

**For workshop on Corrosion of Nuclear Waste Containers
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**YUCCA MOUNTAIN PROJECT CONTAINER FABRICATION,
CLOSURE AND NON-DESTRUCTIVE EVALUATION DEVELOPMENT
ACTIVITIES***

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(Oral Presentation Summary)

In this presentation, I will describe our container fabrication, closure, and non-destructive evaluation (NDE) process development activities. All of these activities are interrelated, and will contribute to our metal barrier selection activity.

The key design parameters for a Tuff environment have been discussed already by Kass and will only be reviewed briefly here. The key points are:

- (i) There will be no significant hydrostatic or lithostatic loading of the container.
- (ii) The flux of water will be very small (~ 1 mm/yr).
- (iii) The water is benign. It is basically J-13 well water; i.e., an oxidizing, dilute sodium bicarbonate solution of neutral pH, containing 7 ppm Cl^- and 10 ppm NO_3^- .
- (iv) The temperature of the borehole wall will attain levels of ~ 250°C over the first 50 to 100 years and then fall to

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about 97°C over the remainder of the 300 year containment period.

Our plan is to use a corrosion-resistant material in the form of a cylinder with a wall thickness of ~ 1 cm (2 cm for pure copper). The materials under consideration have been discussed by Kass, and include the three austenitic alloys: AISI 304L, AISI 316L and alloy 825, as well as the three copper alloys: CDA 102, CDA 613, and CDA 715. It is likely that the container closure method will be welding. Our targets are:

- (a) Controlled, uniform microstructures for the base metal, the weld, and the heat affected zones (HAZ) of the welds;
- (b) Controlled microchemistry;
- (c) Low-residual stresses;
- (d) Small welds and heat-affected zones;
- (e) Reliable methods of flaw detection by both surface and volumetric techniques.

Figure 1 gives an overview of our container process development activities. The first two activities, container fabrication and container closure, are being done by Babcock and Wilcox in Alliance, Ohio, and in Lynchburg, Virginia. The container closure nondestructive evaluations are being developed at Lawrence Livermore National Laboratory. Phase 1 of these activities is essentially complete, and we now have preliminary recommendations which we will pursue in the subsequent phases. Phase 2 will commence in FY89 (fiscal year). During this phase we intend to construct a number of small specimens in the form of rings (container fabrication) and to look at a number of welded specimens, probably in the form of plates as well as rings, (container closure). For the third activity (non-destructive evaluation), we will look at these specimens using ultrasonic and dye-penetration techniques. In particular, we will look at areas where problems may arise, such as welded areas, and areas

where we expect some deformation. In Phase 3, which should start sometime in FY90, we will produce reports which are a set of specifications of the three activities, fabrication, closure and non-destructive evaluation. Then we will construct several prototype containers (fabrication), and demonstrate that we can weld them using the welding technique specified (closure). Finally we will have to prove that we have succeeded in our fabrication and closure efforts using the specified evaluation techniques.

Now that Phase 1 is complete, I would like to review the recommended procedures and processes for fabricating, closing and evaluating each of our candidate materials. First I will list the procedures to be studied or evaluated and then I will discuss the specific procedures in a little more detail.

A. 304L AND 316L STAINLESS STEEL

(a) Fabrication

Three different fabrication processes will be evaluated. The first process is the closed-end extrusion process followed by cold-working. The second, and probably cheapest process is to roll and weld. This is a very common fabrication method. Subsequent thermo-mechanical processing to homogenize the microstructure throughout the weld and HAZ will be investigated. Finally, we will investigate the technique of centrifugal casting also with subsequent thermo-mechanical processing. All three processes would end with a final anneal to further homogenize the microstructure and reduce the residual stresses.

(b) Closure

Three processes have been recommended. These are:

- plasma-arc welding, which is a high density arc welding process;
- electron-beam welding
- friction welding.

(c) Inspection

An ultrasonic technique will be used for volumetric inspection and the dye penetrant technique for surface inspections. If we end up with coarse-grain welds, then special techniques will need to be developed.

B. ALLOY 825

As far as fabrication is concerned we will employ essentially the same fabrication procedures as for the two stainless steels. However, since we anticipate a problem with titanium stabilization, we will not pursue the centrifugal casting technique with this alloy. Instead we will construct an extruded, welded and cold-worked unit. The three methods of container closure and the two methods of container inspection described above for 304L/316L steels will also be employed with alloy 825.

**C. COPPER (CDA 102), COPPER-NICKEL (CDA 715),
ALUMINIUM BRONZE (CDA 613)**

With the exception of friction welding, which is a doubtful process with pure copper (CDA 102), the same fabrication, closure and inspection techniques described above will be employed. The centrifugal casting process will be evaluated for the 70/30 copper nickel and the aluminium bronze but not for the pure copper (CDA 102). Problems are anticipated in the fusion welding of the aluminium bronze since it is known to be prone to cracking and phase separation.

D. CLOSED-END EXTRUSION PROCESS

The closed-end extrusion process is illustrated in Figure 2. This is a simplified series of steps but sufficient to illustrate the process. We start with a forged billet, square it off and place it into a pot, which acts as an external guide. Then we squeeze the billet down, pierce it with a ram, and push it through the guide. The container is extruded in the required form. The benefits of this process include the forged microstructure and the absence of both a long seam weld and a lower head weld. The welds are homogeneous which means they

should be less susceptible to localized corrosion which can often initiate at inhomogeneties.

E. CENTRIFUGAL CASTING PROCESS

Figure 3 is an illustration of a centrifugal casting machine, which is simply a rotated mold. It requires an axisymmetrical shape and a pouring basin to add the molten material. This process is low cost compared to the closed-end extrusion method and commercially available. The material should possess a dense clean microstructure and the container would have a low ovality and no long-seam weld.

The cold-working process to be investigated to break-up the dendritic columnar weld structure and the radial columnar structure anticipated with centrifugal casting is illustrated in Figure 4. This process, which involves an external roll extrusion using two rollers and two rings on bearings, would be followed by several heat treatment steps as required. The cylinder would rotate with an internal mandrel and the external rollers push down on the walls of the cylinder making them a little thinner. The advantages of such therma-mechanical working are mainly microstructural. The material would possess a random grain orientation with a uniform grain size, and the welds would undergo recrystallization. The cylinder would also possess improved tolerances. This thermo-mechanical process could be applied to containers performed by any of the methods described above.

F. PLASMA ARC WELDING (PAW)

Figure 5 shows a conceptual design, for the plasma arc welding process, supplied by B & W (Babcock and Wilcox). The method is derived from the gas tungsten arc welding (GTA) process, the main difference being that it is a high-energy plasma process with currents possibly greater than 100 amps. The process is highly directional and can penetrate to significant depths. It has many advantages including:

- Low-to medium-heat input. We may forego these advantages in order to achieve the deep penetration

and high productivity possible with the high-energy beam.

- The equipment is versatile, allowing both arc and keyhole welding. In keyhole welding you penetrate through the weldment. You attain equilibrium between the plasma and the weld puddle. This enables you to produce a weld much faster than you could with the GTA process.

- No filler is necessary with keyhole welding.
- Repair welding can be done with the same process.
- The equipment is relatively low cost.

Figure 5 shows the PAW arrangement within the hot cell with the waste emplaced. The container is shown standing vertically, though it could be placed horizontally if desired. The centering device is required to maintain the torch-to-work distance. The plasma torch must be inside the hot cell. Also shown is the overhead unit to hoist the containers, and the transfer cart. Located outside the hot cell would be the power supply, control console, cooling system, and shielding gas.

G. ELECTRON BEAM WELDING (EBW)

Figure 6 shows the B & W conceptual design for the electron beam welding process. This process is probably more familiar to you. One disadvantage that we have with our welding procedure is that we intend to fill the containers with argon. The electron beam welding process can accommodate this, but you do not get the narrow beam and small heat-affected zones (HAZ) that would be achieved by welding in a vacuum. The major benefits of the electron beam welding process include:

- Small HAZ and fusion zone;
- Relatively low residual stresses and distortion;
- Welds are easy to inspect;

- It is a fast welding process;
- Welds can be repaired without machining;
- No filler metal is required.

Inside the hot cell the container would be placed within a chamber and rotated while the electron gun and T.V. camera remain stationary. To achieve welding with the normal atmospheric pressures required with argon present, a specially modified electron gun will have to be used.

H. FRICTION WELDING (FRW)

The friction welding process, which is a solid state joining process that produces coalescence using the heat developed between surfaces—one surface stationary, while the other rotates, has the following metallurgical benefits: small HAZ, small fusion zone with no melting, minimum risk for second phases, and low residual stress. This method is illustrated in Figure 7. The major process benefits of this method include its simplicity and ruggedness, and the fact that the parameters are easily controlled. A motor and flywheel are located above the hot cell, and are coupled to the top-head. The flywheel is rotated and the top-head is brought into contact with the container body using a thrust plate for upset force. To avoid torque generated during welding you need a centering and blocking system as shown for the container body, which must be held stationary. The benefits of this process include:

- Small HAZ and fusion zone (without melting);
- Low residual stresses and distortions;
- Easy to inspect;
- Maintenance inside the hot cell is easy, and infrequently required;
- There are very few welding variables to monitor;
- Welding is rapid.

I. NON-DESTRUCTIVE EVALUATION

A conceptual design for a non-destructive evaluation system is shown in Figure 8. This system would be inside the hot cell. It is equipped with a turntable fitted

with two arms; one for the dye penetrant system, the other for the transducer array. A benefit of this system is the simple mechanical arrangement with an optimized coupling, although the coupling remains to be demonstrated. This coupling may present a problem since we want to avoid significant amounts of water within the hot cell. There are other benefits to this system including:

- We expect to detect anticipated flaws of between 1% and 10% of the wall thickness.
- Flexibility of inspection of a selected joining process.
- The possibility of combining this evaluation system with our closure system in order to minimize transport of the container. This could be achieved by having a plasma arc torch on the same turntable.

At Livermore, during Phase 2 of our program, we intend to utilize the UTB (ultrasonics test bed) facility. This is a state-of-the-art robotics system, with 14 axis, multitransducer capability. By using this system we hope to demonstrate its capabilities for our requirements before having to specify the final design of our remote hot cell facility.

In summary, in the completed phase one of our program, we have screened a number of candidate processes for fabricating, closing and final inspecting the containers. We have chosen three fabrication, and three closure methods for further evaluation in Phase 2. For inspection purposes we will use ultrasonic and dye-penetrant techniques. In Phase 3 a specific fabrication/closure process will be chosen for an advanced conceptual design. On the basis of these studies and our corrosion evaluation by the Metal Barrier Task, we will choose the most appropriate container alloy.

CROSTHWAITE: Why do you intend to backfill your container with argon?

RUSSELL: We would like to consider the zirconium fuel cladding as a barrier and the argon will add corrosion protection. Also,

our temperatures are high, and we wish to avoid oxidizing the cladding.

CROSTHWAITE: If you have to backfill, why don't you use helium instead of argon, so that you can simultaneously perform a helium leak test?

RUSSELL: Since argon is a heavier atom it is a little easier to back-fill with.

KASS: Argon is cheaper than helium. However, we have not chosen a particular inert gas. Helium could be used.

CROSTHWAITE: In your discussion of non-destructive evaluation methods you only discussed weld inspection. Do you intend to do a leak test?

KASS: We are not planning to do such a test, but if required to, we will.

INTERRANTE: Backfilling to a fraction of an atmosphere with a heavy gas like argon may be sufficient for your purposes.

RUSSELL: That is a distinct possibility.

INTERRANTE: Do you really need to backflush with argon? Won't you have sufficient corrosion protection for the cladding etc., simply by excluding oxygen during welding? After all, you then seal the container without further ingress of oxygen.

KASS: We have not fully analyzed the situation. However, since we will be getting a wide variety of fuel to dispose of, some of it could be wet. A combination of wet fuel and a partial pressure of oxygen would attack the fuel. Also water radiolysis inside the cladding could produce oxidizing

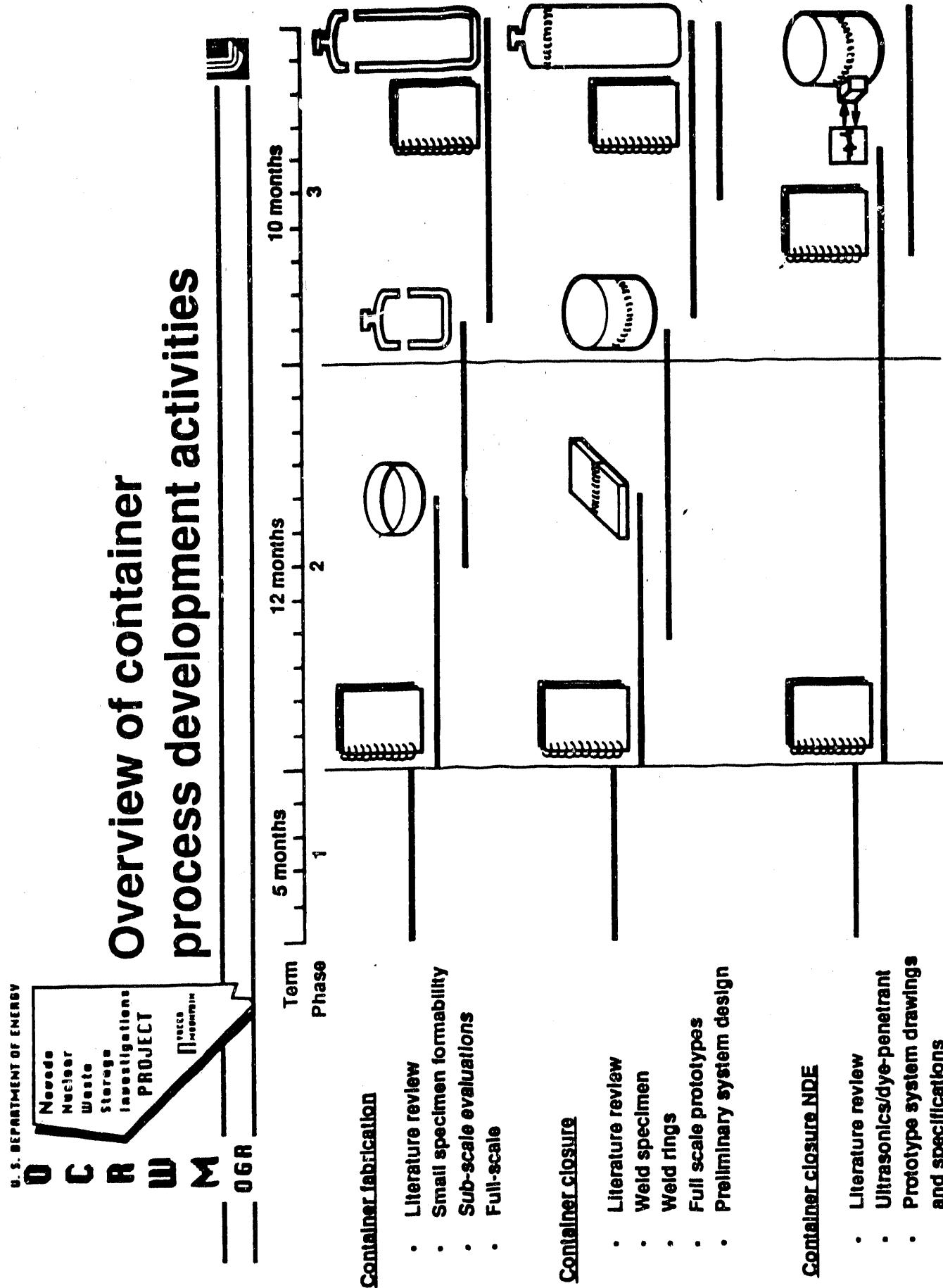
conditions. We need to analyze the situation before we decide whether a partial atmosphere of argon is sufficient.

CROSTHWAITE: Why do you have to take credit for the zirconium cladding?

KASS: In our overall performance assessment we have included a term to take credit for the cladding in our code. We don't need to invoke the cladding as a barrier in order to meet our requirement of 300 years of containment. However, I see no reason not to take credit for it.

STAHL: In our assessment we assume that some of our containers will be faulty but will succeed in passing our inspection. Consequently, we assume that ~ 5% of our containers will fail in the first 300 years. Hence, we take credit for the cladding in order to prevent release of the fission products still present after such a time period.

Figure 1



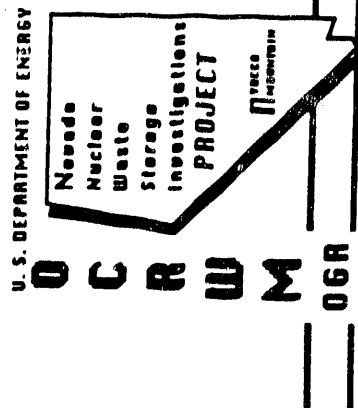
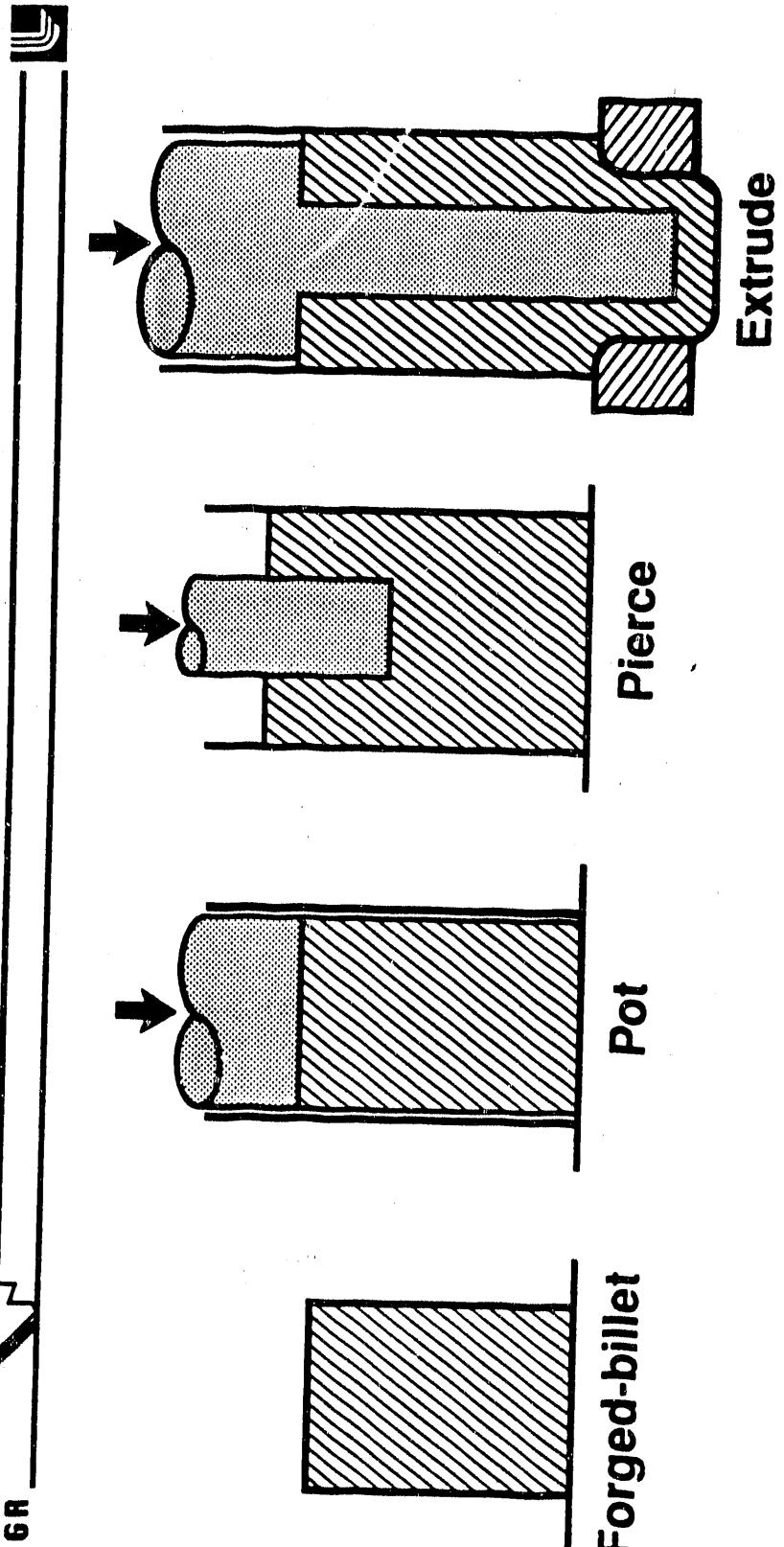


Figure 2

Illustration of closed-end extrusion process



Process benefits

- Forged microstructure
- No long seam weld
- No lower head weld

Figure 3

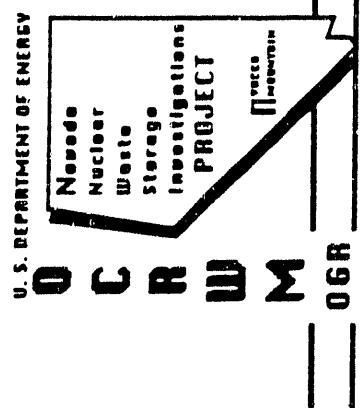
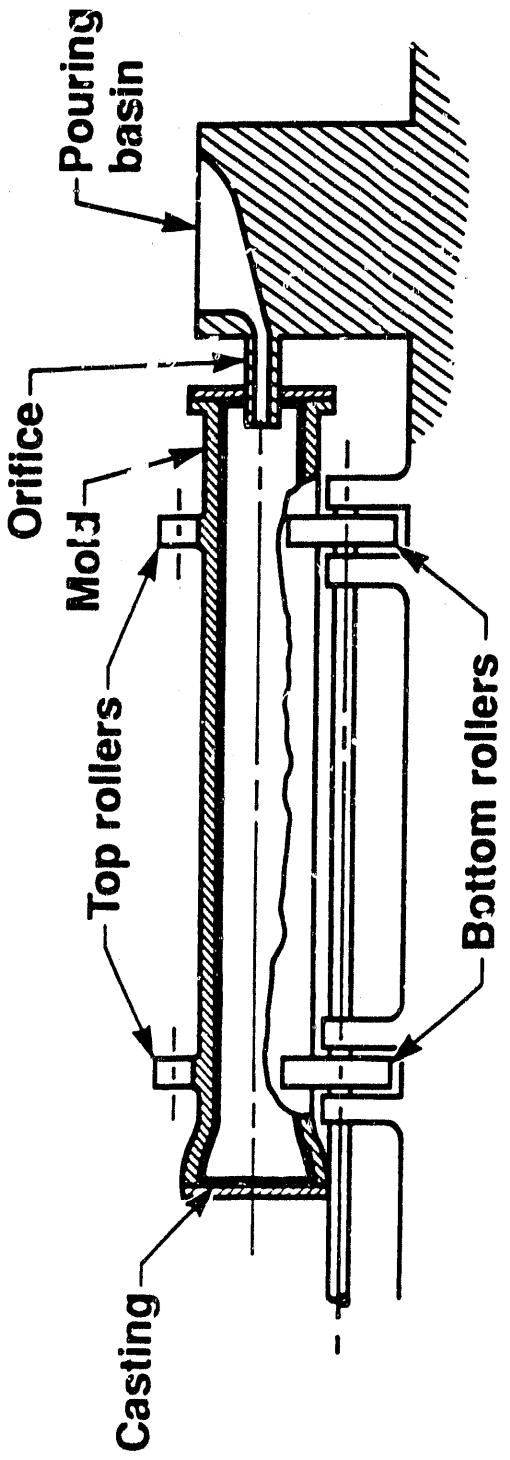


Illustration of centrifugal casting machine



Process benefits

- Commercial process
- Low cost
- No long seam weld
- Low ovality
- Dense, clean microstructure

Figure 4

U. S. DEPARTMENT OF ENERGY

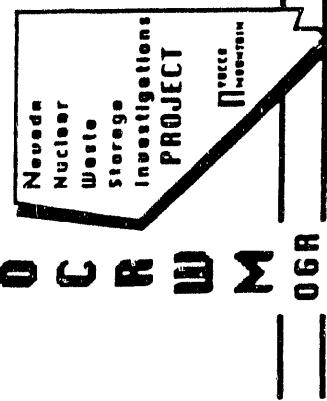
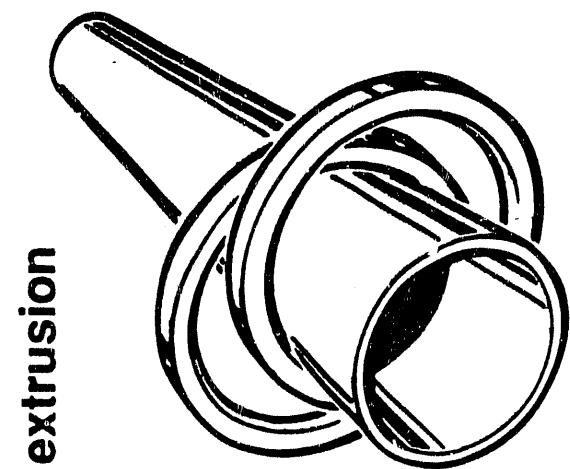
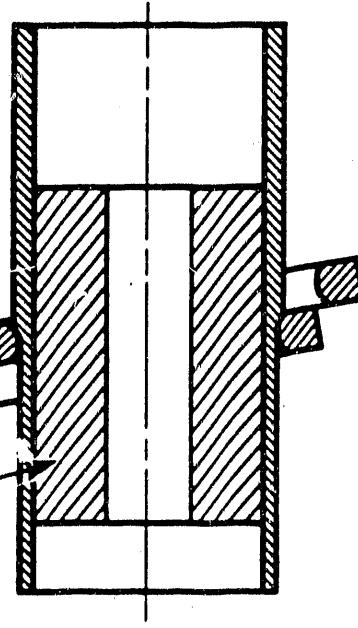


Illustration of process for cold working cylinders

External roll extrusion



External ring rollers
Internal mandrel



Process benefits

Microstructure

- Uniform grain size
- Random grain orientation
- Recrystallized weld for roll and welded

Improved tolerances

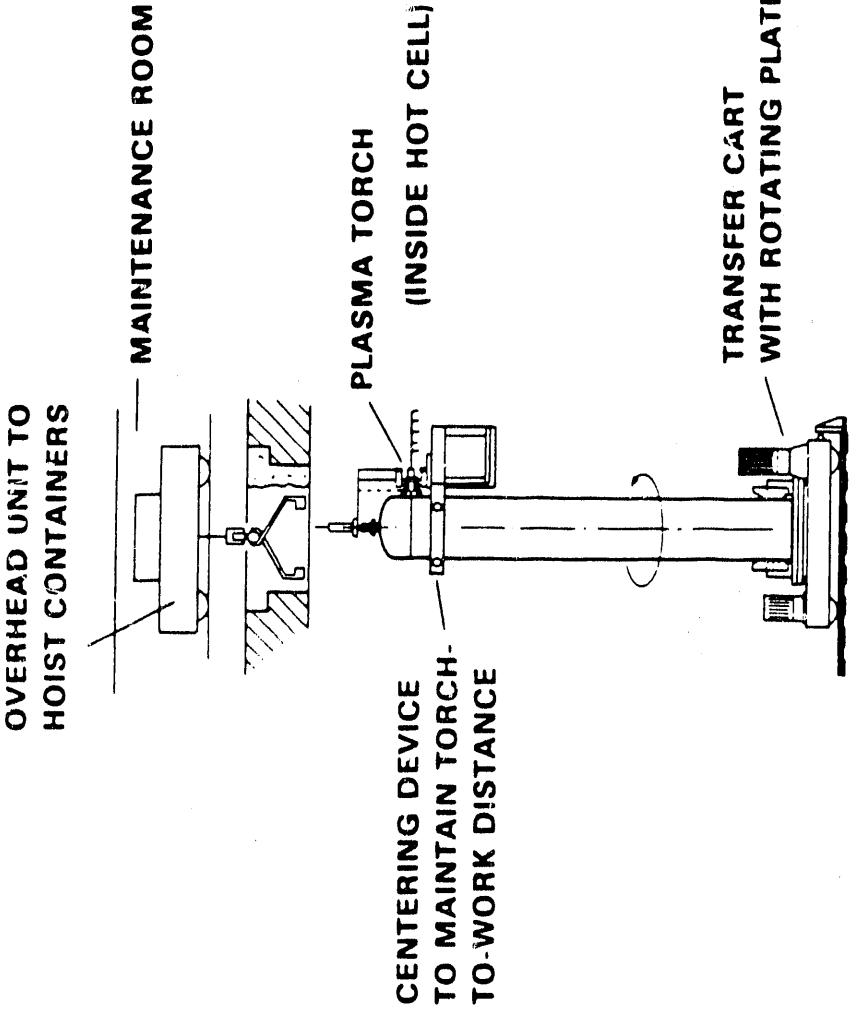
Container preform

Extruded or
Roll and welded or
Centrifugal cast

Plasma Arc Welding

PROCESS BENEFITS

- LOW TO MEDIUM HEAT INPUT
- VERSATILE EQUIPMENT
 - ARC WELDING
 - KEYHOLE WELDING
- NO FILLER WITH KEYHOLE WELDING
- REPAIR WELDING WITH SAME PROCESS
- RELATIVELY LOW COST EQUIPMENT
- PREVIOUS CLOSURE APPLICATION



OVERHEAD UNIT TO HOIST CONTAINERS

MAINTENANCE ROOM

PLASMA TORCH (INSIDE HOT CELL)

CENTERING DEVICE TO MAINTAIN TORCH TO WORK DISTANCE

TRANSFER CART WITH ROTATING PLATE

LOCATED OUTSIDE OF THE HOT CELL

- POWER SUPPLY
- CONTROL CONSOLE
- COOLING SYSTEM
- SHEILDING GAS

Figure 5

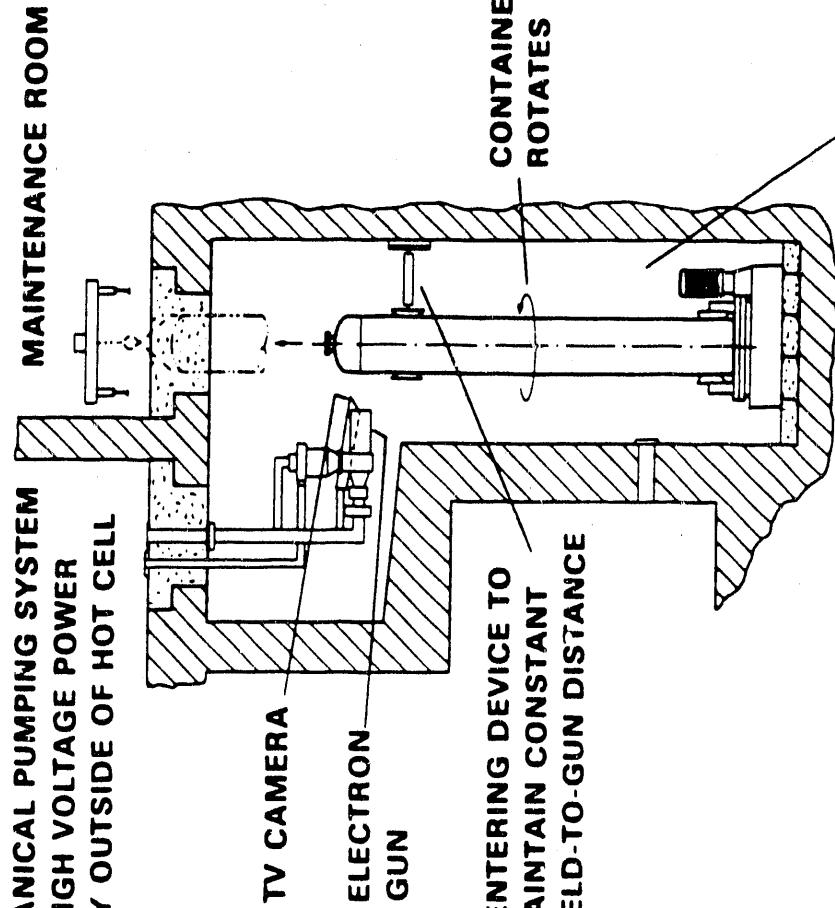
Figure 6

Electron Beam Welding

PROCESS BENEFITS

- RELATIVELY SMALL HAZ AND FUSION ZONE
- RELATIVELY LOW RESIDUAL STRESS AND DISTORTION
- GOOD INSPECTABILITY
- FAST WELD SPEED
- POSSIBILITY OF REPAIR WELDING WITHOUT MACHINING
- NO FILLER METAL

MECHANICAL PUMPING SYSTEM
AND HIGH VOLTAGE POWER
SUPPLY OUTSIDE OF HOT CELL



ELECTRON BEAM WELDING AT NORMAL
ATMOSPHERIC PRESSURE CAN BE ACCOMMODATED
USING SPECIAL ELECTRON GUN MODIFICATIONS

Friction Welding

PROCESS BENEFITS

- SMALL HAZ AND FUSION ZONE
- LOW RESIDUAL STRESS AND DISTORTION
- GOOD INSPECTABILITY
- EASY AND INFREQUENT IN-CELL MAINTENANCE
- FEW WELDING VARIABLES TO MONITOR
- FAST WELD SPEED

NOTE: ONLY THE ROTATING SHAFT PENETRATES THE HOT CELL

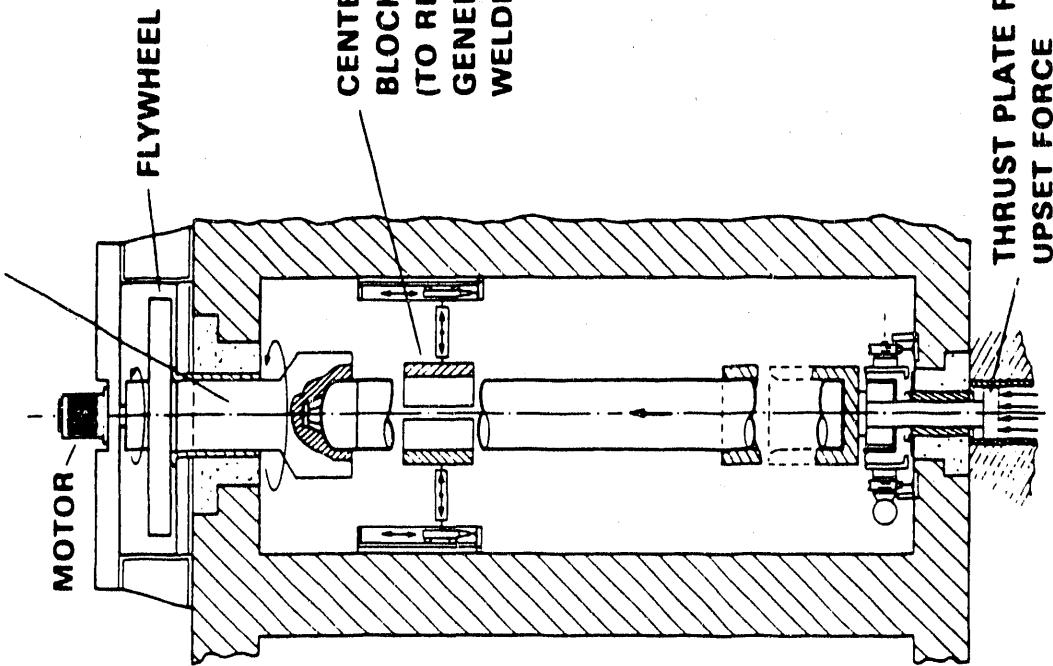
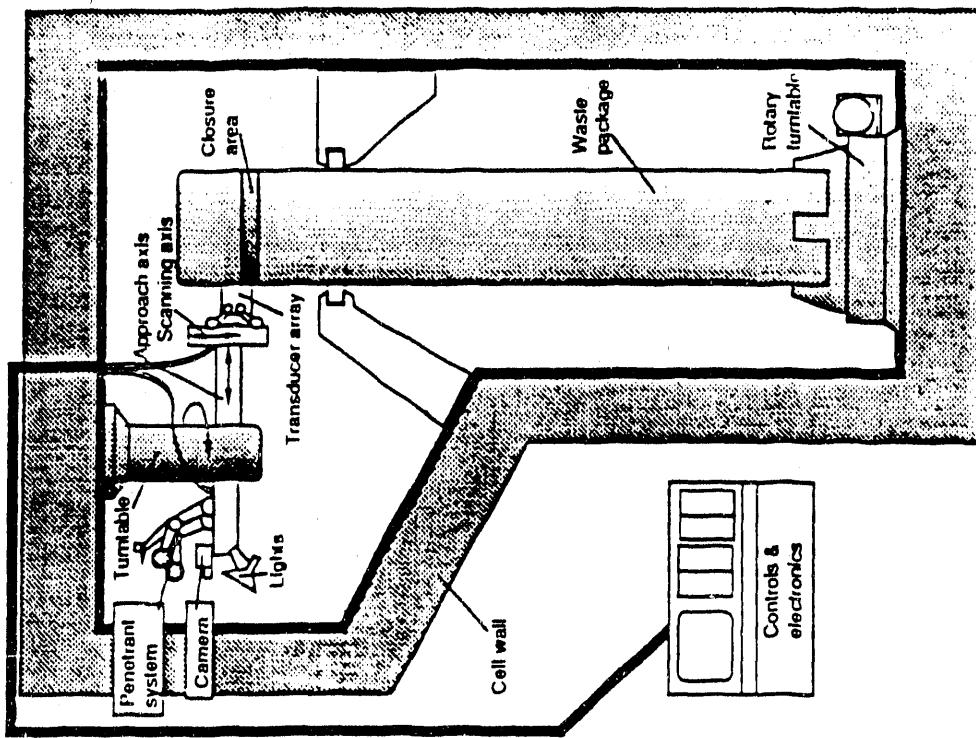


Figure 7

Conceptual Design of Container Closure NDE System



Process Benefits

- Simple mechanical system with optimized coupling.
- Can meet anticipated NNWSI inspection requirements.
- Flexibility allows inspection of selected joining processes.
- Can be combined with closure process system so that transport of the container is minimized.

END

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