

# Bifurcation theory applied to granite under general states of stress

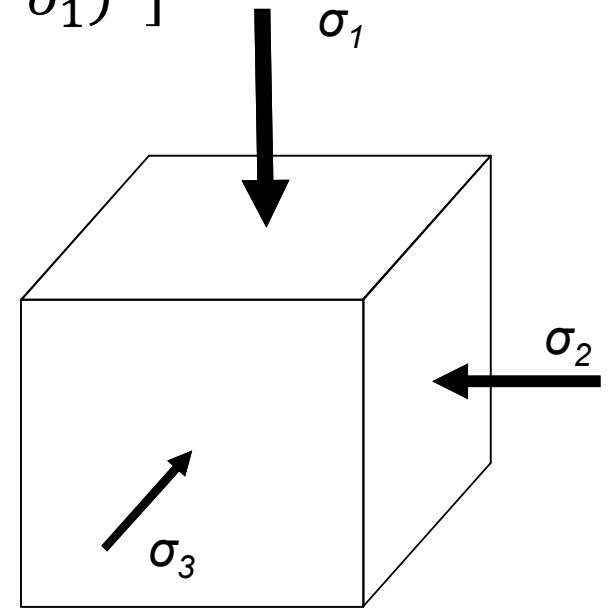
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# Introduction

- 3D stress state
  - Invariants
  - 3D Failure Surfaces
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  - Response to 3D stresses
  - $\sigma_2$  dependence
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- Conclusions

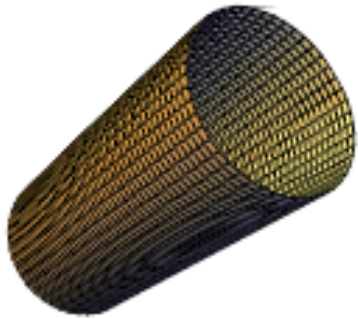
# 3D Stress State: Invariants

- $\theta = \tan^{-1} \left[ \frac{\sigma_1 - 2\sigma_2 + \sigma_3}{\sqrt{3}(\sigma_1 - \sigma_3)} \right]$
- $\sigma_m = \frac{\sigma_1 + \sigma_2 + \sigma_3}{3}$
- $\tau = \sqrt{\frac{1}{6} [(\sigma_1 - \sigma_2)^2 + (\sigma_2 - \sigma_3)^2 + (\sigma_3 - \sigma_1)^2]}$
- $I_1 = 3\sigma_m$
- $\tau = \sqrt{J_2}$
- $\sin 3\theta = -\frac{\sqrt{27}J_3}{2\tau^3}$

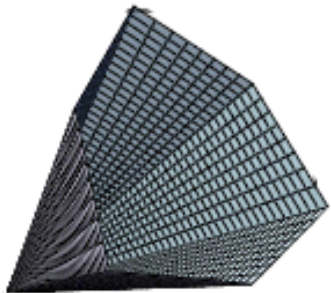


# 3D Failure Surfaces

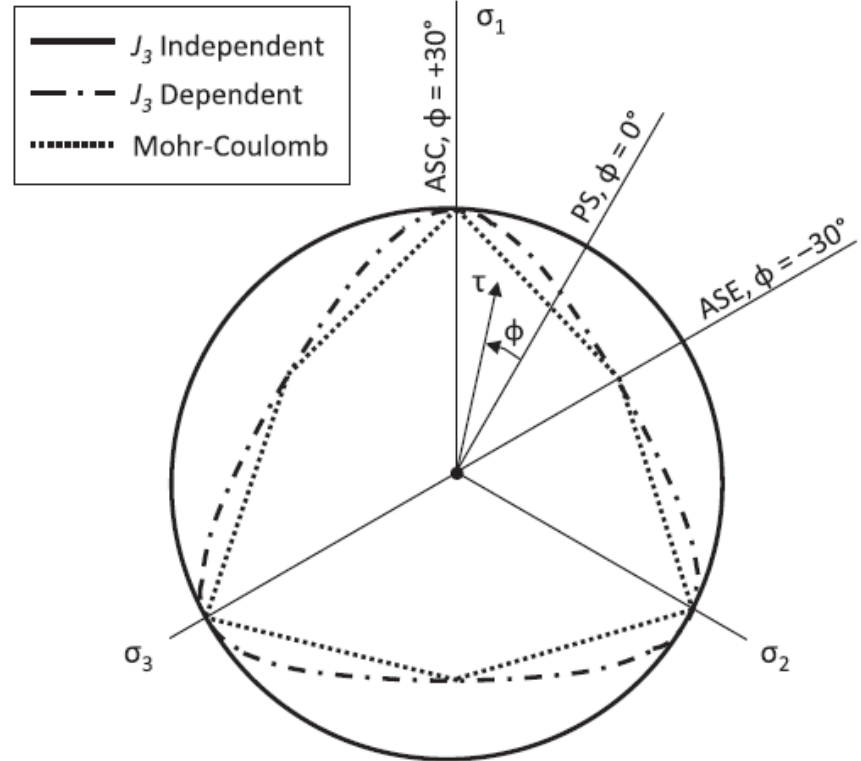
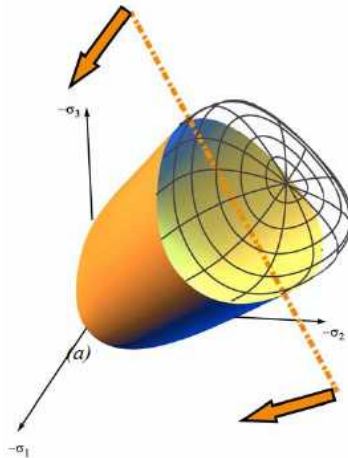
Von Mises



Mohr-Coulomb

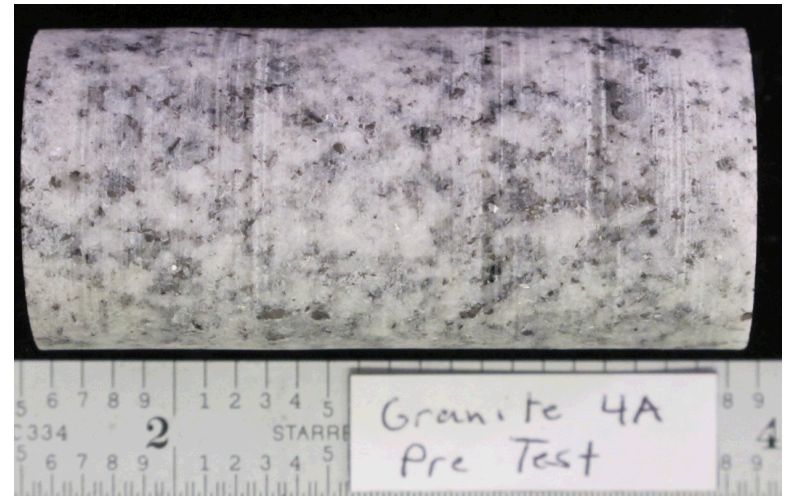


$J_3$  Dependent

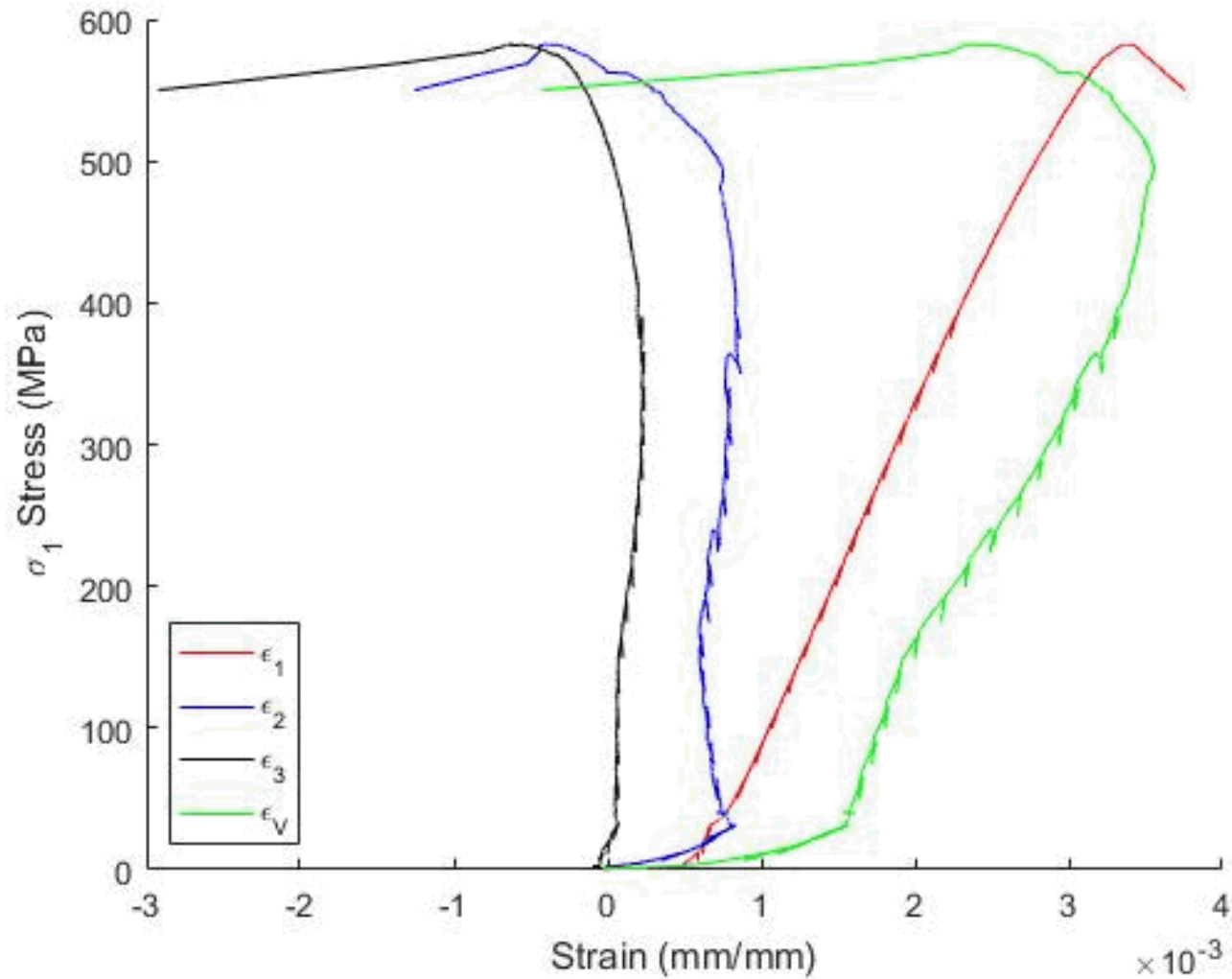


# Sierra White Granite

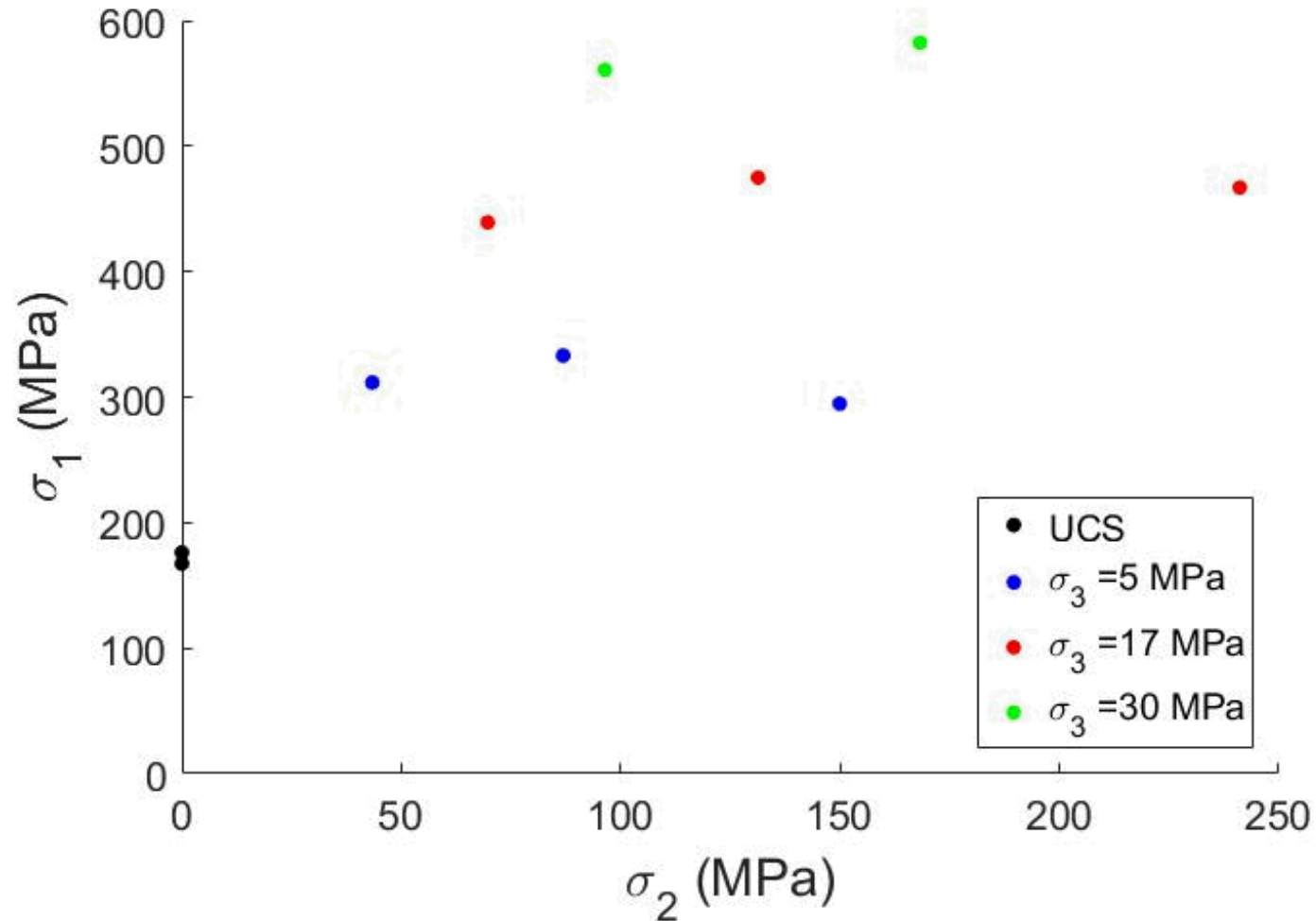
- UCS – 176.2 Mpa
- Density – 2.64 g/cc
- Grain size 1-3 mm
- Youngs Modulus – 48.5 Gpa
- Poisson's Ratio – 0.22
- Comprised of oligoclase, quartz, orthoclase, biotite, muscovite, and other trace.



# Stress-strain response



# $\sigma_2$ Dependence



# Bifurcation Condition

$$\alpha = \frac{\pi}{4} + \frac{1}{2} \sin^{-1} \left[ \frac{\frac{2}{3}(1 + \nu)(\beta + \mu) - N_{II}(1 - 2\nu)}{\sqrt{4 - 3N_{II}^2}} \right]$$

$$N_{II} = \frac{\sigma_m - \sigma_2}{\tau}$$

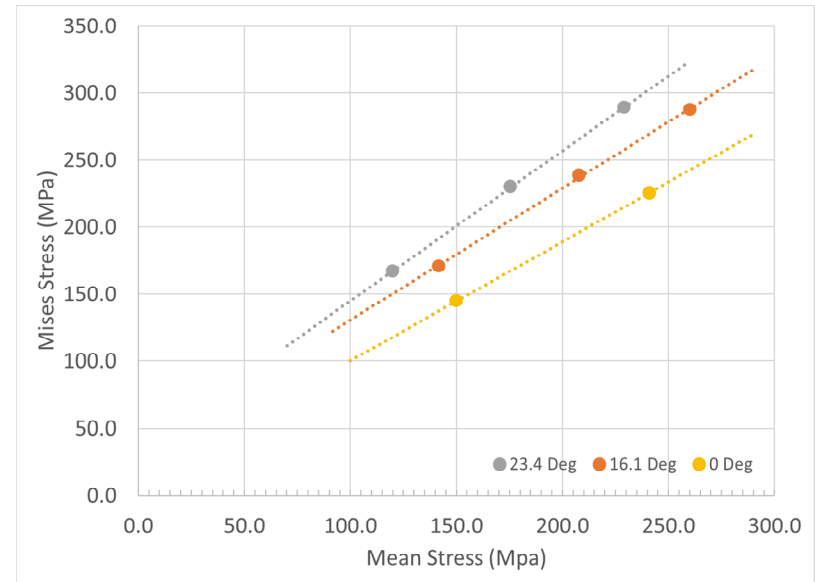
$\nu$  = Poisson's Ratio

$\alpha$  = Band angle

$\beta$  = Plastic potential

$\mu$  = Slope of the yield surface

Bifurcation in this form developed by Rudnicki and Olsson (1998)



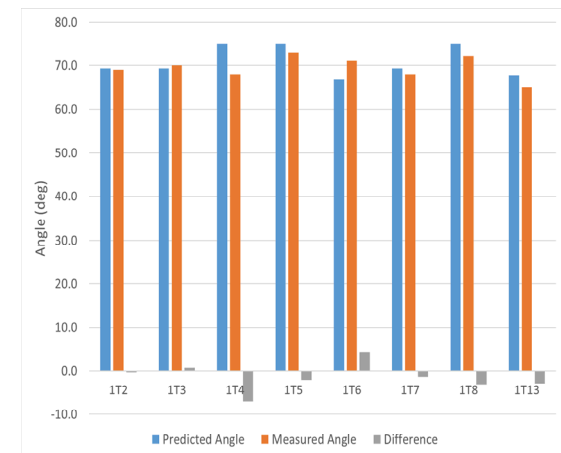
## ■ Assumptions

- Normality of the yield surface ( $\beta = \mu$ )
- Failure surface is an acceptable proxy for yield surface
- In the region of interest the yield surface was represented by a straight line for each Lode angle



# Bifurcation Results

	$\sigma_m$ (MPa)	$\tau$ (MPa)	$\theta^\circ$	$\sigma_3$	$\alpha_m$	$\alpha_p$
1T2	260.2	287.5	16.1	30.1	69	69.4
1T3	141.7	170.8	16.1	5	70	69.3
1T4	120.1	167.0	23.4	5.1	68	75.0
1T5	175.4	230.0	23.4	17.2	73	75.0
1T6	150.0	144.7	0.0	5.3	71	66.7
1T7	207.8	238.4	16.1	17.0	68	69.3
1T8	229.2	289.2	23.4	30.2	72	75.0
1T13	241.2	225.7	0.0	15.5	65	67.8

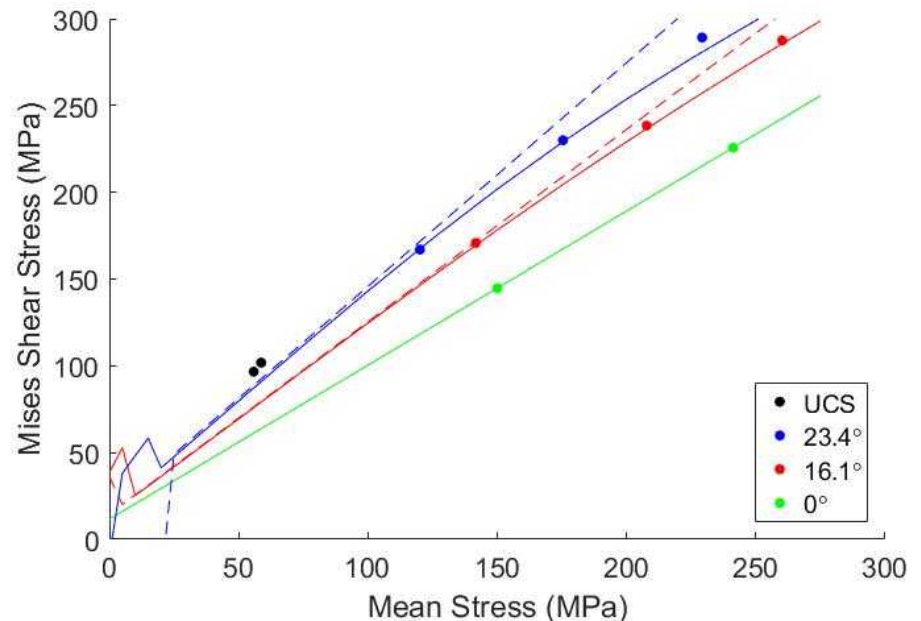


# Modified Matsuoka-Nakai-Lade-Duncan

$$\sqrt{\frac{4}{27}} A(\sigma) \sin(3) \left( \frac{\tau}{\tau_0(\sigma)} \right)^3 + \left( \frac{\tau}{\tau_0(\sigma)} \right)^2 - 1 = 0$$

$$\tau_0(\sigma) = 0.8878\sigma + 11.604$$

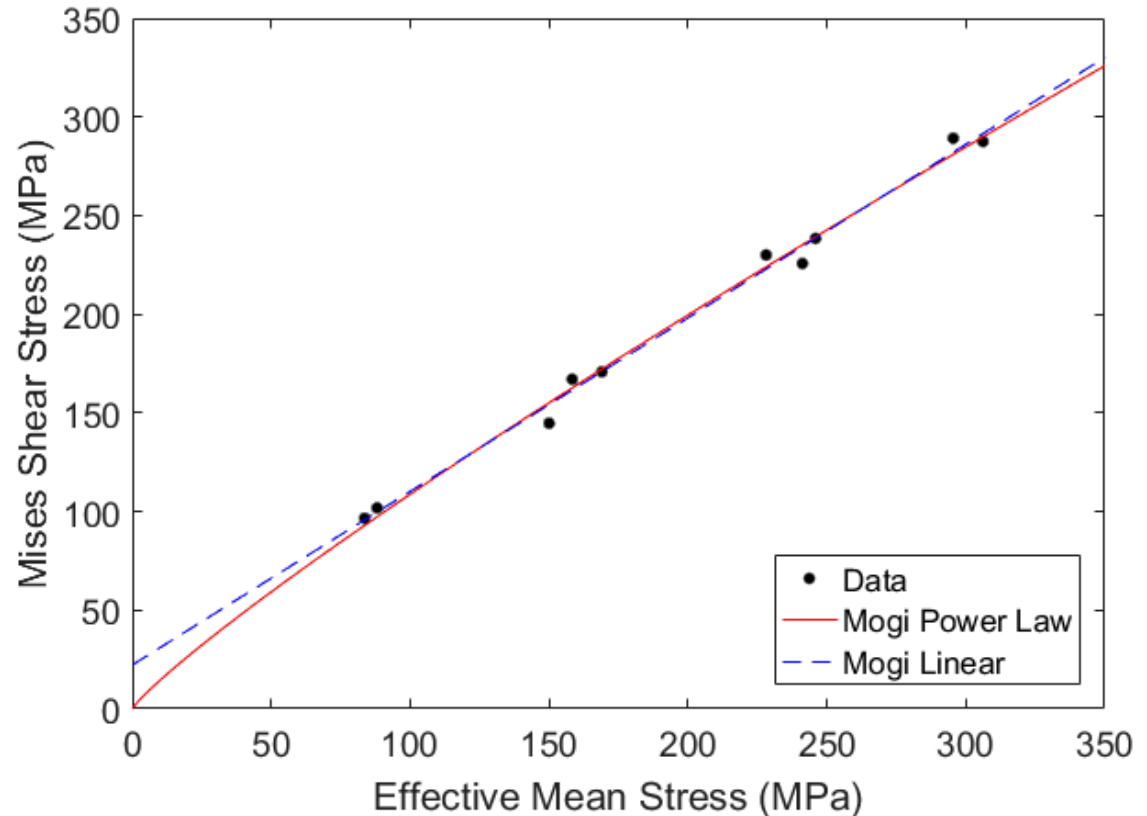
$$A(\sigma) = 5E^{-6}\sigma^2 - 0.0008\sigma - 0.9541$$



	Calculated A	Fit A	$\tau_0$	Calculated $\tau$	Actual $\tau$	$\tau$ Difference
1A	-0.989	-0.984	63.76	100.2	101.8	1.6
3A	-0.989	-0.983	61.13	95.9	96.6	0.7
1T2	-0.844	-0.824	242.65	285.7	287.5	1.8
1T3	-0.987	-0.967	137.40	169.5	170.8	1.3
1T4	-0.975	-0.978	118.20	167.6	167.0	-0.6
1T5	-0.945	-0.941	167.32	229.0	230.0	1.0
1T7	-0.925	-0.905	196.07	236.8	238.4	1.6
1T8	-0.918	-0.875	215.07	281.0	289.2	8.2

# Mogi Criterion

- $\sigma_{me} = \frac{(\sigma_1 + \sigma_3)}{2}$
- $\tau = a + b\sigma_{me}$ 
  - $a=22.21$
  - $b=0.880$
- $\tau = \alpha\sigma_{me}^n$ 
  - $\alpha=1.923$
  - $n=0.8762$



Correlation coefficient is nearly the same for both methods (0.993 and 0.992 respectively)

# Conclusions

- Failure depends on  $\sigma_2$
- Band angle predictions match well with experiments
  - Noteworthy considering assumptions made
- Results are well modeled by both mMNLD model, and both Mogi criteria
- Selection of model depends on data available and intended use for model (are invariants required?)

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