required to test predictions of MagLIF scaling to higher yields



- Larger fields increase the burn time
- Higher fuel densities lower convergence
- Lower inductance feed increases current

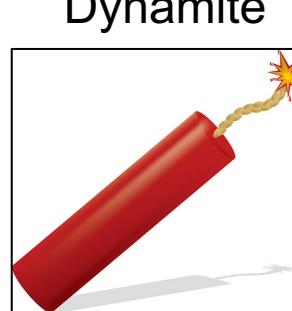
Larger initial magnetic fields are needed!!

# We used pulsed power to create and study *high energy density* (HED) matter

HED conditions are strange on earth, but common in the universe

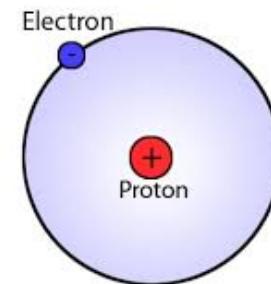


$10^{-5}$  Mbar



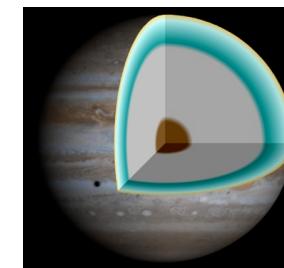
0.1 Mbar

Internal Energy of H atom



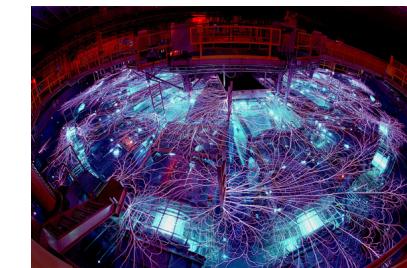
3 Mbar

Metallic H in Jupiter's core



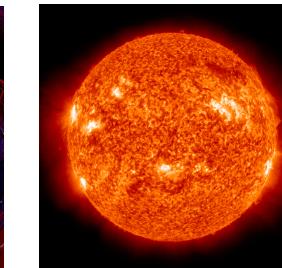
30 Mbar

Z Machine magnetic pressure



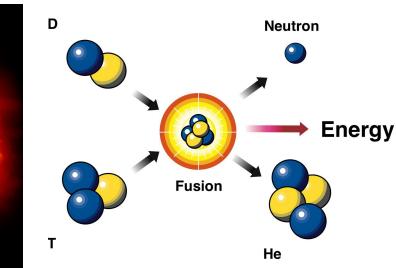
100 Mbar

Center of Sun



250,000 Mbar

Burning ICF plasma



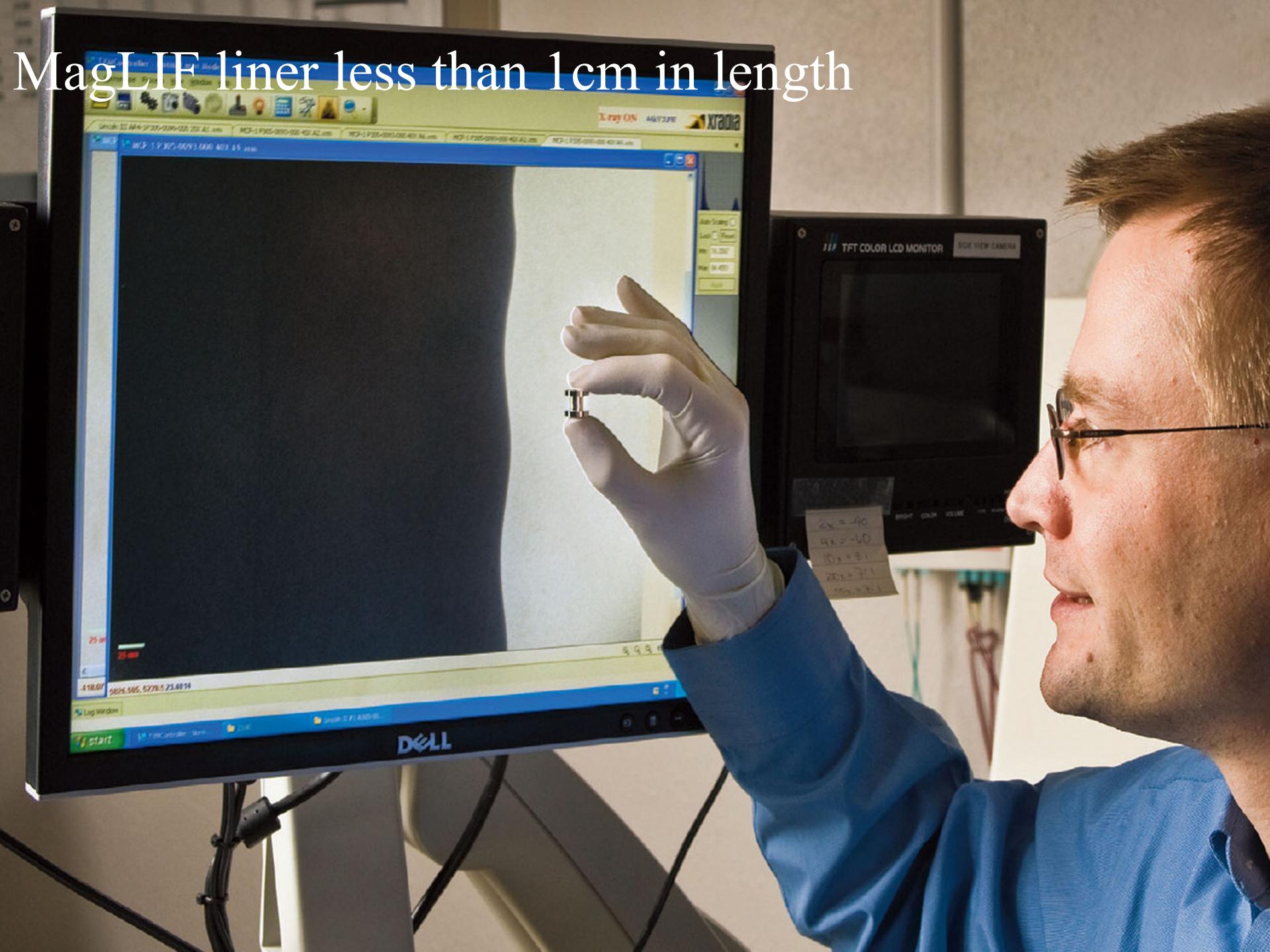
800,000 Mbar

Z can access the HED regime

HED regime ( $P > 1$  Mbar or  $E > 100$  kJ/cm<sup>3</sup>)

← →

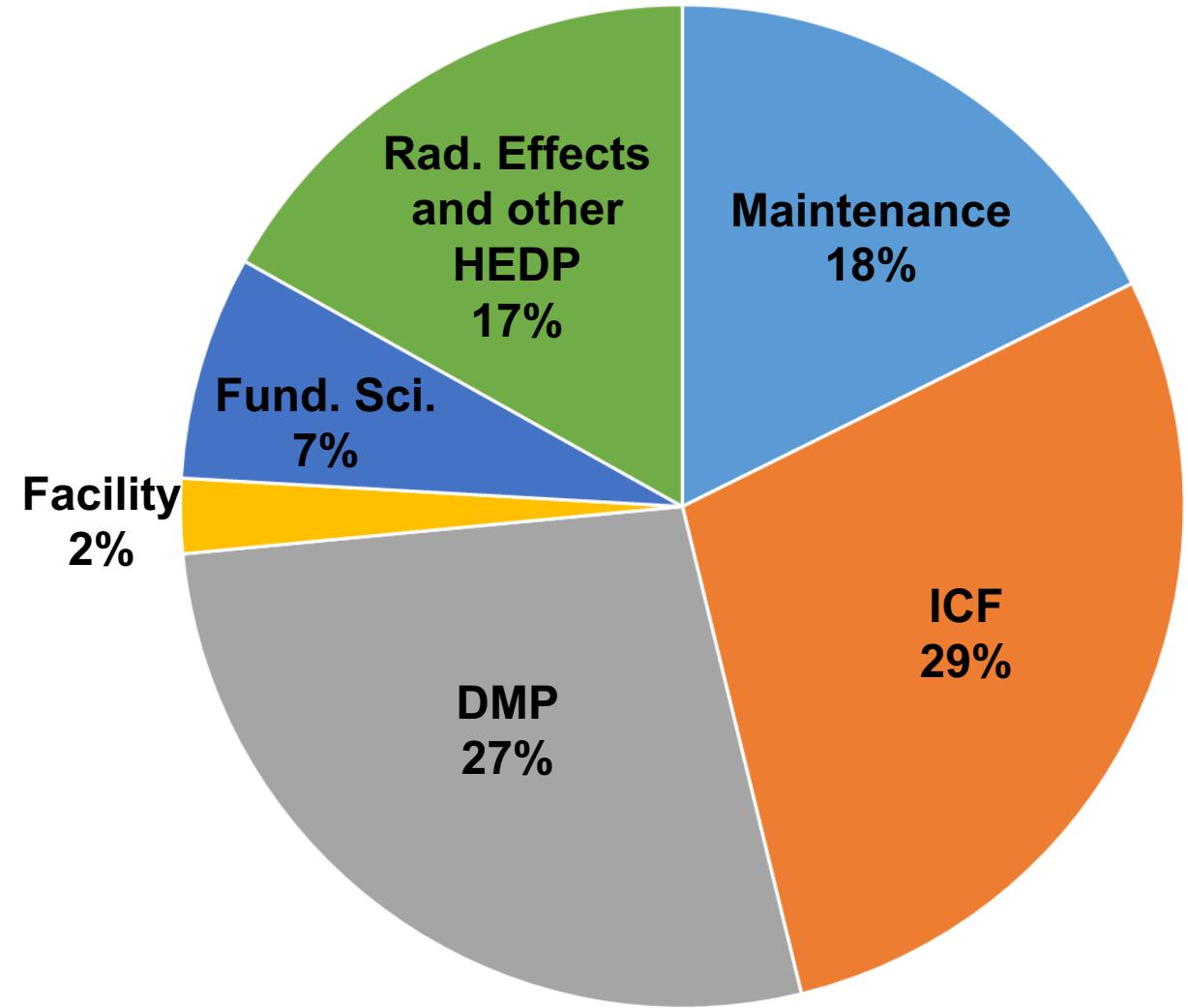
# MagLIF liner less than 1cm in length



# MagLIF hardware ready to load



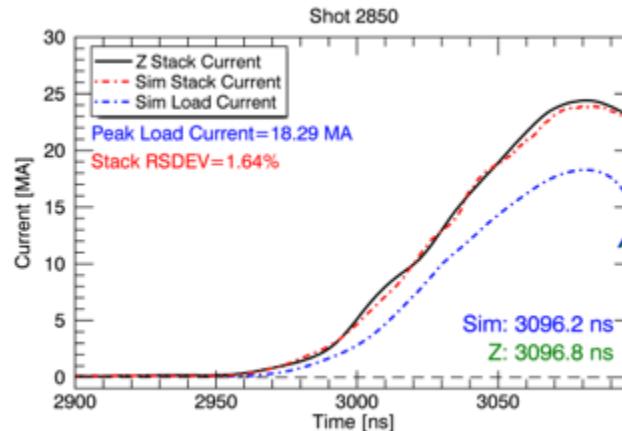
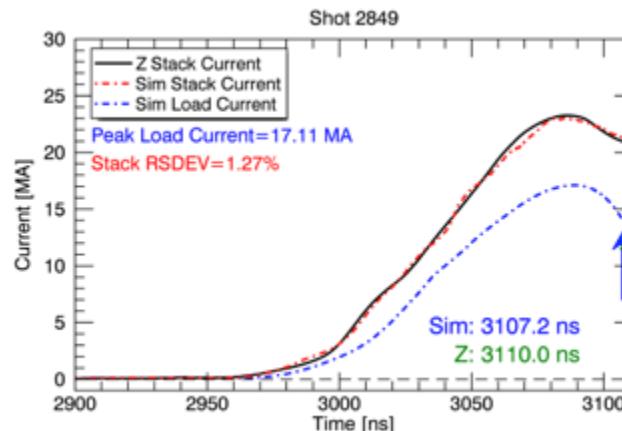
# The Z shot allocation is split between a few major efforts



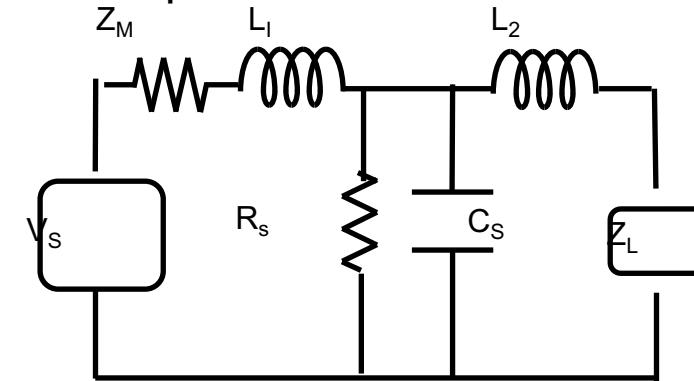
- This is based on our schedule for CY2017
- Approximately 250 working days
- We expect around 160 shots this year
  - Some experiments take more than 1 day to complete
  - We completed an insulator stack rebuild this year (about 20 days)
    - Every few years or so
  - We are rebuilding our transmission line refurbishment facility (about 14 days)
    - Every decade or so

# In MDI, the driver and target are strongly coupled

Adding 2.5mm of liner height (0.8nH) decreases peak current ~1MA



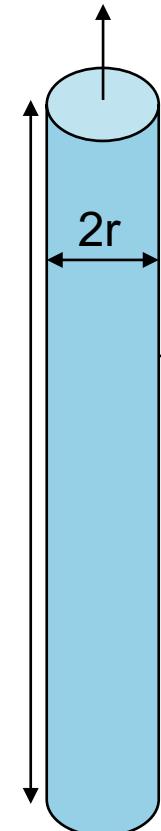
## Simple Circuit Model for Z



- Target inductance must be minimized
  - maximizes current delivery
  - minimizes power flow losses
- Current delivery sensitive to both initial inductance and  $dL/dt$

# Axial Thermal losses are also expected to be acceptable

Axial loss



$$L_{axial} = C\theta^{7/2} (A = 2\pi r^2) (\nabla\theta \sim \theta/L)$$

Radial loss  $L_{rad} = C\theta^{7/2} (A = 2\pi rL) (\nabla\theta \sim \theta/r)$

$$L_{rad}/L_{axial} = (L/r)^2 \sim (0.5/.01)^2 = 2500$$

Axial losses have been addressed with  
fully integrated simulations

# In all concepts, the fuel pressure at stagnation is a key metric of progress

Why is Pressure so important for fusion?

$$\langle \sigma v \rangle \equiv \int \int \sigma(|\mathbf{v}_1 - \mathbf{v}_2|) |\mathbf{v}_1 - \mathbf{v}_2| f(\mathbf{v}_1) f(\mathbf{v}_2) d^3 v_1 d^3 v_2$$

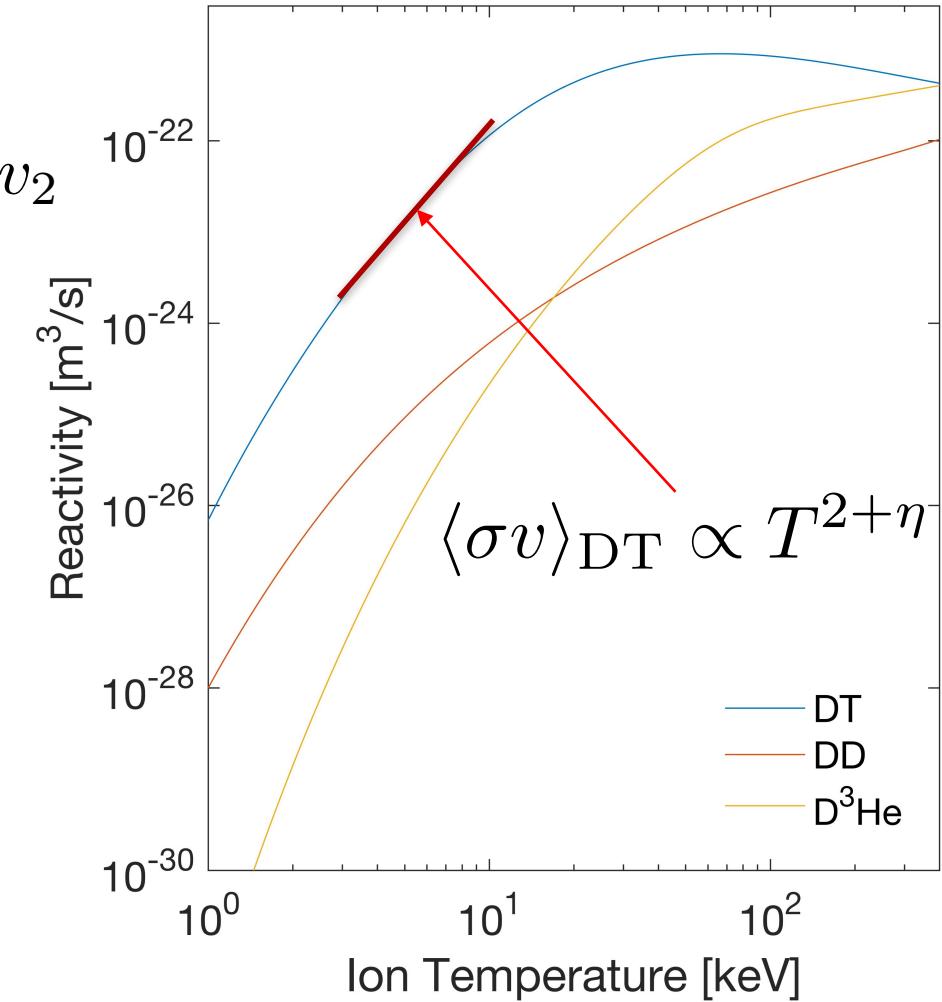
Reaction Rate:

$$f(\mathbf{v}) = \left( \frac{m_i}{2\pi k_b T_i} \right)^{3/2} e^{-\frac{m\mathbf{v}\cdot\mathbf{v}}{2k_b T_i}}$$

$$\mathcal{R}_{\text{fus}} = n_D n_T \langle \sigma v \rangle V$$

$$\mathcal{R}_{\text{fus}} \propto n^2 T^{2+\eta} \propto P^2 T^\eta, \quad \eta \sim 1$$

Pressure is energy density:  $\frac{E_{\text{int}}}{V} = \frac{3}{2} P$



# In all concepts, the fuel pressure at stagnation is a key metric of progress

Why is Pressure so important for fusion?

$$\langle \sigma v \rangle \equiv \int \int \sigma(|\mathbf{v}_1 - \mathbf{v}_2|) |\mathbf{v}_1 - \mathbf{v}_2| f(\mathbf{v}_1) f(\mathbf{v}_2) d^3 v_1 d^3 v_2$$

$$f(\mathbf{v}) = \left( \frac{m_i}{2\pi k_b T_i} \right)^{3/2} e^{-\frac{m\mathbf{v}\cdot\mathbf{v}}{2k_b T_i}}$$

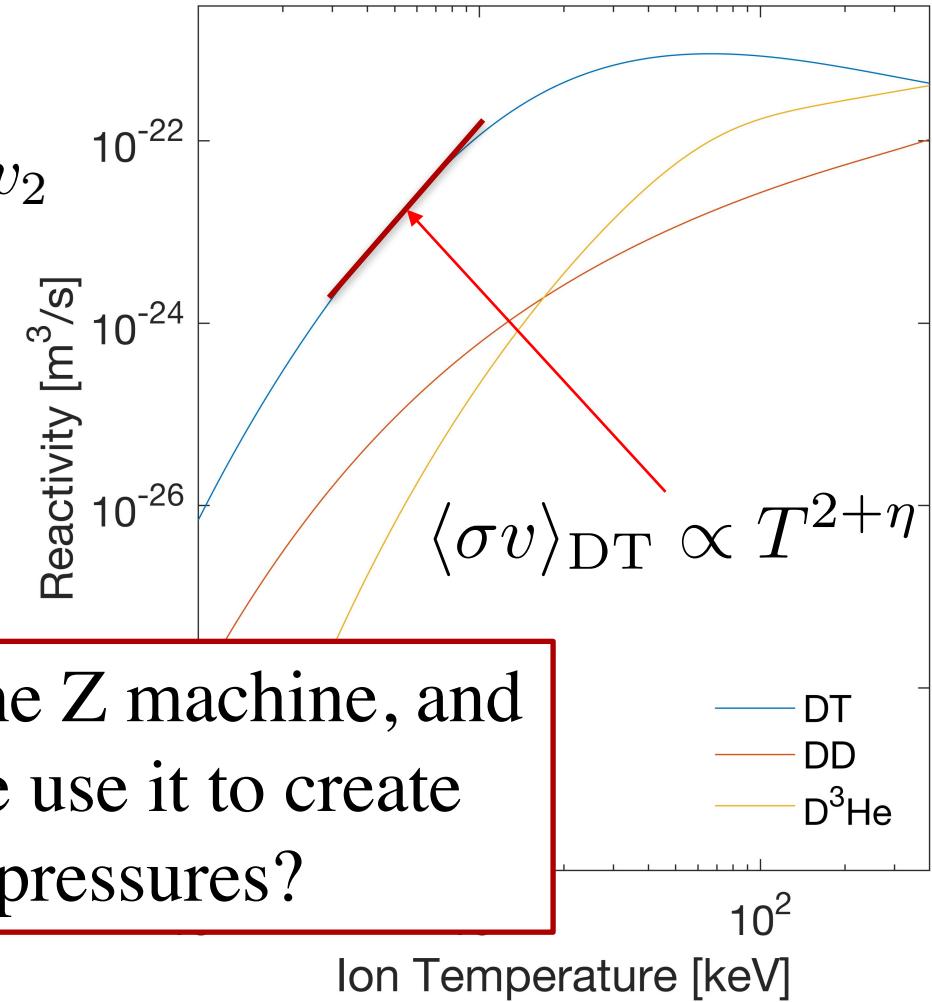
Reaction Rate:

$$\mathcal{R}_{\text{fus}} = n_D n_T \langle \sigma v \rangle V$$

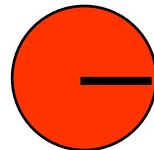
$$\mathcal{R}_{\text{fus}} \propto n^2 T^{2+\eta} \propto P^2 T$$

Pressure is energy density:  $\frac{E_{\text{int}}}{V} = \frac{3}{2} P$

So what is the Z machine, and how do we use it to create high pressures?



# For hot spot ignition fusion fuel must be brought to a pressure of a few hundred billion atmospheres



$\rho, R, T$

For ignition conditions:

$$\left\{ \begin{array}{l} \rho R \approx 0.4 \text{ g/cm}^2 \\ T \approx 5 \text{ keV} \end{array} \right\}$$

$$E_{HS} \propto m_{HS} T_{HS} \propto \rho_{HS} R_{HS}^3 T_{HS} \propto \frac{(\rho_{HS} R_{HS})^3 T_{HS}^3}{P_{HS}^2}$$

$$P_{HS}^2 \sim (CR)^6$$
$$\sim (\text{velocity})^6$$

$$E_{NIF} \sim 15 \text{ kJ} \Rightarrow P \sim 400 \text{ GBar}$$

$$R \sim 30 \mu\text{m} \Rightarrow \text{ and } \rho \sim 130 \text{ g/cm}^3$$

This is consistent with detailed calculations

Note: The key challenge for ICF is to make the fuel both **dense** and **hot**. This leads to challenging compression requirements—a NIF capsule has a radial convergence of 35-45x, for a volume compression of ~50,000!

# Technological limitations also limit laboratory yield

## Imagine hollow shell of fuel:

- Implosion velocity sets drive pressure:

$$M_{\text{shell}} = 4\pi R_0^2 \Delta R_0 \rho_{\text{shell}}$$

$$\dot{V}_{\text{shell}} \sim \frac{u_{\text{imp}}}{t_{\text{imp}}} \sim \frac{u_{\text{imp}}^2}{R_0}$$

$$P_{\text{drive}} \sim \frac{M_{\text{shell}} \dot{V}_{\text{shell}}}{R_0^2} \sim \frac{\Delta R_0 u_{\text{imp}}^2}{R_0}$$

$$\equiv \frac{u_{\text{imp}}^2}{A}$$

- Implosion energy converts to heat at stagnation:

$$E_{\text{fuel}} \sim N k_B T \sim M_{\text{shell}} u_{\text{imp}}^2$$

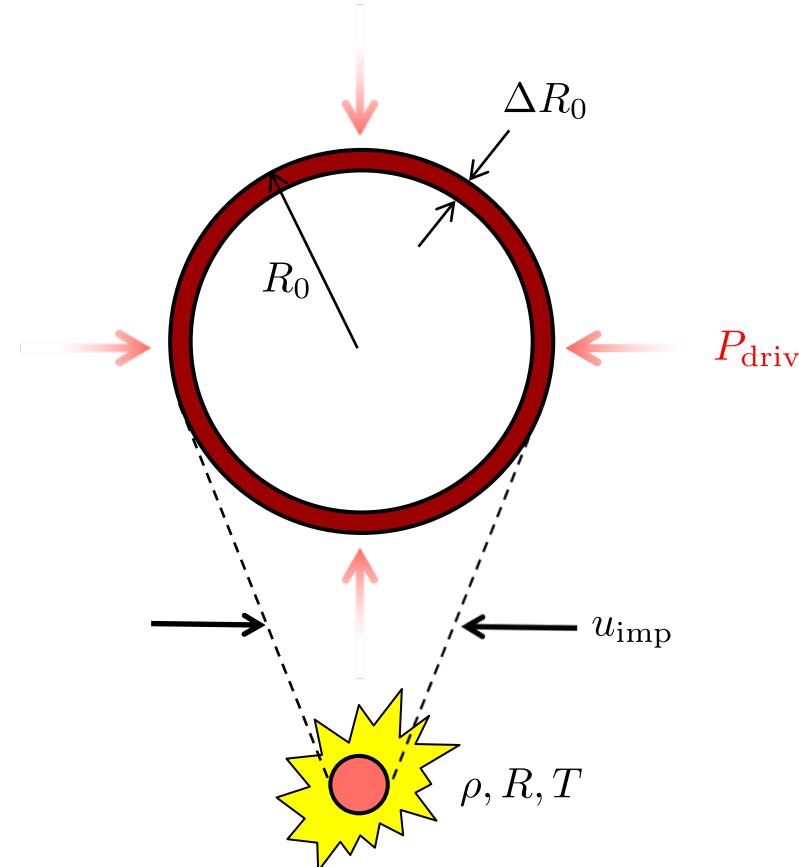
$$\sim \frac{(\rho R)^3}{\rho^2} P_{\text{drive}} A$$

$$\sim \frac{P_{\text{drive}} A^3}{(CR)^6}$$

$A > 1$  (i.e., thin shell) reduces  $P_{\text{drive}}$  needed

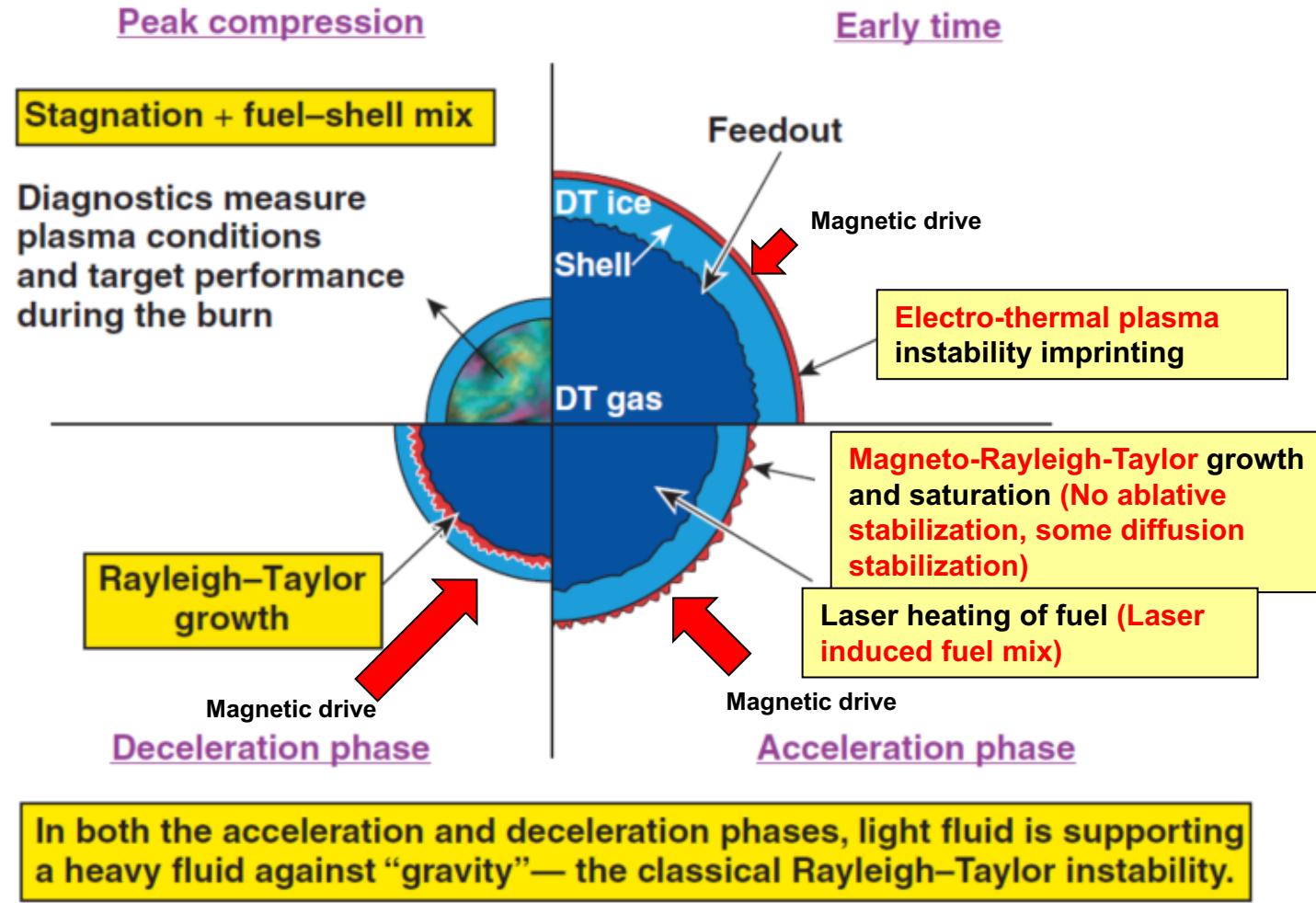
$CR \sim 30 - 40$  set by  $\rho R$  requirements

- Large compression requires enormous pressures! Limited in the laboratory to  $O(100 \text{ Mbar})$

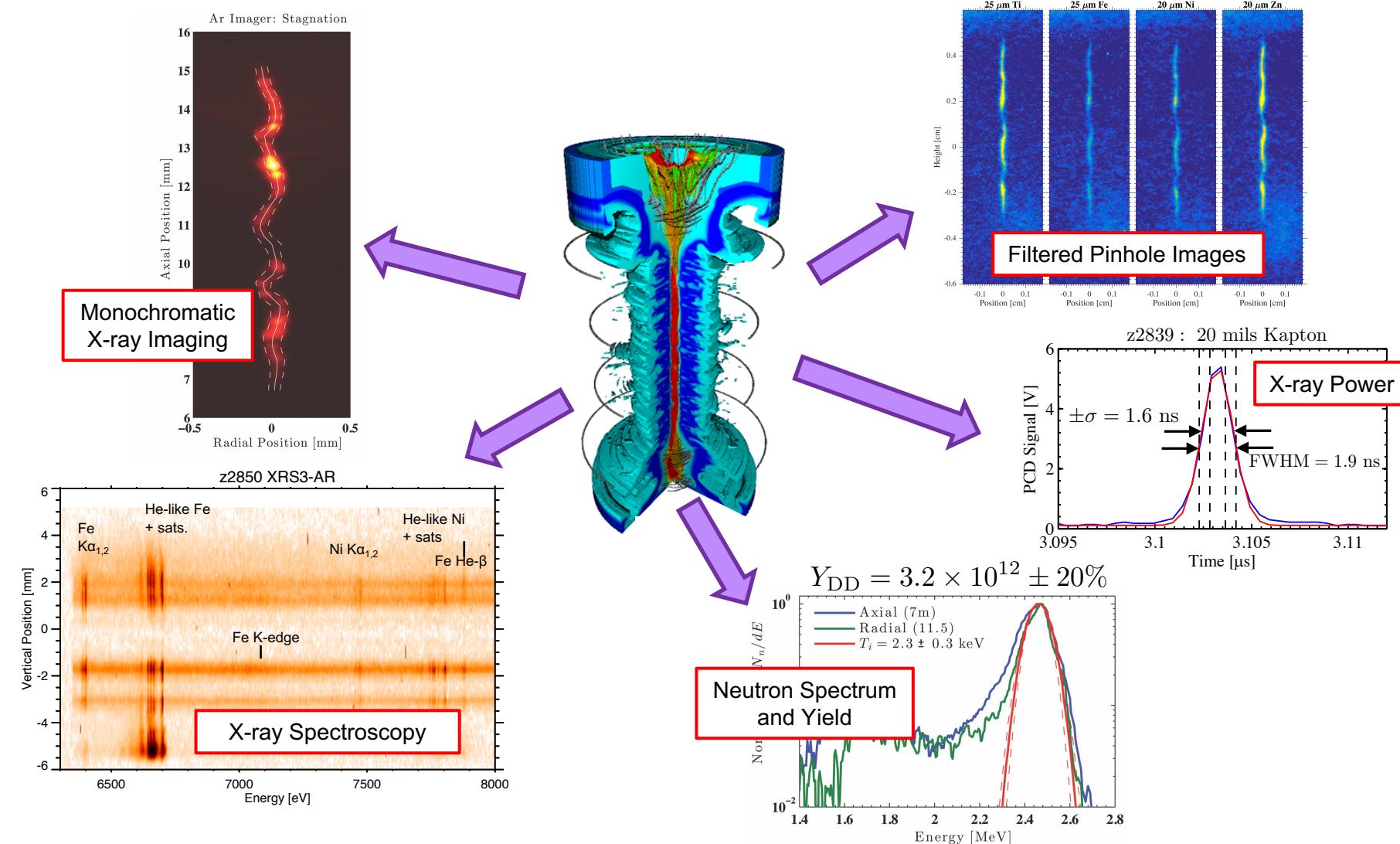


# Magnetically driven implosions have similar challenges with respect to ICF instabilities

## Cylindrical magnetically driven implosions



We have demonstrated key aspects of magneto-inertial fusion on Sandia's Z facility



- Our extensive suite of diagnostics allow us to measure the fuel temperature, density, volume, magnetic field, and burn duration
  - Neutron yield and time-of-flight
  - x-ray imaging and spectroscopy
  - Radiated power and energy

# The Z-Beamlet laser at Sandia\* is being used to radiograph liner targets and heat fusion fuel



Z facility



Z-Beamlet (ZBL) is now routinely used to deliver up to 4.5 kJ of  $2\omega$  light in a 6 ns time window

An advantage of laser heating is that it can be studied and optimized without using Z

