



OMVPE Growth of Al-rich AlGa_N Alloys for Power Electronics

Andrew Allerman, M.H. Crawford, G.W. Pickrell,
R.J. Kaplar, A.M. Armstrong, J.R. Dickerson,
B.A. Klein, M.P. King, & M.S. Van Heukelom

Sandia National Laboratories, Albuquerque, NM

Acknowledgements:

M. Smith, K. Cross, and V. Abate

- Wide bandgap AlGa_N alloys for power electronics
- PN diodes Al_xGa_{1-x}N ($x = 0.3$)
 - Growth of thick, N- drift layers
 - Breakdown voltage and forward ON resistance
- PN diodes Al_xGa_{1-x}N ($x = 0.7$)
 - Growth of low compensation of N-type drift layer
 - Approaches for p-side of diode
- Summary

Ultra-wide-bandgap semiconductors (UWBS, >4eV) for power electronics

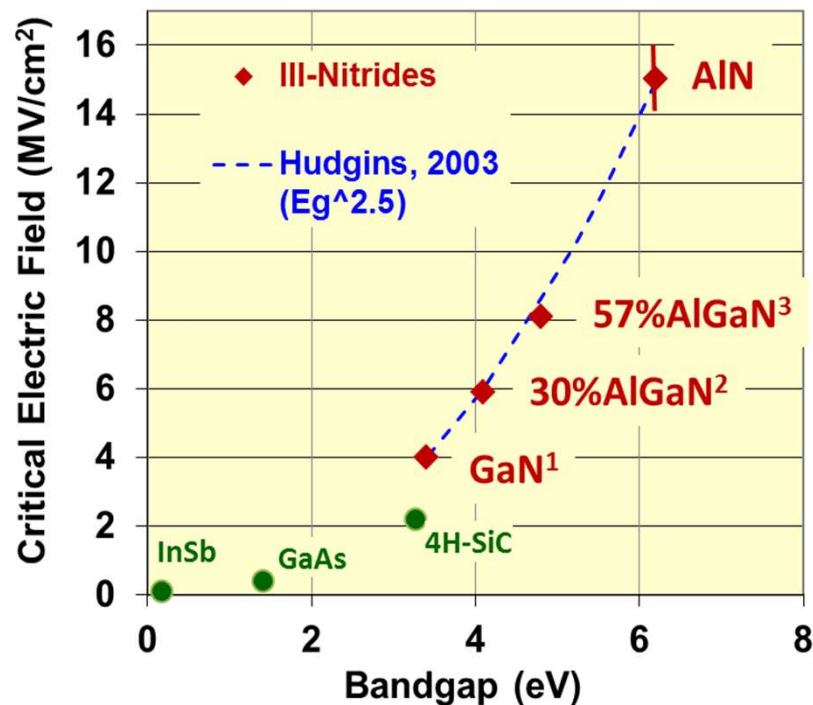
Critical Electric Field (MV/cm)

$$E_c \propto E_g^{2.5} \quad (\text{Direct gap})$$

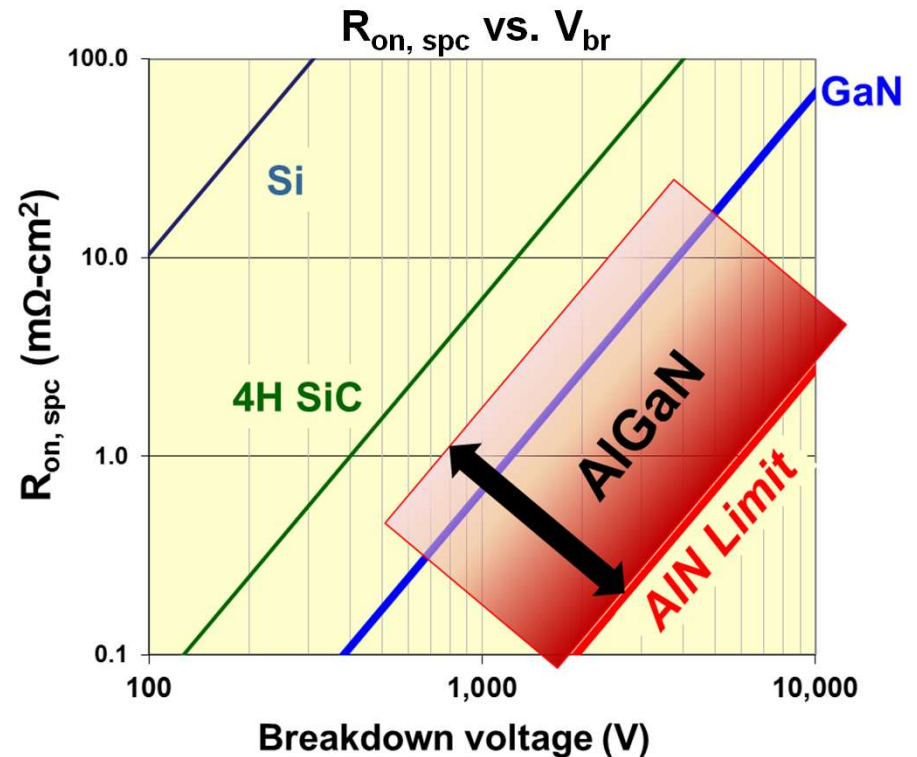
Unipolar Figure of Merit (vertical devices)

$$UFOM = \frac{V_{br}^2}{R_{on,sp}} = \frac{1}{4} \epsilon \mu E_c^3 \propto E_g^{7.5}$$

Critical Electric Field vs. Bandgap



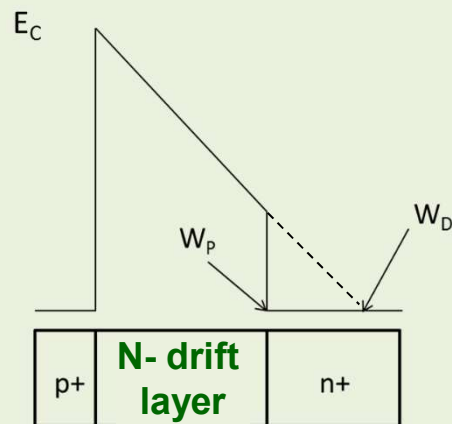
1-Armstrong, EL 2016, 2-Allerman, EL 2016, 3-Nisikawa, JpnJAP 2007



Breakdown voltage of drift layer: doping and thickness

Punch-Through

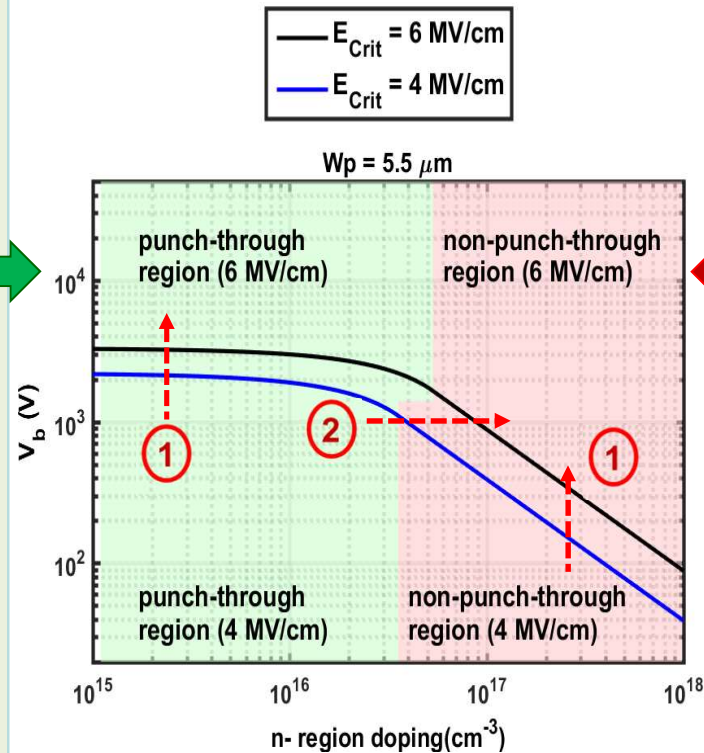
$$W_P < W_D$$



$$V_{br} = E_C W_P - \frac{q N_D W_P^2}{2\epsilon}$$

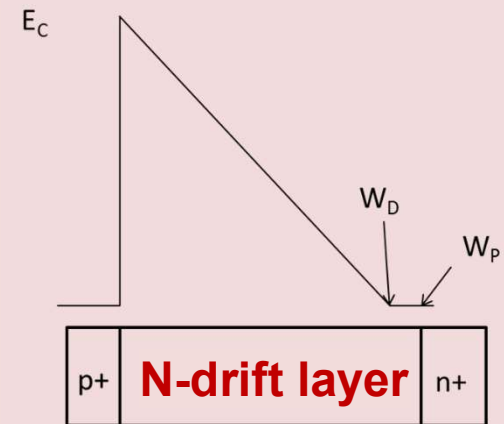
- N_d is lower than optimal

➔ Thickness determines V_{br}



Non-Punch-Through

$$W_P \geq W_D$$



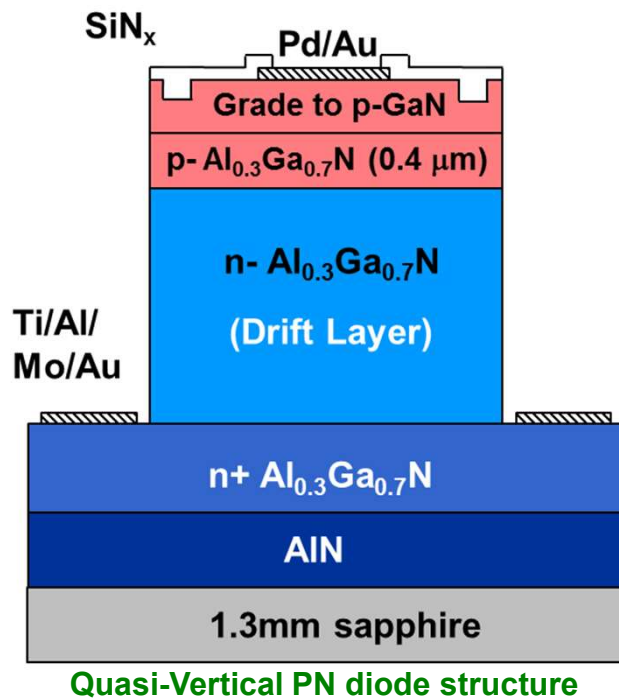
$$V_{br} = \frac{\epsilon E_C^2}{2q N_D}$$

- Drift layer is thicker than optimal

➔ N_d determines V_{br}

$\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ “Quasi-Vertical” PN diode on sapphire

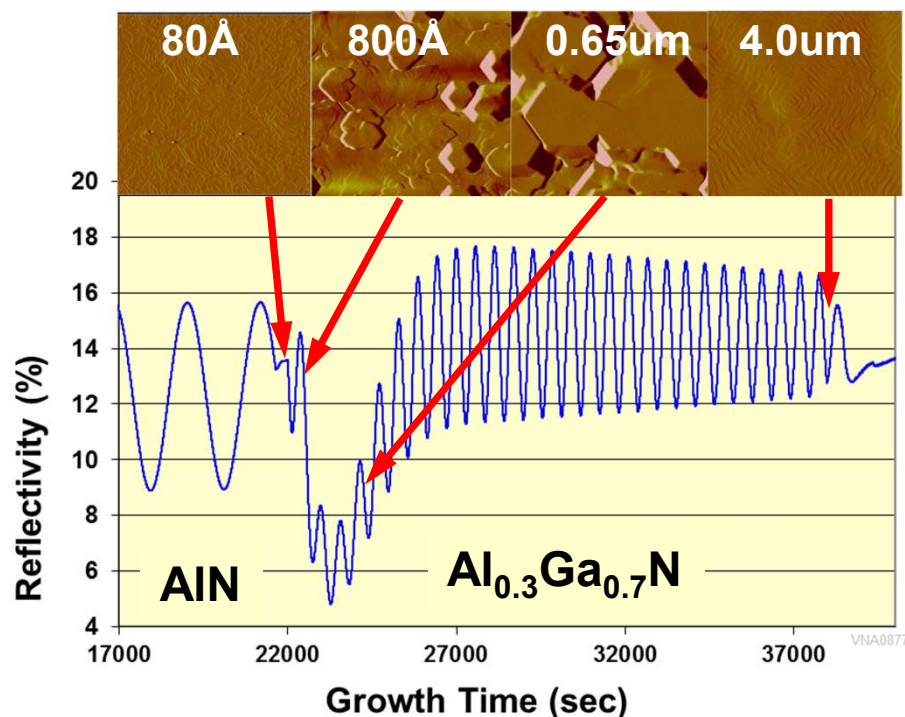
Quasi-Vertical diode structure and processing



- Implanted junction edge termination
- Mesa & p-metal dia.: 300 - 50 μm
- $\text{p-Al}_{0.3}\text{Ga}_{0.7}\text{N}$: 1025 $^{\circ}\text{C}$, 2-4 $\Omega\text{-cm}$, 0.4 μm
[Mg] = $2\text{-}4 \times 10^{19} \text{ cm}^{-3}$
- *Drift Layer: 4.3, 5.5, 7.5, 9, 11 and 15.5 μm*
- Total epi thickness: 7 – 18, 22 μm
- Crack-free (except 15.5 μm drift layer)
- Drift layer doping: mid 10^{15} – mid 10^{16} cm^{-3}
Mobility: 150 cm^2/Vs
- Sheet resistance: 40-80 $\Omega/\text{sqr.}$
- *Threading dislocation density: $1\text{-}3 \times 10^9 \text{ cm}^{-2}$*

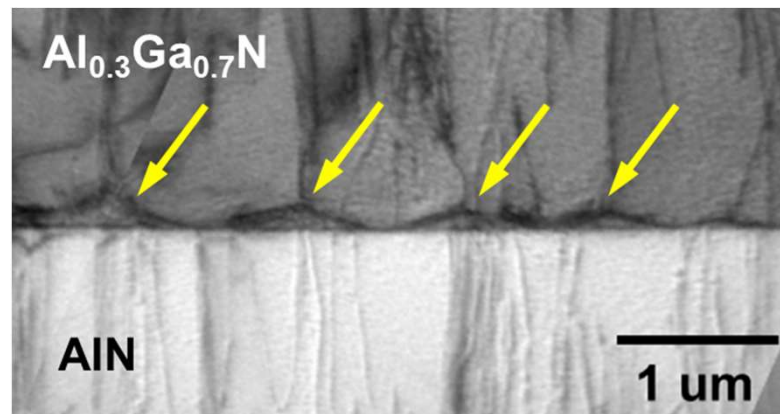
Relaxation and TDD reduction in $\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ on AlN

In-situ Reflectance and AFM



- Surface roughens (3D growth) and then planarization (2D growth)
- $\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ layer is >80% relaxed,
TDD $\sim 2\text{-}4 \times 10^9 \text{ cm}^{-3}$

Cross-section TEM



S. Lee, D. Follstaedt, J. Floro 2009

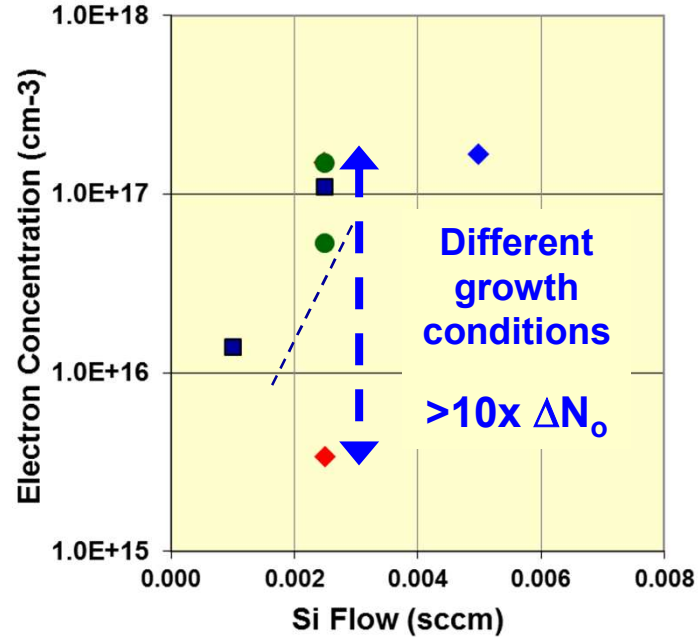
- Strain is relieved by interfacial misfit dislocation networks with hexagonal boundaries
- Threading dislocations “bundle” into triangular features

➔ *2D to 3D to 2D growth relieves strain & lowers TDD*

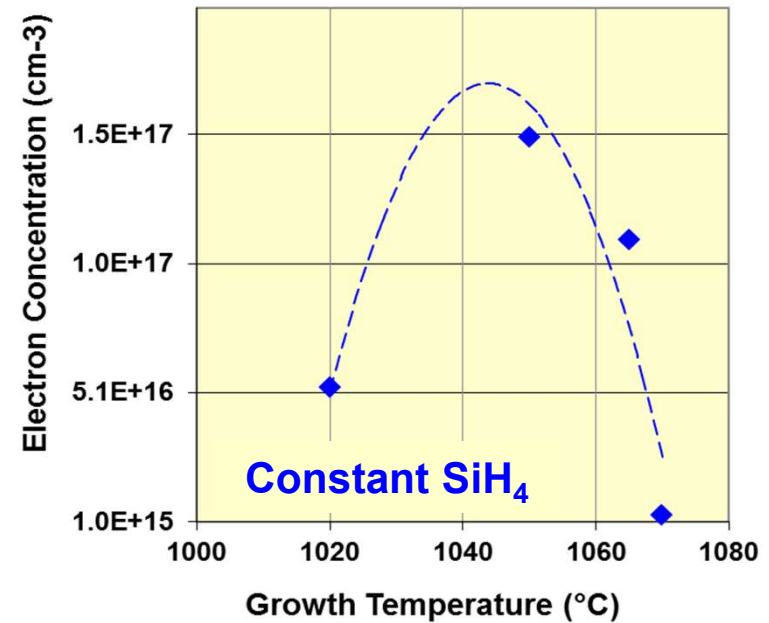
Control of N-type doping of drift region ($\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$)

➔ *Si incorporation is linear in SiH_4 flow but...*

**Electron concentration (hall)
vs. SiH_4 flow (30%AlGaN)**



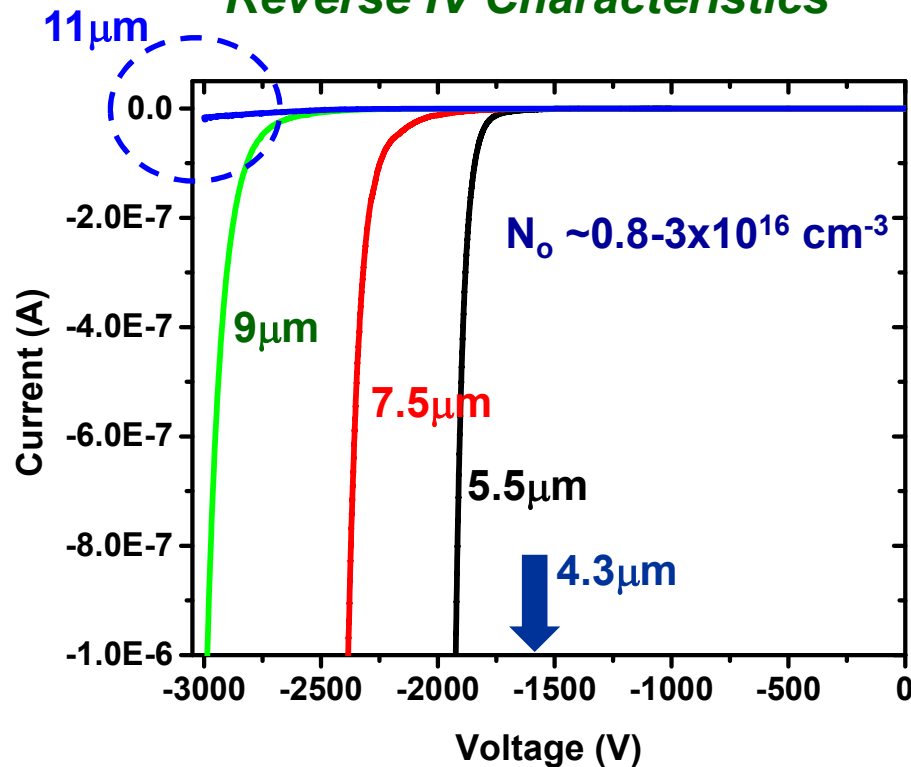
**Electron concentration (hall)
vs. growth temperature (30%AlGaN)**



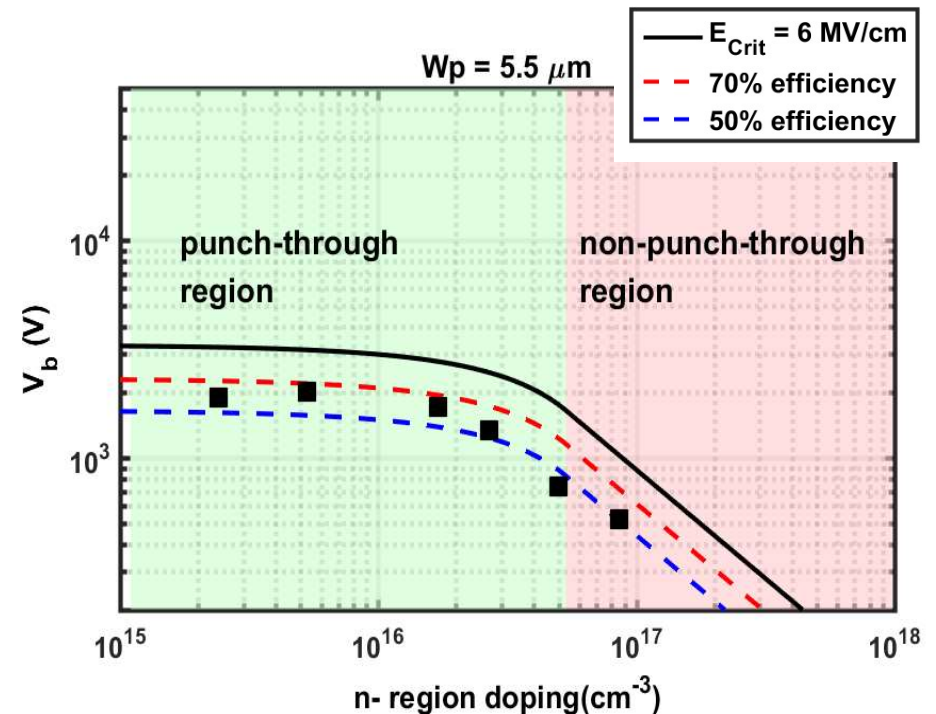
➔ *... electron concentration is highly dependent on growth condition (i.e. the density of compensating defects)*

$\text{Al}_{0.3}\text{Ga}_{0.7}\text{N}$ “Quasi-Vertical” PN diode – thicker drift layers

Reverse IV Characteristics



Breakdown Voltage vs. Drift doping



- Breakdown voltages $\sim 3000\text{V}$ (Drift: 9 & 11 μm)
- V_{br} increases with drift layer thickness for N_o

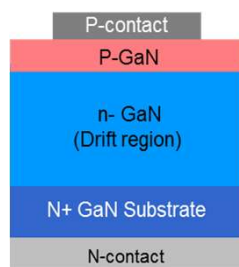
➔ $E_c \sim 5.9 \text{ MV/cm}$

- N_o of devices measured by CV

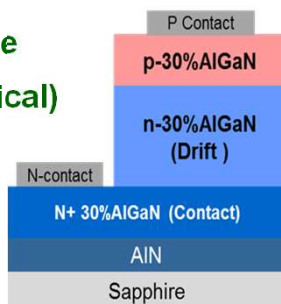
➔ JTE is 50 – 70% effective
(assumes $E_{\text{crit}} = 6 \text{ MV/cm}$)

Breakdown voltages reported for III-Nitride PN diodes

**GaN diode
(vertical)**



**AlGaN diode
(Quasi-vertical)**



III-N PN diodes with > 3 kV breakdown voltage

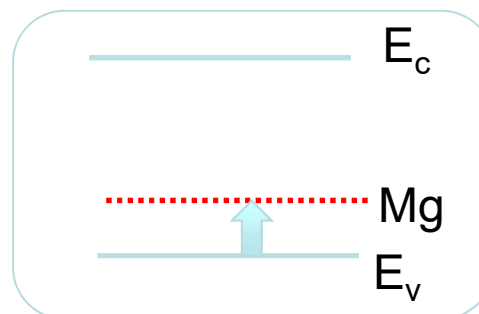
Breakdown (kV)	No (cm ⁻³)	Drift (μm)	Material	Group	Ref
4.7	2/9/16e15	33	GaN	Hosei Univ.	EDL 36p1180_2015
4.0	2-5e15	40	GaN	Avogy	EDL 36p1073_2015
3.9	3e15	30	GaN	Sandia	EL 52p1170_2016
3.7	5e15	>30	GaN	Avogy	EDL 35p247_2014
3.48	1/3/12e15	32	GaN	Hosei Univ.	IEDM15-237_2015
>3	0.8-3e16	11	30%-AGaN	Sandia	This work
3.0	0.8-3e16	9	30%-AGaN	Sandia	This work
3.0	1/10e15	20	GaN	Hitachi	Jpn J Appl Phys 52 p028007_2013

Advantages of wide-bandgap III-Nitride

	GaN	Al _{0.3} Ga _{0.7} N	
N _o (cm ⁻³)	low e15	low e16	] ← Larger E _c (larger E _g)
Drift (μm)	20-30	~10	
TDD (cm ⁻²)	≤ 1e6	low 1e9	← Higher reverse leakage

Approaches to $\text{Al}_{0.70}\text{Ga}_{0.30}\text{N}$ PIN Diodes

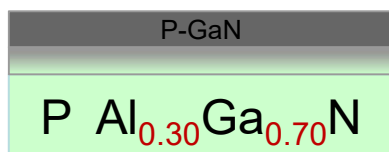
P-type doping very challenging
with increasing Al:
 $E_a(\text{GaN}) \sim 180 \text{ meV}$
 $E_a(\text{AlN}) \sim 500 \text{ meV}$



$kT \sim 0.026 \text{ eV}$
Thermal activation of
holes not viable for high-
Al alloys

Device Designs

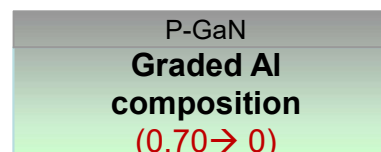
Heterostructure



Homojunction



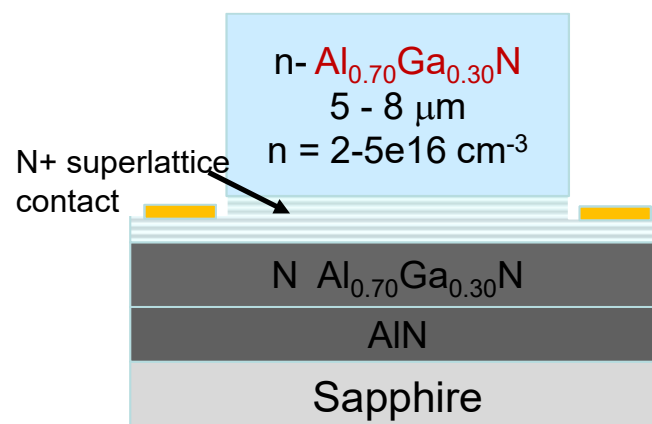
Polarization-doped



p-Superlattice



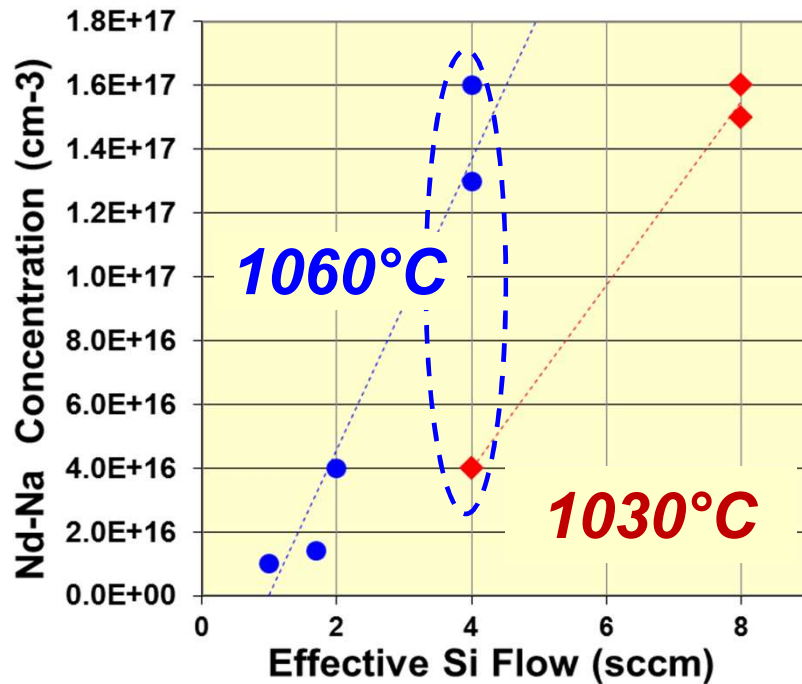
“Quasi-vertical” on sapphire: Common design except for p-side



Vertical on n-GaN: ultimate goal

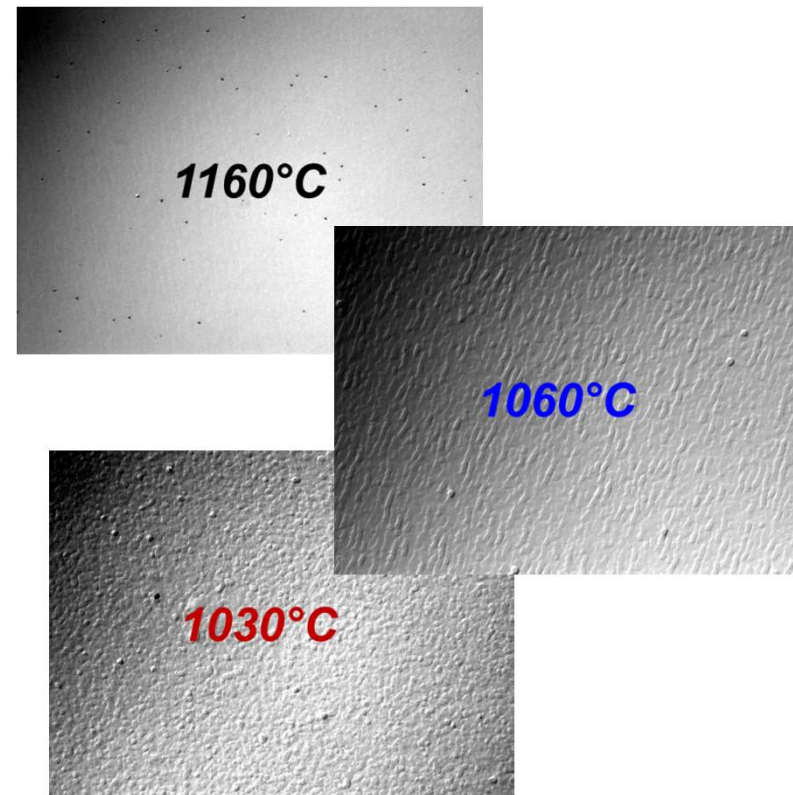
Compensation of Si doped drift region (70%-AlGaN)

*Electron concentration (CV)
vs. SiH₄ flow (70%AlGaN)*



- ➔ Compensation is lower at 1060C
- ➔ TDD, NH₃, pressure *ALL* affect compensation

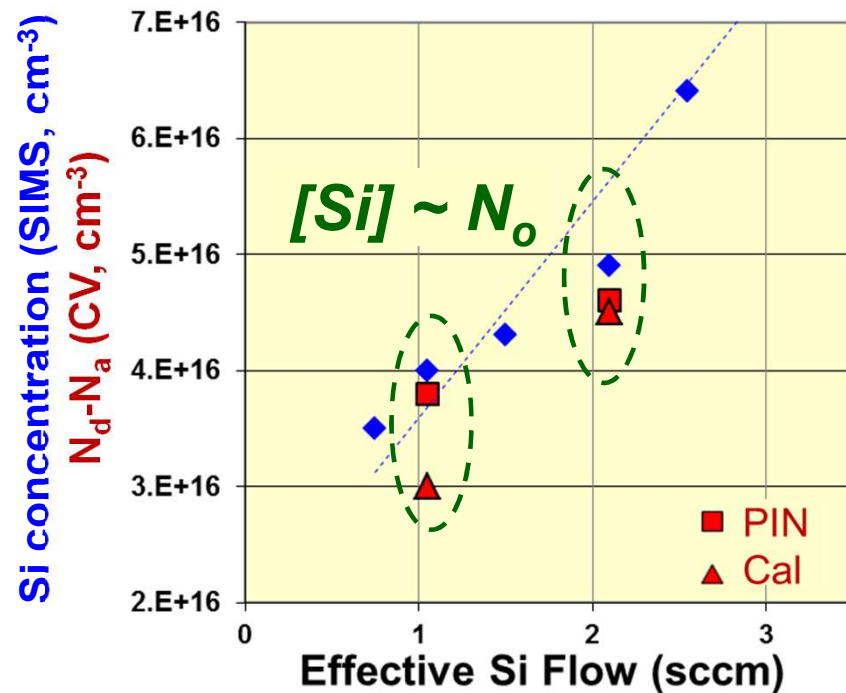
Nomarski DIC (50x) of 70%-AlGaN



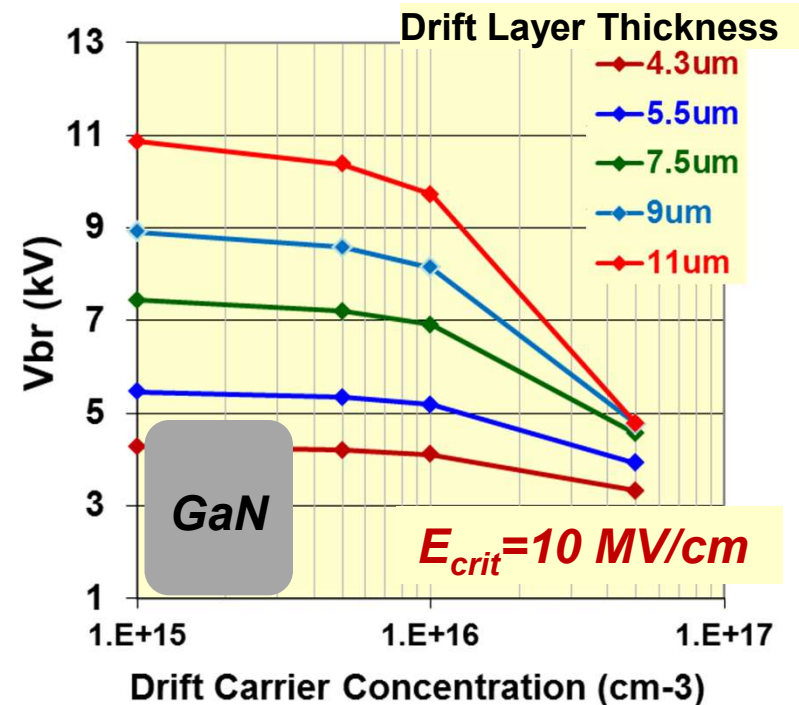
- ➔ Surface morphology depends on growth temperature (and AlN)

Compensation of Si doped drift region (70%-AlGaN)

*Si & electron concentration (CV)
vs. SiH₄ flow (70%AlGaN)*



*Calculated V_{br} (kV) for N_o & thickness
(70%AlGaN)*

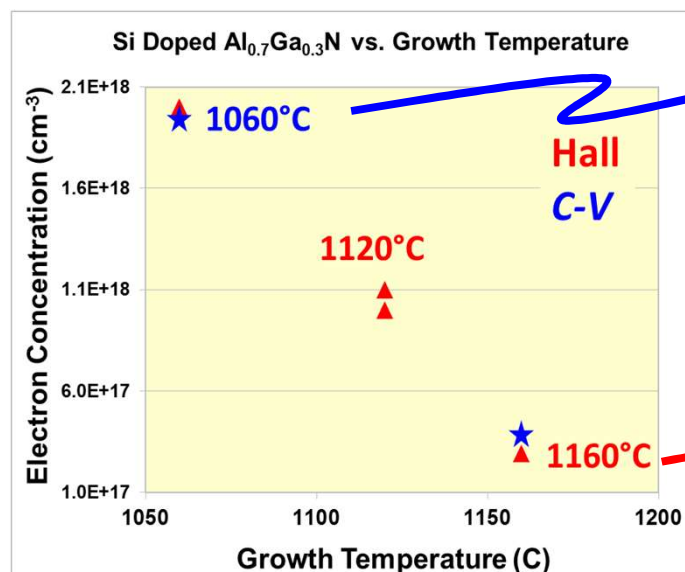


- ➡ Donor compensation ~ 1e16 cm⁻³
- ➡ Similar to GaN!

- ➡ N_o ~ 1e16 cm⁻³ for ~10 kV
- ➡ Si doping is above the level of compensation

Growth temperature & compensation in Si-doped 80%AlGaN

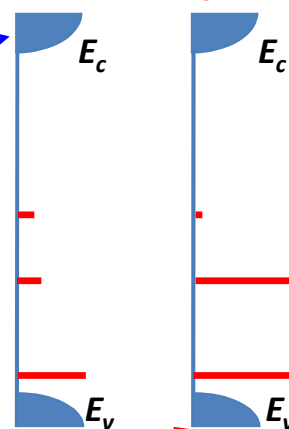
Electron concentration in Si-80%AlGaN



Armstrong JAP 117 (2015)

Deep level traps in Si-80%AlGaN

$T_g = 1060^{\circ}\text{C}$ $T_g = 1160^{\circ}\text{C}$



	1060 $^{\circ}\text{C}$ N_t (cm^{-3})	1160 $^{\circ}\text{C}$ N_t (cm^{-3})
$E_c - 2.38$ eV	2.4×10^{16}	1×10^{16}
$E_c - 3.39$ eV	3.6×10^{16}	5.1×10^{17}
$E_c - 4.74$ eV	1.0×10^{17}	6.6×10^{17}

$V_{\text{III-related}}$

C- or Mg-related

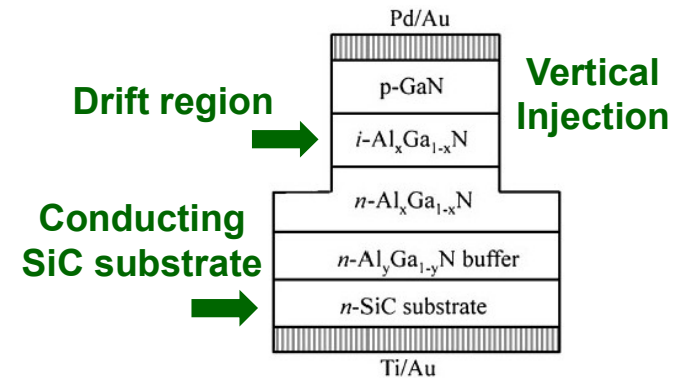
(2x TMGa flow used for HT growth)

- ➡ Si dopant compensation strongly depends on growth temperature
- ➡ Lowering T_g may inhibit the strong thermodynamic drive to form compensating point defects in UWBGs like Al-rich AlGaN

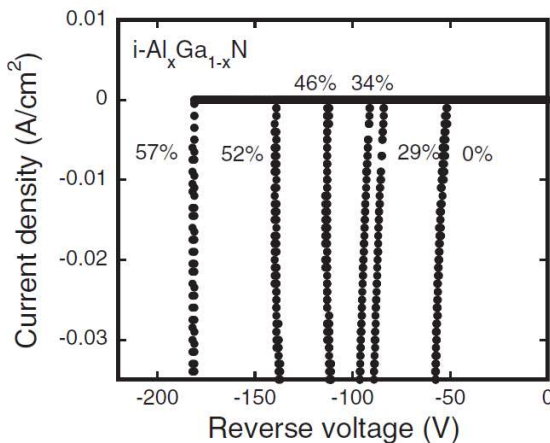
Prior AlGa_xN PIN diode results (Nishikawa, NTT, 2007)

Al_xGa_{1-x}N Vertical PN diode ($0 < X_{Al} < 0.57$)

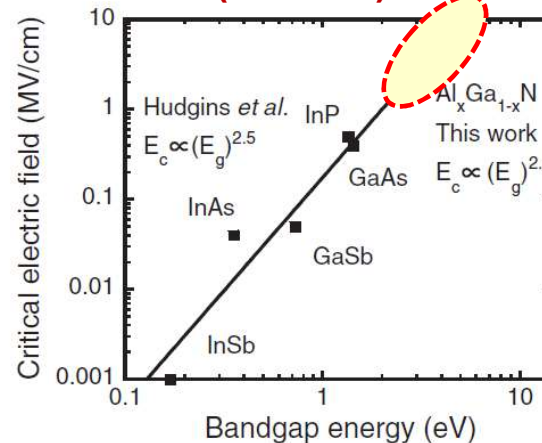
- Drift Layer: $\sim 0.2 \mu\text{m}$, $N_o \sim 2 \times 10^{16} \text{ cm}^{-3}$
- N-SiC substrates, $R_{on,sp} = 1.45 \text{ m}\Omega\text{-cm}^2$ ($X_{Al}=0.22$)



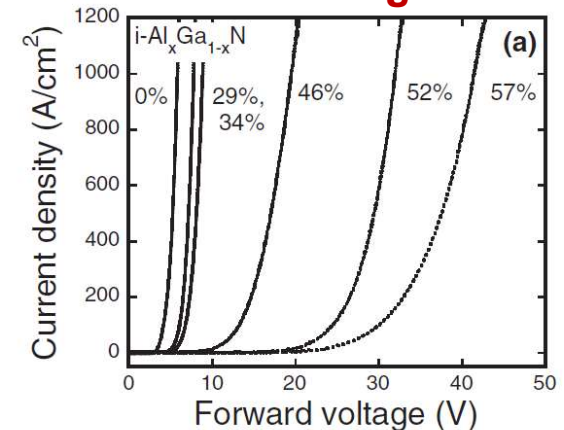
Reverse Breakdown < 200V



$E_{crit} \sim 8 \text{ MV/cm}$ (2x GaN)

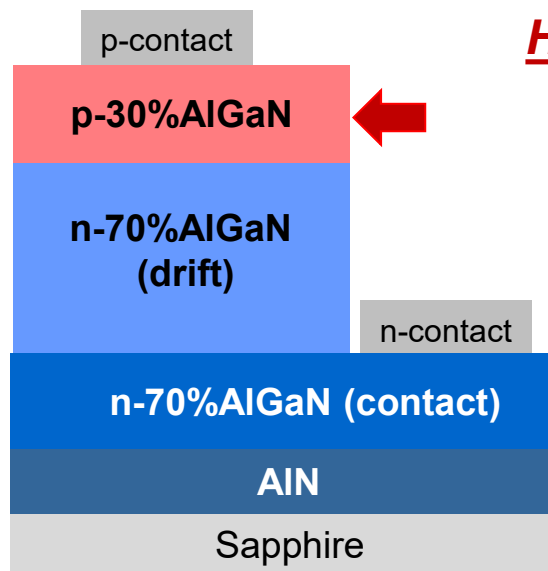


Higher forward turn-on for increasing Al



- ➔ Breakdown voltage increases with larger bandgap
- ➔ Critical electric field scales as $E_g^{2.7}$

“Quasi-vertical” heterojunction PIN in $\text{Al}_{0.70}\text{Ga}_{0.30}\text{N}$



Heterojunction PN diode (p-30% / n-70%)

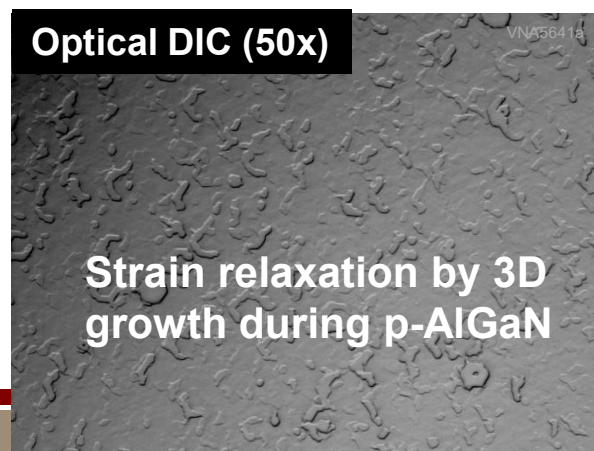
- Same p-type 30%-AlGaN used in 30%AlGaN homojunction ($\sim 0.3 \mu\text{m}$)
- Investigated different transition at pn interface
- Drift layer: $4.4 - 9.0 \mu\text{m}$ (Total: $7.1 - 15.4 \mu\text{m}$)
 ➔ No cracking!
- Drift layer doping: $1-3 \times 10^{16} \text{ cm}^{-3}$
 ➔ Suitable for V_{br} from 4 – 8 kV

Projected V_{br} (kV) for N_o , t_{drift}

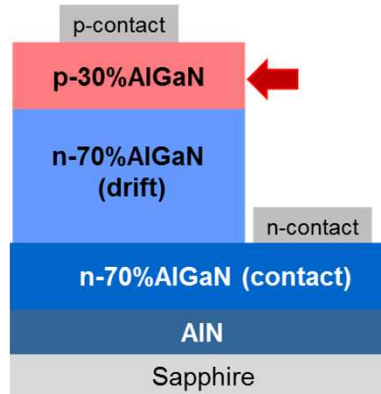
Drift (μm)	5e15	1e16	5e16
4.3	4.2	4.1	3.3
5.5	5.3	5.2	3.9
7.5	7.2	6.9	4.6
9	8.9	8.6	4.8

J. Dickerson


 $E_{crit} = 10 \text{ MV/cm}$



$\text{Al}_{0.7}\text{Ga}_{0.3}\text{N}$ “Quasi-Vertical” PN diode on sapphire



Heterojunction PN diodes (p-30% / n-70%)

- Utilize p-type doping of 30%-AlGaN
- Reverse voltage at 1 μA :

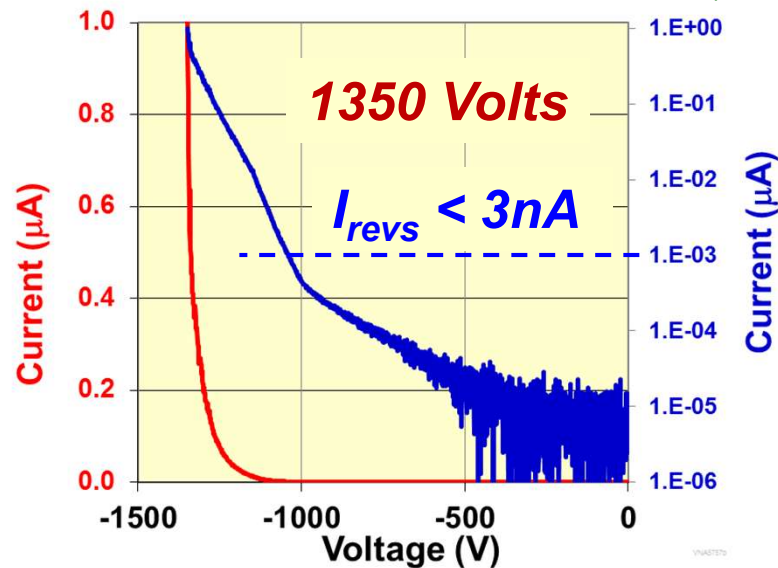
5.5 $\mu\text{m} \Rightarrow 1300\text{V}$

8.0 $\mu\text{m} \Rightarrow 1850\text{V}$

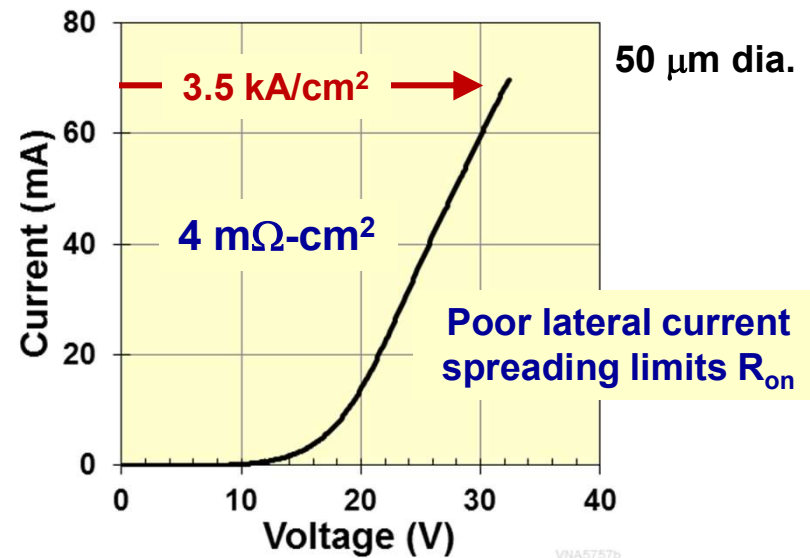
$\Rightarrow E_{\text{crit}} \sim 2.3 \text{ MV/cm}$ (very low)

Q: JTE, p-30%AlGaN or drift layer?

Reverse IV Characteristics (Drift: 5.5 μm)



Forward IV Characteristics



Homojunction $\text{Al}_{0.7}\text{Ga}_{0.3}\text{N}$ “Quasi-Vertical” PN diode

Mg - $\text{Al}_{0.70}\text{Ga}_{0.30}\text{N}$ layer designs

- Modulate [Mg] to change E field / JTE
- Compare V_{br} to heterojunction diode
- On same drift layer $5.5\text{ }\mu\text{m}$ as heterojunction diode

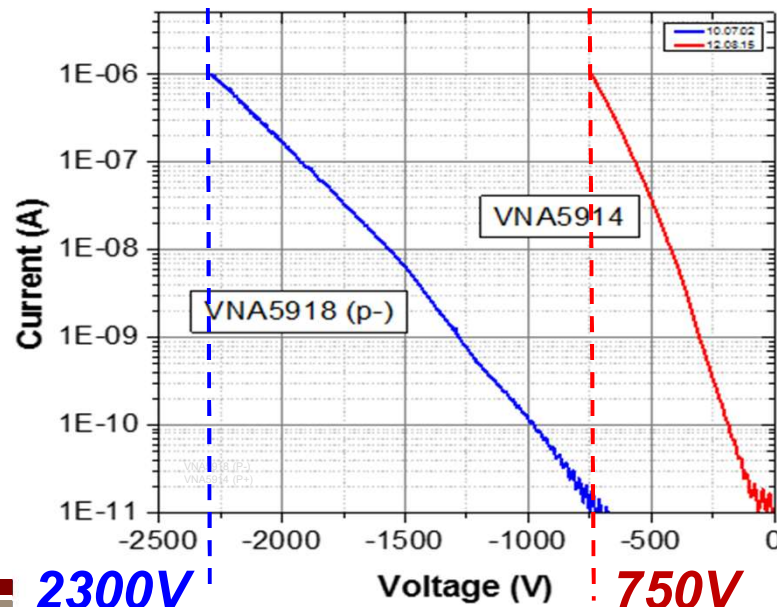
Constant Mg

P-GaN
Grade
$0.22\text{ }\mu\text{m}$, $2\text{e}19\text{ cm}^{-3}$

P-minus

P-GaN
Grade
$4\text{e}19\text{ cm}^{-3}$, $0.14\text{ }\mu\text{m}$
$4\text{e}18\text{ cm}^{-3}$, $0.08\text{ }\mu\text{m}$

Reverse IV Characteristics



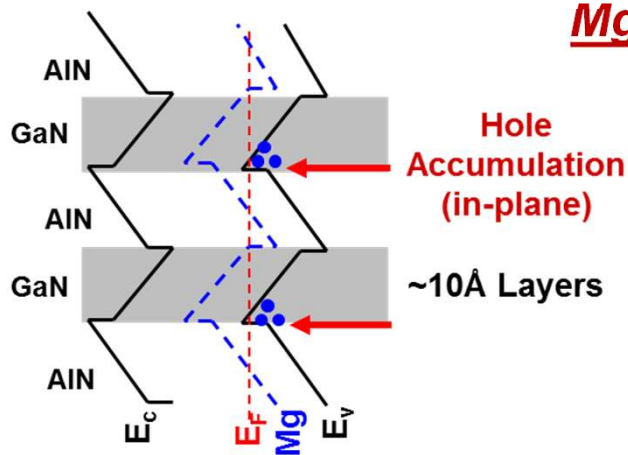
IV Characteristics

- Resistive as expected $\rightarrow V_{fwd} \sim 130\text{V}$ @ $1\text{ }\mu\text{A}$
- Reverse voltage much higher for P-minus (2300V) vs. Constant Mg (750V)
- *Drift layer ($5.5\text{ }\mu\text{m}$) can support 2.3kV*

- $\Rightarrow$ Reverse voltage (1.3kV) in HJ diode is JTE or p-side limited
- $\Rightarrow$ Example of importance of controlling electric fields.

Approaches for hole transport in $\text{Al}_{0.7}\text{Ga}_{0.3}\text{N}$ PN diodes

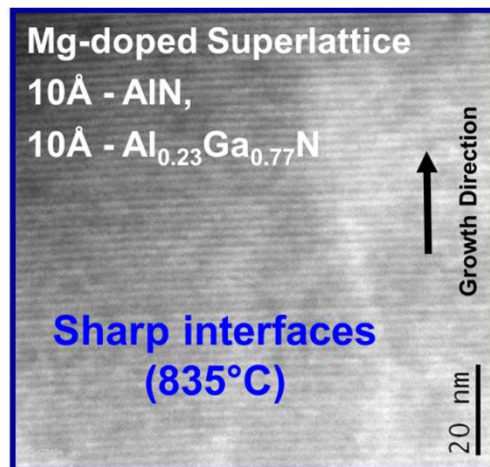
Allerman, JCG 2010



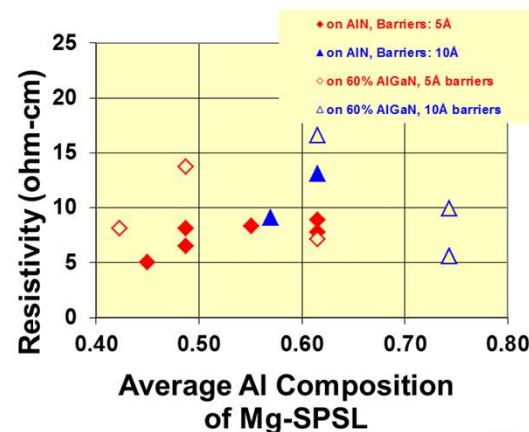
Mg-doped short-period superlattice (Mg-SPSL)

- Strong polarization fields ionized Mg dopants
- Adjust average composition with layer thickness, X_{Al}
- Low in-plane resistivity (5-10 $\Omega\text{-cm}$)
- Heterojunctions increase V_{forward} (vertical transport)

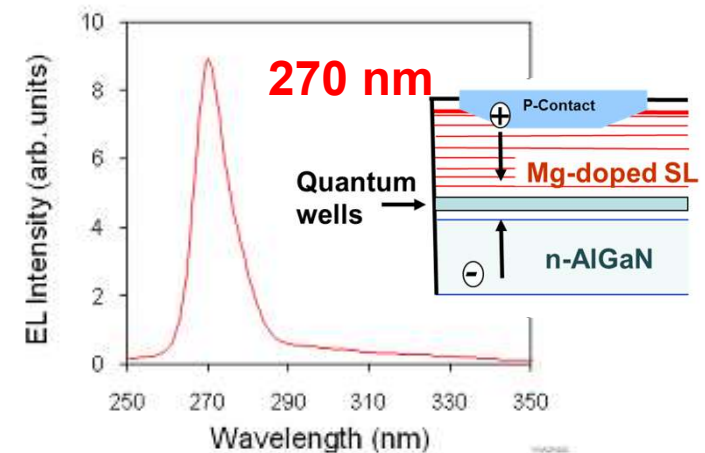
TEM



P-type Resistivity of Mg-SPSL

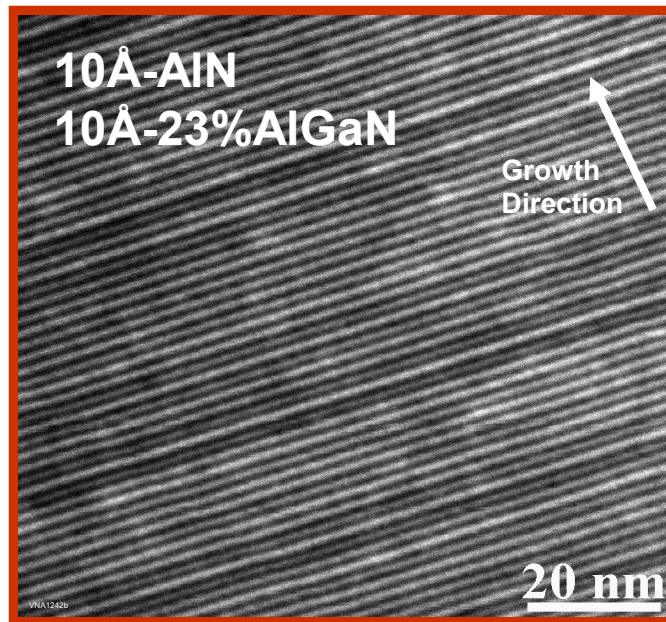


Electroluminescence from p-SPSL LED

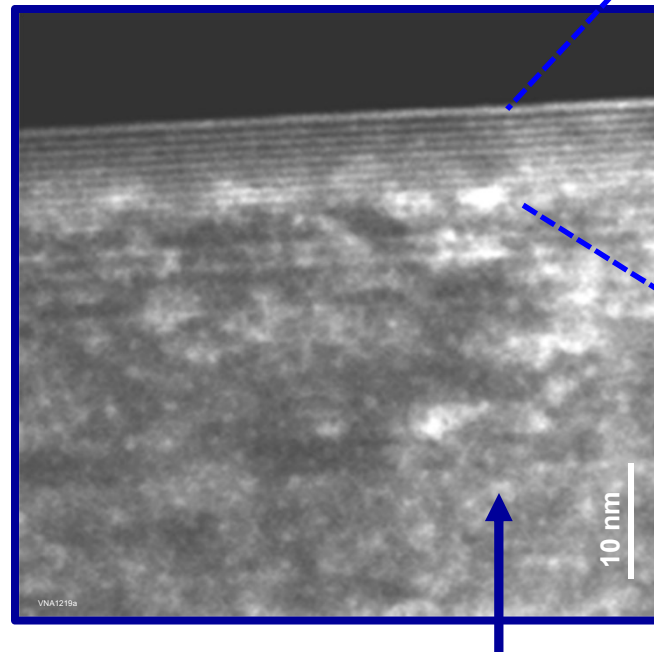


Approaches for hole transport in $\text{Al}_{0.7}\text{Ga}_{0.3}\text{N}$ PN diodes

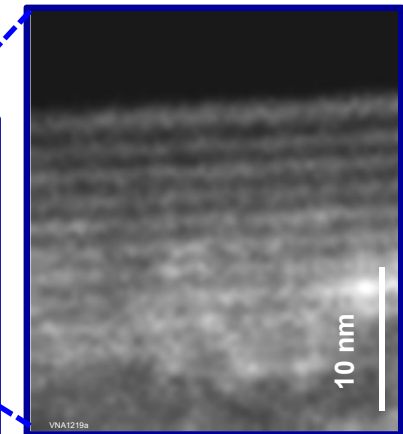
Growth Temperature ~ 980-1000°C



Undoped: Well resolved layers

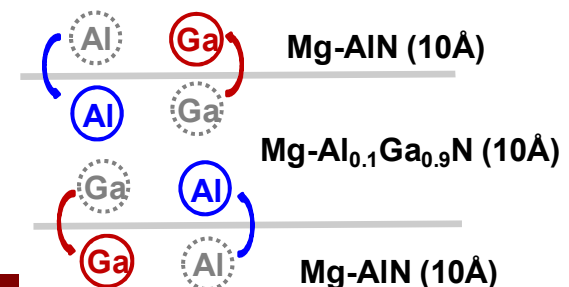


Mg-Doped: Intermixed layers



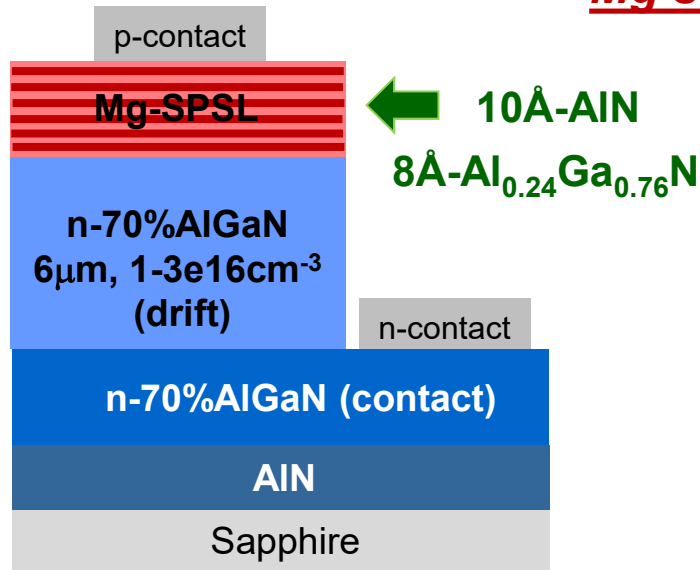
8-10 periods
resolved at top

- ➔ Not intermixing at growth surface
- ➔ Al, Ga diffusion process due to Mg doping



“Quasi-vertical” Mg-doped short-period superlattice PN diode

Mg short-period superlattice (Mg-SPSL) PN diode

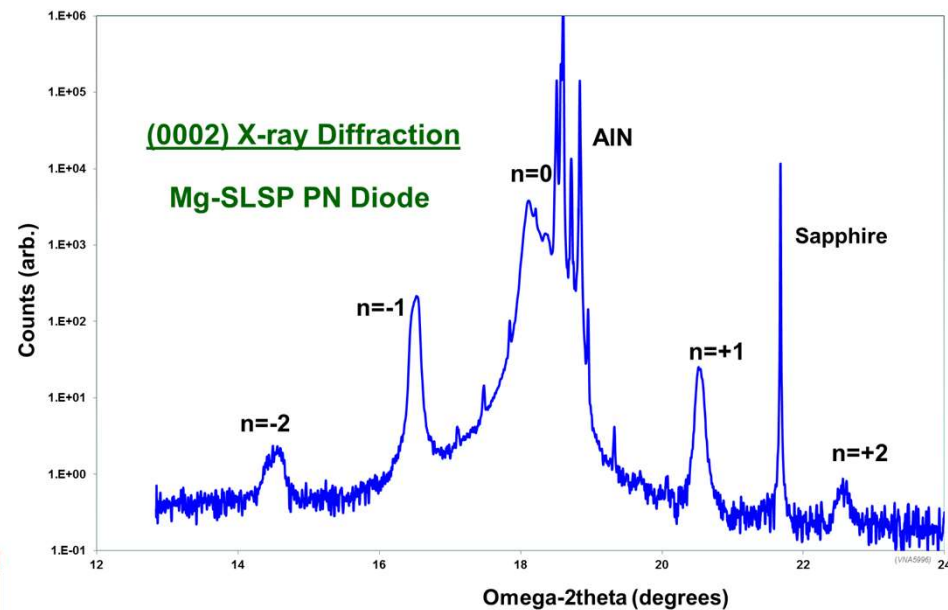


- P-type resistivity: 7-10 Ω -cm
- [Mg] $\sim$ 3-4 e19 cm⁻³
- Thickness: 0.3 μ m (160x)
- Average Xal: 0.66
- Period by XRD: 22.1Å

➔ **Growth temperature: 835 °C**

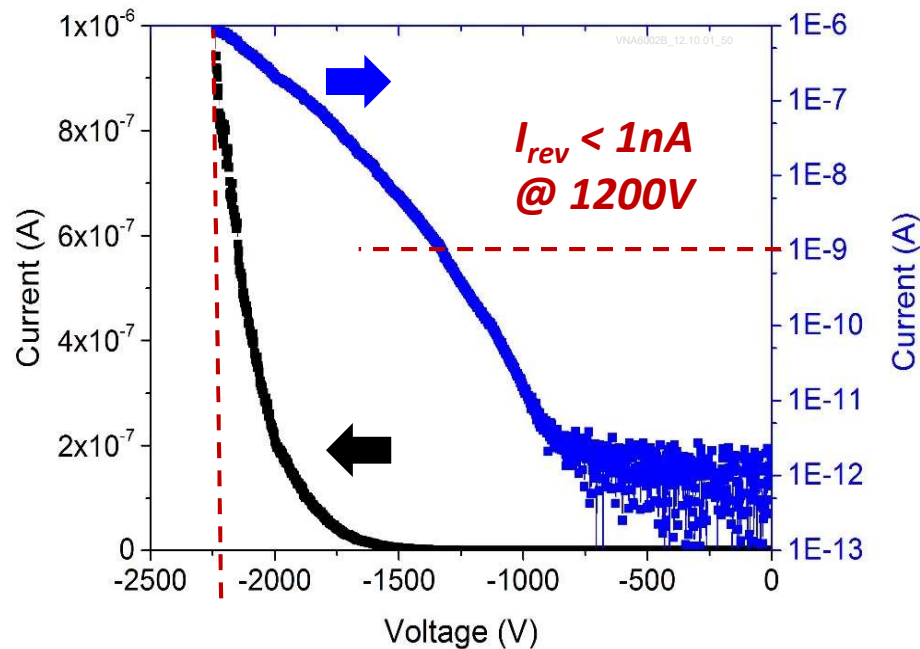
➔ **Mg-SPSL is reproducible**

Date	Period (Å)	Resistivity (Ω -cm)
11/2012	19.2	11.5
2/2013	20.7	6.9
3/2014	21.7	10.4
4/2017	19.8	7.1



“Quasi-vertical” Mg-doped short-period superlattice PN diode

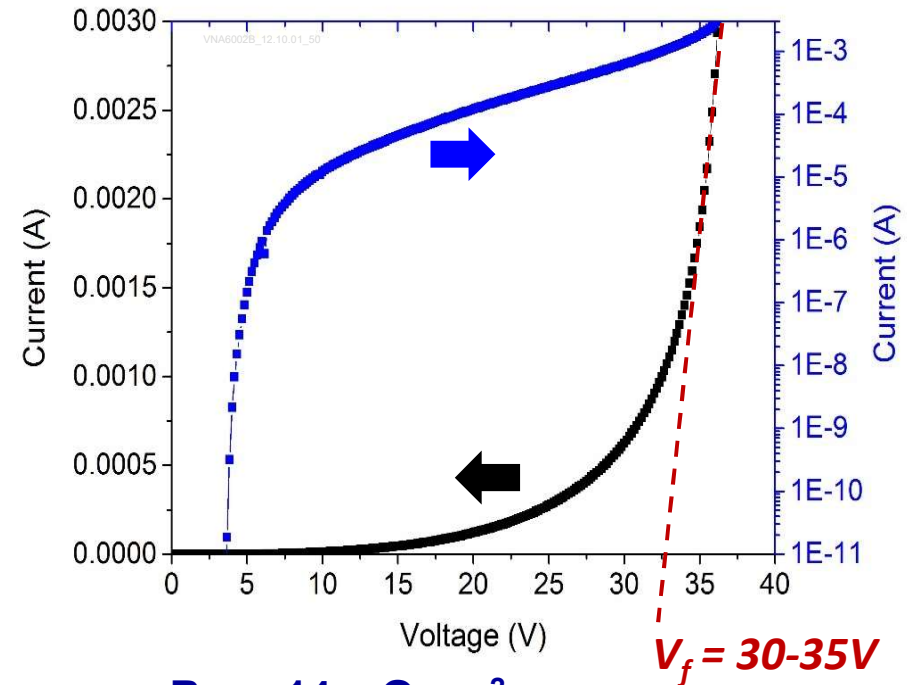
Reverse IV Characteristics



- Breakdown $\sim -2200 \text{ V}$ (@ $1 \mu\text{A}$)

$E_{crit} \sim 3.7 \text{ MV/cm}$

Forward IV Characteristics



- $R_{on} \sim 14 \text{ m}\Omega\text{-cm}^2$
- High forward voltage $\sim 30-35 \text{ V}$

- ➔ Lower forward voltage by adjusting heterobarrier in Mg-SPSL
- ➔ Increase breakdown by optimizing JTE

Summary

- **Quasi-vertical $\text{Al}_x\text{Ga}_{0-x}\text{N}$ PIN diodes ($X_{\text{al}}=0.3$)**
 - Breakdown voltage > 3000V with n-type drift layer of 11 μm
 - Measured a critical electric field of 5.9 MV/cm² for 30%AlGaN
- **Quasi-vertical $\text{Al}_x\text{Ga}_{0-x}\text{N}$ PIN diodes ($X_{\text{al}}=0.7$)**
 - Compensation in drift layer is similar to n-GaN ($\sim 1\text{e}16\text{ cm}^{-3}$)
 - Heterojunction diode (p-30% / n-70%):
 - $V_{\text{br}} \sim 1350\text{V}$, $V_{\text{f}} = 7\text{-}10\text{V}$, problem with JTE & low X_{al} p-layer
 - Mg-short period superlattice:
 - $V_{\text{br}} \sim 2200\text{V}$, V_{f} is higher 30-35V