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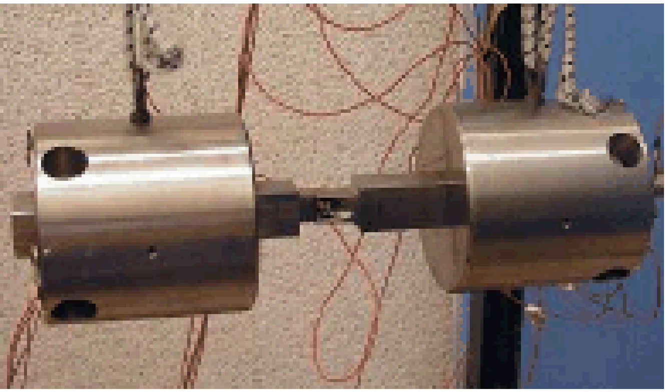
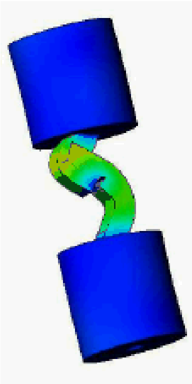
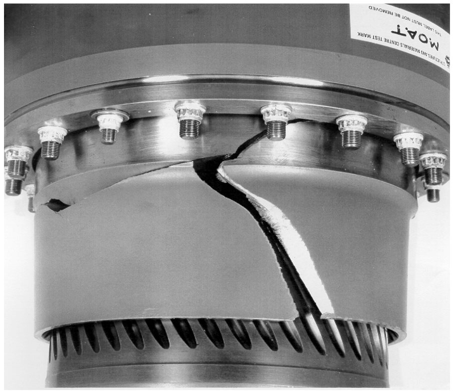
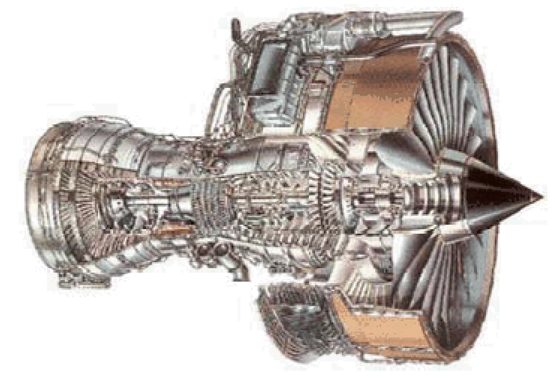

Project 6: Acoustoelasticity Measurements and Modifications

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Mentors: Ryan Schultz (SNL), Matt Brake (Rice), and Micah Shepherd (Penn St.)

U.S. DEPARTMENT OF ENERGY

NNSA National Nuclear Security Administration

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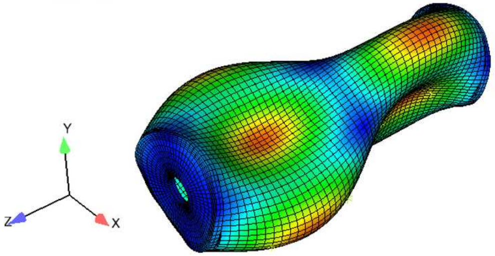
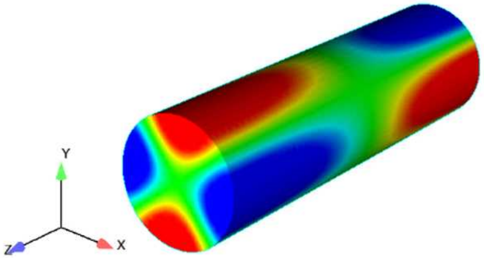
Acoustoelasticity studies the coupling between structural and acoustic modes

- Acoustoelasticity is a subset of the field of structural acoustics
- Structures and acoustics are coupled through the velocity at the interface surface
- Structures and fluids propagate sound waves that form standing waves with specific patterns (mode shapes) at specific frequencies (resonance)

Structural mode shape



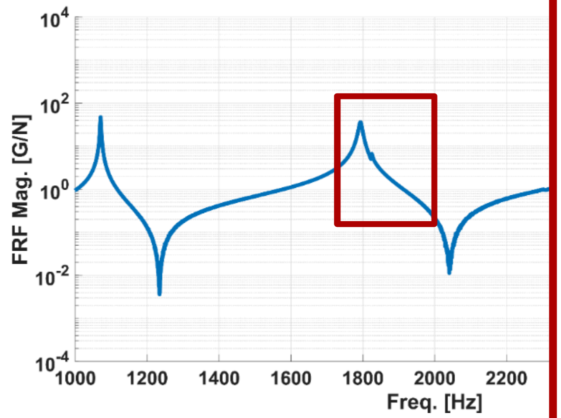
Acoustic mode shape

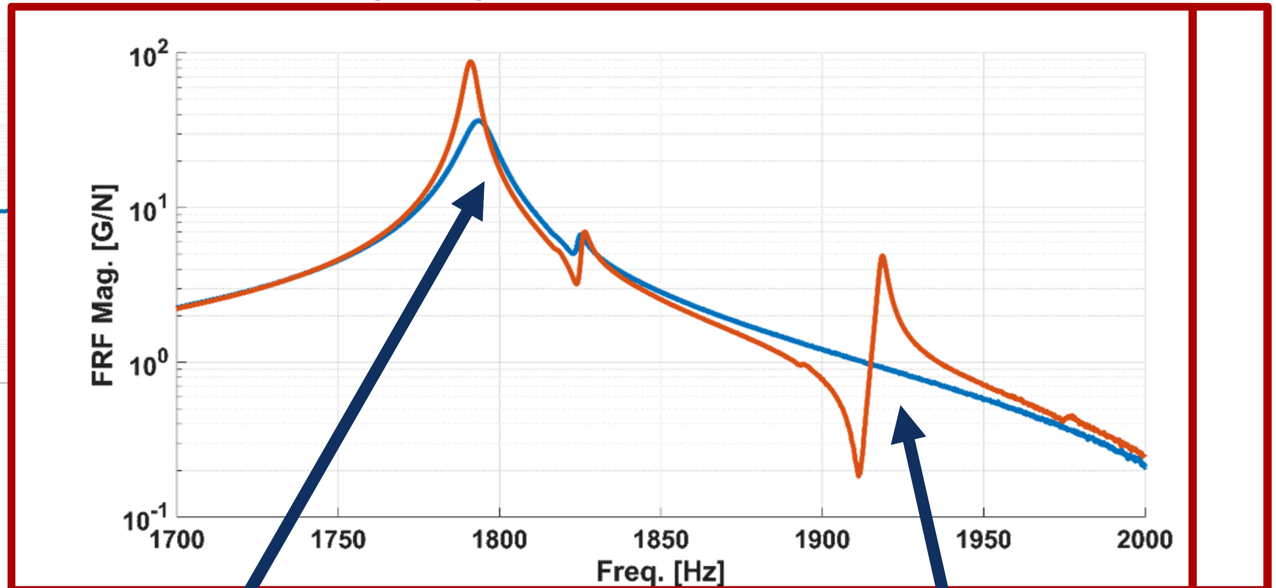


Acoustoelastic Coupling!

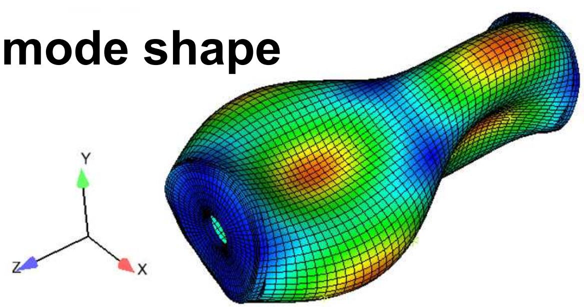
Acoustoelastic coupling generates unexpected peaks in the frequency response

Structural Frequency Response Function (FRF)

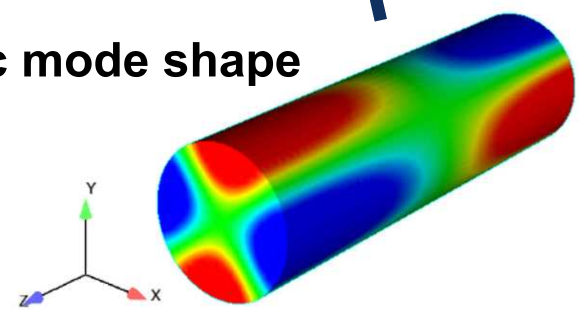




Structural mode shape

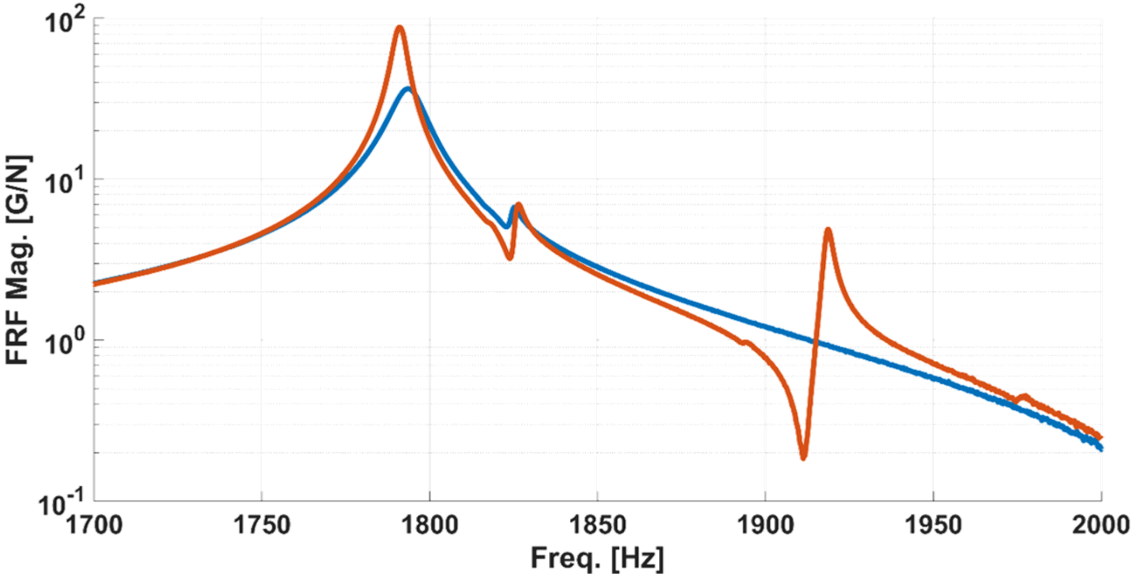


Acoustic mode shape



Presence of coupling causes difficulty in validating analytical models (e.g., finite element)

- One of the main goals of modal testing is to supply experimental data for analytical model correlation
- Finite element models typically assume zero interaction with the surrounding air (in-vacuo, structure-only state)
- Running coupled analyses increase model complexity and computational expense



How can we approach this problem from the experimental side?

We seek to develop methods to…

- Quickly identify when acoustic coupling occurs
- Decouple the structural response by altering boundary conditions of:
  - Acoustic volume
  - Structure

ACOUSTOELASTICITY THEORY

Coupling occurs when mode shapes are similar and frequencies are close in proximity

Modal Equations of Motion:

Structural:

$$M_m \ddot{q}_m + C_m \dot{q}_m + K_m q_m = \rho_0 c_0^{\,2} A_F \sum_n \frac{P_n L_{nm}}{M_n^A} + Q_m^E$$

Acoustic:

$$\ddot{P}_n + (\omega_n^A)^2 P_n = -\frac{A_F}{V} \sum_m L_{mn} \ddot{q}_m$$

Acoustoelastic coupling terms

Coupling coefficient measures the degree of similarity between mode shapes

$$L_{nm} = \frac{1}{A_F} \int_{A_F} \psi_n \phi_m \, dA$$

ψ_n : Acoustic shape

ϕ_m : Structural shape

For excitation at the structural resonance frequency, the acoustic modal amplitude is:

$$\overline{P}_n = \frac{A_F}{V} \frac{(\omega_m^s)^2 L_{nm}}{(\omega_n^A)^2 - (\omega_m^S)^2} \overline{q}_m$$

Minimized when

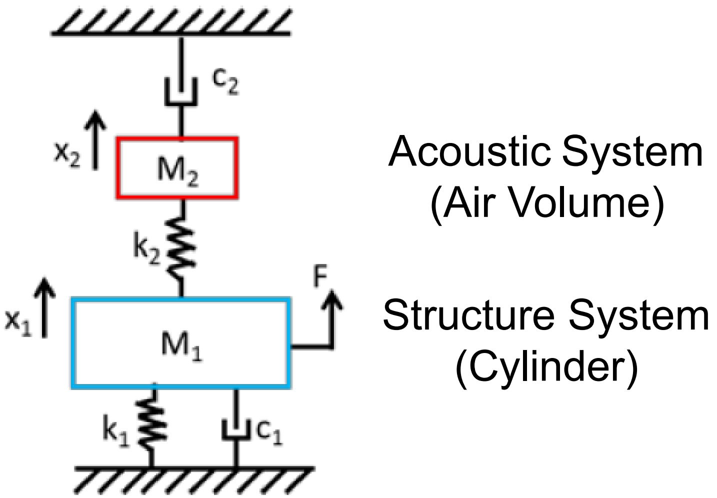
L_{nm} small

$(\omega_n^A)^2 - (\omega_m^S)^2$ large

[1] Dowell E.H. et al. (1977) "Acoustoelasticity: General Theory, Acoustic Natural Modes and Forced Response to Sinusoidal Excitation, Including Comparison with Experiment," Journal of Sound and Vibration, **52**(4), 519-542.

A system with acoustoelastic coupling behaves similar to a tuned mass damper

Tuned mass damper



Reproduced from [2]

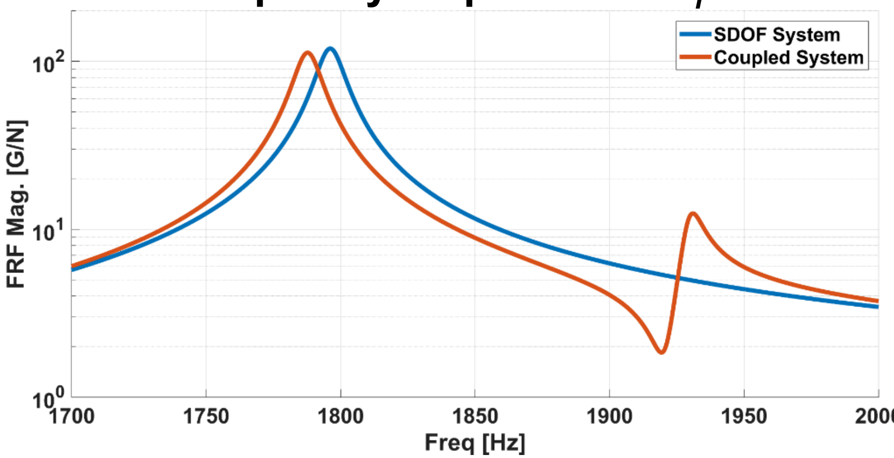
Frequencies

$$f_{1,2} = \frac{1}{2^{3/2}\pi}\left(\frac{k_1+k_2}{M_1}+\frac{k_2}{M_2} \mp \left[\left(\frac{k_1+k_2}{M_1}+\frac{k_2}{M_2}\right)^2 - 4\frac{k_1 k_2}{M_1 M_2}\right]^{1/2}\right)^{1/2}$$

Mode Shapes

$$\begin{Bmatrix} X_1 \\ X_2 \end{Bmatrix}^{(i)} = \begin{Bmatrix} 1 + \dfrac{k_1}{k_2} - \dfrac{\frac{1}{M_1}(2\pi f_i)}{k_2} \end{Bmatrix}$$

Frequency response of M_1



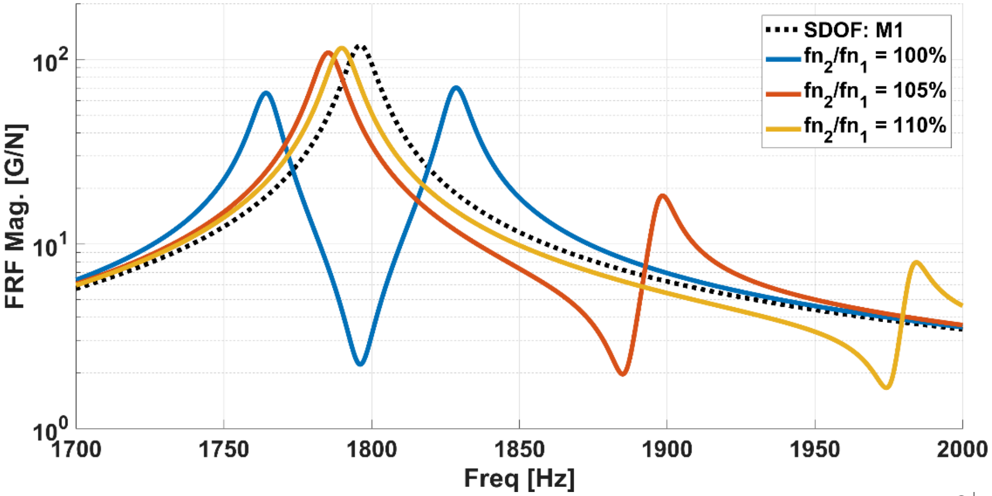
Parameters:

- M_1: structural mass
- M_2: air mass
- k_1: structural stiffness
- k_2: air stiffness
- c_1: structural damping
- c_2: air damping

[2] Schultz R., Pacini B. (2017) "Mitigation of Structural-Acoustic Mode Coupling in a Modal Test of a Hollow Structure," Conference Proceedings of the Society for Experimental Mechanics Series,

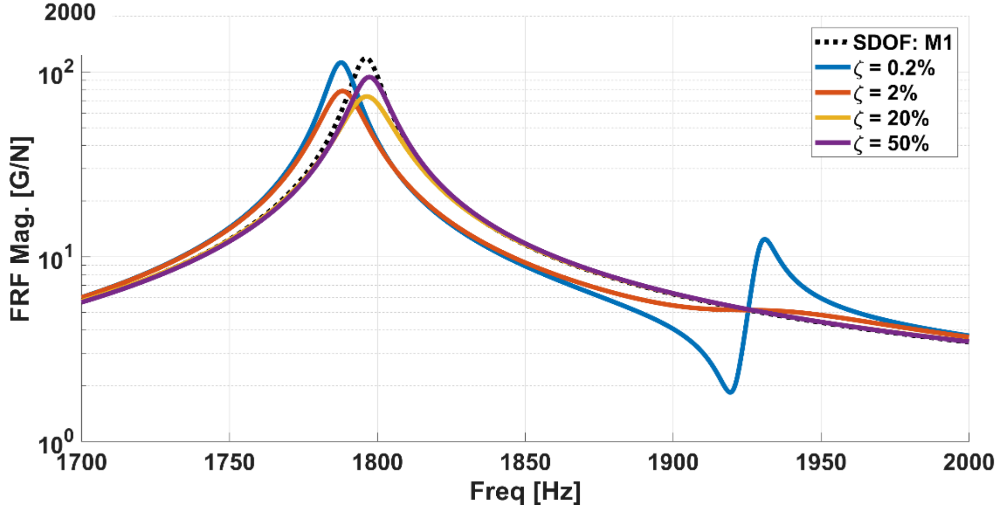
Adjusting air properties can decouple the structural system

Vary air “stiffness” k_2



Increasing air stiffness causes the coupled acoustic frequency to shift away from structural frequency

Vary air damping c_2



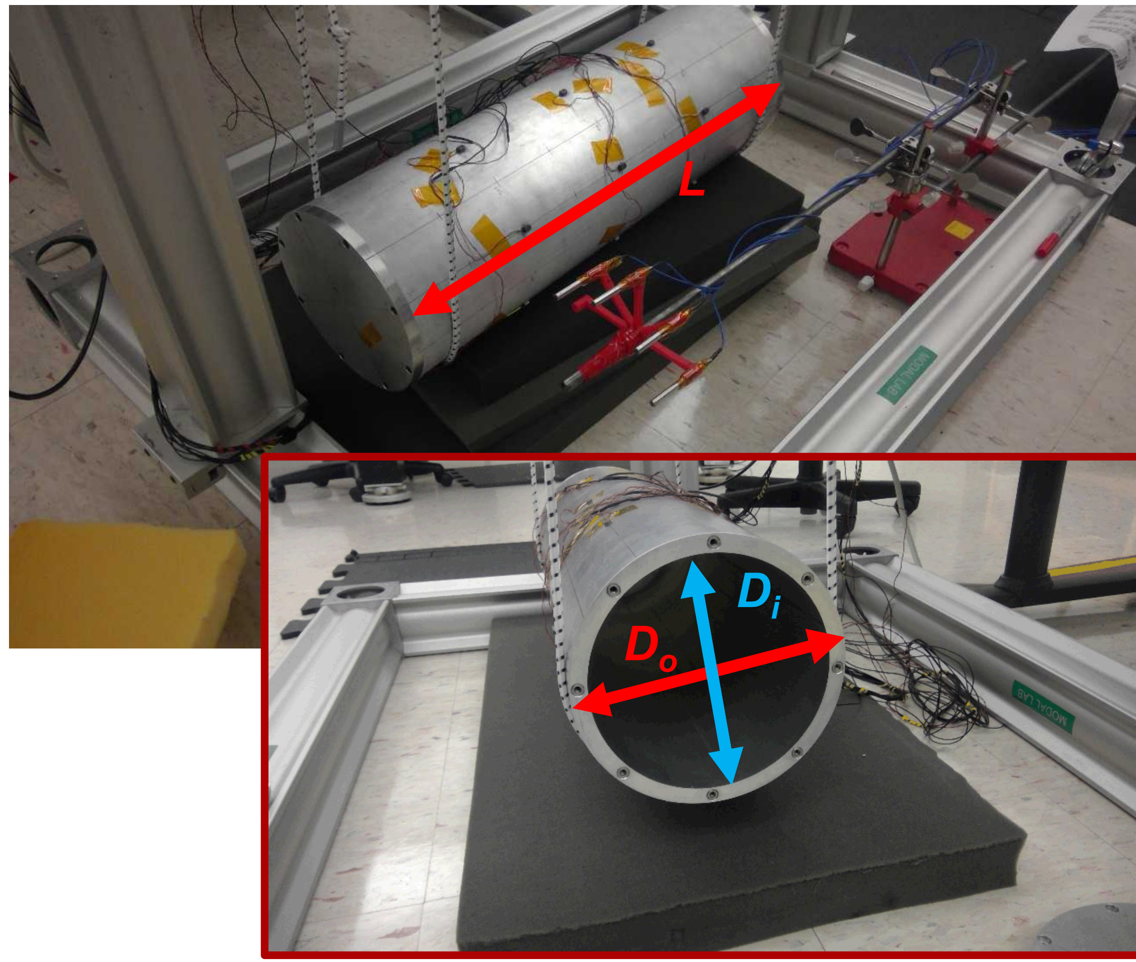
Increasing air damping causes the structural response to first decrease, then increase towards SDOF response

[2] Schultz R., Pacini B. (2017) “Mitigation of Structural-Acoustic Mode Coupling in a Modal Test of a Hollow Structure,” Conference Proceedings of the Society for Experimental Mechanics Series,

HARDWARE AND TEST SETUP

A hollow aluminum cylinder provided a test article that exhibits acoustoelastic coupling

Cylinder suspended from soft bungee cords



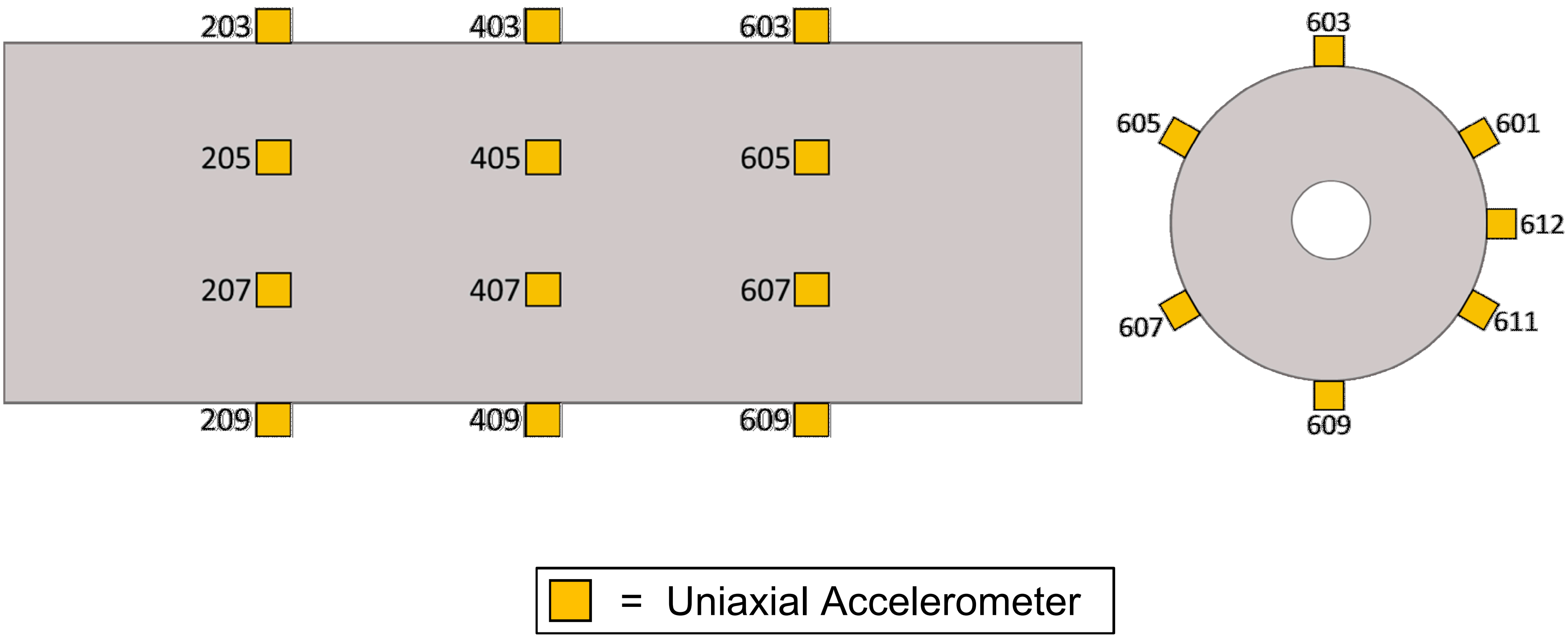
Cylinder dimensions:
Length L: 24 in.
Inner diameter, D_i = 7 in.
Outer diameter, D_o = 8 in.
Wall thickness, t = ½ in.

Measurements:
Accelerometers bonded to surface measure the structural response

Microphones located on rod measure the acoustic pressure

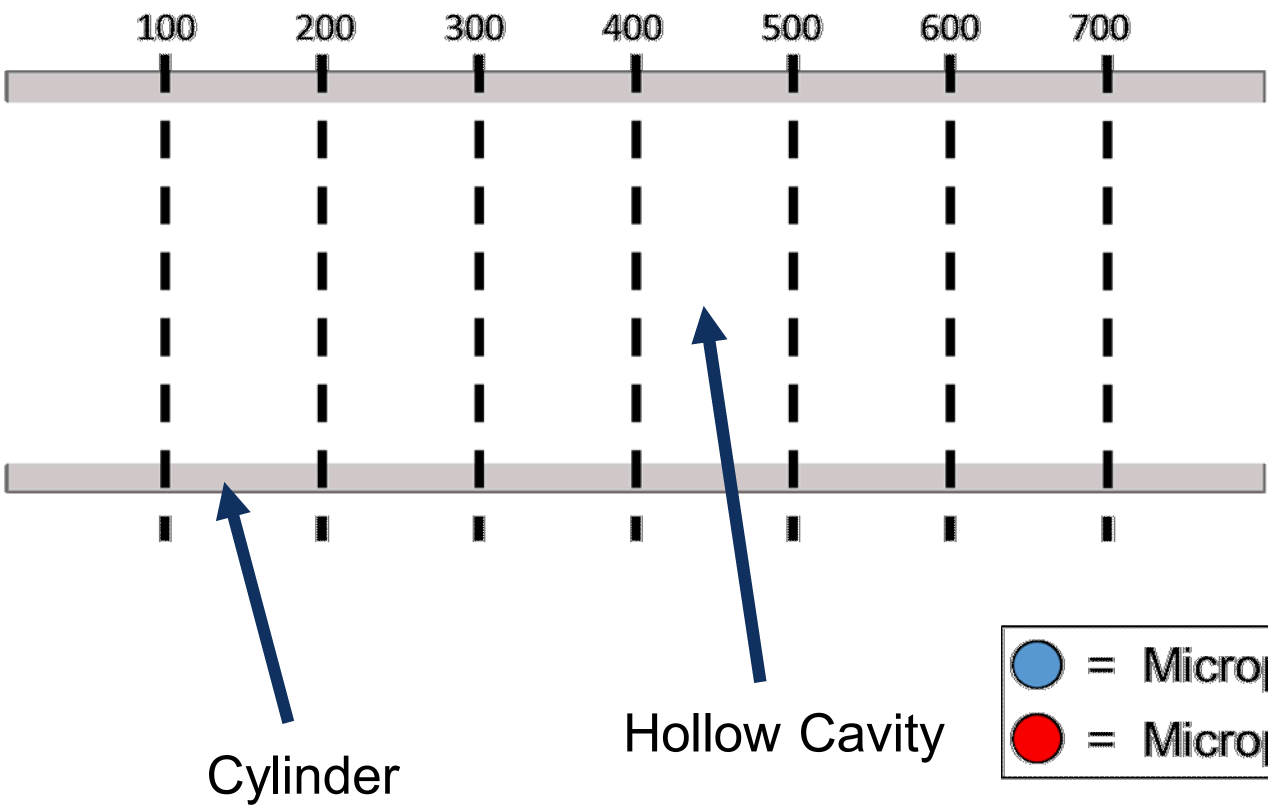
Accelerometers located to adequately capture the structural modes of interest

Axial Locations **Circumferential Locations**

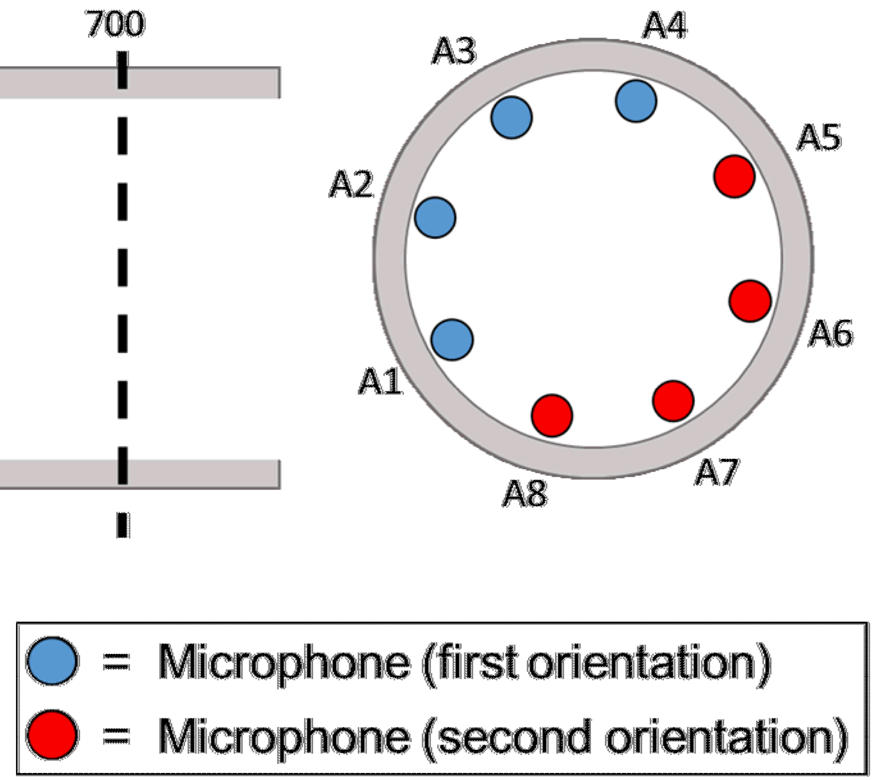


Roving microphone array used to adequately capture acoustic modes of interest

Axial Locations



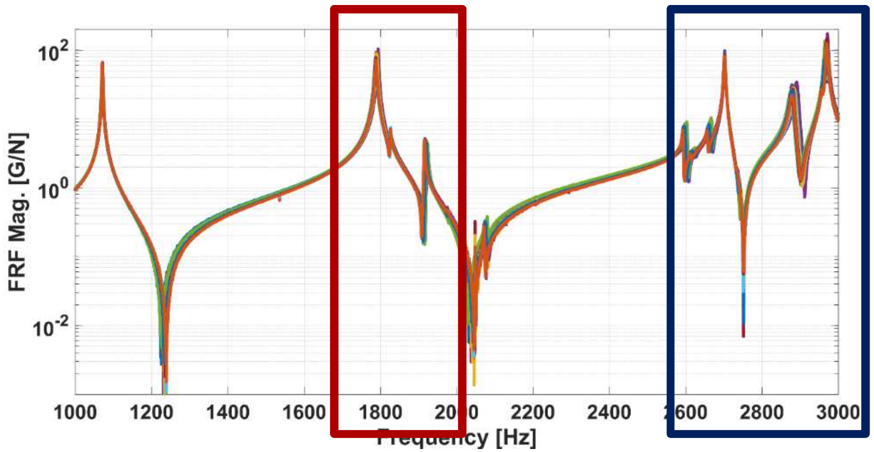
Circumferential Locations



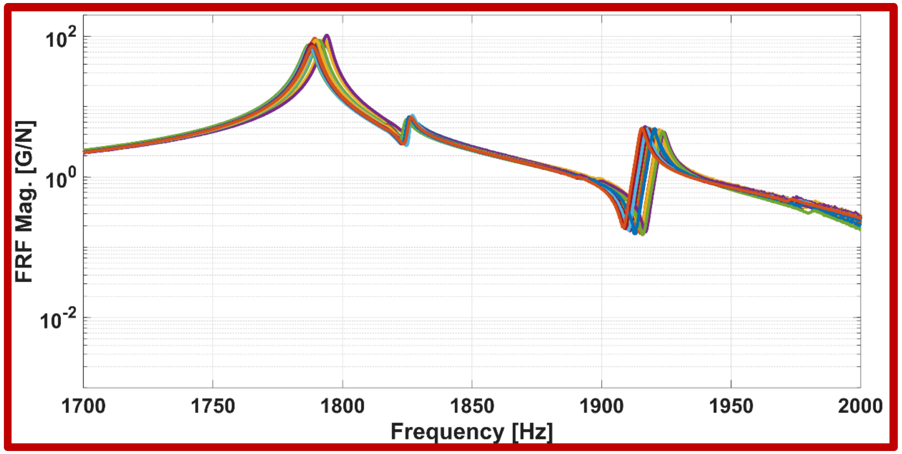
REPEATABILITY TESTING

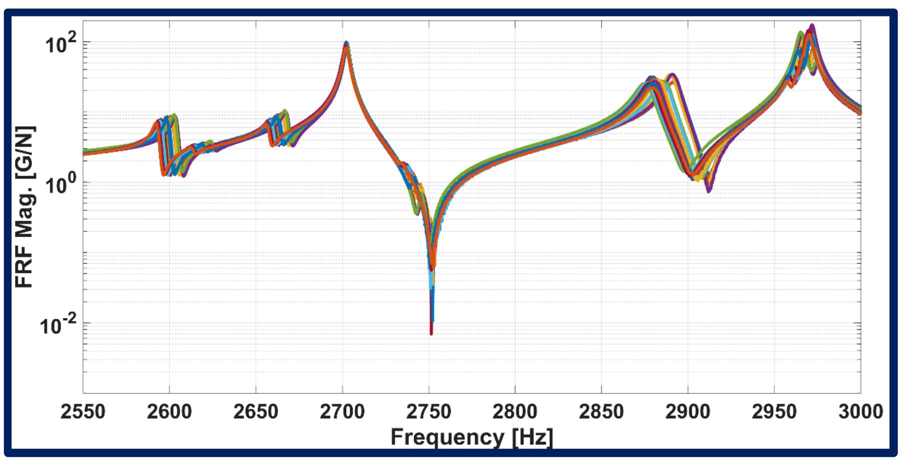
Baseline tests from different days / times altered the system frequency response

FRF variations at various points in time



Zoomed FRF



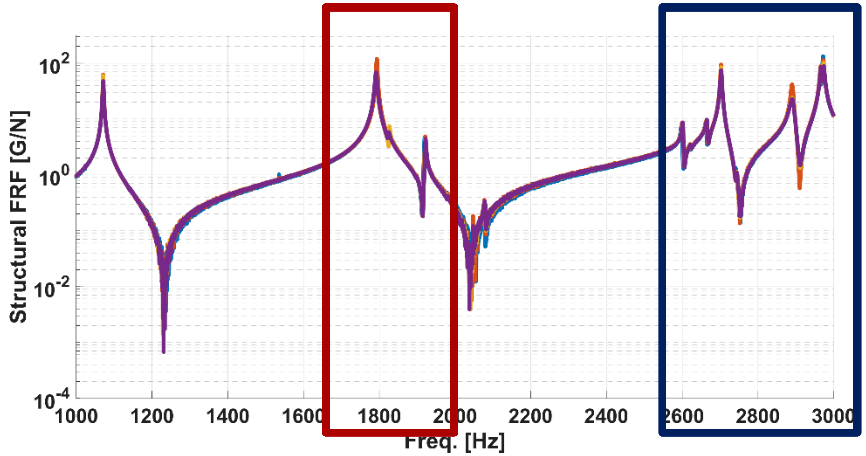


Identified causes include:

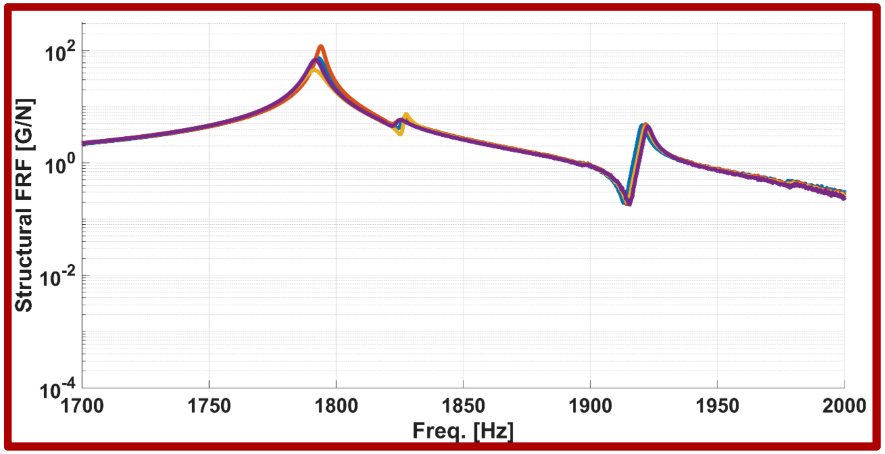
- Bungee chord tension / location
- Cylinder end cap removal / reattachment
- Variations in air properties

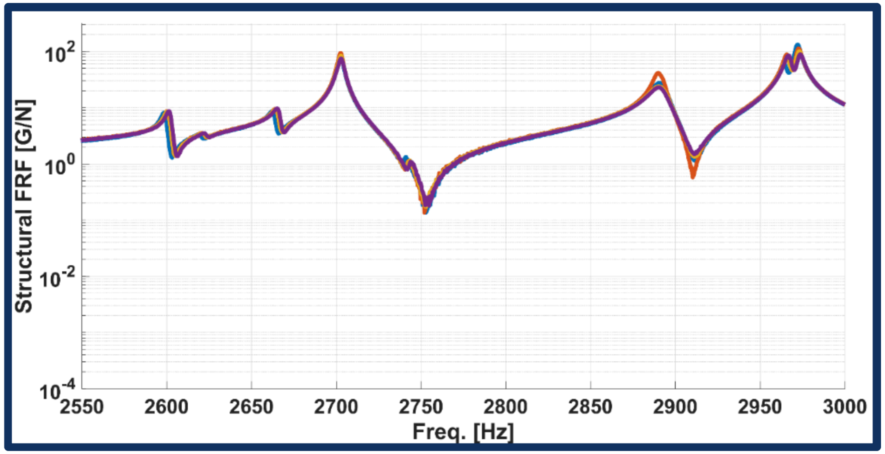
Bungee lengths and connection locations alter amplitudes and shift frequencies

FRF variations due to bungee variations



Zoomed FRF

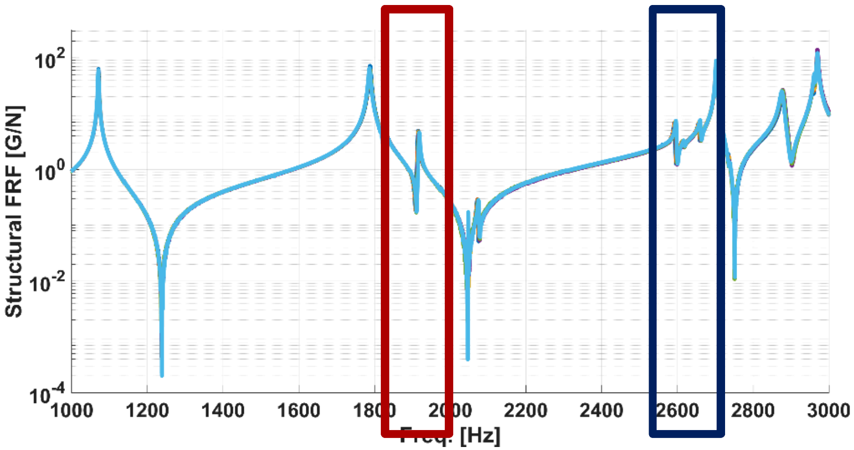


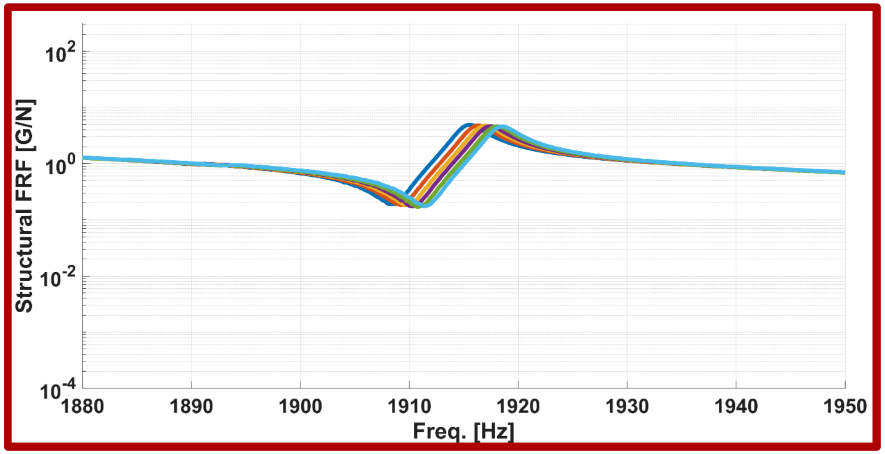


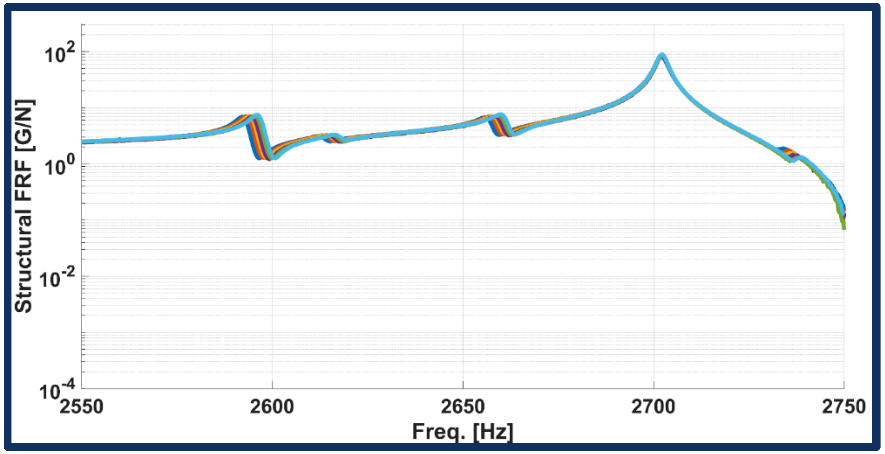
Cylinder end cap removal / reattachment shifts coupled acoustic frequencies

Zoomed FRF

FRF variations due to end cap handling

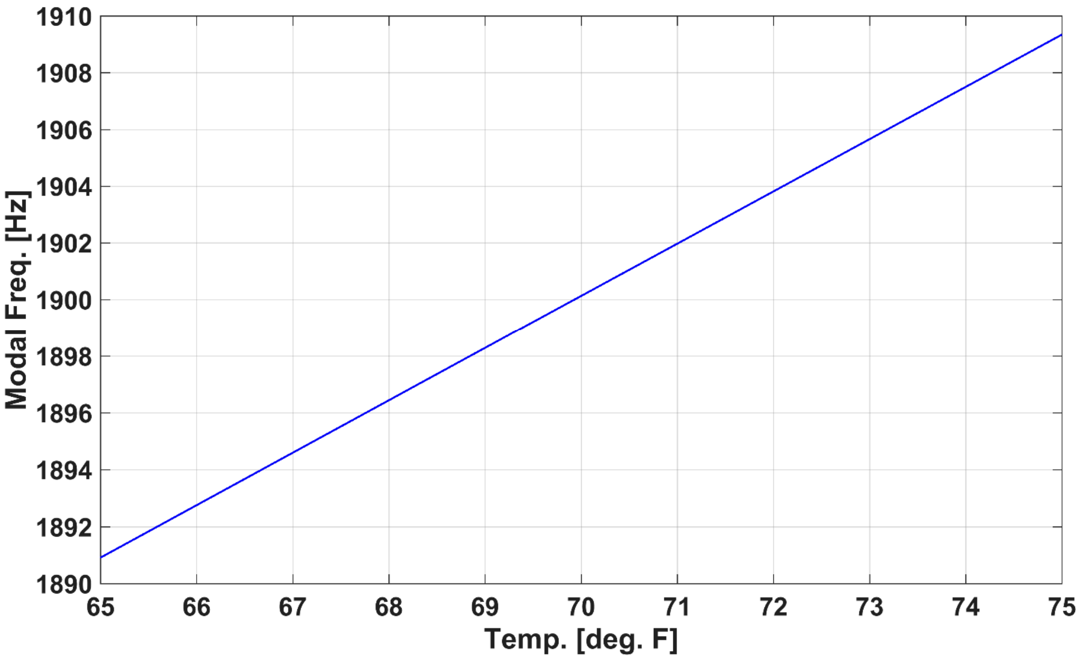




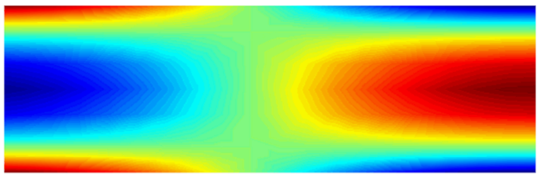


Small temperature changes can shift acoustic mode frequencies significantly

Temperature effects on acoustic (2,1,1) modal frequency



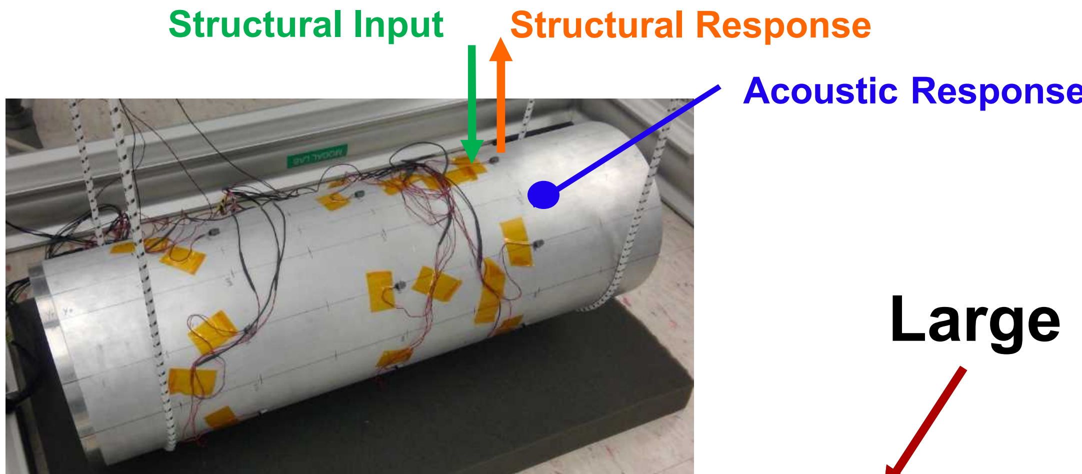
Acoustic (2,1,1) mode shape



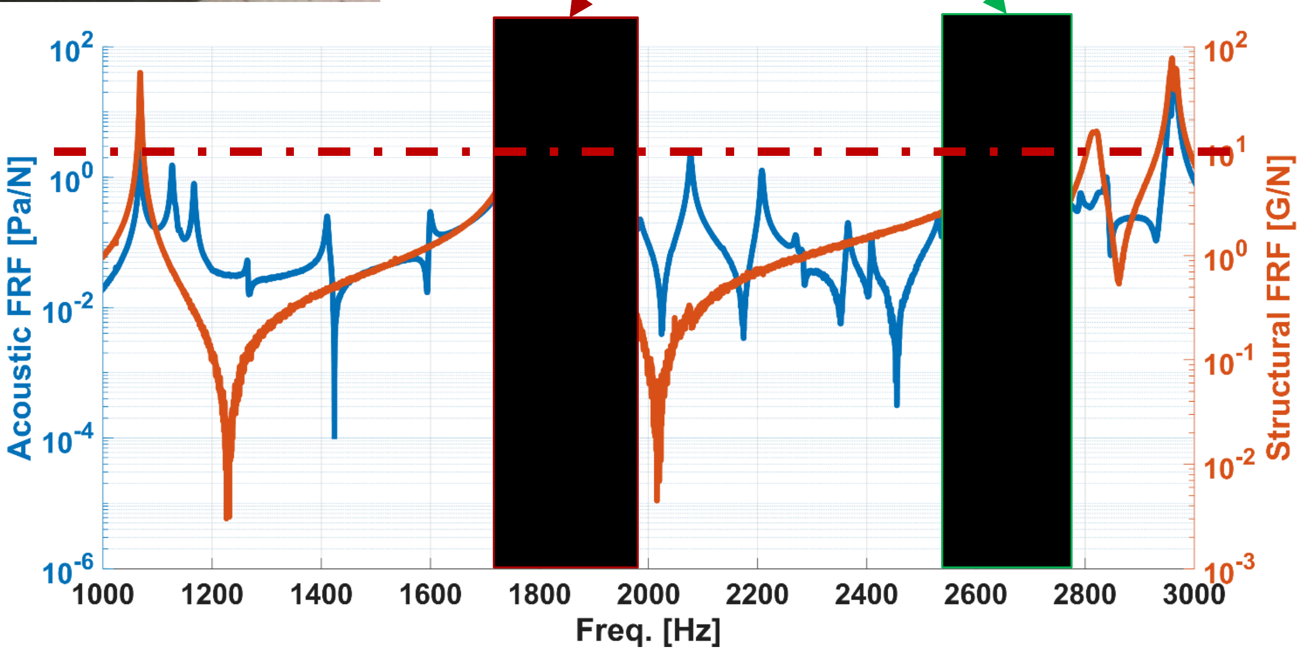
- In a similar manner, static pressure fluctuations can also induce frequency shifts

COUPLING IDENTIFICATION AND MEASUREMENT

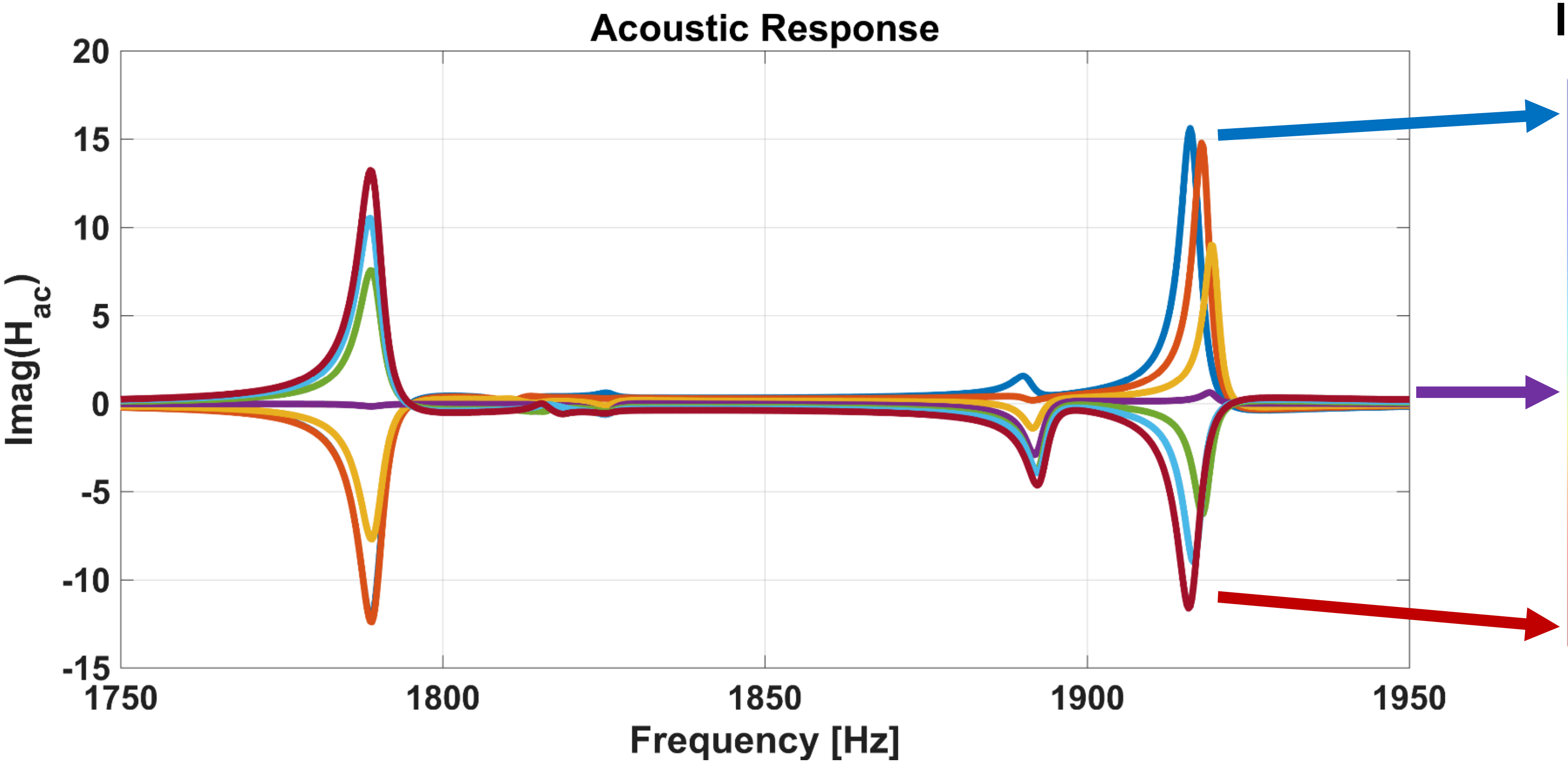
Acoustic response is an order of magnitude larger where coupling exists

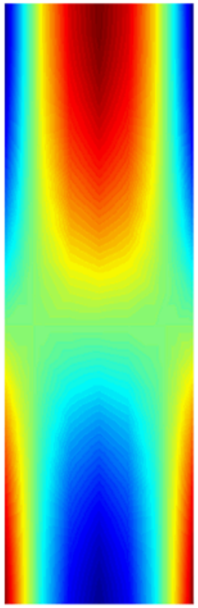


Large coupling



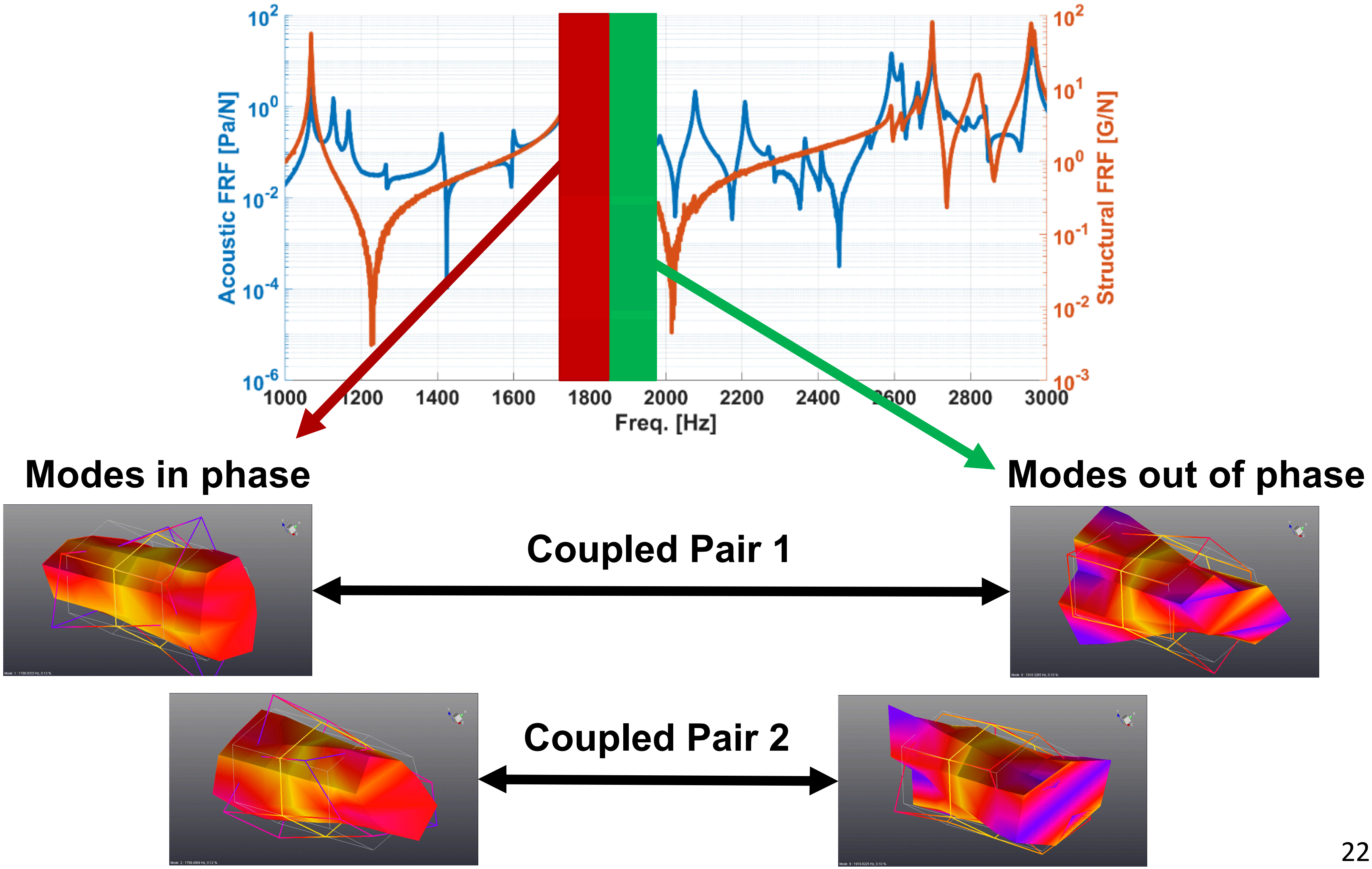
Location of microphones shows appreciable effect on the coupled frequency

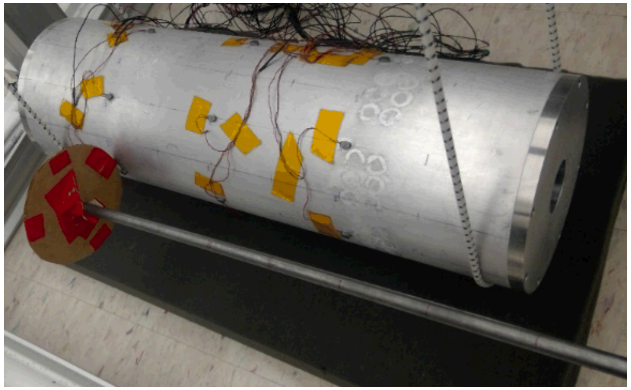
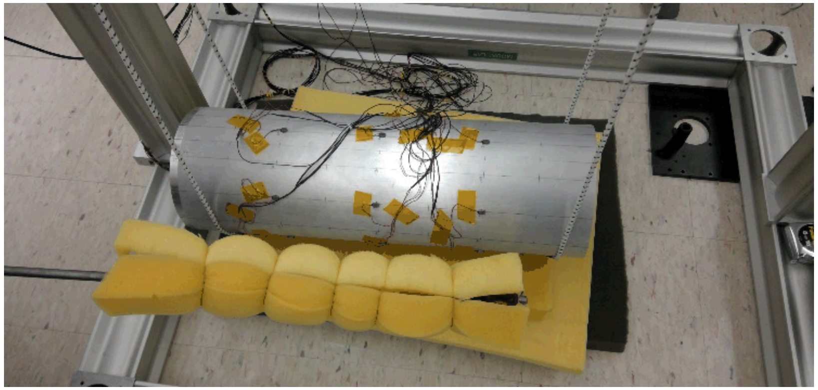
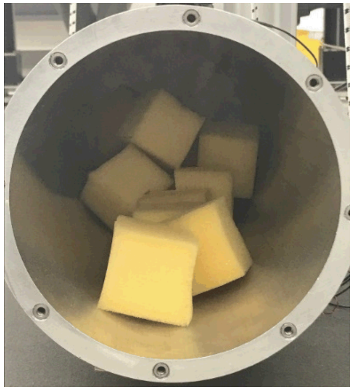




Requires acoustic modal parameters to be extracted at each microphone location!

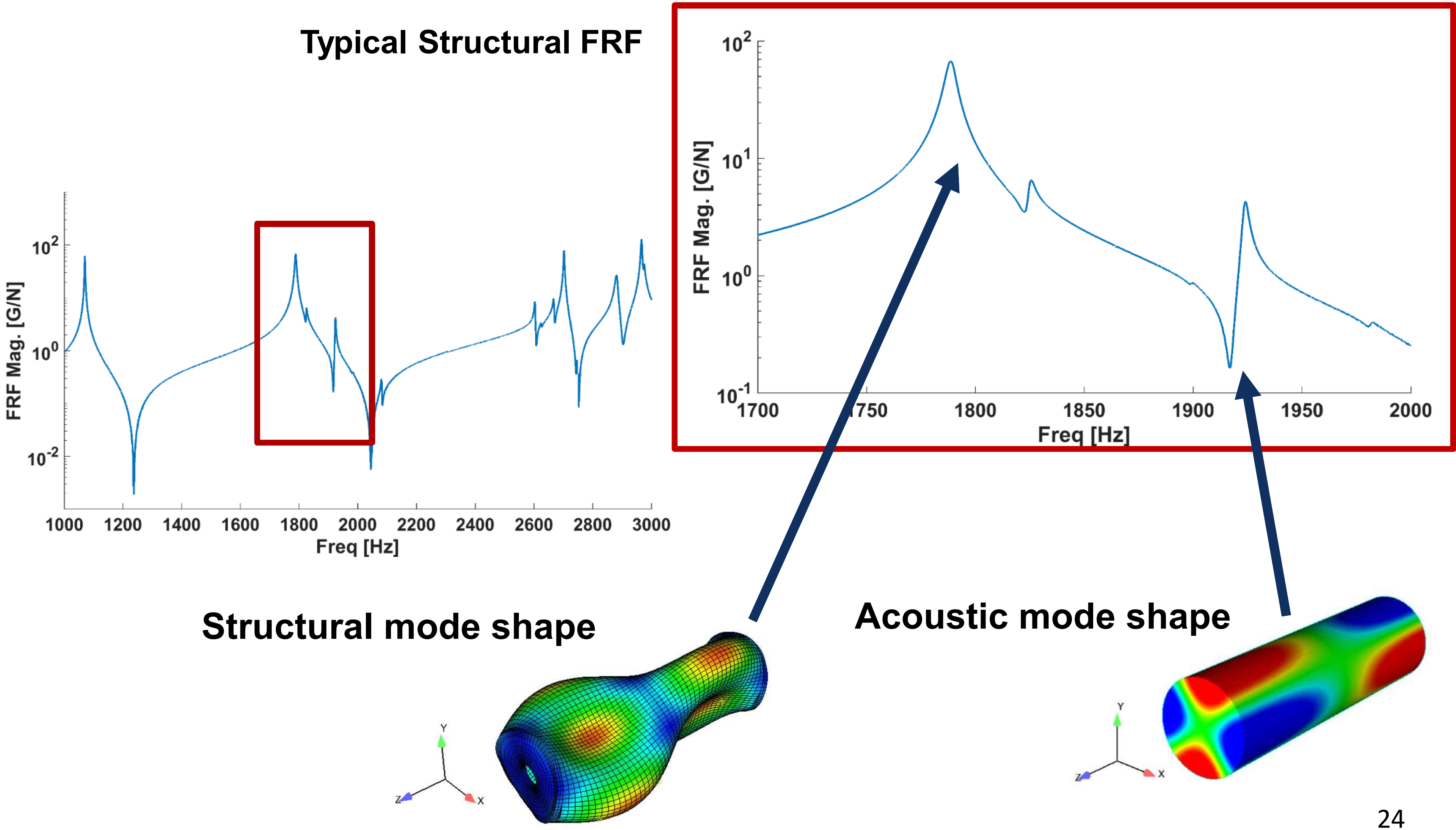
The two peaks of the coupled structural-acoustic pairs have opposite phasing



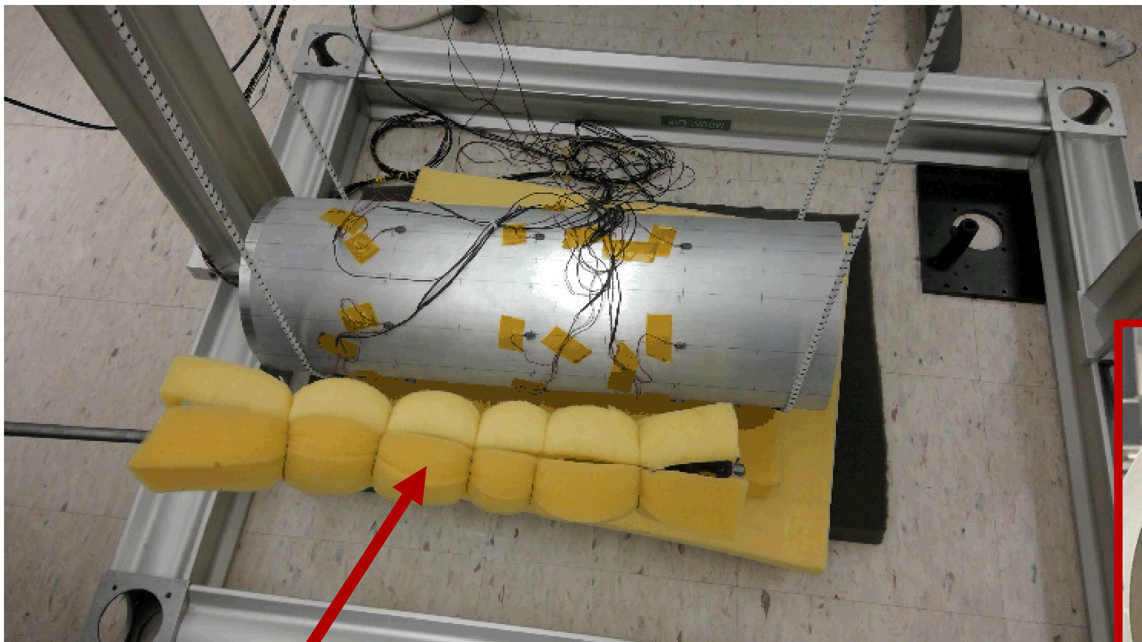
  

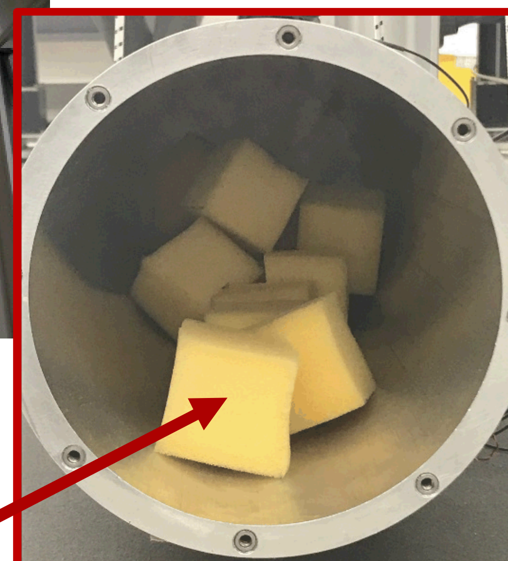
MITIGATION STRATEGIES

Mitigation strategies analyzed using the coupled modes in the 1700-2000 Hz frequency range



Introducing foam into cavity adds a source of acoustic damping

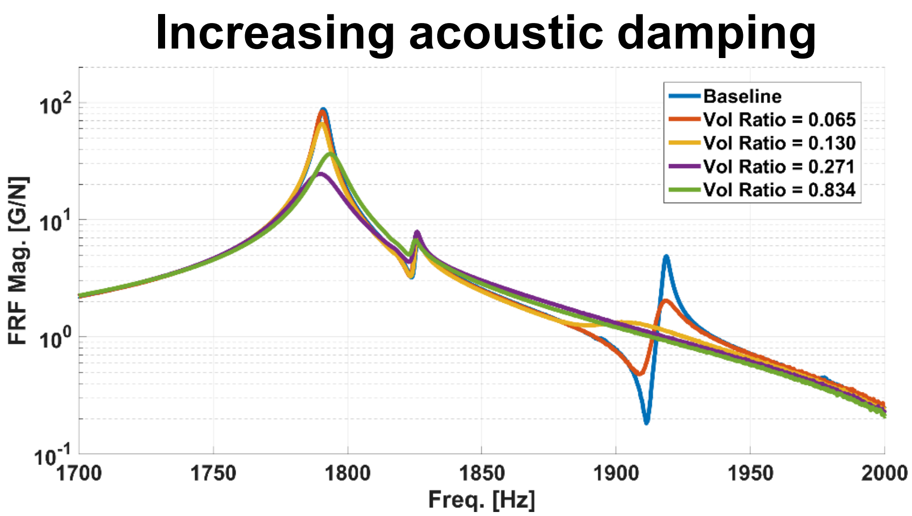




Foam covered rod (non-contact approach)

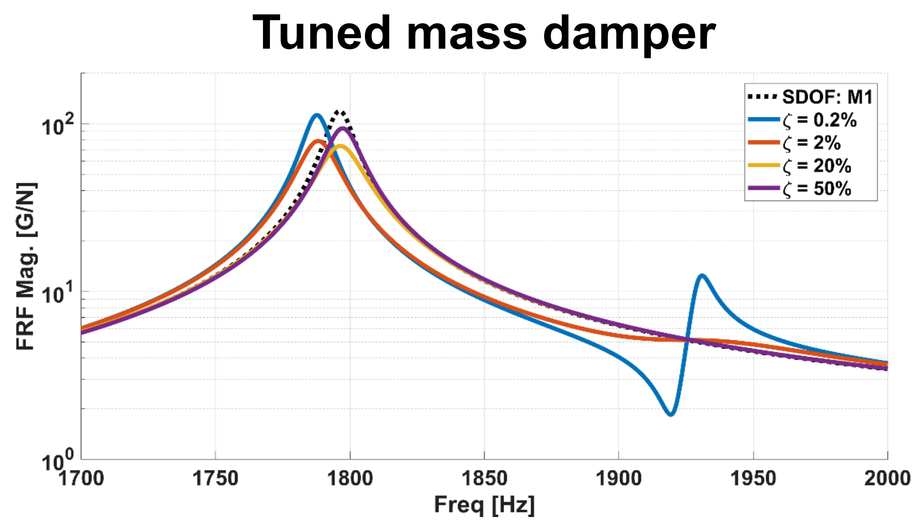
Foam cubes (contact approach)

Using the foam road (non-contact), increasing the foam volume decouples the structural response



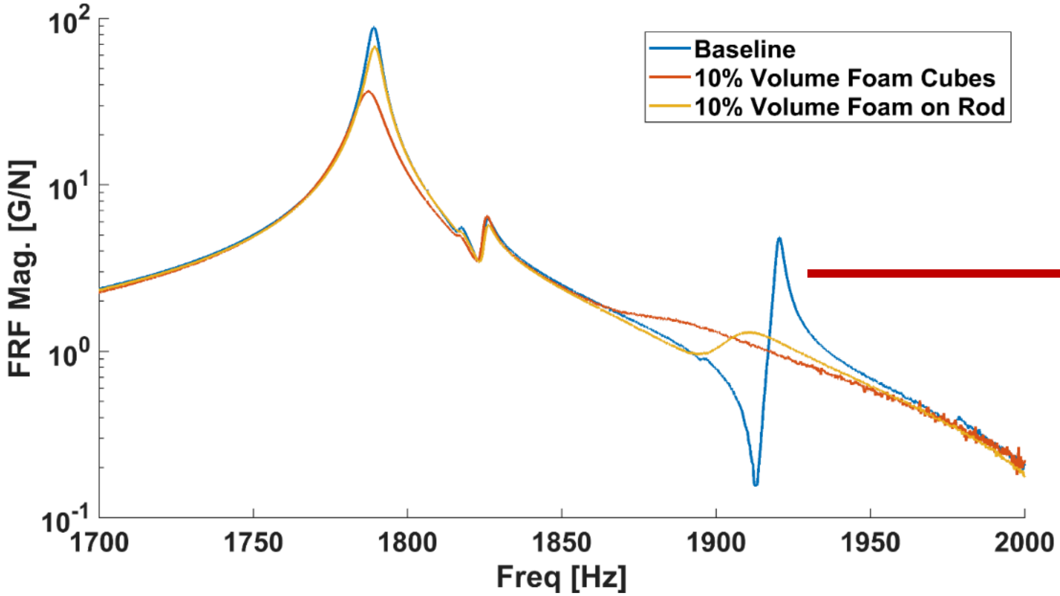
Coupled acoustic response damped out with around 25% of cavity filled with foam

Increasing foam causes structural peak to first decrease, then increase and shift in frequency; similar to a tuned mass damper

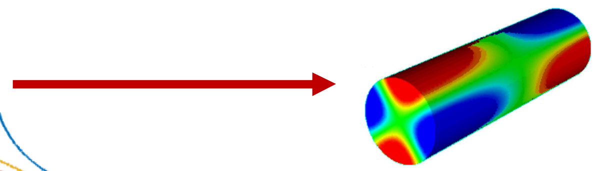


Foam cubes in contact with cylinder increased decoupling potential for same volume of foam

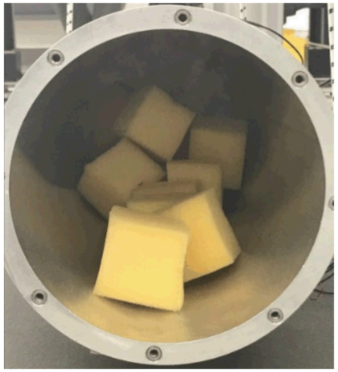
Non-contact vs. contact foam comparison



Acoustic (2,1,1) mode shape

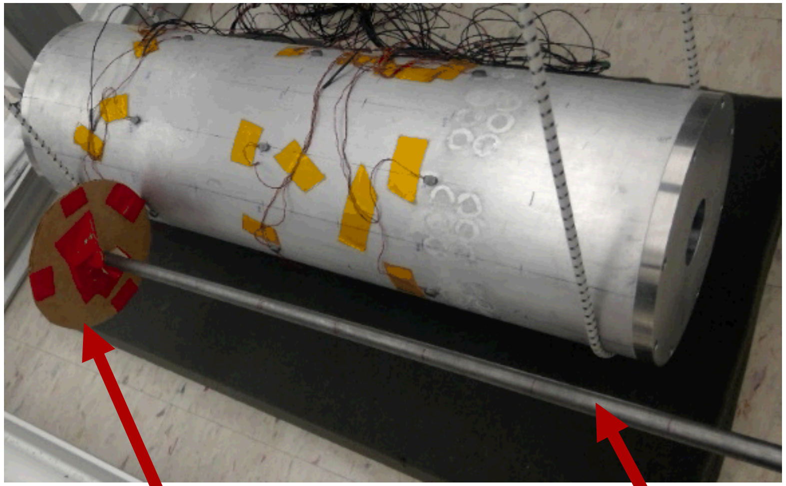


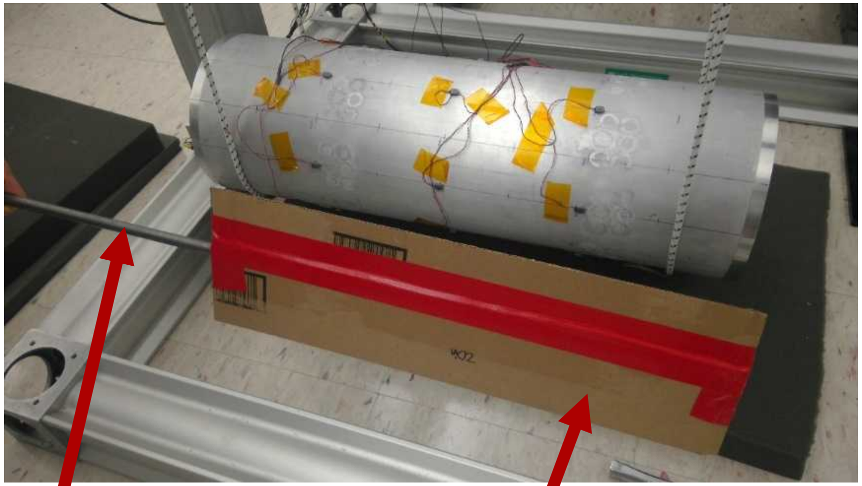
Foam in cavity



- Foam cubes inserted incrementally through hole in endcap
- Foam cubes are less compressed, leading to more effective acoustic absorption

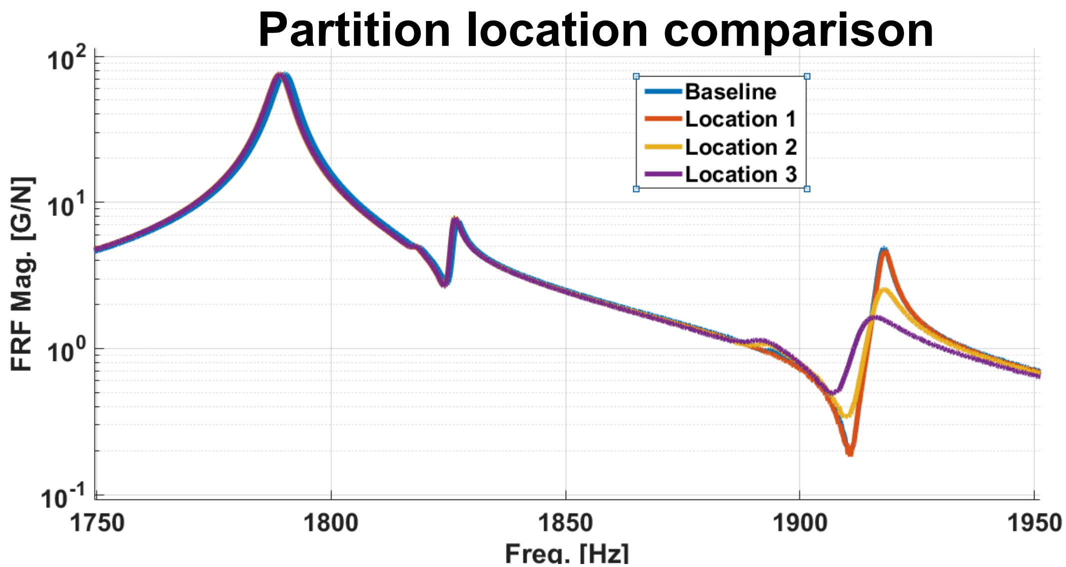
Including partitions in the cavity alters the acoustic mode shape

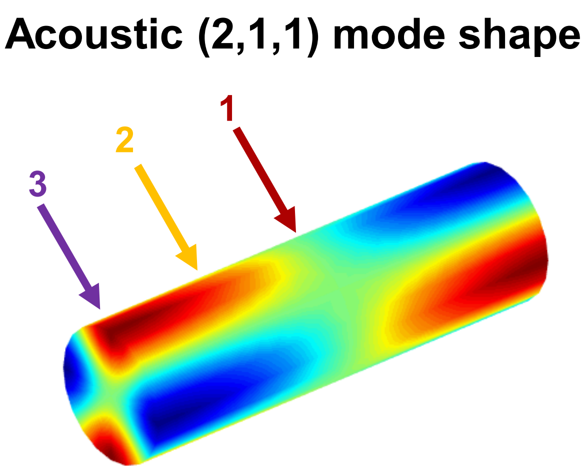




Cardboard disk **Insertion Rod** **Axial Cardboard Partition**

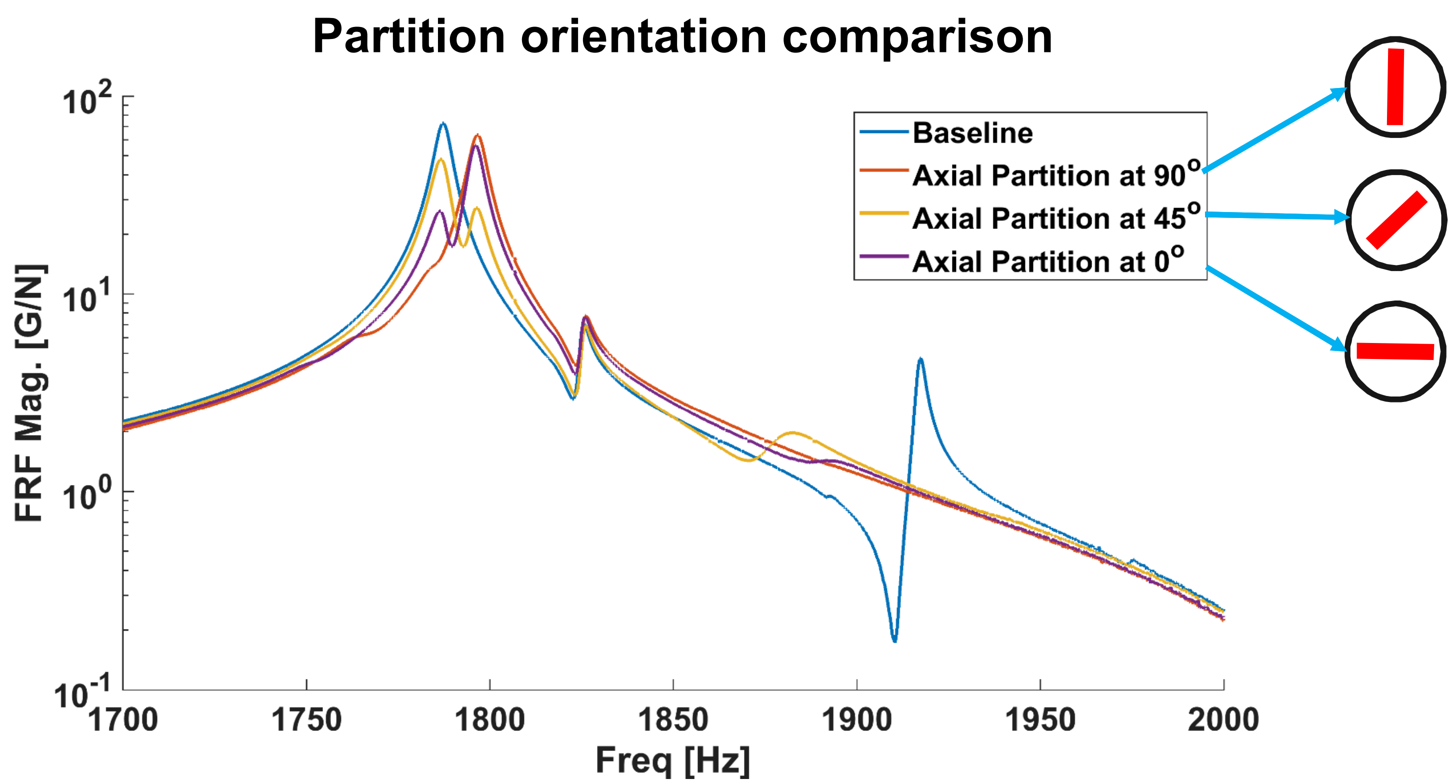
Locating cardboard disk partition at max acoustic pressure reduces coupling





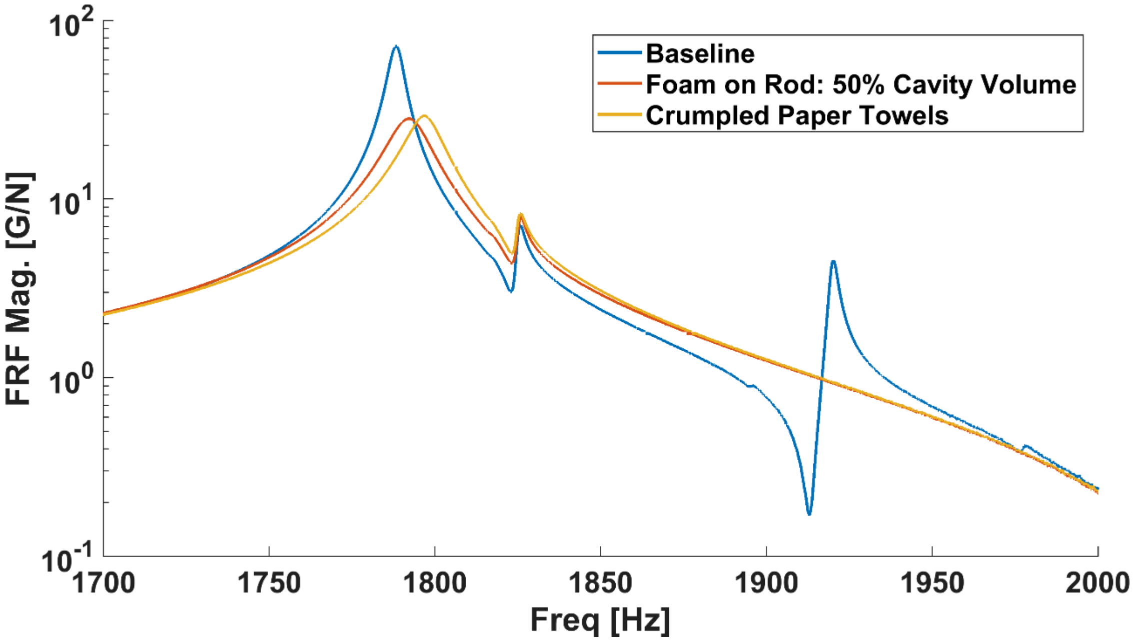
- Single cardboard disk did not adequately remove coupling
- Requires knowledge of mode shape to effectively place partition to reduce coupling

Including the axial cardboard partition further disrupted the coupling behavior

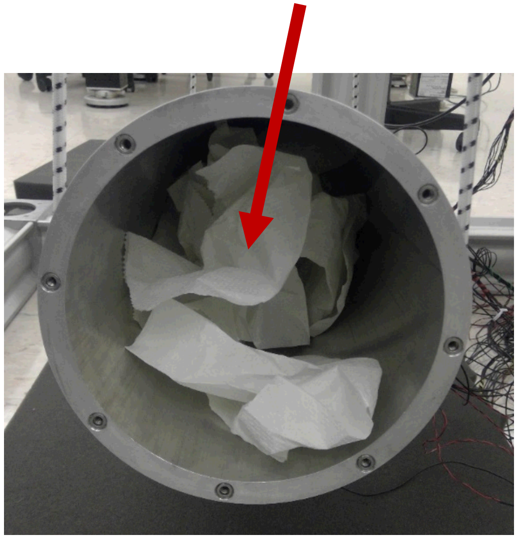


- Unexpectedly induced a frequency splitting in structural peak

Crumpled paper towels are most effective and convenient for decoupling

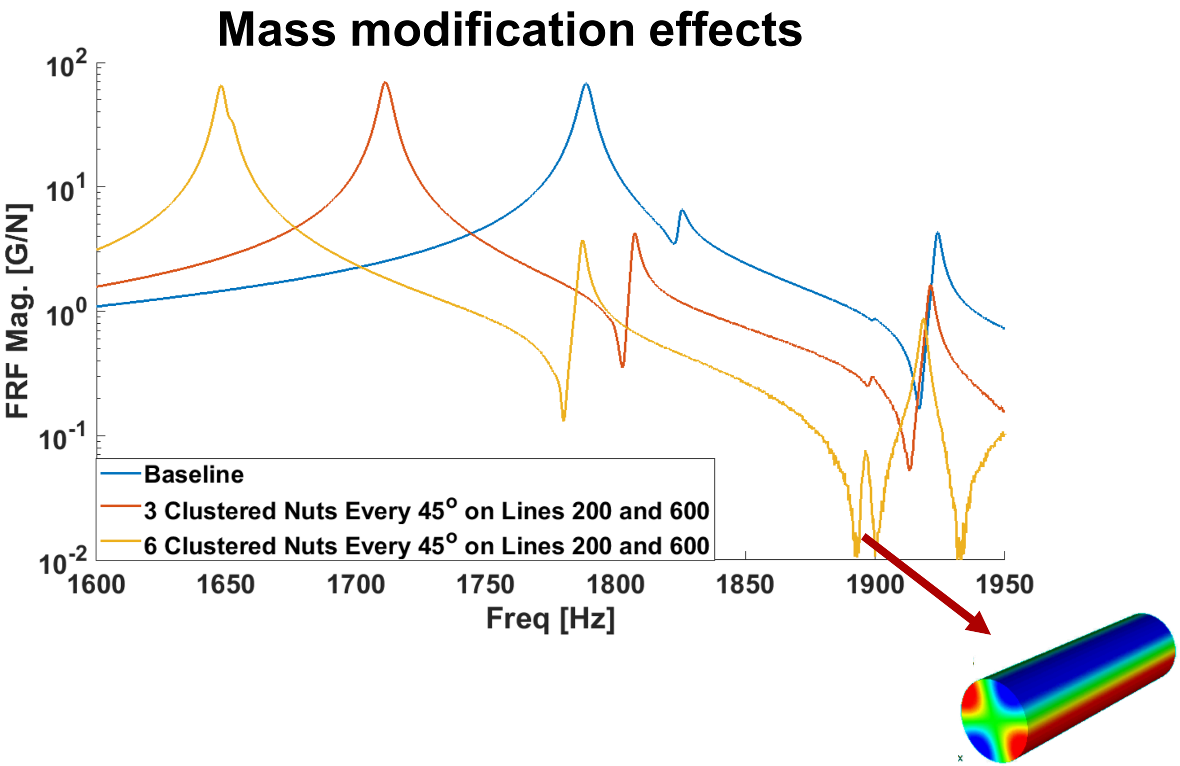


Crumpled paper towels

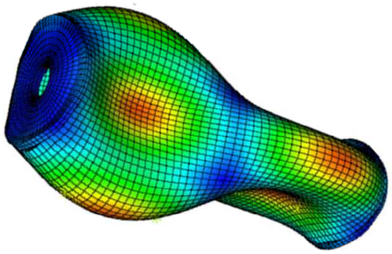


- Paper towels successfully disrupt acoustic modes without adding much mass to the system
- Cheap and readily available solution to both quickly identify and remove coupling

Adding mass at anti-nodes shifts structural peaks but has minimal effect on coupled peak



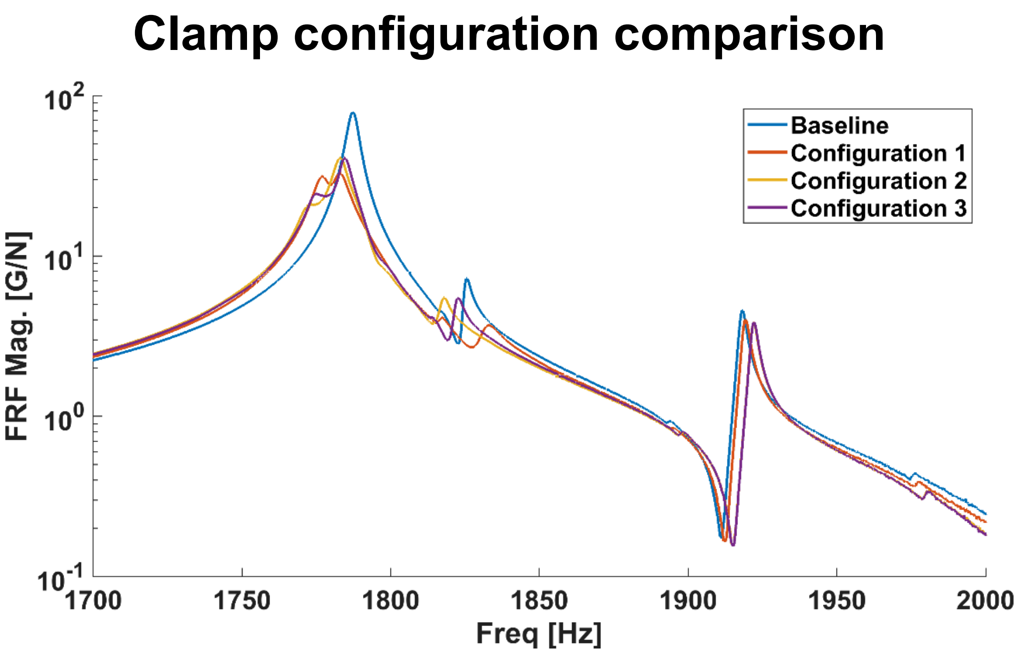
Structural (2,1) Mode Shape

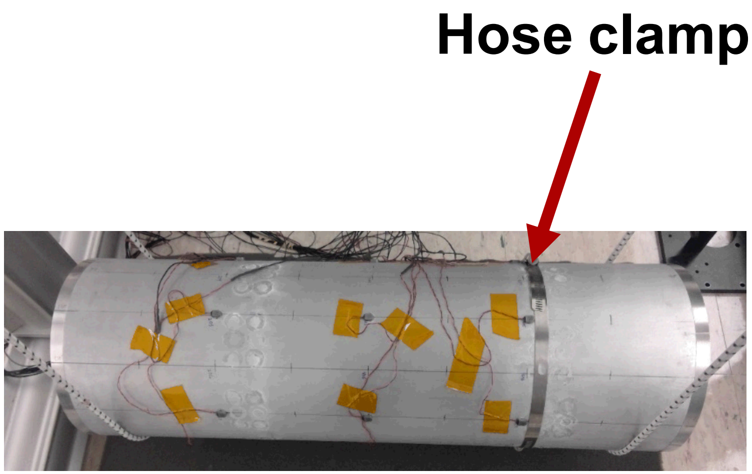


Masses bonded at anti-nodes

- Structural modifications may be necessary if cavity is inaccessible
- The frequency shift caused a second acoustic mode to couple with the structure, though at a small magnitude

Using hose clamps to add stiffness does not have the desired effect





- Structural peak shifted down in frequency, indicating that more mass than stiffness was added to the system
- No effect on decoupling the structure

Summary: Successfully measured acoustoelastic coupling and decoupled the structural response

- The air inside the cylindrical cavity caused coupling in multiple structural and acoustic modes
- Coupling identified and measured using typical structural impact excitation
- When the cavity is accessible, paper towels offer an effective and cheap method of quickly identify and mitigating coupling
- If the cavity is inaccessible, structural modifications have so far been unsuccessful in removing coupling