



Battery Safety Testing

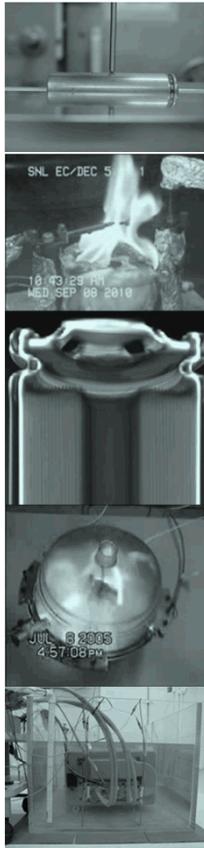
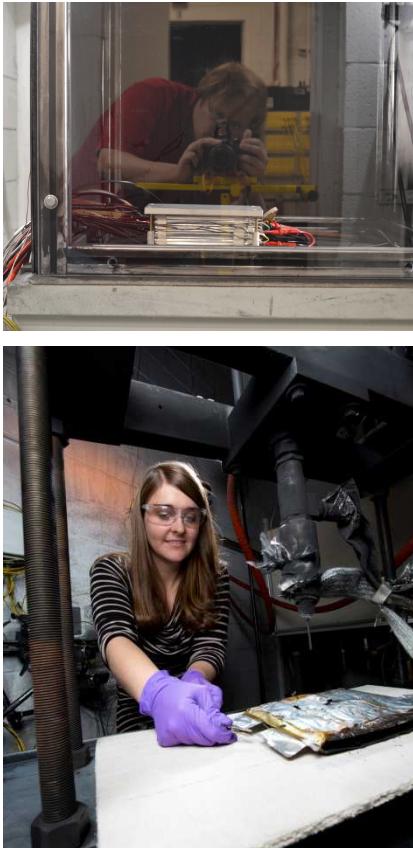
Joshua Lamb, Leigh Anna Steele, Loraine Torres-Castro, John
Hewson and Summer Ferreira

Sandia National Laboratories

Energy Storage Safety Workshop
Santa Fe, NM, February 2017

Approach and Capabilities

Cell and Module Testing Battery Abuse Testing Laboratory (BATLab)



Battery Pack/System Testing Thermal Test Complex (TTC) and Burnsite



Battery Calorimetry



Understanding Battery Safety



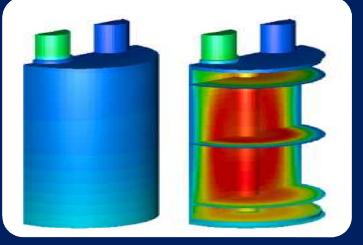
Materials R&D

- Non-flammable electrolytes
- Electrolyte salts
- Coated active materials
- Thermally stable materials



Testing

- Electrical, thermal, mechanical abuse testing
- Large scale thermal and fire testing (TTC)
- Failure propagation testing on batteries/systems
- Diagnostic techniques for battery state of stability
- Development for DOE Vehicle Technologies and USABC



Simulations and Modeling

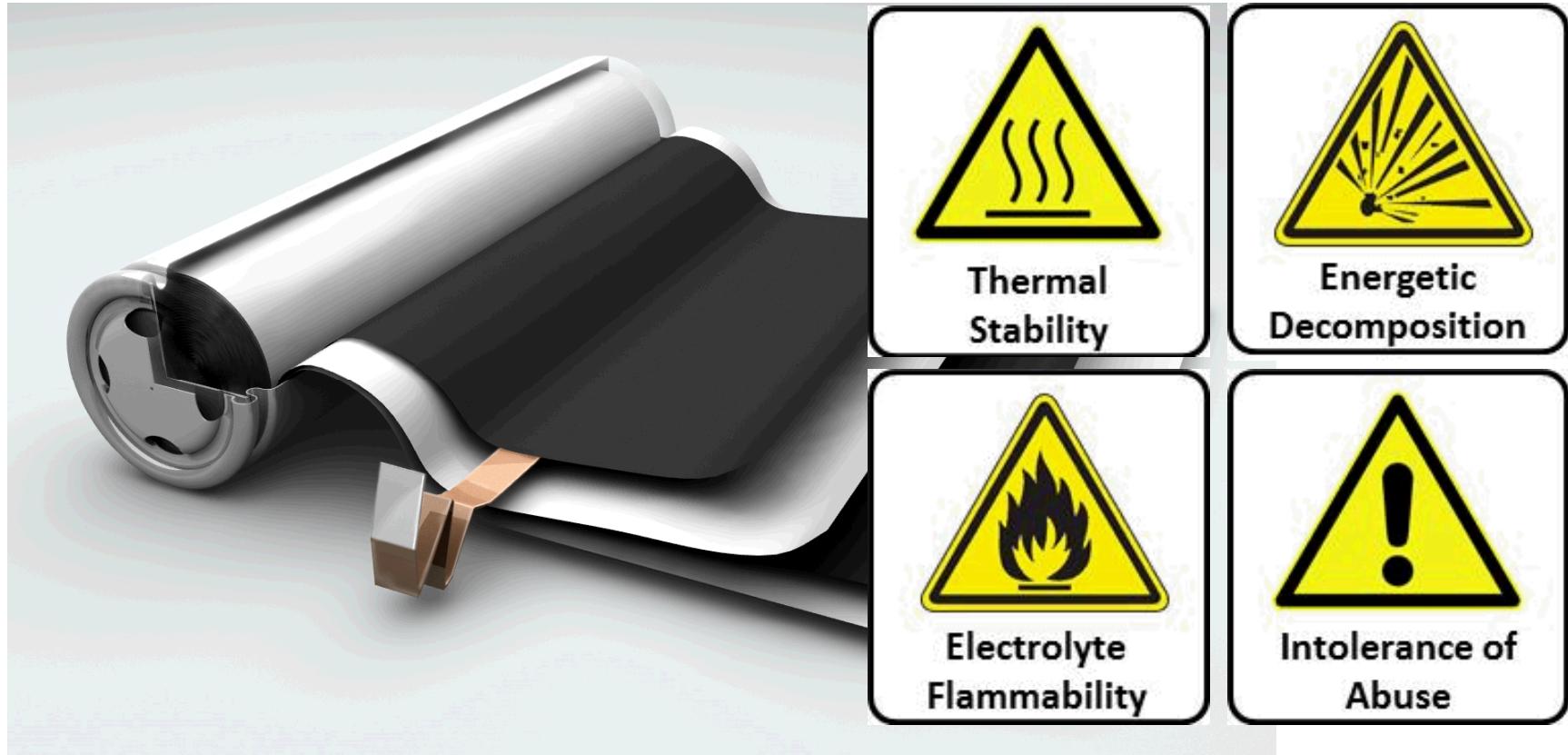
- Multi-scale models for understanding thermal runaway
- Validating vehicle crash and failure propagation models
- Fire Simulations to predict the size, scope, and consequences of battery fires



Procedures, Policy, and Regulation

- USABC Abuse Testing Manual (SAND 2005-3123)
- SAE J2464/UL 1642 procedures and standards
- R&D programs with NHTSA/DOT to inform best practices, policies, and requirements

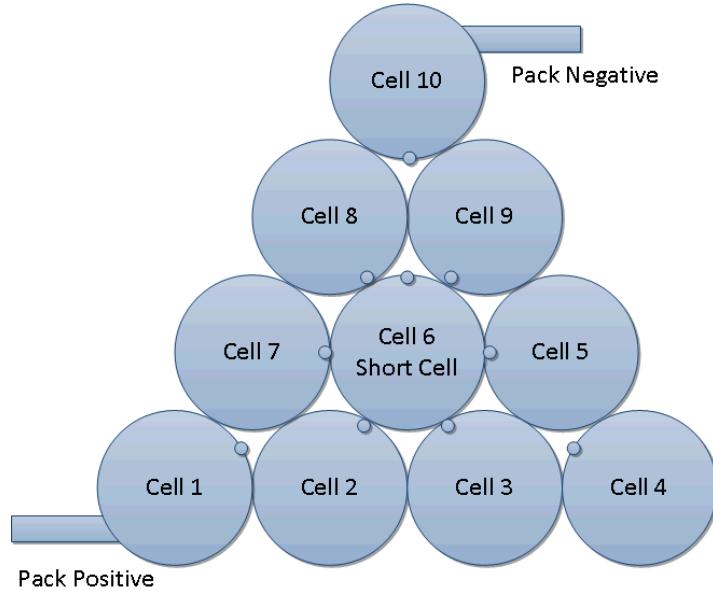
Lithium-ion Safety Issues



*Testing program aimed at understanding and improving
abuse tolerance of energy storage systems*

Battery Failure Propagation

- Simply, the propensity of the energetic failure of a single cell to cause widespread thermal runaway within a battery
- Most large battery systems are designed to withstand the loss of several cells from a performance standpoint
- A point failure becomes more serious if it can send nearby cells into thermal runaway
- Recent events have had battery runaway events that engulfed the entire pack



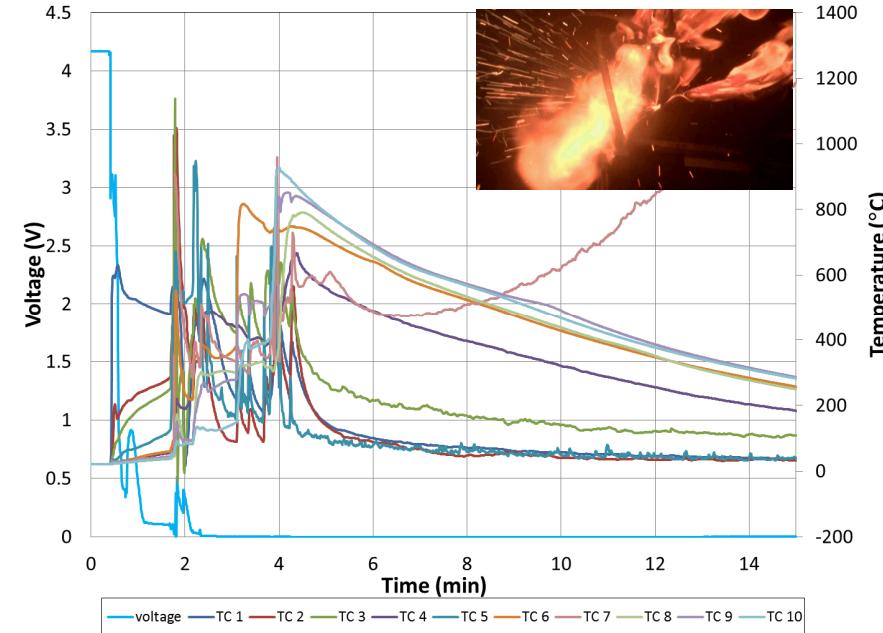
- Diagram showing cell and thermocouple locations*
- Series and parallel constructions used, series pack wired in order from Cell 1 to cell 10*

Cells:
 Panasonic
 Model CGR18650CG
 2250 mAh nominal capacity
 Avg wt. 44g

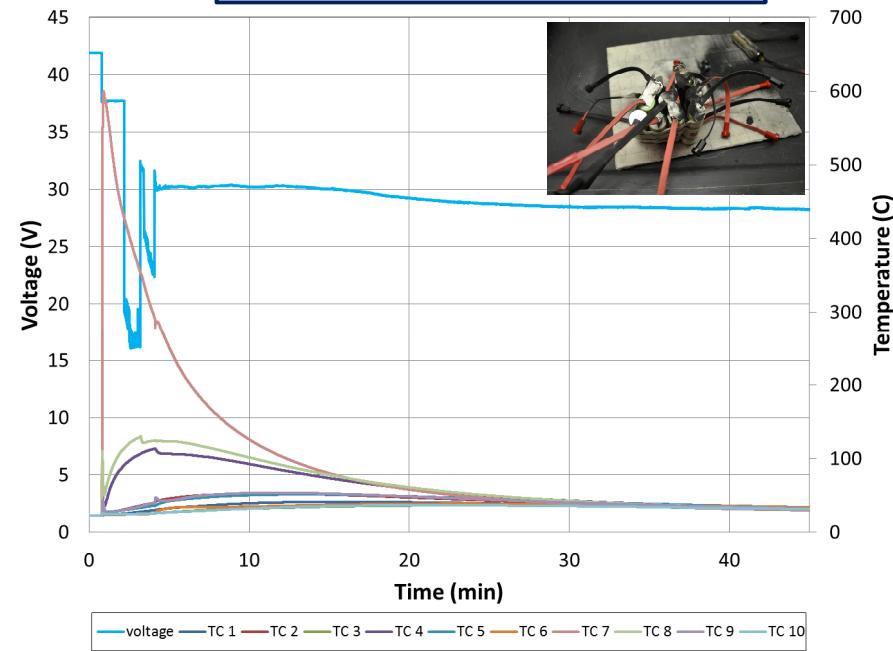
Failure Propagation: Edge Cell Failure

Failures initiated by mechanical insult to edge cell of parallel and series COTS LiCoO_2 packs

LiCoO_2 - 1S10P(parallel)



LiCoO_2 - 10S1P (series)

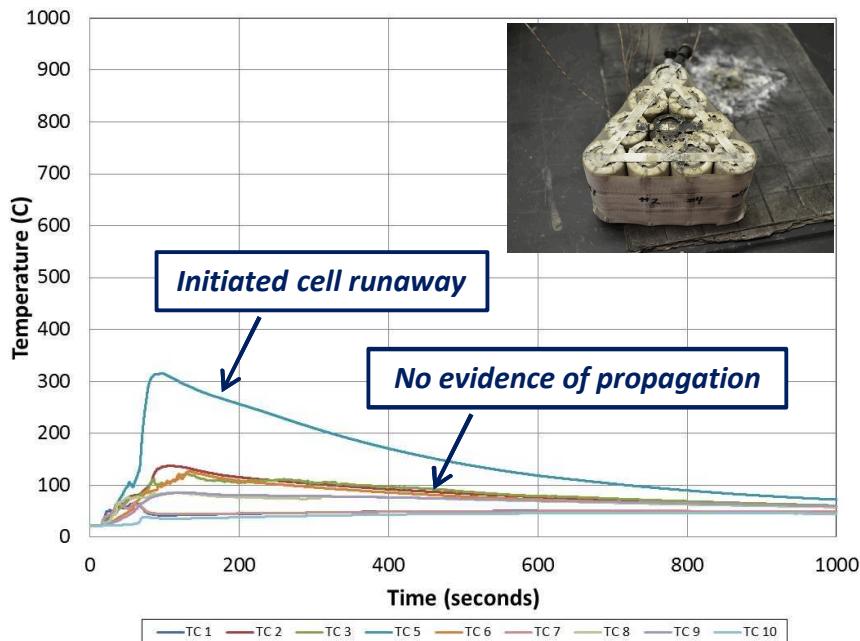


- Previous testing with center cell failure point in LiCoO_2 packs: limited propagation in 10S1P and complete propagation in 1S10P pack
- Edge cell failure: complete propagation for 1S10P and a range of responses for 10S1P: limited (cells next to failure point engaged) to complete propagation
- Parallel packs, regardless of initiation point, have full propagation while there is variation within series packs (limited to full propagation)

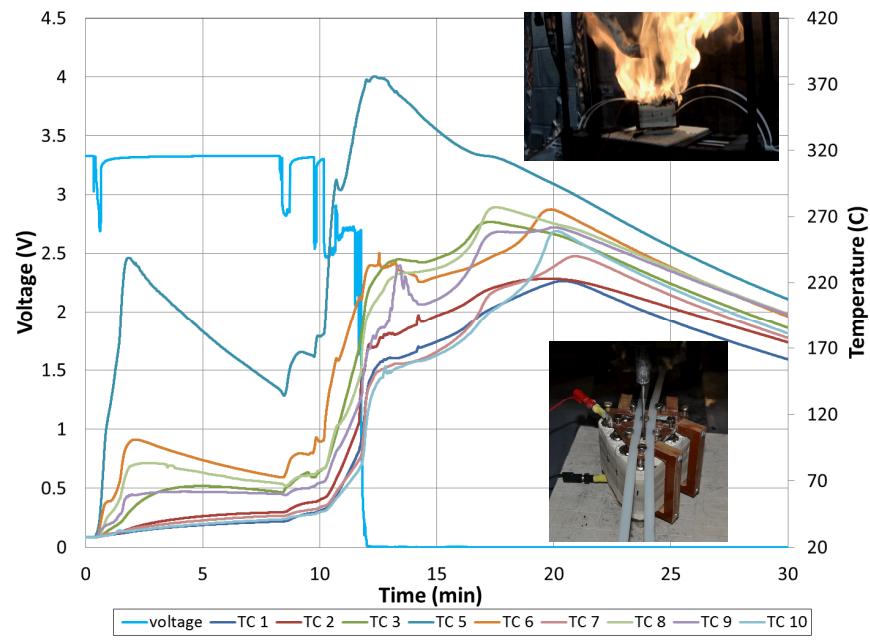
Failure Propagation: Design Effects (Connections)

Failures initiated by mechanical insult to center cell of LFP COTS packs

LFP - 1S10P connected using nickel tabs



LFP - 1S10P connected using copper bus

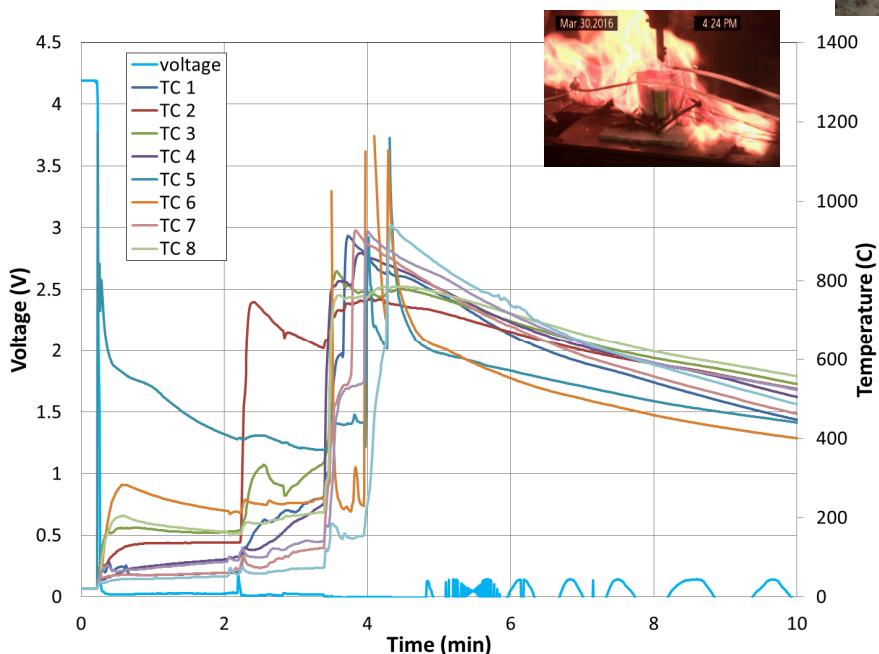


- Packs with alternative designs were assembled using 26650 LFP COTS cells in 1S10P configurations
- The pack connected with nickel tabbing show no evidence of propagation
- Complete propagation failure occurred once a copper bus was installed
- Pack design impacts the ability for failures to propagation

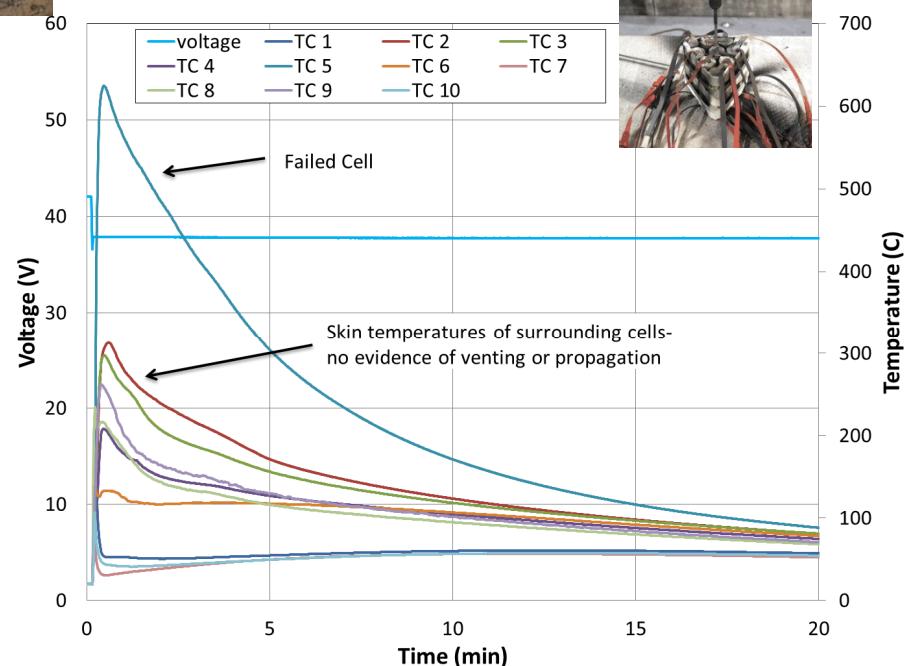
Failure Propagation: Design Effects (Air Gap)

Failures initiated by mechanical insult to the center cell: 2mm air gap between cells

18650 LiCoO₂ - 1S10P



18650 LiCoO₂ - 10S1P



- Complete propagation in parallel pack regardless of air gap
- No propagation in series pack with 2mm air gap between cells
 - Center cell went into thermal runaway and reaches 600°C
 - Neighboring cells skin temperatures see 150-300°C during failure of center cell but do not go into runaway
- Air gap allowed for heat to dissipate quickly in the series pack to eliminate propagation
- The electrical configuration of the parallel pack allows for propagation to occur regardless of the air gap between cells

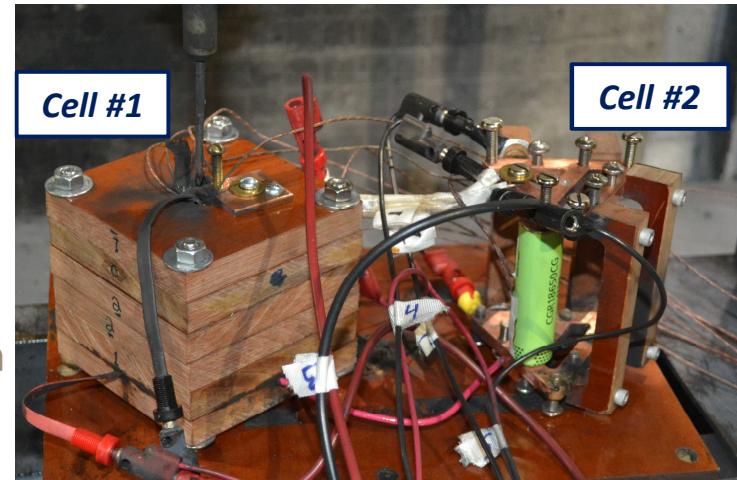
Short Circuit Current During Failure Propagation

Methodology:

- Use mechanical nail penetration along longitudinal axis to initiate thermal runaway in cell #1
- Develop fixturing to enable short circuit evaluation
- Evaluate the short circuit current between initiation point and cells in parallel

Experiment

- COTS LiCoO₂ 18650 and LFP 18650 and 26650 cells in 1S2P configurations
- Cells electrically connected by constantan wire of known resistance
- The current effort is focused on evaluation of the short circuit current when cell #1 undergoes a runaway event
- Method will be applied to larger cell strings and with complex electrical connections

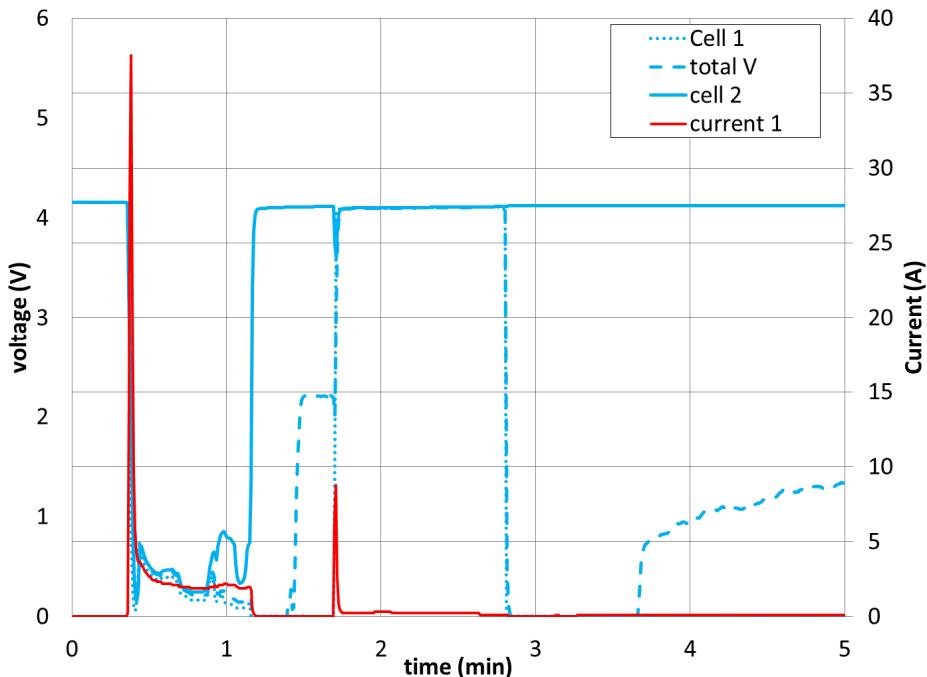


1S2P Battery: Constantan bridge wire connecting cells. Failure initiation point at Cell #1

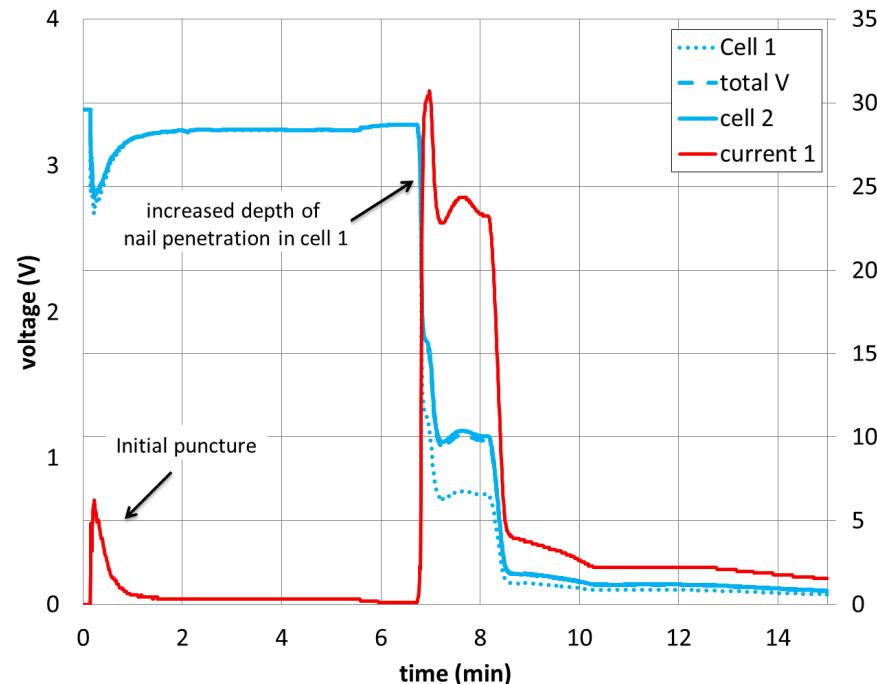
Short Circuit Current During Failure Propagation

Failures initiated by mechanical insult to cell 1 which is connected to cell 2 through constantan bridge wire

18650 LiCoO₂ cells – 1s2p



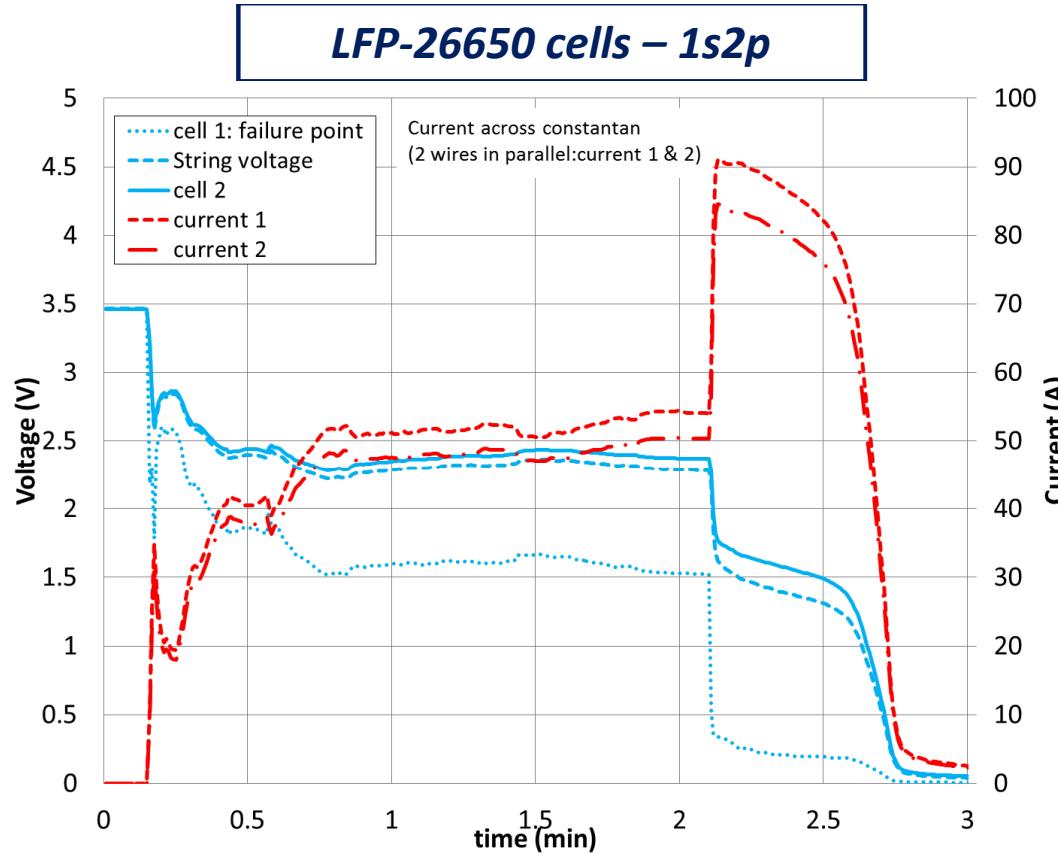
18650 LFP cells – 1s2p



- Peak currents across constantan bridge during failure propagation of 18650 LiCoO₂ and LFP string reached 37A and 30A respectively
- Energy output during discharge for duration of 1 hour was 0.49 Wh for LiCoO₂ and 1.04 Wh for LFP

Short Circuit Current During Failure Propagation

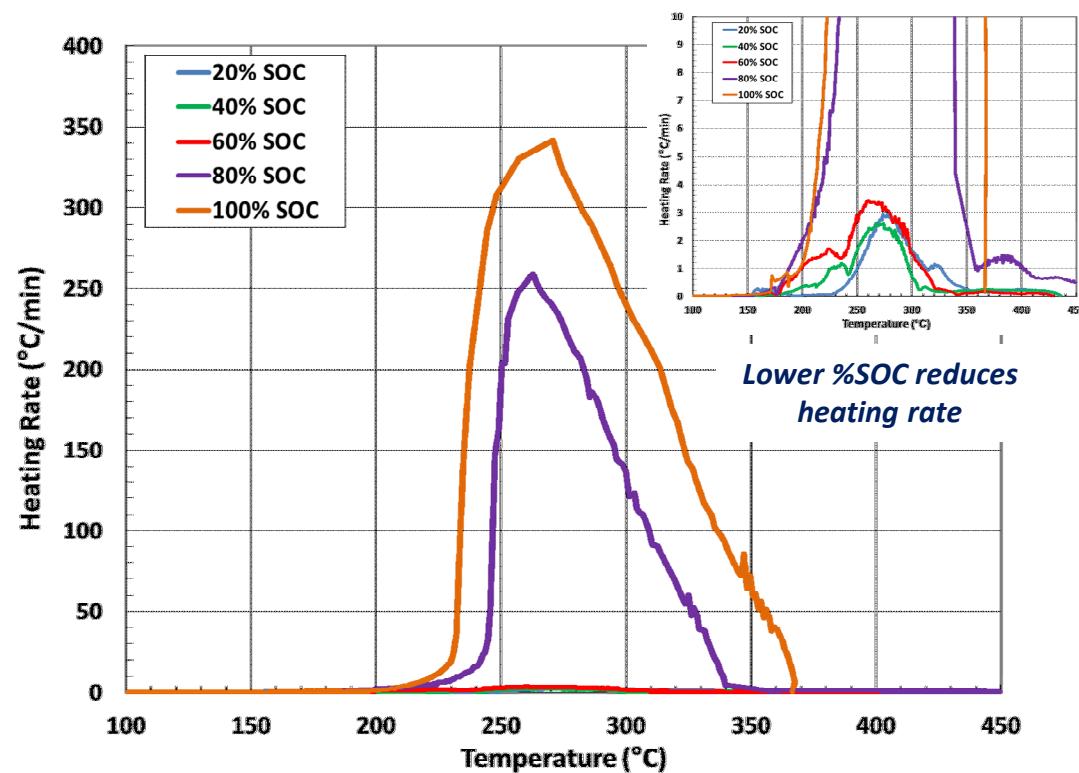
Failures initiated by mechanical insult to cell 1 which is connected to cell 2 through constantan bridge wire



- Peak currents across constantan bridge during failure propagation of LFP 26650 string reached 90A
- Energy output during discharge for a duration of 1 hour was 4.77Wh

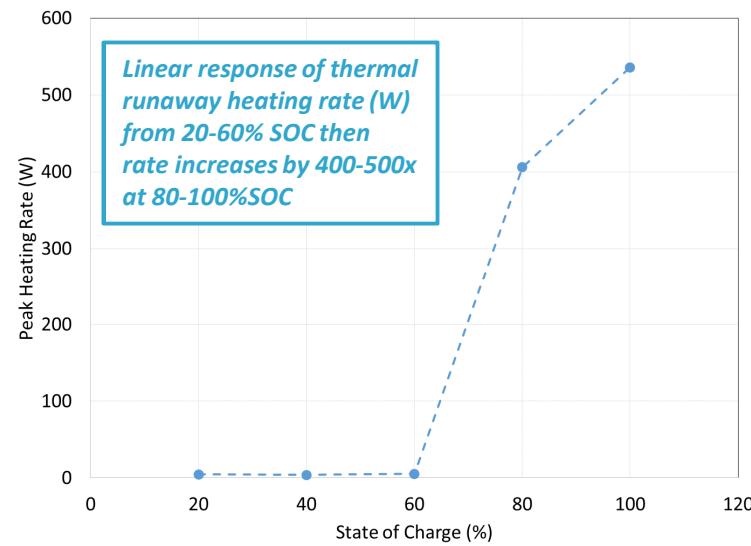
Impact of SOC on Abuse And Propagation

Fresh cells 20-80% SOC (80-20%DOD):Sanyo



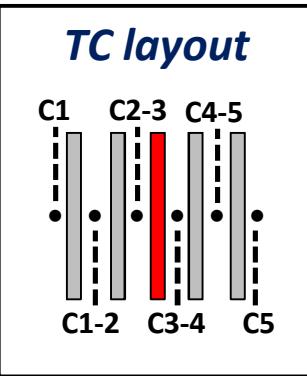
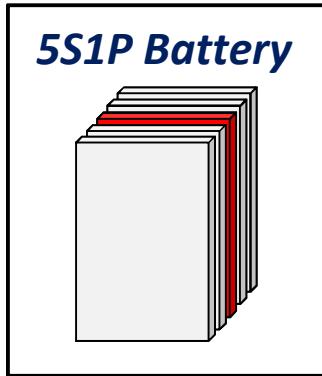
Energies as a function of %SOC

%SOC	KJ	KJ/Ah	W	W/Ah
20	19.5	78.0	4.64	18.6
40	23.9	47.8	4.14	8.27
60	25.7	34.3	5.37	7.17
80	31.0	31.0	406	406
100	25.5	20.4	536	429

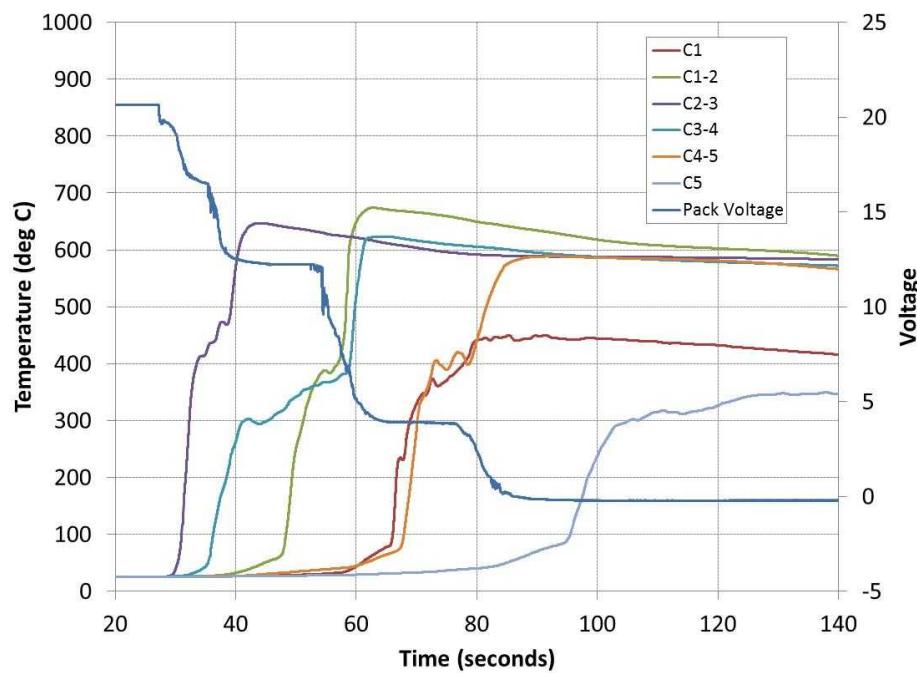
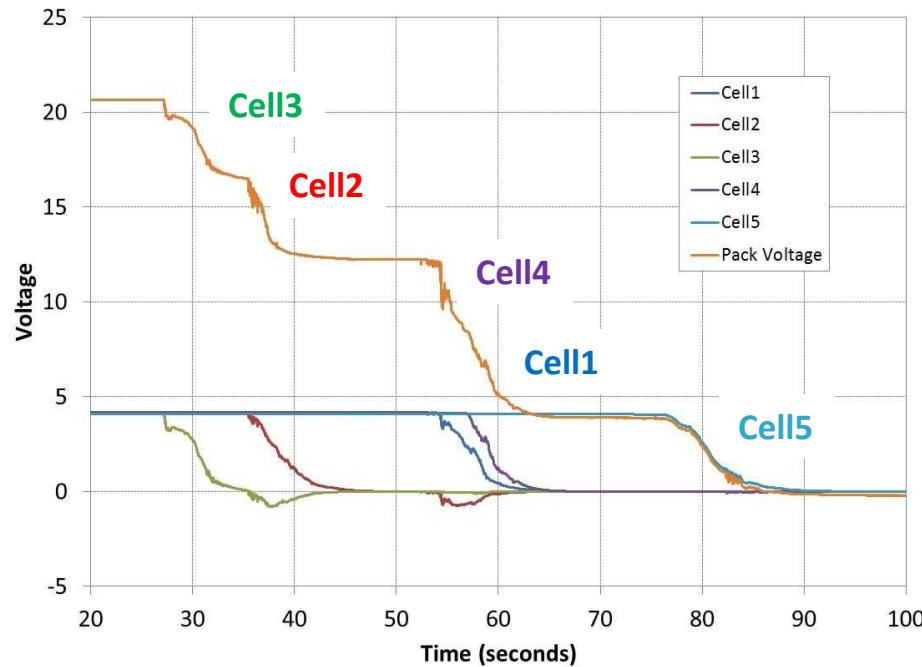


- Peak heating rate profiles are similar for lower states of charge (20-60%) then drastically increase at 80% and 100% SOC as shown by the total energy output (W)
- The onset of thermal runaway increases as the %SOC decreases

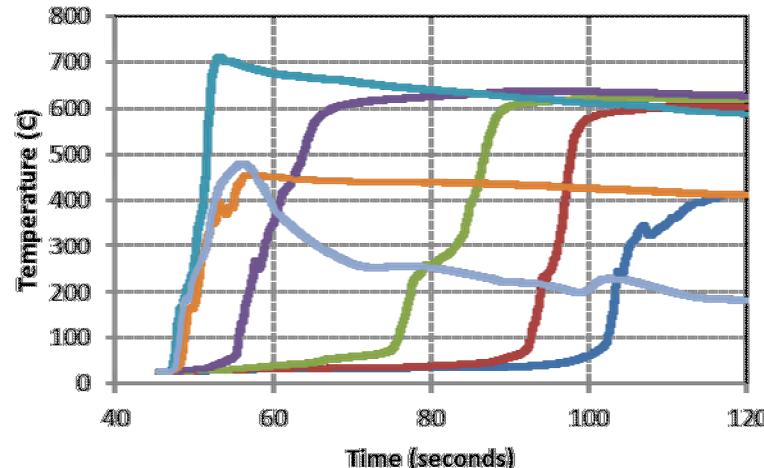
Propagation Testing (5S1P) – 100%



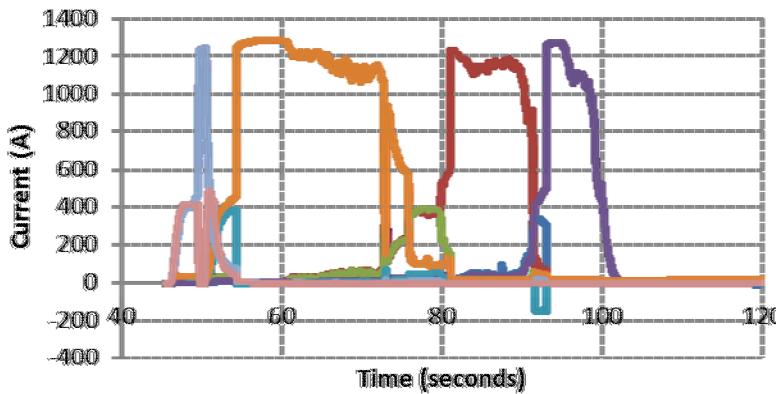
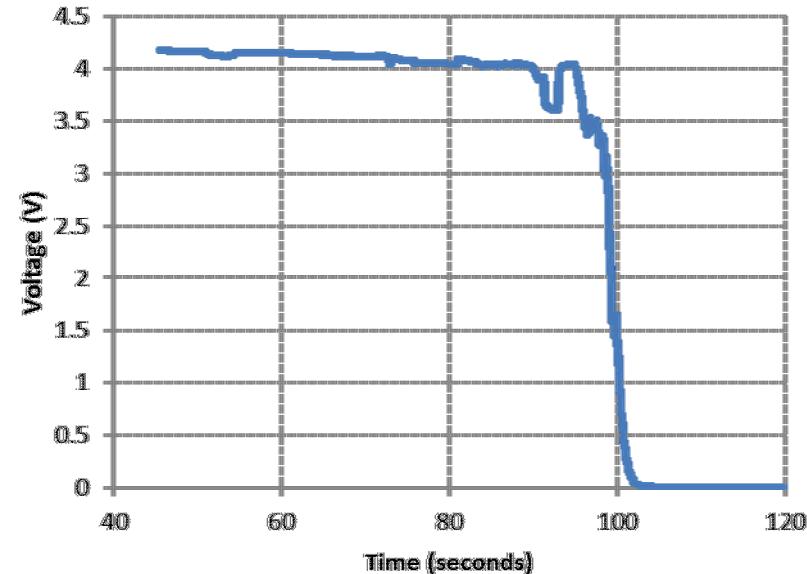
- Successful initiation at Cell #3
- Propagation to adjacent cells
- Cascading failure to entire battery over 60 s



Propagation Testing (1S5P)



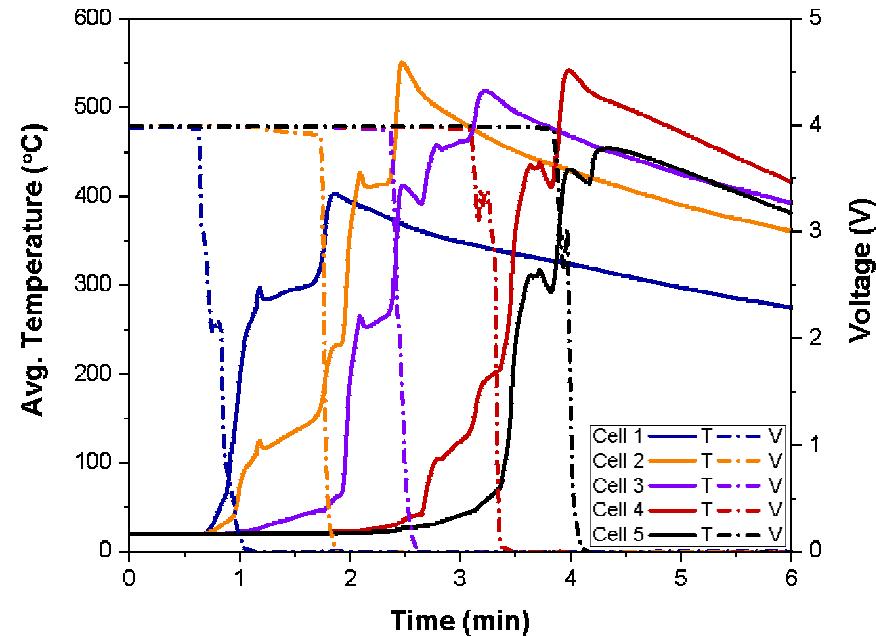
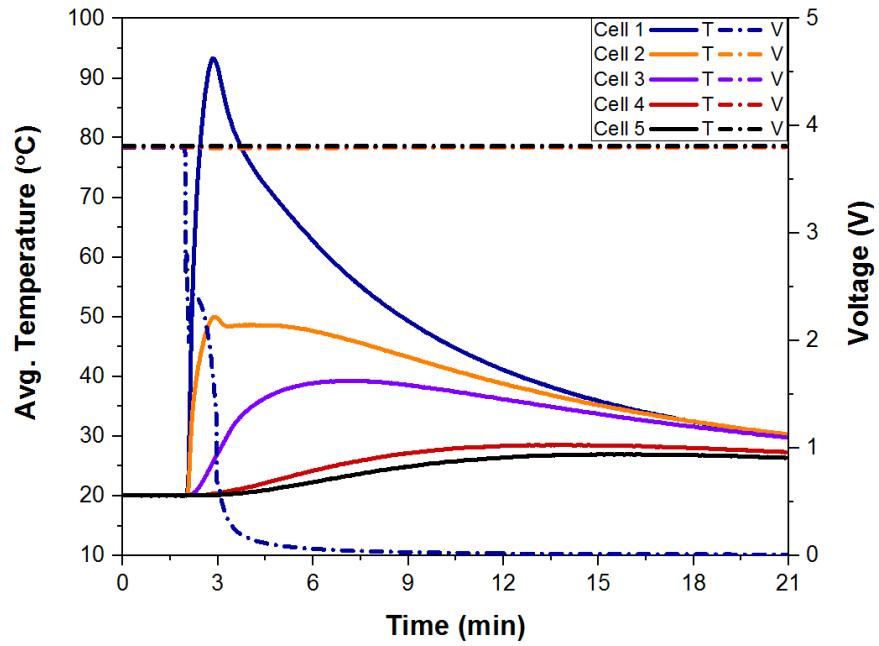
Cell 1 — Cell 1-2 — Cell 2-3 — Cell 3-4
Cell 4-5 — Cell 5 — Bridge 4+



Bridge 1+ — Bridge 2+ — Bridge 3+ — Bridge 4+
Bridge 1- — Bridge 2- — Bridge 3- — Bridge 4-

- Failure and runaway initiated at Cell #5
- Current measurements taken on nickel connections

50% vs 80% Pouch cell propagation



- 50% SOC no cell to cell propagation observed
- “Pulsating” propagation observed during failure of 80% pouch pack
- Total pack propagation observed after ~4 minutes

Summary

- Failure propagation behavior observed in both cylindrical cell strings and pouch cell strings
- Electrical and cell configuration observed to play a significant role in how cylindrical cells propagate
- Electrical configuration shows a smaller impact in pouch cells, owing to the large area of thermal contact
- Propagating failure is possible at reduced SOC; current work is ongoing to determine how cell configuration might impact the severity of failure at reduced SOC

Acknowledgements



- **Dave Howell (DOE)**
- **Imre Gyuk (DOE - OE)**
- **Brian Cunningham (OVT)**
- **Jim Barnes (OVT)**
- **Jack Deppe (OVT)**
- **Chris Orendorff**
- **Chris Grosso**
- **Jerry Quintana**
- **Lorie Davis**
- **Mani Nagasubramanian**

