

Aerosol Deposition as a Method of Room Temperature Thick-Film Deposition

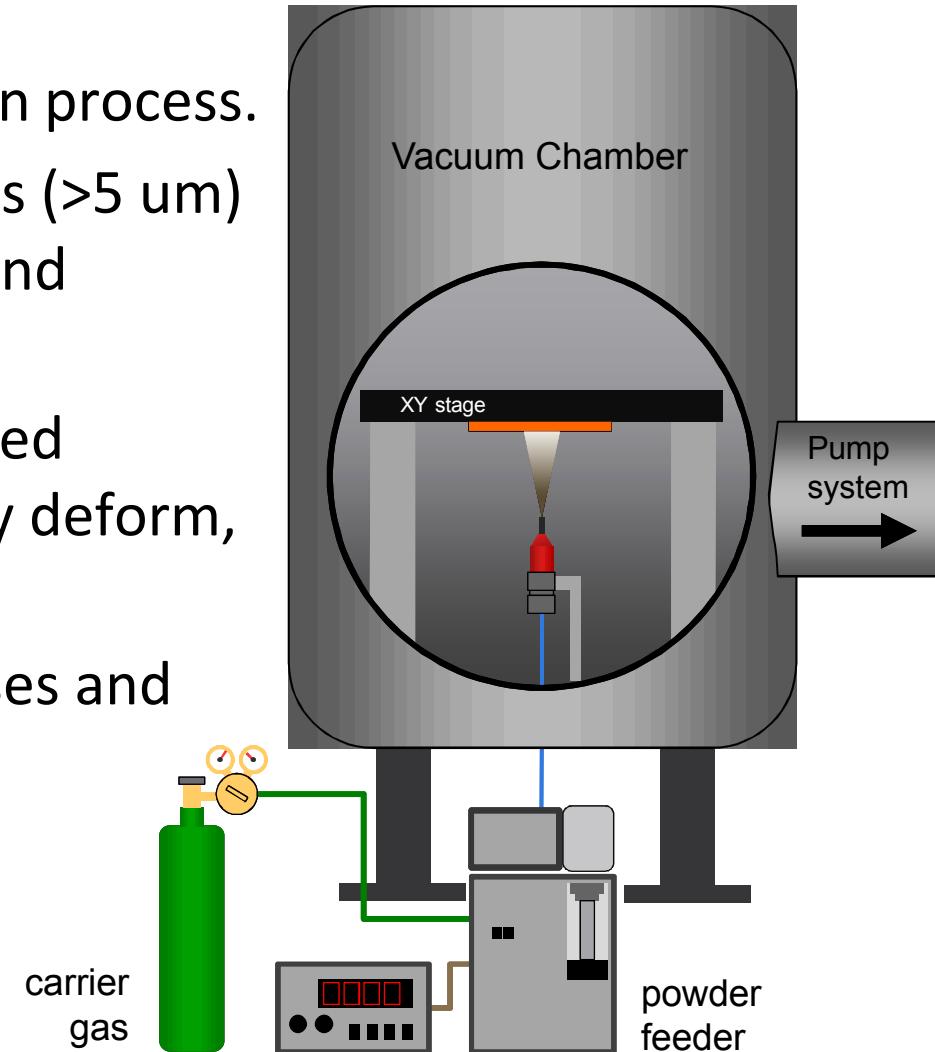
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Aerosol Deposition (AD) Process

- Room temperature deposition process.
- Deposits thick and dense films ($>5 \text{ um}$) of metal, ceramic, polymer, and composites.
- Utilizes micron-submicron sized powders to impact, plastically deform, and bond to the substrate.
- Vacuum environment increases and maintains particle velocity.



Aerosol Deposition (AD) Process

Deposition methods

Characteristics of various deposition processes

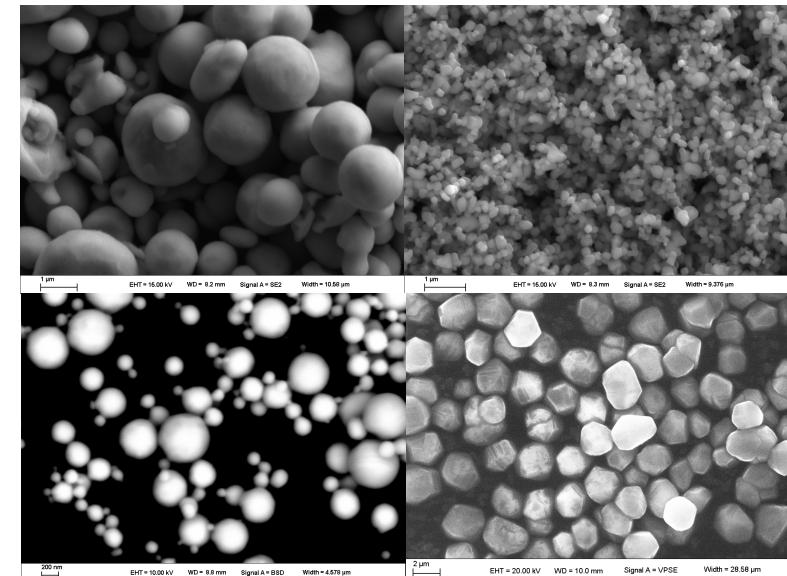
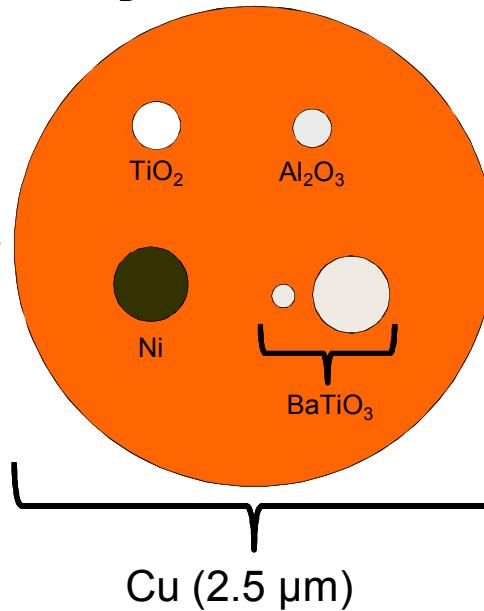
Process Parameters	PVD [1]	Aerosol Deposition	Thermal Spray
Temperature	>500 °C	20 °C	>1000 °C
Pressure	<10 ⁻² torr	<10 torr	760 torr (1 atm)
Max Film Thickness	1 µm	100 µm	1 mm
Feedstock	Granule	Micropowder	Powder
Substrate prep	Clean/smooth	None	Grit blasting
Transport phase	Vapor	Solid	Solid/Liquid
Particle Size	Molecular	<5 um	40 um
Deposition rate	µm/hr	µm/min	µm/s
Gas consumption	none	10 SLPM	50 SLPM

AD Powders Characteristics

- Utilizes micron to submicron powders
- Not intuitive whether a powder will deposit well
 - Agglomeration
 - Compressibility index [2]

$$CI = 100 \cdot \frac{V_B - VT}{V_B}$$

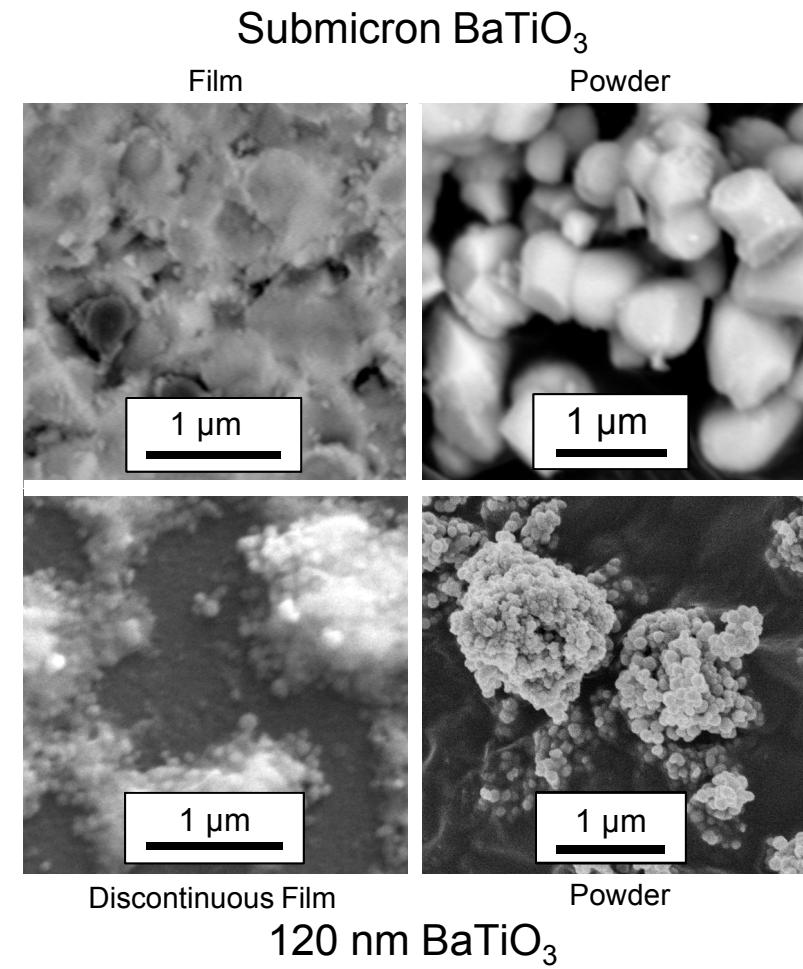
Relative particle sizes
of AD powders



SEM images of aerosol
deposited powders

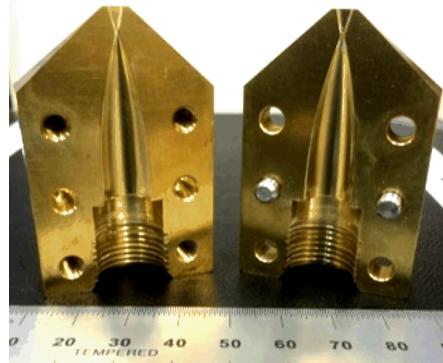
AD Powders

- Larger Particles (>400 nm)
 - Show evidence of plastic deformation in the form of “pancake” structure.
 - Can damage the substrate if highly agglomerated.
- Small particles (<200 nm)
 - Adhere to the substrate poorly
 - Retain their initial structure

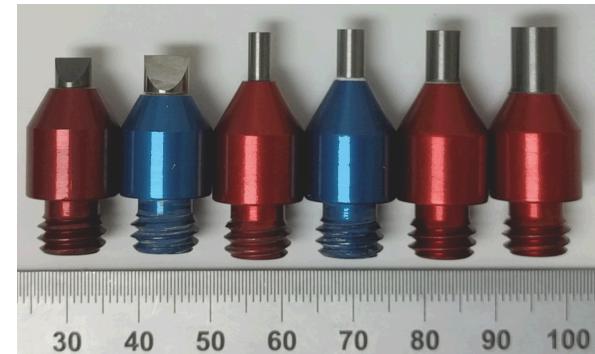
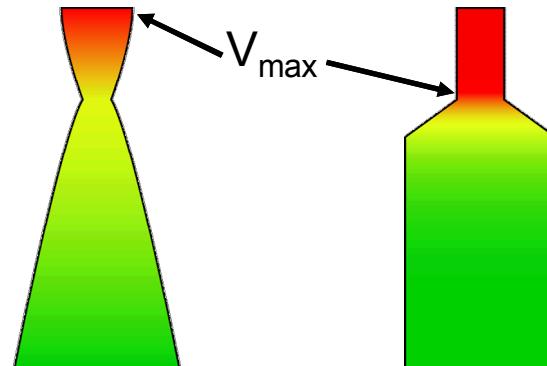


Velocity of Gas & Particles

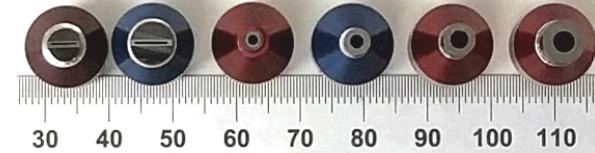
- Different Nozzles
 - Choked flow
 - Gas expansion
- “Critical velocity”
- Particle size and density



Converging-Diverging
De Laval Nozzle



Different cross sections of converging tungsten carbide nozzles (mm)



Kinetic Theory of Gases

- Approximations of drag on particles
- Neglect change in gas viscosity
- Molecular weight of gas

Drag force	$F_D = 3\pi\eta\nu d_p$
Slip corrected drag force equation for particles $< 1 \mu\text{m}$	$F_D = \frac{3\pi\eta\nu d_p}{C_c}$
Cunningham (Slip) Correction factor	$C_c = 1 + \frac{2.5\lambda}{d_p}$
Mean free path of a gas	$\lambda = \frac{1}{\sqrt{2}\pi n(d_m)^2}$

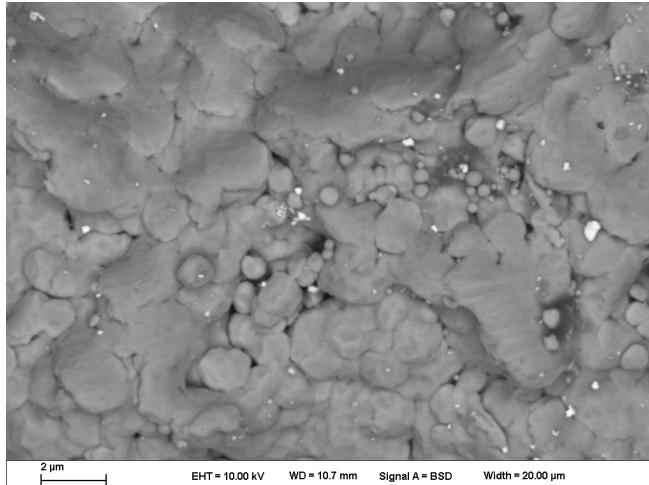
	760 torr	10 torr
F_D	$2.03 \cdot 10^{-8} \text{ N}$	$4.05 \cdot 10^{-9} \text{ N}$
λ	61 nm	4.65 μm

Parameters for a 1 μm
particle at 300 m/s

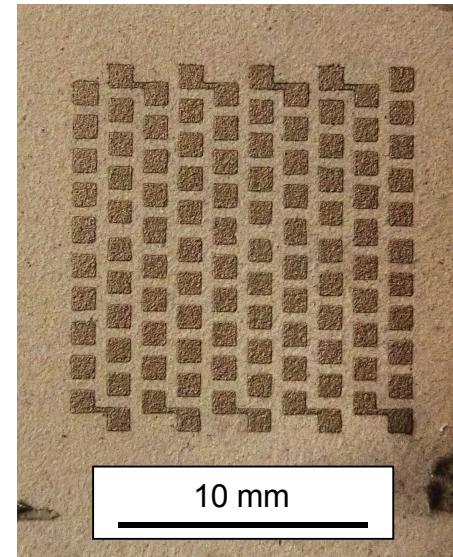
Equations for approximating
effects of gases on particles [3]

Metallic Electrical Interconnects

- Easy to deposit metals
 - High plasticity of particles
 - Films over 100 μm
- Patterned by direct applied masks



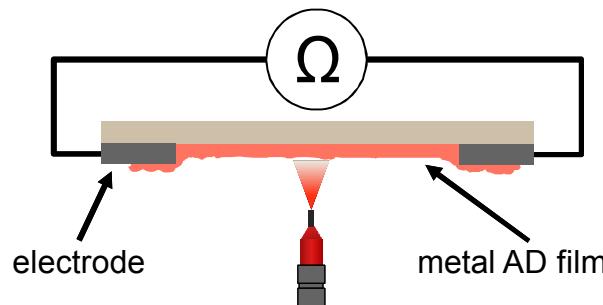
SEM image of Copper deposited by AD



Patterned Nickel interconnects deposited through a mask

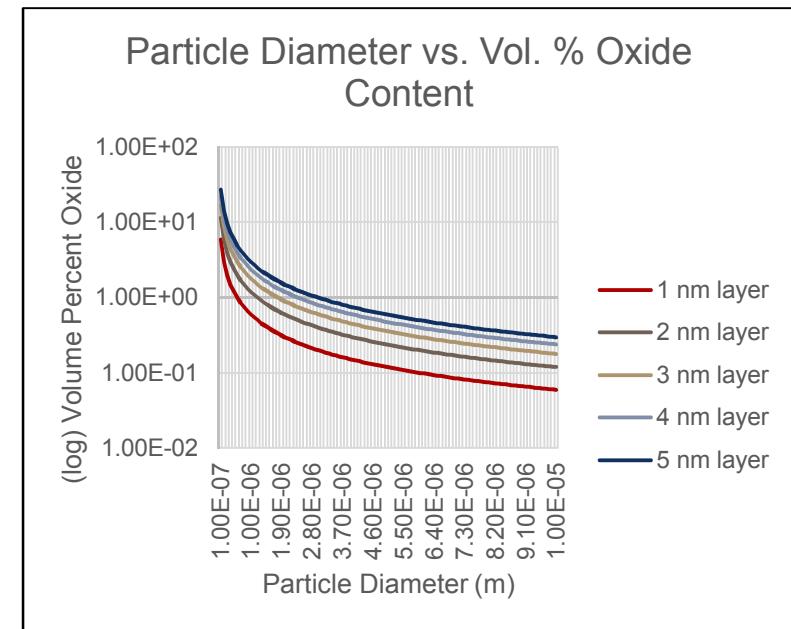
Metallic Electrical Interconnects

- Oxide content approximation (EDX images of Cu/Ni)
- Resistivity approximations
 - Nordheim's equation (mixing rule)
 - Grain boundary scattering
- Resistivity measurements
 - Four point probe method
 - In-situ measurement



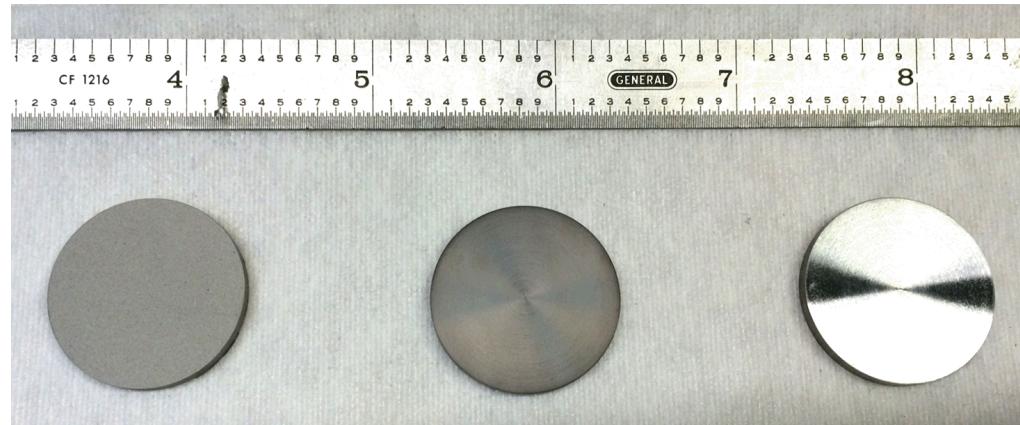
Apparatus for In-Situ
resistivity Measurements

$$\rho_{eff} = \rho_c \frac{1 + \frac{1}{2} \chi_d}{1 - \chi_d}$$



Thermal & Electrical Barriers

- Limits thermal damage
 - Maintain room temperature phases
 - Phonon scattering on grain boundaries
- Prevent conduction between surfaces
- Allow high temperature circuitry

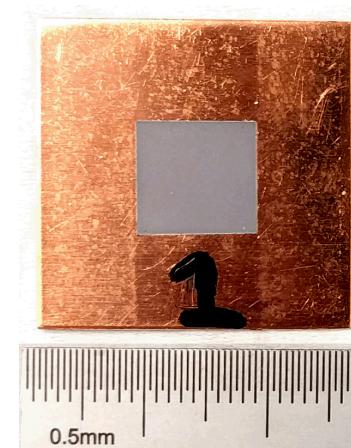


Thermal Spray
YSZ

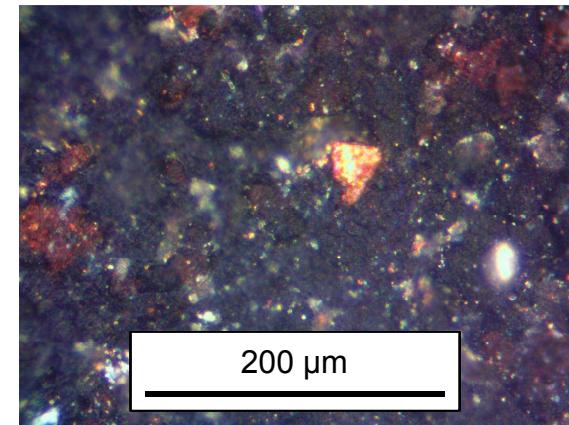
Aerosol
Deposited TiO₂

Uncoated

Hiperco Substrates



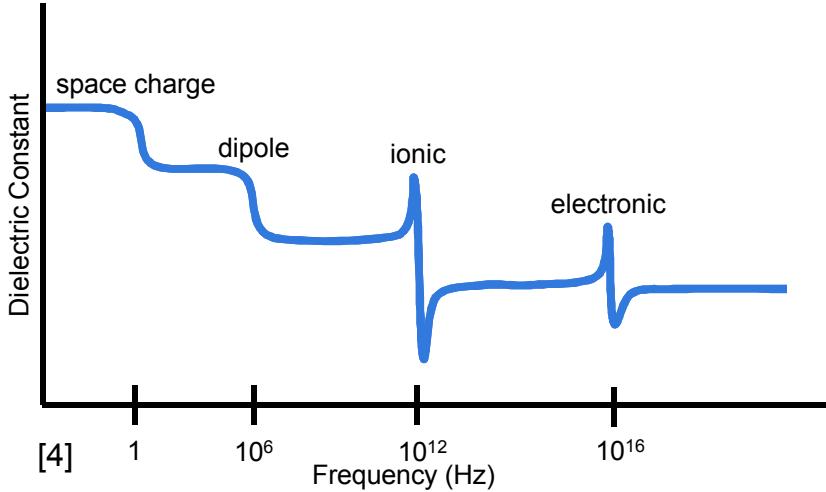
Insulating ceramic layer
deposited on copper



Pinholes through insulating
ceramic layers

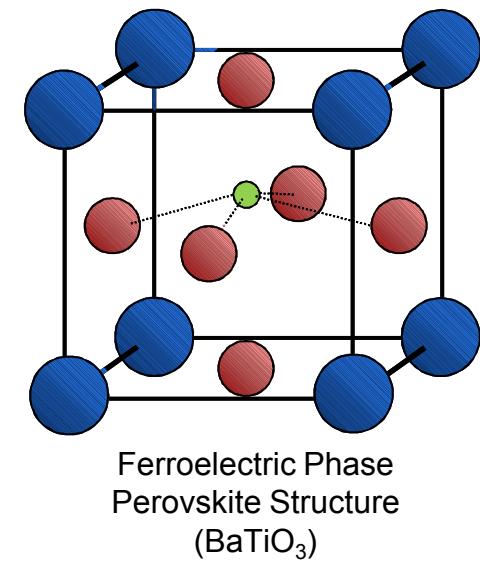
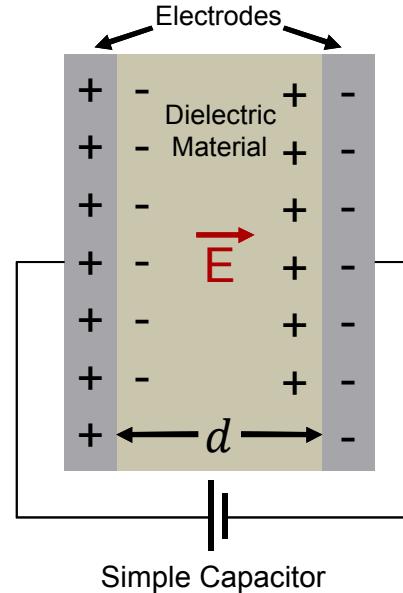
Dielectric Materials

- Dielectric Constant
- Barium Titanate
 - Ferroelectric property
- Polarization mechanisms
 - Frequency dependence
 - Dependence on grain size



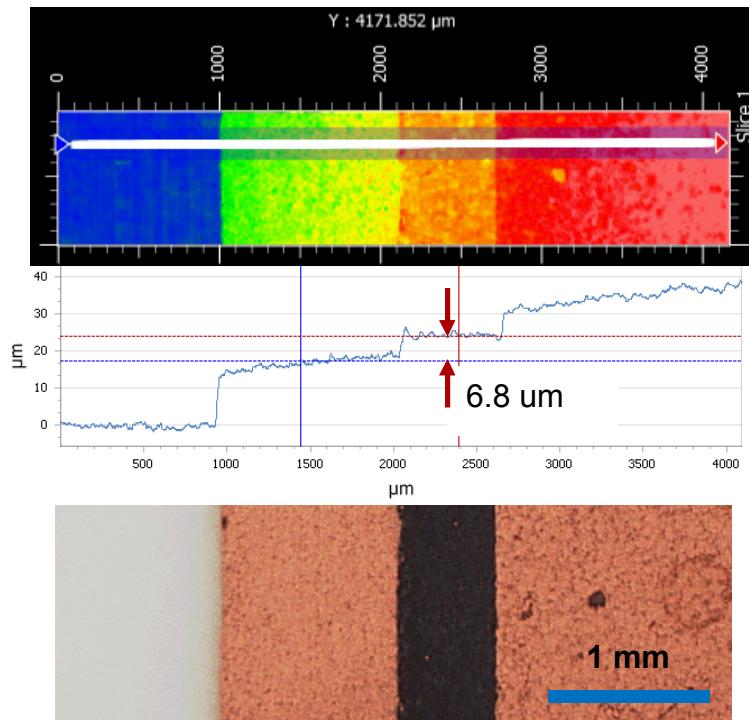
$$C = \frac{\epsilon_0 k A}{d}$$

Capacitance equation

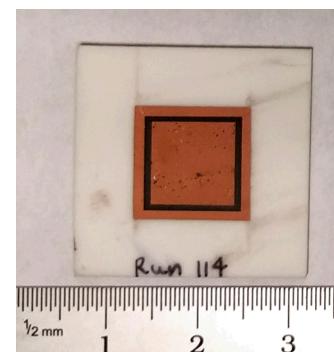


Multilayered Ceramic Capacitors

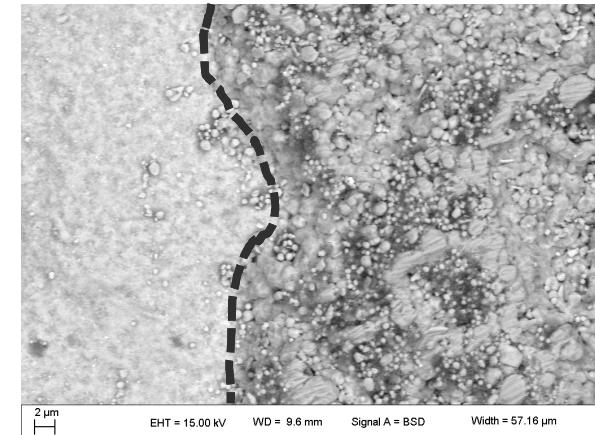
- Combines electrical interconnects and insulating barriers
- Directly applied electronic components



Cu-BaTiO₃-Cu Capacitor



BaTiO₃



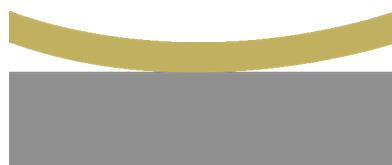
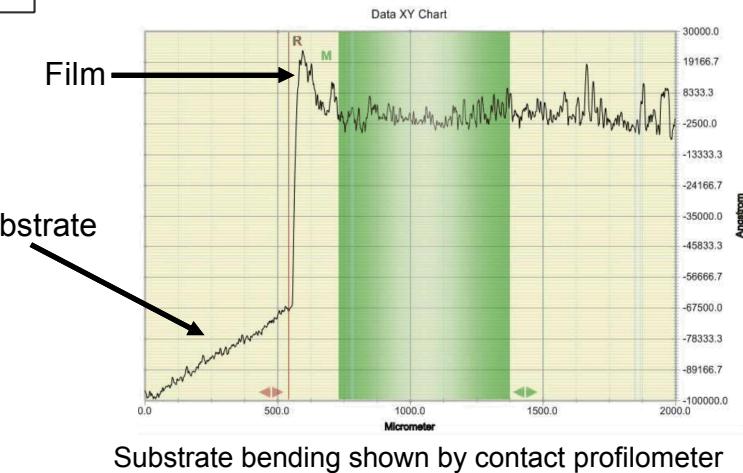
Cu

Stress in AD Films

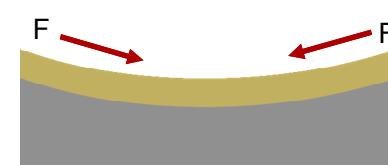
- High film stress
 - Substrate bending
- Film delamination
- Poor anchoring layer
- Stress higher than adhesion force
- Mitigation
 - Annealing
 - Energetic milling

$$\sigma = \frac{E_s h_s^2}{6h_f(1 - \nu_s)R}$$

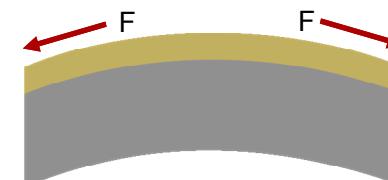
Stoney formula



Film Delamination
(compressive)



Compressive Stress



Tensile Stress

Conclusion

- Uniqueness of AD Process
 - Room temperature
 - Multi-material
 - Nanocrystalline structure
- Future Work
 - Develop process for higher deposition efficiency
 - Property measurements
 - Explore materials for AD

References

- [1] D. M. Mattox, *Handbook of Physical Vapor Deposition (PVD) Processing*. Park Ridge, N.J.: Noyes Publications, 1998.
- [2] J. Exner et al., “Powder requirements for aerosol deposition of alumina films”, *Adv. Powder Technol.*, vol. 26, no. 4, pp. 1143-1151, Jul. 2015.
- [3] W.C. Hinds, *Aerosol Technology: Properties, Behavior, and Measurement of Airborne Particles*. New York: Wiley, 1999.
- [4] S. Kasap, *Principles of electronic materials and devices*. Boston: McGraw-Hill, 2006.

End

Questions?