



SAND2017-1108PE

Adhesive Joint Failure and the Aging of Adhesive Joints

TCG-XIV – Munitions Reliability and Lifecycle Technology

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Our Vision: Validated Model-Based Lifecycle Engineering for Packaging Design

Polymer Nonlinear Viscoelastic (NLVE) Model

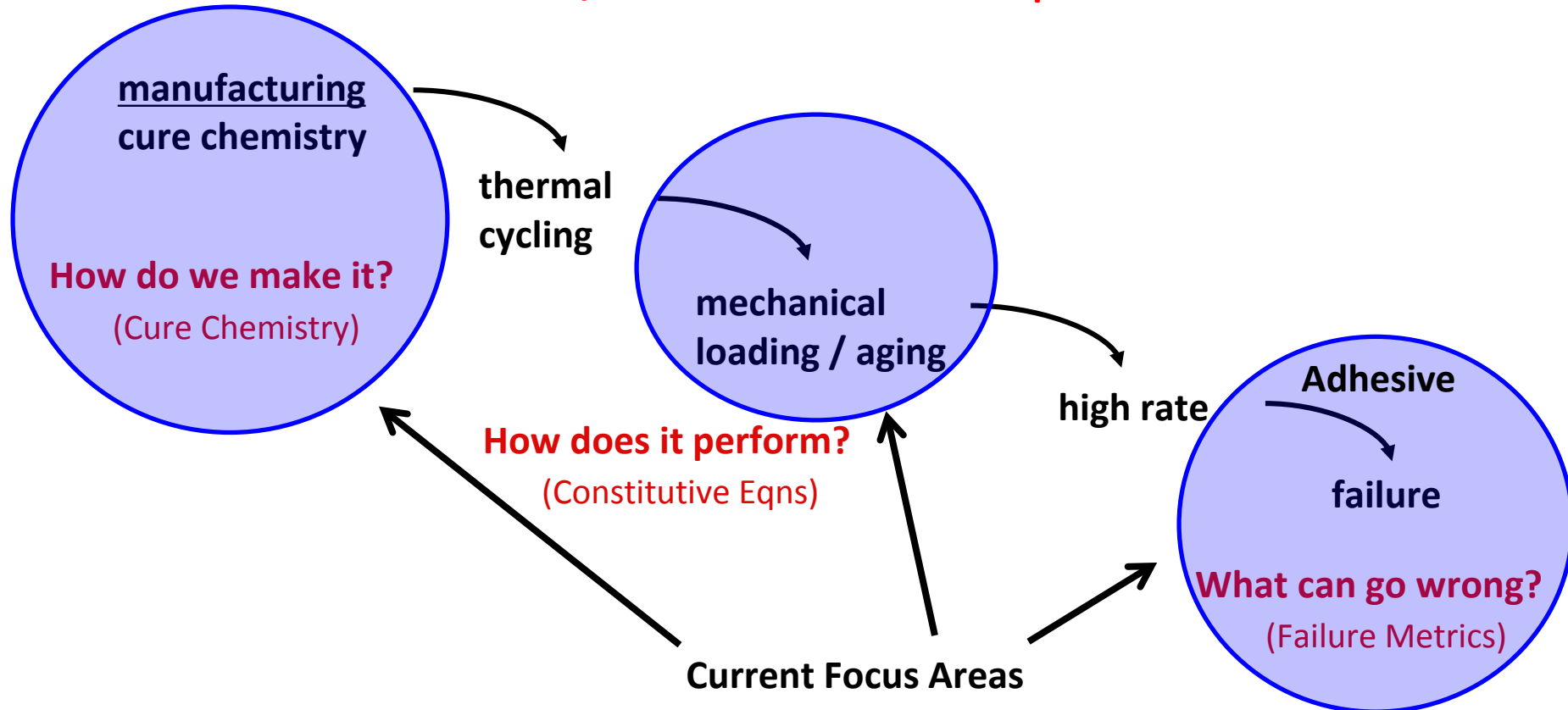
J.M. Caruthers, et al., *Polymer*, 2004, 45, 4577

D.B. Adolf, et al., *Polymer*, 2004, 45, 4599

D.B. Adolf, et al., *Polymer*, 2009, 50, 4257

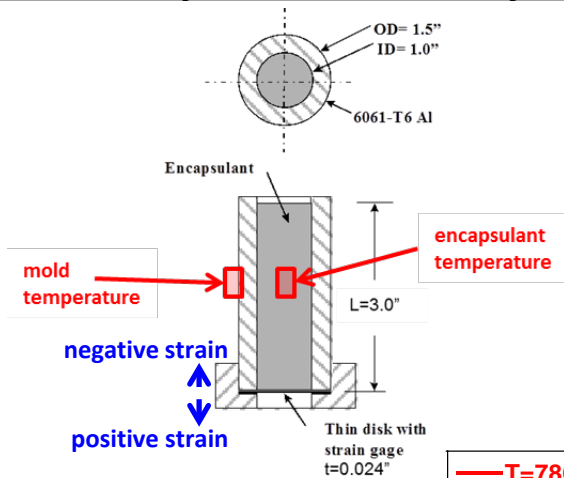


Current talk Predict Stress/Strain and Understand Impact on Performance

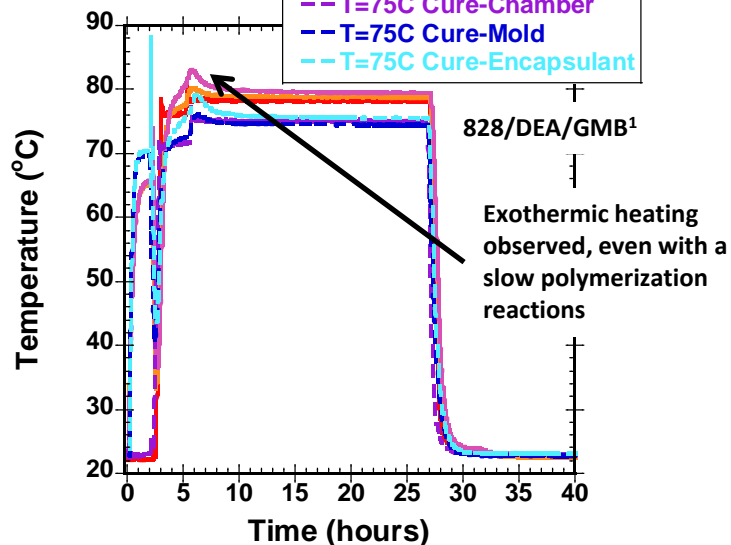


Why is Cure Stress Important?

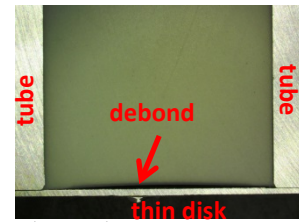
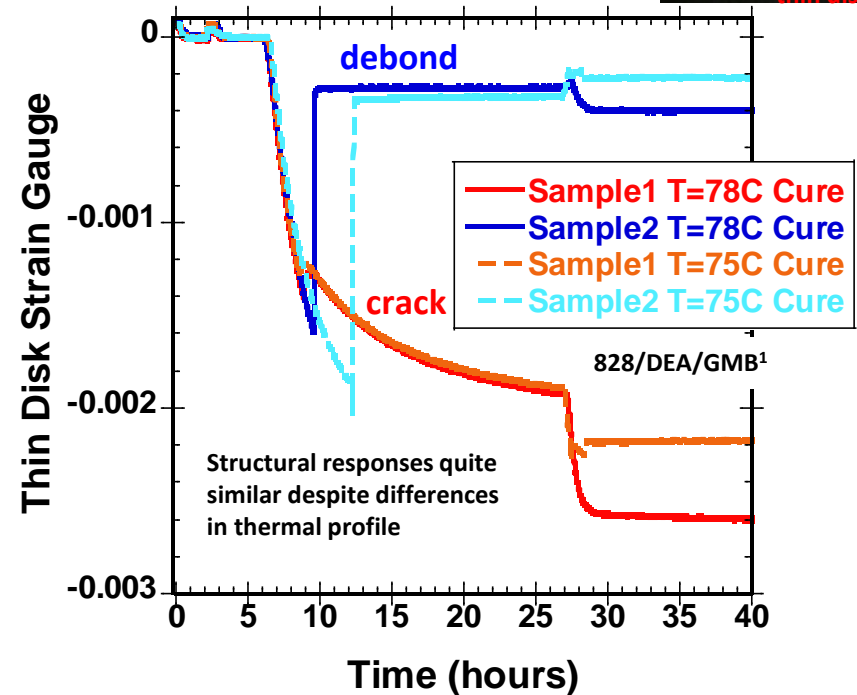
Geometry: Thin Disk on Cylinder



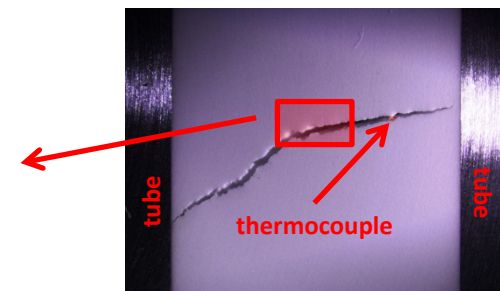
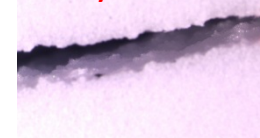
Temperature Profile



Structural Response



Rough crack surface consistent with "tearing" in rubbery state?



Failure can occur during cure!

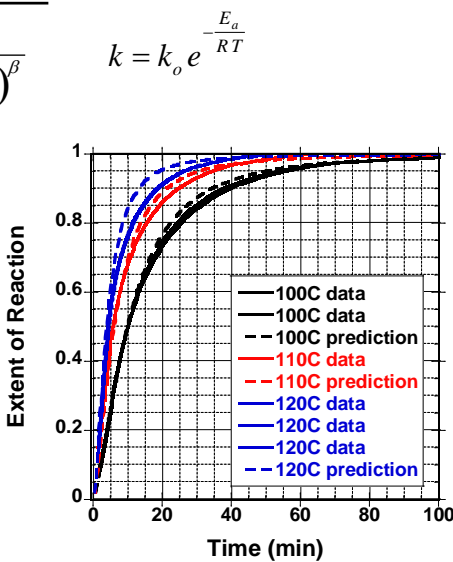
¹http://www.sandia.gov/polymer-properties/828_DEA_GMB.html

Predicting Cure Stress: Parameterizing the SPEC Cure Model

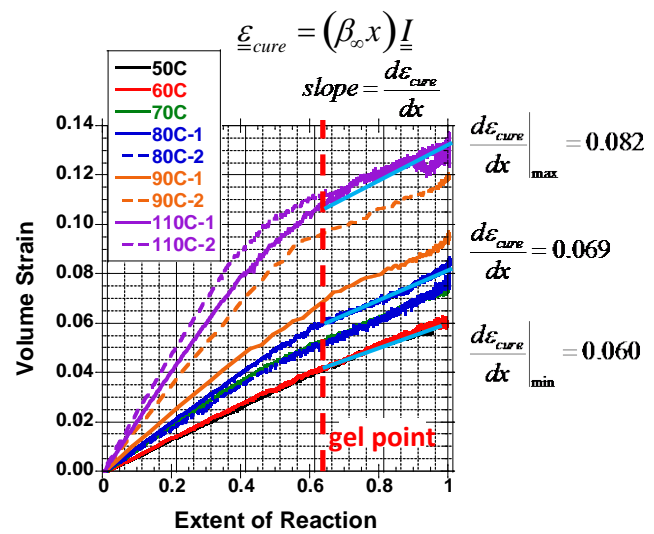
Reaction Kinetics

$$\frac{dx}{dt} = \hat{k}(b + x^m)(1 - x)^n \quad \hat{k} \equiv \frac{k}{(1 + w a)^\beta}$$

828/T403 Chemistry Limited Reaction Parameters	
Parameter	Value
E_a	13.8 kcal/mole
k_o	$2.17 \times 10^5 \text{ s}^{-1}$
b	0.17
m	0.33
n	1.37



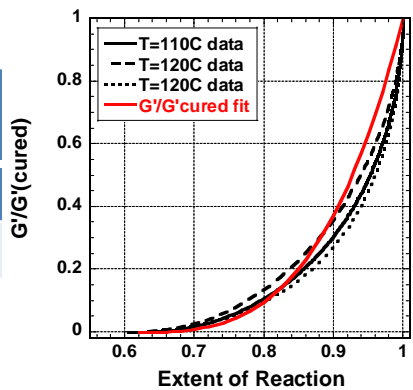
Volumetric Cure Shrinkage



Evolution of Equilibrium Shear Modulus During Cure

$$\frac{G_\infty(x)}{G_\infty(1)} = \left[\frac{x^2 - x_{gel}^2}{1 - x_{gel}^2} \right]^{8/3}$$

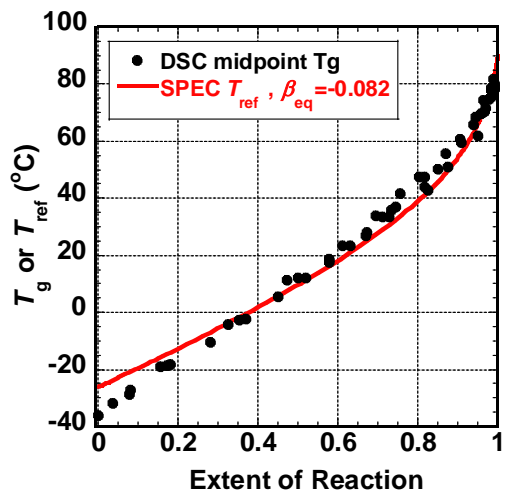
828/T403 $G_\infty(x)$ Parameterization	
Parameter	Value
x_{gel}	0.62



Evolution of Glass Transition Temperature During Cure

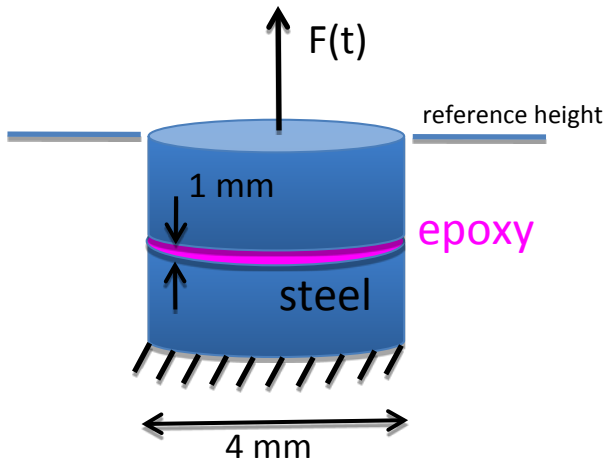
$$T_{ref}(x) = T_{ref} - \frac{[C_3\beta_\infty + C_5(x(t))](x(t) - x_{ref})}{(1 - C_3\alpha_\infty)} \quad C_5(x(t)) = C_{5a} + \frac{C_{5c}}{(C_{5d} - C_{5b}x)^{C_{5e}}}$$

828/T403 T_{ref} Parameterization	
Parameter	Value
C_3	900 C
α_∞	500 ppm/C
C_{5a}	10 C
C_{5b}	0.97
C_{5c}	-105 C
C_{5d}	1.0088
C_{5e}	0.73

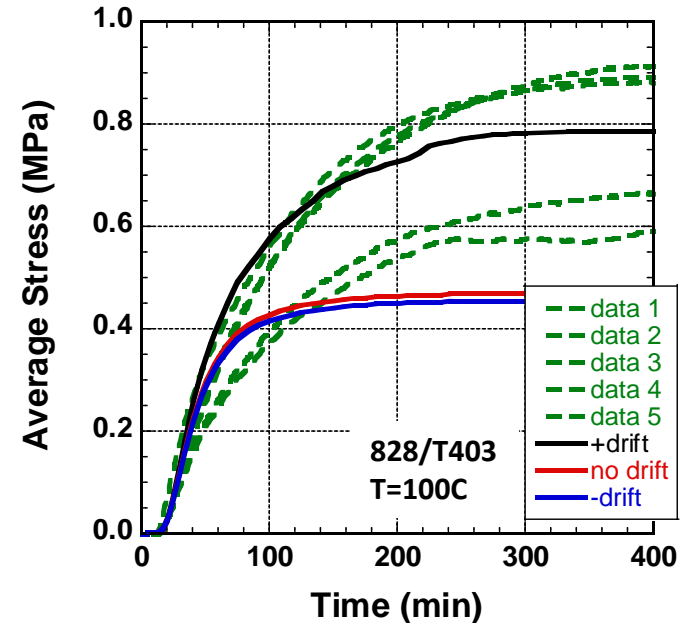


Predicting Cure Stress: Validation Tests

The Simple Test



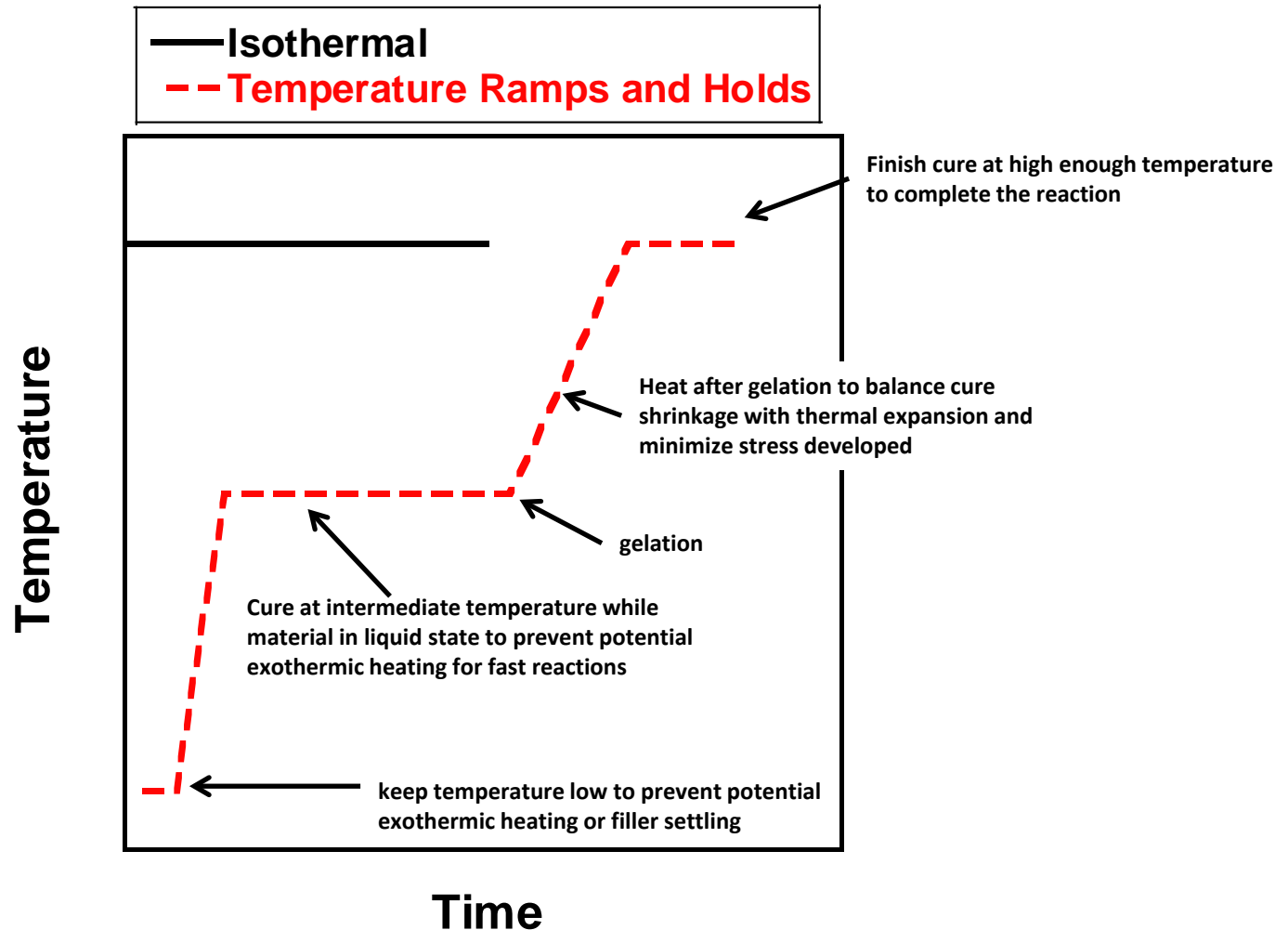
Rubbery Cure Results



Good agreement between predictions and data, with known variations in boundary conditions during the test accounting for the spread in the data

This capability will enable the design of cure schedules to minimize stress

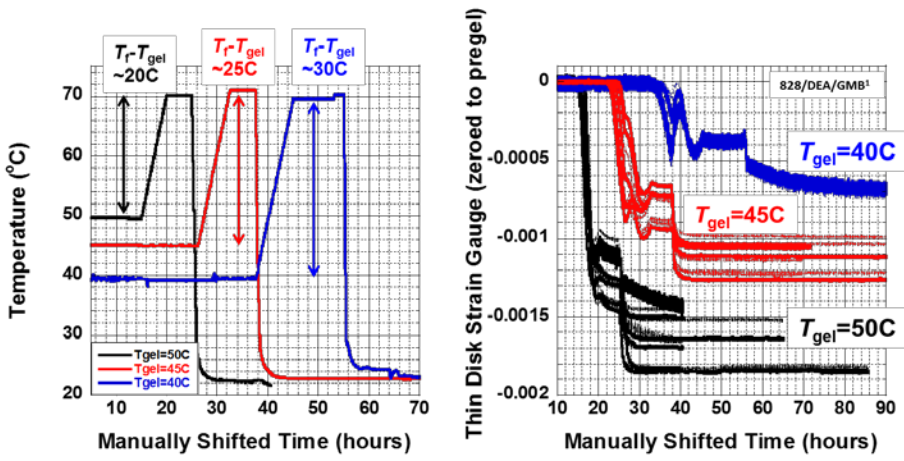
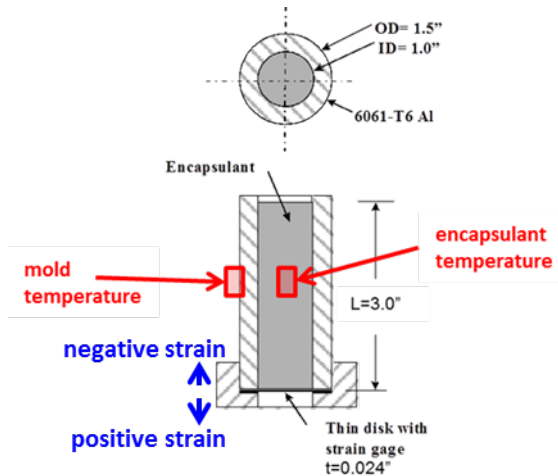
Designing an Optimum Cure Schedule



Isothermal reaction at a high temperature may be the fastest method to achieve complete cure, but other factors may drive the time-temperature profile in a different direction

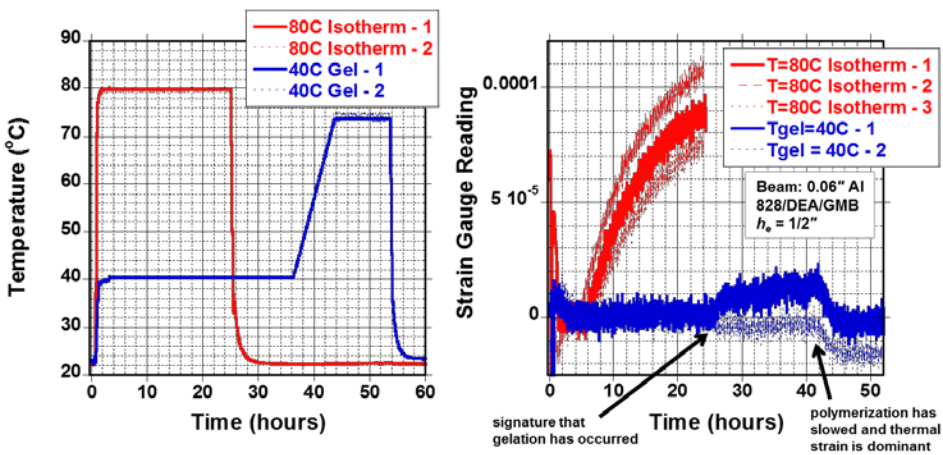
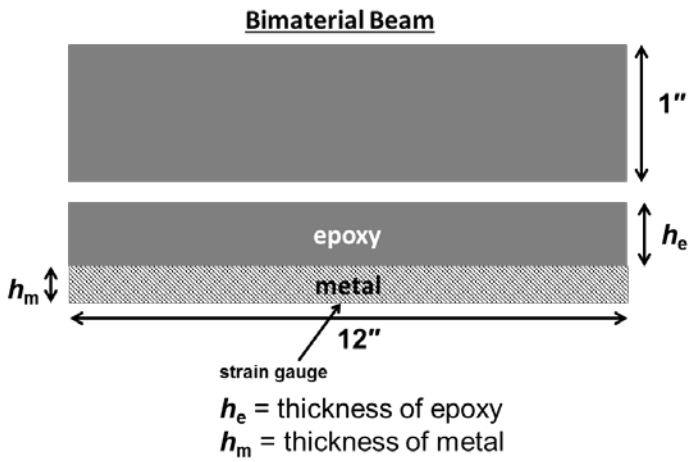
Designing Cure Schedules to Minimize Stress

Confined Cure



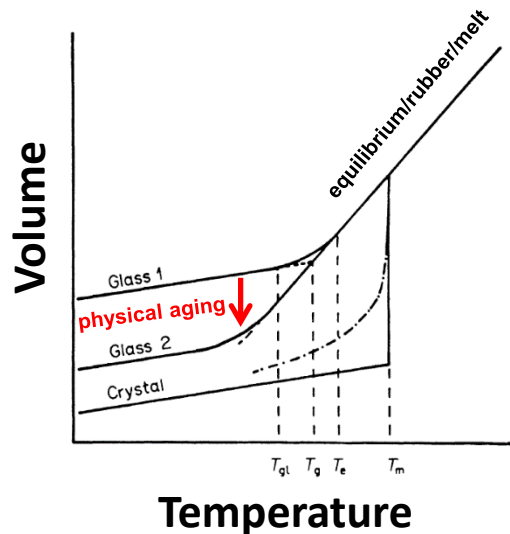
The difference between gel temperature (T_g) and final cure temperature (T_f) appears to be a primary factor in determining residual stress developed

Free-Surface Cure

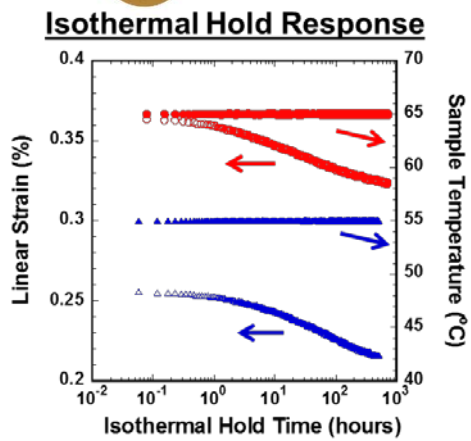
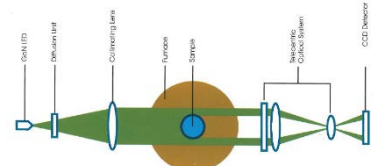
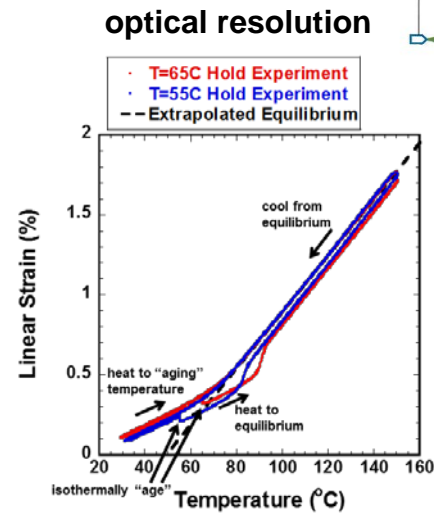


Stress developed during free-surface cure can be reduced by implementing a post-gelation temperature ramp, as observed in confined cure

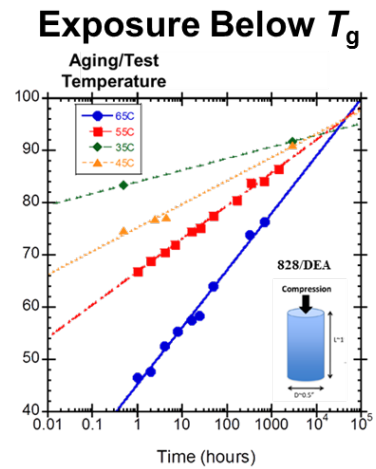
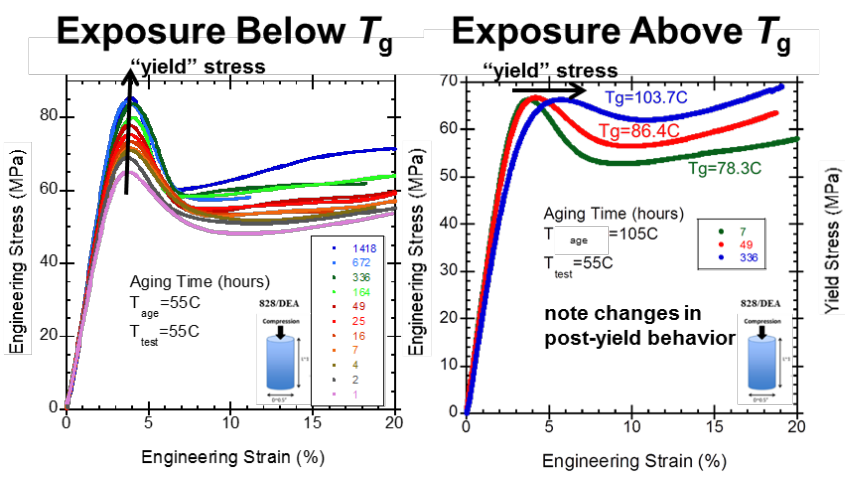
Polymer Glass Aging



Material Volume Changes



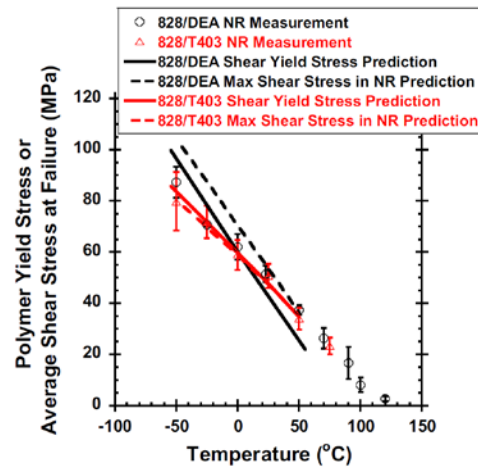
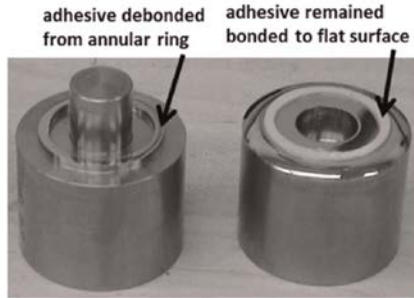
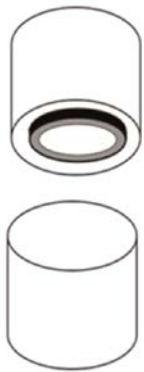
Material Mechanical Response Changes



SNL NLVE polymer models (e.g., SPEC) have the framework to predict the aging behavior and are currently being tested against measurements

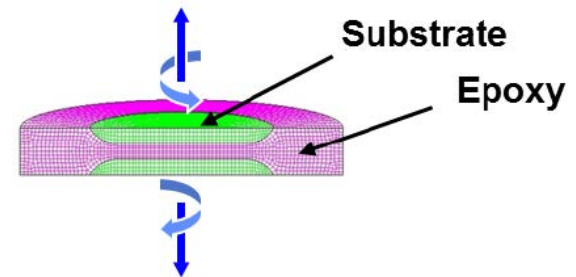
Polymer Failure: Adhesive Joints

Shear Loading: Napkin Ring



Combined Shear and Tension/Compression Loading: Saucer

Kropka et al., *Int. J. Adhn. & Adhs*, 63 (2015) 14-25



Test geometries to measure the initiation of adhesive failure at an “embedded interface”