



Co-Optimization of  
Fuels & Engines

better fuels | better vehicles | sooner

## Fuel Property and Engine Combustion Research of the US Co-Optima Initiative

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## Tailor-Made Fuels From Production to Propulsion 5th International Conference

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Eurogress, Aachen Germany

Co-Optima Leadership Team: John Farrell (NREL), John Holladay (PNNL), Chris Moen (SNL), Robert Wagner (ORNL)



Energy Efficiency &  
Renewable Energy

US Department of Energy (DOE) Bioenergy Technologies  
Office Program Managers: Alicia Lindauer, Borka Kostova  
US DOE Vehicle Technologies Office Program Managers:  
Gurpreet Singh, Kevin Stork, Leo Breton & Michael Weismiller

# US DOE Co-Optimization of Fuels & Engines (Co-Optima): increase efficiency, diversify fuels



## Light-duty

Up to 15% fuel economy (FE) improvement\*  
Phase 1: boosted SI; Phase 2: multi-mode SI/ACI

## Heavy-duty

Up to 1-4% FE improvement (worth \$1-5B/year)\*  
Potential lower cost path to meeting next tier of criteria emissions regulations

## Fuels

Diversifying resource base  
Providing economic options to fuel providers to accommodate changing global fuel demands  
Increasing supply of domestically sourced fuel by up to 25 billion gallons/year

## Cross-cutting goals

Stimulate domestic economy  
Adding up to 500,000 new jobs  
Providing clean-energy options

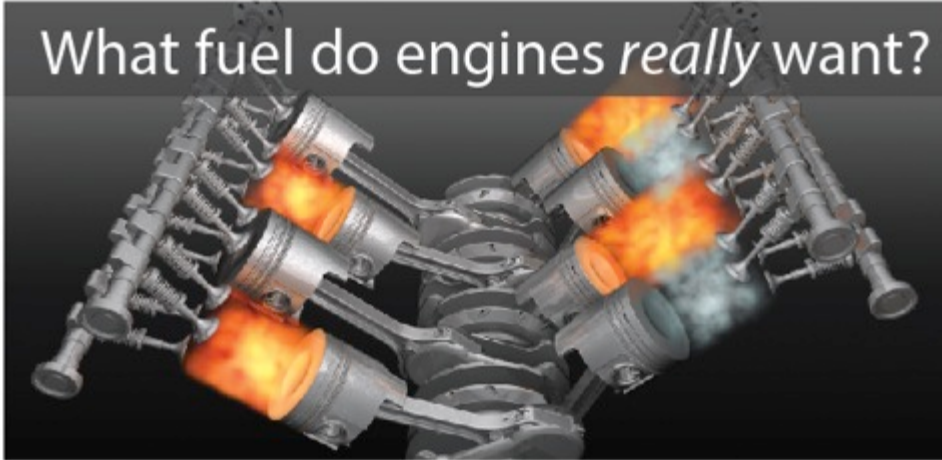
\* Beyond projected results of current R&D efforts. The team is actively engaging with OEMs, fuel providers, and other key stakeholders to refine goals and approaches to measuring fuel economy improvements



# Primary technical challenges of Co-Optima: Target fuel properties? How to make them?



What fuel do engines *really* want?



Identifying key fuel properties that impact efficiency for advanced spark ignition and compression ignition combustion approaches

What fuels *should* we make?



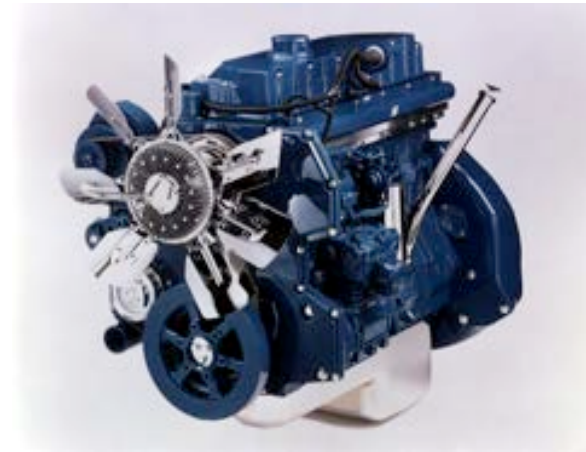
Identifying fuel formulations that provide target ranges of key fuel properties when blended with petroleum blendstocks

# Co-Optima research is structured around two guiding hypotheses on engines and fuels



## **Central Engine Hypothesis**

There are engine architectures and strategies that provide higher thermodynamic efficiencies than are available from modern internal combustion engines; new fuels are required to maximize efficiency and operability across a wide speed / load range



## **Central Fuel Hypothesis**

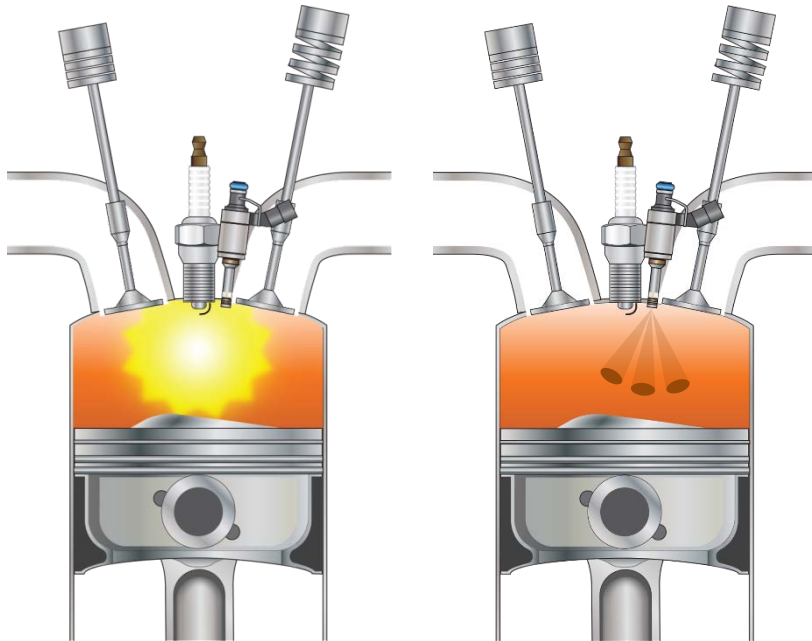
If we identify target values for the critical fuel properties that maximize efficiency and emissions performance for a given engine architecture, then fuels that have properties with those values (regardless of chemical composition) will provide comparable performance



# Co-Optima engine & fuel research proceeds along two parallel application/mode tracks



## Light-Duty



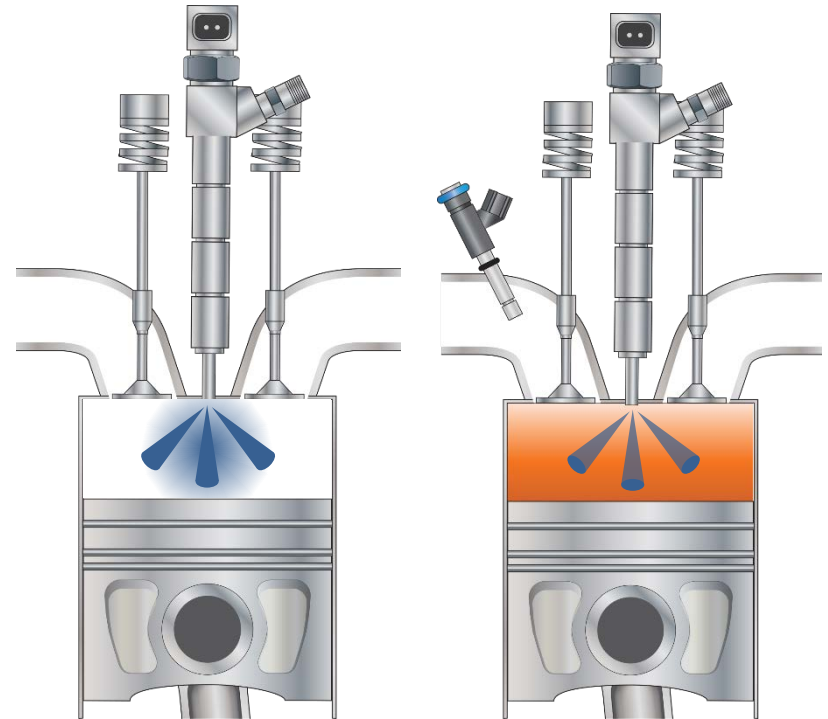
Boosted SI

Multi-mode  
SI / ACI

Near-term

Mid-term

## Medium and Heavy-Duty



Mixing  
Controlled

Kinetically  
Controlled

Near-term

Longer-term

# Three-tiered approach to screen, measure, analyze, and evaluate candidate blendstocks



## Tier 1

**> 470** blendstocks

**14** chemical families

Identify broad range of potential hydrocarbon and oxygenated blendstocks

Utilize property information on blendstocks from literature or estimates to identify Tier 2 blendstocks

## Tier 2

**41** blendstocks

**10** chemical families

Measure blendstock properties

Evaluate blendstock performance in BOBs at 10-30% blend levels

Remove candidates from list if improved data indicate they do not meet criteria

Add new candidates as our understanding improves of how fuel structure impacts key properties

## Tier 3

**8** representative\* blendstocks

**5** chemical families

Refine property measurements

Develop improved blending models

Produce/procure blendstocks in quantity for testing and validate engine and fuel economy performance

Characterize/compare benefits and identify challenges for commercial introduction

\*These blendstocks constitute a representative subset of a broader range of molecules/mixtures that meet the Tier 3 criteria



# Properties of many Tier 1 blendstock candidates are catalogued in a publicly accessible database\*



## Tier 1

> 470 blendstocks

14 chemical families

Identify broad range of potential hydrocarbon and oxygenated blendstocks

Utilize property information on blendstocks from literature or estimates to identify Tier 2 blendstocks

**Found Pure Compound** [Correct or Update this record](#)

IUPAC name: **1,4-Pentanediol**

Molecular Weight: **104.15**

Molecular Formula: **C5H12O2**

CAS#: **626-95-9**

Functional Group: **Alcohol**

Drop an image of the Structure here:

**SEARCH PROPERTIES**

Both "pure" IUPAC compounds and "methyl" Point all records with both "methyl" in the name AND a boiling point range between 0 and 14 will be searched. (IE)

Boiling: 0 - 14° finds all records with both "methyl" in the name AND a boiling point range between 0 and 14 will be searched. (IE)

Molecular Weight:  Molecular Weight

Molecular Formula:  Molecular Formula

CAS#:  CAS Number

**Safety**

LFL LEL (%)  UPL UEL (%)

Flash Point (°C)  Autoignition Temp (°C)

Peroxide Former

**Health**

Rat Oral LD50 (mg/kg)

**Properties**

Melting Point (°C)	Boiling Point (°C)	Peroxide Value	T50 (°C)
<input type="text"/>	<input type="text"/>	<input type="text"/>	<input type="text"/>
Cloud Point (°C)		IBP (°C)	T80 (°C)
<input type="text"/>		<input type="text"/>	<input type="text"/>
Density (g/cm³)	Heat of Vaporization (kJ/mol)	FBP (°C)	Surface Tension (dynes/cm)
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Viscosity (cSt)	Vapor Pressure (kPa)	Corrosion	PMI
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MON	RON	Lubricity	
<input type="text"/>	<input type="text"/>	<input type="text"/>	
UNF	DCN	Stability	Functional Group
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Critical Pressure (kPa)	Critical Temperature (K)	Oxidation Stability	Thermal Stability
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Acentric Factor	Acid Value	Water Solubility (mg/L)	Dispersion
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\* Available at: <https://fuelsdb.nrel.gov/fmi/webd#FuelEngineCoOptimization>

# 41/470 candidate blendstocks passed through Tier 1 screening for boosted SI engines



- Tier 1 screening applies criteria based on boiling point, melting point, solubility, corrosion, toxicity, fuel handling safety, biodegradation, and autoignition characteristics (e.g., RON for boosted SI)

Alcohols (9)	
1	Methanol
2	Ethanol
3	1-Propanol
4	Isopropanol
5	1-Butanol
6	2-Butanol
7	Isobutanol
8	2-Methylbutan-1-ol
9	2-Pentanol

Ethers	
10	Anisole

Esters (13)	
11	Methyl acetate
12	Methyl butanoate
13	Methyl pentanoate
14	Methyl isobutanoate
15	Methyl-2-methylbutanoate

Esters (13)	
16	Ethyl acetate
17	Ethyl butanoate
18	Ethyl isobutanoate
19	Isopropyl acetate
20	Butyl acetate
21	2-Methylpropyl acetate
22	3-Methylpropyl acetate
23	mixed esters

Ketones (9)	
24	2-Butanone
25	2-Pentanone
26	3-Pentanone
27	Cyclopentanone
28	3-Hexanone
29	4-Methyl-2-Pentanone
30	2,4-Dimethyl-3-Pentanone
31	3-Methyl-2-butanone
32	Ketone mixture

Furans	
33	2,5-Dimethylfuran/2-methylfuran

Branched alkanes	
34	2,2,3-Trimethylbutane

Alkenes	
35	Diisobutylene

Multicomponent mixtures (6)	
36	Methanol-to-gasoline
37	Ethanol-to-gasoline
38	Bioreformate via multistage pyrolysis
39	Bioreformate via catalytic conversion of sugar
40	Mixed aromatics via catalytic fast pyrolysis
41	Aromatics and olefins via pyrolysis-derived sugars



# The “merit function” is an algebraic expression for determining what fuel properties engines want



Project Lead: Paul Miles, Sandia National Laboratories

The overall engine and emissions-control system thermal efficiency can be expressed as a product of sub-efficiencies

$$\eta_{th} = \eta_{ideal} * \eta_{glh} * \eta_{comb} * \eta_{pump} * \eta_{ht} * \eta_{emiss} \dots$$

$$\eta_{ideal} = 1 - \frac{1}{CR^{\gamma-1}}$$

$\eta_{glh}$  = combustion phasing (“degree of constant V combustion”)

$\eta_{comb}$  = combustion efficiency

$\eta_{pump}$  = pumping losses

$\eta_{ht}$  = heat transfer losses

$\eta_{emiss}$  = emission control losses

# Fuel properties play roles in many of the sub-efficiency terms of the merit function



Project Lead: Paul Miles, Sandia National Laboratories

Since we are interested in relative efficiency, we can differentiate to get:

$$\frac{d\eta_{th}}{\eta_{th}} = \frac{d\eta_{CR}}{\eta_{CR}} + \frac{d\eta_{\gamma}}{\eta_{\gamma}} + \frac{d\eta_{glh}}{\eta_{glh}} + \frac{d\eta_{comb}}{\eta_{comb}} + \frac{d\eta_{pump}}{\eta_{pump}} + \frac{d\eta_{ht}}{\eta_{ht}} + \frac{d\eta_{emiss}}{\eta_{emiss}} + \dots$$

Diagram illustrating the differentiation of the merit function (relative efficiency) into sub-efficiency terms, with color-coded arrows indicating associated fuel properties:

- $\frac{d\eta_{CR}}{\eta_{CR}}$  (blue circle) points to **RON, octane sensitivity, HOV**
- $\frac{d\eta_{glh}}{\eta_{glh}}$  (green circle) points to **Flame Speed**
- $\frac{d\eta_{pump}}{\eta_{pump}}$  (red circle) points to **HOV**
- $\frac{d\eta_{emiss}}{\eta_{emiss}}$  (purple circle) points to **PMI,  $T_{c,90}$**

How can we quantify these in terms of fuel properties for each combustion mode?

# Boosted SI merit function quantifies engine & fuel effects on percentage change in efficiency



Project Lead: Paul Miles, Sandia National Laboratories

- First term is based on the Octane Index (OI), where K is indicative of the engine operating condition
  - K=0: “Research Octane Number” (RON) test condition (cold)
  - K=1: “Motor Octane Number” (MON) test condition (hot)
  - K<0: “beyond RON,” e.g., boosted spark ignition (SI)
  - K>1: “beyond MON,” e.g., advanced compression ignition

$$Merit [\Delta\%] = \frac{(RON_{mix} - 91)}{1.6} - K \frac{(S_{mix} - 8)}{1.6}$$

$$OI = RON - K \cdot S$$

$$= RON - K \cdot (RON - MON)$$

$$+ \frac{0.085[ON / kJ / kg] \cdot ((HoV_{mix} / (AFR_{mix} + 1)) - (415[kJ / kg] / (14.0[-] + 1)))}{1.6}$$

$$+ \frac{((HoV_{mix} / (AFR_{mix} + 1)) - (415[kJ / kg] / (14.0[-] + 1)))}{15.2} + \frac{(S_{Lmix} - 46[cm / s])}{5.4}$$

$$- H(PMI_{mix} - 1.6)[0.7 + 0.5(PMI_{mix} - 1.4)] + 0.008^{\circ}C^{-1}(T_{c,90,conv} - T_{c,90,mix})$$

# Boosted SI fuel matrix designed to determine if octane index can predict engine efficiency limits

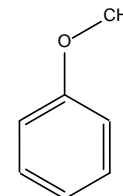


Project Lead: Jim Szybist, Oak Ridge National Laboratory

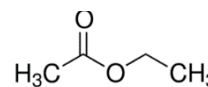
	Co-Optima "Alkylate"	Co-Optima "Aromatic"	Co-Optima "E30"	"Tier III" E10 EEE	25 mol% Methyl Butyrate Blend "MB"	25 mol% Ethyl Acetate Blend "EA"	25 mol% "Anisole" Blend
RON	97.9	98	98.3	91.8	98.1	98.5	98.8
MON	96.7	87.3	87.6	84.2	90.9	92.6	90.5
S	1.2	10.7	10.7	7.6	7.2	5.9	8.3
Aromatic	0	35.8	8.1	22.6	23 mol%	23 mol%	23 mol%
Saturates	100	65	57.1	71.2	47 mol%	47 mol%	47 mol%
Olefins	0	4.2	5	5.2	5 mol%	5 mol%	5 mol%
Ethanol	0	0	29.95	9.8	0	0	0
T10	93.1	59.4	60.7	54.6	-	-	-
T50	100.3	108.1	74.3	89.9	-	-	-
T90	105.9	157.9	155.2	157.9	-	-	-
C (wt%)	83.75	87.22	74.78	82.63	79.37	79.18	83.95
H (wt%)	15.80	13.12	13.79	13.66	12.89	12.85	12.23
O (wt%)	0	0	11.19	3.71	7.74	7.97	3.82

Fuels: Co-Optima "core" fuels, tier III cert gasoline, and 3 bio-blendstock candidates

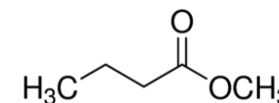
**Anisole**  
RON = 103  
S = 12



**Ethyl Acetate**  
RON = 118  
S = -2



**Methyl Butyrate**  
RON = 107  
S = 2



Operating Conditions: Constant fueling rate (14.5-19.0 bar IMEP), varying intake temperature, backpressure, and EGR

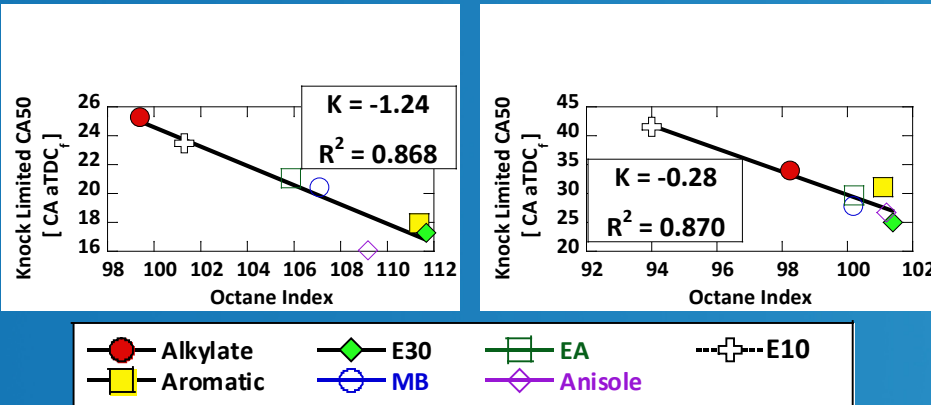
	Sweep 1	Sweep 2	Sweep 3	Sweep 4	Sweep 5	Sweep 6	Sweep 7	Sweep 8
Intake T [°C]	35	35	35	35	90	90	90	90
Manifold DP [kPa]	>20	8	8	8	>20	8	8	8
EGR [%]	0	0	10	20	0	0	10	20



# Boosted SI: For $\phi \approx 1$ , octane index correlates well with knock-limited combustion phasing



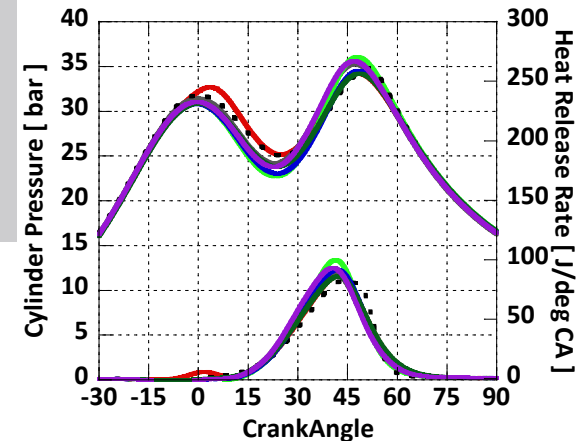
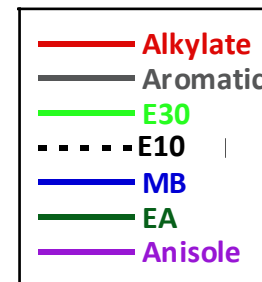
Project Lead: Jim Szybist, Oak Ridge National Laboratory



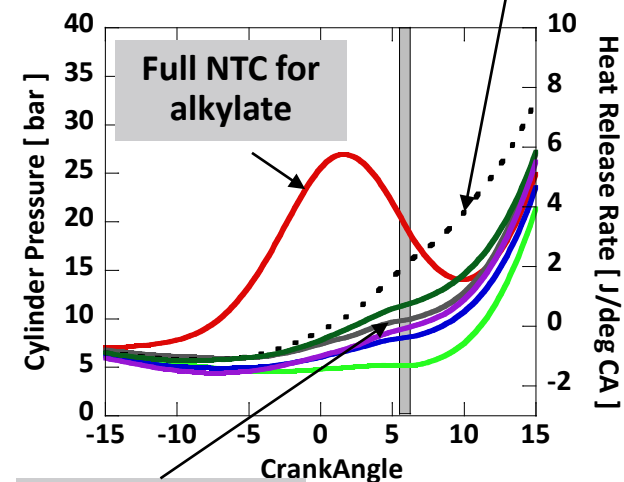
$$OI = RON - K * S$$

- Octane index includes the two most impactful terms in the merit function
- Experiments confirm that OI correlates with knock-limited phasing much better than AKI, RON, or MON
- Despite good correlation coefficients, significant outliers were observed
  - Anisole fuel blend generally out-performs OI prediction (earlier knock-limited CA50)
  - Aromatic fuel blend under-performs with high intake manifold temperature

Focusing on retarded phasing, significant differences in early combustion phases are apparent



Pre-Spark Heat Release (PSHR) for E10 Fuel is between alkylate & aromatic



# Premixed ACI: at $\phi = 0.4$ , different CA50 for fuels with same RON & S; “O<sub>2</sub>” OI analysis works well



Project Lead: John Dec, Sandia National Laboratories

## Advanced Compression Ignition (ACI)

- Designed fuel test matrix with five fuels with RON  $\approx 98$ , four with S  $\approx 10.5$ , one with S  $\approx 1$

Co-Optima Core Fuels	Alkylate	E30	Aromatic	Olefin	Cyclo- alkane
RON	98.0	97.4	98.1	98.2	98.0
MON	96.6	86.6	87.8	88.0	87.1
S	1.4	10.8	10.3	10.2	10.9
Aromatics	0.7	13.8	39.8	13.4	33.2
n+i-Paraffin	98.1	40.5	46.2	56.4	40.6
Cycloalkane	0.0	7.0	8.0	2.9	24.2
Olefins	0.1	6.0	4.5	26.5	1.6
Ethanol	0.0	30.4	0.0	0.0	0.0

# Premixed ACI: at $\phi = 0.4$ , different CA50 for fuels with same RON & S; "O<sub>2</sub>" OI" analysis works well



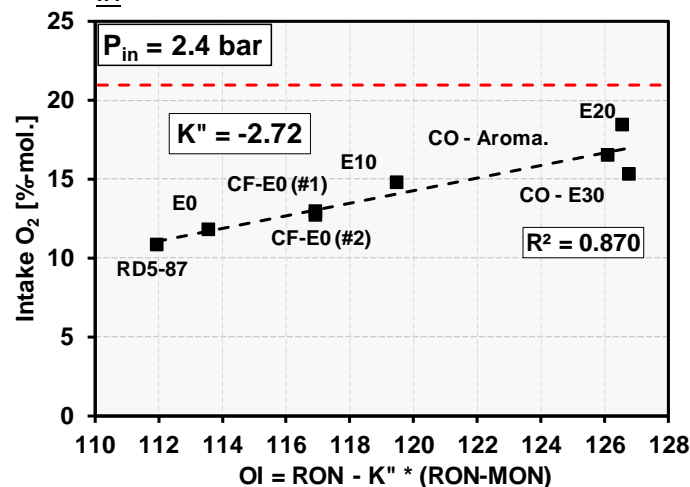
Project Lead: John Dec, Sandia National Laboratories

## Advanced Compression Ignition (ACI)

- Designed fuel test matrix with five fuels with RON  $\approx 98$ , four with S  $\approx 10.5$ , one with S  $\approx 1$
- $P_{in} = 1.0$  bar: Surprisingly, reactivity varies among matched RON&S fuels: E30 >> Aromatic

- For LTGC at  $P_{in} = 1$  bar with these fuels, Octane Index (OI) gives poor correlation ( $R^2 = 0.536$ )
- RON and MON appear insufficient for specifying fuel reactivity for lean LTGC ( $\phi = 0.4$ ) at this cond.
- Perhaps this is because E30 is less  $\phi$ -sensitive, or differences in HOV  $\Rightarrow$  Further studies are planned

- $P_{in} = 2.4$  bar: Try OI" based on intake O<sub>2</sub>, since

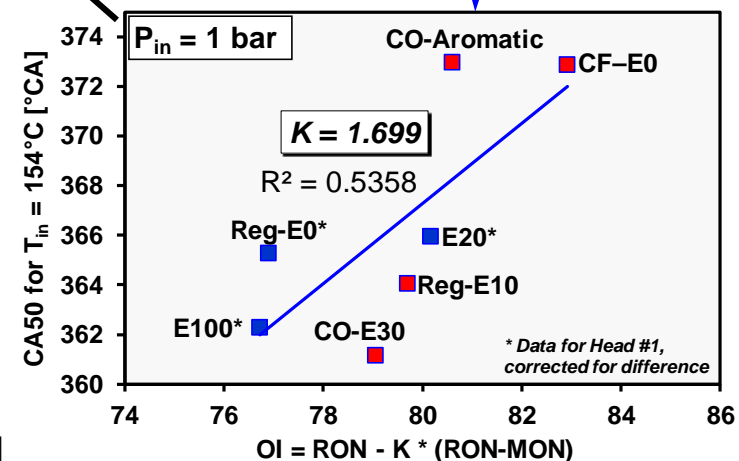
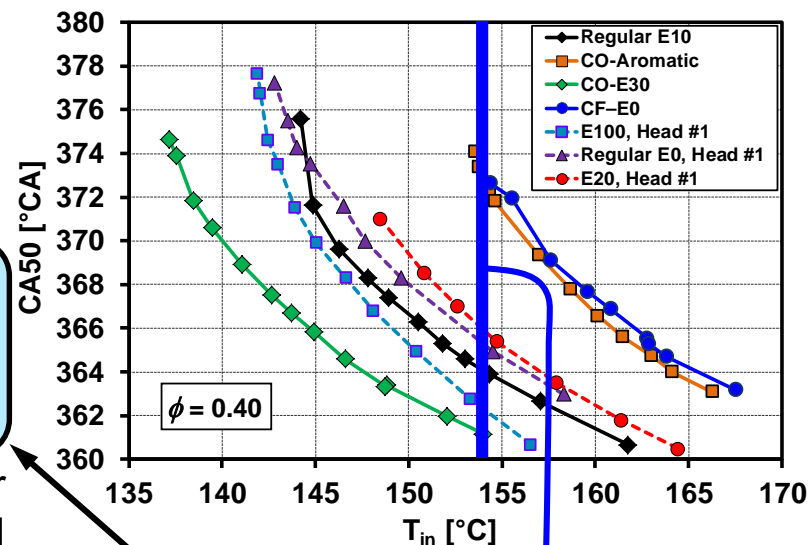


$T_{in} = 60^\circ\text{C}$  for all

- OI" correlates fuels fairly well at  $P_{in} = 2.4$  bar,  $R^2 = 0.870$

- Improved understanding of this intake-O<sub>2</sub> based OI" is needed

Required  $T_{in}$  for  $P_{in} = 1.0$  bar, Indicates Reactivity



# Premixed ACI: Reactivity of E30 (high RON & S) similar to E0, correlates with ITHR & $\phi$ -sensitivity



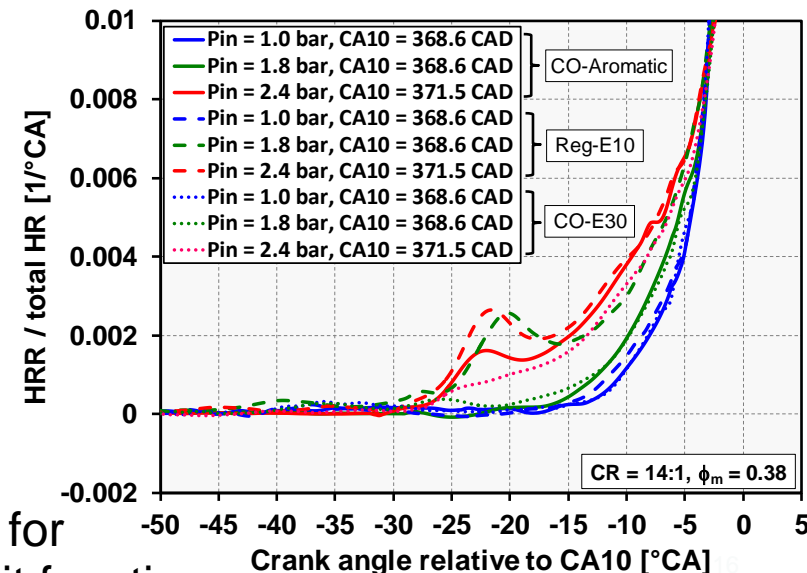
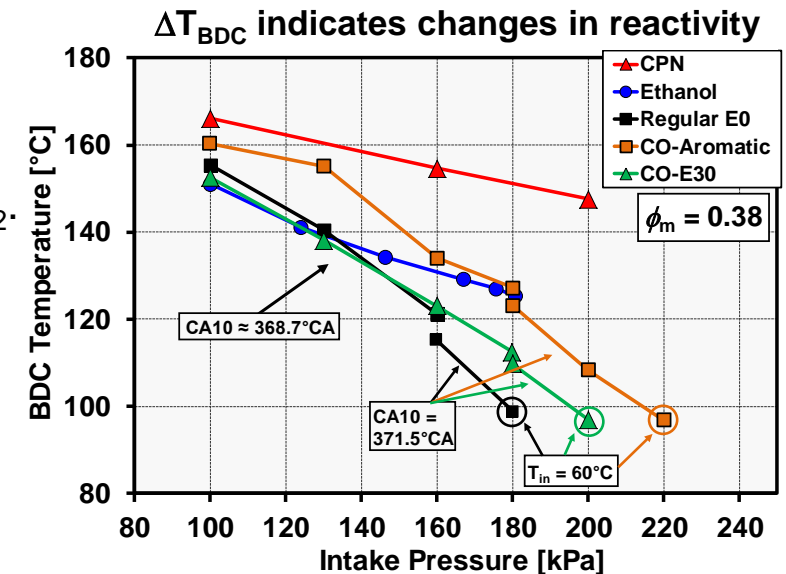
Project Lead: John Dec, Sandia National Laboratories

## Reactivity Changes w/ Boost

- Increased fuel autoignition reactivity with boost is a key challenge for both LTGC and SI
  - LTGC: High EGR required for CA50 control limits  $O_2$ .
  - SI: Increased knock propensity limits CR
- Despite higher RON & S, E30 has similar reactivity to Reg-E0 for  $P_{in} = 1.0 - 1.6$  bar  $\Rightarrow$  Somewhat less reactive for higher  $P_{in}$
- Higher RON & S aromatic fuel is much less reactive than Reg-E0, esp. at  $P_{in} \geq 1.8$  bar
  - At  $P_{in} = 1.8$  bar, aromatic & E30 have lower ITHR than Reg-E10  $\Rightarrow$  may affect reactivity trends
  - Also agrees with lower  $\phi$ -sensitivity (for PFS)

## Future Work:

- Evaluate E30  $\phi$ -sensitivity & high load behavior
- Evaluate the other three fuels in test matrix  $\Rightarrow$  High-Olefin, High-Cycloalkane, & Alkylate
- Investigate Co-Optima fuels with good potential for full-time LTGC-ACI engines  $\Rightarrow$  Support ACI merit function





# Reactivity Controlled Compression Ignition (RCCI): LD multi-cyl. metal & HD single-cyl. optical engines



Project Lead: Scott Curran, Oak Ridge National Laboratory

## Motivation for Using RCCI in ACI Engines

On-the-fly in-cylinder mixing of two fuels =  
**Control of combustion phasing & HRR**

- Global octane number adjusted by fuel ratio
- Reactivity stratification by injection timing

## RCCI Challenges

Peak pressure rise rate (PPRR) limits high load

- E30 extends limit  $\Rightarrow$  not well understood

Incomplete combustion at lowest loads

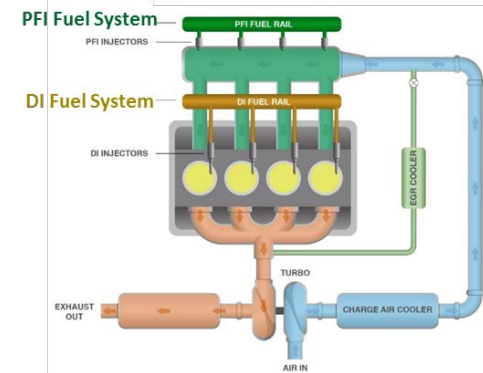
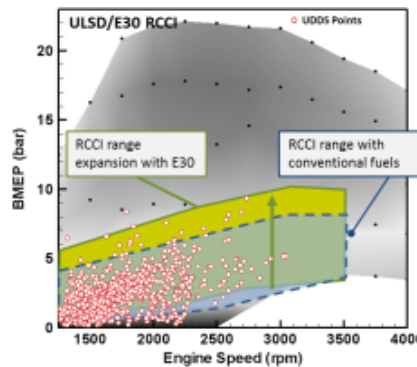
- Reasons are unclear

## Approach for RCCI Work

- Use ORNL multi-cylinder metal engine to identify key fuel-property & operating-condition combinations where an improved understanding is required
- Use SNL single-cylinder optical engine to image in-cylinder mixing, ignition, and combustion processes at these conditions

## ORNL Metal Engine

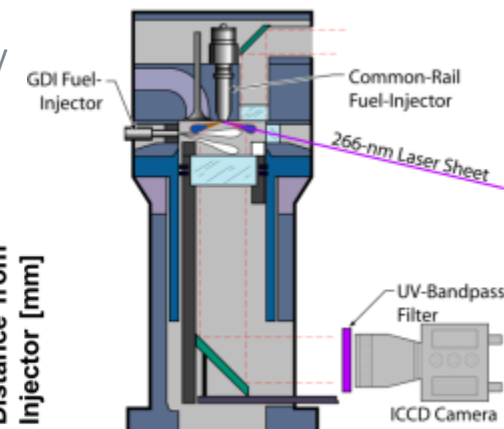
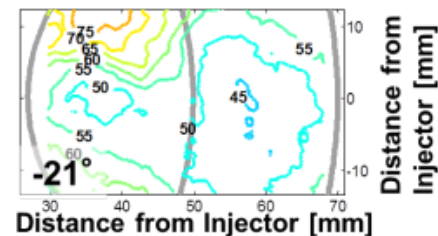
- Multi-cylinder light-duty diesel engine (PFI + DI)
- Transient capable + emissions characterization



Project Lead: Mark Musculus, Sandia National Laboratories

## SNL Optical Engine

- Single-cylinder heavy-duty diesel engine (GDI + DI)
- Image combustion & in-cylinder mixing (PRF)

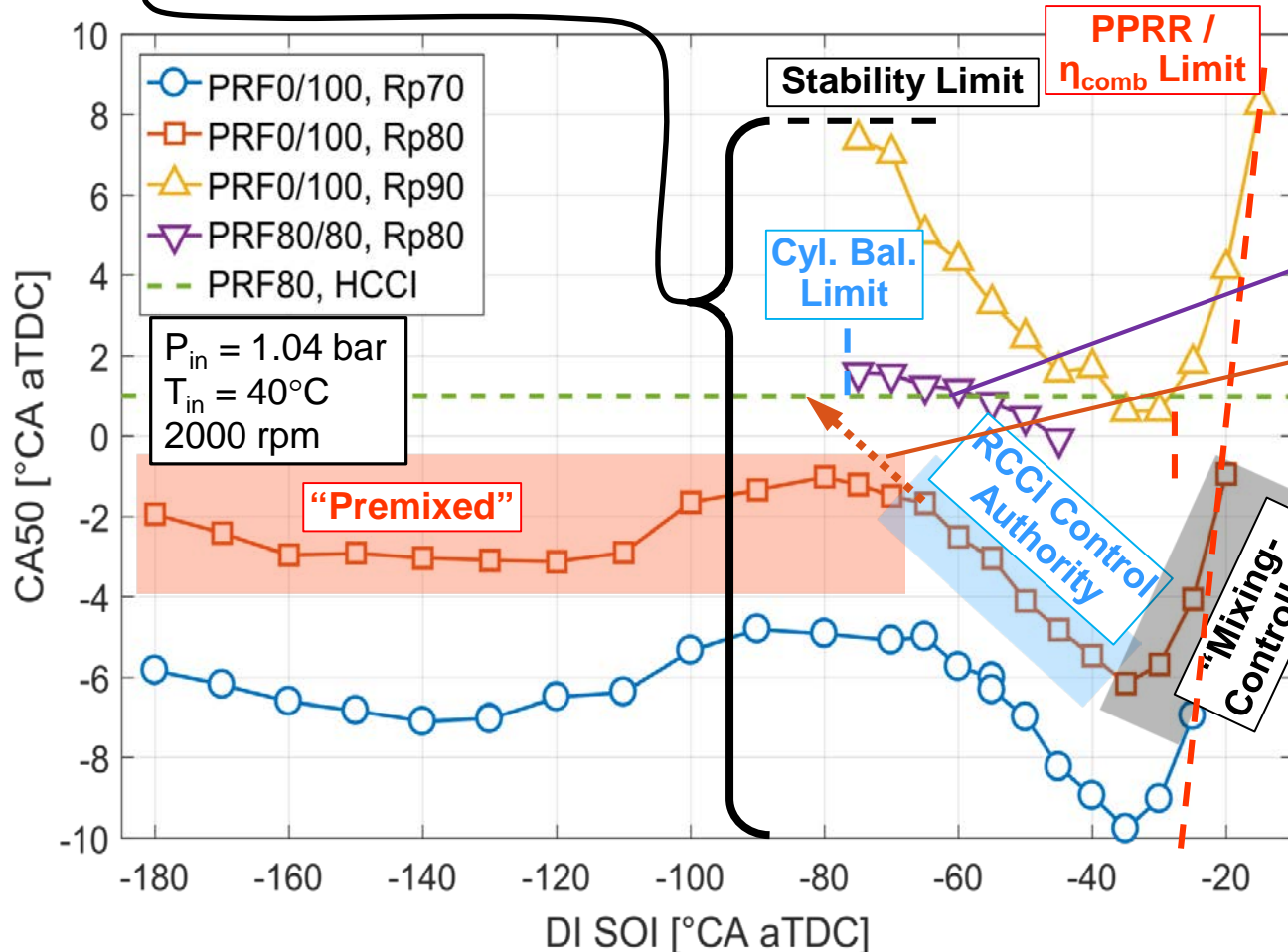


# RCCI: At constant PRF, CA50 control authority limits approach premixed & mixing-controlled



Project Lead: Scott Curran, Oak Ridge National Laboratory

- Use PRFs (iso-octane & n-heptane): similar physical properties, different reactivity
  - DI SOI from -70 to -35 °CA aTDC have characteristic RCCI CA50 control authority
  - Control authority is limited by constant PRF in each sweep
    - > Varying PRF by changing premixed ratio (Rp) would yield much greater CA 50 control



- Two limits of control authority range:

## 1. "Premixed"

- Premixed + DI PRF80 reaches premixed "HCCI"
- Premixed PRF100 + DI PRF0 does not reach premixed "HCCI" CA50

- > Wall wetting?
- > Incomplete mixing?

## 2. "Mixing-Controlled"

- Late DI SOI: control authority trend reverses
  - > Fuel-rich mixing-controlled combustion?

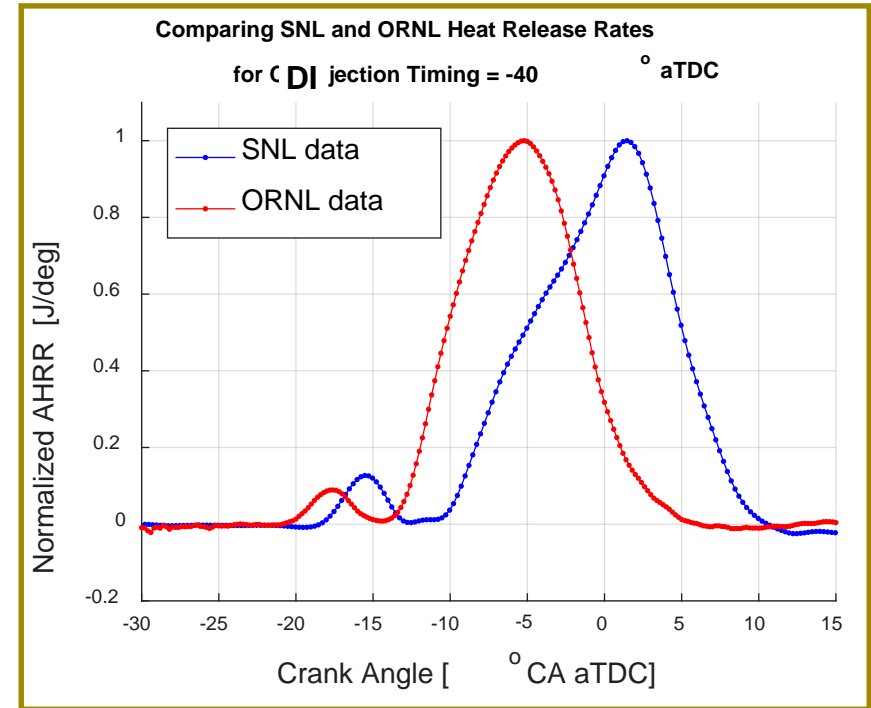
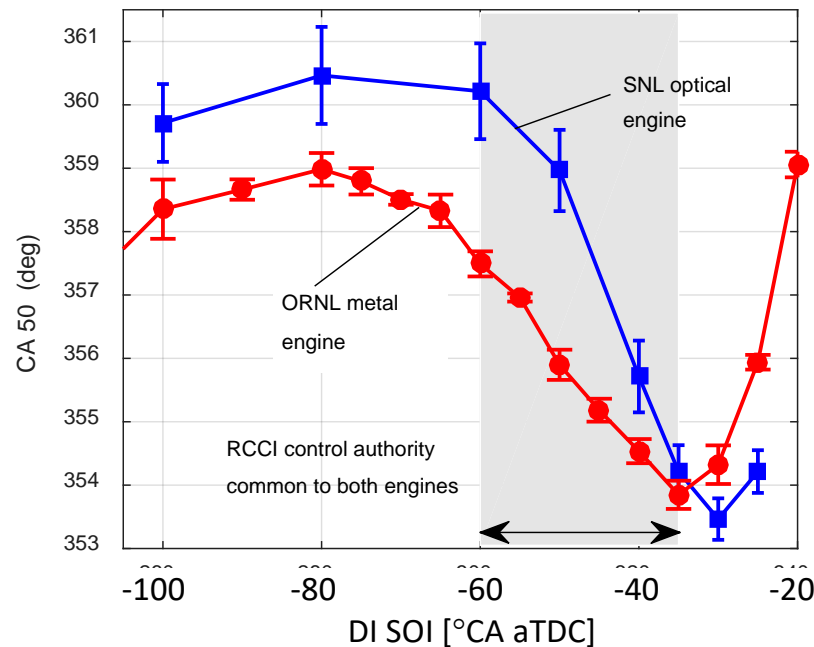
Gain insight from optical diagnostics

# RCCI: Good matching of combustion phasing & control authority in optical & metal engines



Project Lead: Mark Musculus, Sandia National Laboratories

The mid-point of combustion heat release (CA50) depends on the injection timing of high-reactivity (PRF 0) fuel from the common rail (CR) DI injector

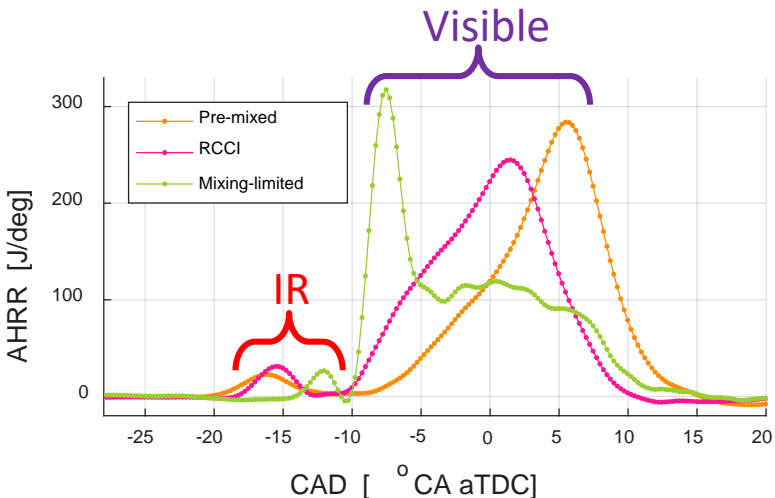
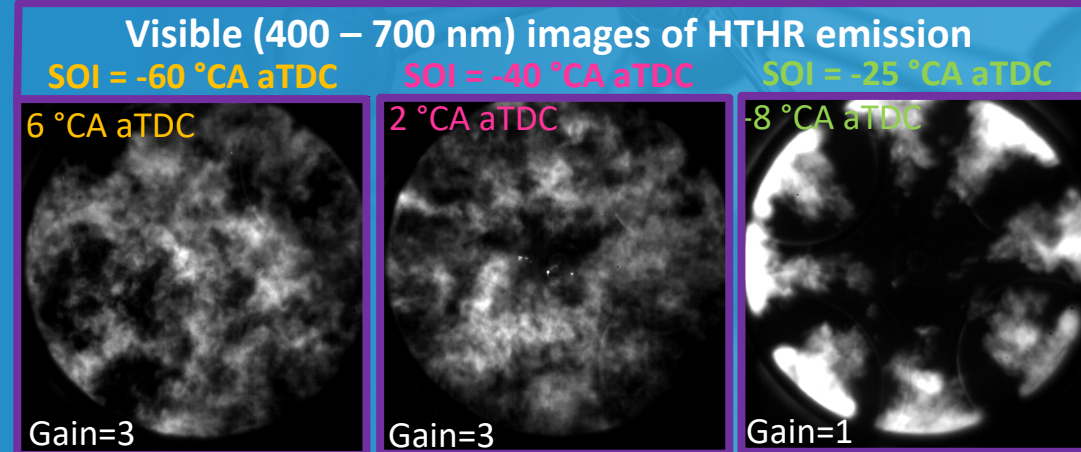
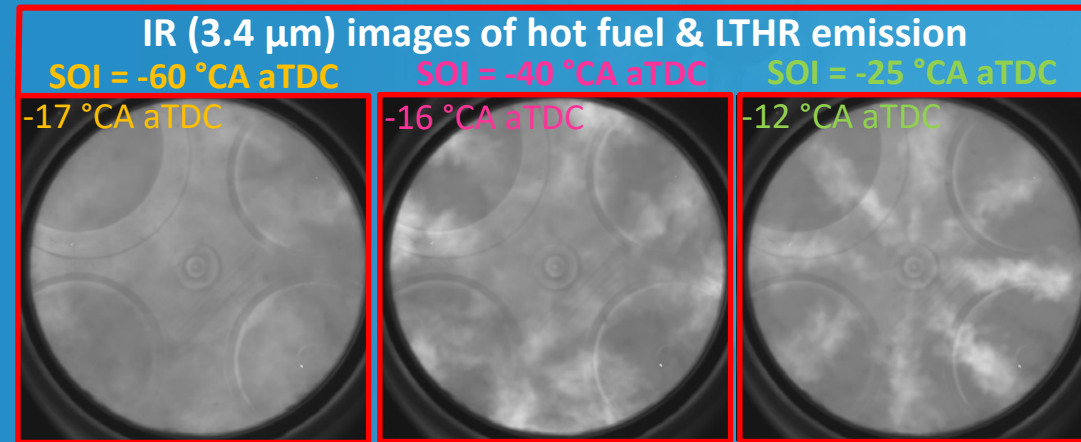
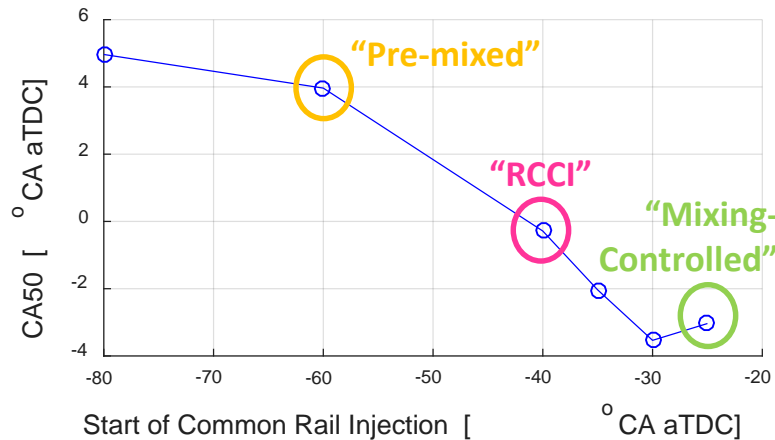


Heat release phasing is shifted, but the 2 engines yield the same characteristic shapes

- Matching SNL HD optical engine with ORNL LD metal engine: **1. charge-gas  $\rho$  &  $T$  @ mid-control-authority DI injection, 2. premixed iso-octane (80%), 3. global  $\Phi$  (0.35)**
- Even with different engine displacement (heavy-duty vs light-duty), compression ratios, and piston geometry, the combustion characteristics are similar, with three CA50 regimes (pre-mixed, RCCI, & mixing-controlled) and similar heat release shapes

# Fundamental Stratified ACI (SNL, Musculus): Structure in IR & visible images (=incomplete mixing?), bright @ late DI (=rich?)

Project Lead: Mark Musculus, Sandia National Laboratories



- Structure in IR imaging of 1<sup>st</sup>-stage and visible imaging of 2<sup>nd</sup>-stage ignition at all conditions – incomplete mixing?
- Brightening jet structure in visible imaging indicates transition to richer mixtures

## Next steps

- Follow up with laser-sheet mixing diagnostics to quantify mixing effects for these PRFs
- Image combustion phenomena for ORNL fuels with different physical properties



# Mixing-Controlled Compression Ignition (MCCI): Ducted fuel injection for high efficiency, low soot



Project Lead: Chuck Mueller, Sandia National Laboratories

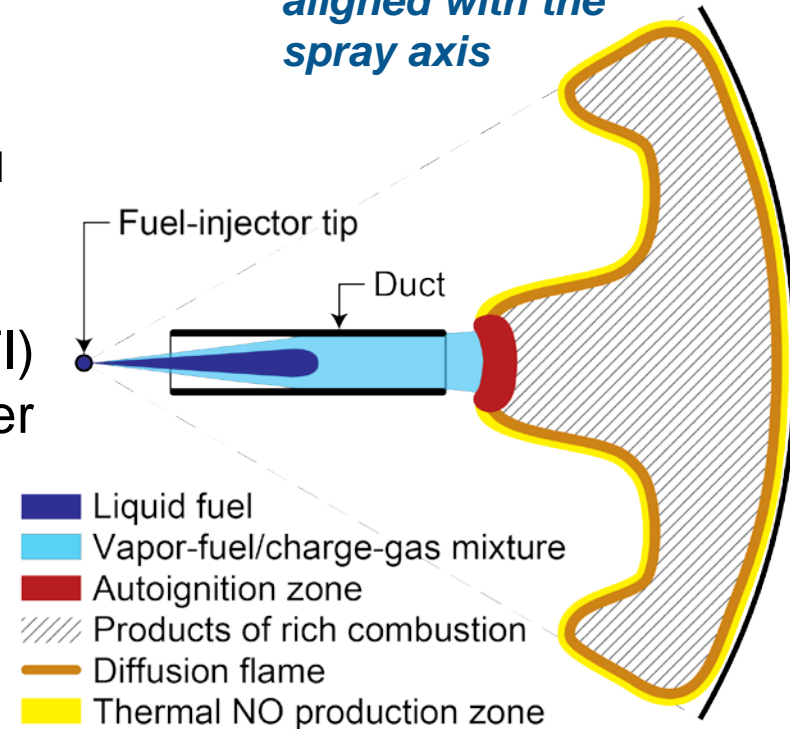
- Mixing-controlled CI combustion is desirable for many reasons

- > Inherently high efficiencies, low HC & CO emissions
- > Ignition timing easily controlled by injection timing
- > Inherently fuel-flexible (cetane # is key fuel parameter)
- Soot is a barrier to fully achieving the above benefits
  - > Soot is a potent toxin
  - > 2<sup>nd</sup> only to CO<sub>2</sub> as a climate-forcing species
  - > Limits amount of EGR possible for NO<sub>x</sub> control
  - > Aftertreatment is expensive, has efficiency penalties (backpressure, regeneration)

- **Approach:** Use Ducted Fuel Injection (DFI) to make richest autoigniting mixtures leaner

- **Effective at lowering soot** (next slide)
- Geometrically & conceptually simple
- Tolerant to dilution for NO<sub>x</sub> control
- Synergistic with Co-Optima oxygenated fuels, but does not require oxygenation
- Might increase comb. efficiency by limiting over-mixing at spray periphery

**DFI Concept:**  
*Inject fuel down a  
small tube/duct  
aligned with the  
spray axis*

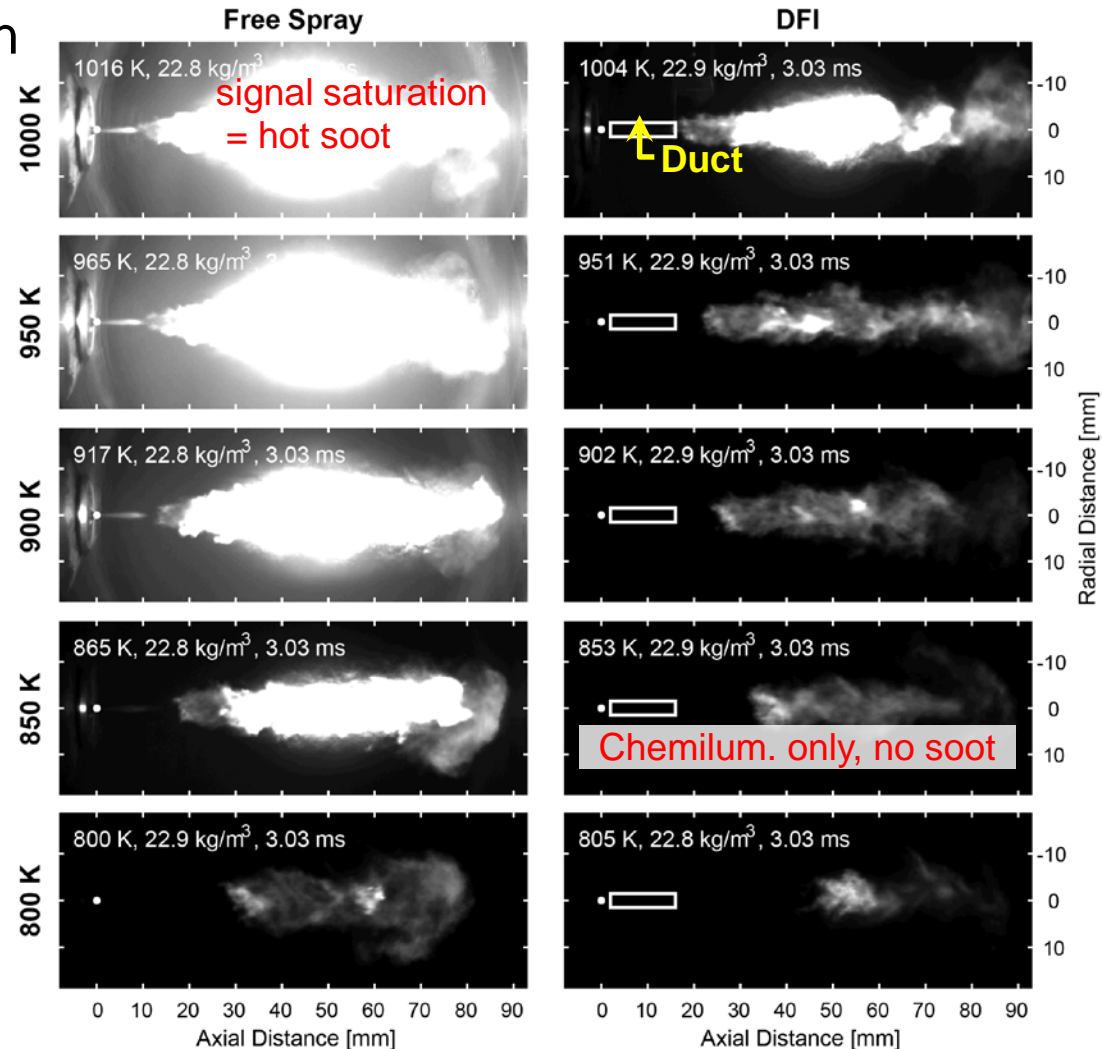
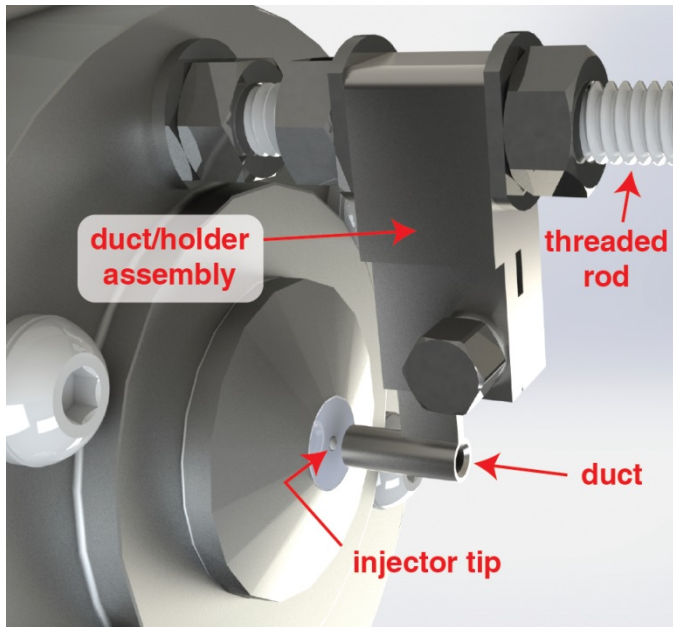


# MCCI: Initial DFI data show considerable soot reduction even with non-oxygenated fuel, no EGR



Project Lead: Chuck Mueller, Sandia National Laboratories

- Ducted Fuel Injection (DFI) in Sandia constant-volume combustion vessel
  - 90  $\mu\text{m}$  orifice diameter
  - 1500 bar injection pressure
  - 21 mol% oxygen (no EGR)
  - n-dodecane fuel (not oxygenated)

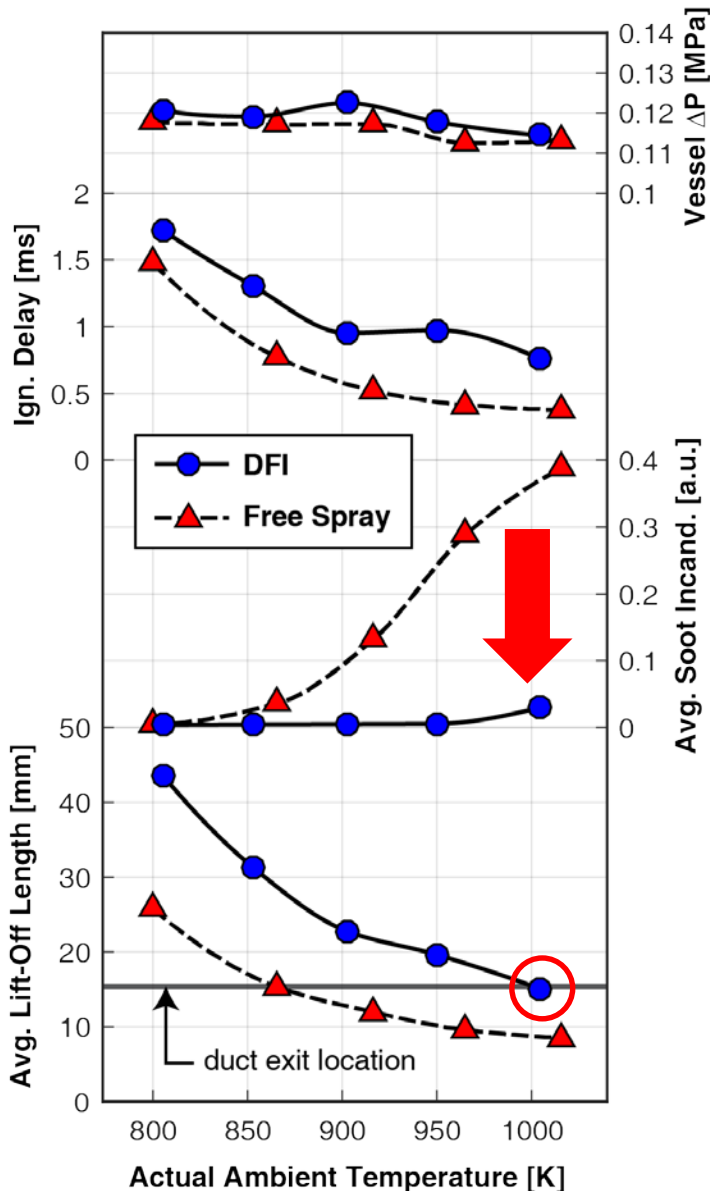


**DFI is effective at lowering or preventing soot incandescence over a range of temperatures**

# MCCI: DFI reduces in-cylinder soot by factor of ~10, longer lift-off, higher pressure rise



Project Lead: Chuck Mueller, Sandia National Laboratories

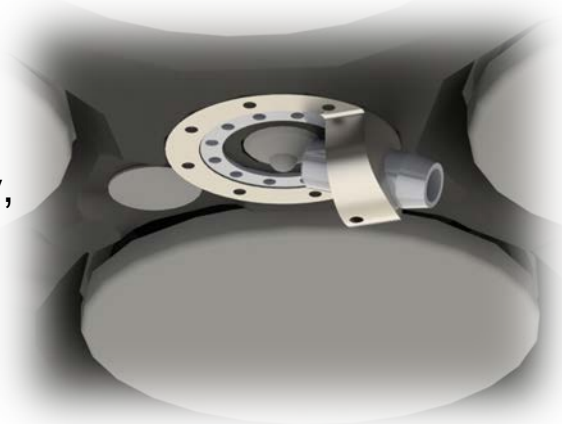


- Effects of DFI on combustion observables

- Lift-off lengths increase with DFI
  - > Flame anchors to duct exit at 1000 K
  - > Longer ignition delay could increase noise
- Soot incandescence decreases by 10×
  - > Similar for quantitative in-cylinder soot
- Total pressure rise ( $\Delta P$ ) in vessel is slightly, but consistently larger with DFI
  - > Higher combustion efficiency?
  - > Reduce over-mixing at spray periphery?

- Future Work:

- Optical engine tests
  - > emissions, efficiency, & fuel effects
  - > Vertical-sheet LII
- Develop merit function

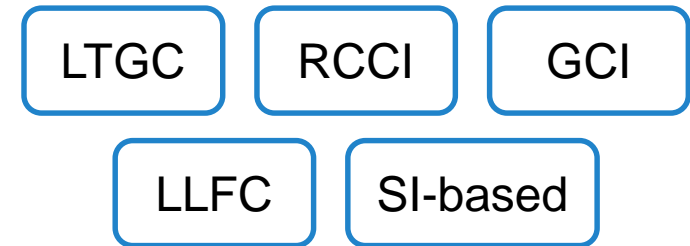


# ACI Merit Function: Quantify how fuel properties & engine conditions enable high-efficiency ACI



Project Lead: Andrew Ickes, Argonne National Laboratory

- ACI merit function: quantify enabling engine conditions & fuel properties
  - Boosted SI merit function quantifies efficiency effects to guide fuel and engine co-optimization
  - ACI approaches already have high efficiency; quantify enabling fuel & engine effects to guide co-optimization
- Will synthesize results from multiple Co-Optima ACI approaches
  - > Highlight key enabling fuel properties for each combustion approach
  - > Relate fuel properties to engine features that affect operating range and efficiency
- Design engine and fuel experiments to inform merit function(s) across the suite of ACI combustion concepts



(Industry solutions incorporated based on published literature and industry support/guidance)

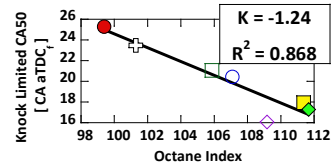
Identify enabling fuel properties and engine features and quantify their effects for each ACI approach

Specific focus on properties/ranges that preclude each ACI approach

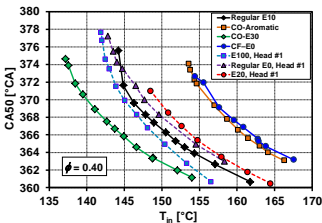
Property guidance and merit function to direct ACI engine & fuel co-optimization



# Summary: US DOE Co-Optimization of Fuels & Engines (Co-Optima) Initiative

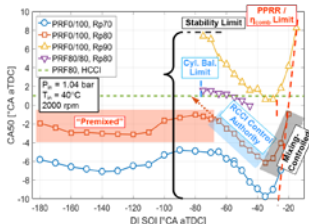


SI MF { Blendstock screening focuses on optimal fuel properties  
•SNL lead  
•Miles { SI merit function quantifies fuel property effects on efficiency

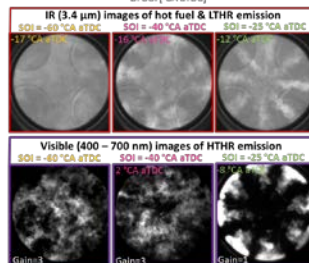


SI { At  $\phi \approx 1$ , octane index correlates well with knock-limited CA50  
•ORNL  
•Szybist { Large pre-spark heat release variations among fuels tested

ACI { At  $\phi = 0.4$ , same RON & S, diverging CA50; “O2” OI works well  
•SNL  
•Dec { E30 reactivity similar to E0, correlates w/ ITHR &  $\phi$ -sensitivity

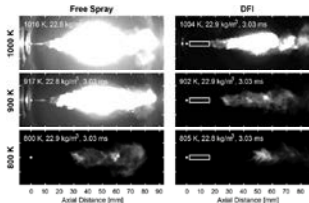


RCCI { Const. PRF control-authority limits = premixed, mixing-control  
•ORNL  
•Curran { Wall-wetting/incomplete-mixing may narrow premixed limit



RCCI { Matched optical/metal engine comb. phasing & control auth.  
•SNL  
•Musculus { Image struct. (=incomplete mixing?), bright @ late DI (=rich?)

MCCI { DFI reduces in-cyl. soot 10X w/ non-oxygenated fuel, no EGR  
•SNL  
•Mueller { Longer lift-off & ignition delay (noise?), higher  $\Delta P$  (efficiency?)



ACI MF { Identify/quantify fuel properties enabling high-efficiency ACI  
•ANL lead  
•Ickes { Merit function to guide ACI engine & fuel co-optimization

# Acknowledgement



- Portions of the work on boosted SI merit function development, premixed ACI, Stratified ACI (RCCI), and MCCI were performed at the Combustion Research Facility, Sandia National Laboratories, Livermore, CA.

Sandia National Laboratories is a multi-mission laboratory managed and operated by National Technology and Engineering Solutions of Sandia, LLC, a wholly owned subsidiary of Honeywell International, Inc., for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-NA0003525.

# Backup Slides



# Tiered Blendstock Identification



## Tier 1

> 470 blendstocks

14 chemical families

Identify broad range of potential hydrocarbon and oxygenated blendstocks

Utilize property information on blendstocks from literature or estimates to identify Tier 2 blendstocks

Hydrocarbons  
Normal paraffins  
Iso-paraffins  
Cycloparaffins  
Olefins  
Aromatics  
Multi-ring aromatics

Alcohols

Furans

Ethers

Carbonyls

Ketones

Aldehydes

Esters

Volatile fatty acid esters

Fatty esters

Carboxylic Acids

Present in commercial fuels

Not present in commercial fuels

A major goal of Co-Optima is to conduct a comprehensive and consistent survey of blendstock options:

What blendstocks are able to increase boosted SI performance?

# Tiered Blendstock Identification



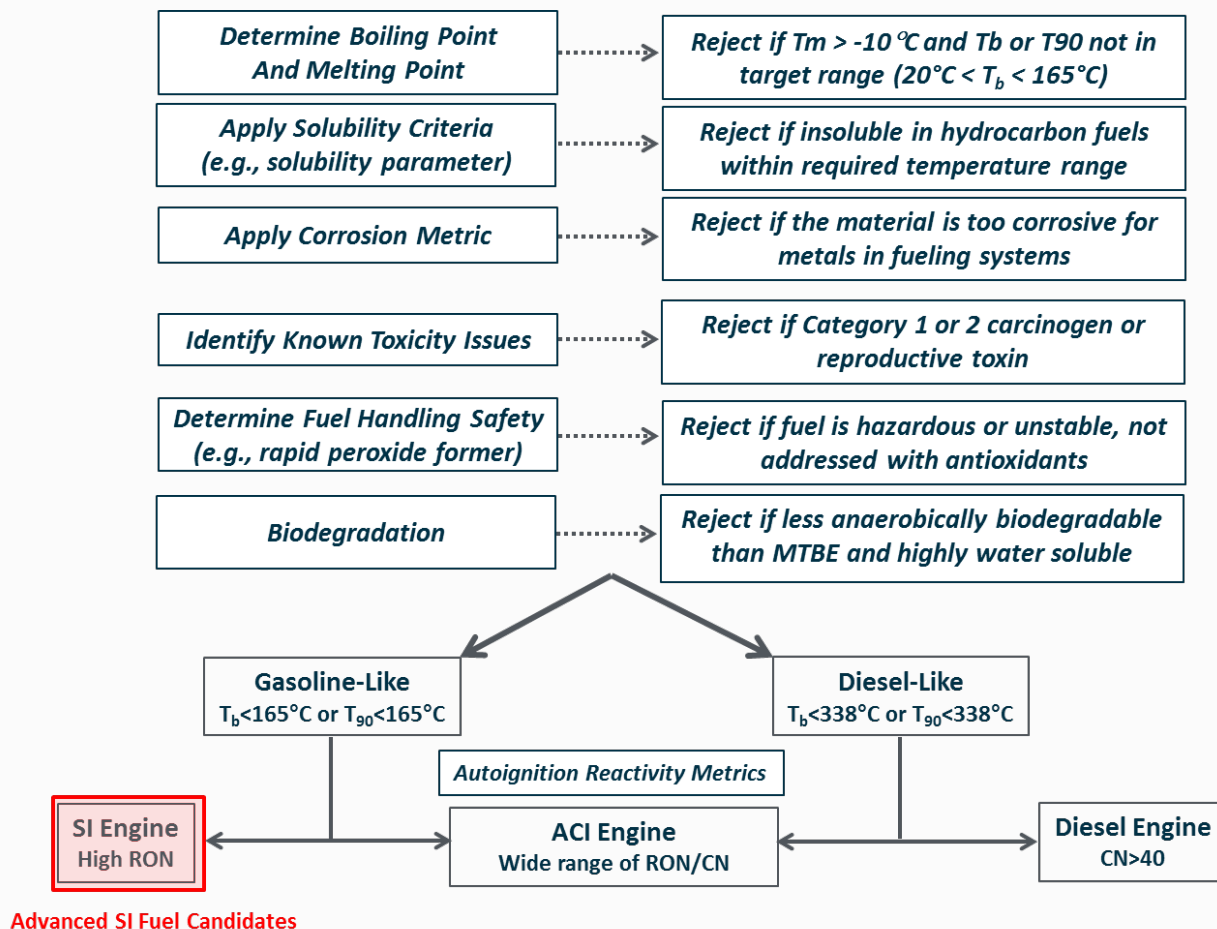
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# Tier 1: Blendstock Screening



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Multi-ring aromatics

Alcohols

Furans

Ethers

Carbonyls

Ketones

Aldehydes

Esters

Volatile fatty acid esters

Fatty esters

Carboxylic Acids

YES

Normal paraffins  
Iso-paraffins  
Cycloparaffins  
Olefins  
Alcohols

YES FOR SOME

Aromatics  
Ketones  
Volatile fatty acid esters  
Furans  
Ethers

NO

Multi-ring aromatics  
Aldehydes  
Fatty esters  
Carboxylic acids