

Bifurcation theory applied to granite under general states of stress

M.D. Ingraham, T.A. Dewers, M. Williams, C.S.N. Cheung, B.C. Haimson

Introduction

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 - 3D Failure Surfaces
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3D Stress State: Invariants

- $\theta = \tan^{-1} \left[\frac{\sigma_1 - 2\sigma_2 + \sigma_3}{\sqrt{3}(\sigma_1 - \sigma_3)} \right]$

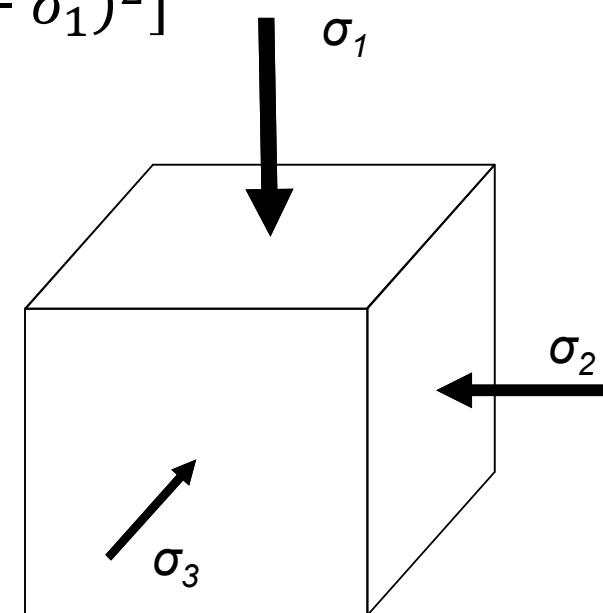
- $\sigma_m = \frac{\sigma_1 + \sigma_2 + \sigma_3}{3}$

- $\tau = \sqrt{\frac{1}{6} [(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2]}$

- $I_1 = 3\sigma_m$

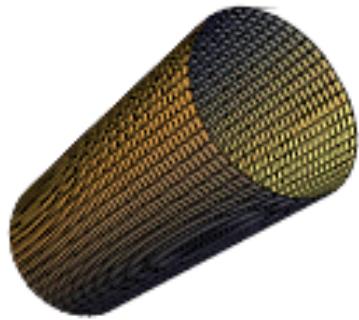
- $\tau = \sqrt{J_2}$

- $\sin 3\theta = -\frac{\sqrt{27}J_3}{2\tau^3}$

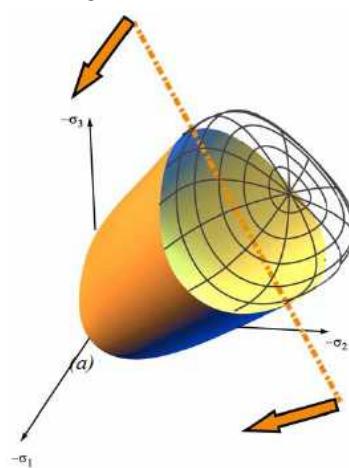


3D Failure Surfaces

Von Mises



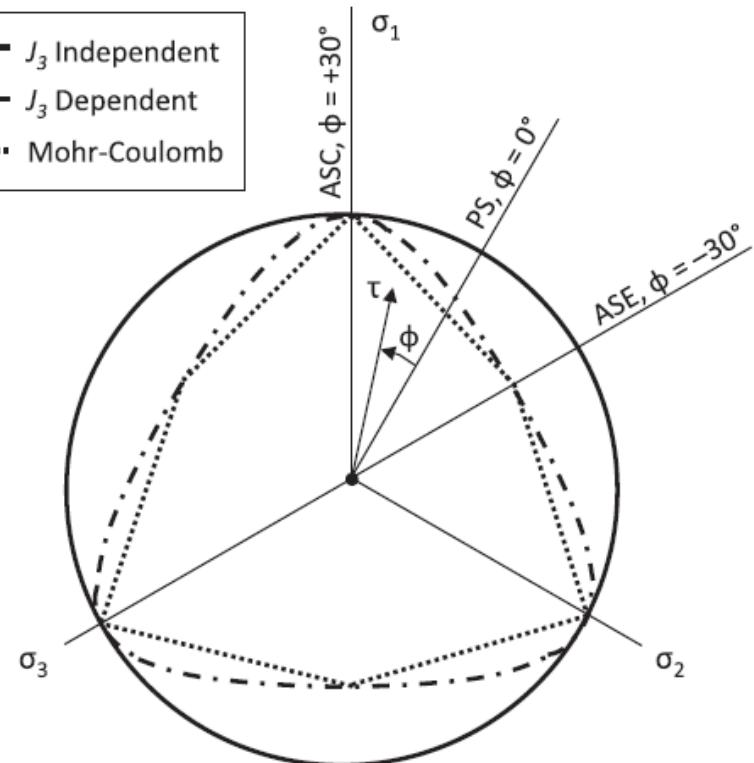
J_3 Dependent



Mohr-Coulomb

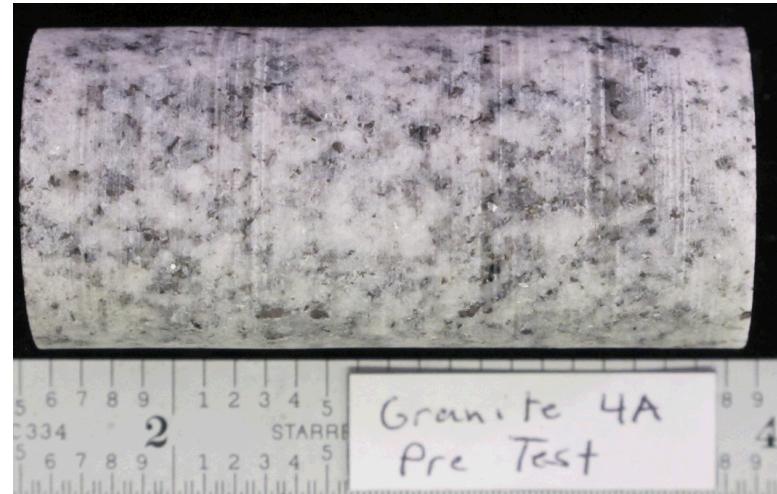


- J_3 Independent
- · — J_3 Dependent
- Mohr-Coulomb

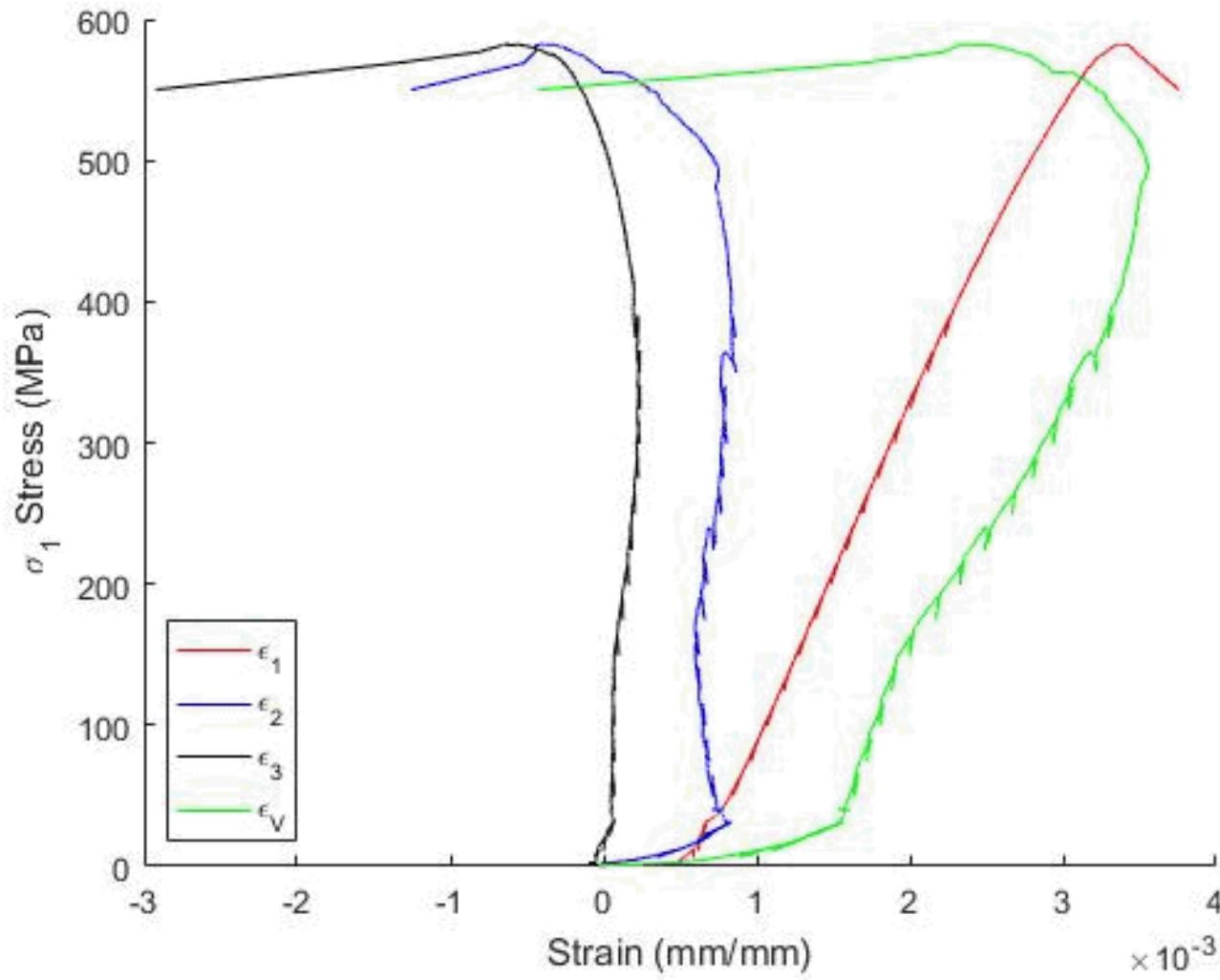


Sierra White Granite

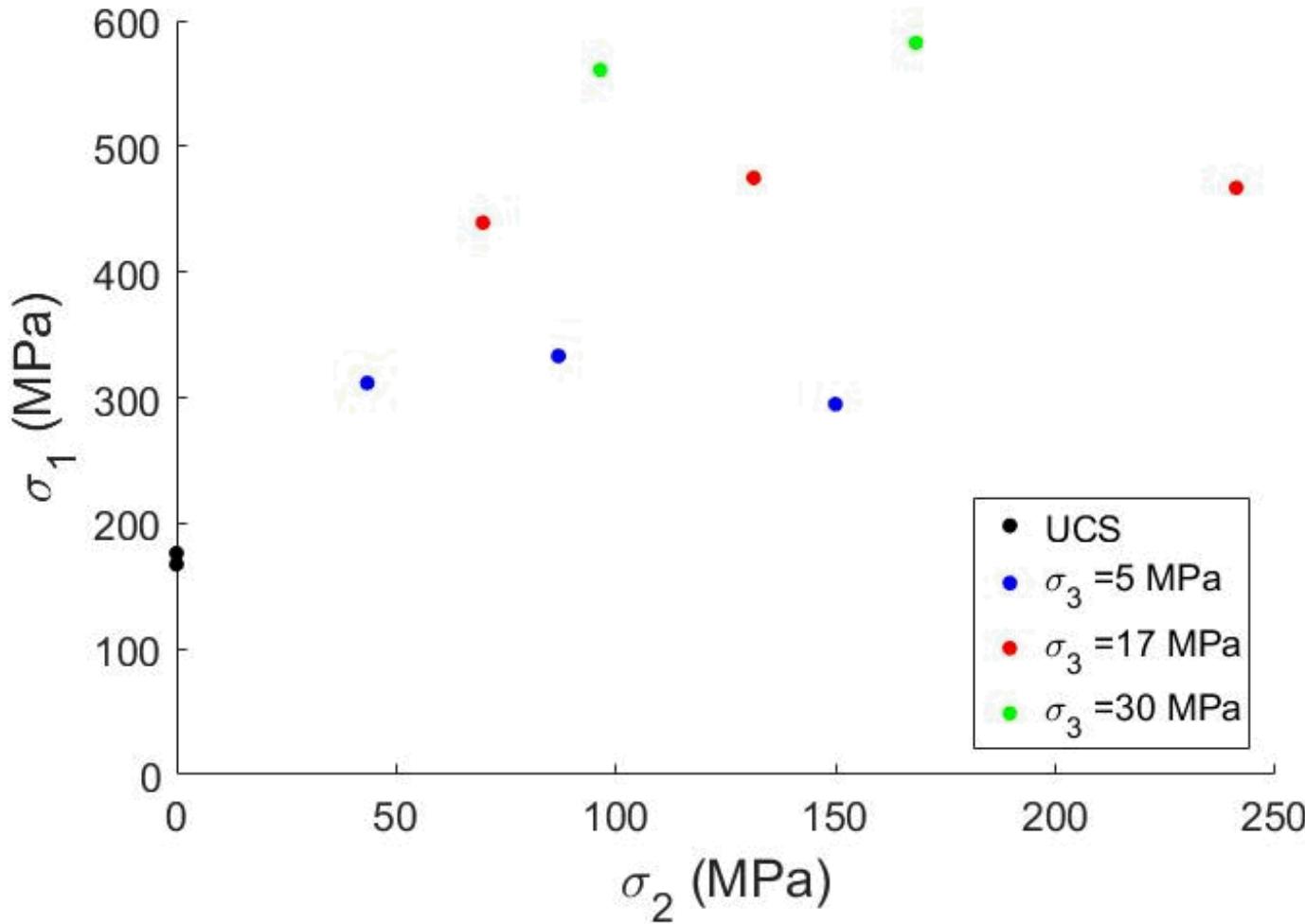
- UCS – 176.2 Mpa
- Density – 2.64 g/cc
- Grain size 1-3 mm
- Youngs Modulus – 48.5 Gpa
- Poisson's Ratio – 0.22
- Comprised of oligoclase, quartz, orthoclase, biotite, muscovite, and other trace.



Stress-strain response



σ_2 Dependence



Bifurcation Condition

$$\alpha = \frac{\pi}{4} + \frac{1}{2} \sin^{-1} \left[\frac{\frac{2}{3}(1+\nu)(\beta+\mu) - N_{II}(1-2\nu)}{\sqrt{4-3N_{II}^2}} \right]$$

$$N_{II} = \frac{\sigma_m - \sigma_2}{\tau}$$

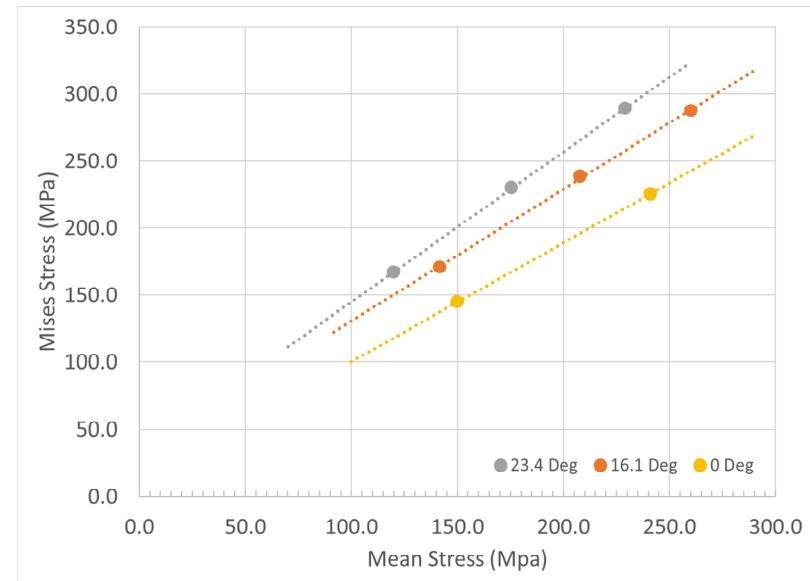
ν = Poisson's Ratio

α = Band angle

β = Plastic potential

μ = Slope of the yield surface

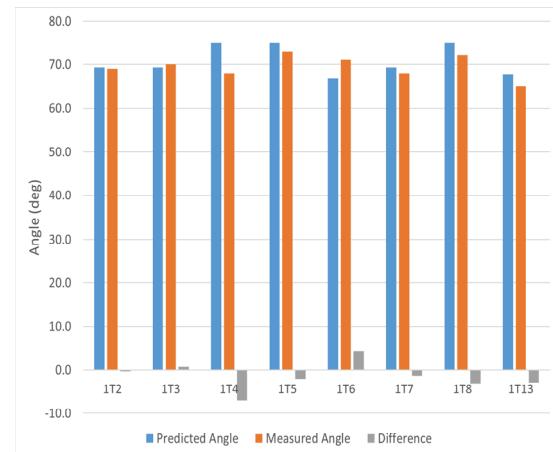
Bifurcation in this form developed by Rudnicki and Olsson (1998)



- Assumptions
 - Normality of the yield surface ($\beta = \mu$)
 - Failure surface is an acceptable proxy for yield surface
- In the region of interest the yield surface was represented by a straight line for each Lode angle

Bifurcation Results

	σ_m (MPa)	τ (MPa)	θ°	σ_3	α_m	α_p
1T2	260.2	287.5	16.1	30.1	69	69.4
1T3	141.7	170.8	16.1	5	70	69.3
1T4	120.1	167.0	23.4	5.1	68	75.0
1T5	175.4	230.0	23.4	17.2	73	75.0
1T6	150.0	144.7	0.0	5.3	71	66.7
1T7	207.8	238.4	16.1	17.0	68	69.3
1T8	229.2	289.2	23.4	30.2	72	75.0
1T13	241.2	225.7	0.0	15.5	65	67.8

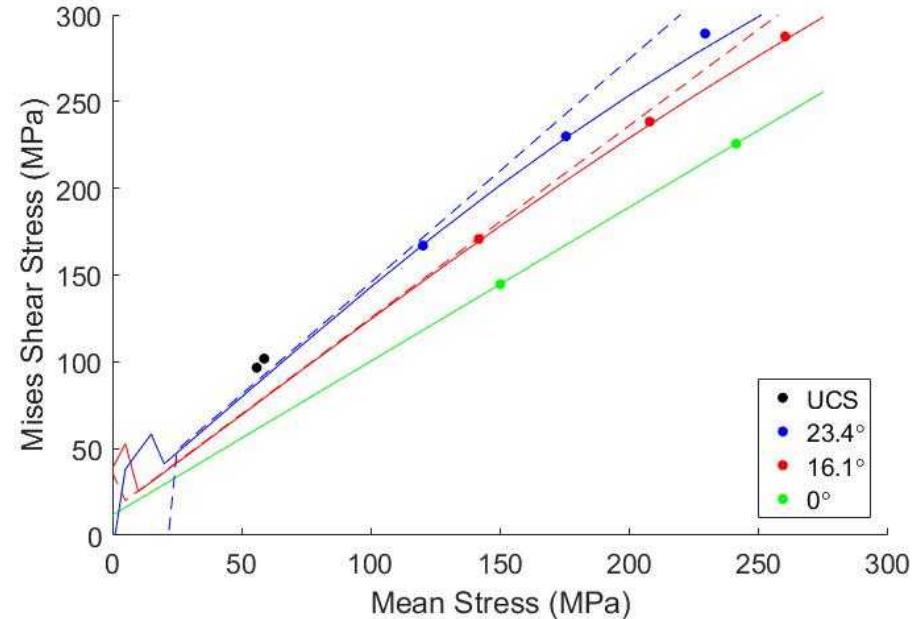


Modified Matsuoka-Nakai-Lade-Duncan

$$\sqrt{\frac{4}{27}} A(\sigma) \sin(3) \left(\frac{\tau}{\tau_0(\sigma)} \right)^3 + \left(\frac{\tau}{\tau_0(\sigma)} \right)^2 - 1 = 0$$

$$\tau_0(\sigma) = 0.8878\sigma + 11.604$$

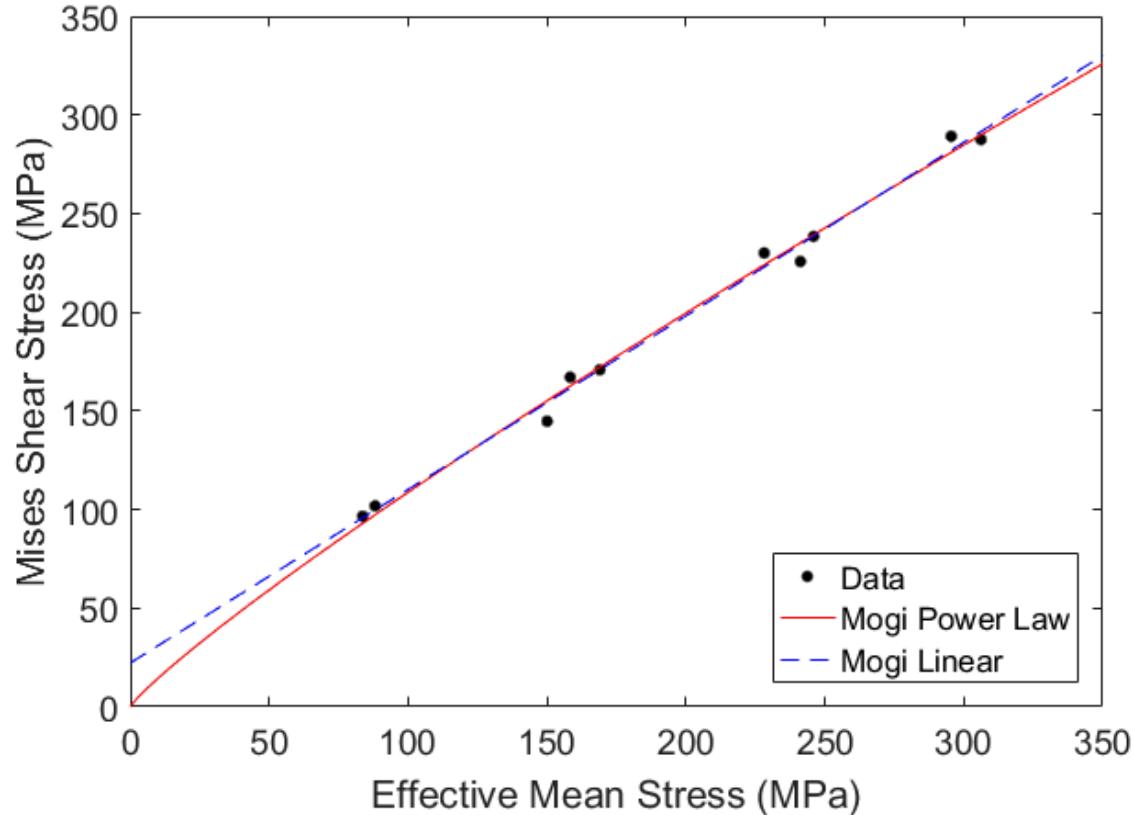
$$A(\sigma) = 5E^{-6}\sigma^2 - 0.0008\sigma - 0.9541$$



	Calculated A	Fit A	τ_0	Calculated τ	Actual τ	τ Difference
1A	-0.989	-0.984	63.76	100.2	101.8	1.6
3A	-0.989	-0.983	61.13	95.9	96.6	0.7
1T2	-0.844	-0.824	242.65	285.7	287.5	1.8
1T3	-0.987	-0.967	137.40	169.5	170.8	1.3
1T4	-0.975	-0.978	118.20	167.6	167.0	-0.6
1T5	-0.945	-0.941	167.32	229.0	230.0	1.0
1T7	-0.925	-0.905	196.07	236.8	238.4	1.6
1T8	-0.918	-0.875	215.07	281.0	289.2	8.2

Mogi Criterion

- $\sigma_{me} = \frac{(\sigma_1 + \sigma_3)}{2}$
- $\tau = a + b\sigma_{me}$
 - $a=22.21$
 - $b=0.880$
- $\tau = \alpha\sigma_{me}^n$
 - $\alpha=1.923$
 - $n=0.8762$



Correlation coefficient is nearly the same for both methods (0.993 and 0.992 respectively)

Conclusions

- Failure depends on σ_2
- Band angle predictions match well with experiments
 - Noteworthy considering assumptions made
- Results are well modeled by both mMNLD model, and both Mogi criteria
- Selection of model depends on data available and intended use for model (are invariants required?)

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