

Evaluation of the impact of drive impedance on the performance of spark gap switches

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Outline

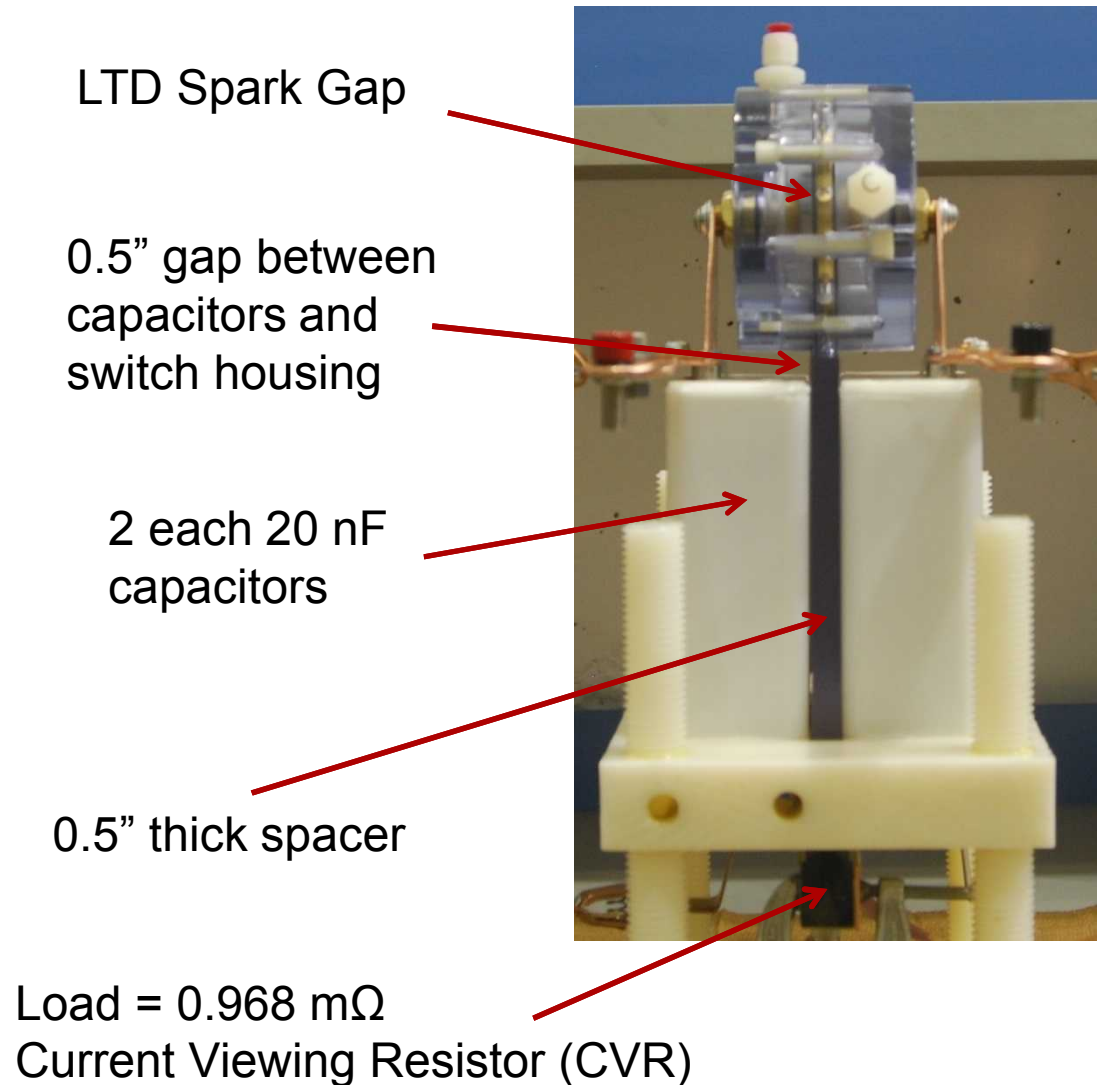
- Background / Motivation
- Circuit model development for Linear Transformer Driver (LTD) circuits and switches
- Experimental setup for characterizing LTD switches in a simplified geometry to isolate switch arc behavior
- Circuit modeling results
- Future work

Background

- Many models have been developed to describe the resistance profile of an arc in a spark gap switch
- At Sandia we often use a circuit model developed by Tom Martin
 - Resistance is determined from the arc channel radius - based on work by Braginski
- This model works well, but in practice we often tweak inputs such as number of parallel arcs to improve agreement with experimental data.
- Here we evaluate a test platform that could lead to better switch models

In LTD bricks we've used short circuit tests to evaluate circuit parameters

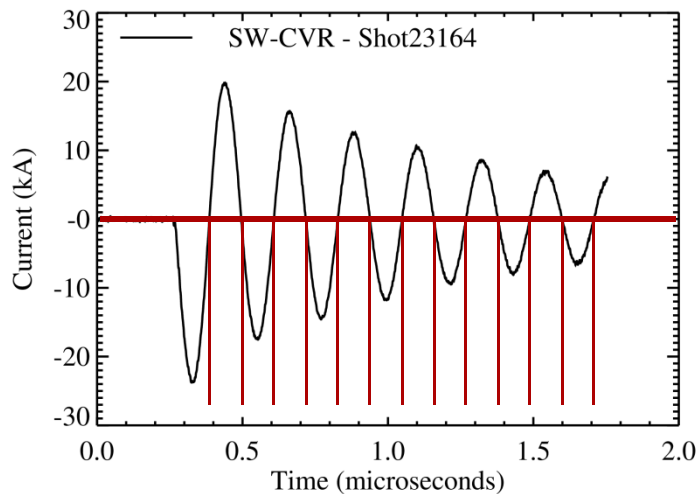
- Shown here is a single brick from a Linear Transformer Driver (LTD) circuit.
- This test circuit uses a near short circuit load to evaluate circuit parameters



Short circuit tests are used to determine inductance and series resistance

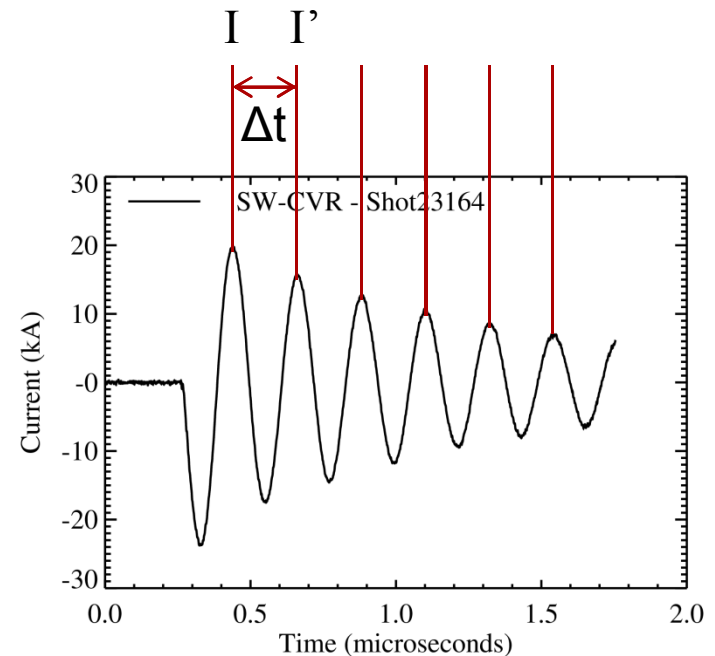
- Circuit inductance is calculated from the ringing period:

$$L = \left(\frac{T}{2\pi}\right)^2 / C$$



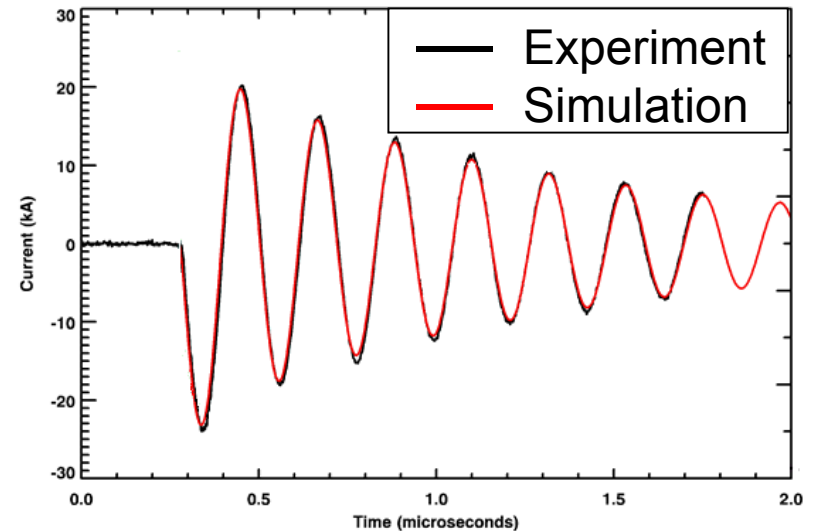
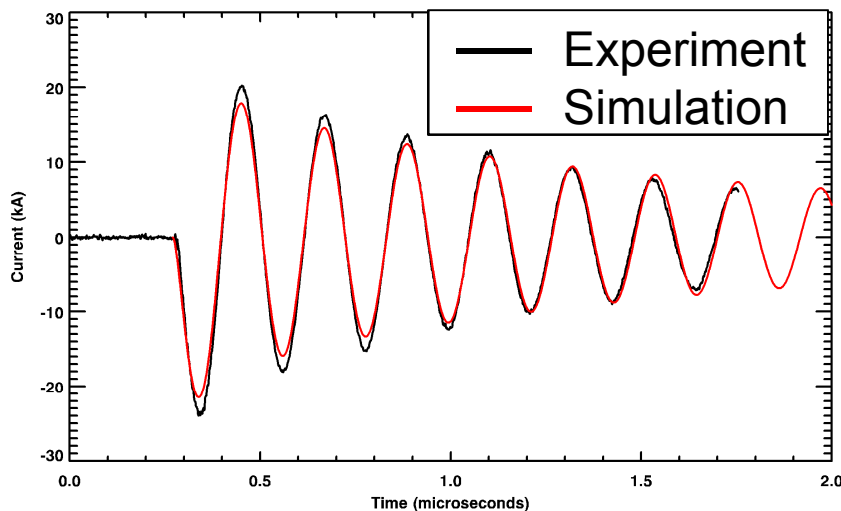
- Late time resistance is calculated from the decay rate of the oscillation:

$$R = 2L \frac{\ln(I/I')}{\Delta t}$$



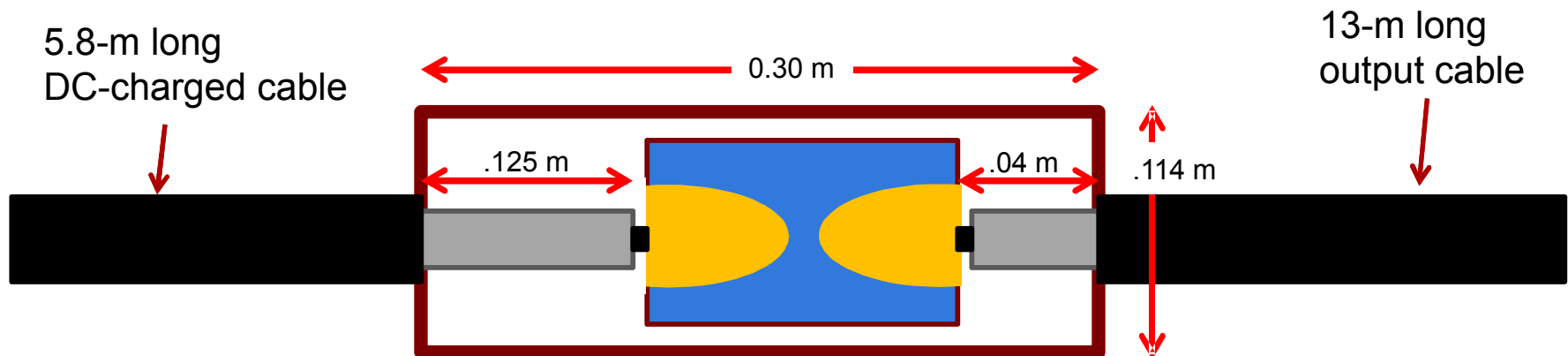
Circuit models of the LTD circuit require small adjustment to match experiment

- Using the measured circuit values we can simulate the experiment.
- Switch model uses experimental gap length, air pressure, and assumes 1 arc channel.
- Improve matching during the first cycle by adjusting switch model inputs:
 - Switch pressure cut in half
 - Number parallel arcs increased to 2.

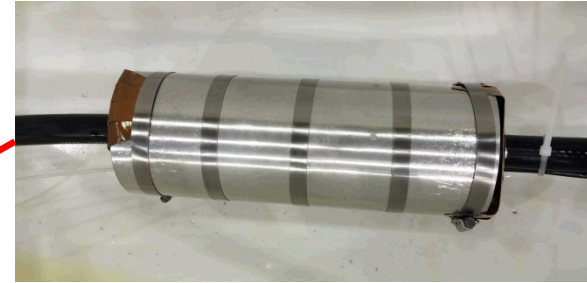
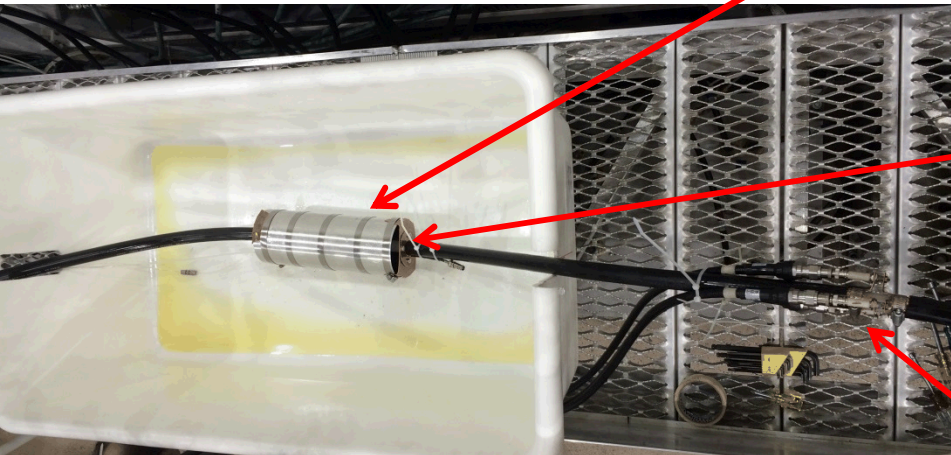


We put together a simple circuit to evaluate switch arcs

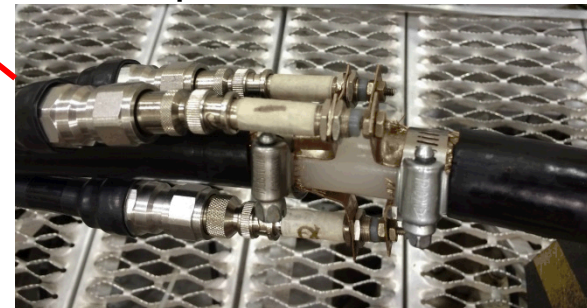
- Single gap self-break switch with no trigger plane or pin. Installed in a 0.11 m OD plastic tube surrounded in metal.
- The simple geometry simplifies circuit modeling
- Self-break testing with static air pressure. Charge voltage slowly increased until the switch arced.
- CVR installed in the ground braid of the output cable ~1 m from the switch.



Simplified Switch Test Experimental Setup



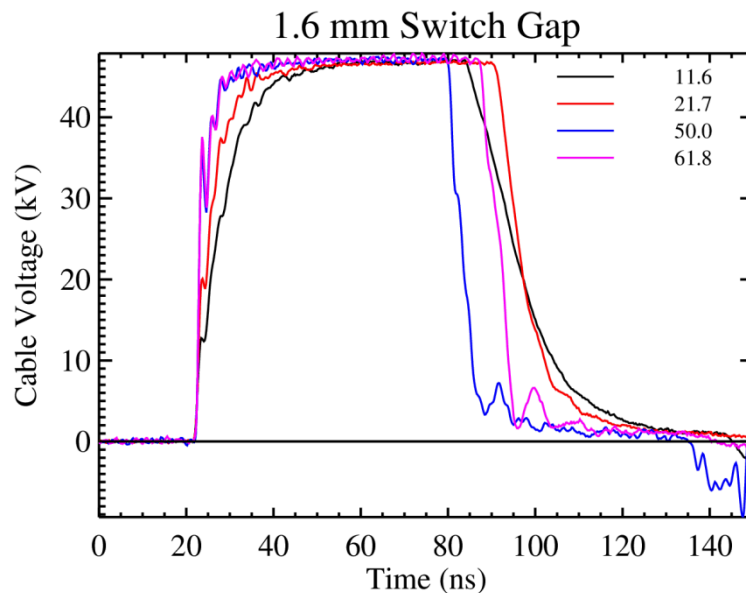
3 parallel CVRs



Switch was tested with four cable impedances and four switch gap lengths

Pulse Risetime (5-95%)

	1.6 mm Gap	2.5 mm Gap	5.0 mm Gap	10.0 mm Gap
11.6-ohm	19.4 ns	----	26.1 ns	30.4 ns
21.7-ohm	11.8 ns	13.9 ns	18.2 ns	23.4 ns
50.0-ohm	9.1 ns	11.0	11.9 ns	----
61.8-ohm	8.0 ns	10.2 ns	11.1 ns	17.8 ns



Observed Risetime Trend:

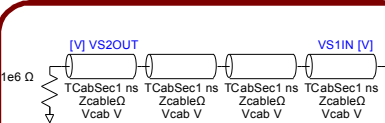
- Proportional to switch arc length
- Inversely proportional to cable impedance

Setup Notes:

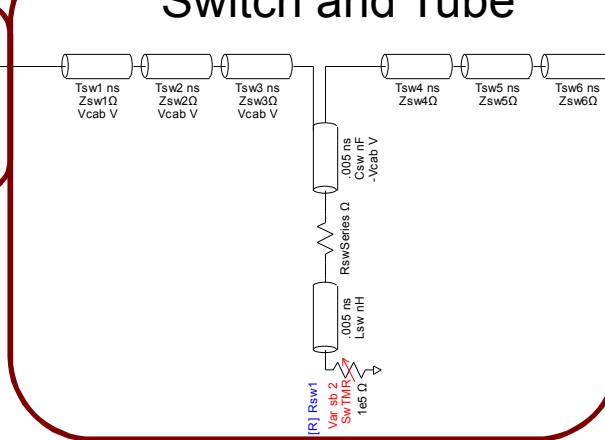
- Vcharge = 100 kVDC
- Each waveform is average of 5 shots

Circuit model of the system is very simple

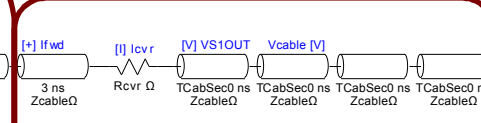
Charged Cable



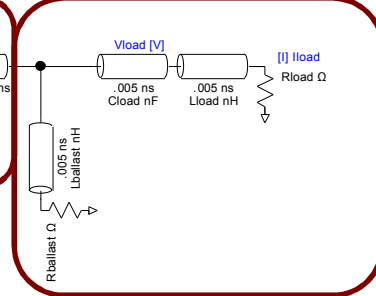
Switch and Tube



Output Cable & CVR



Load

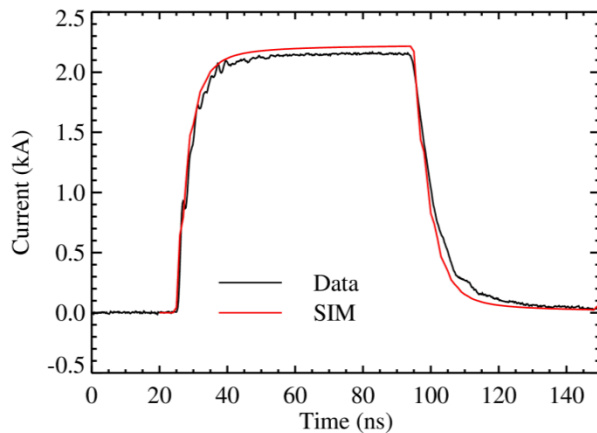


- Switch modeled with Tom Martin switch model which calculates resistance based on gas pressure, arc length, number of parallel arcs, and the current thru the arc.
- Switch also includes series arc inductance, switch capacitance, and constant series resistance.
- Switch connections are simple coaxial geometry
- Cables are broken into four series elements of equal length to reduce length of the longest segment – this helps Bertha (transmission line based circuit code).

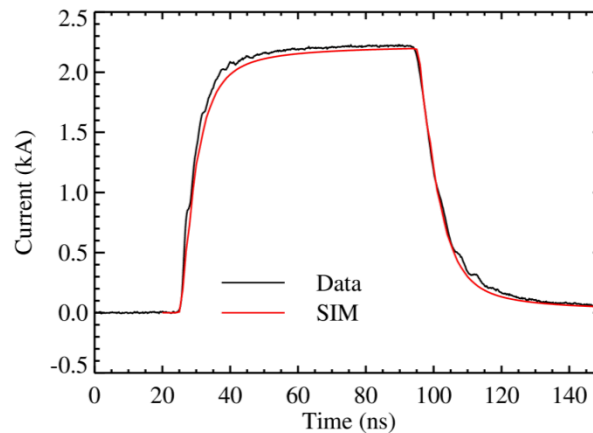
The circuit model does not accurately predict all pulse features

- The three cases below use the same circuit geometry (21.7-ohm cable), only changing the switch arc length.
- The Tom Martin arc resistance model does not accurately capture the resistance profile thru the entire pulse
- No one parameter adjustment (such as number of parallel switch arcs) would correct all three cases.

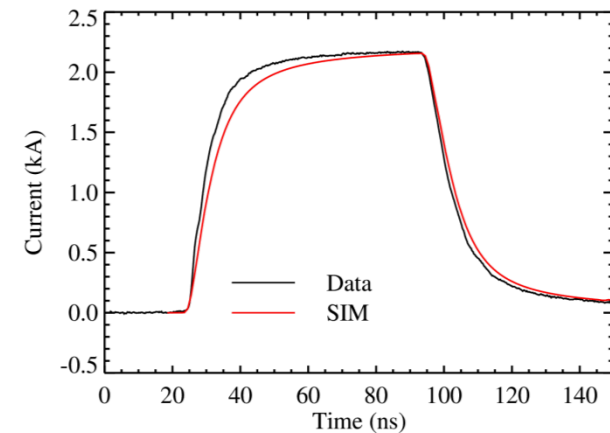
1.6 mm arc



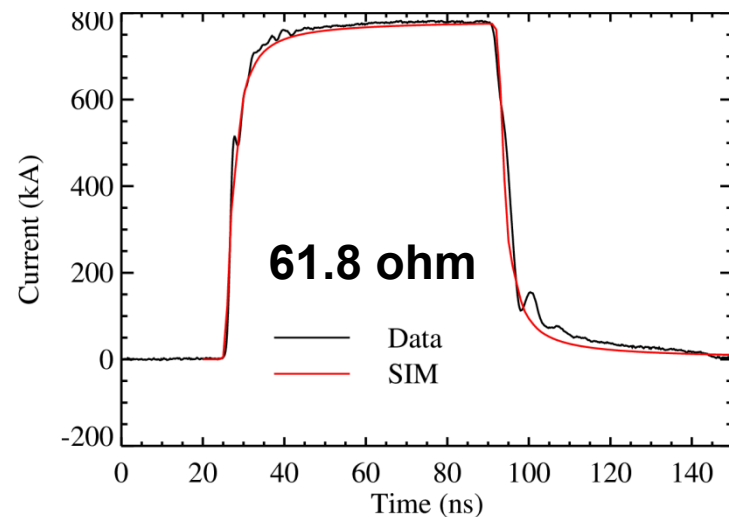
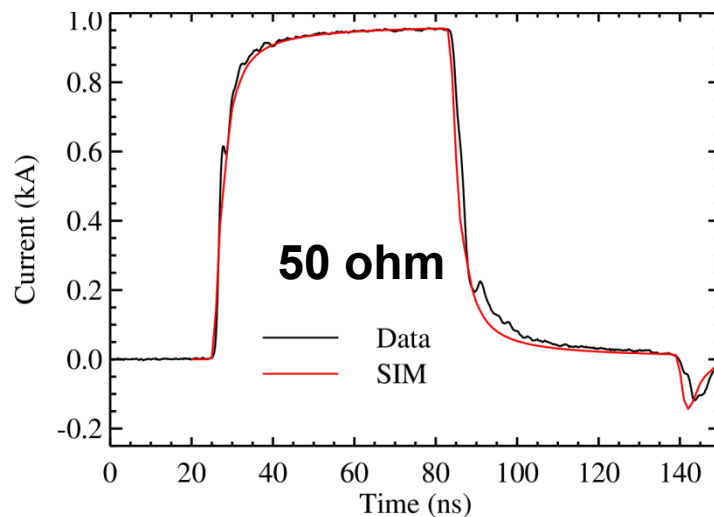
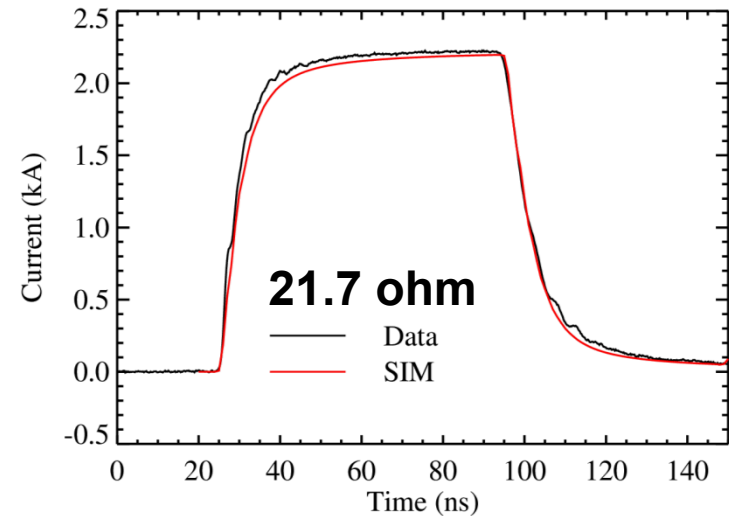
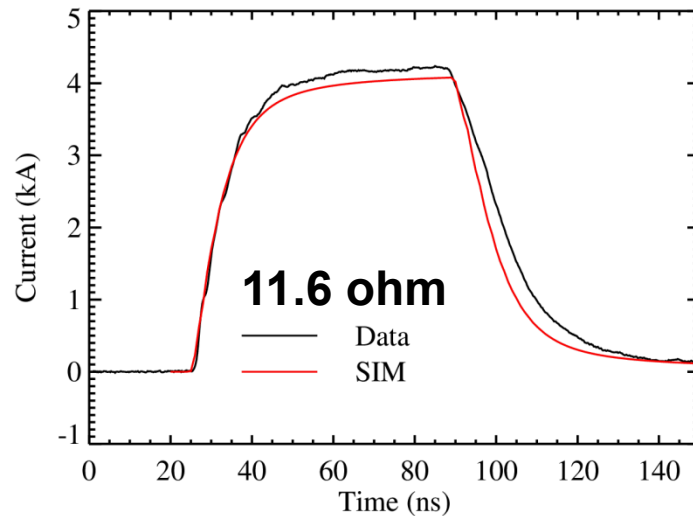
5.0 mm arc



10 mm arc



Circuit model doesn't match all 5.0 mm switch gap experiments equally well



Conclusion

- The Tom Martin switch model works very well, but does not accurately predict all configurations.
- Our experiments were not diagnosed well enough to help guide development of an improved model.
- Possible Future Work
 - Repeat experiment with improved voltage and current measurements
 - Develop a model for time varying inductance based on Braginski arc radius (similar to Tom Martin switch resistance model)