

Modeling Porous PMDI-based Polyurethane Foam Decomposition in Pressurizing Systems

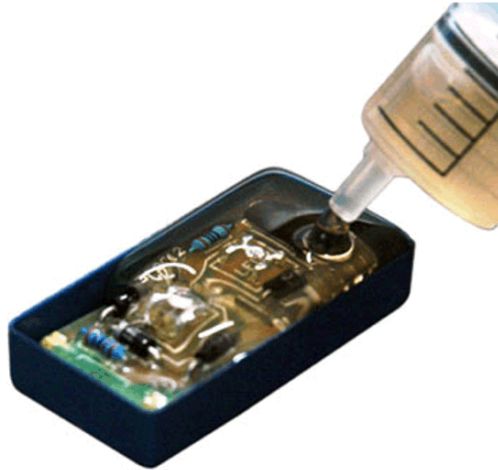
Sarah Scott, Amanda Dodd, Victor Brunini, and Ryan Keedy

10th U. S. National Combustion Meeting
April 24th 2017



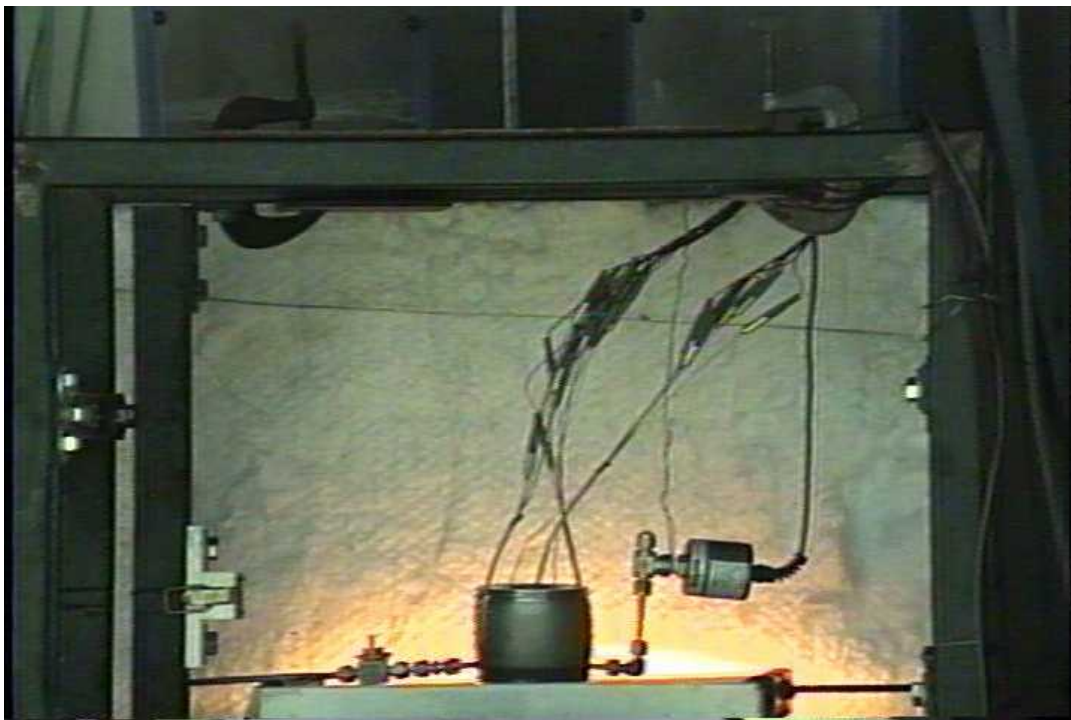
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Motivation



- Electronic devices need protection from mechanical and thermal shocks under normal operating conditions
 - Foams can be used for this purpose
- Foams pyrolyze at relatively low temperatures (250C – 300C)
 - In a fire environment and in sealed systems, the foam pyrolysis can cause pressurization
- Need a model of heat transfer and pressurization
- Medium scale experiments for validation

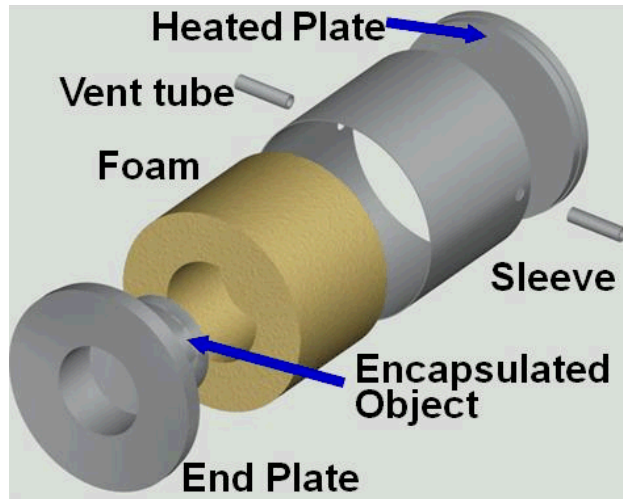
Foam in a Can



- Medium Scale Experiment
 - Foam in a Can (FIC)

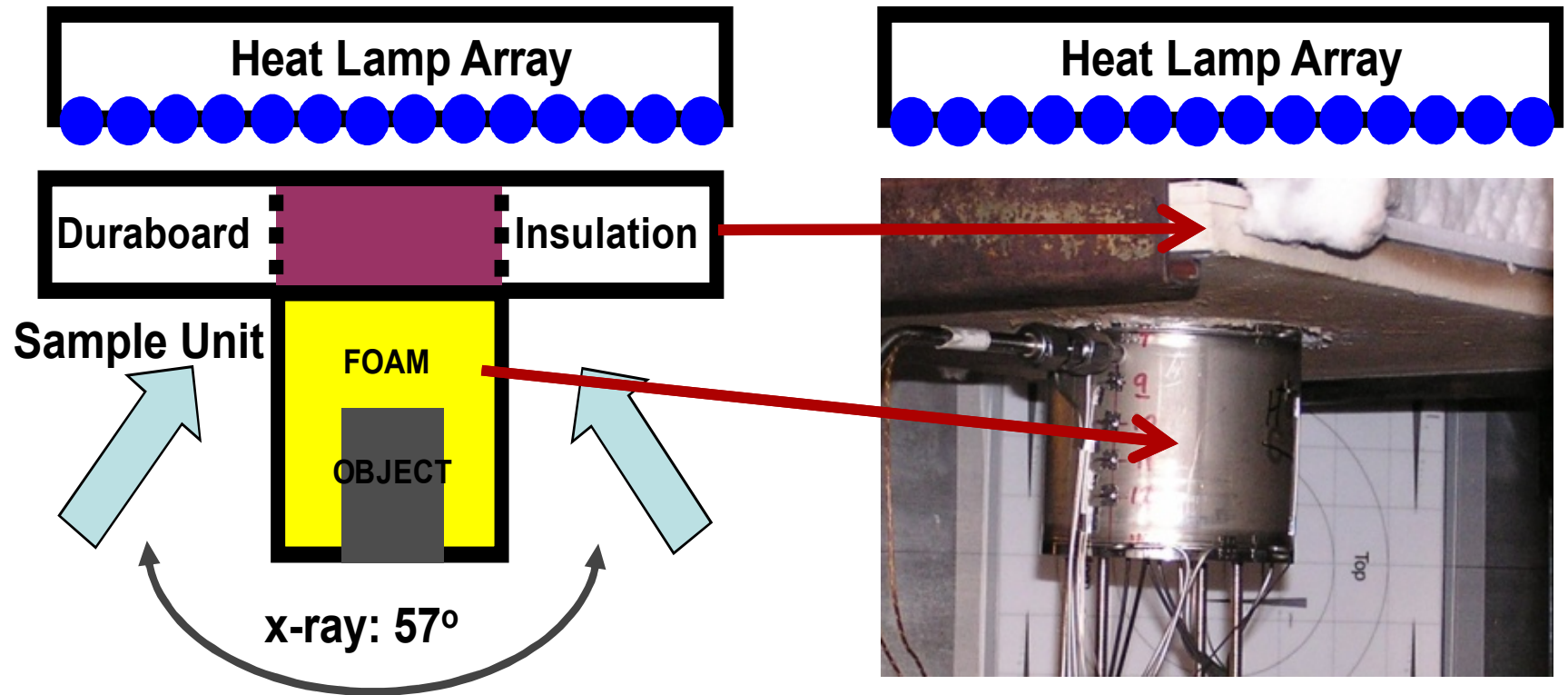
Encapsulating foam heated to 900 C at a rate of
200 C/min

Foam in a Can Experiment



- Data Sets:
 - 320 kg/m³ PMDI polyurethane foam (rigid, closed cell)
 - Heated to 800 C at a rate of 150 C/min and 50 C/min.
- Can dimensions are approximately
 - Diameters: 9 cm
 - Length: 6.5 cm
 - Side Wall Thickness: 0.5 mm

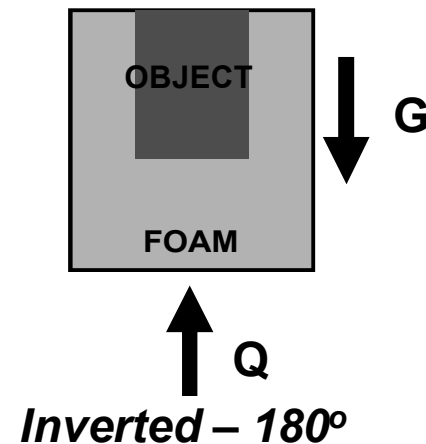
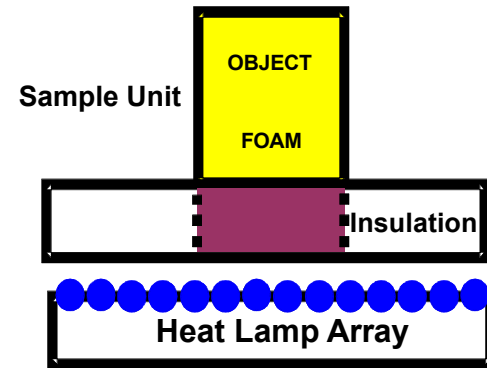
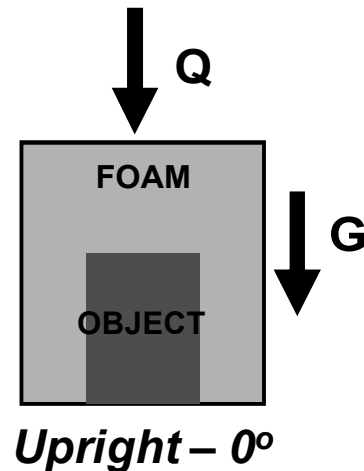
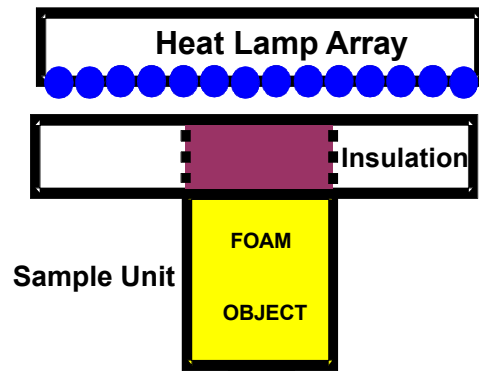
Foam in a Can Experiment



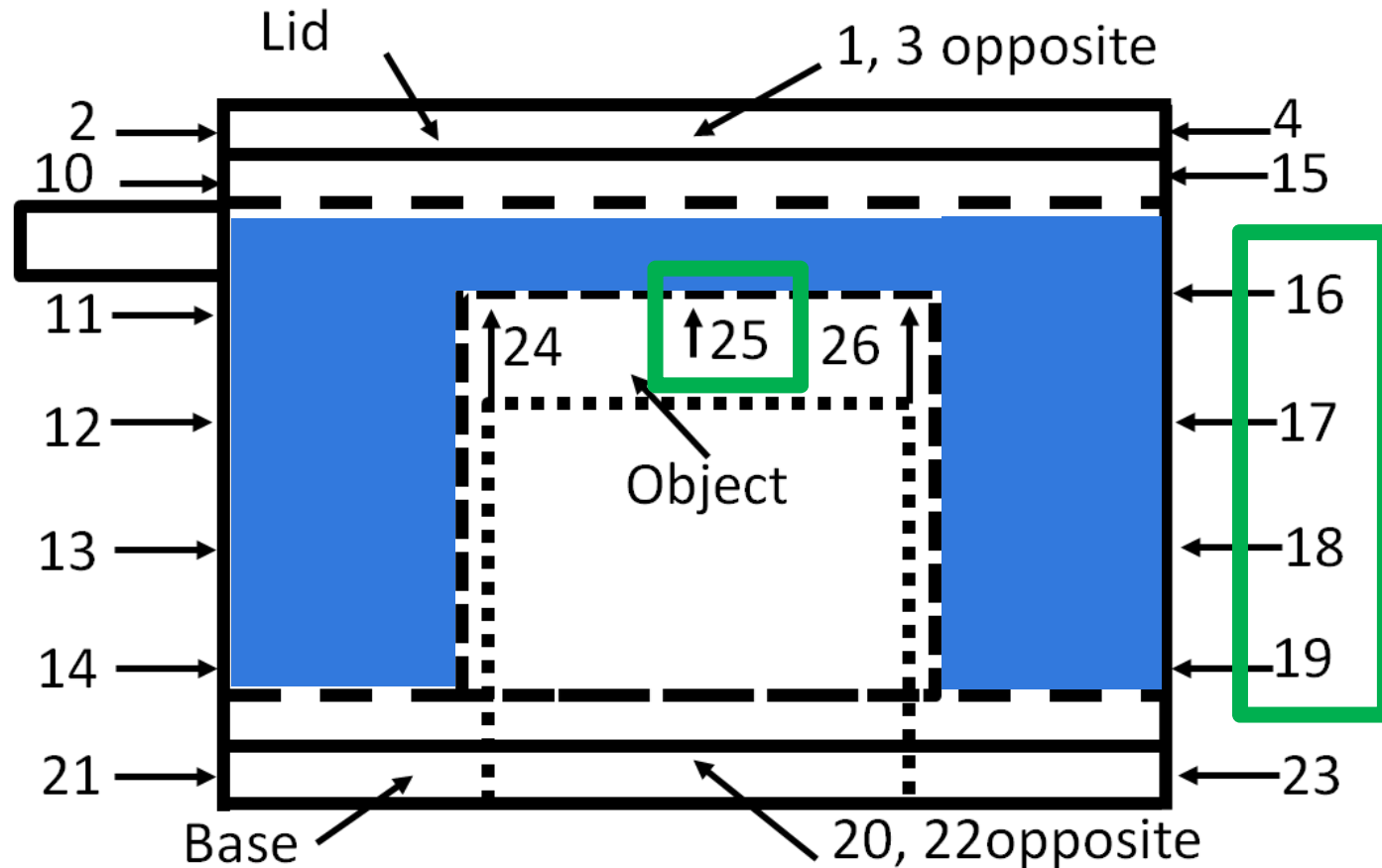
- Monitor pressure and temperature
- X-Rays to view can interior
- Experiments run to breach

Foam in a Can Experiment

- Experiment conducted in upright and inverted orientations
 - Material bulk movement towards or away from heat source



Foam in a Can Experiment



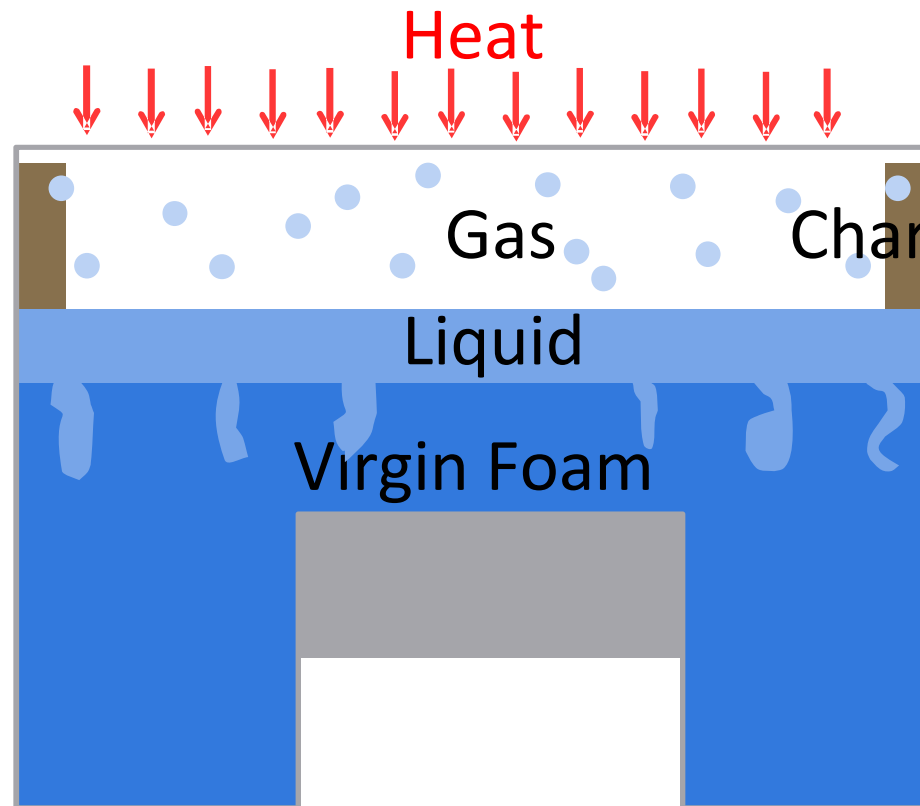
Temperature is monitored on the top, along the sides, and on the bottom of the can as well as on an embedded object.

Decomposing Foam

Virgin Material + Heat



Decomposition Products
(solids, liquids, gases)

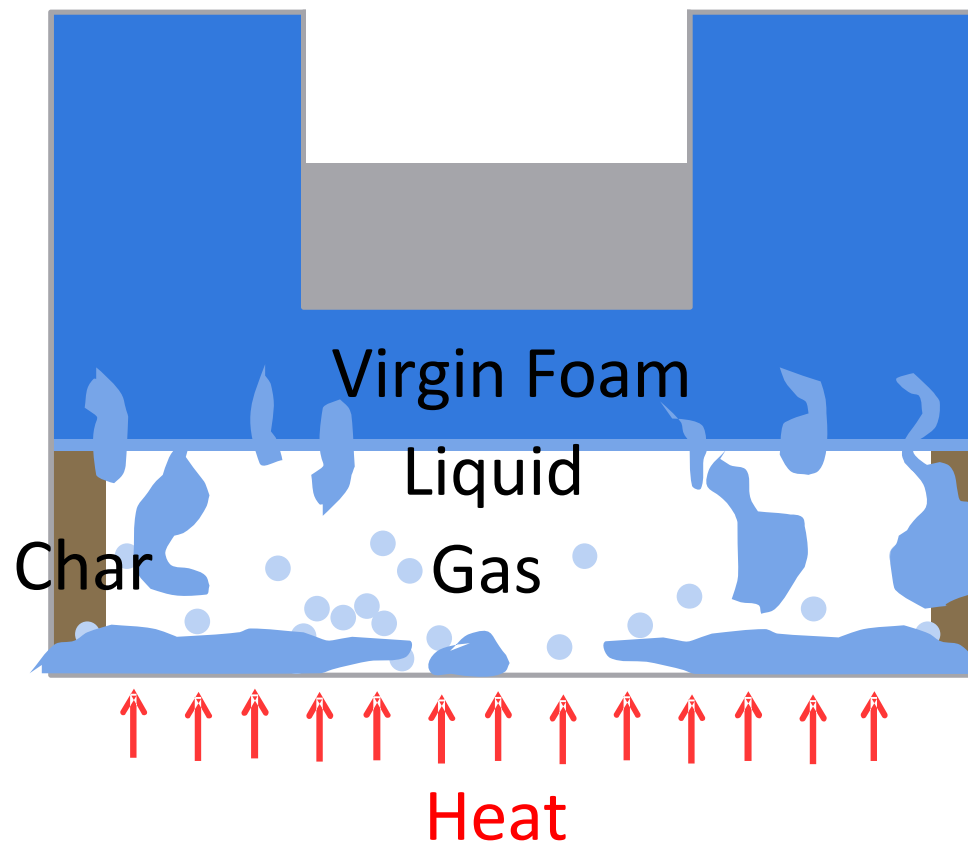


Decomposing Foam

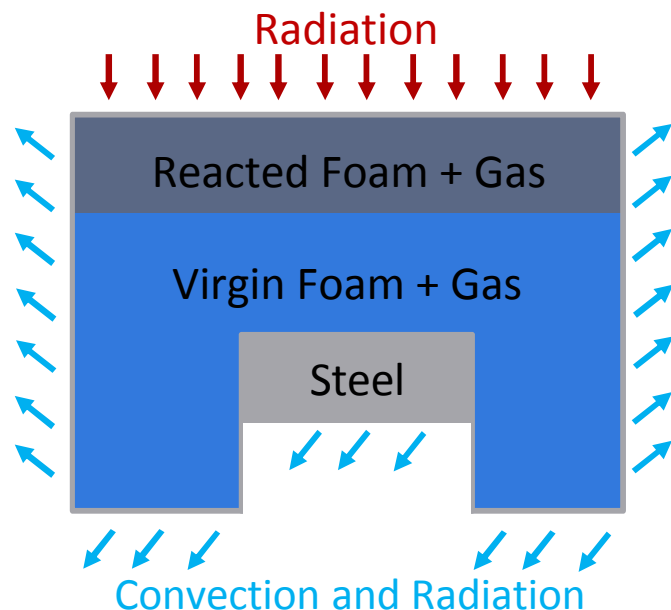
Virgin Material + Heat



Decomposition Products
(solids, liquids, gases)



Porous Flow Model Description



- 3D Model in Aria
- Three step reaction mechanism
 - PMDI Polyurethane \rightarrow CO_2 , light and heavy organics (gas phase), char
- Continuity, species, and enthalpy equations
 - Solved for in condensed and gas phases
 - Gas velocity solved using Darcy's approximation for flow through a porous material
 - Ideal gas law used to relate density to pressure
 - Radiative and Convective boundary conditions
- Material Properties
 - Foam Effective Conductivity, Foam Porosity, Foam Permeability
 - Function of reaction
 - Other material properties
 - Constant or function of temperature

- Porous media equations introduce variables into that are unknown
 - Virgin foam permeability
 - The foam is closed cell, therefore a permeability can't be tested.
 - Virgin Foam Range: 10^{-14} to 10^{-7}
 - Char foam permeability
 - Can't be measured in-situ
 - Char Foam Range: 10^{-8} to $10^{-6.5}$
 - Organic gas fraction
 - Unclear what fraction of the decomposition products are in the gas vs condensed phase
 - Range: 0 to 0.44
 - Rosseland-mean extinction coefficient (β_R) to calculate the radiation contribution to the effective conductivity in the char
 - Absorption and scatter can't be measured in-situ
 - Range: 200 to 1990

Organic Gas Fraction

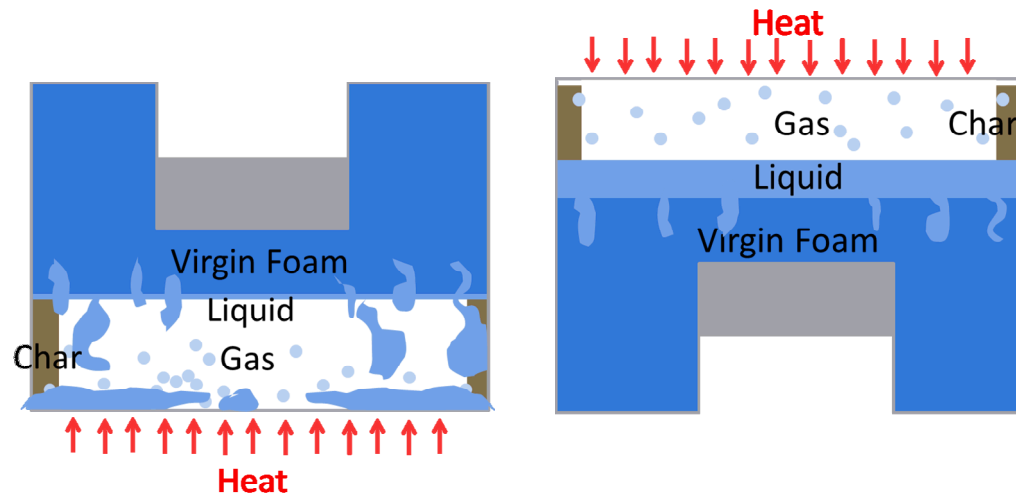
$$PMDI\ RPU = 0.45\ FOAMA + 0.15\ FOAMB + 0.4\ FOAMC$$

$$FOAMA \rightarrow [0.56]\ CO_2 + [0.44 - \text{gasorg}]\ LMWO + [\text{gasorg}]\ char$$

$$FOAMB \rightarrow [1 - 2 * \text{gasorg}]\ HMWO + [2 * \text{gasorg}]\ char$$

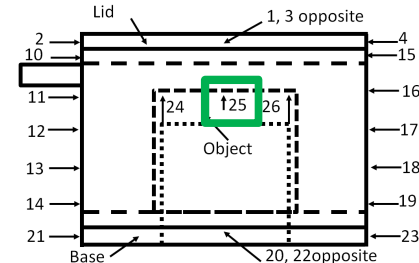
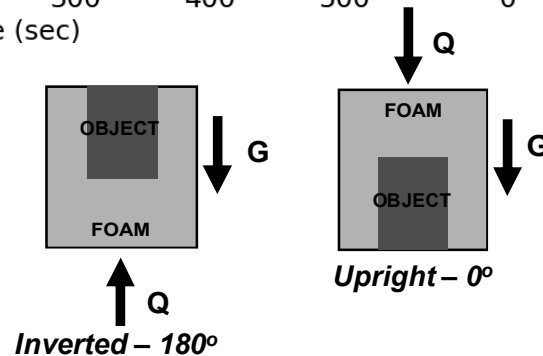
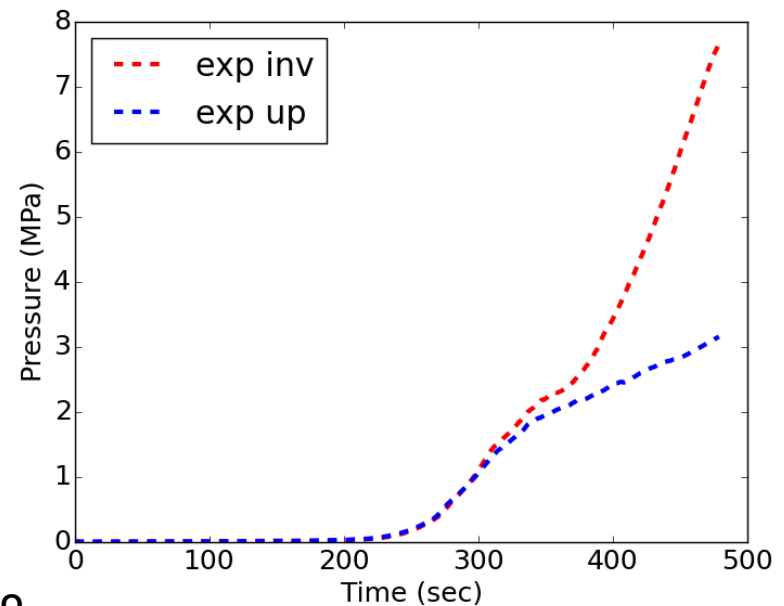
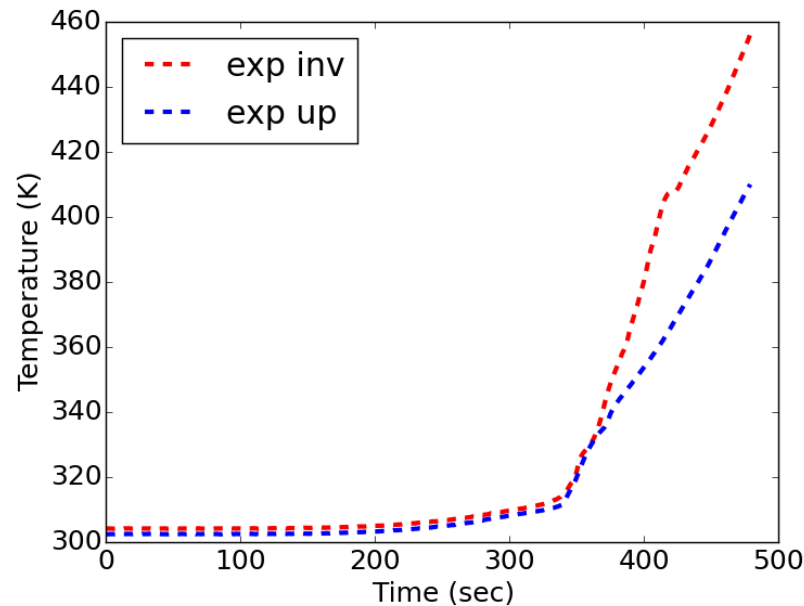
$$FOAMC \rightarrow [0.5 - \text{gasorg}]\ HMWO + [0.5 + \text{gasorg}]\ char$$

- Varied from 0 to 0.44
- Separate values for inverted and upright to approximate liquid dripping

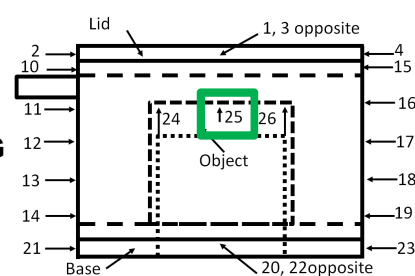
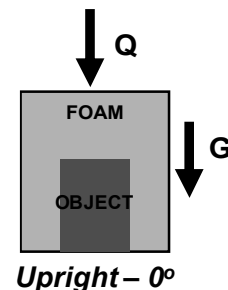
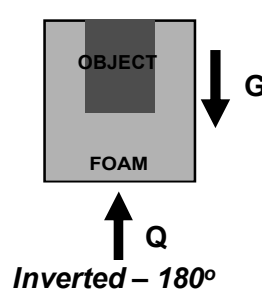


Parameter Calibration/Optimization

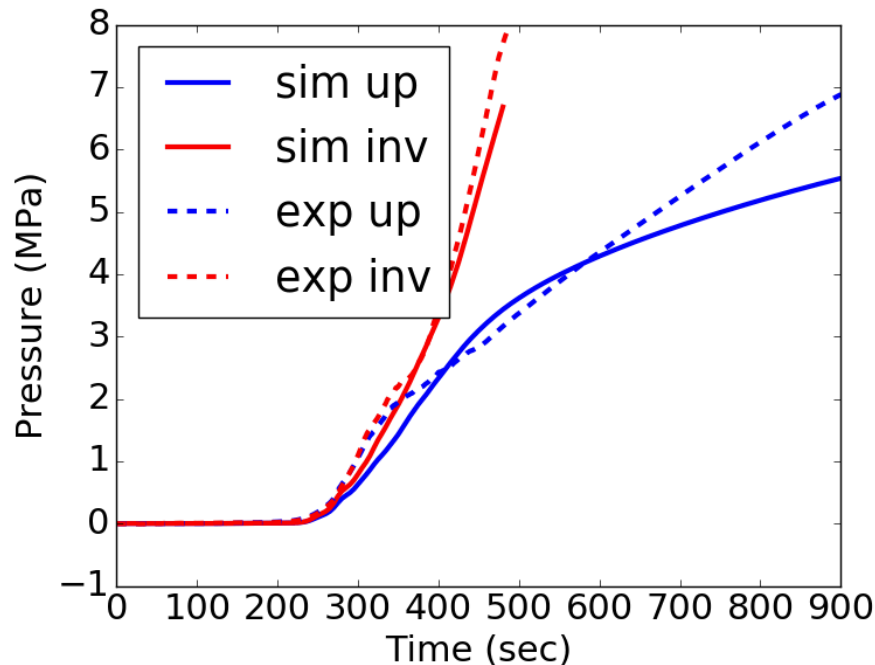
- Global method was used
- Pressure and temperature of the slug are the optimized response quantities (from 150 C/min data set)



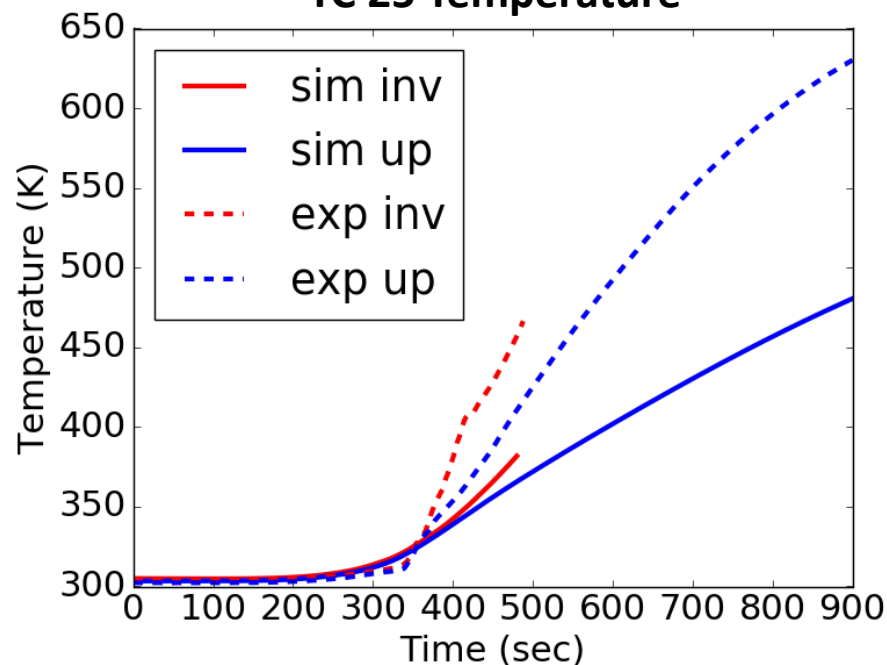
150 C/min



Pressure

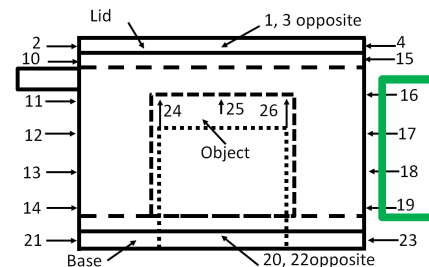
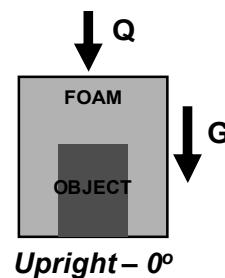
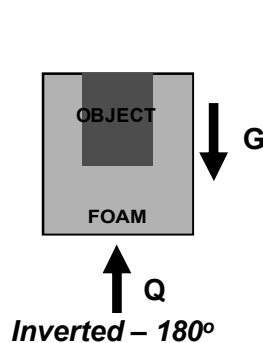
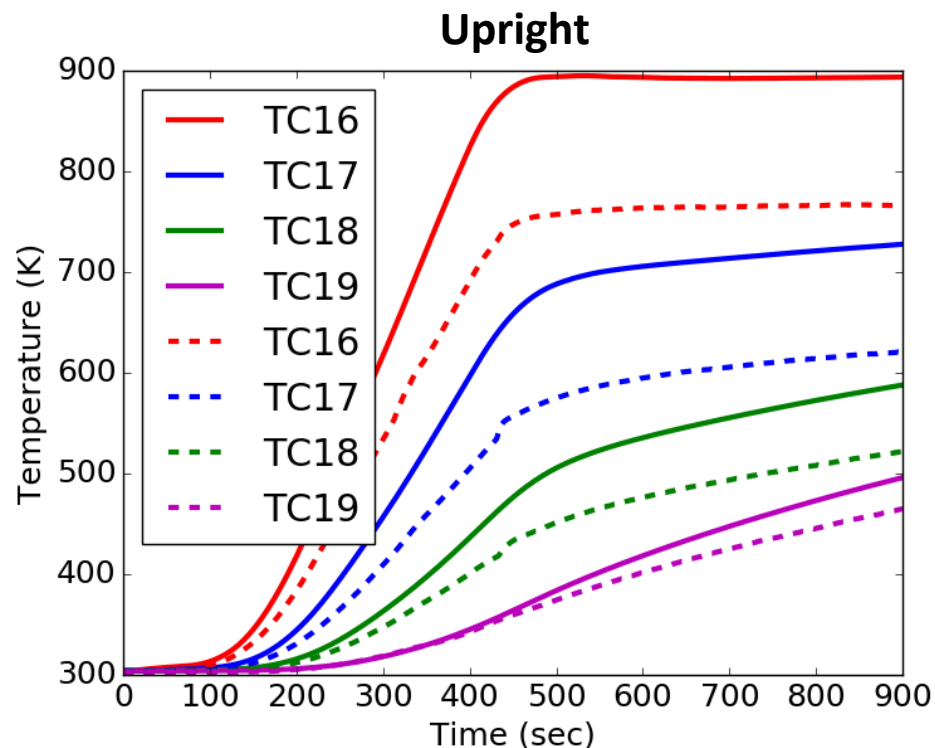
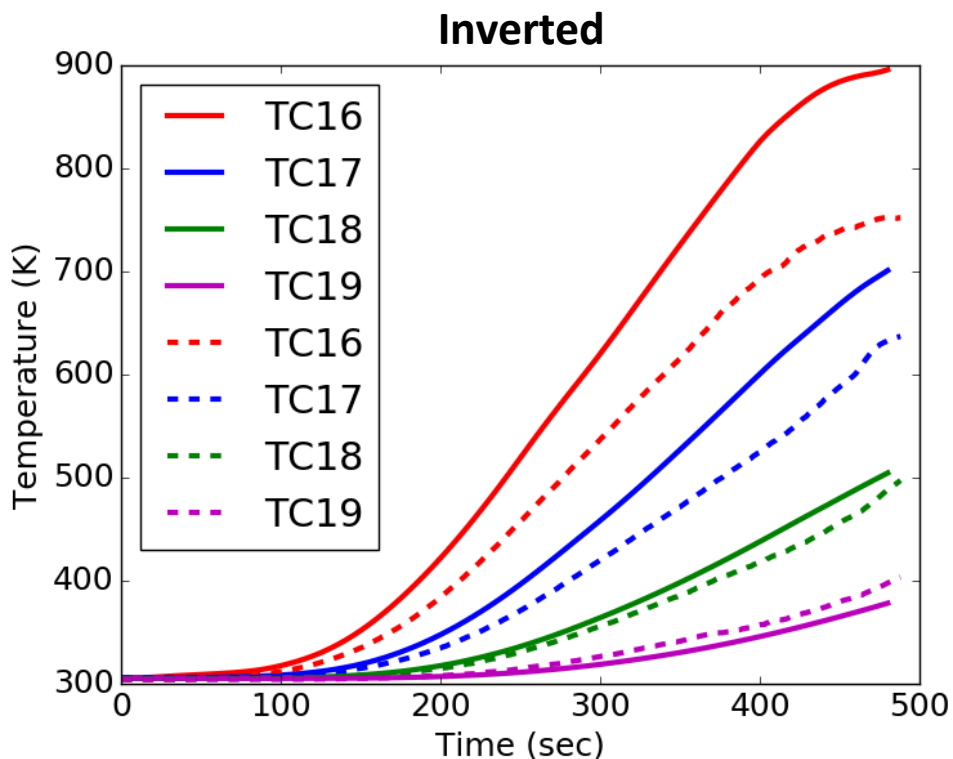


TC 25 Temperature



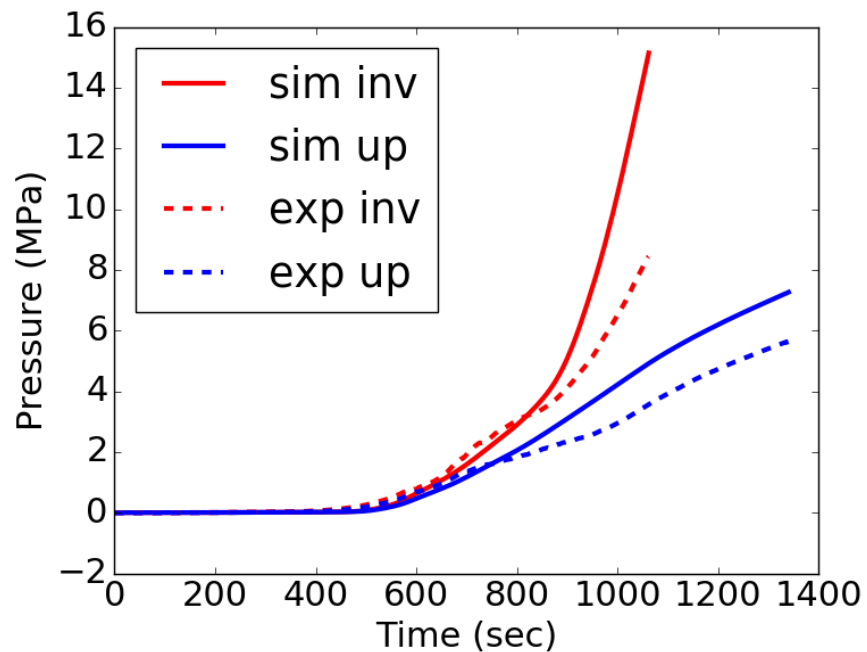
	Low Bound	High Bound	Optimized Value
Virgin Foam Permeability [m^2]	1×10^{-14}	1×10^{-8}	7.76×10^{-13}
Char Foam Permeability [m^2]	1×10^{-8}	$1 \times 10^{-6.5}$	1.48×10^{-8}
Upright Organic Gas Fraction	0	0.44	0.37
Inverted Organic Gas Fraction	0	0.44	0.22
Char β_R [mK]	200	1990	579

150 C/min

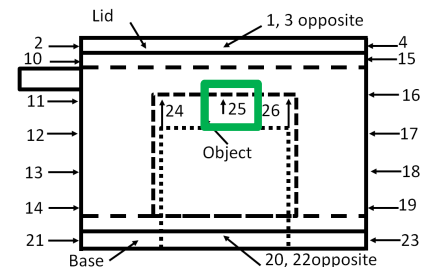
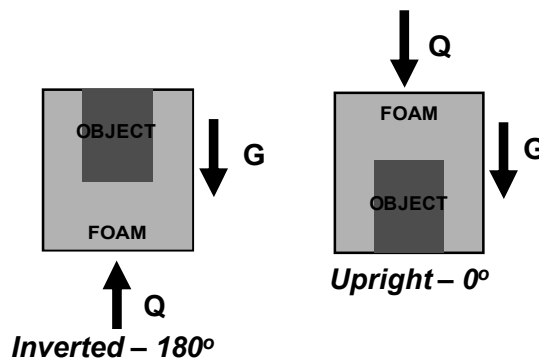
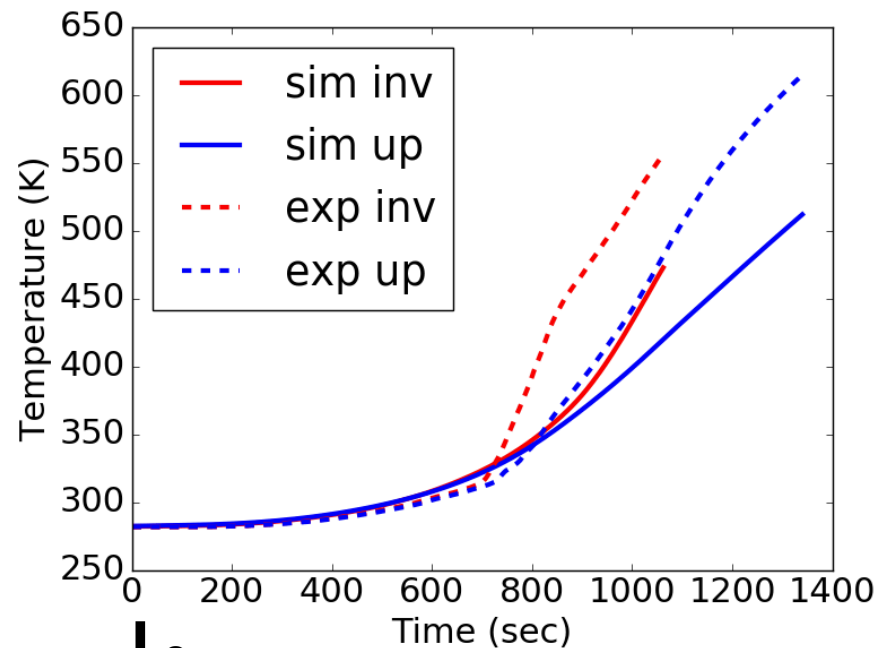


50 C/min

Pressure

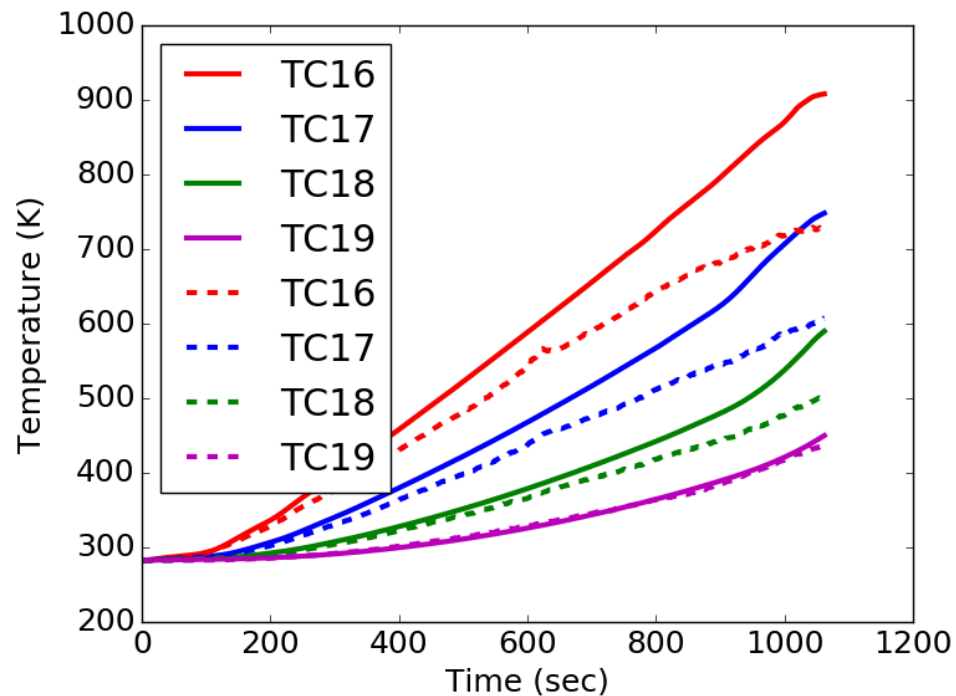


TC 25 Temperature

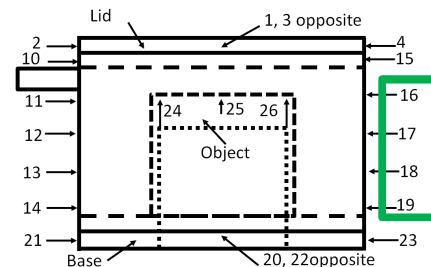
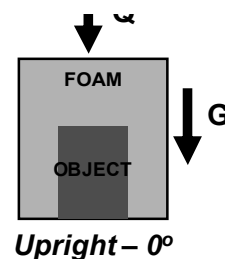
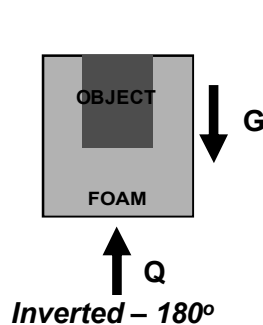
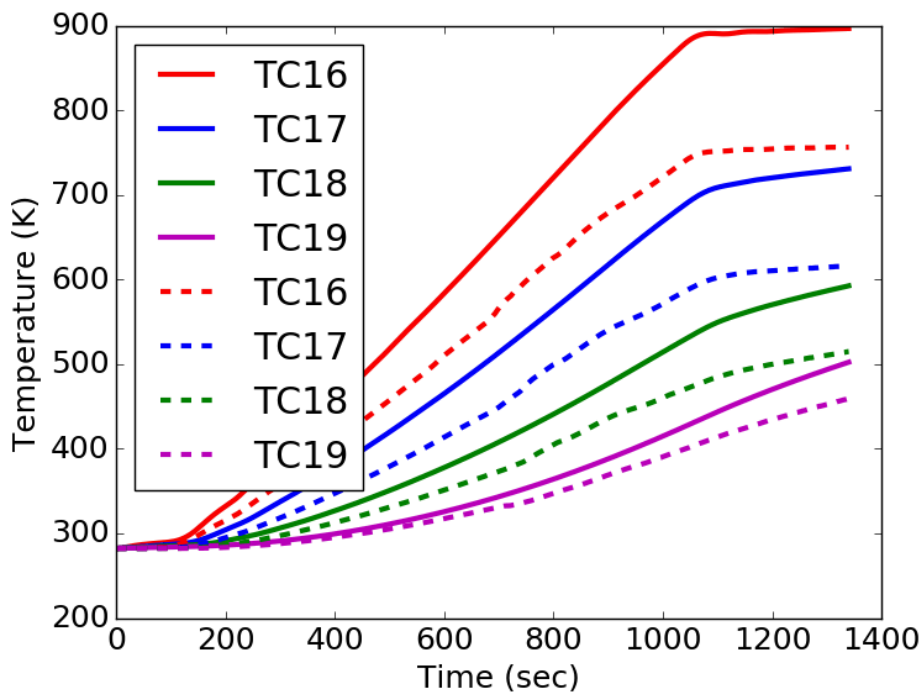


50 C/min

Inverted

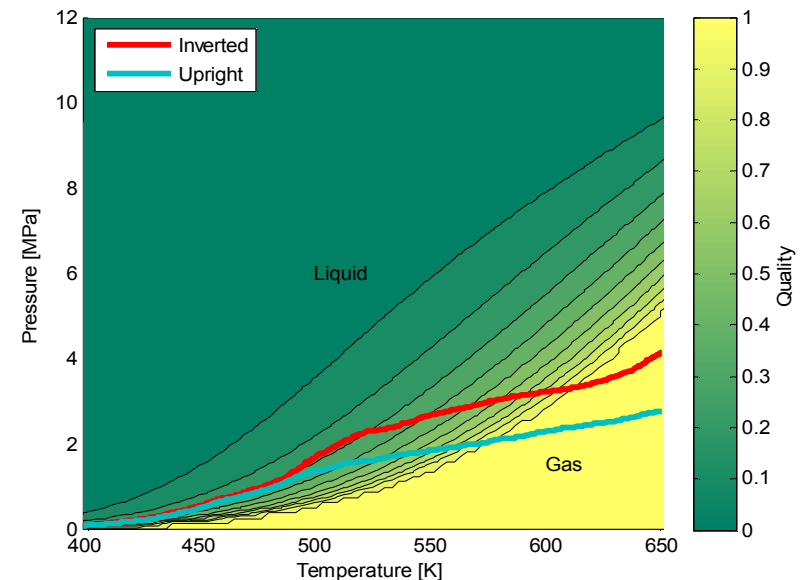
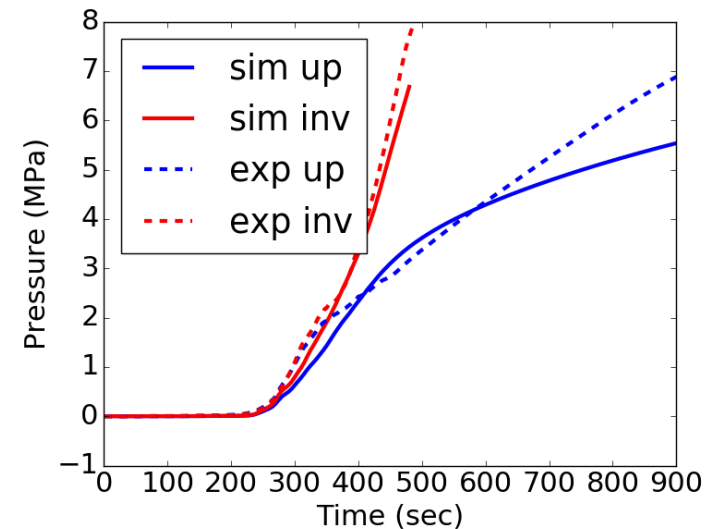
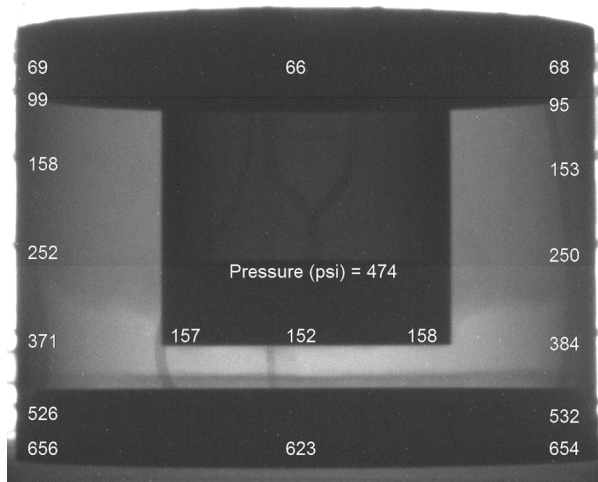


Upright



Future Work - Vapor Liquid Equilibrium

- This study more closely matched experimental data when separate values controlled the rate of gasification
- X-Rays of the experiments show what looks to be liquid decomposition products
- Early investigations show that major decomposition products can be liquids at pressures and temperatures seen in the experiments.



QUESTIONS?

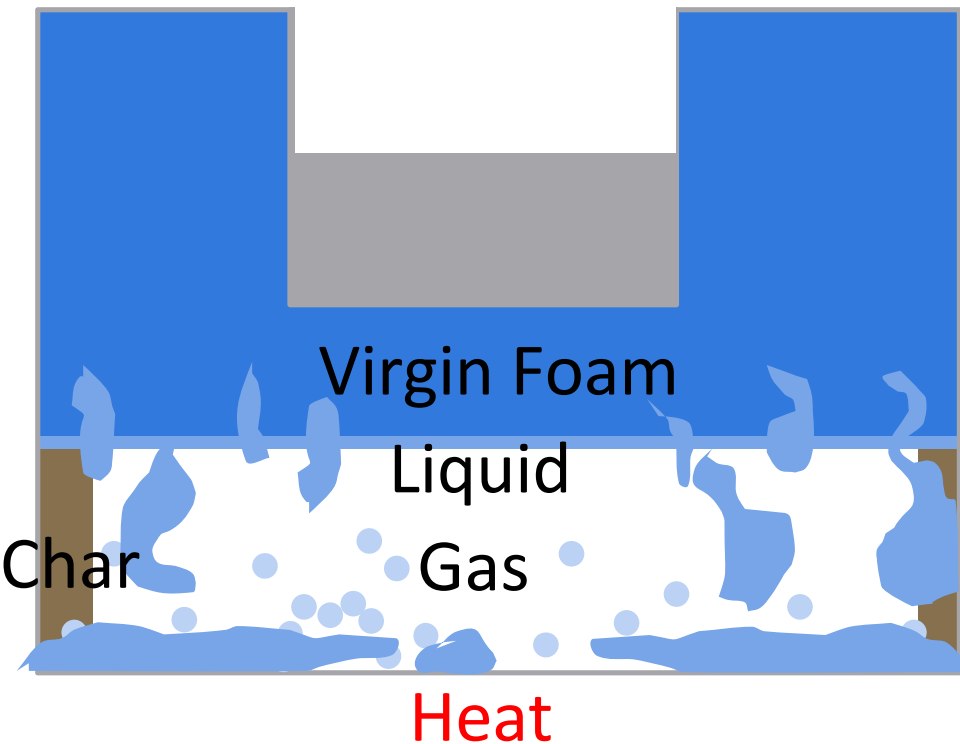
Previous Work

- Previous Model Development
 - No flow model
 - Model developed with foams that leave structured char
 - Good agreement in temperature and pressure with experiments
 - Erickson, K.L., *et al.* Proceedings of BCC 2010, Stamford, CT, May 2010
- Previous PMDI Polyurethane Development using Erickson (no flow) model
 - Scott, S.N., *et al.* Fire Technology Dec 2014
 - Validation of 150 C/min data set
 - Mean Value and Latin Hyper Cube were compared
 - Scott, S.N., *et al.* Mediterranean June 2015
 - Want understand the effect of heating rate

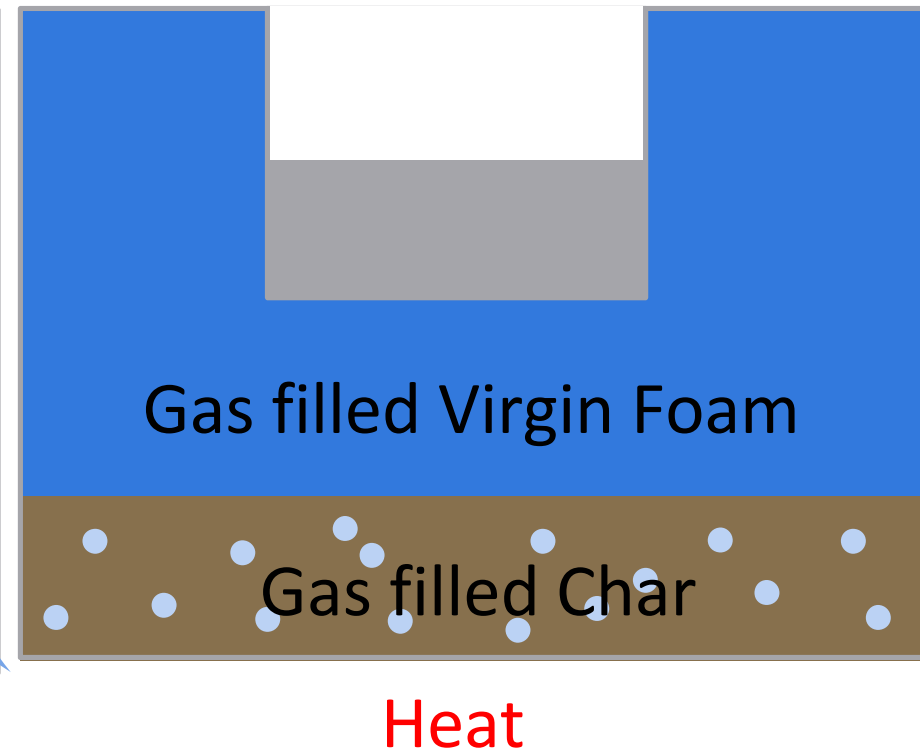
BACKUP SLIDES

Modeled Physics

Reality



Model



Permeability

- Appears in the Darcy approximation

Flow velocity $\rightarrow u_{j,g} = - \frac{\overset{\text{Permeability}}{\bar{K}}}{\underset{\text{Gas Viscosity}}{\mu_g}} \left(\underset{\text{Pressure Gradient}}{\frac{\partial P_g}{\partial x_j}} + \rho_g g_j \right) \leftarrow \text{Body Force}$

- Virgin Foam Range: 10^{-18} to 10^{-7}
- Char Foam Range: 10^{-9} to 10^{-6}
- Exponent is varied
- Check to ensure Virgin Foam Permeability is lower than Char Foam Permeability

Rosseland-mean Extinction Coefficient

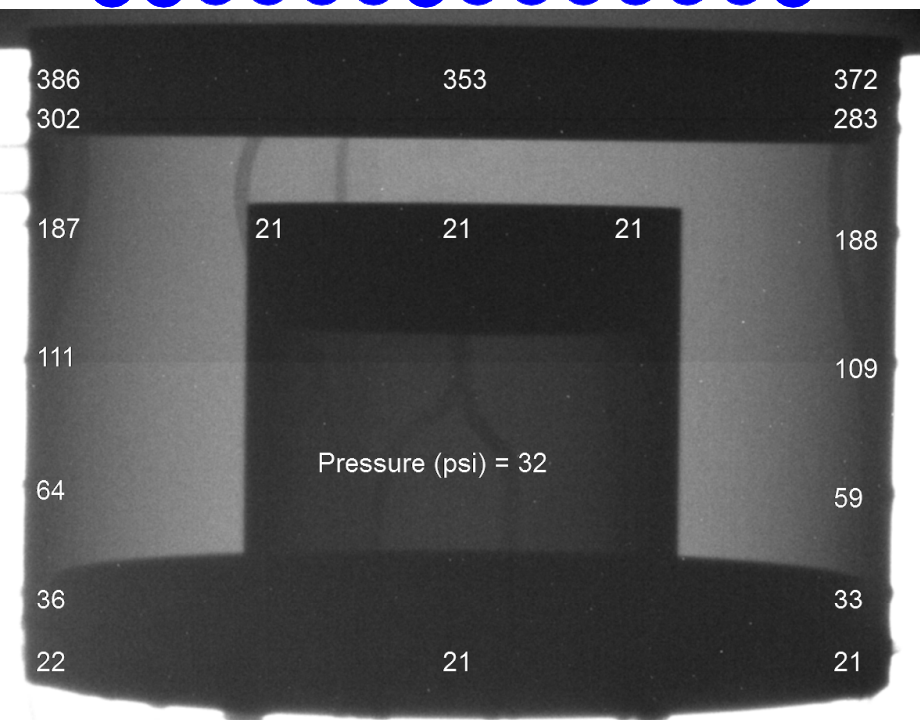
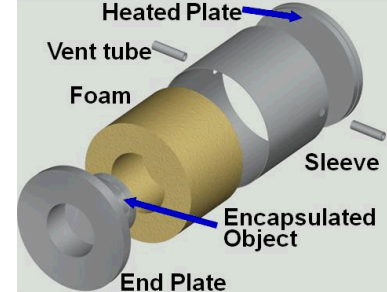
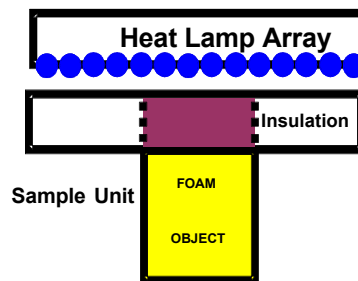
Radiation Effective Conductivity $\rightarrow k_{rad} = \frac{16\sigma}{3\beta_R} T^3$

Stefan-Boltzmann \swarrow
Temperature \nwarrow
Rosseland-mean Extinction Coefficient \nearrow (points to β_R)

- Varied from 200 to 1900

X-Ray Video

Upright Experiment
50 C/min



X-Ray Video

Inverted Experiment
50 C/min

