

Dependence of Grain Boundary Structure on Radiation Induced Segregation and Void Denuded Zones in a Model Ni-Cr Alloy

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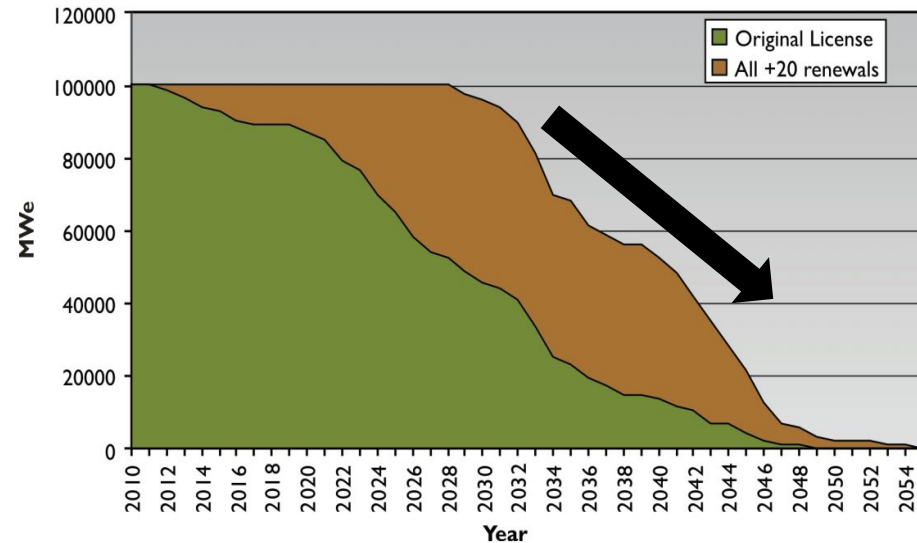
* Currently at Sandia National Laboratory, work presented here completed while at Drexel University

Motivation: Aging Reactors and Materials Failure

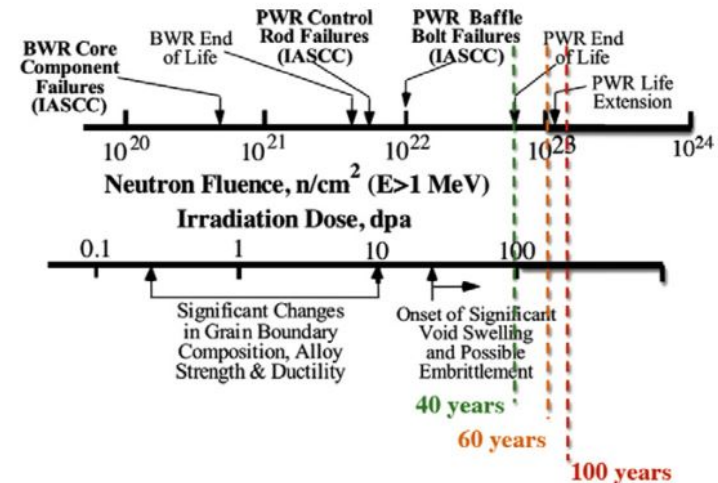
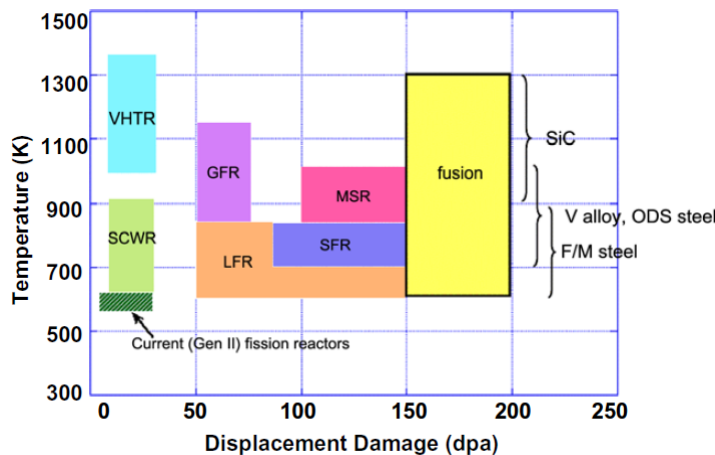
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- Key non-fossil fuel energy system for electrical demand in emerging and existing markets
- Safe and reliable material extension for current LWR materials and future nuclear reactor designs
- Ageing fleet, average age is > 35 years: high maintenance and upgrade cost
- **Next generation → new alloy development**

Estimated energy output from existing reactors

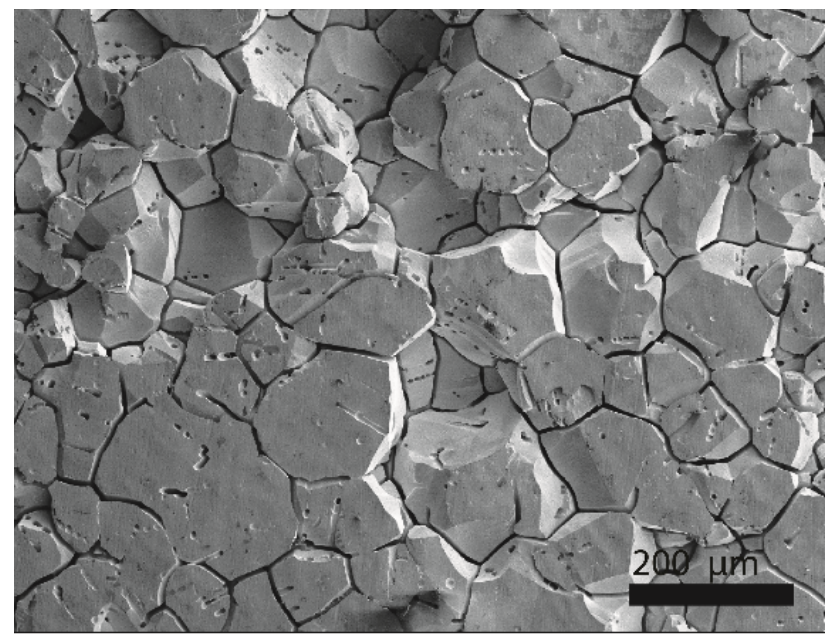


US-DOE Report to congress, 2012



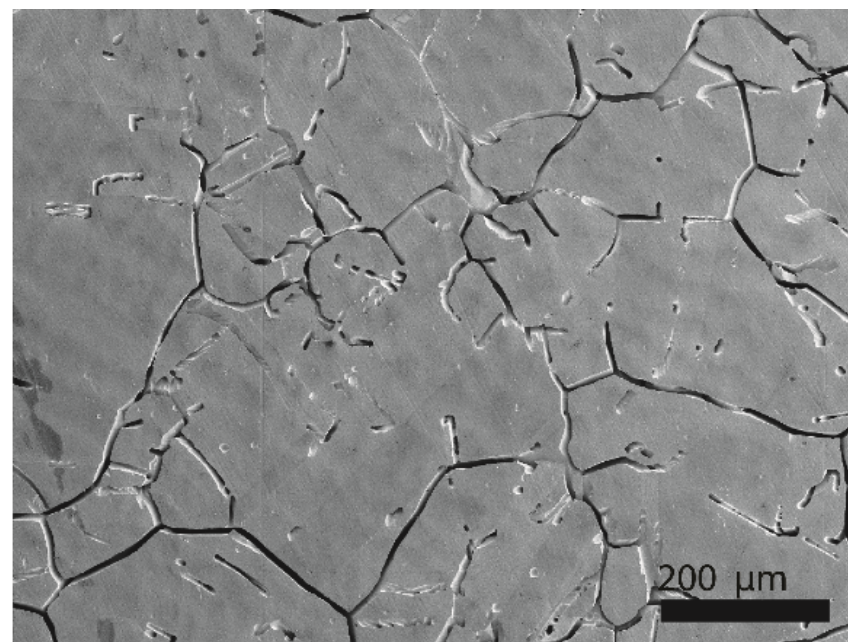
- Grain boundaries (GBs) are a critical material interfaces → tailoring network provides method for sophisticated microstructures
- **GB character** → variations in GB structure/properties can lead to subsequent changes in response to extreme environments

Standard 316: 4.2 mm/yr.

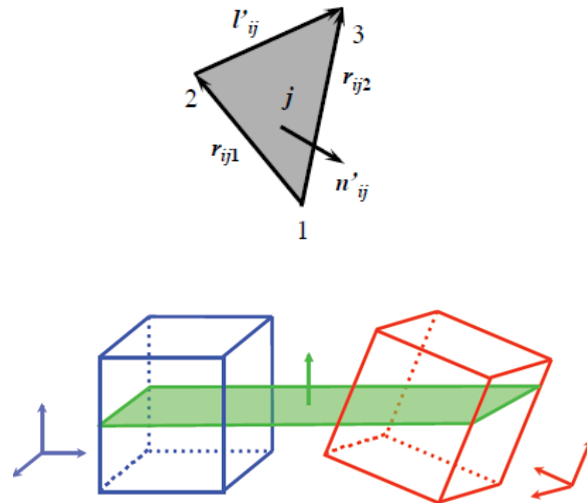
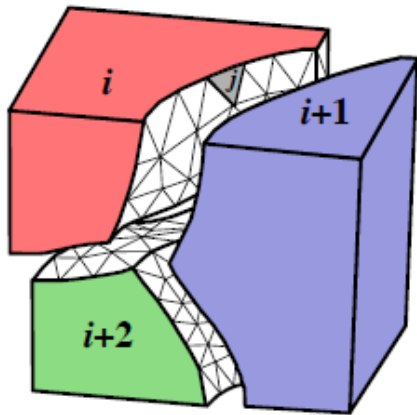


➔
Increased
corrosion
resistance

Engineered 316L: 2.2 mm/yr.



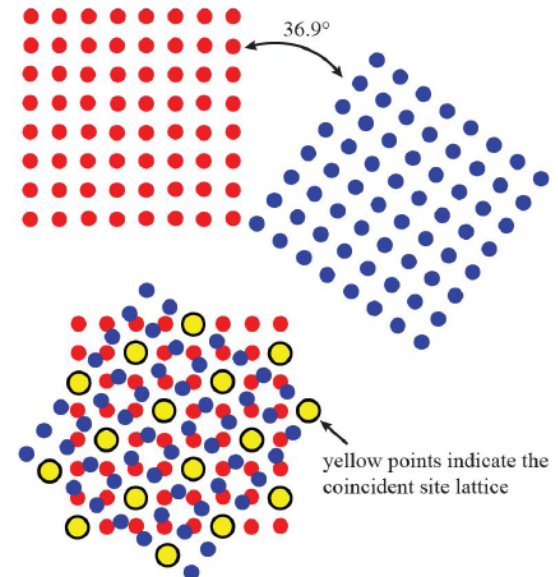
- High and low angle GBs, tilt/twist, symmetric/ asymmetric
- Coincidence Site Lattice (CSL) notation (geometric model)
- Reports indicate a link between some CSL GBs (e.g. $\Sigma 3$) and improvements in intergranular corrosion, stress corrosion cracking, and hydrogen embrittlement



Misorientation (Δg) and grain boundary plane normal (n)

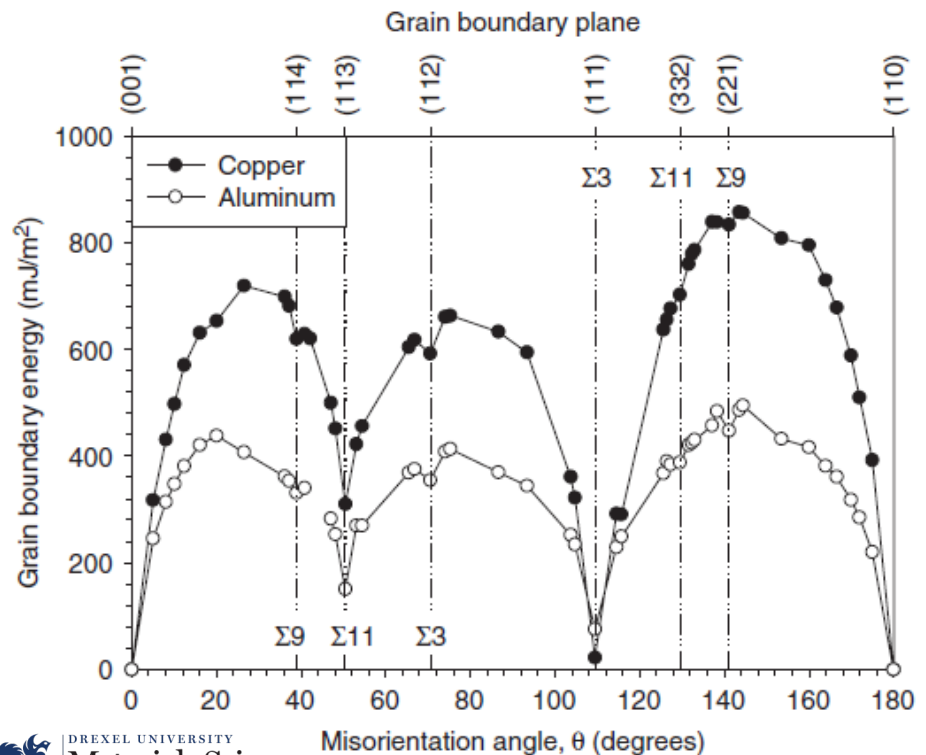
CSL Boundary Notation

36.9° rotation
Axis of rotation: 100
Boundary type: $\Sigma 5$

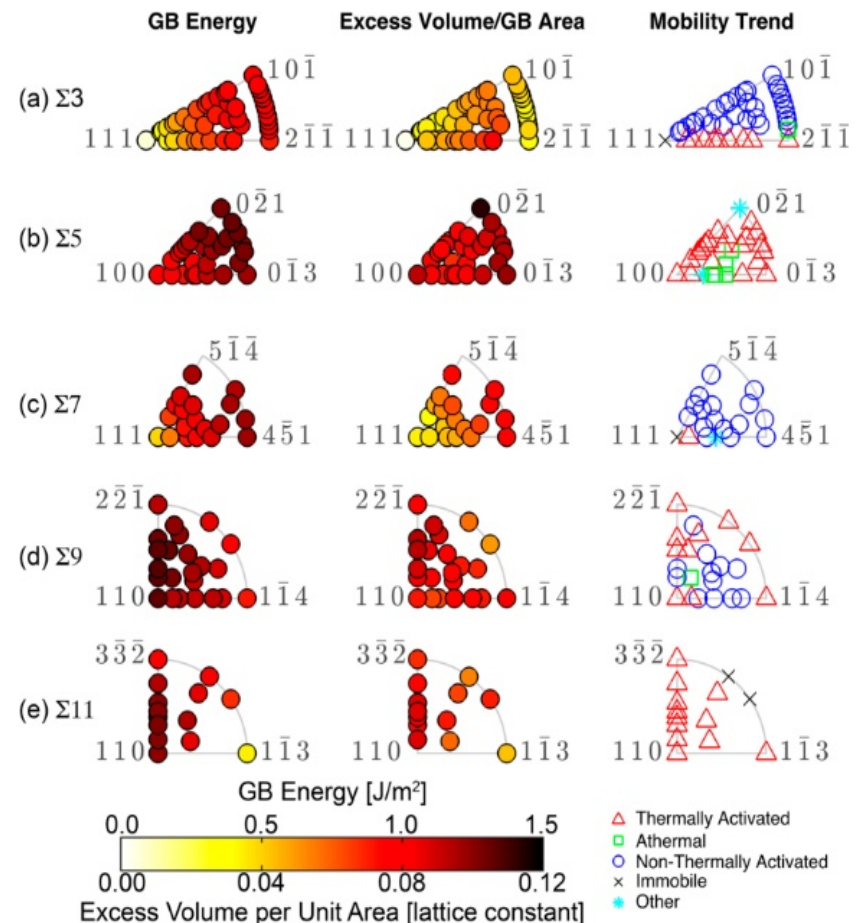


E.A. West, Michigan (2010)

- GB landscape highlights specific GBs that have low energy or excess volume
- GB energy does not correlate with “low” coincidence site lattice (CSL) Σ GBs
- GB-defect interactions: formation energies, load/pristine GBs, interaction widths



Tschoep et al., Phil Mag (2009)



Homer et al., Sci. Reports (2015)

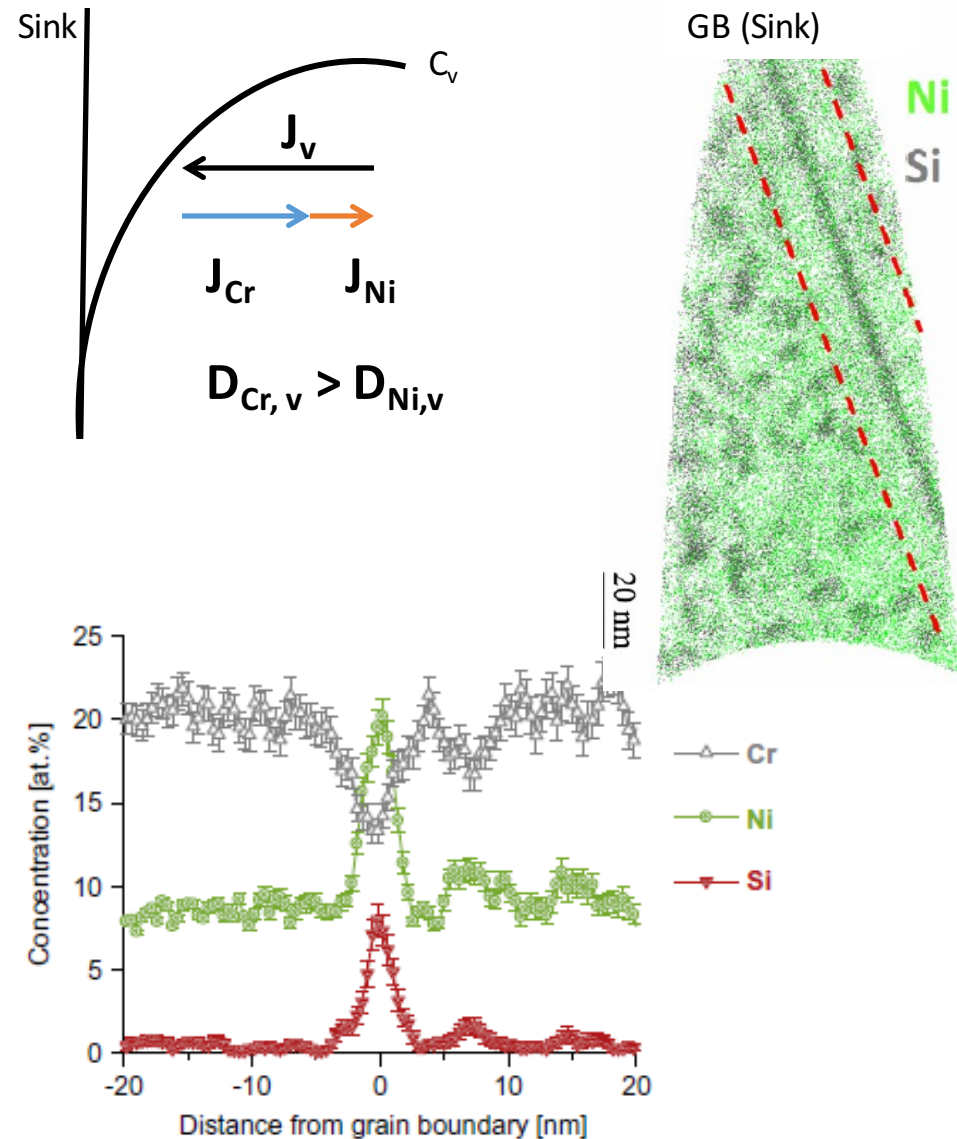


Radiation Induced segregation (RIS):

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- Non-equilibrium segregation of alloying elements caused by flux of irradiation induced defects
- Alloying elements segregate when a specific species is preferentially interacting with a defect flux
- **Vacancy-species preferential interaction**
 - **Vacancy-solute exchange mechanism**
- Interstitial-solute exchange mechanisms

Model Binary alloy with vacancy dominated RIS

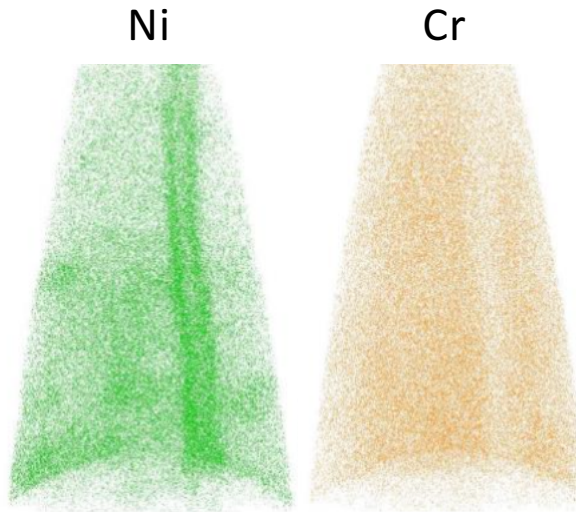


T. Toyama, et al., JNM, 2012 Jiao et al. Acta Mat. (2011)

Project Goals:

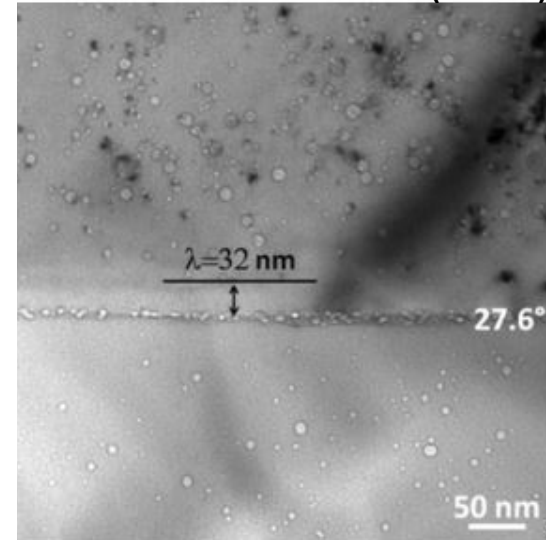
- 1) Design microstructure capable of obtaining particular improvement in irradiation response through GB character evolution
- 2) Provide predictive understanding of how particular GB structures respond under radiation induced segregation and void denuded zones.

Two Case Studies: Engineering Alloy 316 and Model Ni-Cr Alloy



Barr et al., submitted JNM (2016)

Void denuded zones (VDZs):



Han et al., Acta (2012)

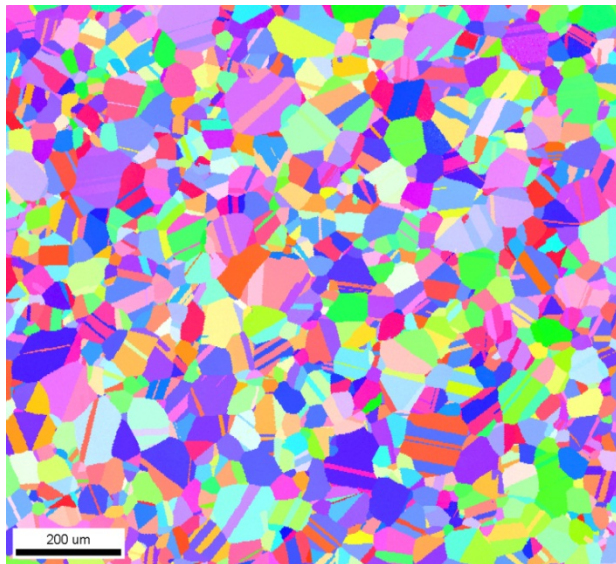
Grain Boundary Engineering (GBE) in 316L:

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- GBE structure → design of experiment with different strain, time, and temperature

Alloy	Fe	C	Mn	P	Si	Ni	Cr	Mo	Cu
wt. %	Bal	0.02	2.0	0.02	0.3	14.7	17.5	2.8	0.1

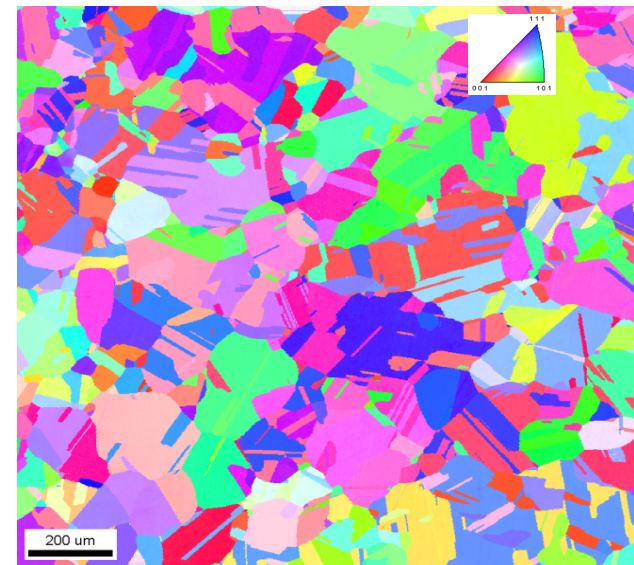
Solution Anneal:



GBE Processing



GBE: 5% RR-1000°C-60 minutes

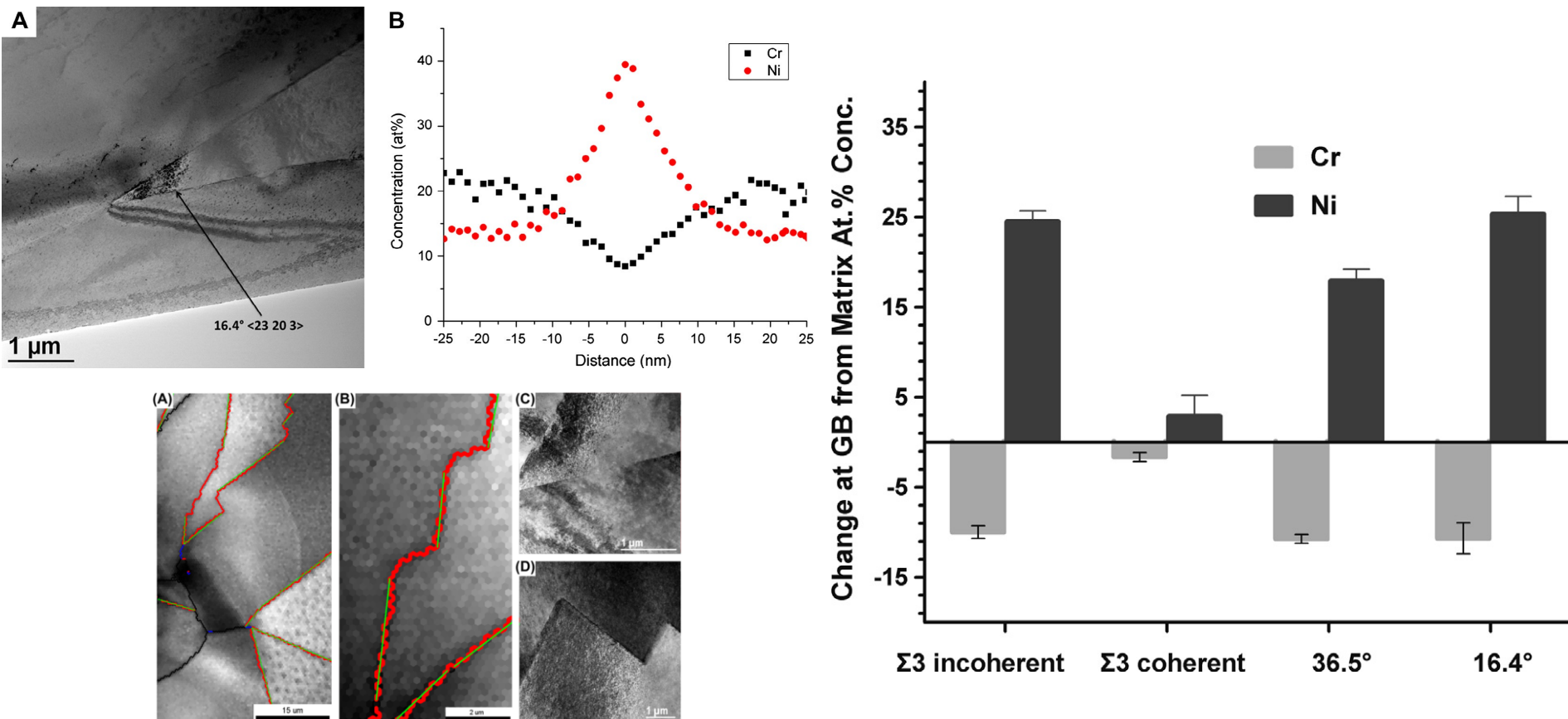


GB Population Statistics

	$\Sigma 3$	$\Sigma 9 + \Sigma 27_{a,b}$	$\Sigma 3n$	HV	Grain dia (μm)	TJD: $\Sigma 3c - \Sigma 3c - \Sigma 9$	TJD: $\Sigma 3c - R - R$	TJD: $\Sigma 3i - \Sigma 3c - \Sigma 9$
Sol Anneal	47	0.9	47.9	150	47	2.6	50.9	1.1
GBE	68.2	8.9	77	143	100	9.5	32.5	10.1

Triple Junction Distribution (TJD)

Grain Boundary Dependent RIS in 316L:

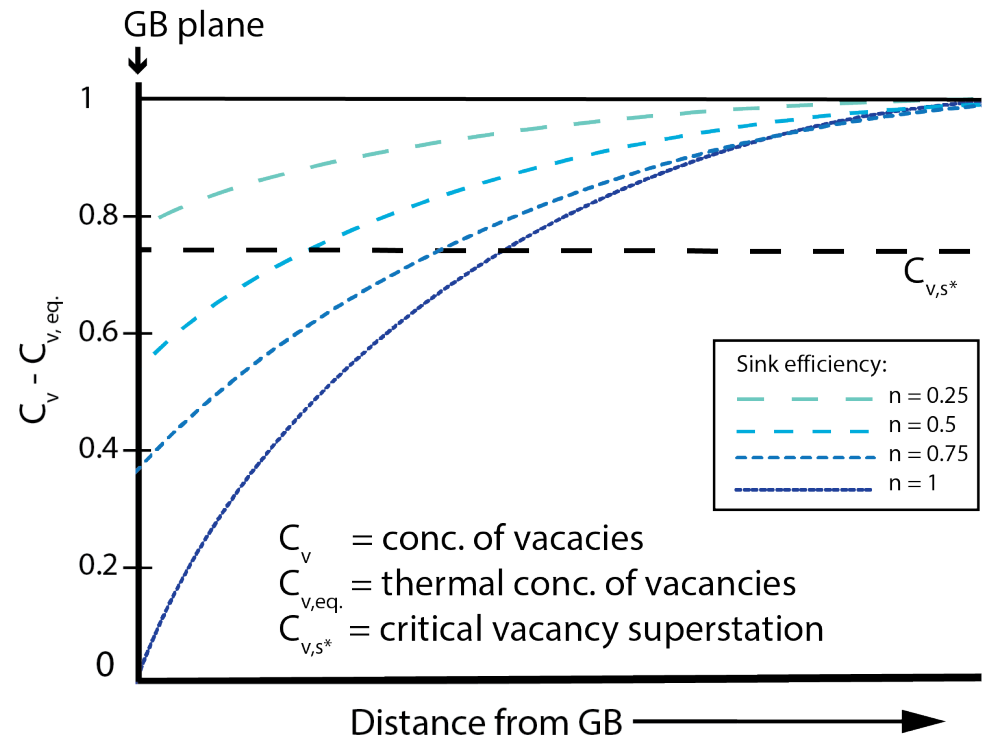


- 11 dpa, 1.6×10^{16} ions cm^{-2} , 3 MeV Cu^{2+} heavy ion irradiation, 500°C
- Strong dependence on grain boundary coherency
- Minimal Cr depletion variation observed between random HAGB types

Simple binary alloy provides more direct comparison to models

→ Correlated model-experiments provide ideal approach for predictive microstructural evolution under irradiation

- Variations in the radiation response should exist as function of GB character and subsequently have **different sink efficiency** dependent upon:
GB energy/free volume:
misorientation + inclination



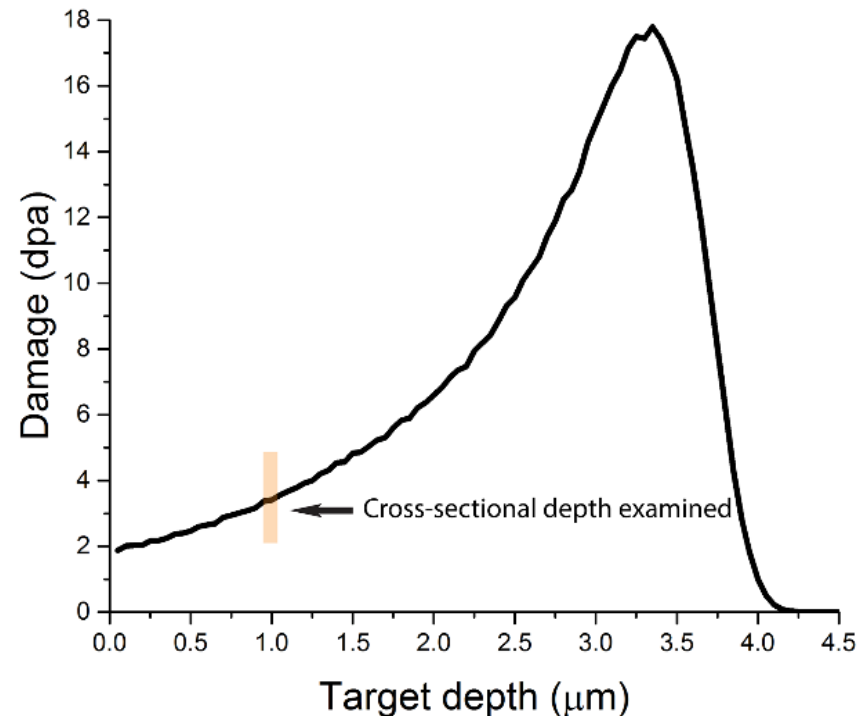
Experimental Methods – Ion Beam Irradiations:

- Thermomechanical processing used to induced wide range of available GBs
- 20 MeV Ni⁴⁺ at 500°C on bulk Ni-5Cr to 3.4 dpa at 1μm depth
- SRIM used to calculate dpa using Kinchin-Pease method with quick cascade based

Heater and sample for bulk irradiations:

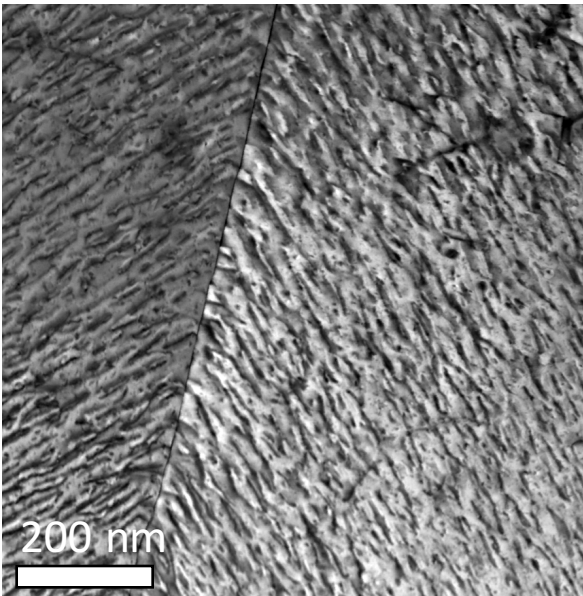


SRIM determined damage profile for sample cross-sectional

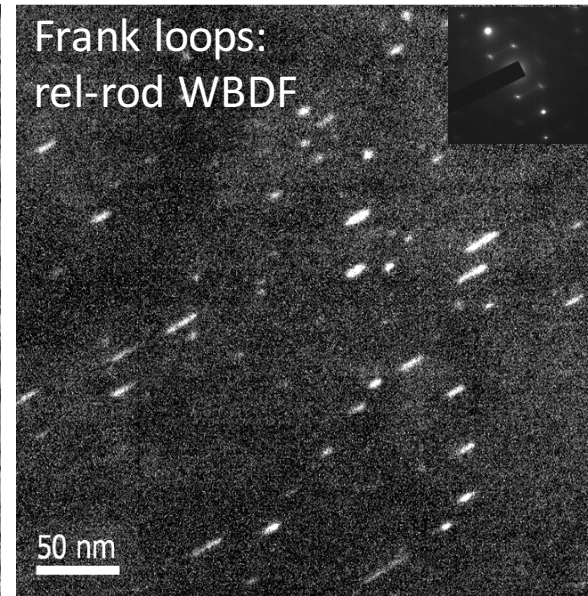


- 1.9×10^{16} ions/cm²
- 3.4 dpa at 1 μ m depth
- Avoided injected interstitial effects at examined cross-sectional depth

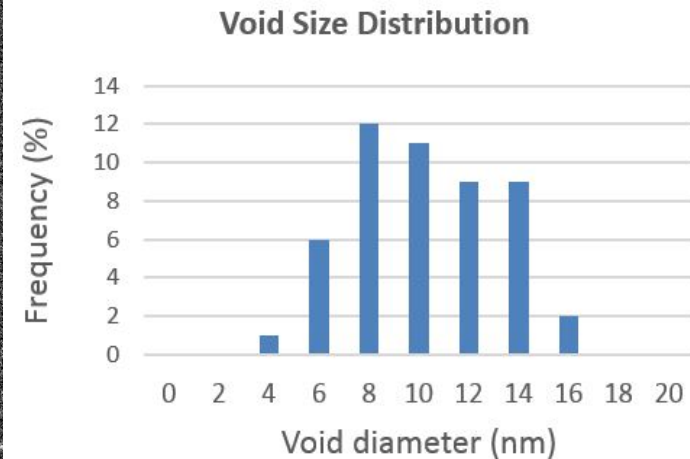
BF-STEM:

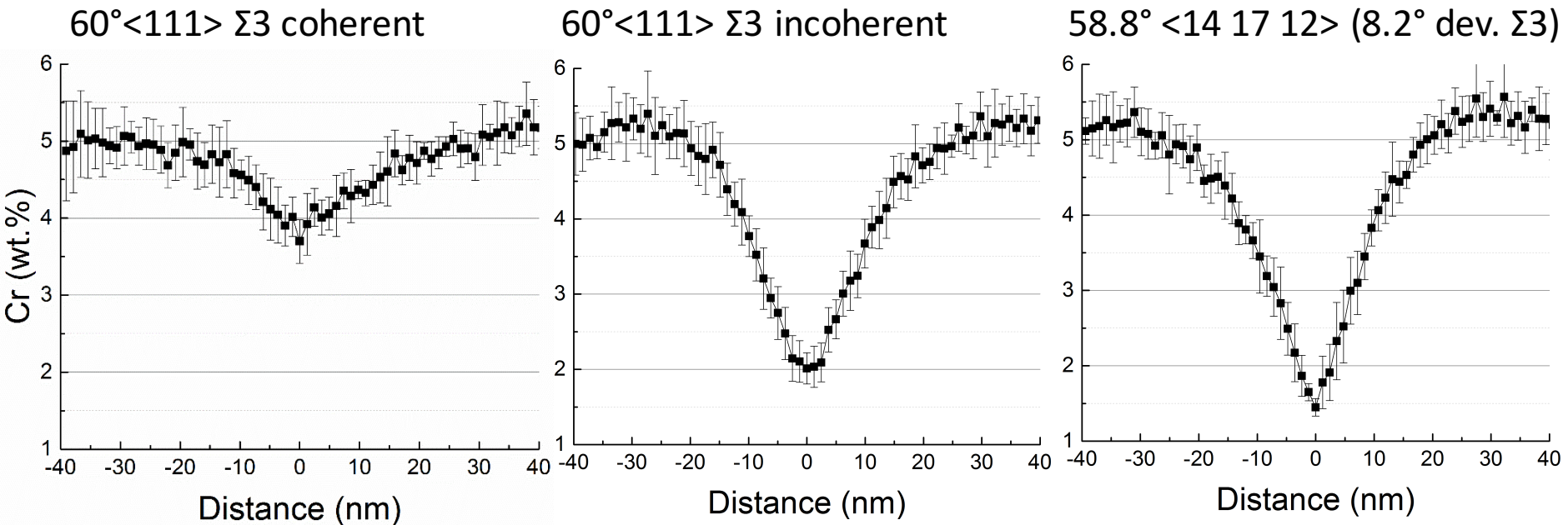


Defect density: $1.16 \times 10^{22} \text{ m}^{-3}$



Void density = $9.09 \times 10^{20} \text{ m}^{-3}$

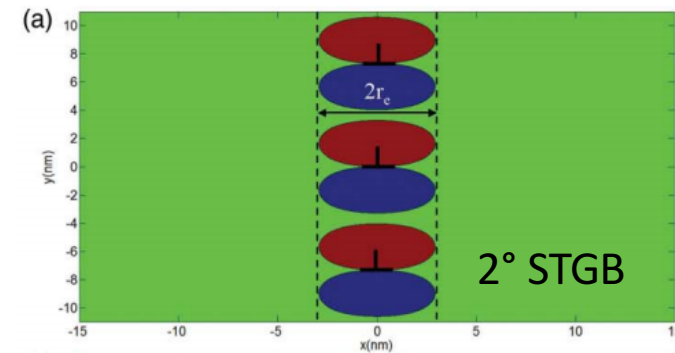
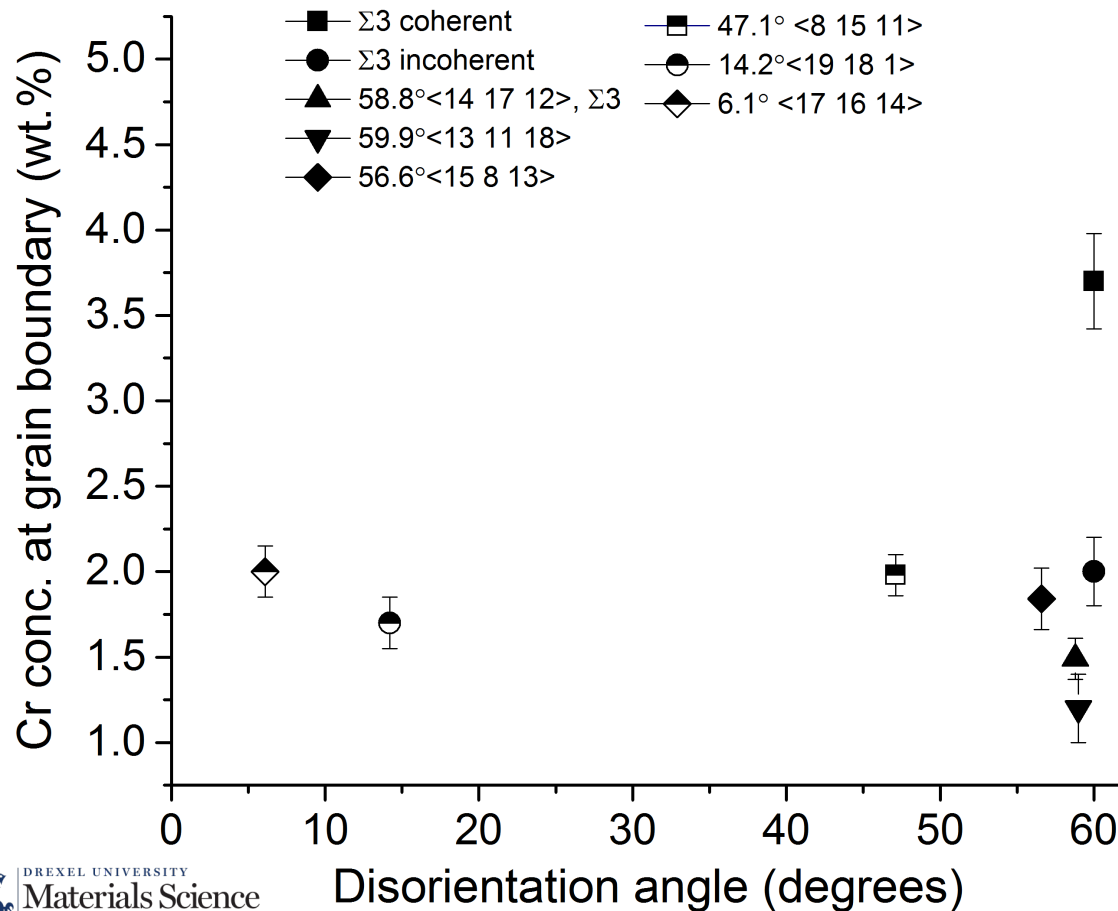




- Heavily anisotropic RIS within GBs considered “ $\Sigma 3$ ”
- Clear distinction and response between coherent and incoherent twins
- Sink efficiency low for coherent plane $\{111\}$ twin compared to incoherent plane $\{112\}$
- 58.8° heavily deviated $\Sigma 3$ behaves like random HAGB

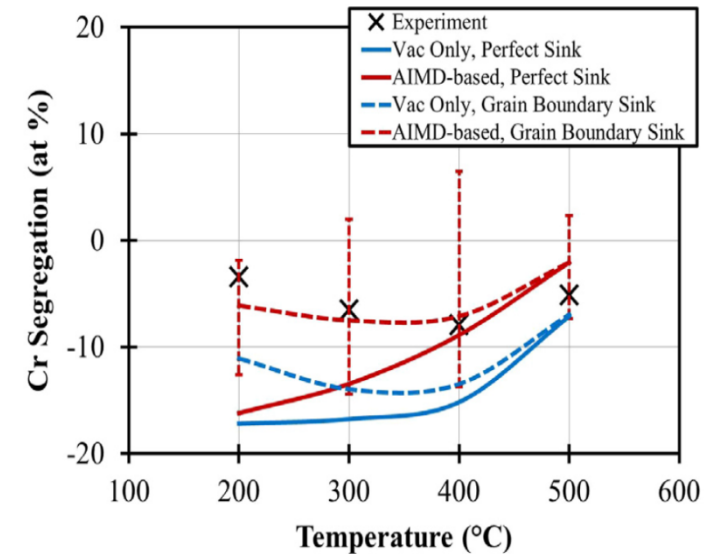
GB Character Irradiation – Low and High Angle GBs: 14

- No statistical difference between RIS response at high and low angle GBs
- RIS measured at a ~ 3.4 dpa in steady-state irradiation regime
- Possible reason for the absence of the expected reduction in sink efficiency for low GB angles are GB strain effects

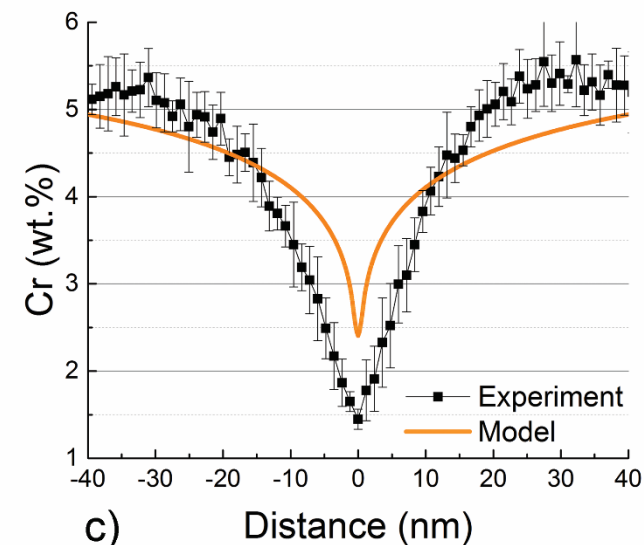
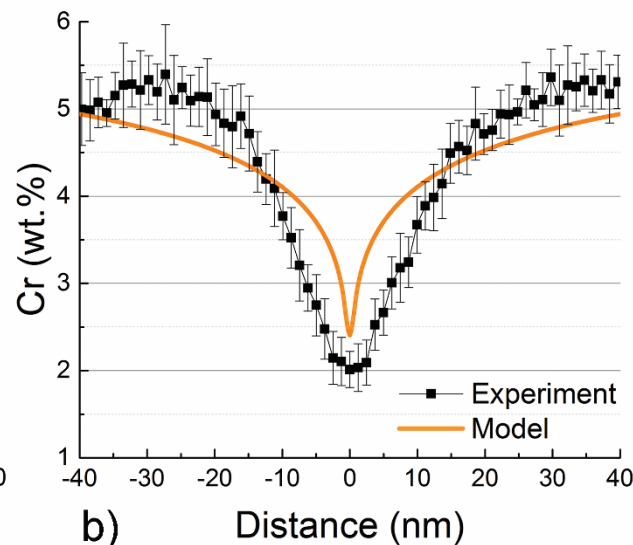
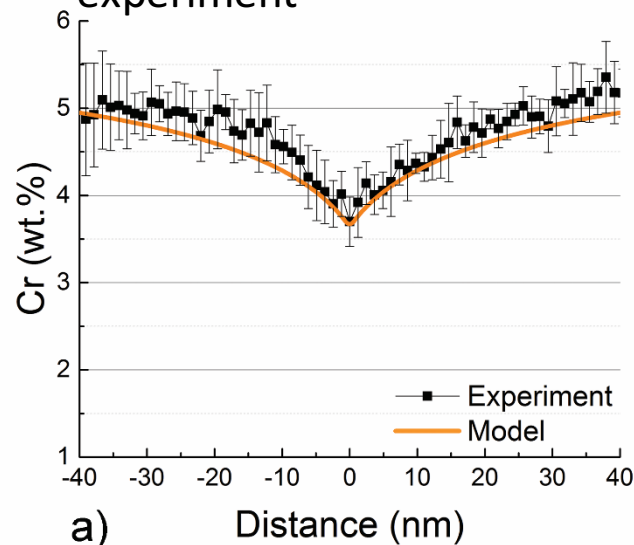


Jiang et al., MRL, 2, (2014)

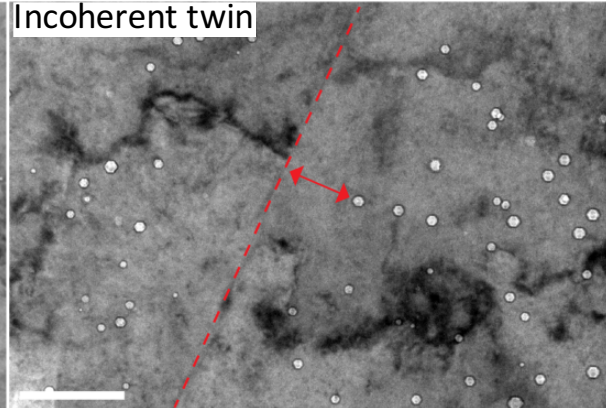
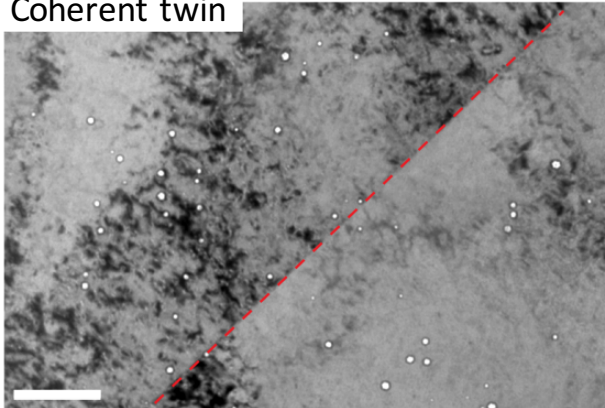
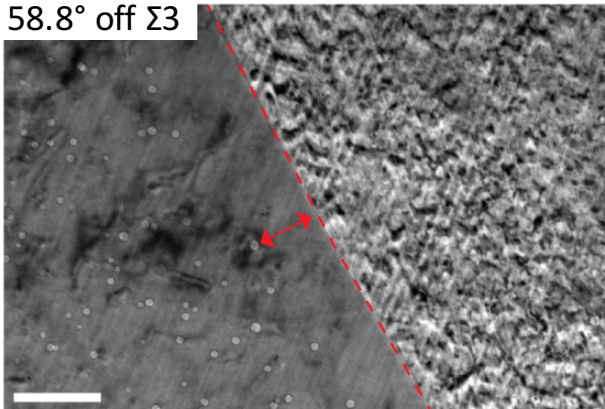
- Compared experimental RIS values to Wiedersich type rate theory model of RIS in Ni-Cr
- Modified to account differences in sink strength based on misorientation (and plane for $\Sigma 3$ system)
- Bias is greater for the vacancy mechanism, which result in Cr depletion by RIS
- Comparison yields good agreement in high angle regime and for the coherent twin
- Low angle GBs RIS is underestimated compared to experiment



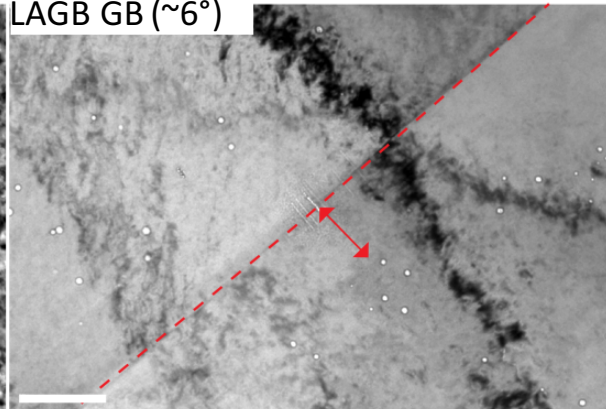
Barnard and Morgan, JNM 2014



Coherent twin


58.8° off $\Sigma 3$


LAGB GB (~6°)

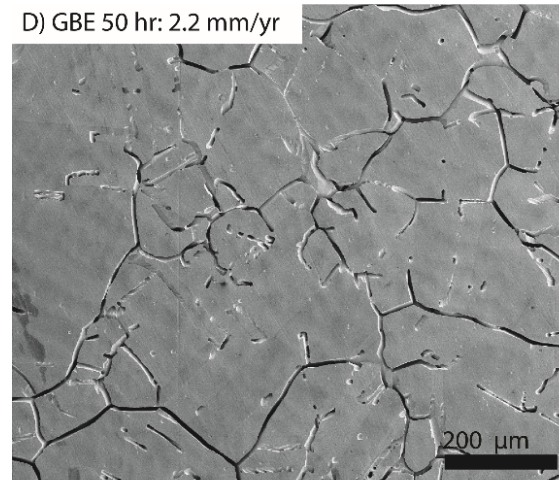
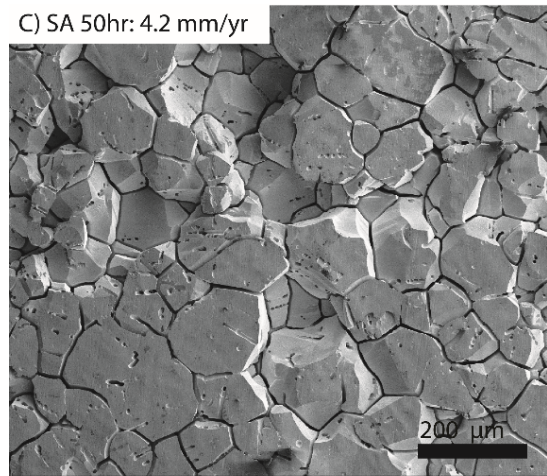


GB Character	VDZ Avg.
60° $\langle 111 \rangle \{111\} \Sigma 3$	0
60° $\langle 111 \rangle \{112\} \Sigma 3$	128
58.8° $\langle 14 \ 17 \ 12 \rangle$, $\Sigma 3$ Dev=8.2	115
59.0° $\langle 13 \ 11 \ 18 \rangle$	155
56.6° $\langle 15 \ 8 \ 13 \rangle$	145
47.1° $\langle 8 \ 15 \ 11 \rangle$	137
14.2° $\langle 19 \ 18 \ 1 \rangle$	135
6.1° $\langle 17 \ 16 \ 14 \rangle$	132

Scale bars = 200 nm

- Minimal different in low verse high angle VDZ behavior based on misorientation angle
- Indicates misorientation (only 3 of 5 DOF) insufficient to determine GB sink efficiency
- Observed asymmetry in VDZ in most GBs

- Effective light rolling followed by high temperature annealing induces formation of GBE microstructures consistent with large twin related domains in 316L
- RIS in 316 clearly indicate GB sink efficiency variations between coherent twin and incoherent twin while minimal difference in random HAGBs.
- GBE provides opportunity to increase $\Sigma 3$ coherent length fraction \rightarrow improved corrosion resistance and minimized Cr depletion during RIS



- No apparent sink efficiency difference between random high and low angle GBs
- Highly anisotropic sink efficiency in $\Sigma 3$ GB plane for RIS and VDZs. Agreement here in model-experimental approach.
- Sink efficiency increases with deviation from twin plane
- Breakdown in model-experiment at low angle GB – need for better estimate of solute-defect interactions in low angle GBs: GB energy insufficient boundary term for estimating RIS
- **Future Direction:**
 1. Broader GB characters including $\Sigma 11$ $\{113\}$ tilt versus asymmetric tilt; screw and edge components of low angle GBs for point defect accommodation.
 2. Determination of GB plane normal for random GBs

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Questions?

