

The Effect of Hydrous Supercritical Carbon Dioxide on the Mohr Coulomb Failure Envelope in Boise Sandstone

SAND2017-2119C

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Sustaining Injectivity

Changes in rock strength could lead to development of fracture networks, creating high permeability pathways into the reservoir

Reduction of bonding strength in granular rocks could lead to consolidation and reduced permeability

Storage Efficiency

Induced fractures and dilatant deformation create additional porosity for storage and improved sweep

Consolidation reduces porosity and decreases available storage space

Controlling Emergence

Movement along induced fractures and faults could pierce overlying seal

Consolidation of the reservoir induces deformation in overlying seal, jeopardizing integrity



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Acknowledgments

- This work was supported as part of the Center for Frontiers of Subsurface Energy Security, an Energy Frontier Research Center funded by the U.S. Department of Energy, Office of Science, Basic Energy Sciences under Award Number DE-SC0001114
- Sandia National Laboratories is a multi-mission laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.
- Boise cores purchased from Kocurek Industries, Caldwell, Texas
- Anastasia Ilgen performed geochemical analysis, Josh Feldman assisted in sampling
- Michael Aman performed scratch test measurements under supervision of Nicolas Espinoza
- Tom Dewers provided insight and guidance



Introduction

- Atmospheric CO₂ levels are at their highest recorded levels for over 400,000 years; surface temperatures show a >0.85°C increase since 1880
- Renewable power sources are becoming increasingly competitive, but fossil fuels are still necessary, as well as other large CO₂ sources like cement and fertilizer production
- Geologic carbon storage (GCS) is a potential tool to decrease CO₂ emissions, mitigate climate change
- CO₂ is stripped from emissions and injected into depleted reservoirs and deep saline aquifers as a supercritical phase (scCO₂) for at least 10,000 years
- To make a significant impact, 3.5 billion tons of CO₂ needs to be sequestered



Field Trials

- Sleipner Field, offshore Norway
 - Best example of GCS. Stripping CO₂ from natural gas, reinjecting into overlying reservoir at rate of 1 megaton per year since 1996. Highly porous injection target, minimal pressure increases and pore space utilization.
- In Salah field, Algeria
 - CO₂ from natural gas production injected in fracture, tight sandstone reservoir. 4 megatonnes have been stored, 12 MPa pressure increase, 2 cm uplift and fault reactivation
- Weyburn field, Canada
 - CO₂ EOR transition to storage. Pressure had risen by 5 MPa and reactivated pre existing faults



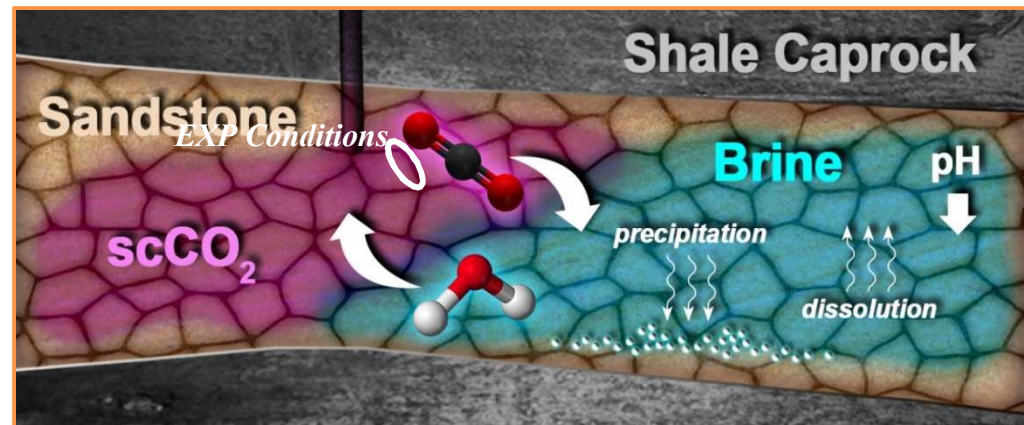
Previous Experimental Work

- Crystal Geyser, natural analog for GCS
 - Reservoir rocks exposed to natural CO₂, flow channelized into fault and fracture networks
 - Fracture toughness, scratch toughness lower in bleached rocks exposed to scCO₂ than country rock
- Limestones and anhydrites
 - Reductions in failure strengths due to reactions caused by low p.H. CO₂ solution
- Artificial calcite cemented rocks
 - Low p.H. solutions dissolve cement and weaken rock
- Sandstones
 - Lacking reactive phases, no change in strength due to exposure to CO₂



Objectives

- Following Sleipner example, US has lots of potential targets in offshore Gulf of Mexico
- This study focuses on fluid rock interactions between scCO_2 , water, and an analog for Tertiary, offshore Gulf of Mexico reservoir rocks, Boise sandstone
- During injection, scCO_2 forms a buoyant plume. At brine-plume interfaces, scCO_2 dissolves over time into the brine, water from the native brine can dissolve into the scCO_2 plume where it is present as humidity.
- Experiments are conducted to investigate the effect of hydrous scCO_2 on the shear failure of Boise sandstone.
- Decreases in failure strength injectivity, storage, and seal integrity



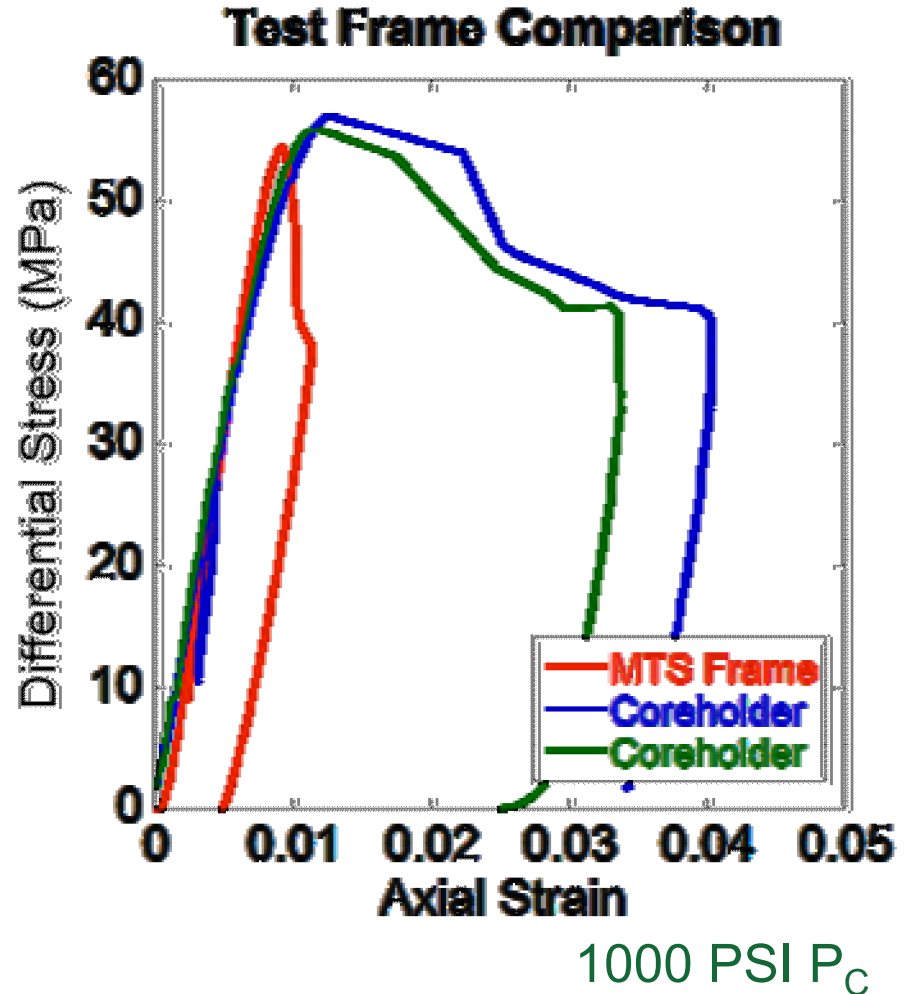
Methods

- Experiments were conducted using partial humidity and fully saturated scCO₂ on analog reservoir rock, Boise SS
 - 29% porosity; quartz, albite, microcline, illite-smectite, and calcite
 - Water present as a vapor phase in scCO₂
- Long term changes in strength due to chemical reactions
- Hydrous scCO₂ generated using pressure vessel, recirculating pump, at 70C and 2000PSI
- Partial humidity scCO₂, water added in 5mL increments via Rheodyne injector valve, 0-40 mL total
- Boise samples in separate vessel at 70C and 2250PSI
 - Cylindrical core and thin disc stacked together
- scCO₂ recirculated through sample for 24 hours
- After depressurization, samples removed for triaxial testing, scratch testing
 - Remaining fluids that condensed from hydrous scCO₂ chemically analyzed in ICPMS
- Triaxial experiments conducted at 500, 1000, and 1500 PSI confining pressure
 - Experiments performed in CoreLabs Coreholder, MTS servo-hydraulic load frame
 - Room temperature, dry
- Scratch testing performed at UT

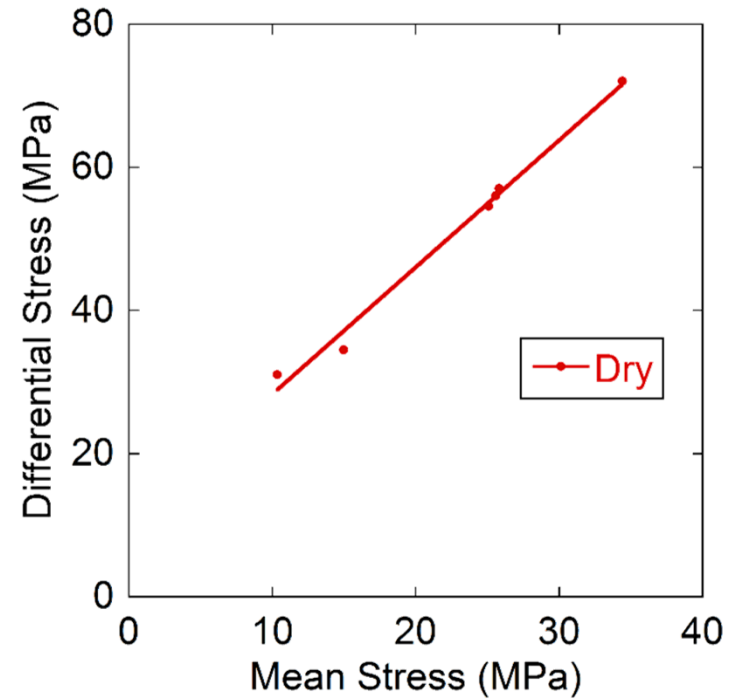
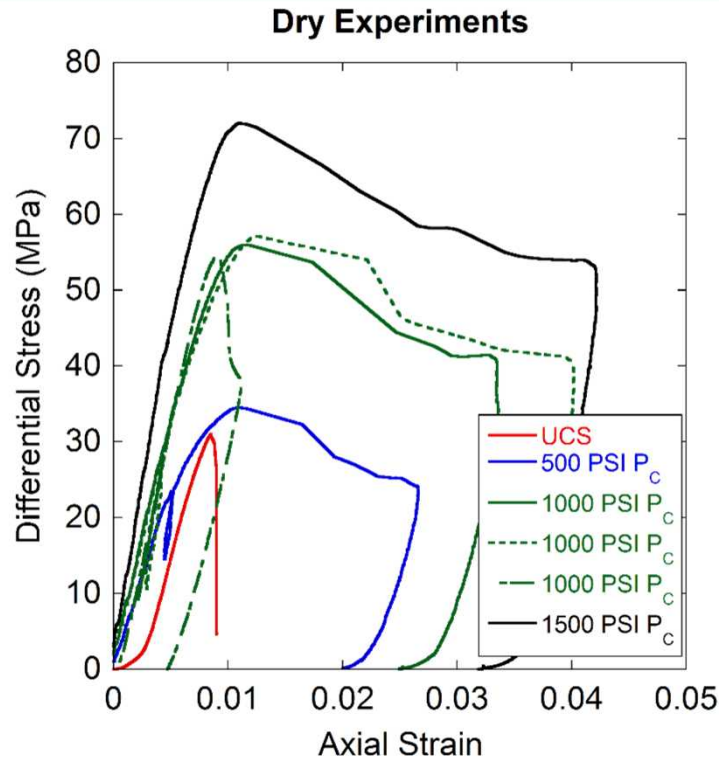


Load Frame Comparison

- Two different load frames used
 - MTS servo-hydraulic 220 kn frame
 - CoreLabs “Temco” triaxial core holder
- Core holder initially used for corrosion resistance
 - Jacket permeable to scCO_2
- MTS frame incompatible with acidic fluids
 - Dry tests
- Stiffnesses different, strengths same



Dry Experiments



- Triaxial experiments performed on room dry samples
- Increasing strength with increasing confining pressure
- Increasing stiffness with increasing confining pressure
- Linear failure envelope



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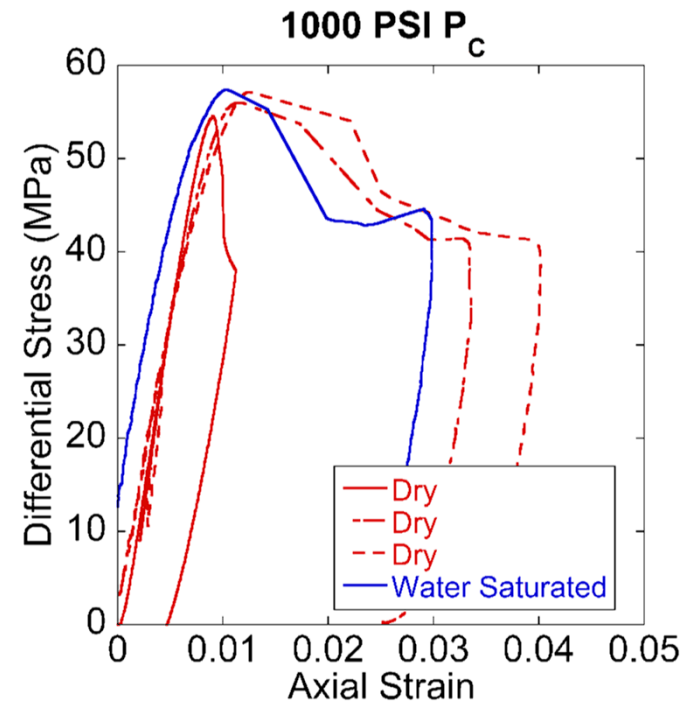
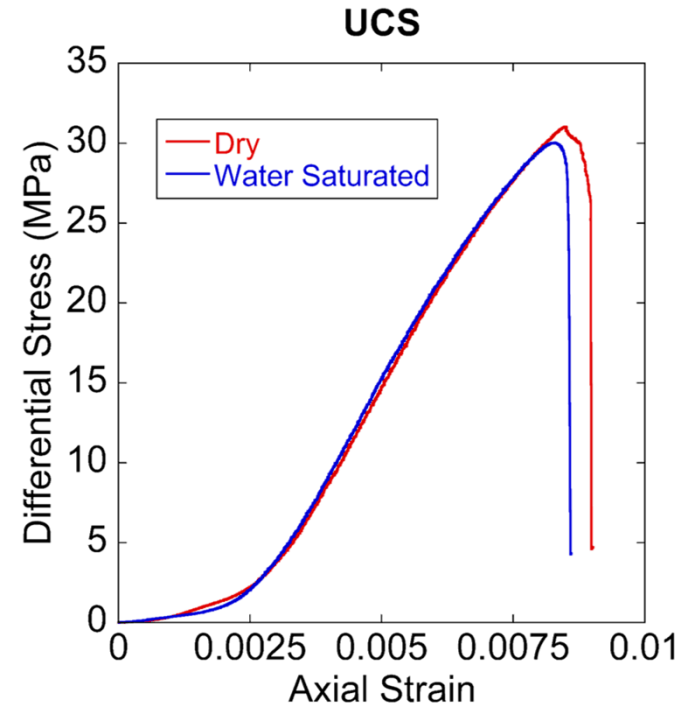
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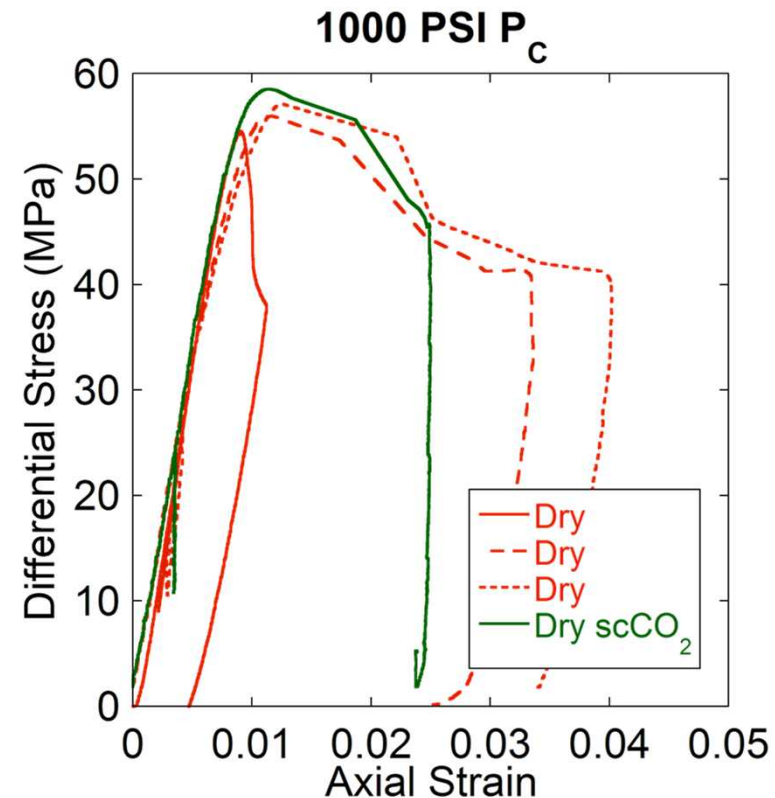
Control Experiments

- Triaxial experiments performed on room dry and wet samples
 - UCS test saturated
 - 1000 PSI P_c test flowing at 0.2 mL/min, heated at 70°C
- Strength agrees within natural variability of the rock
- Water does not have an effect on strength
- Temperature does not affect strength
- Any variations in strength due to exposure to scCO_2

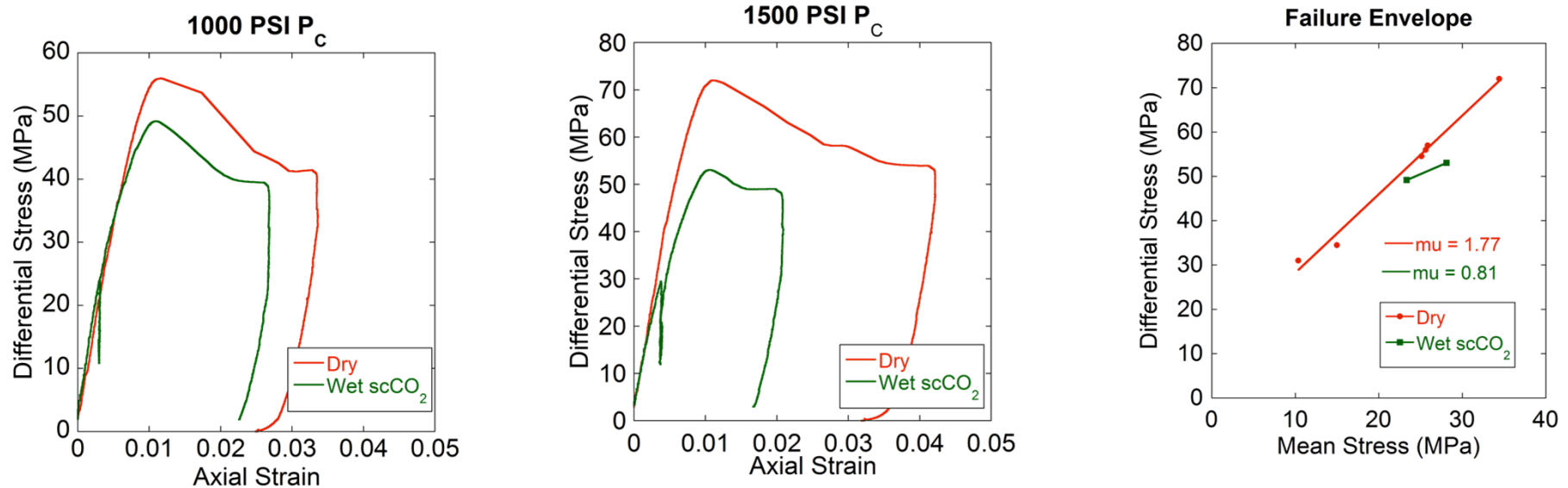


Dry scCO₂

- scCO₂ generated in 2.5L pressure vessel, heated to 70°C, pressurized to 2000 PSI
- Core in jacketed and pressurized in separate pressure vessel at 2250 PSI and 70°C
- scCO₂ recirculated through core for 24 hours, allowed to depressurize and cool overnight
- Tested separately at dry, room temperature conditions
- No effect from scCO₂



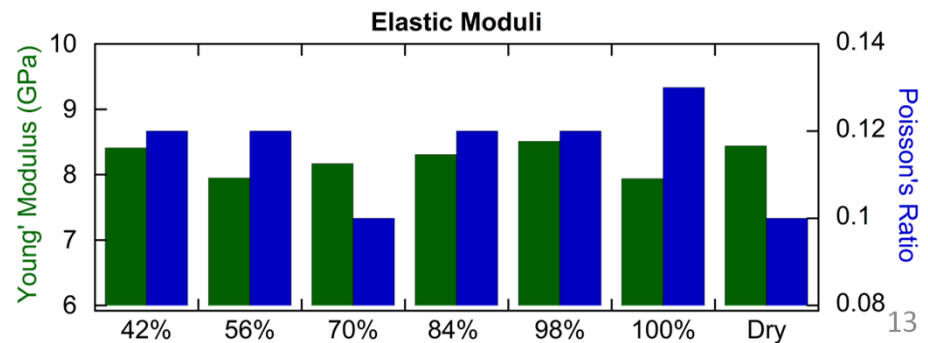
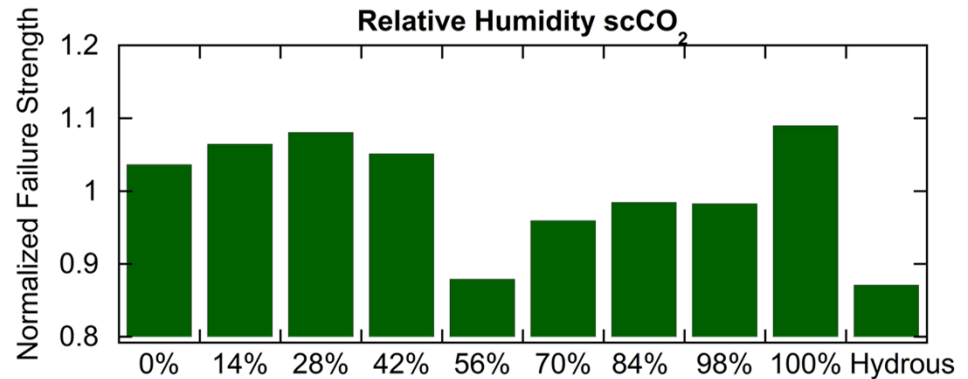
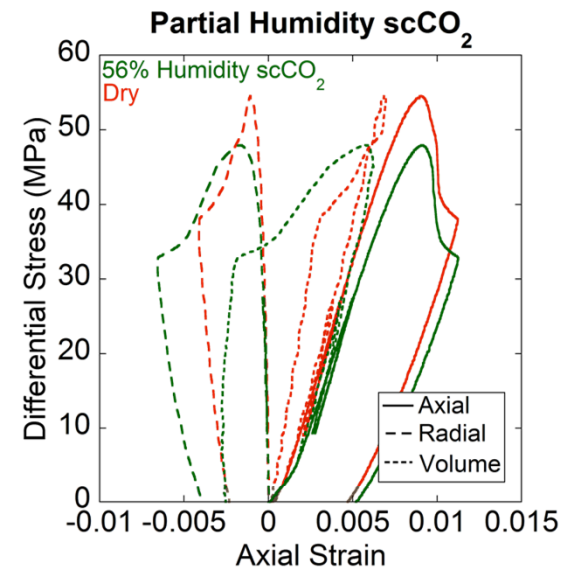
Fully Saturated scCO₂



- Preliminary experiments added 500mL of water to hydrous scCO₂ generator prior to pressurization
- Samples deformed experimentally post reaction at 500, 1000, and 1500 PSI confining pressure
- Fully saturated scCO₂ reduces failure strength, exacerbated at higher confining pressure tested
- Reduction in failure envelope due to exposure to hydrated scCO₂
 - Water, temperature, and dry scCO₂ don't have an effect
 - Chemical reactions caused by low p.H. solutions condensing at grain contacts

Parital Saturation

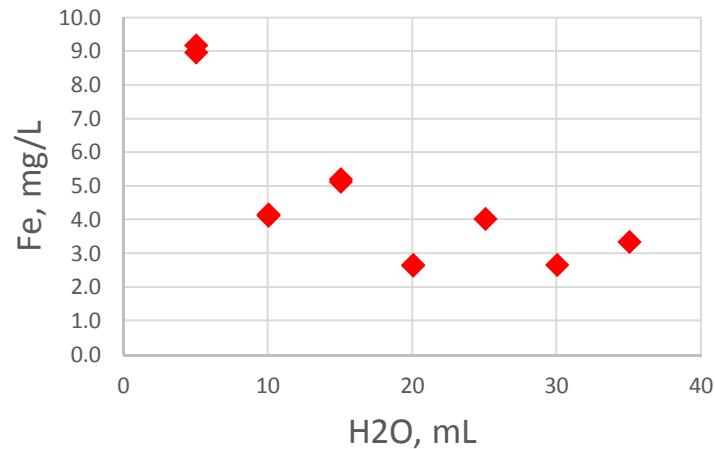
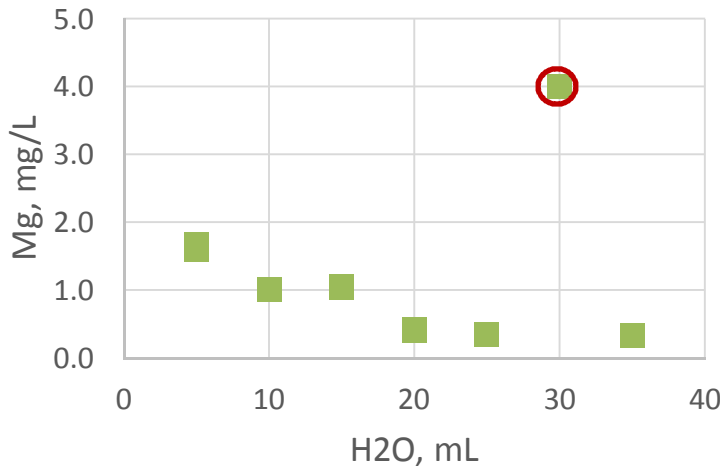
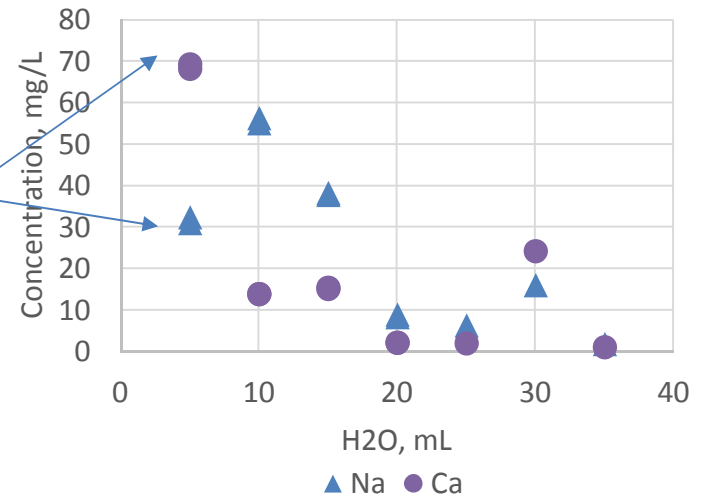
- Partial humidity scCO_2 prepared with 5mL increments of water, up to 40mL total
 - Added via Rheodyne injector valves after achieving supercritical state
 - Fully saturated ~ 38mL water
- Samples deformed experimentally post reaction at 1000 PSI confining pressure
- No clear trend in failure strength with partial humidity
 - Don't observe same decrease at full saturation as preliminary tests
- No variation in elastic moduli
- One sample showed weakening
 - Slightly reduced Young's modulus, elevated Poisson's ratio
- Fluid remaining in supercritical scCO_2 generator analyzed on ICP-MS for ion concentrations



Aqueous chemistry data

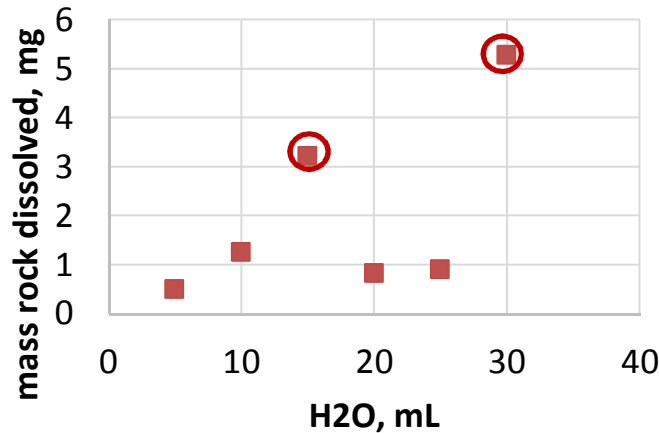
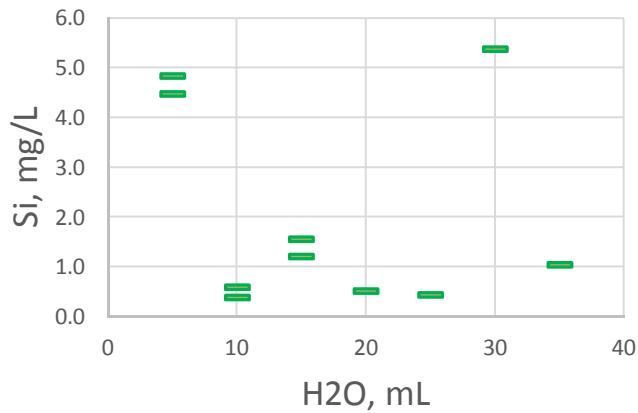
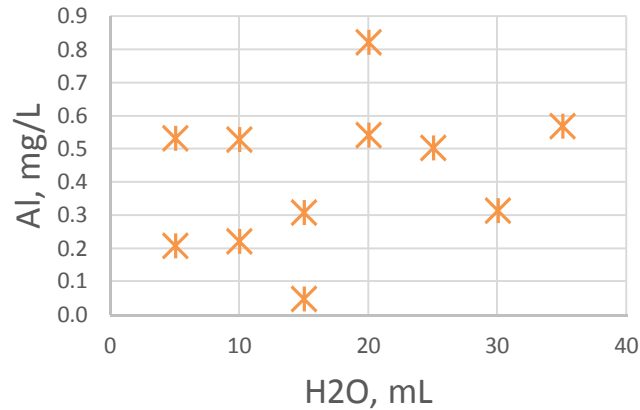
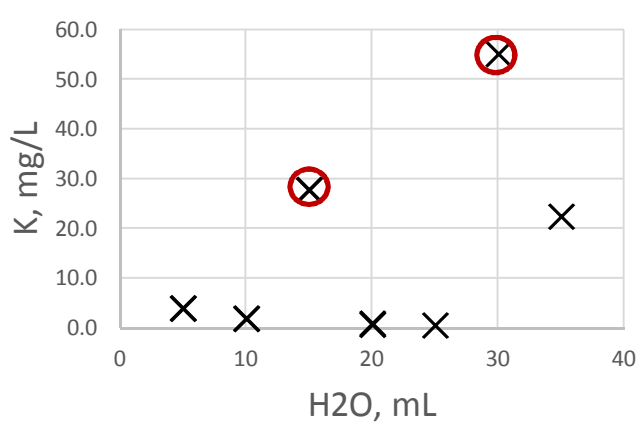
Minerals
 Quartz SiO_2
 Albite $\text{NaAlSi}_3\text{O}_8$
 K-feldspar KAISi_3O_8
 Calcite CaCO_3
 Illite
 $(\text{K}, \text{H}_3\text{O})(\text{Al}, \text{Mg}, \text{Fe})_2(\text{Si}, \text{Al})_4\text{O}_{10}[(\text{OH})_2, (\text{H}_2\text{O})]$

$\Delta G(\text{hydr})$:
 $\text{Ca}^{2+} = -1553 \text{ kJ mol}^{-1}$
 $\text{Na}^+ = -371 \text{ kJ mol}^{-1}$



- Detectable movement of ions, carried by humidity
- Observable trend of decreasing concentration as fluid volume increases
- Flip between sodium and calcium at low fluid volumes
 - Calcium outcompetes
- Outlier in measurements

Aqueous chemistry data



Minerals

Quartz SiO_2

Albite $\text{NaAlSi}_3\text{O}_8$

K-feldspar KAlSi_3O_8

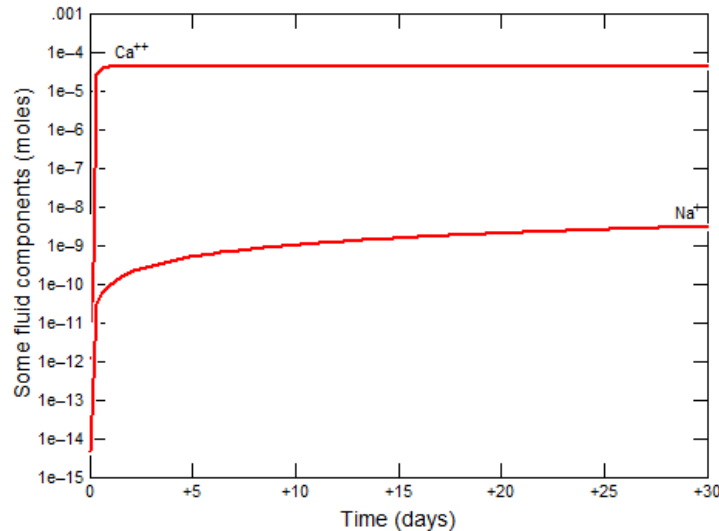
Calcite CaCO_3

Illite

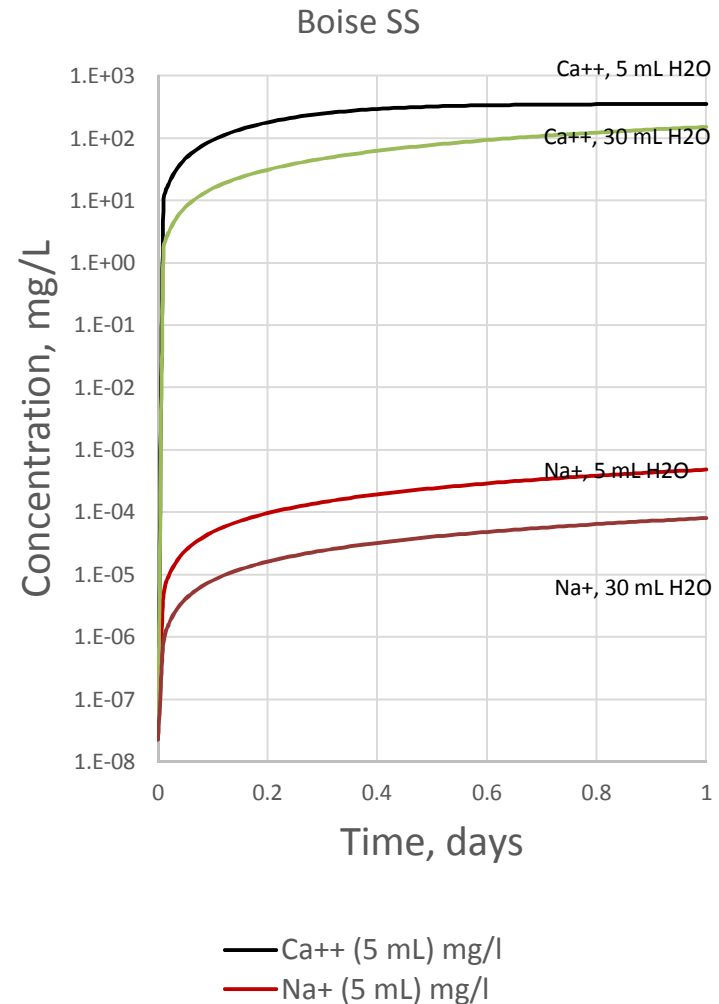
$(\text{K}, \text{H}_3\text{O})(\text{Al}, \text{Mg}, \text{Fe})_2(\text{Si}, \text{Al})_4\text{O}_{10}[(\text{OH})_2, (\text{H}_2\text{O})]$

- Si – close or at the detection limit;
- Al is under detection level
- Outliers – 15 and 30 mL H₂O
- Dissolved rock constant across humidity levels

Preliminary geochemical models



- Model predicts higher Ca++, compared to Na+
- Model predicts decrease in Ca++ and Na+ concentrations with increasing volume H₂O



(t = 25C, V H₂O=V exper, fugacity of CO₂=1 atm)



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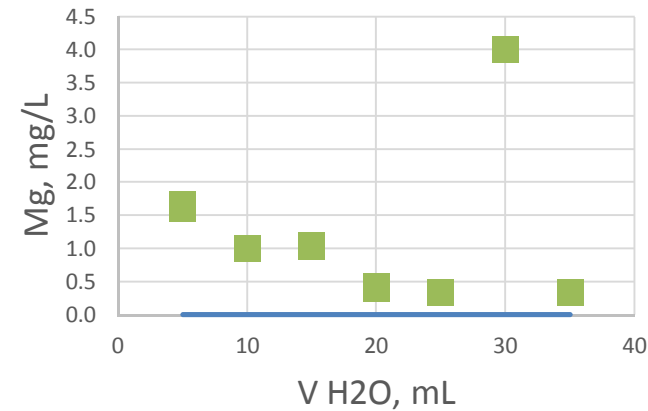
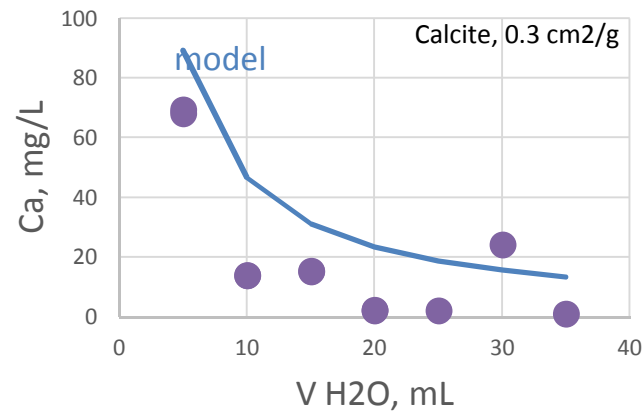
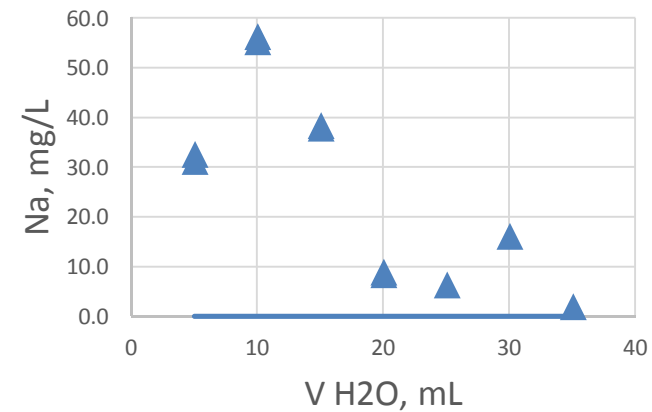
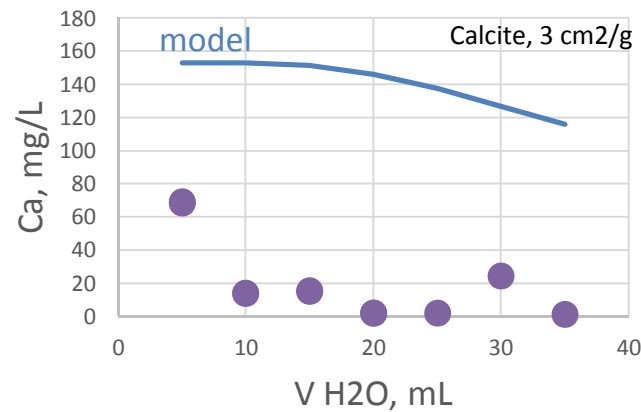


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Model Comparison

Kinetic parameters

| | |
|--|-----------------------------------|
| React c:\users\agilgen\documents\projects\cfses_2\tom_dewers | |
| File Edit Run Config Window Help | |
| Basis | Reactants Command Run |
| Reactants and kinetic reactions | |
| Kinetic Quartz | 3.1 g |
| surface area | 3 cm ² /g |
| Rate constant | 1.023e-18 mol/cm ² sec |
| Kinetic Albite | 2.8 g |
| surface area | 3 cm ² /g |
| Rate constant | 1.445e-16 mol/cm ² sec |
| Kinetic K-feldspar | 1.7 g |
| surface area | 3 cm ² /g |
| Rate constant | 3.89e-17 mol/cm ² sec |
| Kinetic Calcite | .9 g |
| surface area | 3 cm ² /g |
| Rate constant | 5.012e-10 mol/cm ² sec |
| Kinetic Illite | 1.5 g |
| surface area | 3 cm ² /g |
| Rate constant | 1.66e-17 mol/cm ² sec |
| Fix fugacity of CO ₂ (g) | |
| add | |
| reactants times 1 | |



- Model does not match observed concentrations
- Calcium matches depending on available surface area



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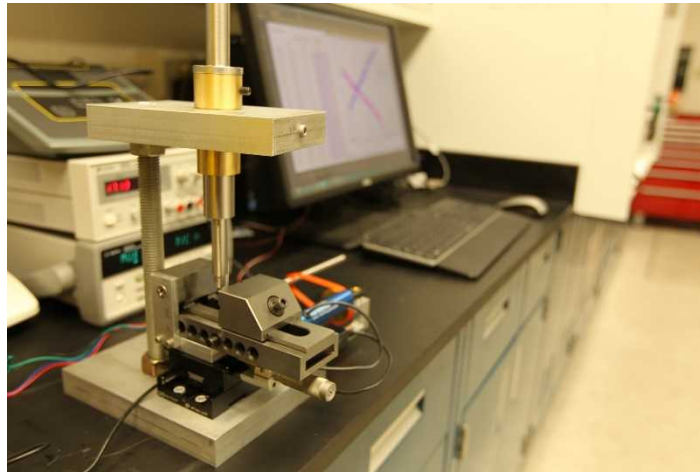


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Scratch Testing



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Conclusions

- Boise sandstone is generally insensitive to water, dry scCO_2
- Fully saturated scCO_2 causes weakening in Boise sandstone that is exacerbated at higher confining pressures, leading to a decrease in the slope of the failure envelope
- Partial humidities of scCO_2 do not show clear weakening or strengthening trends
- Water present as humidity in scCO_2 does transport ions, is reactive
- Total amount of water available in partially saturated scCO_2 is very small, not enough to drive significant chemical reactions; but if there is sufficient amount of water available, chemical reactions can cause significant changes in strength.



Planned Manuscripts

The Effect of Hydrrous scCO₂ on the Mohr-Coulomb Failure Envelope in Boise Sandstone

Choens, Dewers, Ilgen, Espinoza, Aman, Wheeler, Ganis

The Effect of Hydrrous scCO₂ on Deformation Band Development in Boise Sandstone

Choens, Dewers, Wheeler, Ganis

The Effect of Hydrrous scCO₂ on the Consolidation of Boise Sandstone

Choens, Dewers, Prodanović, Mirabolghasemi

The Effect of Hydrrous scCO₂ on the Fracture Toughness of Boise Sandstone

Choens, Dewers, Eichubl, Majors, Espinoza, Aman

Reservoir Response Induced by the presence of Hydrrous scCO₂

Choens, Dewers



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