

Fracture mechanics of shales under chemically reactive conditions

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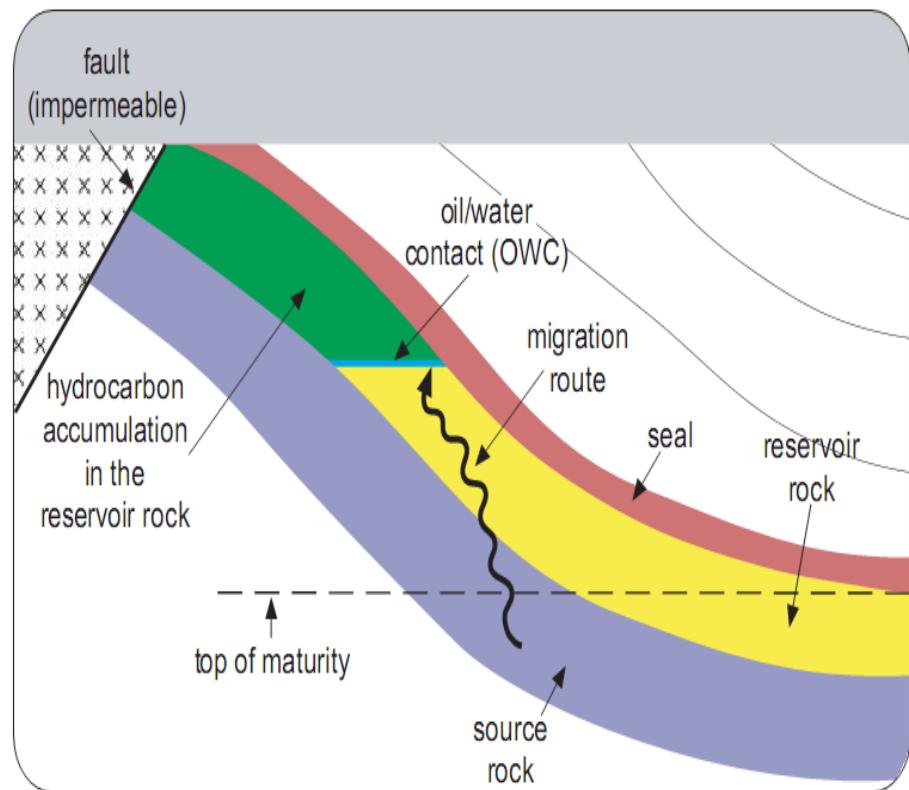
Acknowledgments:

DOE-NETL DE-FE0023316 Geomechanics of CO₂ Reservoir Seals
Fracture Research and Applications Consortium FRAC

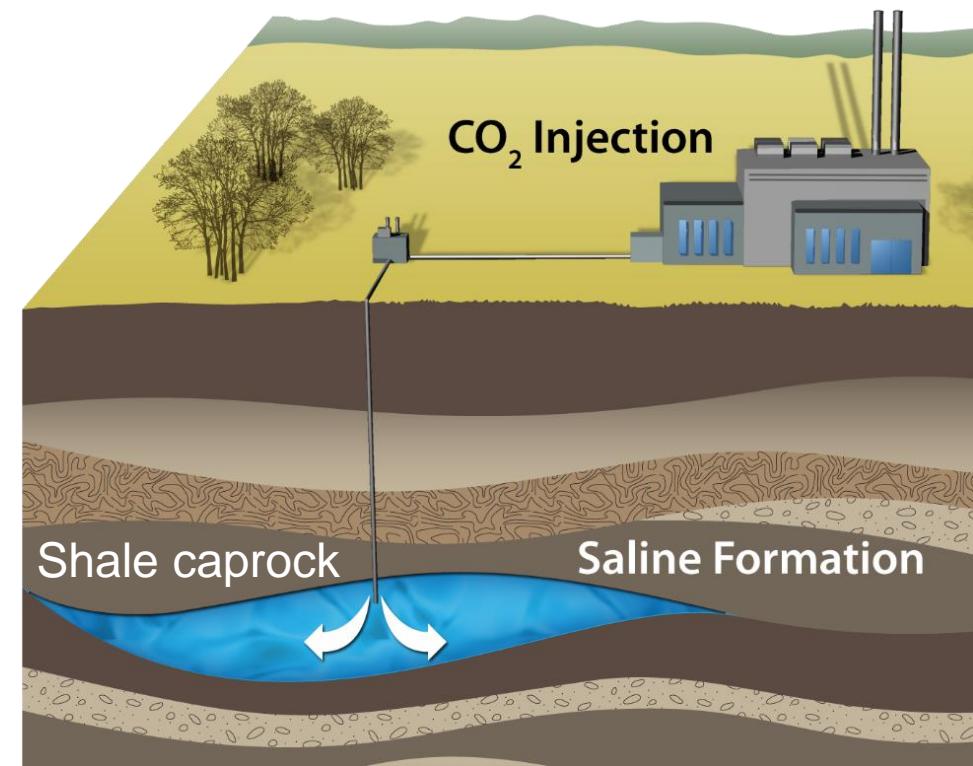
Motivation

Problem: fracture growth under chemically reactive conditions.

Fluid-rock interactions

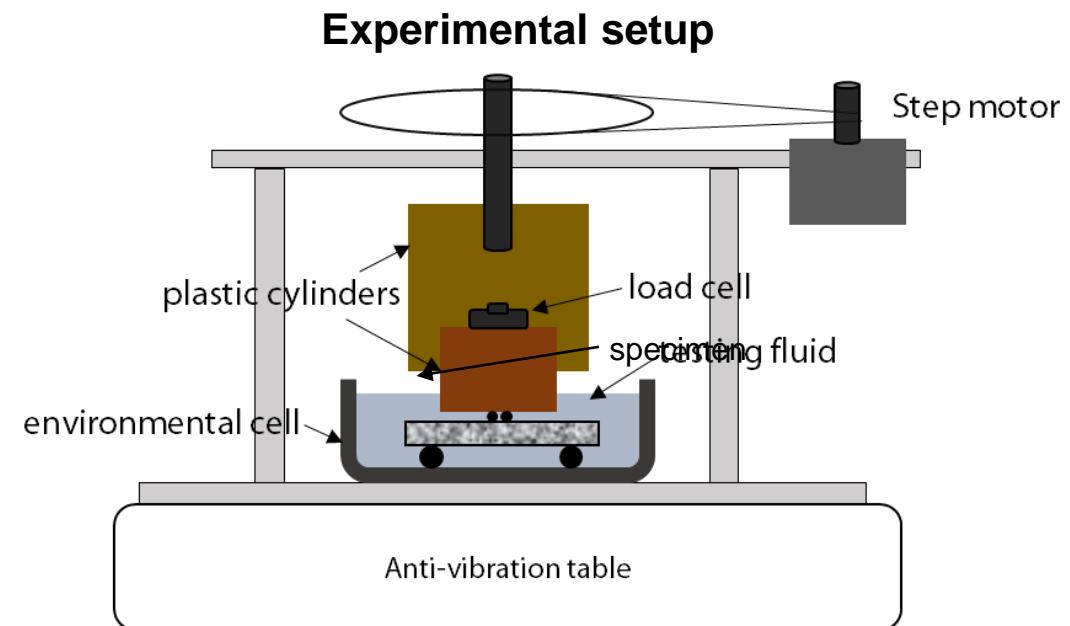
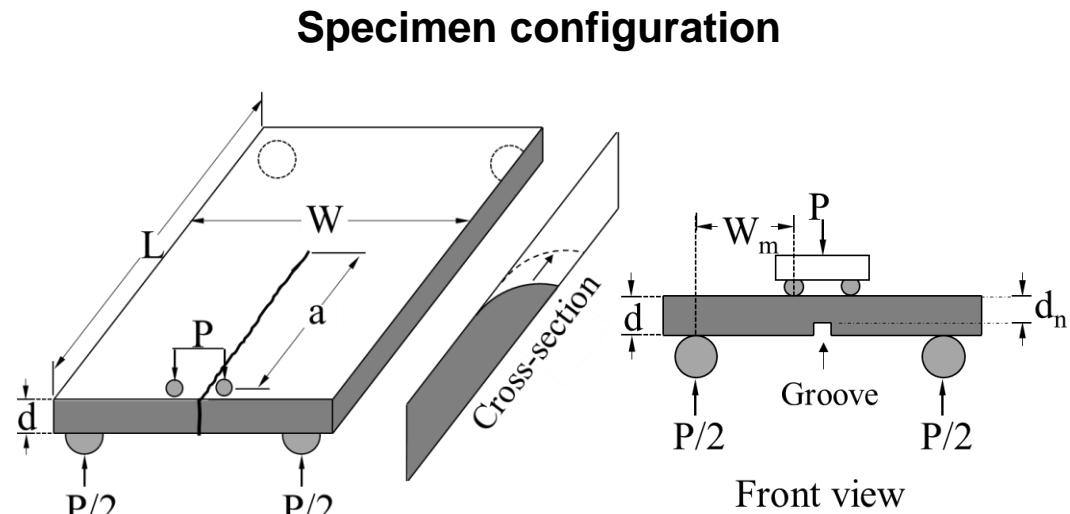
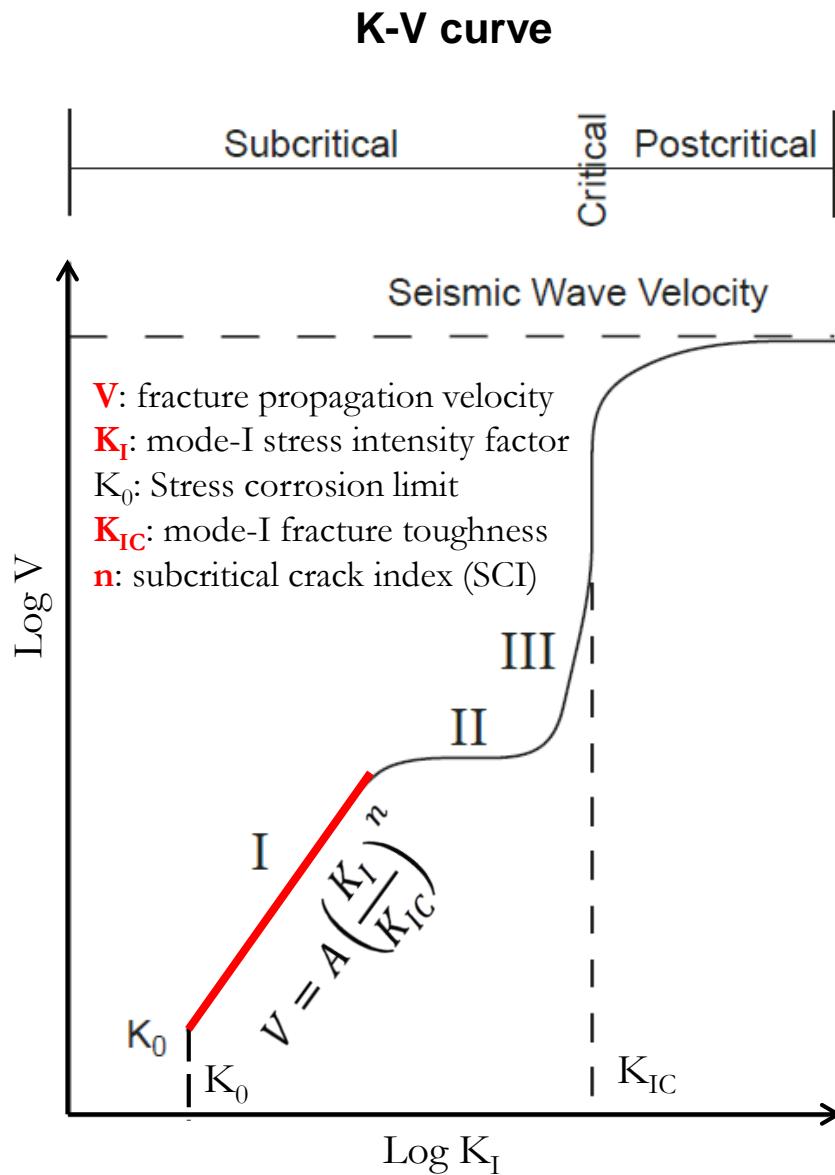


Fracture growth.



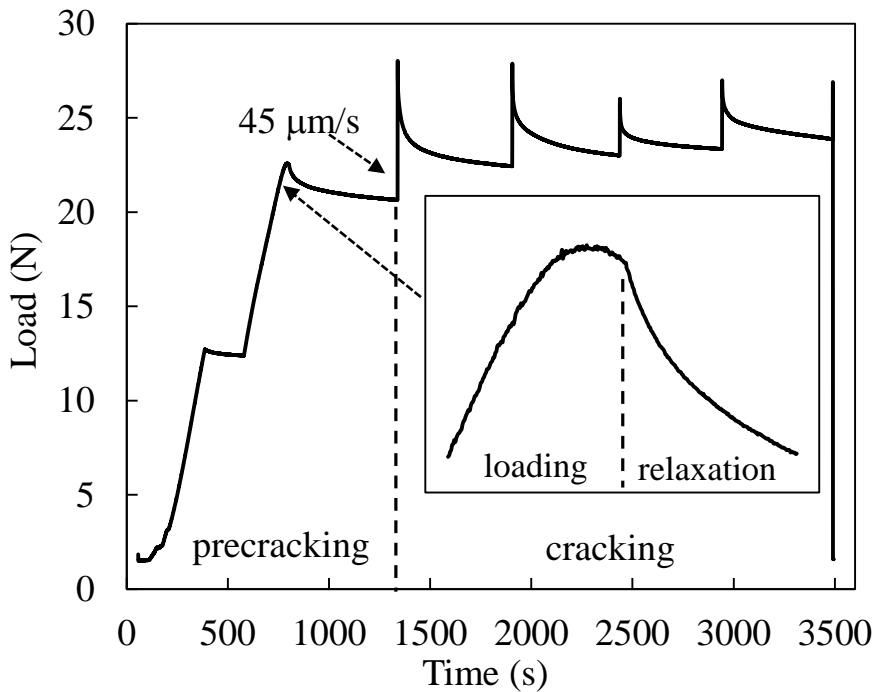
Approach: subcritical fracturing tests under chemically reactive conditions.

Mode I fracture testing

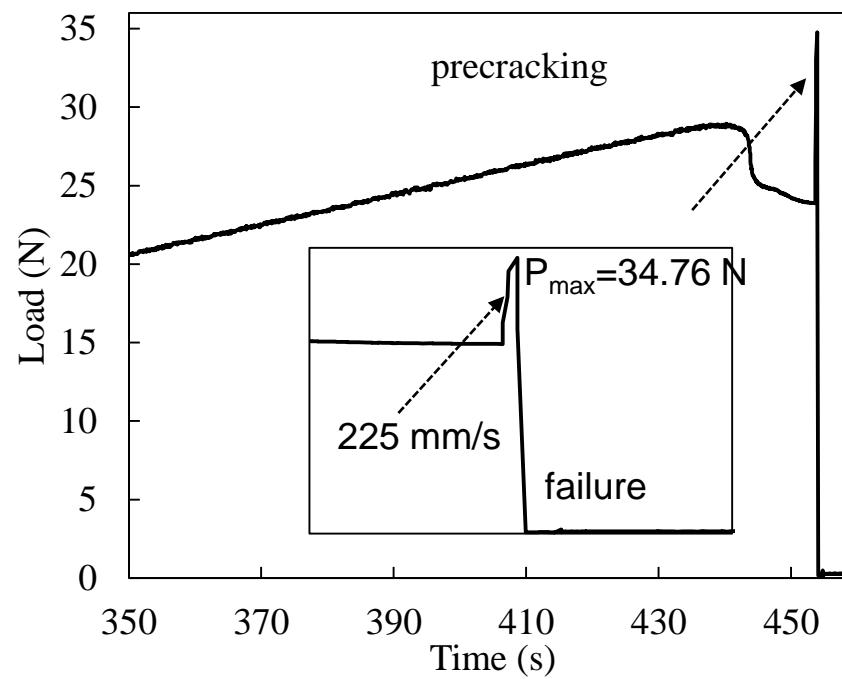


Mode-I fracture testing

Load relaxation: SCI and K-V curves



Critical failure: K_{IC}



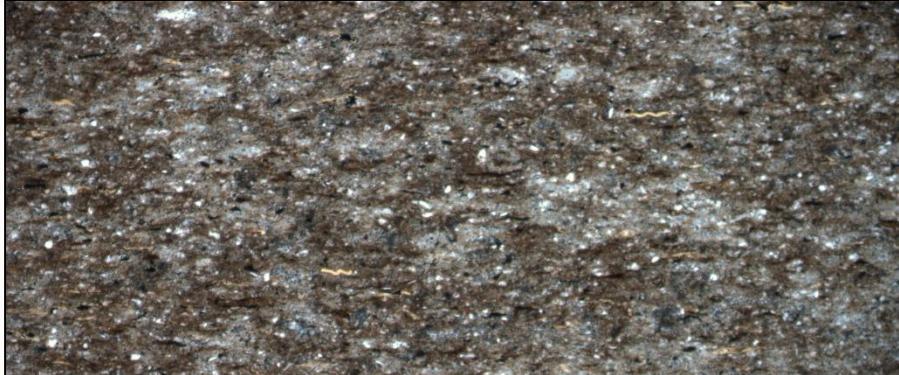
$$K = PW_m \left[\frac{3(1+\nu)}{Wd^3 d_n \psi} \right]^{1/2} \quad V = -\phi \frac{P_0 a_0}{P^2} \frac{dP}{dt}$$

Testing protocol

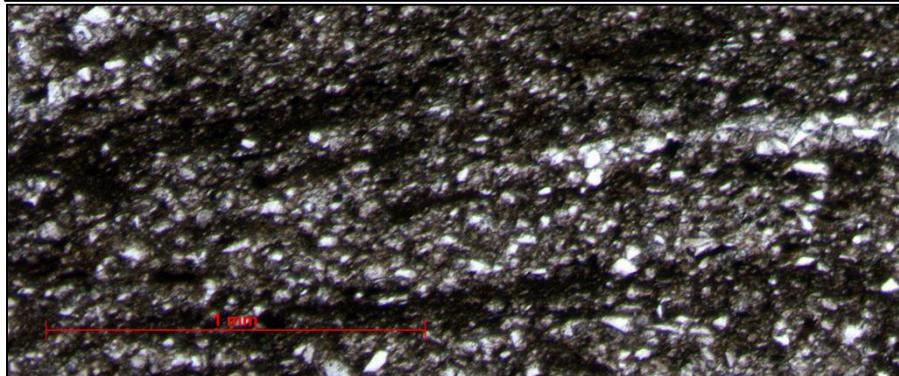
- Three shale types
 - Woodford, Mancos, Marcellus
 - Also sandstones for comparison/integration
- Room dry, $\text{CO}_{2\text{gas}}$, DI water
- Varying salinity, NaCl , KCl
- Varying pH
- Room temperature, 65°C
- Some samples coated with hydrophobic agent to limit fluid/rock interaction to fracture tip

Three shale lithologies

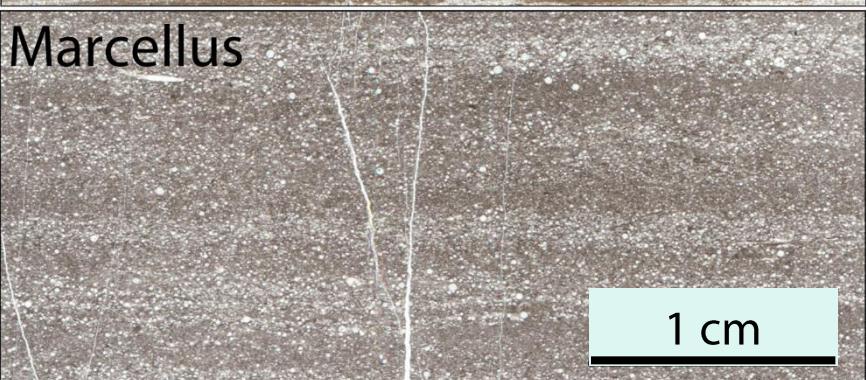
Woodford



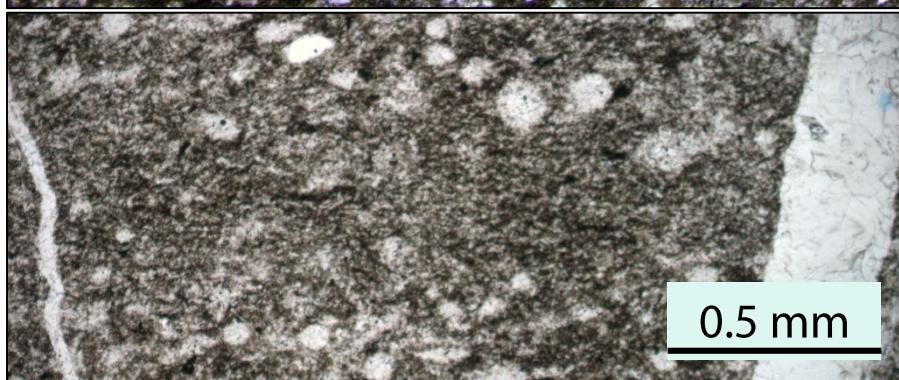
Mancos



Marcellus

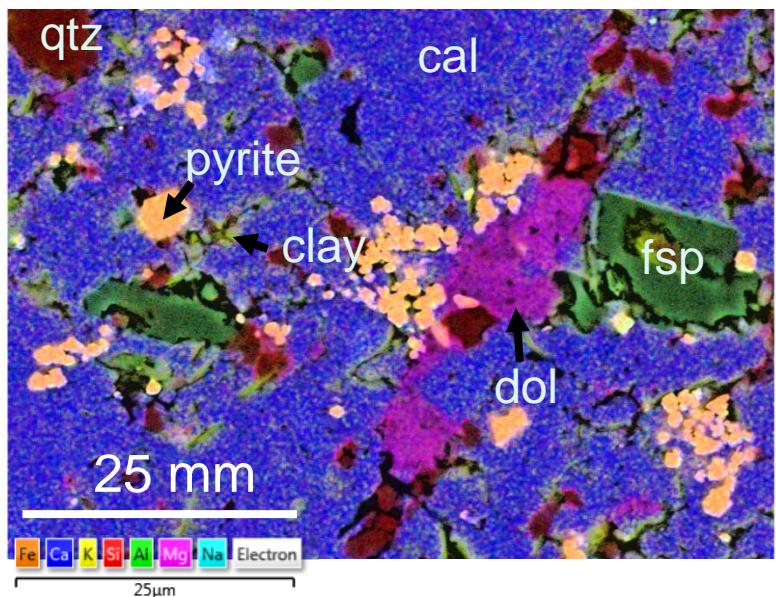
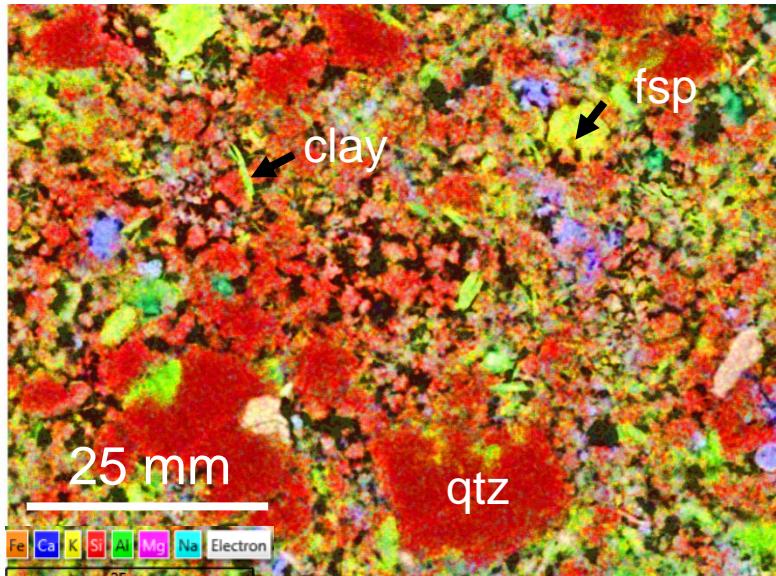


1 cm

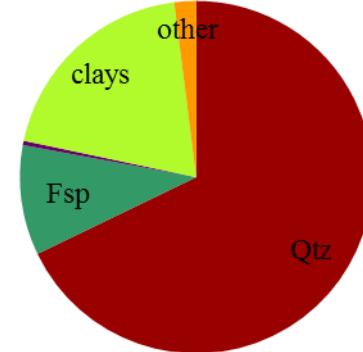


0.5 mm

Shale sample composition

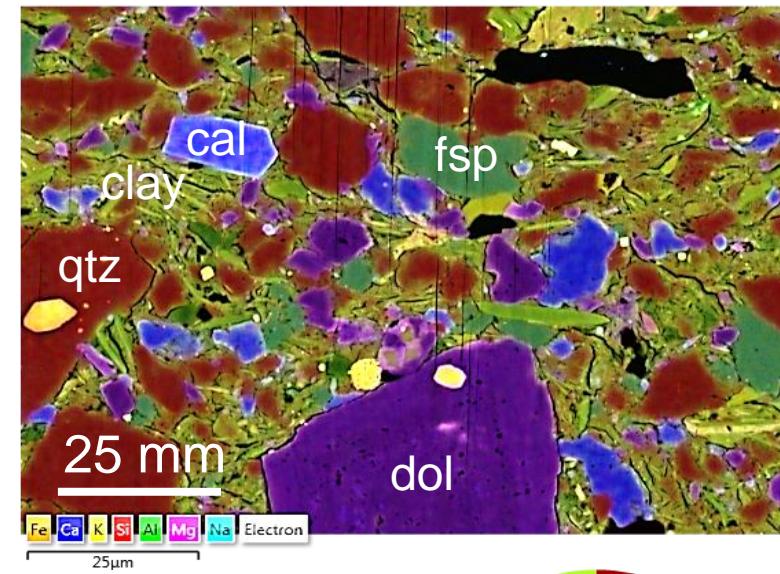


Woodford shale

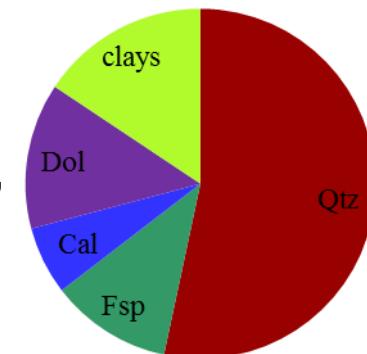


Quartz, clays, fsp

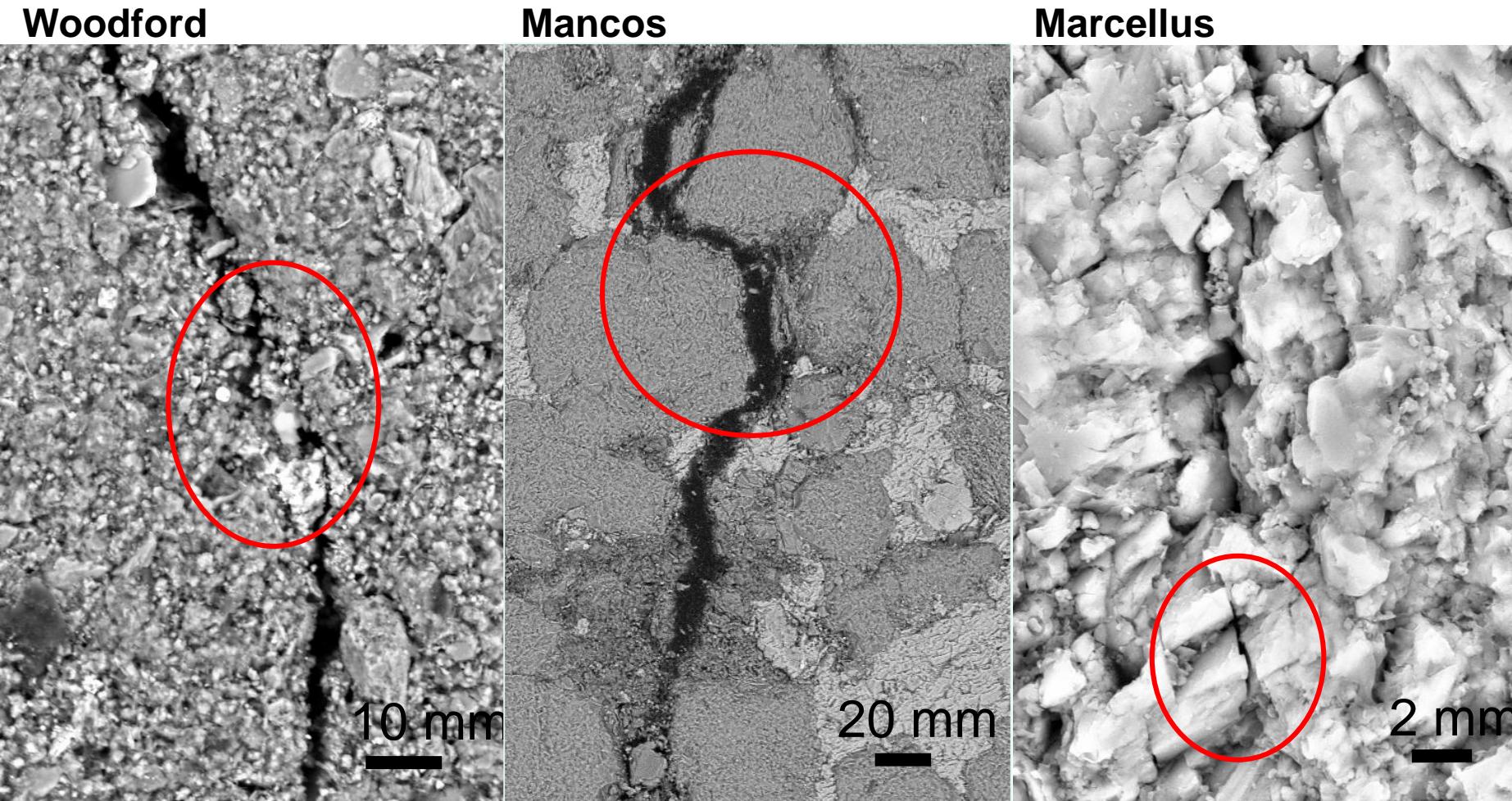
Mancos shale



Quartz, clays, carbonate



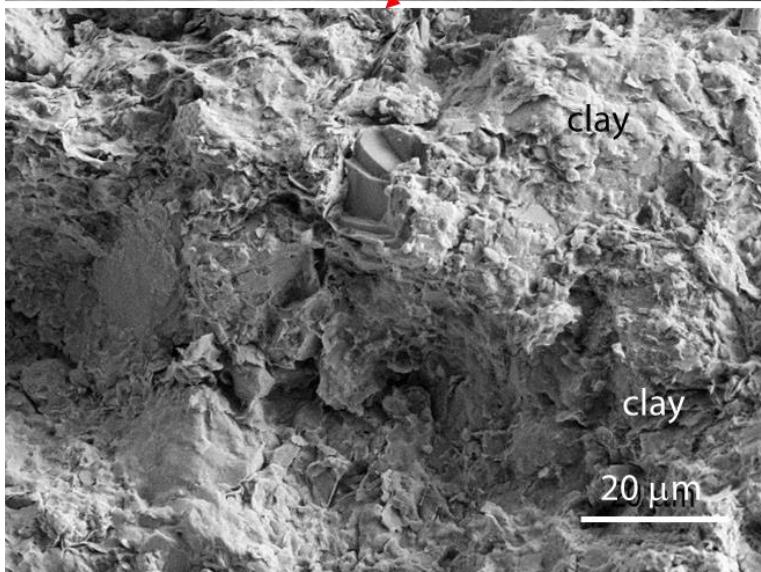
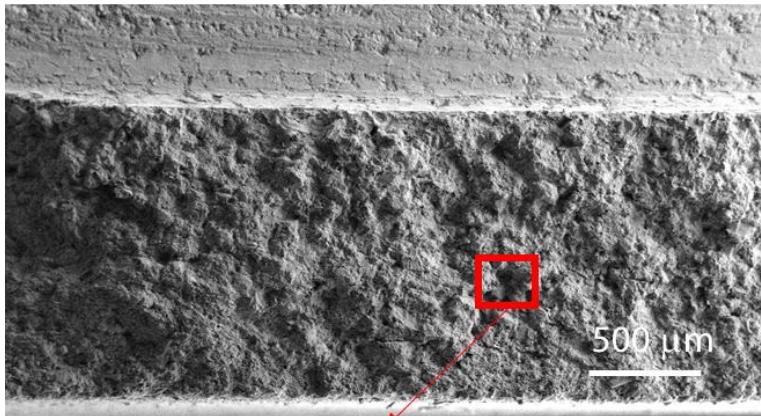
Fracture trace imaging



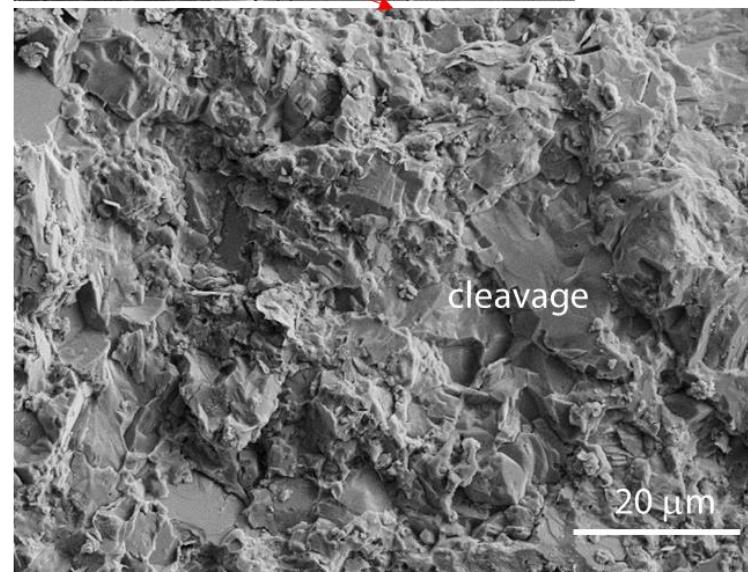
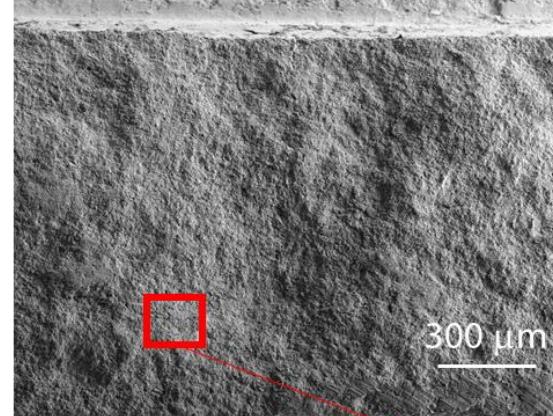
- Woodford, Mancos: intergranular fracture (through clay matrix)
- Marcellus: intragranular (cleavage) fracture

Fracture surface imaging

Mancos shale

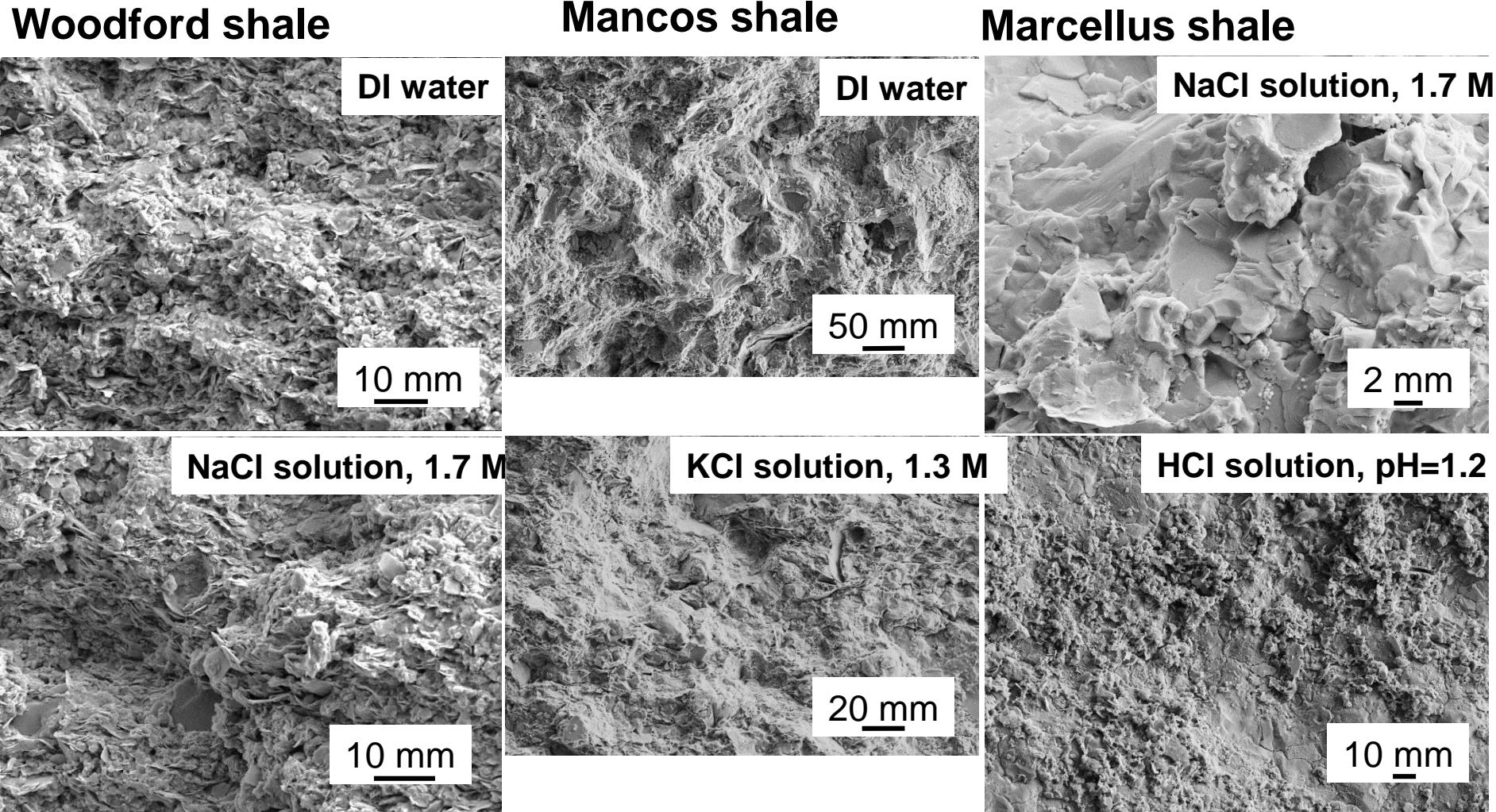


Marcellus shale



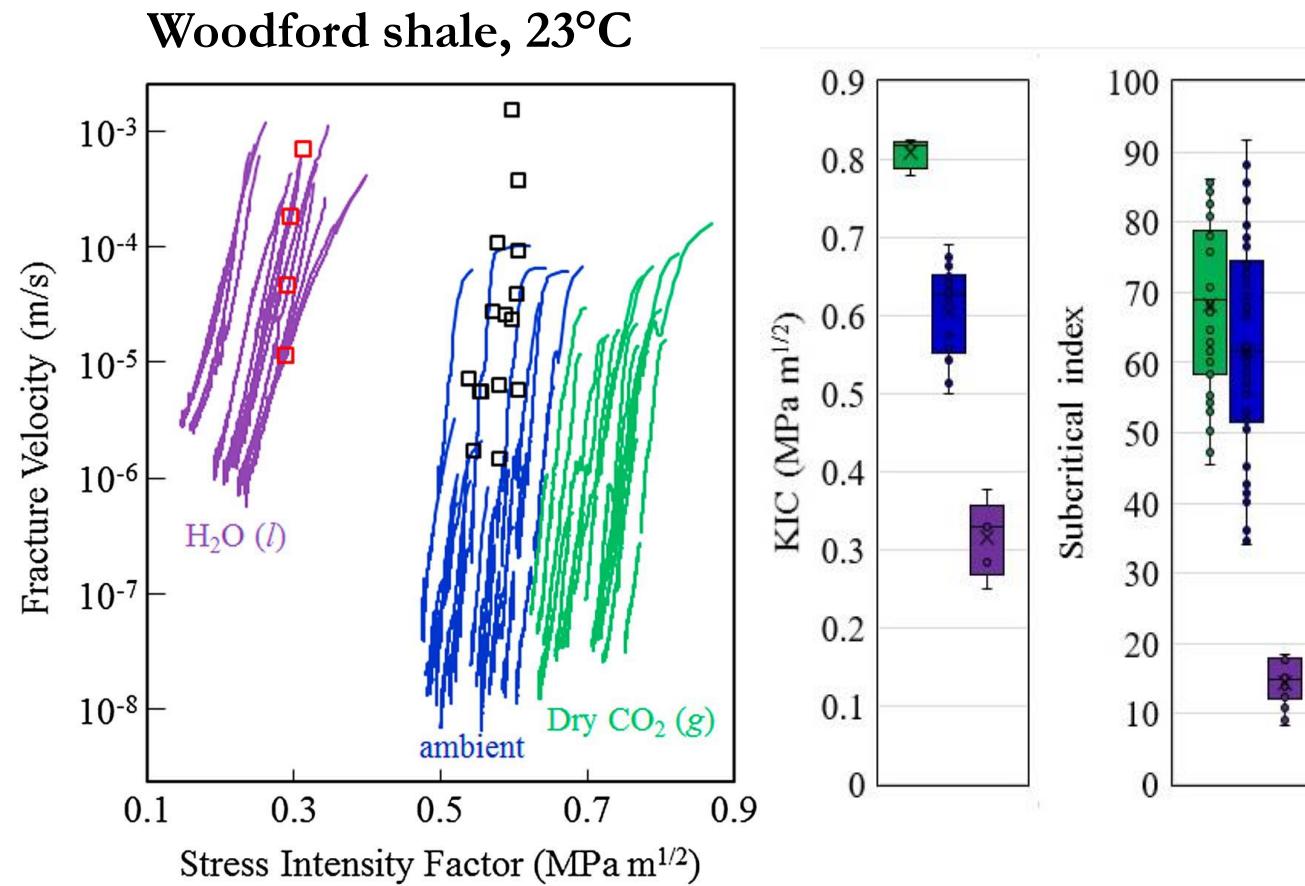
- Roughness variation, but no plumose structure
- Grain boundary breakage vs transgranular breakage

Fracture surface imaging



Fracture surface features invariable with fluids conditions, indicating similar subcritical fracturing process.

Fracture response: Water content

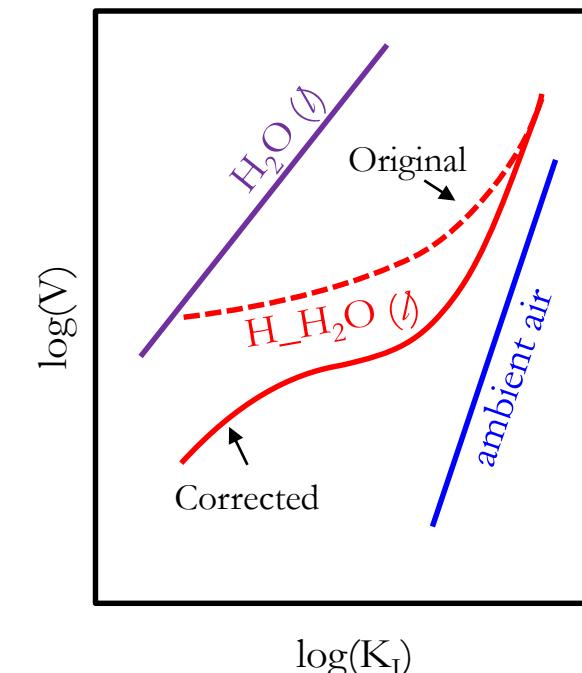
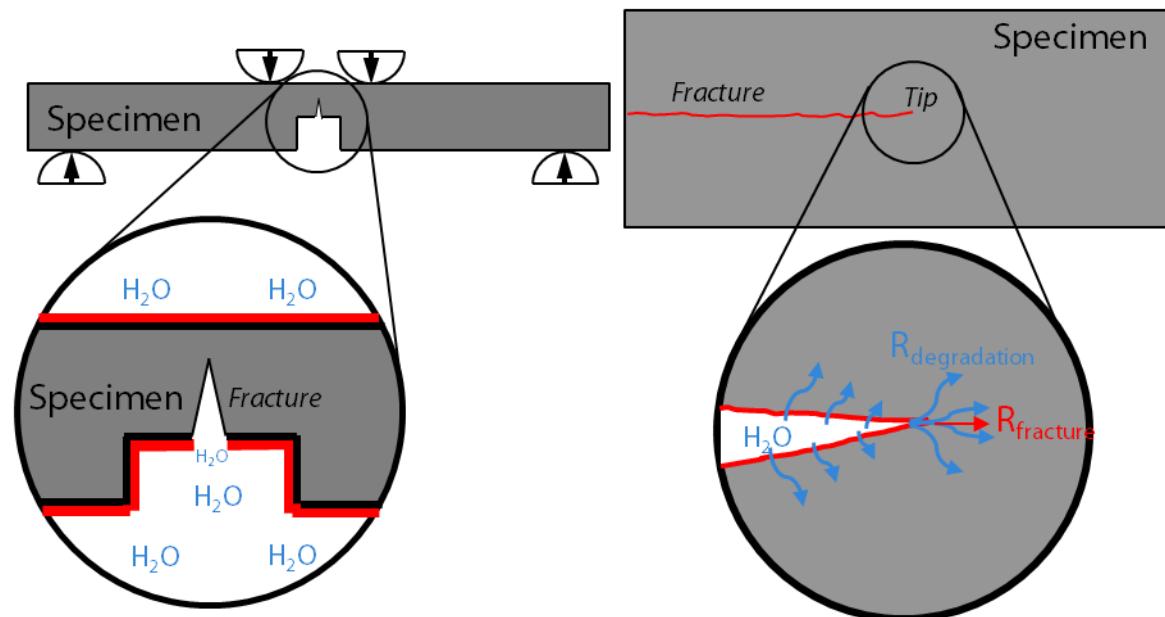


Water enhances subcritical fracturing for clay-rich shales

- Strong reduction of K_{IC} (48%) and SCI (75%) with increasing water content
- K-V curves obey power-law, indicating fracturing in stress-corrosion regime (I)
- Load relaxation technique (lines) matches constant loading rate method (squares)

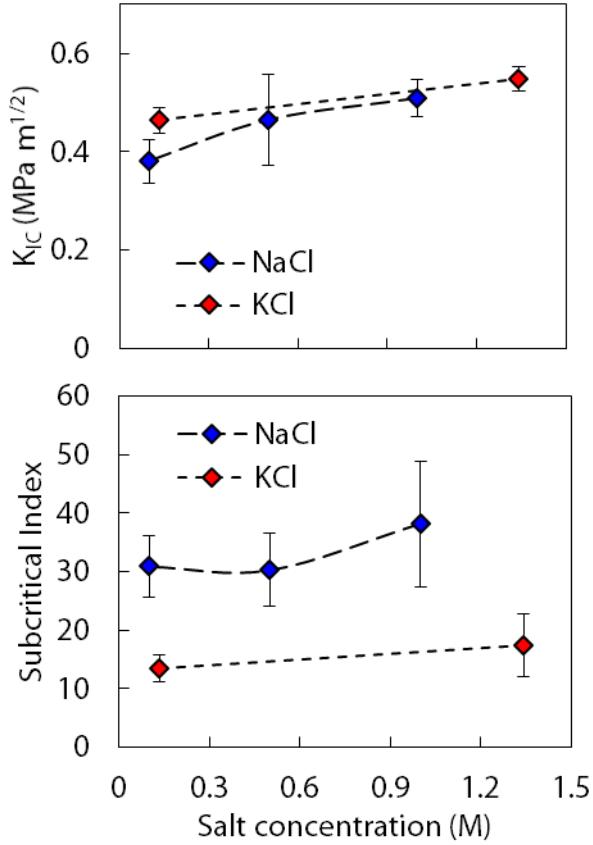
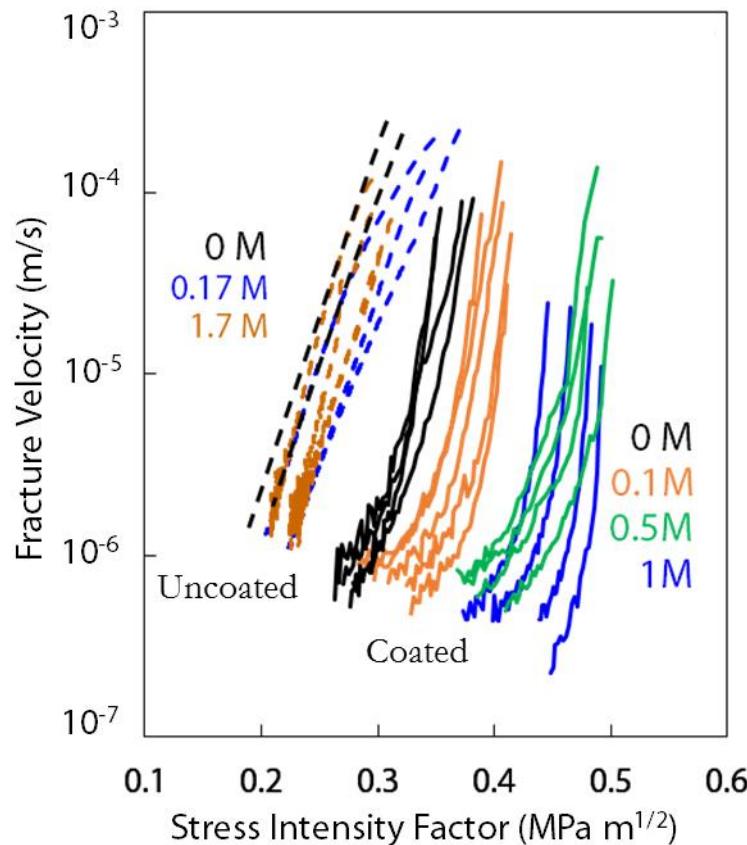
Transient weakening response: Coated samples

- Hydrophobic coating restricts water-sample interaction to the fracture tip
- Coating temporarily protects specimens from weakening except at fracture tip
- Transient K-V curves.
 - Only for clay-rich Woodford and Mancos shales
 - Competition between **fracture growth** and **rock degradation** by H_2O -rock interaction



Fracture response: Salinity

Woodford shale, NaCl brine, 23°C

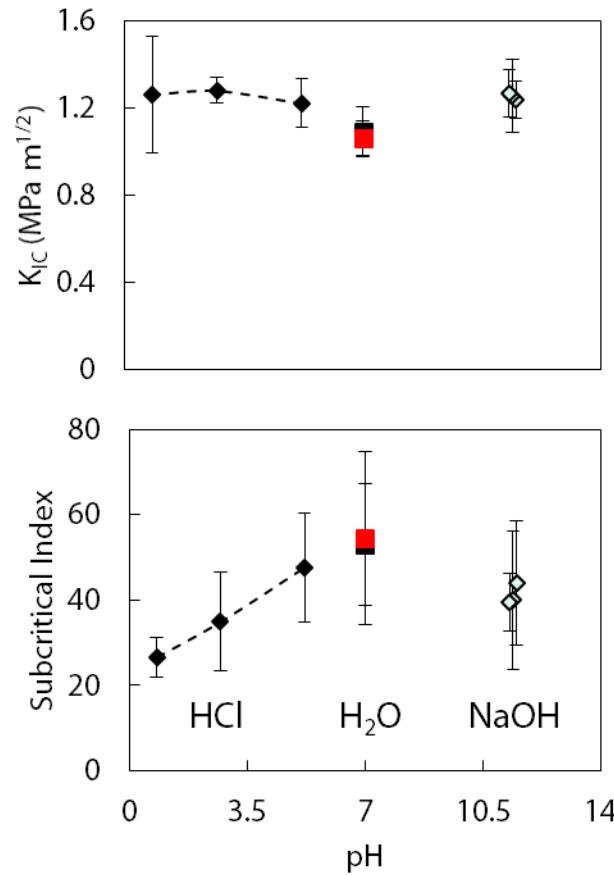
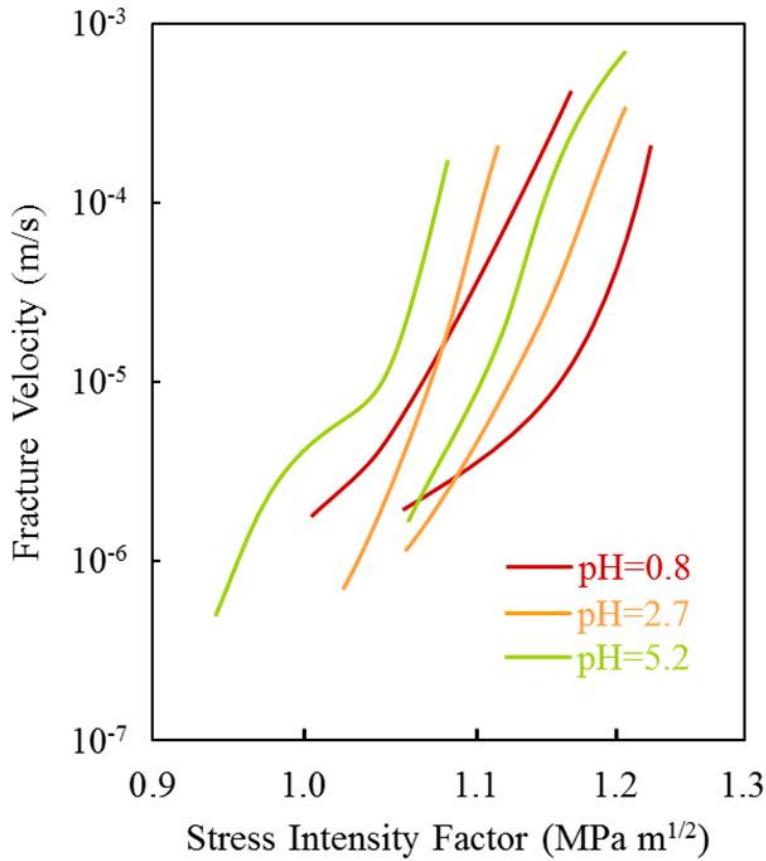


Increase of fluid salinity increases K_{IC} and SCI in clay-rich Woodford and Mancos shales

- Less weakening in KCl brine than in NaCl brine
- Clay swelling

Fracture response: pH

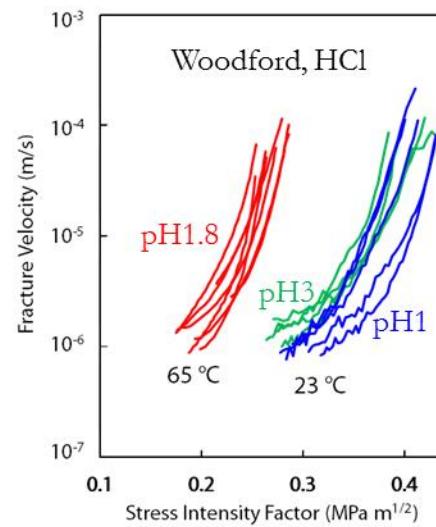
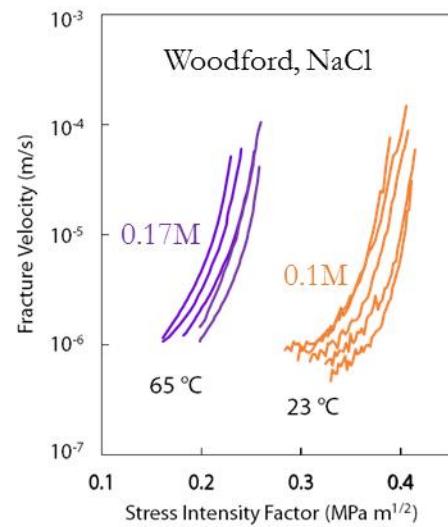
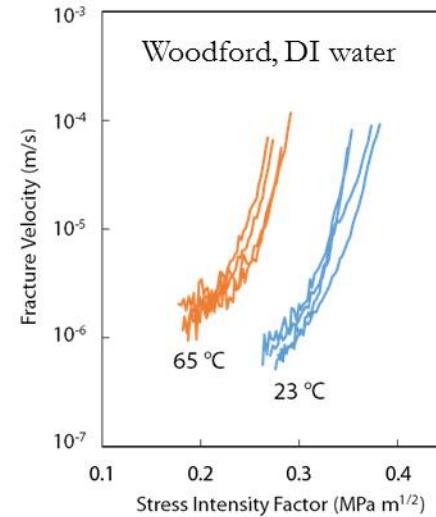
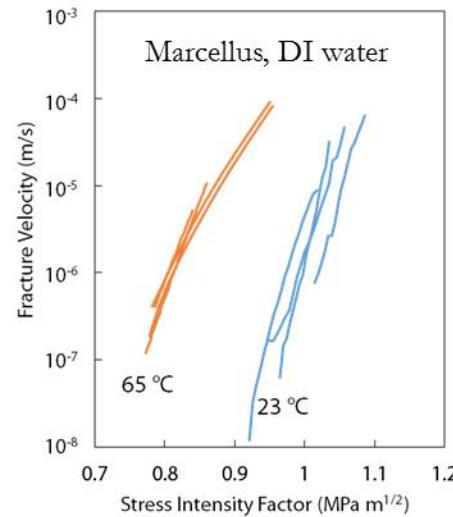
Marcellus shale, HCl solution, 23°C



SCI decreases with decreasing pH for carbonate-rich Marcellus shale

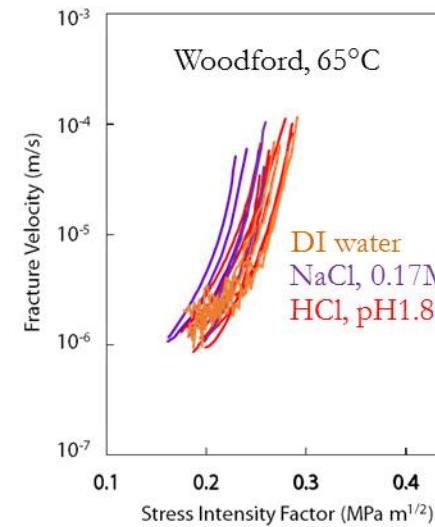
- K_{IC} is independent of pH
- SCI effect opposite to that in glass and quartzite
- Calcite dissolution

Fracture response: Temperature

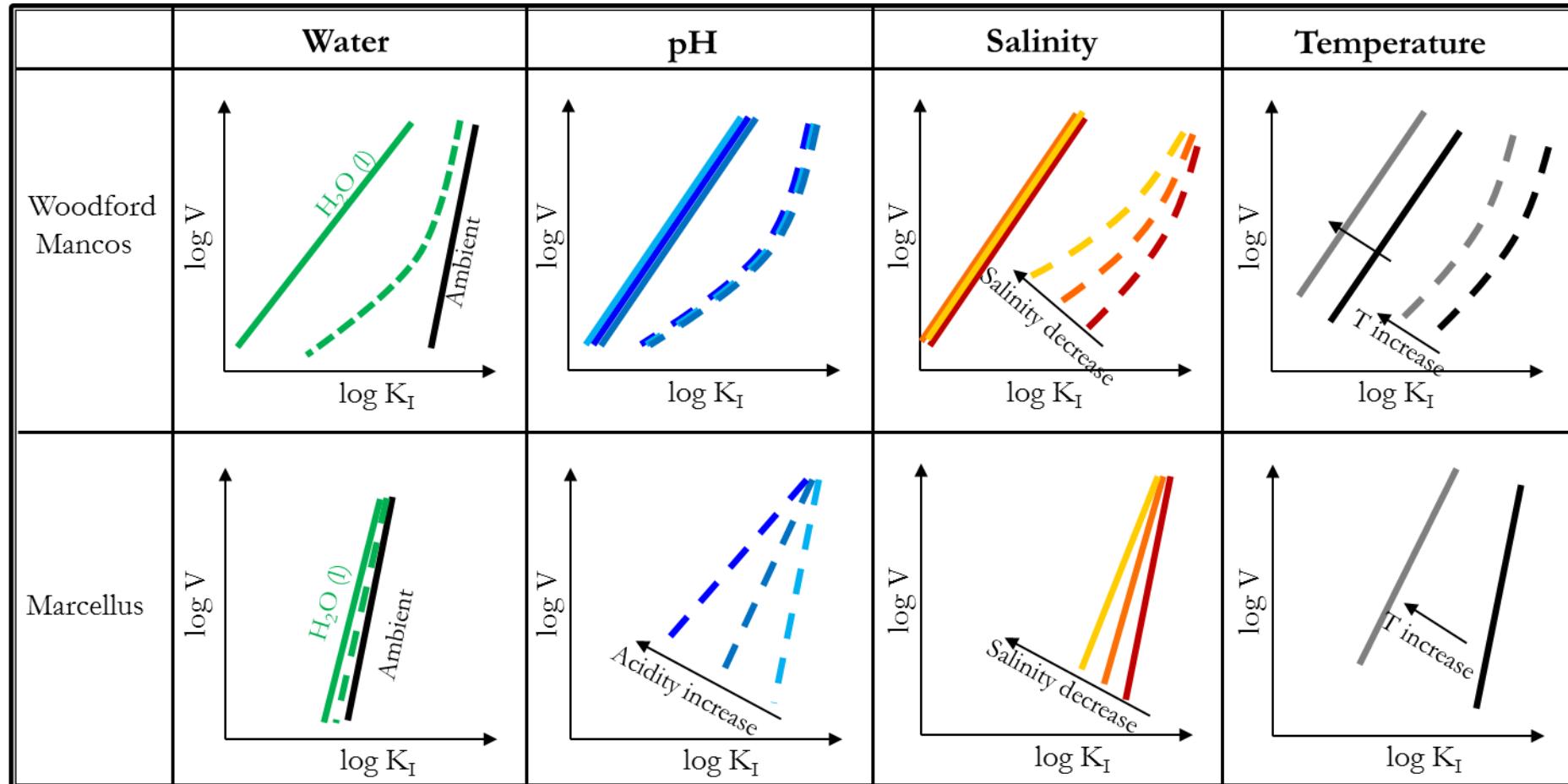


Increase in temperature enhances subcritical fracturing

- Left-ward shift for all shales
- Concentration effects less pronounced at elevated T

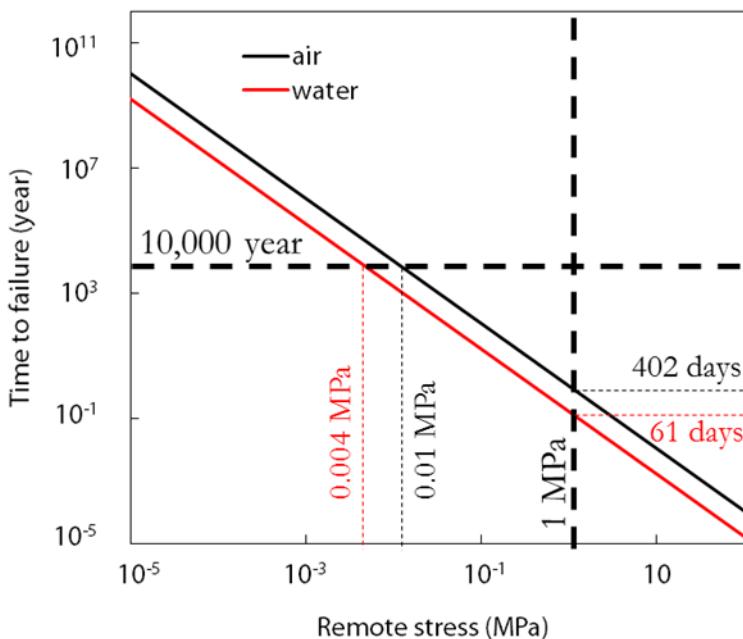
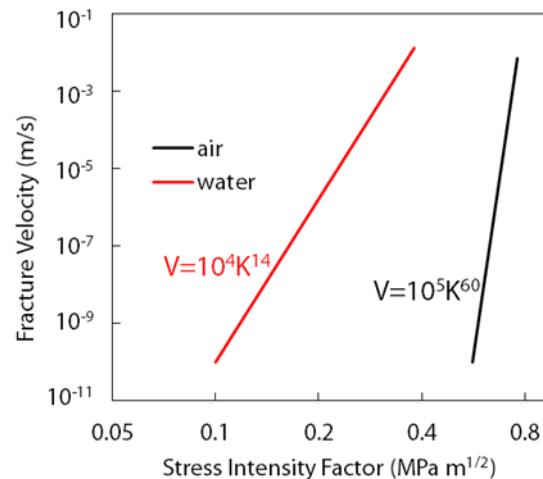


Environmental effects on K-V behavior



— Uncoated
- - - Coated

Time-to-failure analysis



Constant stress loading:

$$\left. \begin{aligned} K &= \sigma Y \sqrt{a} \\ V &= A K^n \end{aligned} \right\} \Rightarrow t_f = \int dt = \int_{a_0}^{a_f} \frac{da}{V} = \frac{2}{\sigma^2 Y^2} \int_{K_0}^{K_{IC}} \frac{K}{V} dK$$

$$\Rightarrow t_f = \frac{2}{(2-n) A \sigma^2 Y^2} (K_{IC}^{2-n} - K_0^{2-n})$$

Evans (1972) & Nara et al. (2015)

Assume subcritical crack growth limit @ 10^{-10} m/s :

- To meet safe storage time $> 10^4$ years, $\sigma < 0.004 \text{ MPa}$ for wet, $\sigma < 0.01 \text{ MPa}$ for dry conditions.
- Under $\sigma = 1 \text{ MPa}$, failure occurs at 61 days for wet, 402 days for dry.

Summary

- Chemical environments, rock mineralogy, and temperature influence shale fracture properties.
- Stronger wet-dry differences in clay-rich shales (Woodford and Mancos) than in carbonate-rich shale (Marcellus).
 - “Wet” fracture growth rate faster by one-order of magnitude
- Increasing temperature enhances subcritical fracturing.
- Carbonate-rich Marcellus: carbonate dissolution
 - SCI sensitive to acidic pH
 - K_{IC} independent of chemical environment
- Woodford & Mancos: clay-fluid interaction
 - K_{IC} and SCI sensitive to water content and salinity.
 - Water-weakening enhances subcritical fracturing
- Environmental effects controlled by competition between fracture growth rate and rate of rock degradation by fluid-rock interactions.

Implications

- Fracture growth strongly affected by water content variations
 - Natural fractures: lithification, diagenesis, oil-water system, gas charging
 - Engineered systems: hydraulic fracturing, EOR, CO₂ sequestration
- Higher temperature systems have higher propensity for subcritical fracture growth.
- Clay-rich rocks:
 - more sensitive to water-weakening.
 - high salinity suppresses water-weakening.
 - higher risk for seal failure with subcritical fracture growth.
- Carbonate-rich rocks:
 - more prone to subcritical fracture by pH decrease (CO₂ EOR, CO₂ sequestration, organic acids).