

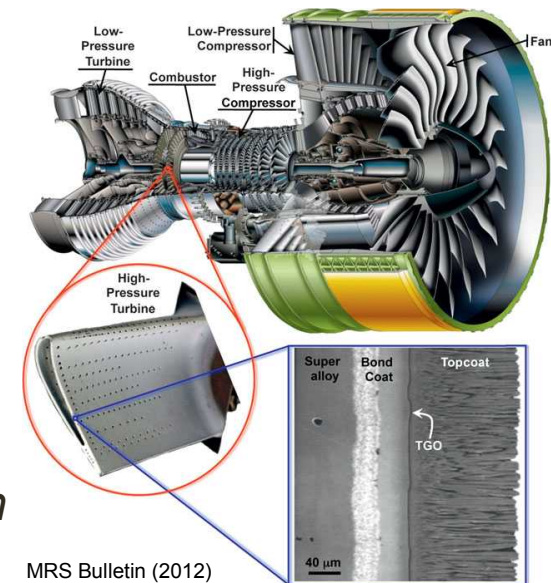
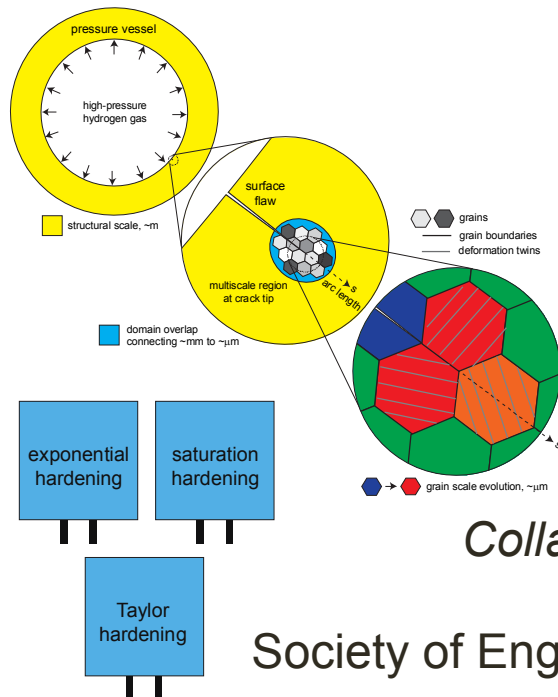


Concurrent multiscale modeling of microstructural effects on localization behavior in finite deformation solid mechanics

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Alejandro Mota*

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Society of Engineering Science 53rd Annual Technical Meeting
October 4, 2016

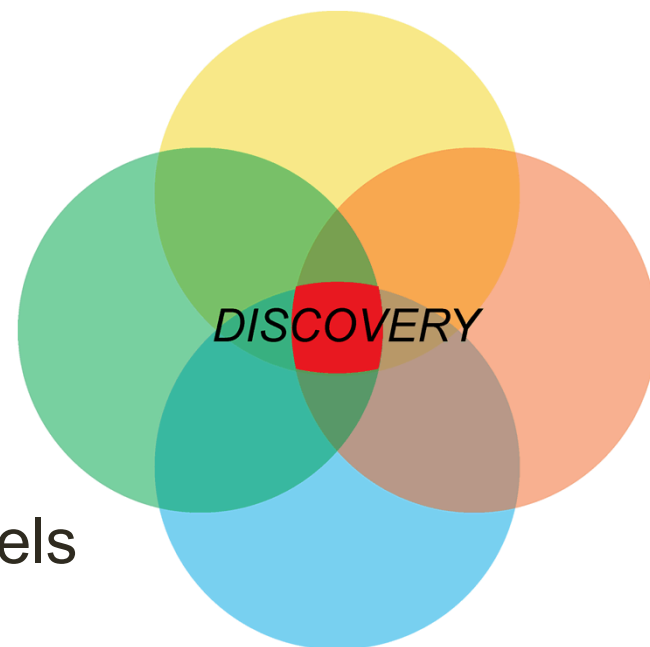


MRS Bulletin (2012)

Overview

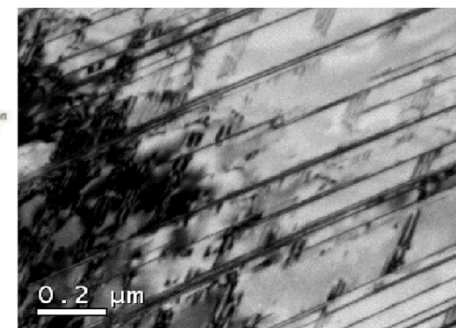
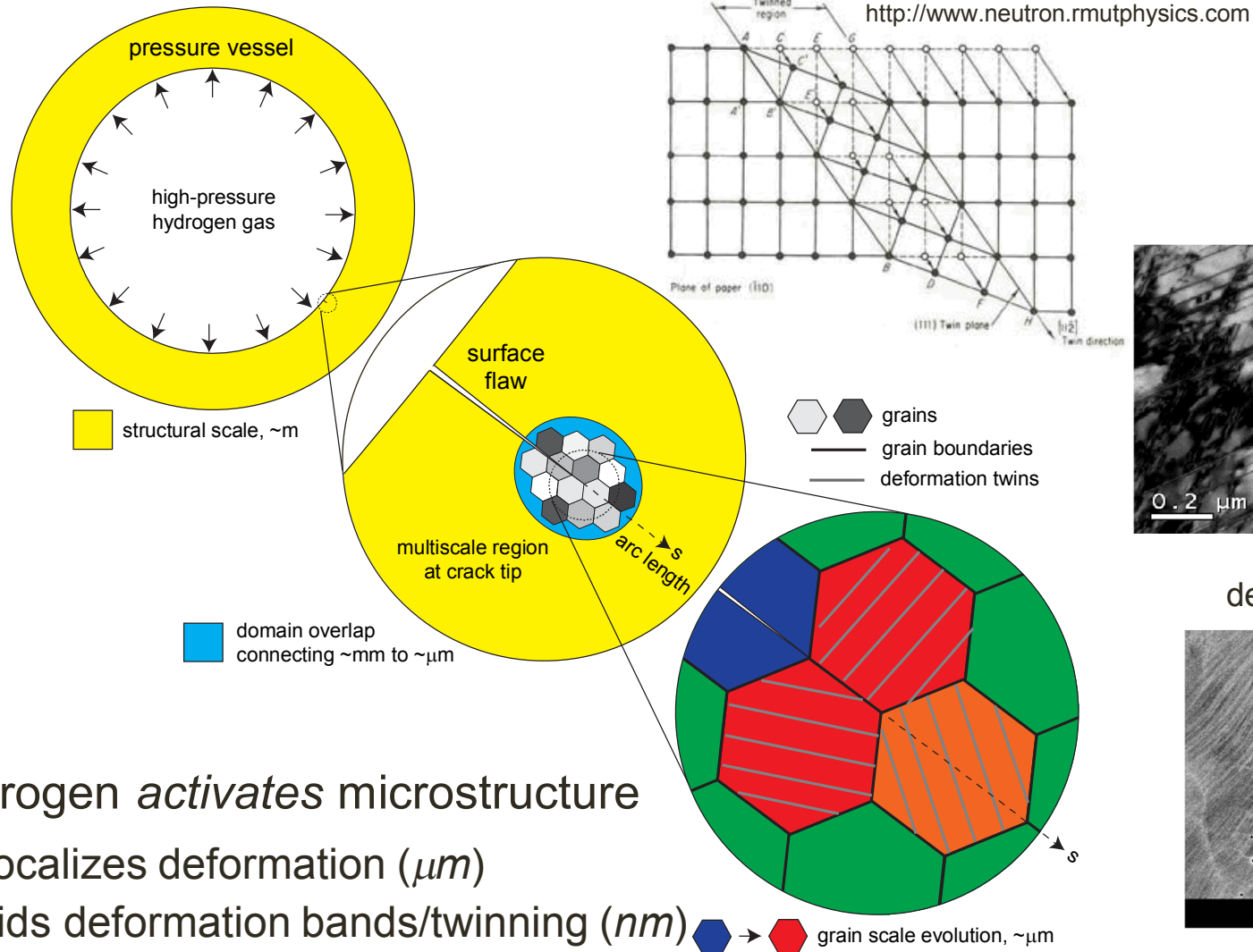
Developing strong, concurrent, multiphysics, multiscale coupling to understand the impact of microstructural mechanisms on the structural scale

- Applications invoke microstructure
- Explicitly connecting scales
- Resolving strong multiphysics
- Developing discrete microstructural models
- Resolution through manycore/GPUs

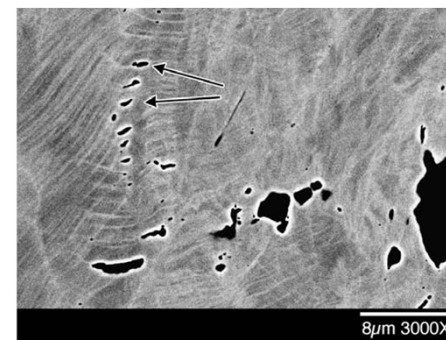


Goal: Predict void nucleation at the microscale

Hydrogen activates microstructure (stainless steel)



extensive slip and deformation twinning

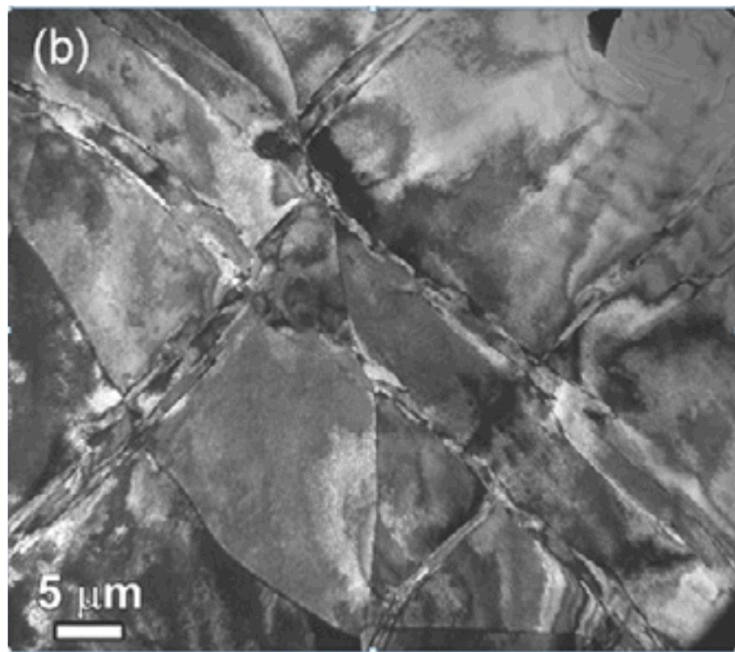


premature void nucleation*

Hydrogen *activates* microstructure

- Localizes deformation (μm)
- Aids deformation bands/twinning (nm)
- Accentuates boundary interactions (nm)

Temperature/strain-rate activates microstructure (Ta)



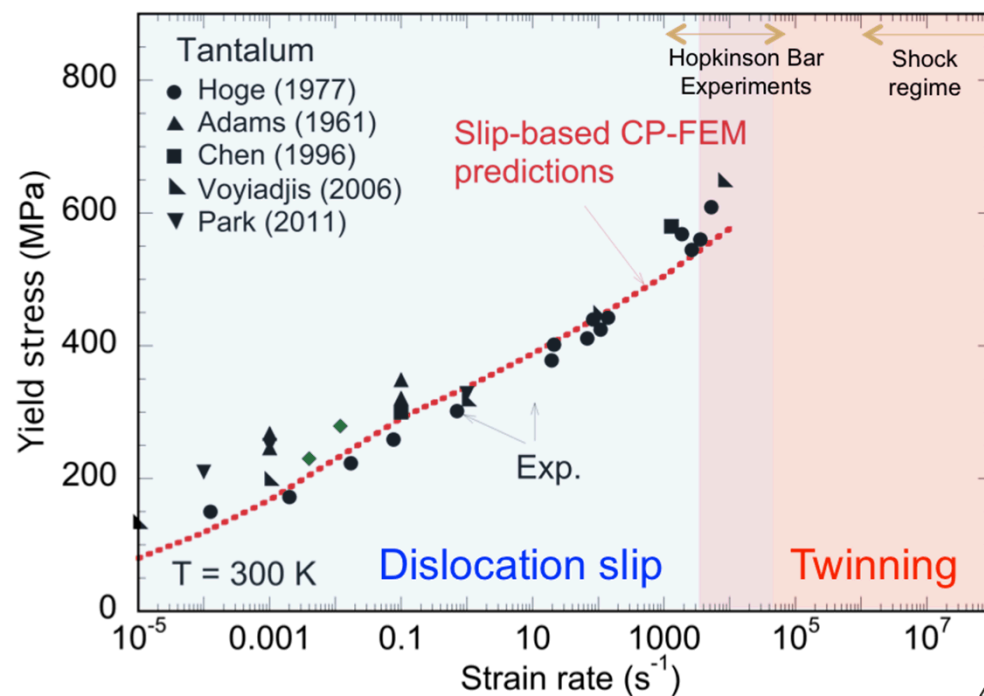
TEM micrograph of deformation twins in Ta¹
($T=77\text{ K}$ and $\dot{\epsilon} = 2.2 \times 10^4\text{ s}^{-1}$).

Length scales span $10\mu\text{m} - 1\text{mm}$

- Extensive slip within grains
- Twins evolve within steep gradients

Strain rate & temperature *activates* microstructure and *localizes* deformation

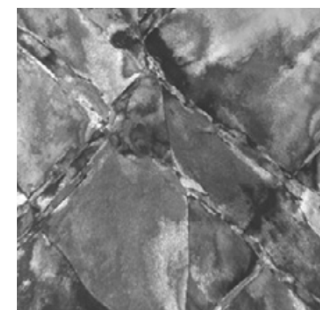
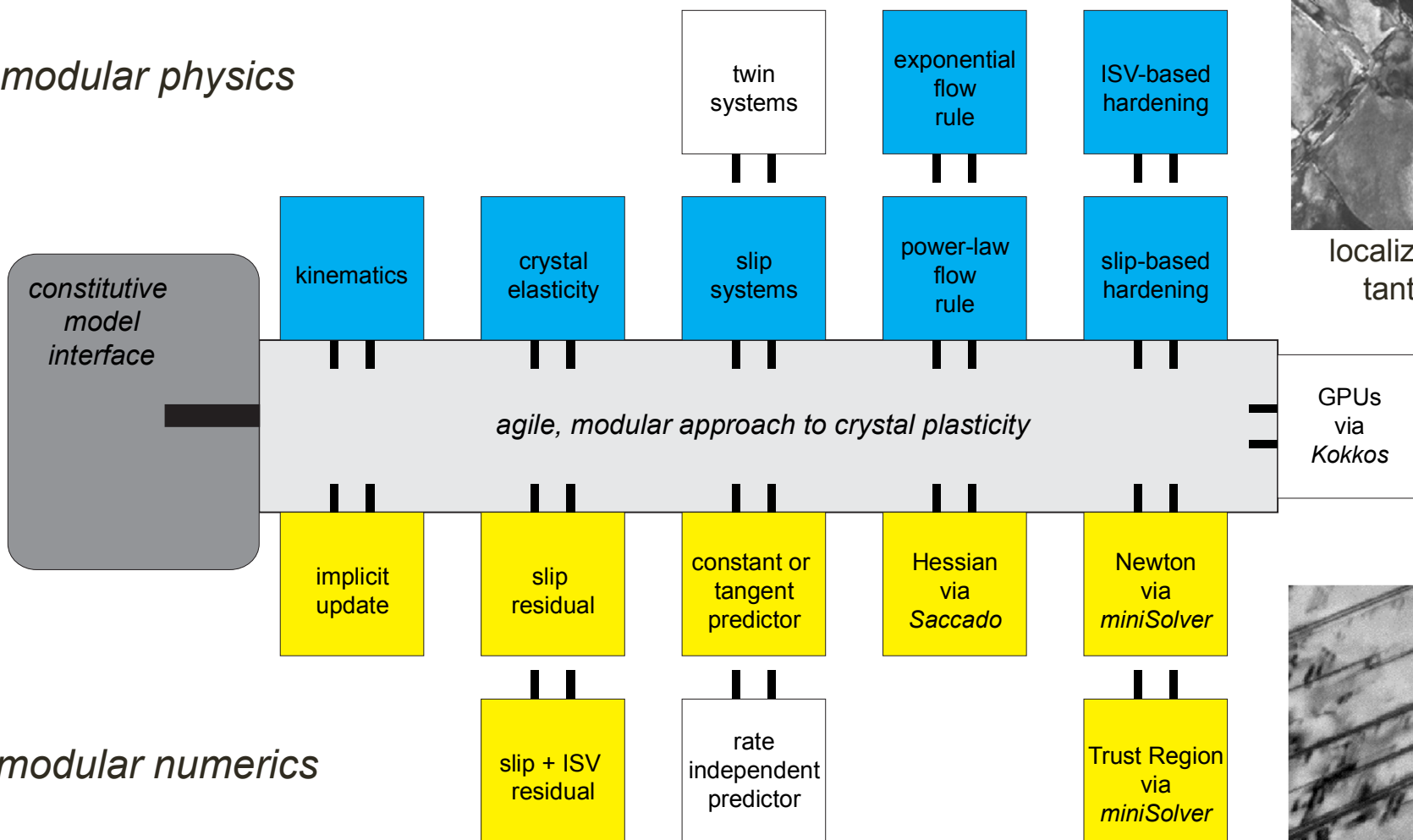
- Increased strain rate ($10^3, 10^4$) and decreased temperature aids twinning (nm)
- Accentuates grain boundary interactions (nm)



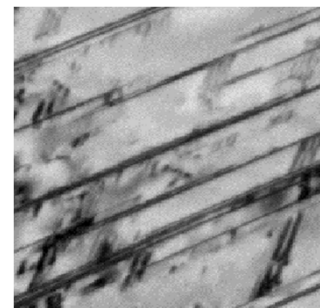
¹Chen, C. Q., Hu, G., Florando, J. N., Kumar, M., Hemker, K. J., Ramesh, K. T., Interplay of dislocation slip and deformation twinning in tantalum at high strain rates, *Scripta Materialia* 69 (2013) 709 – 712.

Agile components of crystal plasticity

modular physics



localization in tantalum



localization in stainless steel

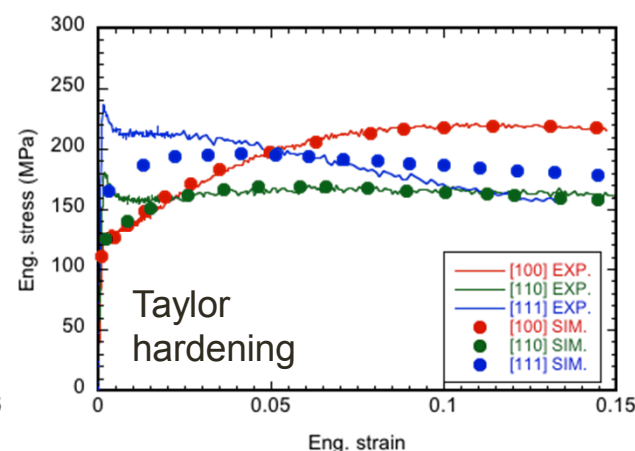
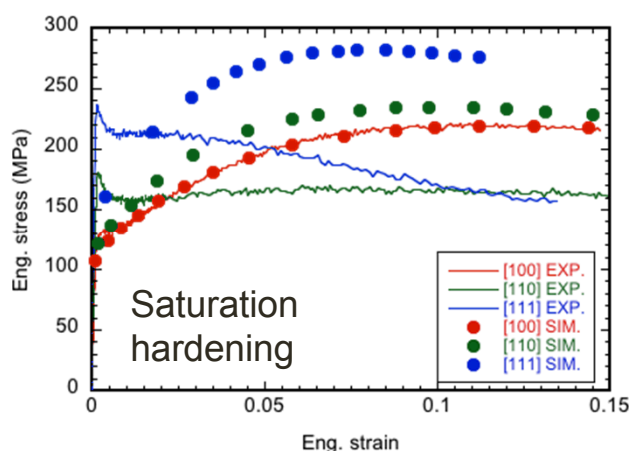
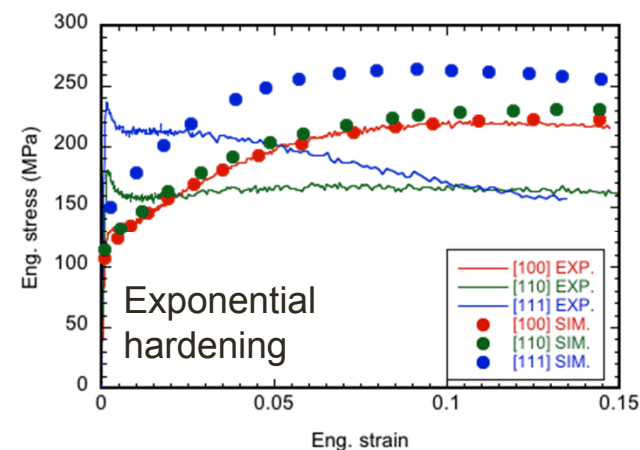
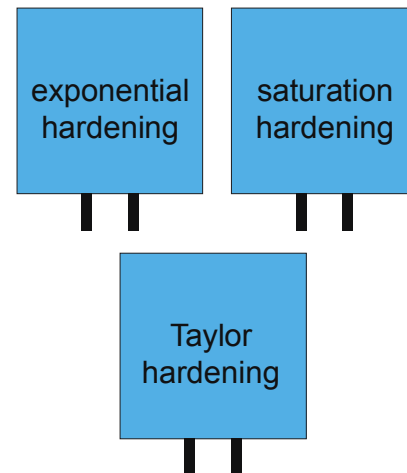
Multiple methods facilitate learning and lower the barrier for new advances.

Predictions in single crystal Ta with physics++

Exponential hardening $g^\alpha = H_0 + \frac{H_1}{H_2} (1 - \exp(-H_2 \varepsilon^\alpha))$

Saturation hardening $\dot{g}^\alpha = \dot{g}_0 \left(\frac{g_s - g^\alpha}{g_s - g_0} \right) \sum_\beta 2 |S_{ij}^\alpha S_{ij}^\beta| |\dot{\gamma}^\beta| \quad g_s = g_{s0} \left| \frac{\dot{\gamma}}{\dot{\gamma}_0} \right|^\omega$

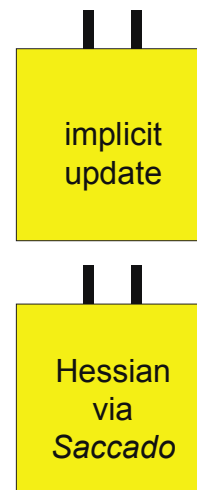
Taylor hardening
(dislocation density) $g^\alpha = A\mu b \sqrt{\sum_{\beta=1}^{24} \mathbf{H}^{\alpha\beta} \rho^\beta} \quad \dot{\rho}^\alpha = \left(\kappa_1 \sqrt{\sum_{\beta=1}^{NS} \rho^\beta} - \kappa_2 \rho^\alpha \right) \cdot |\dot{\gamma}^\alpha|$



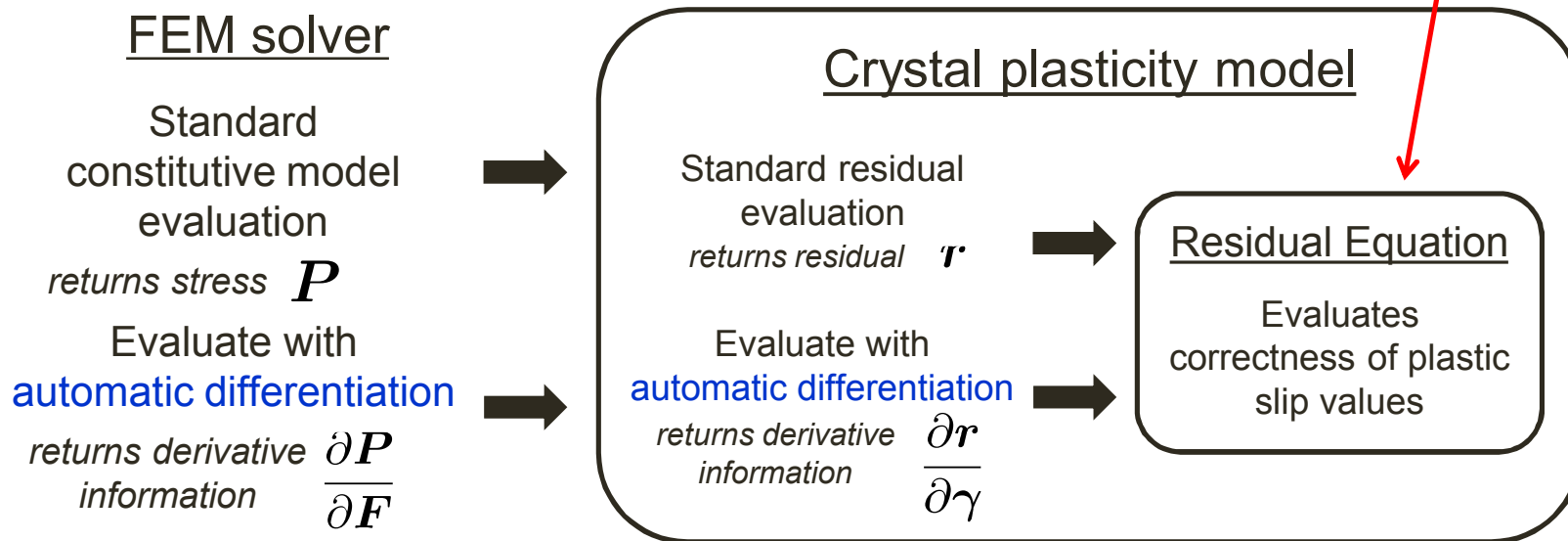
- Increment physics through an array of hardening models in crystal plasticity framework
 - Parameterize through BCC Ta single crystal experiments in [100] orientation
 - Predict response in [110] and [111] orientations.
- Dislocation density based Taylor hardening model* most accurately reflects anisotropy.

Automatic differentiation enables modularity

- *Goal:* Allow users to mix and match crystal plasticity features
 - Crystal structure, flow rule, hardening law, etc.
- *Challenge:* Altering the crystal plasticity equations requires difficult changes to the model's state update routine (implicit update)
- *Strategy:* Automatic differentiation using the *Sacado* package dramatically reduces the required changes to material model



minimal coding required!



Measuring robustness through application

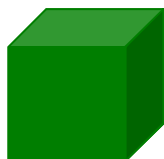
Robustness suite

small
step

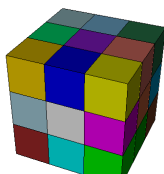
medium
step

large
step

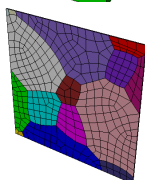
single-slip
multi-slip



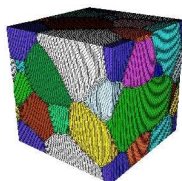
Rubik's
cube



polycrystal
(2D)



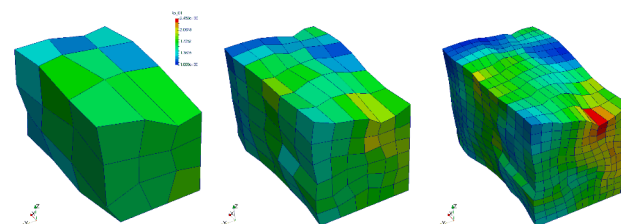
polycrystal
(3D)



increasing
complexity

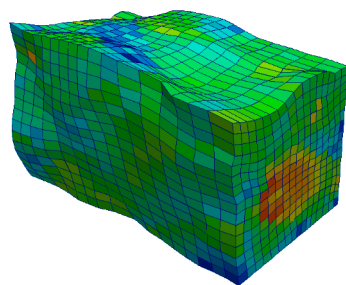
Rubik's cube case

- Random texture
- 100% engr. strain
- Vary elements/grain
- Vary step size
- Vary solution methods

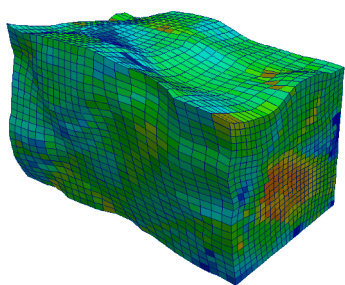


Sample microstructures with

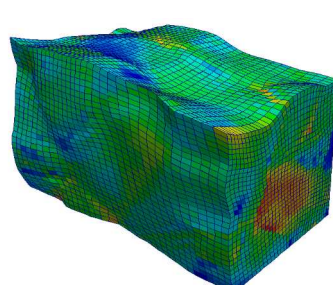
- Voxlated grain boundaries
- Conformal grain boundaries



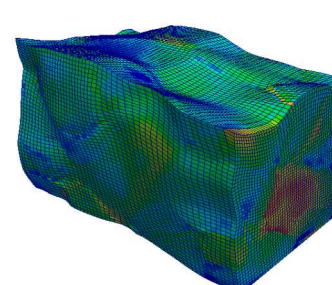
871 steps



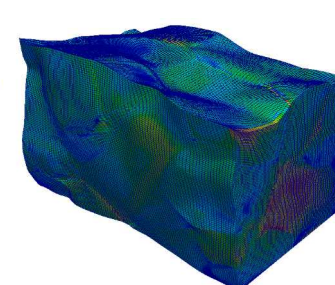
929 steps



1062 steps

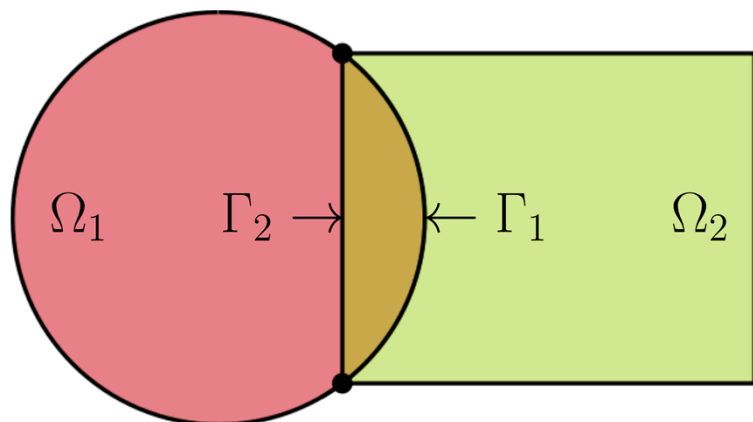


1170 steps



1545 steps

Update on the Schwarz alternating method



Hermann Schwarz (1870)

Initial conditions for Partial Differential Equation (PDE)

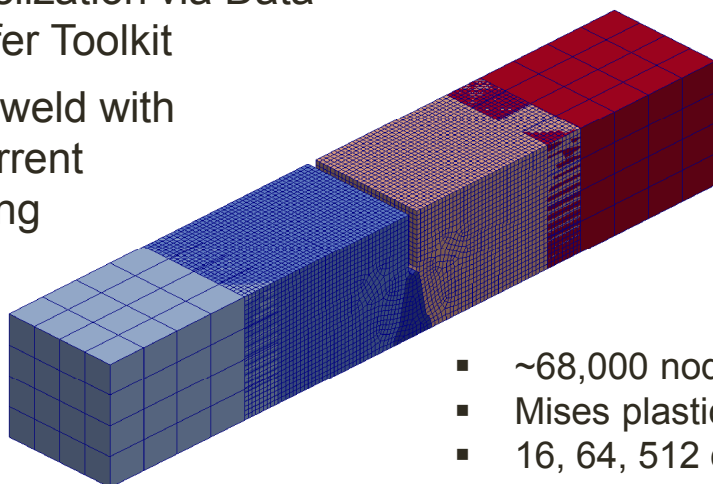
- Solve PDE by any method on Ω_1 using an initial guess for Dirichlet BCs on Γ_1 .

Iterate

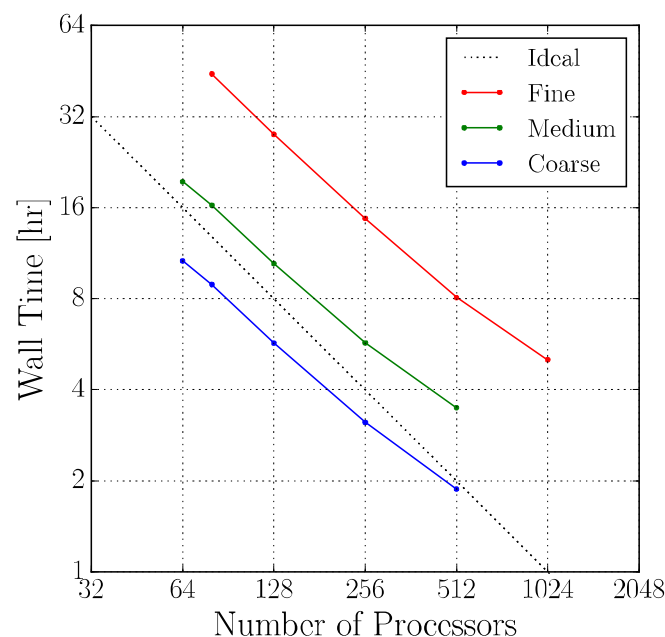
- Solve PDE by any method on Ω_2 using Dirichlet BCs on Γ_2 that are the values just obtained for Ω_1 .
- Solve PDE by any method on Ω_1 using Dirichlet BCs on Γ_1 that are the values just obtained for Ω_2 .

Parallelization via Data
Transfer Toolkit

Laser weld with
concurrent
coupling



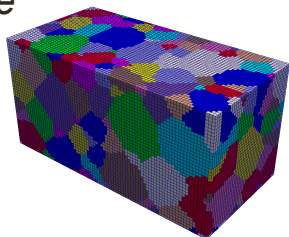
- ~68,000 nodes
- Mises plasticity
- 16, 64, 512 cores



Ingredients of a Schwartz analysis

1 part mesoscale

voxelated microstructure derived
from phase-field evolution
(F. Abdeljawad)



cubic elastic constant : $C_{11} = 204.6$ GPa

cubic elastic constant : $C_{12} = 137.7$ GPa

cubic elastic constant : $C_{44} = 126.2$ GPa

reference shear rate : $\dot{\gamma}_0 = 1.0$ 1/s

rate sensitivity factor : $m = 20$

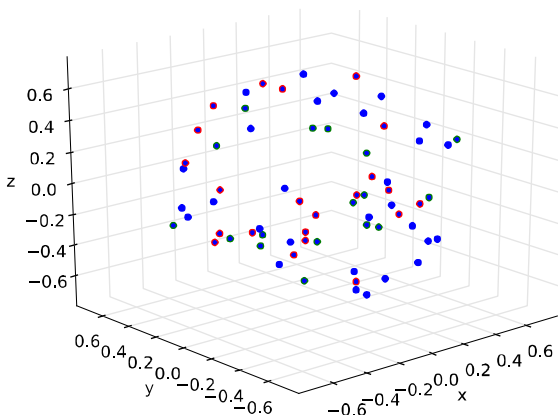
hardening rate parameter : $\dot{g}_0 = 2.0 \times 10^4$ 1/s

initial hardness : $g_0 = 90$ MPa

saturation hardness : $g_s = 202$ MPa

saturation exponent : $\omega = 0.01$

IS

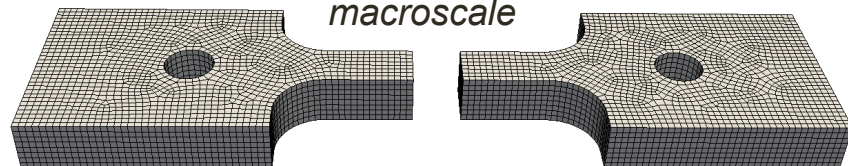


151 axial vectors
from 3 of the 10
ensembles of
random rotations
(blue, green, red)

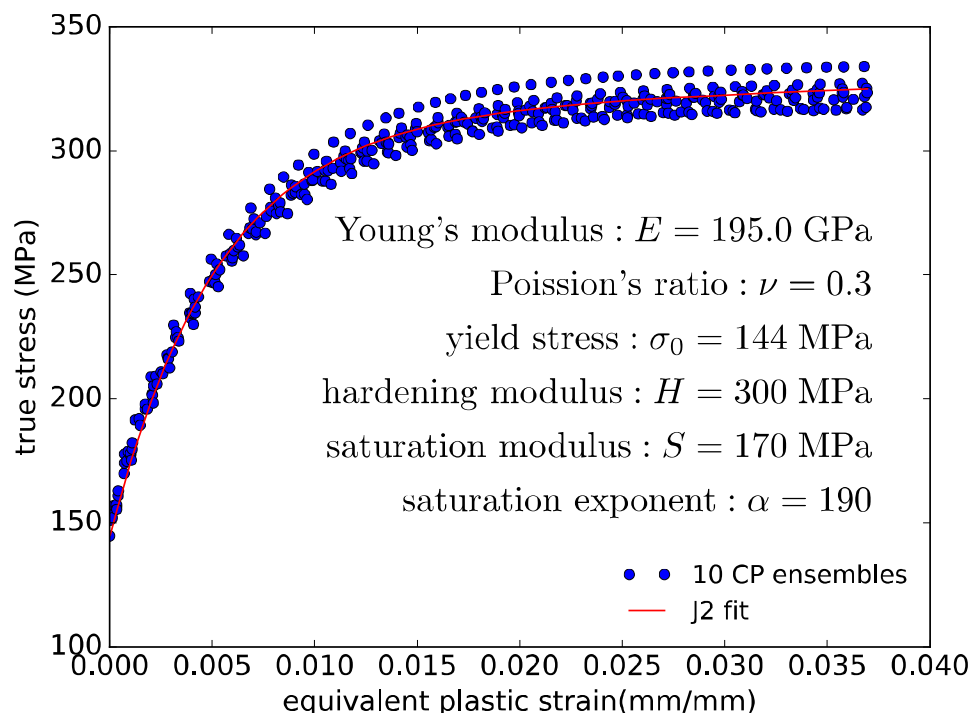
Point of
collaboration with
Multiscale
Reliability LDRD

+

2 parts
macroscale

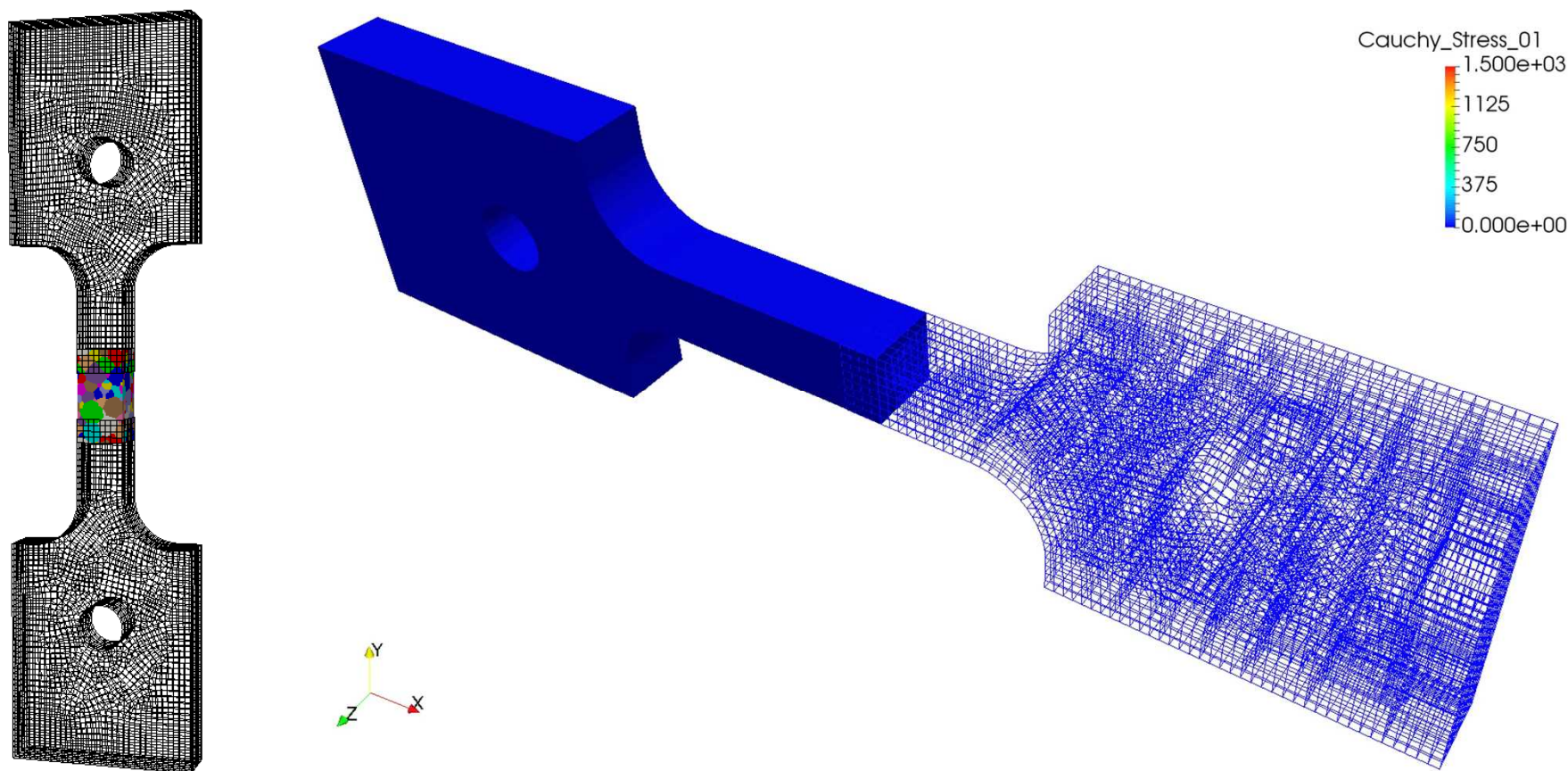


- Load microstructural ensembles in uniaxial stress
- Convert load/displacements to flow curves
- Fit flow curves with a macroscale J_2 plasticity model



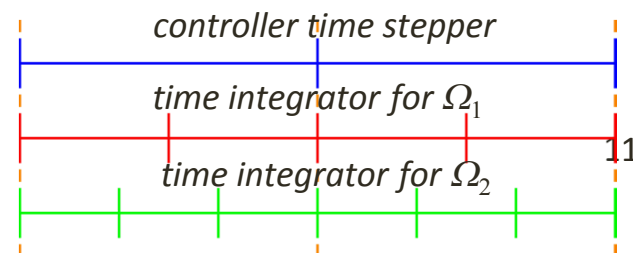
$$\sigma_y = \sigma_0 + H\epsilon_p + S(1 - e^{-\alpha\epsilon_p})$$

Coupling components to microstructure

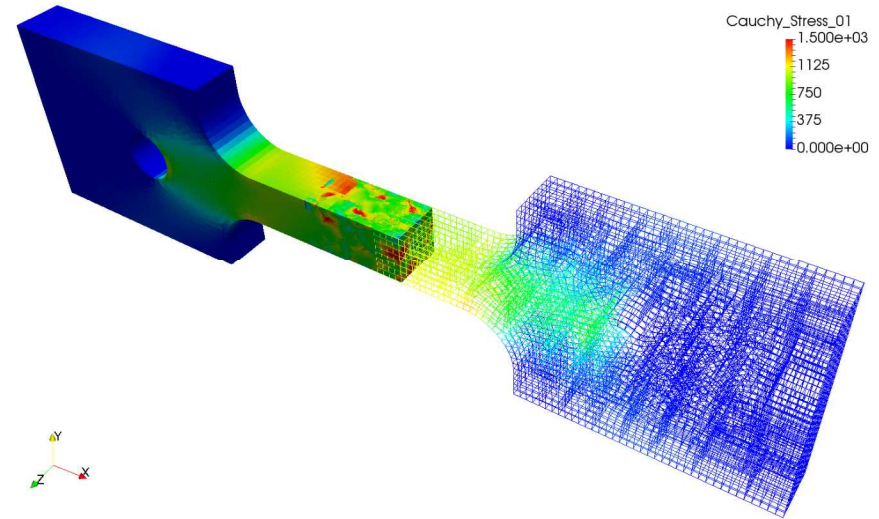
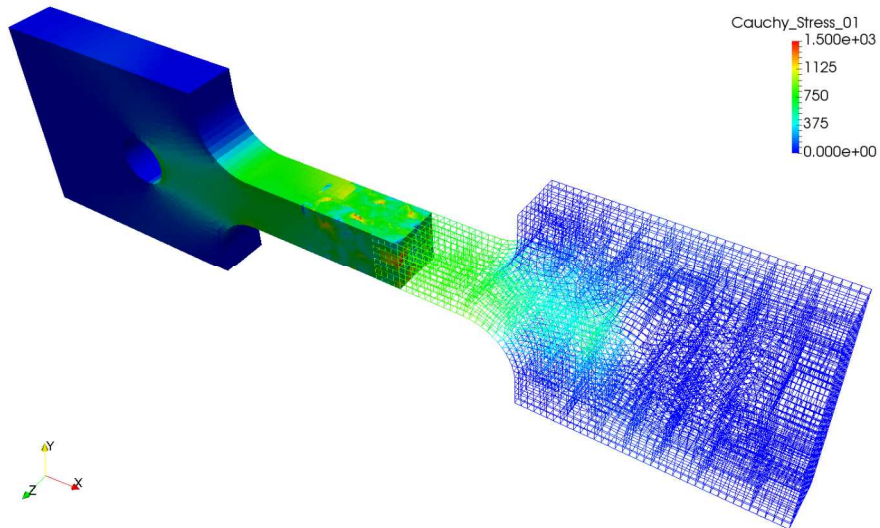
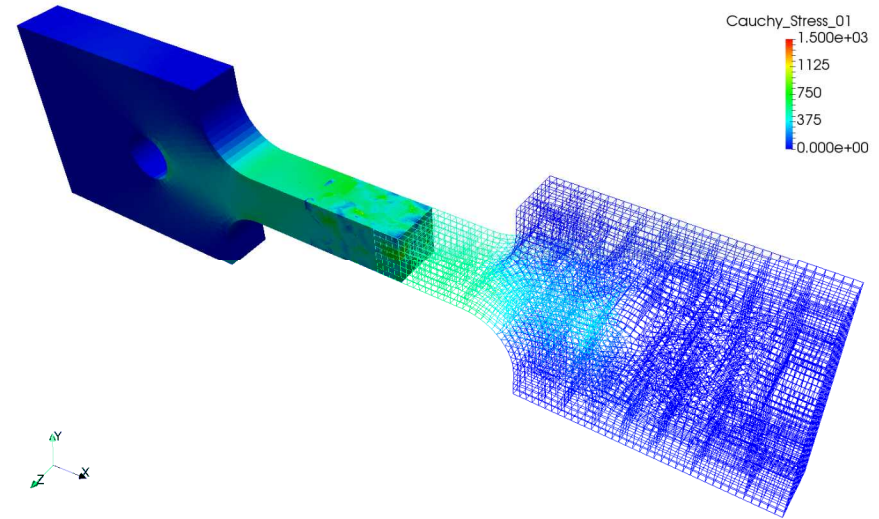
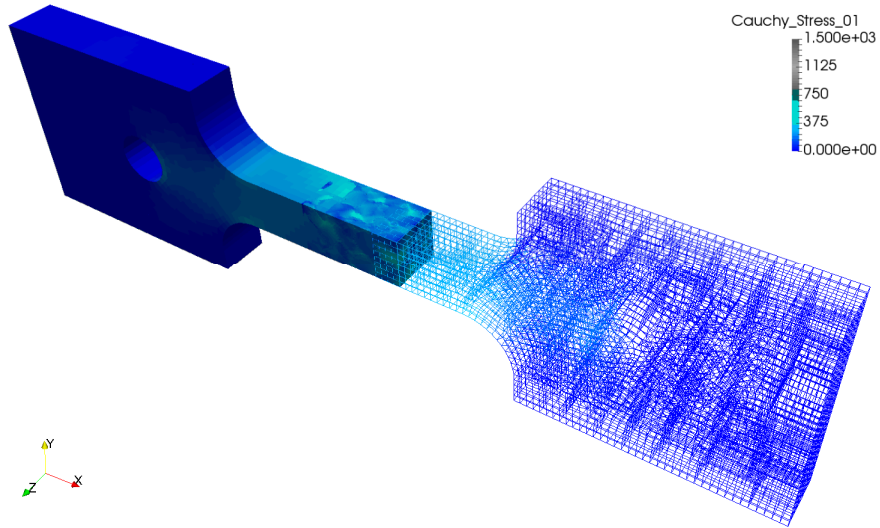


Embed microstructure in
ASTM tensile geometry

- Currently extending Schwarz coupling to dynamics
- Extending approach to multiphysics



Coupling components to microstructure

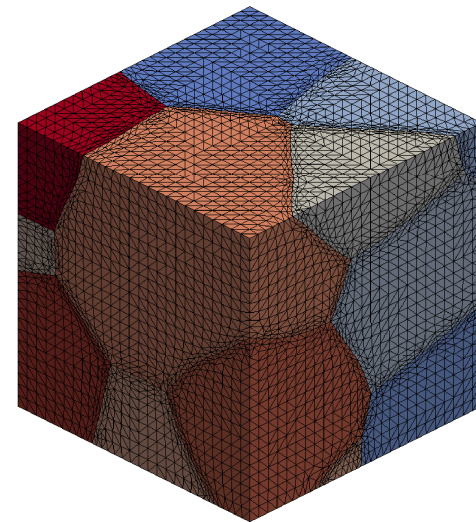
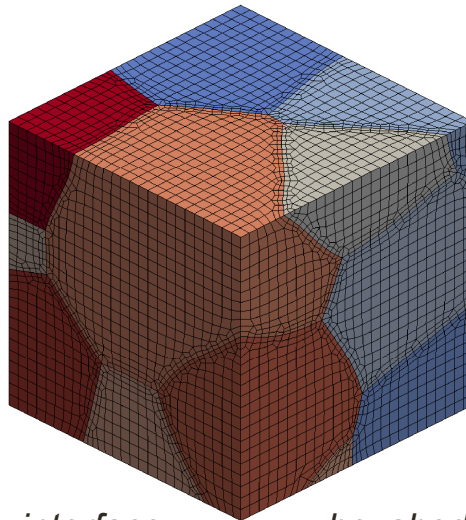
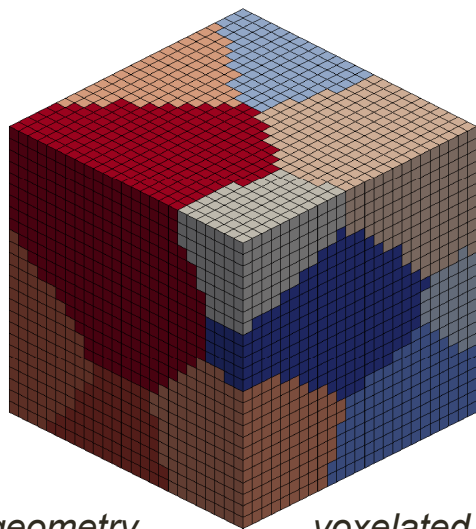


SCULPT, conformal boundaries, tet meshing

DREAM.3D, KMC, or phase field

SCULPT

Cubit



*geometry
+ physics*

*voxelated
microstructure*

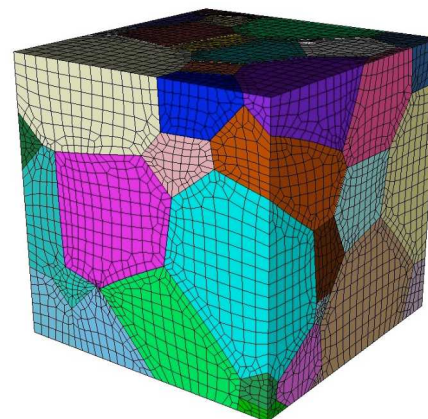
*interface
reconstruction*

*hexahedral
discretization*

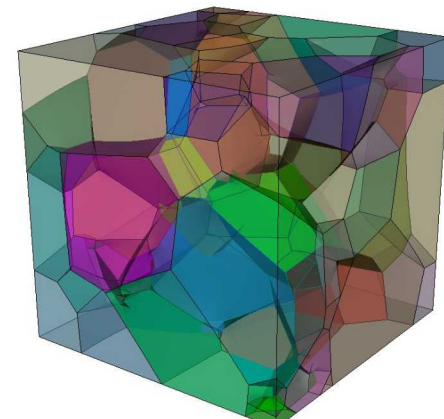
*mesh
geometry*

*tetrahedral
discretization*

- SCULPT powerful tool for microstructure
- Performs interface reconstruction & meshing
- All-hex meshes can be problematic
- Mesh refinement requisite for solution
- Move from reconstruction to geometry
- Export STL or // tet mesh in SCULPT
- Leverage new surface & volume tet meshers



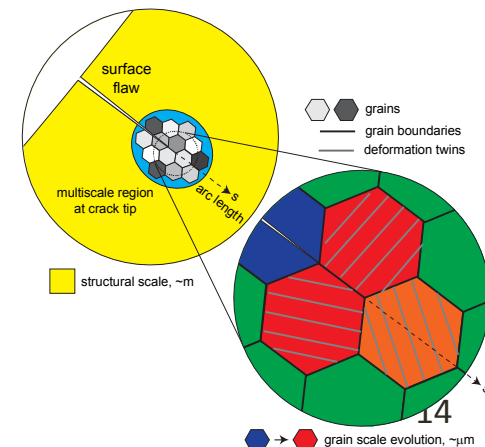
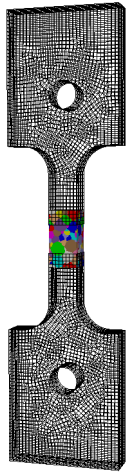
hexes problematic



geometry for tets

Filling gaps and overcoming barriers

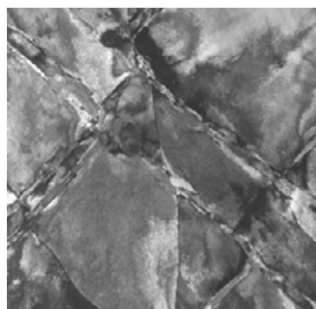
- Develop a more fundamental understanding of localization in
 - Austenitic stainless steel structures exposed to hydrogen gas
 - Tantalum structures subjected to high rates of loading
- Discovery enabled through
 - Intimate connection between structure and microstructure (Schwarz)
 - Strong multiphysics capable of capturing autocatalytic processes
 - Systematically increasing microstructural physics
 - Robust solution methods for increasing complexity
 - Extension to next generation platforms



Part of a top down strategy (macro to micro) to provide context, identify disconnects, and provide drivers.

Additional slides

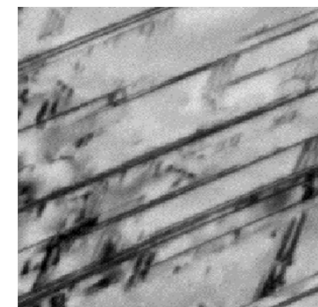
Intersection of materials science, engineering science, and computer science



localization in tantalum



Phalanx for multiphysics



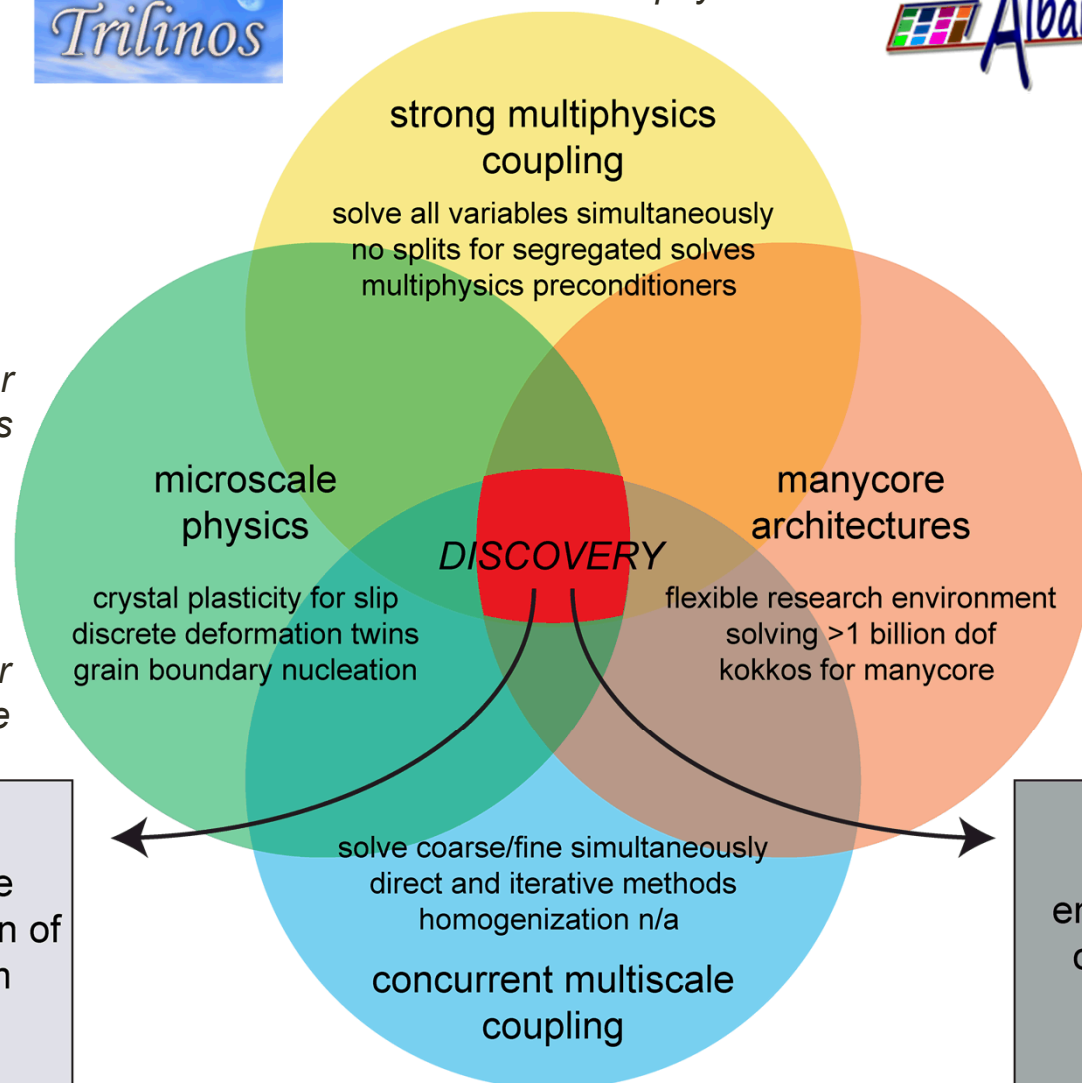
localization in stainless steel

miniTensor for mechanics

Sacado for the Hessian

miniSolver for constitutive update

high-rate deformation of tantalum



Intrepid for element library

Massively parallel solvers

Kokkos for next generation platforms

hydrogen embrittlement of stainless steels

Teko & Data Transfer Toolkit for spatial multiscale

Finite deformation, strong, multiphysics coupling

Fox and Simo (1990), Callari, Armero, Abati (2010)

redefine
space

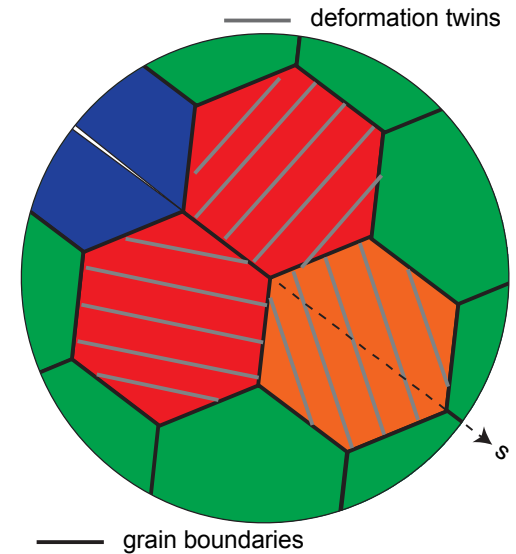
$$\mathbf{X} = \Phi(\xi^1, \xi^2, \xi^3) = \bar{\Phi}(\xi^1, \xi^2) + \mathbf{N}(\xi^1, \xi^2)\xi^3$$

include jump in
concentration

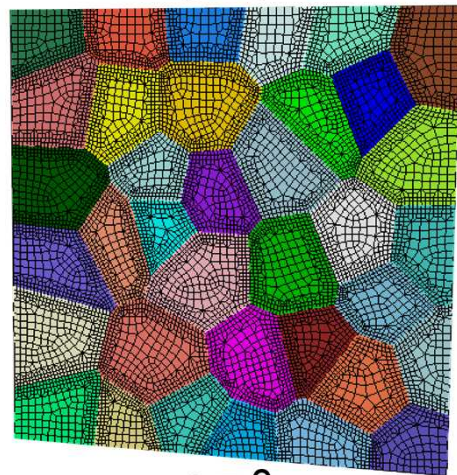
$$C(\mathbf{X}) = \bar{C}(\phi[\xi^1, \xi^2]) + \frac{[[C]](\phi[\xi^1, \xi^2])}{h}\xi^3$$

$$\mathbf{G}_i = \Phi_{,i} = \frac{\partial \mathbf{X}}{\partial \xi^i} \quad \nabla_{\mathbf{X}} C = (\nabla \Phi)^{-T} \frac{\partial C}{\partial \xi^i}$$

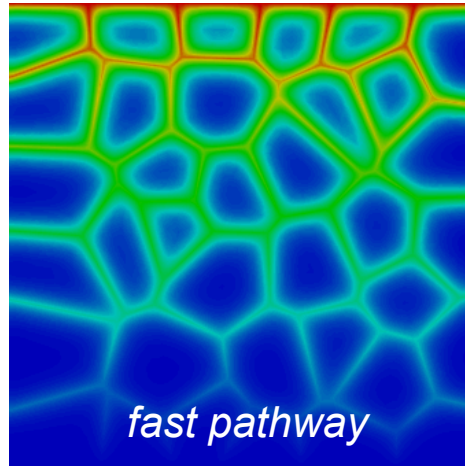
finite element implementation is straightforward



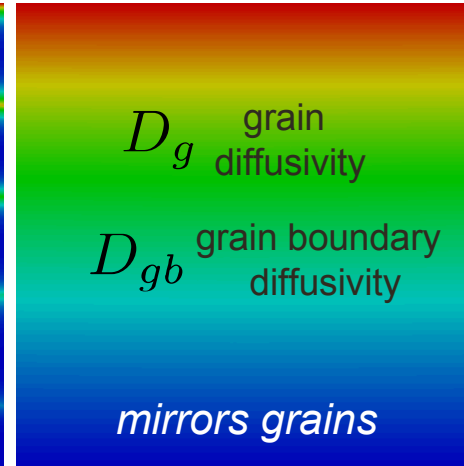
$c = 1$



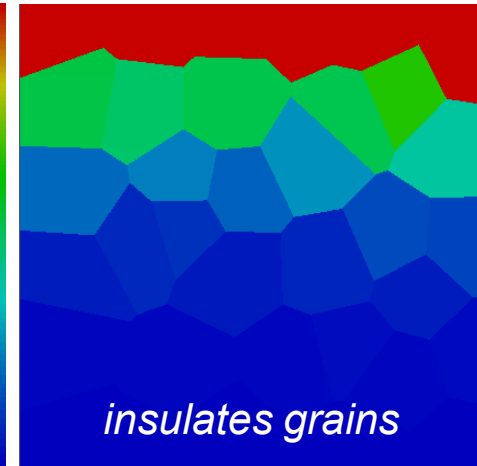
$c = 0$



$$D_{gb} = 1 \times 10^5 D_g$$



$$D_{gb} = D_g$$



$$D_{gb} = 1 \times 10^{-5} D_g$$

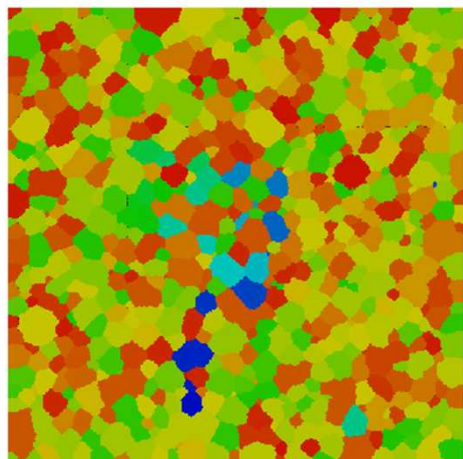
Lessons learned: Block solves require robust methods for scaling. Work in progress.

Collaboration through Georgia Tech

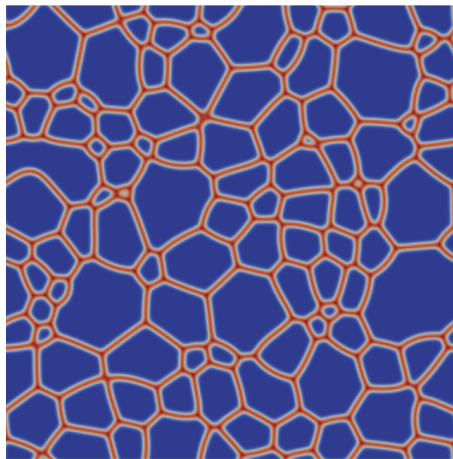
Exploring microstructure-mechanical property relationship using statistical data analysis

Multiscale/multiphysics LDRD. SNL PI: Hojun Lim. GT PI: Professor Surya Kalidindi

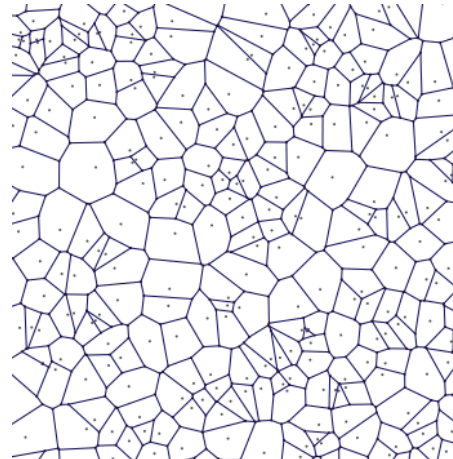
Rigorous statistical quantification of polycrystalline microstructures



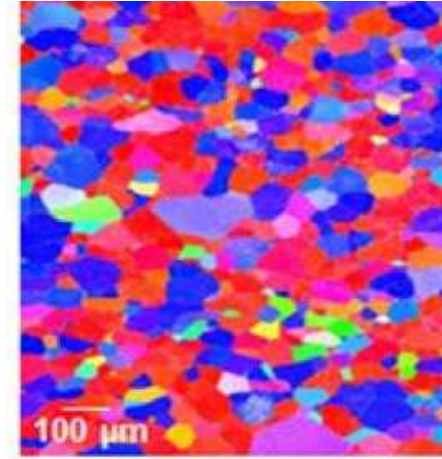
KMC grain growth



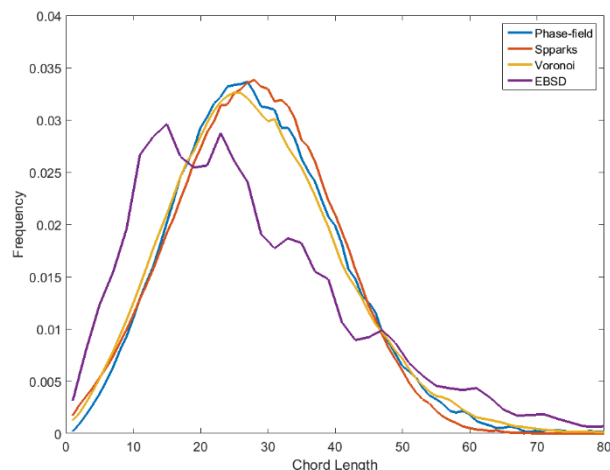
Phase field grain growth



Voronoi tessellation



EBSD



grain boundary chord lengths

Future work w/ focus on *Data Science* (~100K)

- Method for creating statistically equivalent microstructures from 2-D EBSD data (03/17)
- Conduct CP-FEM simulations of Ta and stainless steel using statistically generated 3-D polycrystalline microstructures (09/17)
- At least two papers will be submitted to archival journals and a final report with the same information will be submitted (09/17)

Professor: S. Kalidindi, Postdoc: E. Popova, PhD student: D. Patel