

Responses of Structures to SDoF vs MDoF Vibration Testing

IMAC XXXV

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Outline

- Motivations & Objective
- Test Equipment
- Test Article and Instrumentation
- Visual Comparison
- Comparison Metrix
- Observations
- Conclusions

Motivations

- Sequential single axis testing has been firmly established as the preferred test method for environmental vibration characterization and analysis
- Recent developments in electrodynamic shaker capabilities have enabled reliable and controllable simultaneous multi-axis testing
- Growing body of evidence indicates shortcomings in conventional single axis testing.
- Multi-axis testing is shown to produce loading conditions that more closely simulate real world environments.

Motivations

- Traditional multi-axis testing conducted by developing a control scheme based on rigid body acceleration at the base of a component.
- Limitations of instrumentation during field tests, it is rare to be able to directly derive 6DoF inputs at the component or sub-system level.
- Coherence and phase between axes is not adequately quantified.

Objective

- Use directly measured field data to drive a multi-axis vibration test
- Benchmark the performance of other methods for deriving a 6DoF test inputs from field data with limited instrumentation
- Compare the results of tests conducted with input signals derived from only response channels which would have been available during a standard field test to those conducted with the true input signals directly measured

Test Equipment

- Shaker System: Team Corporation Tensor™ 18kN
 - Simultaneous or sequential excitation of X, Y, and/or Z axes
 - Complete control of rotations around all axes

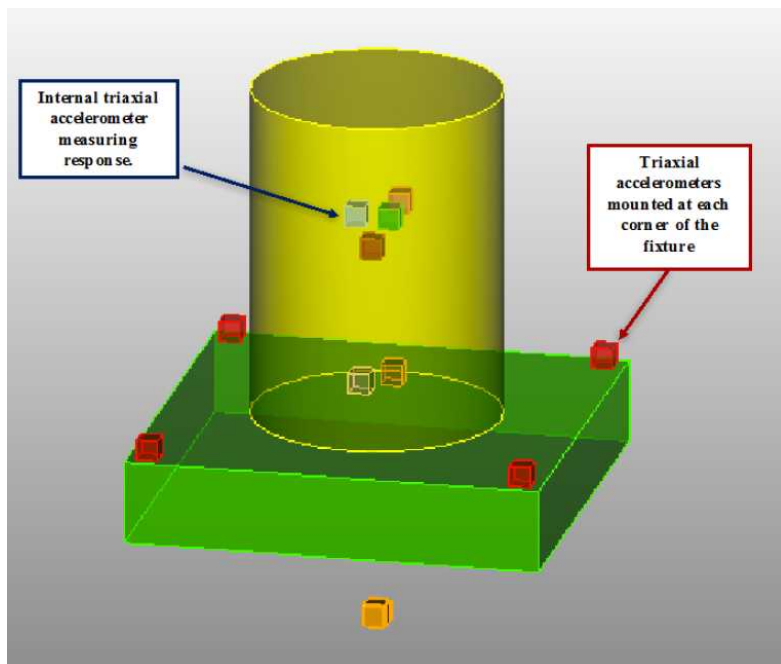
Specifications

| | |
|----------------------------------|---------------|
| Table First Frequency | 4,000 Hz |
| Test Frequency Range | 10 - 4,000 Hz |
| Max Displacement | 1.0 in |
| Max Acceleration (w/max payload) | 10 g |



- Controller Software: Data Physics Control and Analysis System
 - Multi-Input and Multi-Output Control
 - Input and Output Transformation for 6DOF Control
- Data Acquisition: National Instruments™ LabVIEW and NI Data Acquisition Modules

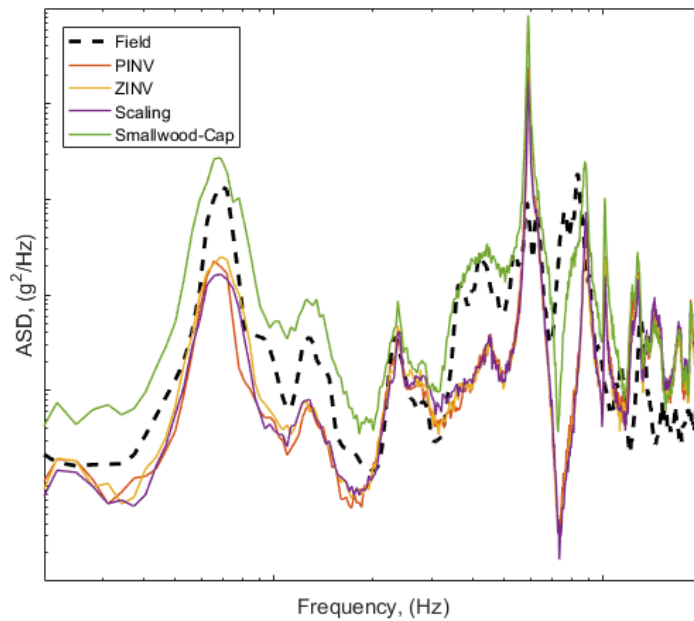
Test Article and Instrumentation



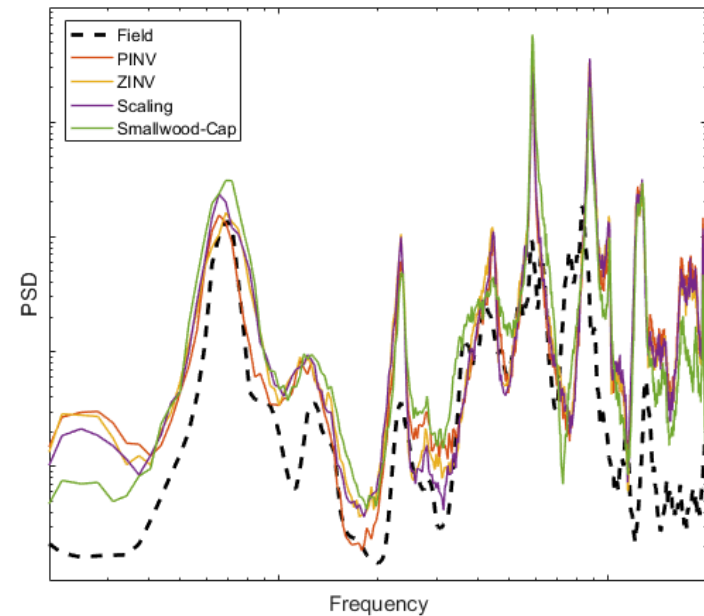
- Test article equipped with array of triaxial accelerometers for control
- Control accelerometers positioned symmetrically about both lateral axes
- Additional Accelerometers internally to the system

Visual Comparison

3DoF Inputs



6DoF Inputs



Which response best matches the field test?

Comparison of Responses

- Features of interest
 - Shape of the PSD curve – gives information about the frequency content of the response
 - Over all energy in the response
- Challenges in comparison
 - Small differences in natural frequencies between field and test units could show up as shifts in the PSD
 - Small shifts of peaks in the PSD could lead to low correlation coefficient, even if the shapes are very similar
- Converting the data from all the frequency lines to sixth octave spacing smooths out the shifts in frequency due to unit to unit variability

Metrics Comparing Energy Levels

- Mean in the RMS

- $error_{rms} = 20\log\left(\frac{rms_{test}}{rms_{flight}}\right)$
- $normalized_{rms} = 1 - \frac{TotalRmsError}{MaxRmsError}$
- $metric_{rms} = \frac{normalized_{rms}}{\max(normalized_{rms})}$

- Mean dB Error

- $error_{dB} = \frac{1}{N} \sum_{f_{min}}^{f_{max}} 10 \left(\log \left(\frac{test(f)}{flight(f)} \right) \right)$
- $normalized_{dB} = 1 - \frac{TotaldBError}{MaxdBError}$
- $metric_{dB} = \frac{normalized_{dB}}{\max(normalized_{dB})}$

Metrics Comparing PSD Shapes

- Correlation Coefficient

- Correlation coefficient (*corr*) is calculated using the `corrcoef` function in Matlab
- $\textit{normalized}_{corr} = 0.5(\textit{corr} + 1)$
- $\textit{metric}_{corr} = \frac{\textit{normalized}_{corr}}{\max(\textit{normalized}_{corr})}$

- Cross Correlation Coefficient

- Cross correlation coefficient (*xcorr*) is calculated using the `xcorr` function in Matlab
- $\textit{normalized}_{xcorr} = 0.5(\textit{xcorr} + 1)$
- $\textit{metric}_{xcorr} = \frac{\textit{normalized}_{xcorr}}{\max(\textit{normalized}_{xcorr})}$

Comparison Metrics

| Method | No Cross Products | | Coherence Only | | Coherence & Phase | |
|-----------------------------------|-------------------|------|----------------|------|-------------------|------|
| | Metric | Rank | Metric | Rank | Metric | Rank |
| 6th Octave 3DoF | 2.710 | 14 | ++ | ++ | ++ | ++ |
| 6th Octave 6DoF | 1.935 | 25 | ++ | ++ | ++ | ++ |
| PINV 3DoF | 3.139 | 8 | 2.938 | 12 | 3.253 | 5 |
| PINV 6DoF | 2.707 | 15 | 2.457 | 17 | 2.187 | 23 |
| ZINV 3DoF | 3.140 | 7 | 2.934 | 13 | 3.324 | 4 |
| ZINV 6DoF | 2.411 | 19 | 2.278 | 21 | 2.444 | 18 |
| Scaling 3DoF | 3.032 | 9 | 2.681 | 16 | 3.025 | 10 |
| Scaling 6DoF | 2.220 | 22 | 2.323 | 20 | 2.034 | 24 |
| Smallwood-Cap 3DOF | 3.152 | 6 | 3.723 | 2 | 3.763 | 1 |
| Smallwood-Cap 6DOF | ** | ** | 3.005 | 11 | 3.372 | 3 |

** No data available

++ Not Specified

Observations

- Using the full 6DoF inputs as measured in the field yielded responses least like those in the field
 - Boundary conditions in the field and the laboratory are different
 - Unit tested in laboratory is different than the one in the field test
 - Inverse methods could account for those differences, allowing for the laboratory response to be closer for the inverse methods than the field data
- 3DoF tests matched field data better than their 6DoF counterparts
- Smallwood-Cap 3DoF method gave the best match to the field test data no matter how the cross spectra were defined
- In general, including the coherence and phase in the cross spectra yielded closer matches with the field data

Conclusions

- Recent field tests at Sandia National Laboratories had sufficient instrumentation to derive the full 6DoF inputs using a variety of methods.
- With the exception of the Smallwood-Cap method, the 3DoF input produced a response that was lower than field data
- The 6DoF inputs produced a response that matched well at low frequencies, but was too high at higher frequencies
- The inverse methods seem to remove some of the effects of the different boundary condition and unit to unit variability
- It is difficult to use a visual inspection of the data to draw any conclusions about which methods performed best

Conclusions (con't)

- Multiple metrics are needed to capture comparisons between energy and shape of the PSDs
- The 3DoF tests matched the 6DoF tests better than their 6DoF counterparts
- The Smallwood-Cap 3DoF method gave the best match to the field test data, no matter how the cross spectra were defined
- In general, including both the coherence and phase improved the response of the system

Thank you for your attention!

QUESTIONS?