

*Update Report on Fracture Flow in
Saturated Tuff: Dynamic Transport Task
for the Nevada Nuclear Waste Investigations*

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Update Report on Fracture Flow in Saturated Tuff:
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by

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ABSTRACT

This report summarizes the results of continuing experiments on the behavior of tracers during fracture flow in saturated, welded tuff. These experiments were completed during the past year as part of the Dynamic Transport Task of geochemical investigations for the Yucca Mountain Project sponsored by the US Department of Energy. These experiments are designed to investigate the effects of fluid movement in fractures when coupled with matrix diffusion and sorption but isolated from the effects of capillary suction and two-phase flow characteristic of unsaturated conditions. The experiments reported here are continuations of experimental efforts reported previously.

The behavior of three tracers [HTO (tritiated water), TcO_4^- (pertechnetate), and sulforhodamine B dye] have been investigated during flow through a saturated column of densely welded tuff from the Topopah Spring Member of the Paintbrush Tuff, Yucca Mountain, Nye County, southern Nevada. This rock column is cut by a natural fracture network similar to networks characterized elsewhere in these tuffs. Experimental problems in HTO experiments make interpretation difficult. However, it appears that breakthrough occurs rapidly, consistent with the other tracer behavior. Recoveries for HTO are between 60 and 70%. The other tracers exhibit higher recoveries than HTO. This is interpreted as a function of size exclusion of molecular species from an increasing proportion of the matrix pores for pertechnetate and sulforhodamine B dye. Pertechnetate may also be affected by anion exclusion and sorption, but these effects have not yet been quantified. Modeling the experiments by using a formulation for a single, parallel-sided fracture in a porous rock matrix and appropriate values for adjustable parameters produces consistent elution curves and aids in interpreting HTO experimental data.

I. INTRODUCTION

The Yucca Mountain Project (YMP) of the US Department of Energy is studying the suitability of the Yucca Mountain area, Nye County, southern Nevada, as a potential geological repository for high-level nuclear waste. The mountain is composed of numerous strata of ash-flow and ash-fall tuffs, with a stratigraphic thickness exceeding 3000 m in Yucca Mountain and Crater Flat (Snyder and Carr, 1982). The proposed repository location is in densely welded, devitrified tuff of the Topopah Springs Member of the Paintbrush Tuff.

The Yucca Mountain site has unique features with respect to evaluating hydrologic transport and isolation of waste radionuclides. The proposed repository horizon is above the water table, and the matrix of the surrounding host rock has significant porosity (Peters *et al.*, 1984). Abundant secondary minerals, such as the zeolites clinoptilolite, heulandite, and mordenite as well as smectite clays and calcite, are found in the rock matrix and lining fractures of rocks beneath and hydrologically down-gradient of the potential repository horizon (Vaniman *et al.*, 1984). These minerals have significant capabilities to sorb dissolved species from solution, including waste radionuclides (Rundberg, 1984; Thomas, 1985). The unsaturated matrix with high porosity will tend to draw water and dissolved radionuclides from the fractures into the pore space of the surrounding tuff (Travis *et al.*, 1984), thus providing favorable conditions for limiting transport by impeding flow and by increasing access to sorbing minerals (Neretnicks, 1980).

The abundance of fractures in the tuffs of Yucca Mountain has been documented in the reports of the US Geological Survey (USGS) (Montazer and Wilson, 1984; Spengler and Chornack, 1984; Bentley, 1984; Craig *et al.*, 1983; *Geohydrologic*, 1983; Thordarson, 1983). In addition, large faults are known to cut the section, intersecting welded and bedded tuff strata in both unsaturated and saturated zones (Scott and Bonk, 1984). Hydrologic tests have found the more permeable zones are in the welded tuff strata, presumably as a result of abundant cooling joints in the welded tuff zones (Winnograd and Thordarson, 1975). Zones below the present water table have significant components of both fracture and matrix permeability (Scott *et al.*, 1983). The potential repository horizon is above the water table at present, and the arid climate of southern Nevada will probably lessen the likelihood of situations that would result in saturated conditions in the repository zone. However, in assessing the overall performance of a repository, the consequences of future geologic events that lead to saturation of the fractures and surrounding rocks must be considered. In addition, the presence of alteration minerals in faults and fractures, such as zeolites, clays, and carbonates, suggests that there has been water in the fractures at some time (Arney-Carlos, 1985). These complexities require that the effects of fracture flow on aqueous transport of radionuclides be thoroughly investigated.

Modeling the hydrology and transport of contaminants in materials with significant fracture permeability is difficult for several reasons: (1) the hydrologic properties of the media become heterogeneous and anisotropic, and (2) the distribution of component phases of rocks, which have varying sorptive or reactive

characteristics, becomes heterogeneous relative to flow pathways. Thus, standard simplifying assumptions about homogeneous porous flow are not valid, and relationships between chemical measures, such as sorption ratio and breakthrough or retention volumes for radionuclides, are not simple. Thus, modeling requires development and validation of three dimensional heterogeneous transport models. The extreme opposite of assuming homogeneous porous flow is to assume isolated fracture flow. Models that assume only fracture flow limit sorption of radionuclides to minerals exposed on fracture surfaces. This results in retardation factors that are extremely close to 1.0 implying limited adsorption properties. This latter approach, while conservative, is as unrealistic as the homogeneous porous flow model for Yucca Mountain because demonstrated permeability in tuffs is not limited to either fractures or matrix pores. Thus, the abundant zeolites and clays, which are excellent adsorbers and cation exchangers, are accessible. This critical access may significantly retard radionuclide mobility.

A central question examined by our research effort is the extent to which interchange between fracture flow and porous matrix flow occurs in samples of densely welded tuff from Yucca Mountain. Experiments are being conducted to determine not only geochemical transport of radionuclides in heterogeneous media but also hydrologic flow and properties. Thus, combined effects of fracture flow, matrix diffusion in both connected porosity and dead-end pores, and accessibility of sorbing minerals in each environment are being examined. Basic experimental data provide a basis for theoretical modeling of the interplay between physical/hydrologic processes and chemical reactions in the Yucca Mountain situation. In addition, the experiments provide an empirical basis for applying laboratory data such as batch sorption K_d s to the prediction of radionuclide transport in the field. They **also** provide an understanding of the interplay between physical and chemical processes in the complex system presented by water movement through fractures in rock. This understanding is needed to extrapolate observations from the scale and breadth of conditions simulated in laboratory experiments to conditions in the field. This ability to extrapolate is essential; because it is nearly impossible to replicate in the laboratory, with a high degree of assurance, the conditions that exist in the field.

This report and its predecessor "Fracture Flow Under Saturated Conditions" (Rundberg *et al.*, 1986) review results of experiments that were designed to investigate the effects of fluid movement in fractures,

coupled with matrix diffusion and sorption but isolated from the effects of capillary suction and two-phase flow. This work is similar in concept to experiments performed by Neretznicks *et al.* (1984) and Moreno *et al.* (1985), but it specifically addresses processes occurring in Paintbrush Tuff that might affect siting and performance of a waste repository in Yucca Mountain, Nevada. These experiments collected data under carefully controlled conditions to help validate the effect of matrix diffusion on the retardation of radionuclides during transport by fracture flow. Theoretical analyses indicate that matrix diffusion may be beneficial in mitigating radionuclide migration. However, experimental validation is necessary for site-specific conditions because parameters such as pore tortuosity, fracture roughness, fracture coating by minerals, and matrix permeability vary with rock type and affect the transport of material in fractures. Previous experiments that involved singly fractured tuff samples have been used to examine a variety of important tracers [HTO, Sr, Ce, TcO_4^- , Ba, and Pu (Rundberg *et al.*, 1986)]. This report presents the results of a subsequent set of experiments using a rock column cut by a fracture network.

II. EXPERIMENTAL

A. Description of Fracture Network Sample

The block of fractured tuff used in these experiments was collected from surface outcroppings of the Topopah Springs Member of the Paintbrush Tuff. This sample is composed of devitrified ash-flow tuff and was selected for its network of natural fractures. Its mineralogy is similar to other Topopah Springs samples used for previous fracture flow experiments (Rundberg *et al.*, 1986).

Pictures of block faces are shown in Fig. 1. When the sample was collected, fractures in the block were filled with carbonate minerals. Such fracture cements are common constituents of surficial samples but absent in deeper drill core samples. After the block was partially encapsulated, the fracture carbonate cements were removed by leaching with a dilute HCl solution. Accessible matrix porosity and fracture network volume, 149 cm^3 ($21.3 \text{ cm}^3/\text{kg}$ dry weight), were determined from measurements of block dry weight and total saturated weight. An estimate of the roughness and space intersected by the fracture network has been obtained by analysis of the box dimension of fractures cutting the block faces (Fig. 2); this analysis resulted in a fractal dimension of approximately 1.1 (H_d) (Mandelbrot, 1975; Mandelbrot 1983; Lovejoy and

Mandelbrot, 1985; Pentland, 1984). These results are consistent with studies of fracture networks intersecting pavements in the Yucca Mountain area (Barton, 1985). Information received from K. Boring, Los Alamos National Laboratory (1986).

B. Apparatus

The block of tuff was encased in a LEXAN box and sealed with SILACIC. This box was designed to eliminate leakage of solutions around the seals, but is not capable to simulating natural lithostatic or hydrostatic loads.

Tracer-loaded solutions were flowed through the fracture network sample with a SAGE syringe pump using 60-cm³ syringes. The syringe pump was chosen because it could provide steady flow at low to high rates for the large volumes and time periods necessary to obtain data for these experiments. Pressure drops across the fracture were measured by placing Kistler 4053A1 piezoresistive transducers at the enclosure's inlet and outlet ports.

C. Methods of Measurement

An estimate of the fracture aperture for the fracture network sample (5.92×10^{-5} m) was determined by establishing an initial head of 2.0 m of water and measuring the flow rate and pressure drop across the network at 2.0- to 0.05-m head. The aperture was calculated using the cubic law for fracture flow (Witherspoon *et al.*, 1979), as previously described by Rundberg *et al.* (1986). This approach assumes plane sheet flow and hydraulically smooth fractures.

During a tracer injection experiment, flow rates were determined by measuring the weight loss of the supply syringe as a function of time. The effluent concentration of tracer was determined by assaying the column effluent relative to a sample of the injected solution. Specific activities for tritiated-water (HTO)-spiked samples were determined by liquid scintillation counting using a Packard model 460C automatic scintillation counter. Activities of Tc^{95m} were determined by standard gamma-ray counting techniques using NaI detectors. Sulforhodamine B dye concentrations were determined by comparing standard and sample absorption over the 300- to 700- μ m wavelengths using a Hewlett-Packard UV/VIS spectrophotometer.

III. EXPERIMENTAL RESULTS

Table I contains the relevant operating parameters for each of the fracture elutions completed on the fractured tuff network column. The results of elutions through the fractured tuff network column, as relative concentrations (concentration eluted relative to the input concentration of tracer tabulated) vs total volume eluted, are plotted in Figs. 3-8.

TABLE I. Experimental Parameters for Network Fracture Flow Tracer Experiments Using Devitrified, Densely Welded Tuff From the Topopah Spring Member of the Paintbrush Tuff

Tracer	Flow Rate (ml/hr)	Concentration (cpm/ml)	Volume (ml)
HTO	0.91	511.55	43.9
HTO	0.94	494.80	44.9
HTO	0.98	973.70	51.0
TcO ₄ -	0.94	3360.	45.1
TcO ₄ -	0.95	2616.	45.5
Sulforhodamine B dye	54.3		110.4

V. Discussion and Theoretical Results

A. Experimental Results and Discussion

Elution curves for pertechnetate and sulforhodamine B dye are relatively smooth and for pertechnetate, reproducible (Figs. 6-8). In contrast, HTO elution curves are irregular and not reproducible (Figs. 3-5). The first two HTO experimental results indicate significantly delayed breakthrough and jumps in tracer concentration at $\sim 175\text{-cm}^3$ cumulative volume. The sample, which exhibits the jump in tracer concentration in both experiments, represents the first sample collected in a capped bottle rather than in an open fraction collection tube. This suggests that earlier samples have lost HTO as a result of volatilization in the fraction collector system. In contrast, the third HTO run has a smoother elution curve with a much earlier breakthrough (Fig. 5). Theoretical models of the experiments (Sec. V.B) support the interpretation that the first two experiments did not collect HTO efficiently, whereas the third experiment is a more accurate representation of HTO tracer behavior.

Differentiation of breakthrough volumes between tracers for these experiments is not resolvable (Figs. 5-8) because of the small number of samples taken during this interval. However, calculated total elution vs injection balances for these experiments (Figs. 9-14) indicates that approximately 75, 82, and 88% of injected HTO, pertechnetate, and sulforhodamine B dye, respectively could be rapidly flushed out of the network. The approximate per cent of HTO eluted was calculated by using the third experiment to define early elution and adding the later elution of the first two experiments, thus partially accounting for the proposed evaporative loss (Figs. 3-5 and 9-11). Percentage of total tracers eluted can be qualitatively related to molecular sizes [and molecular diffusivities (Miller, 1982; Sherwood *et al.*, 1975)], which increase from HTO to pertechnetate to sulforhodamine B dye. Thus, modeling of these experiments could provide direct information on the size, accessibility, and connectivity of matrix porosity relative to flow in the fracture network. Elution rates for all three tracers are evidently dominated by flow in the fracture network, resulting in similarly shaped elution curves following maximum eluted tracer concentrations (Figs. 3-20).

B. Theoretical Results and Discussion

A series of models have been developed to examine coupling between fracture flow and matrix diffusion in these experiments. These models assume a single parallel-sided fracture in a porous matrix (Tang, 1981) and use the parameters listed in Table II. Initial calculations were focused on pertechnetate experiments because all the necessary input data to the models was available and the experiments showed excellent reproducibility (Figs. 6-7). The first set of models used the fracture aperture (0.00592 cm) calculated by the cubic law for fracture flow (Witherspoon *et al.*, 1979; Rundberg *et al.*, 1986). Adjusting parameters within wide limits failed to result in a good fit between the model calculations (Fig. 21) and experimental results. Choosing an aperture of 0.1 cm, however, produced a good fit to the experimental results (Fig. 22), which could be improved by slight adjustments to dispersivity (Fig. 23).

In models of the sulforhodamine B dye experiments, the diffusivity of the dye was assumed to be equivalent to pertechnetate, and flow rate and injected volume were set to match experimental conditions. The initial model did not match experimental results, but a good fit was obtained by adjusting the dispersion constant to make the longitudinal dispersivity constant (Tang, 1981) (compare Figs. 24 and 25 with Fig. 3).

TABLE II. Parameters Used to Model Single Fracture in a Porous Matrix for Relative Tracer Concentration Eluted as a Function of Volume Eluted

Model	Tracer	Tracer Diffusivity (cm ² /s)	Flow Rate ^a (ml/s)	Pulse Duration ^b (ml)	Tracer K _d
0	TcO ₄ ⁻	0.0000150 ^b	0.000253	43.9	0.
1	TcO ₄ ⁻	0.0000150	0.000253	43.9	0.
2	TcO ₄ ⁻	0.0000150	0.000253	43.9	0.
3	Sulforhodamine B dye	0.0000150 ^c	0.015100	110.4	0.
4	Sulforhodamine B dye	0.0000150	0.015100	110.4	0.
5	HTO	0.0000244 ^d	0.000253	43.9	0.

^a Experimental parameters.

^b Miller, 1982.

^c Assumed equivalent to TcO₄⁻.

^d Sherwood *et al.*, 1975.

TABLE II. Parameters Used to Model Single Fracture in a Porous Matrix for Relative Tracer Concentration Eluted as a Function of Volume Eluted (cont)

Model	Dry Bulk Density ^a (g/cm ³)	Porosity ^b (cm ³ /g)	Dead Volume ^c (ml)	Dispersivity ^d (cm ² /s)
0	2.3	0.047	0.8	0.003
1	2.3	0.047	0.8	0.003
2	2.3	0.047	0.8	0.002
3	2.3	0.047	0.8	0.002
4	2.3	0.047	0.8	0.120
5	2.3	0.047	0.8	0.002

^a Average tuff density.

^b Measured by change in weight of block after saturation.

^c Measured for encapsulated block.

^d Adjustable parameter in model.

TABLE II. Parameters Used to Model Single Fracture in a Porous Matrix for Relative Tracer Concentration Eluted as a Function of Volume Eluted (cont)

Model	Width ^a (cm)	Length ^b (cm)	Aperture ^c (cm)	Constrictivity ^d	Tortuosity ^e
0	17.6	27.0	0.00592 ^f	0.10	1.410
1	17.6	27.0	0.10000	0.10	1.410
2	17.6	27.0	0.10000	0.10	1.410
3	17.6	27.0	0.10000	0.10	1.410
4	17.6	27.0	0.10000	0.10	1.410
5	17.6	27.0	0.10000	0.10	1.410

^a Estimated from xerox pictures of block faces.

^b Estimated from xerox pictures of block faces.

^c Calculated from hydraulic head and flow rate measurements or estimated (see text).

^d Estimated from tortuosity and analysis of diffusion experiments where $\text{constrictivity}/(\text{tortuosity})^2 \cong 0.05$.

^e (Walters and Kidd, 1979).

^f Calculated fracture aperture (see text).

Setting model parameters for diffusivity and experimental conditions equivalent to those of HTO experiments results in the elution curve shown in Fig. 26. This model confirms the suggestions that experimental samples (Figs. 3 and 4) lost HTO during sampling and that elution curves for all three tracers should have essentially the same shape. The model also is consistent with lower total elution of HTO (Figs. 9-11, also see discussion above) relative to pertechnetate and sulforhodamine B dye (Figs. 12-14). A lower maximum concentration of HTO in the model, compared to that in the third HTO experiment (Fig. 5), may indicate that there is a significant difference in parameters between HTO and the other tracers (for example, constrictivity).

VI. Conclusions

Breakthrough of HTO, pertechnetate, and sulforhodamine B dye occurs rapidly in these experiments. The fraction of injected tracer eluted is ~75, 82, and 88% for HTO, pertechnetate, and sulforhodamine B dye, respectively. The relative differences in recovered tracer is interpreted as a function of size exclusion of molecular species from an increasing proportion of the matrix pores. Modeling the experiments by using

a formulation for a single parallel-sided fracture in a porous rock matrix produces elution curves that are consistent with experimental results. The calculations do, however, require a significantly larger value for fracture aperture than if they were measured experimentally. Differing fracture apertures for fluid flow analysis and tracer data have been observed previously and were attributed to roughness of the fracture surface (Tsang and Tsang, 1984).

This experimental program continues to demonstrate the significance of coupled fracture flow and porous matrix flow/diffusion in tuff under saturated conditions. Hydrologic/geochemical modeling of radionuclide transport for the Yucca Mountain Project must accurately account for these combined phenomena. Modeling of the experimental results shows promise for providing well-constrained and robust—but relatively simple—formulations that can be used in site-performance assessment models.

VII. References

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Fig. 1. Photo of a block face.

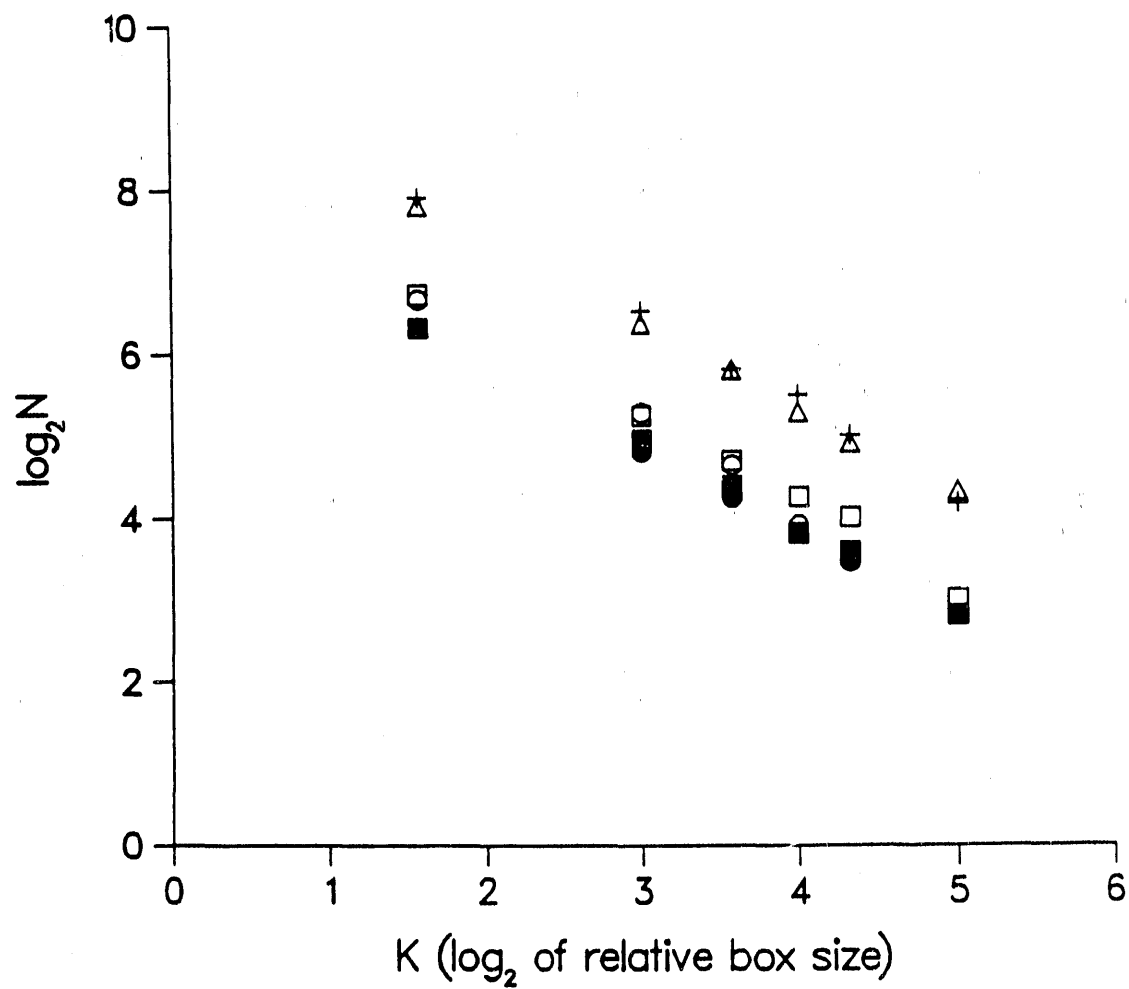


Fig. 2. Fractal box dimension analysis of fracture network.

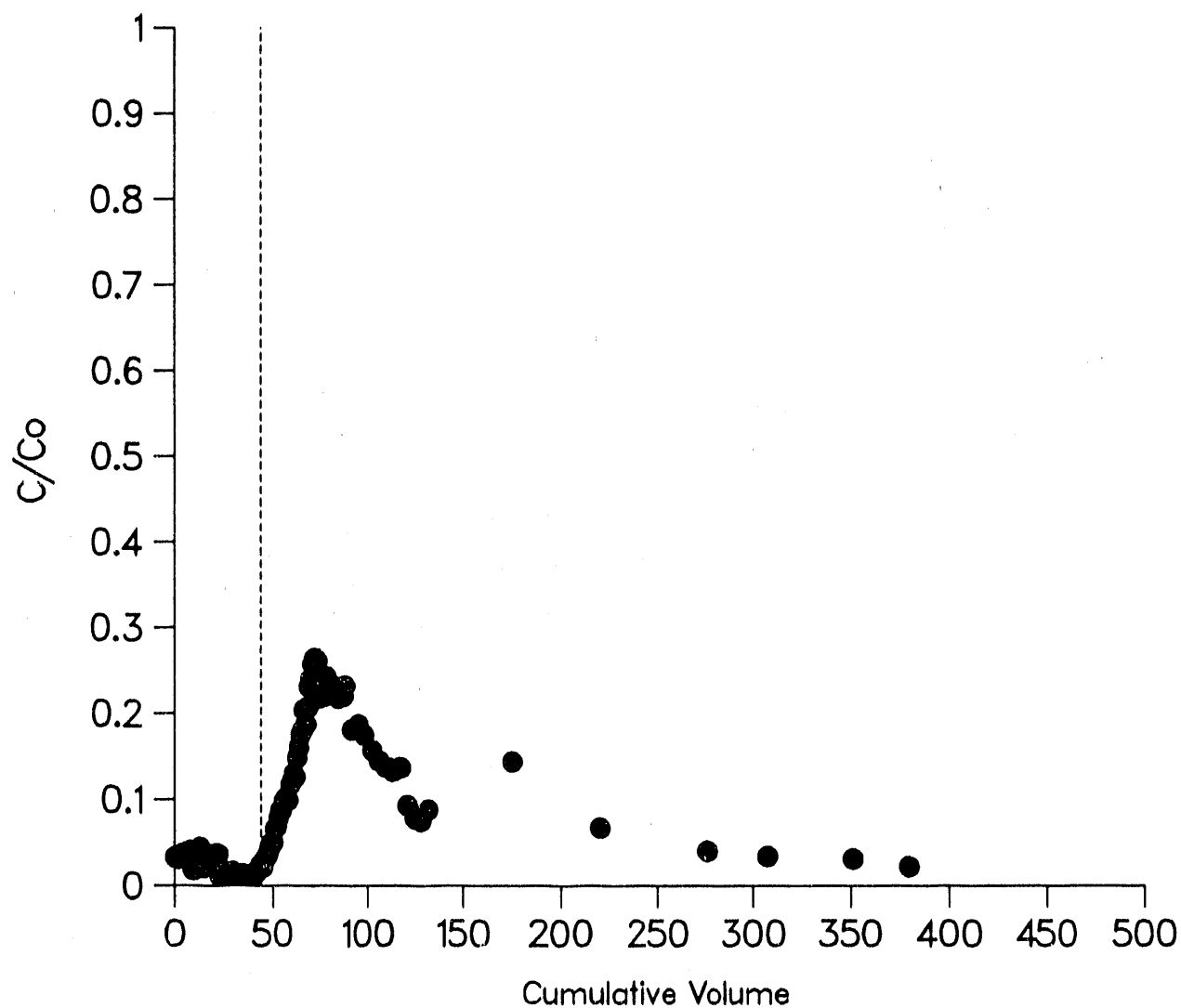


Fig. 3. First run of HTO-spiked J-13 water in Topopah Spring Member fracture network column at a flow rate of 0.91 ml/hr; initial HTO concentration was 511.55 cpm/ml. After 43.9 ml of eluent was collected, the input solution was changed to pure J-13 water (dashed line).

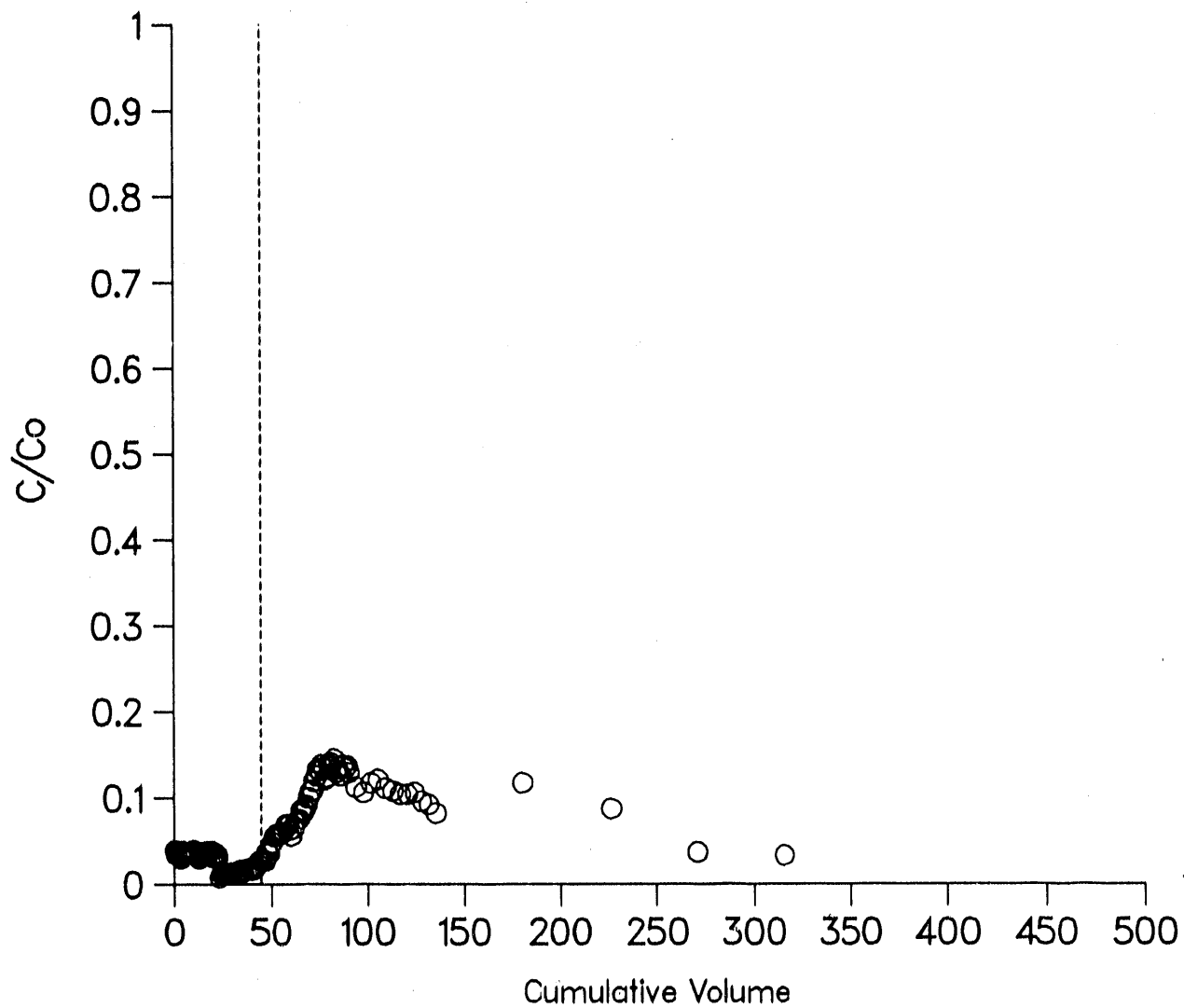


Fig. 4. Second run of HTO-spiked J-13 water in Topopah Spring Member fracture network column at a flow rate of 0.94 ml/hr; initial HTO concentration was 494.80 cpm/ml. After 44.9 ml of eluent was collected, the input solution was changed to pure J-13 water (dashed line).

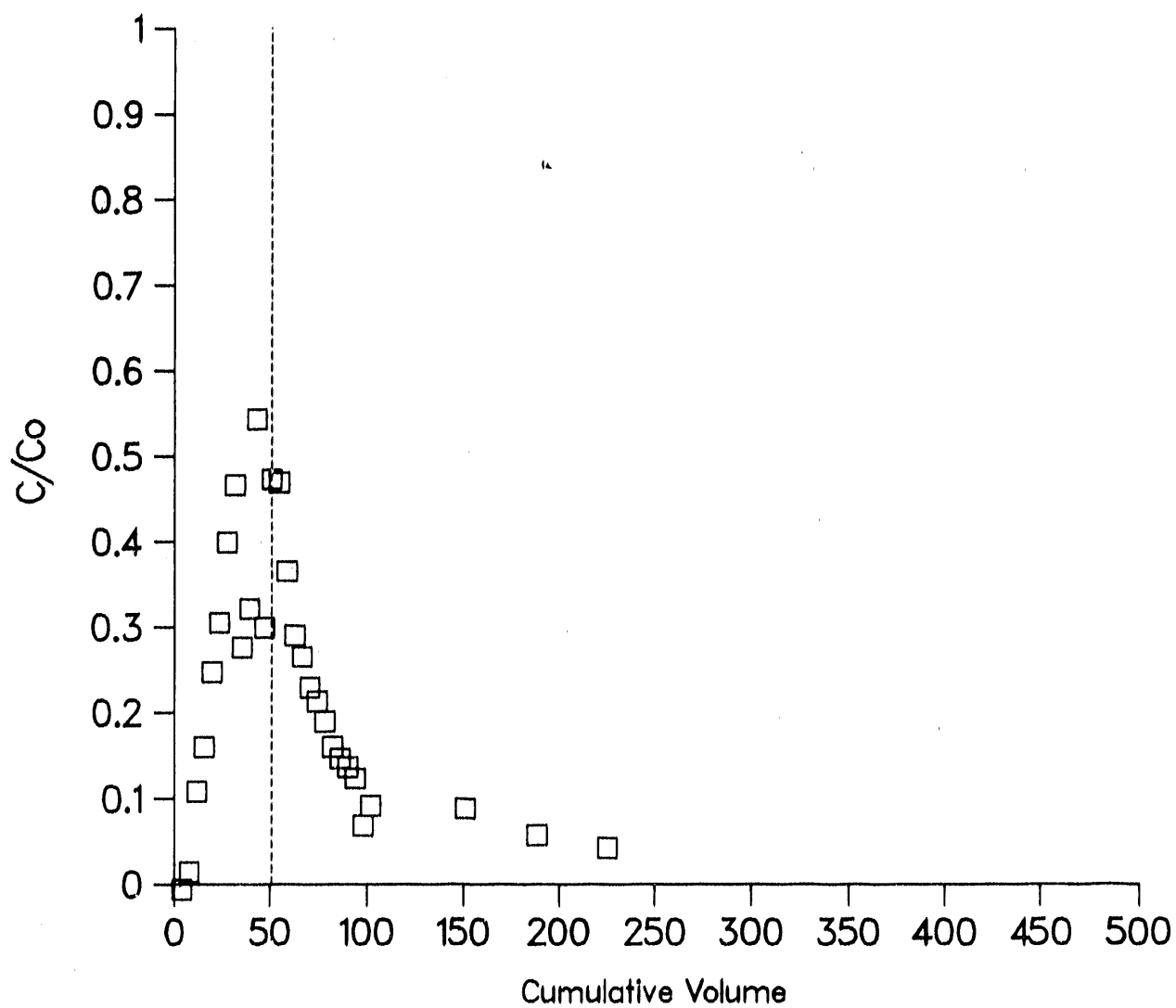


Fig. 5. Third run of HTO-spiked J-13 water in Topopah Spring Member fracture network column at a flow rate of 0.98 ml/hr; initial HTO concentration was 973.70 cpm/ml. After 50.96 ml of eluent was collected, the input solution was changed to pure J-13 water (dashed line).

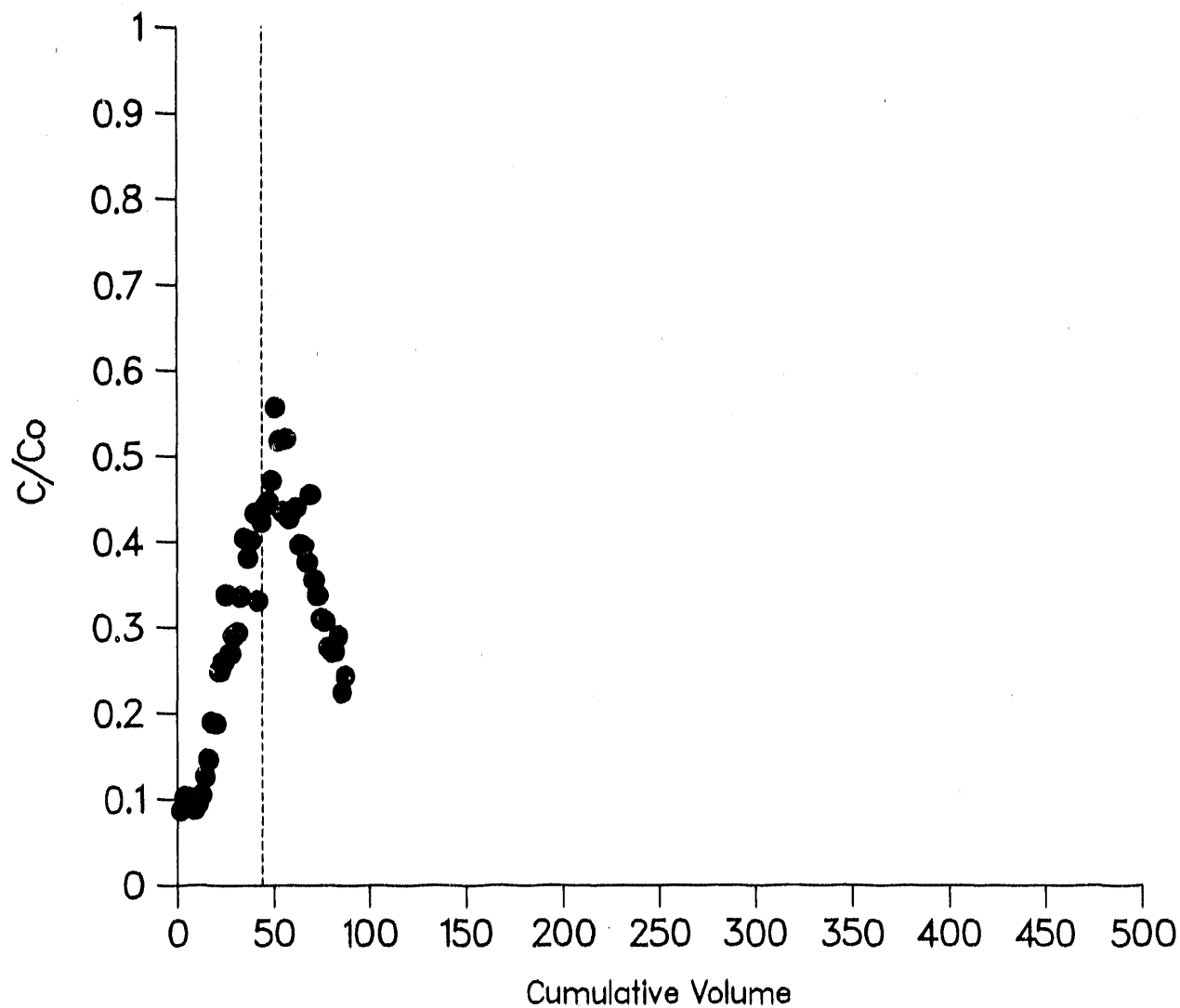


Fig. 6. First run of TcO_4^- -spiked J-13 water in Topopah Spring Member fracture network column at a flow rate of 0.94 ml/hr; initial TcO_4^- concentration was 3360. cpm/ml. After 45.1 ml of eluent was collected, the input solution was changed to pure J-13 water (dashed line).

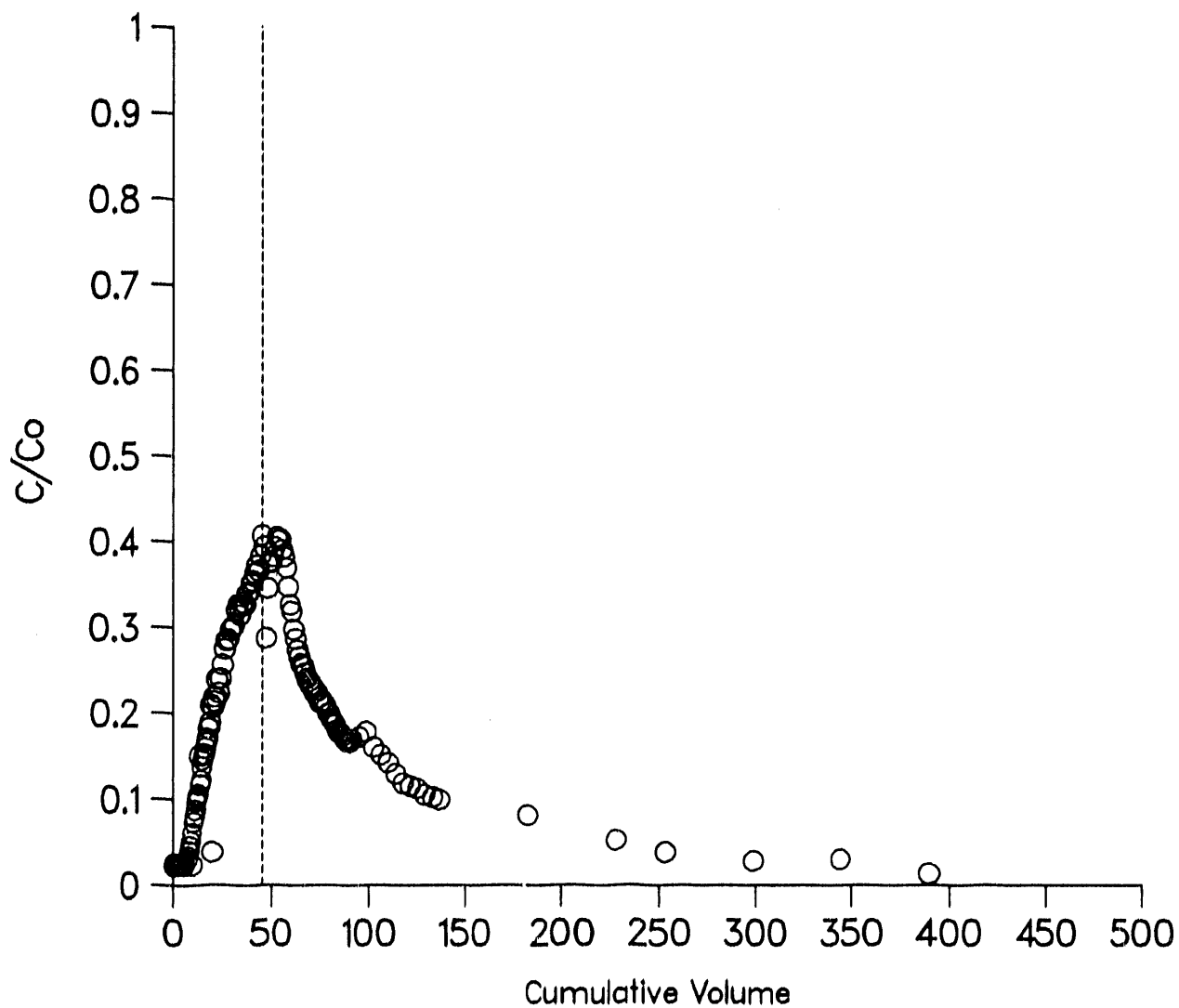


Fig. 7. Second run of TcO_4^- -spiked J-13 water in Topopah Spring Member fracture network column at a flow rate of 0.95 ml/hr; initial TcO_4^- concentration was 2616. cpm/ml. After 45.5 ml of eluent was collected, the input solution was changed to pure J-13 water (dashed line).

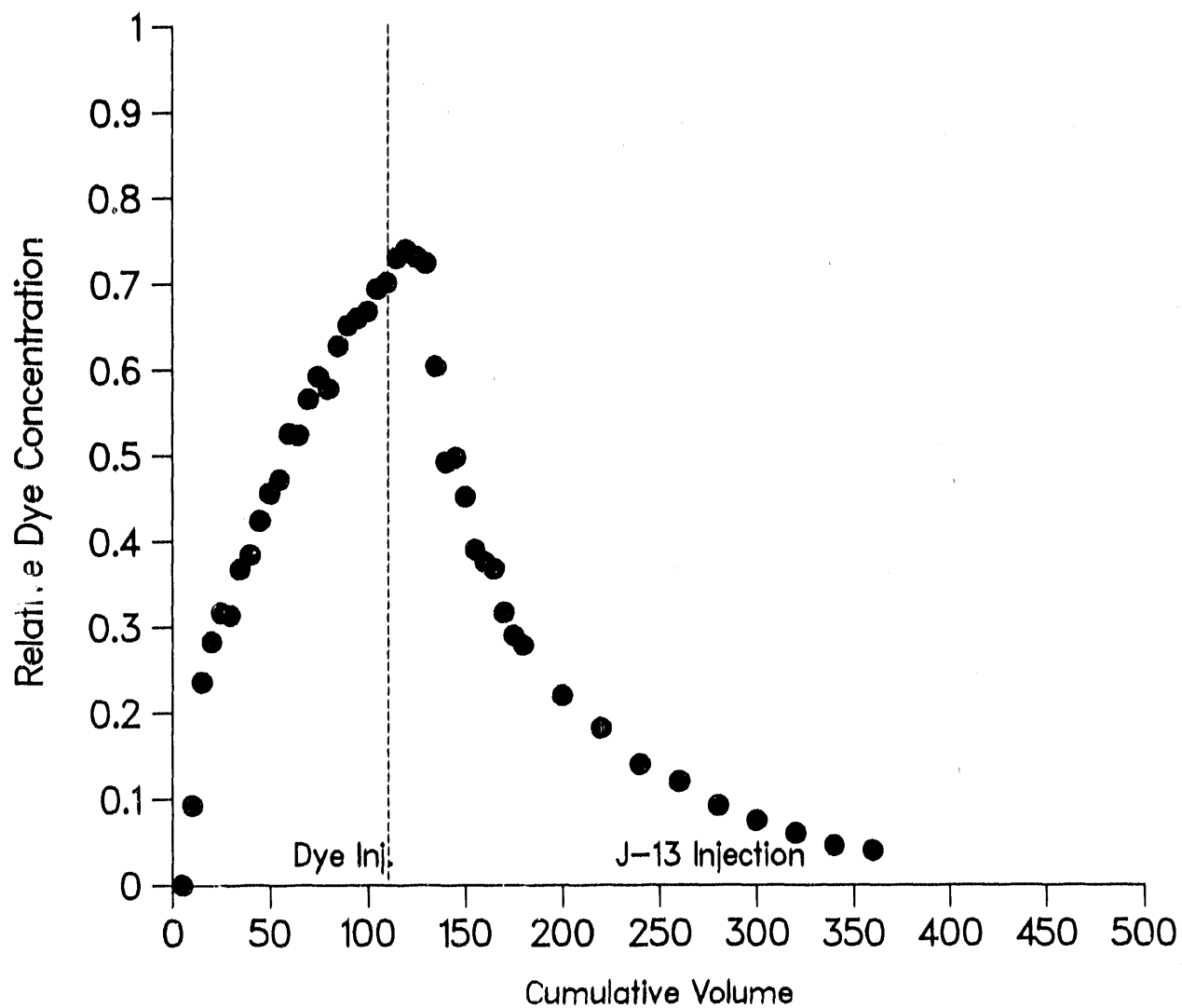


Fig. 8. Run of sulforhodamine B dye-spiked J-13 water in Topopah Spring Member fracture network column at a flow rate of 54.3 ml/hr. After 110.4 ml of eluent was collected, the input solution was changed to pure J-13 water (dashed line).

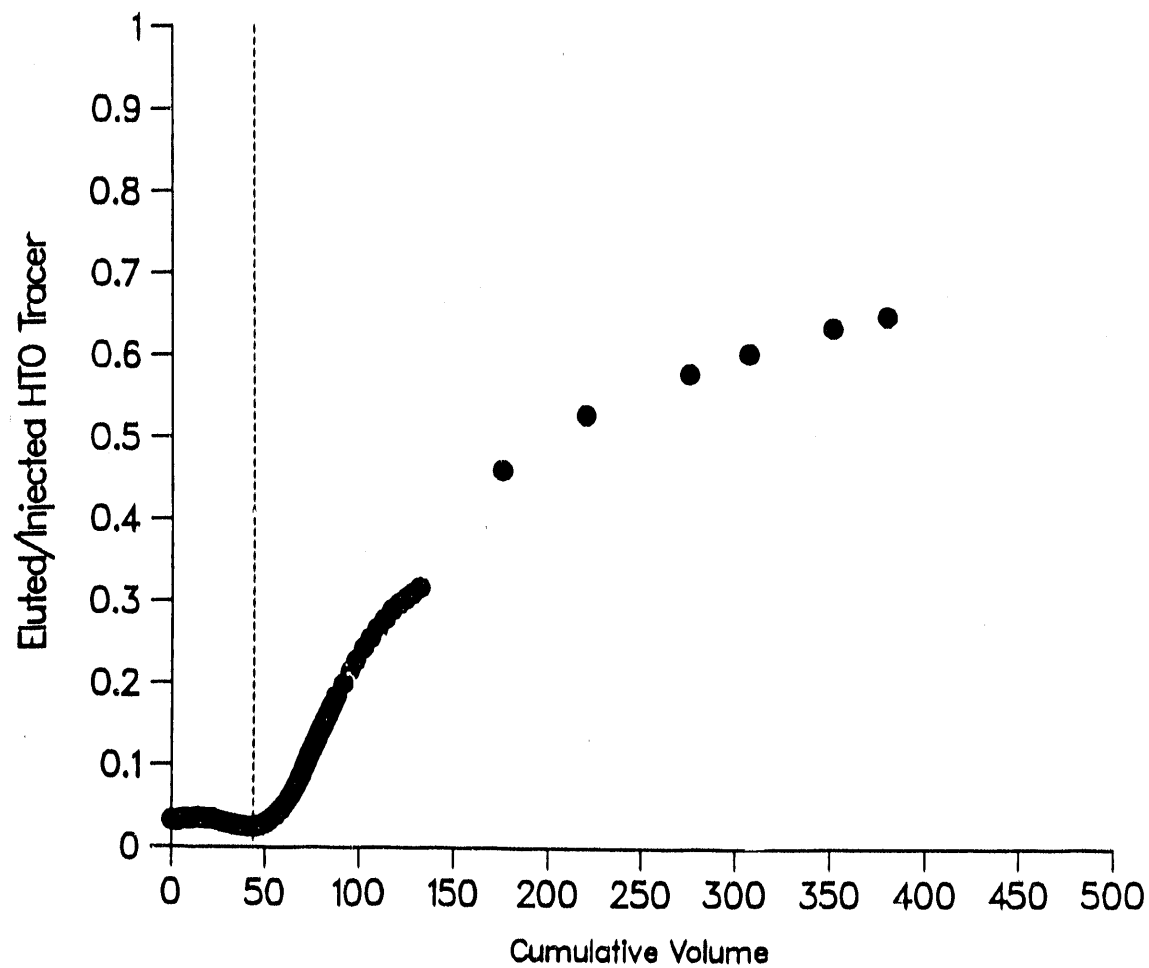


Fig. 9. Calculated sum of eluted tracer relative to sum of injected tracer for first run of HTO-spiked J-13 water in Topopah Spring Member fracture network column. Data shown in Fig. 3. Dashed line indicates change to unspiked J-13 water.

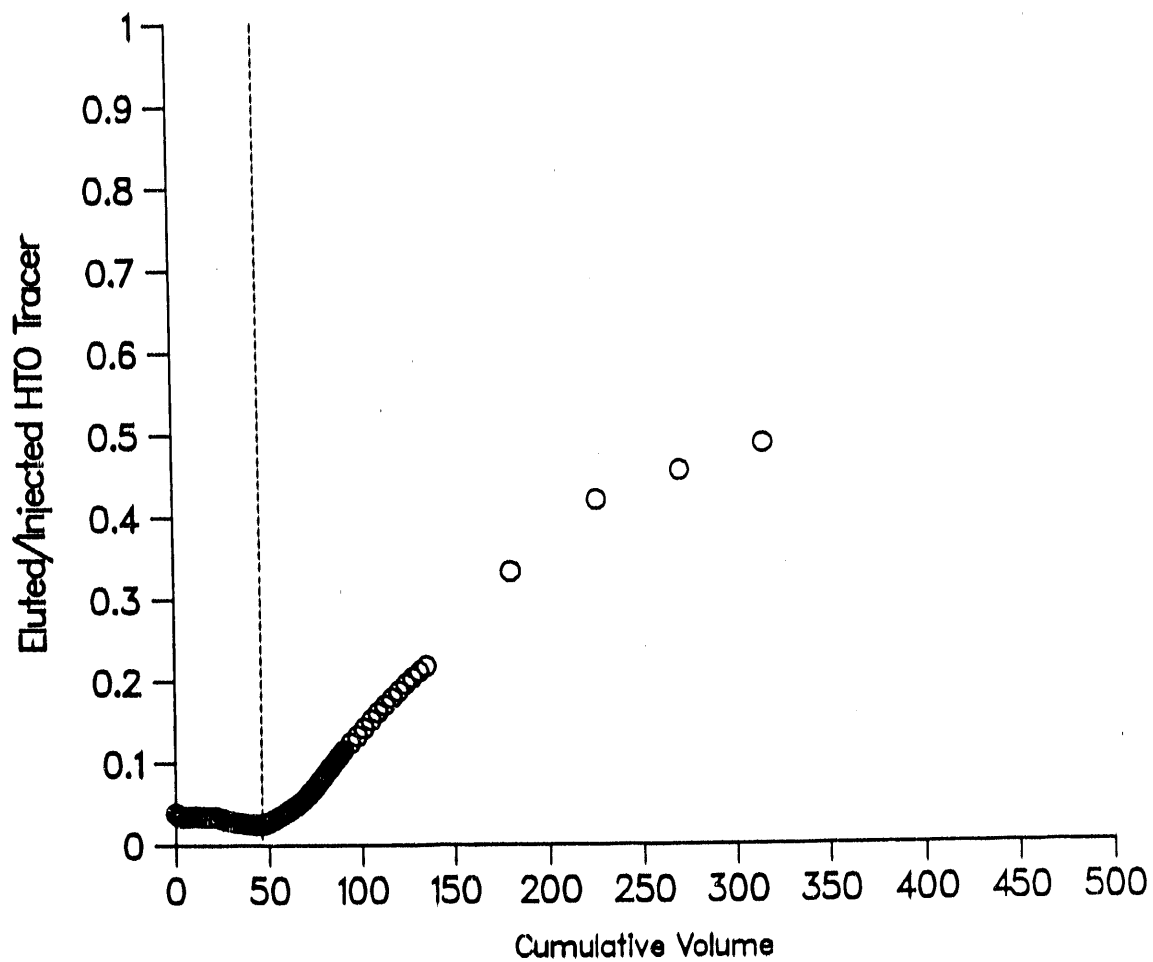


Fig. 10. Calculated sum of eluted tracer relative to sum of injected tracer for second run of HTO-spiked J-13 water in Topopah Spring Member fracture network column. Data shown in Fig. 4. Dashed line indicates change to unspiked J-13 water.

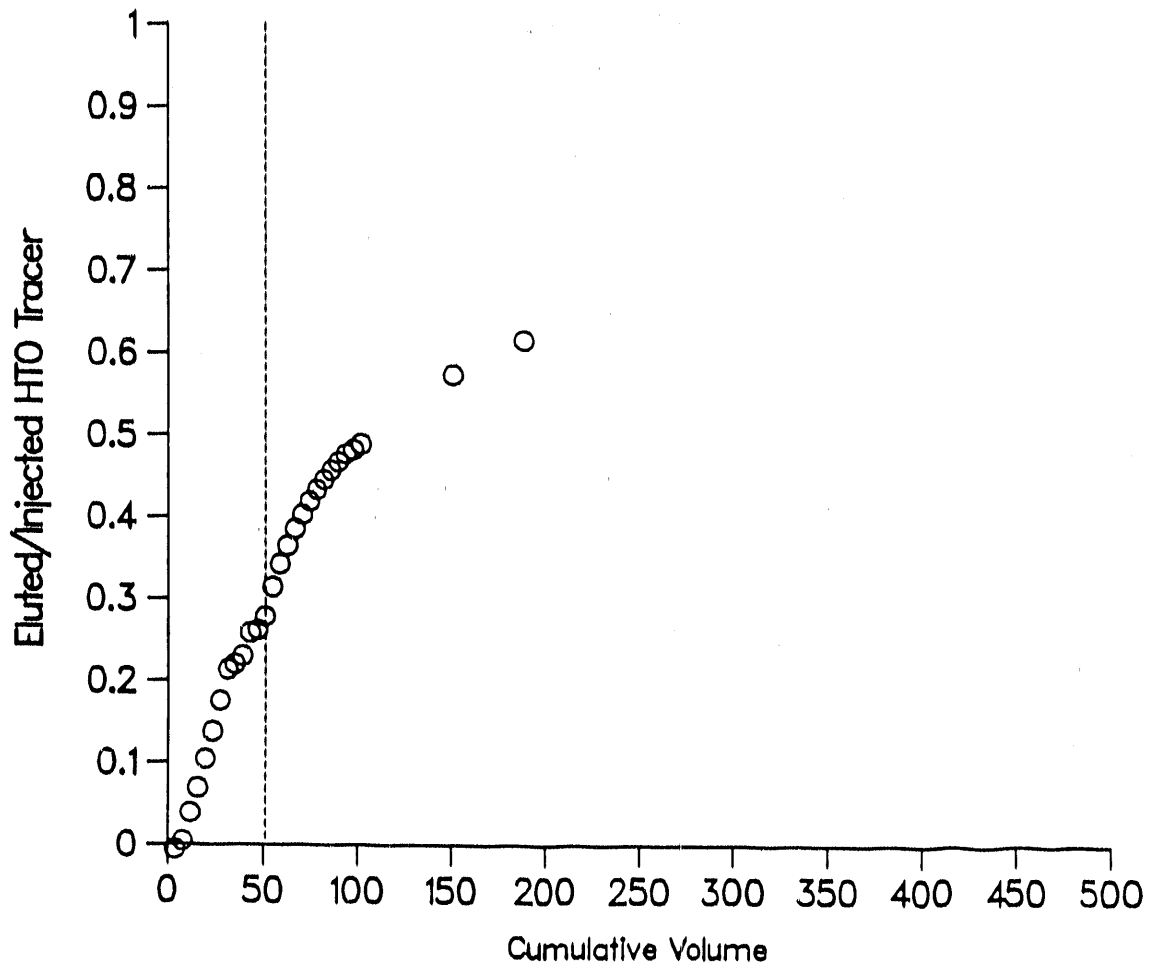


Fig. 11. Calculated sum of eluted tracer relative to sum of injected tracer for second run of HTO-spiked J-13 water in Topopah Spring Member fracture network column. Data shown in Fig. 5. Dashed line indicates change to unspiked J-13 water.

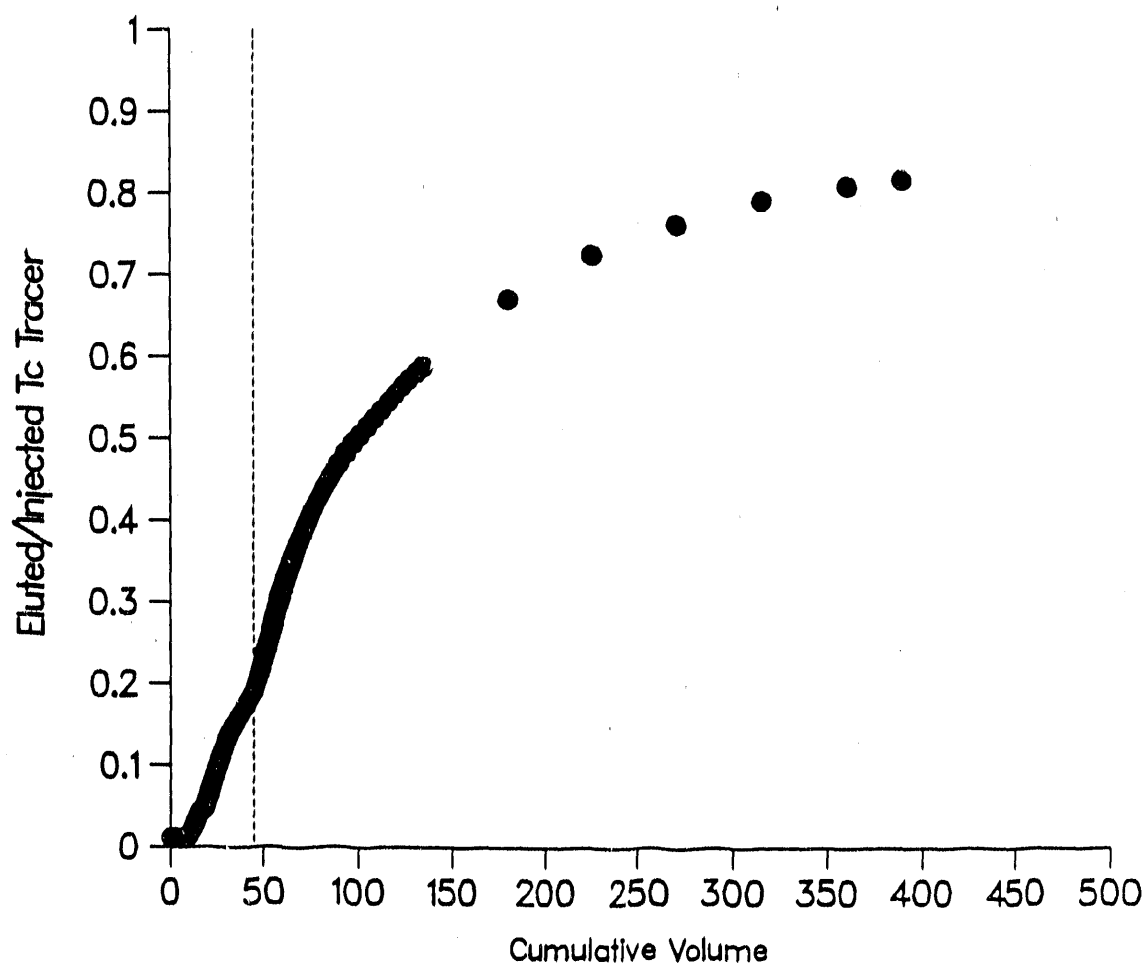


Fig. 12. Calculated sum of eluted tracer relative to sum of injected tracer for first run of pertechnetate-spiked J-13 water in Topopah Spring Member fracture network column. Data shown in Fig. 6. Dashed line indicates change to unspiked J-13 water.

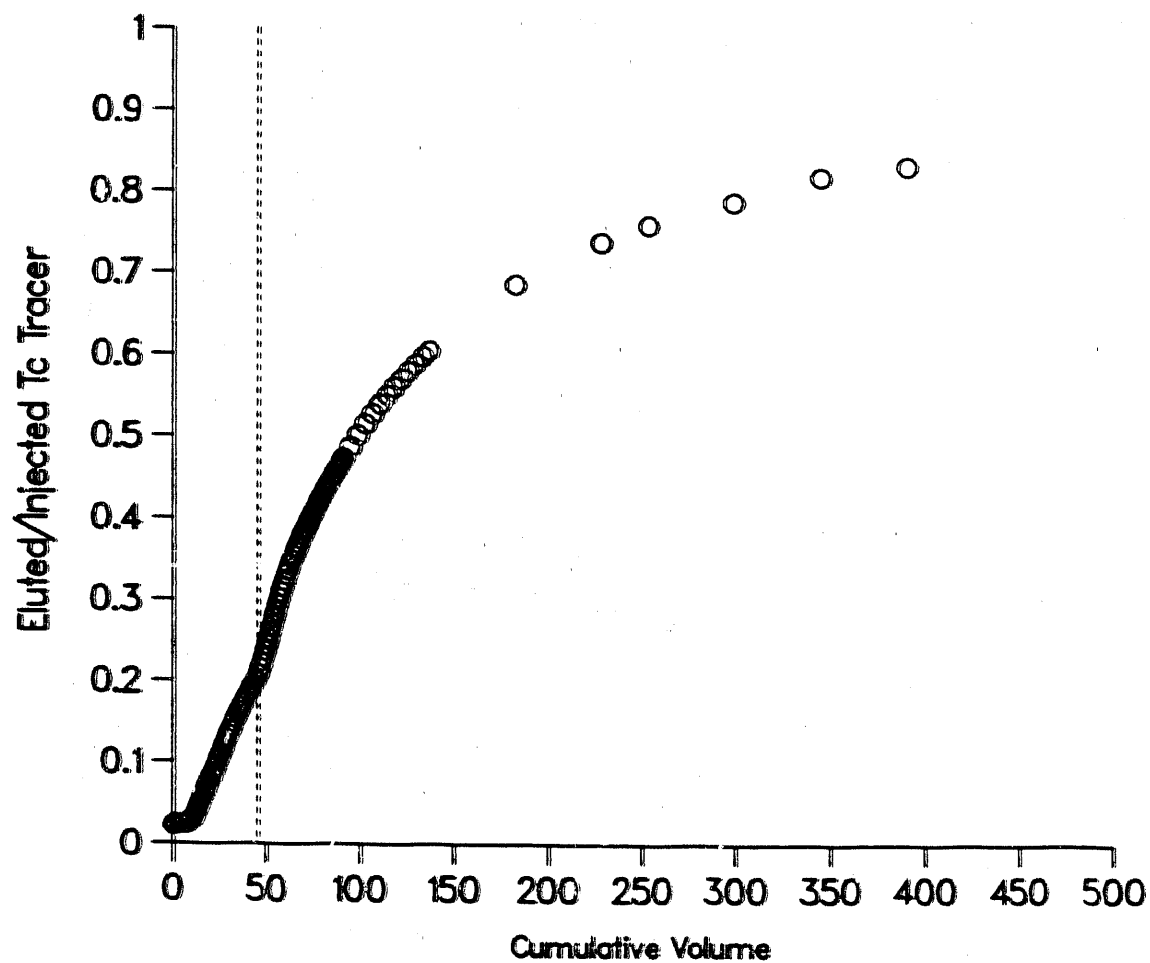


Fig. 13. Calculated sum of eluted tracer relative to sum of injected tracer for second run of pertechnetate-spiked J-13 water in Topopah Spring Member fracture network column. Data shown in Fig. 7. Dashed line indicates change to unspiked J-13 water.

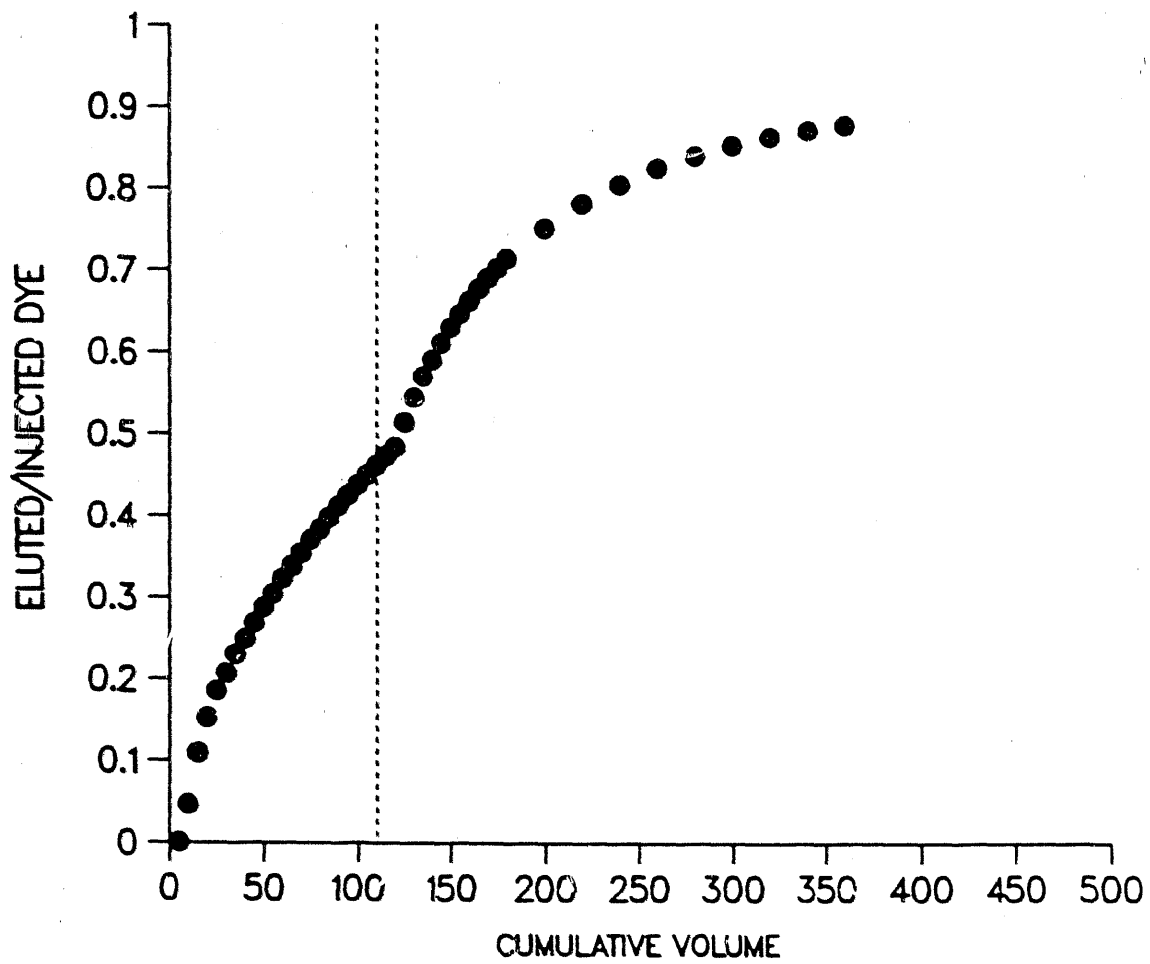


Fig. 14. Calculated sum of eluted tracer relative to sum of injected tracer for run of sulforhodamine B dye-spiked J-13 water in Topopah Spring Member fracture network column. Data shown in Fig. 8. Dashed line indicates change to unspiked J-13 water.

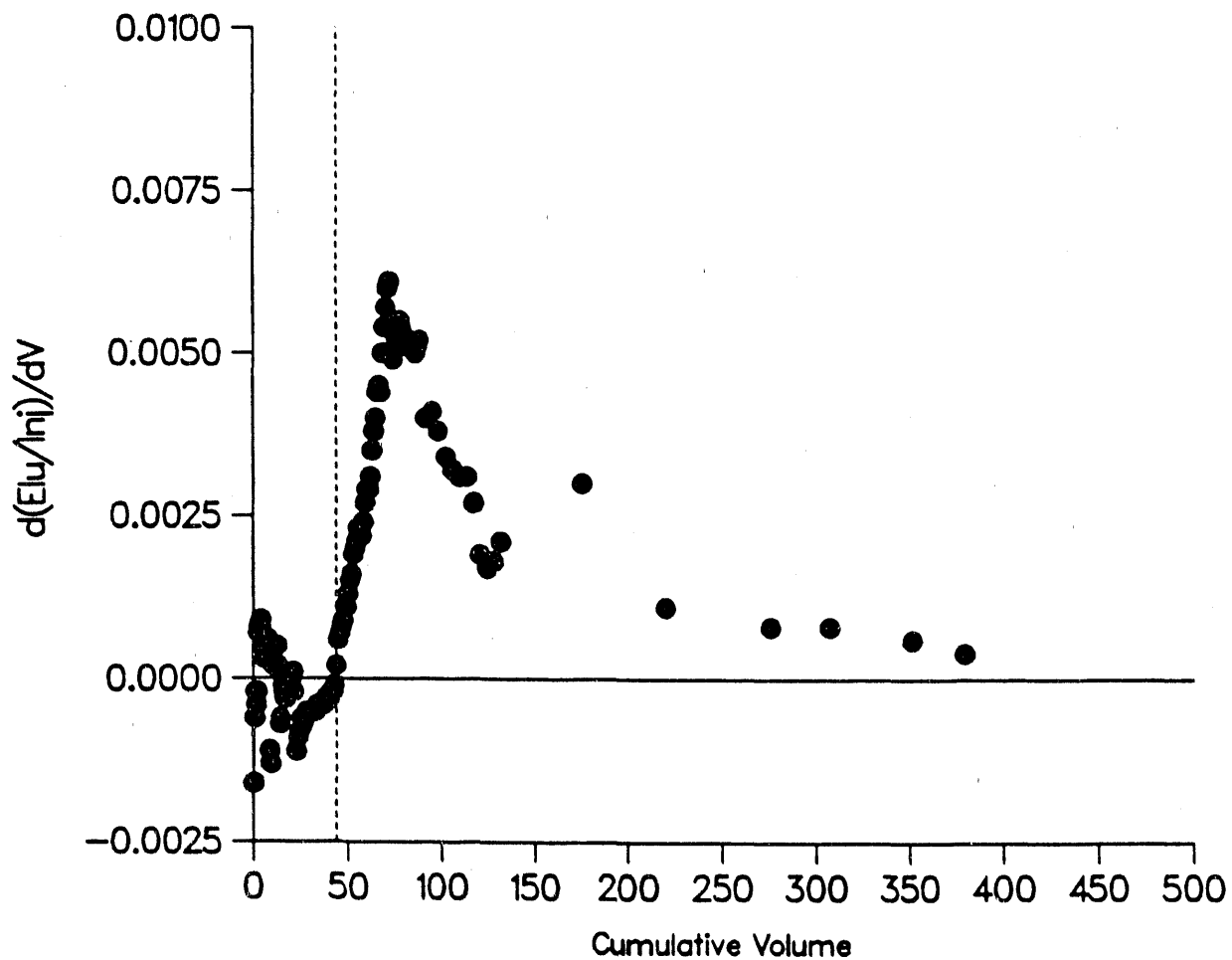


Fig. 15. Calculated rate of change for sum of relative eluted tracer from first run of HTO-spiked J-13 water in Topopah Spring Member fracture network column. Data shown in Fig. 9. Dashed line indicates change to unspiked J-13 water.

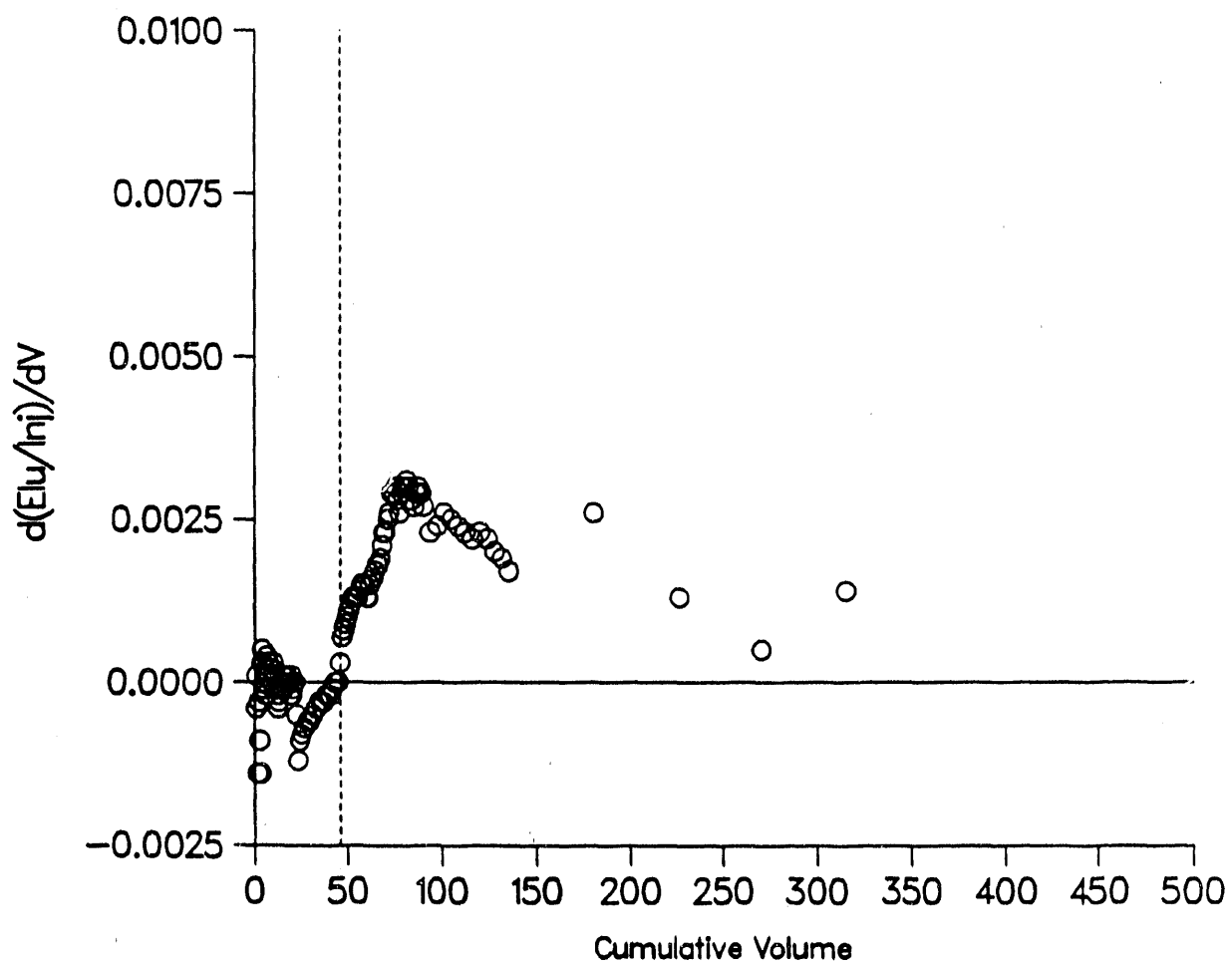


Fig. 16. Calculated rate of change for sum of relative eluted tracer from second run of HTO-spiked J-13 water in Topopah Spring Member fracture network column. Data shown in Fig. 10. Dashed line indicates change to unspiked J-13 water.

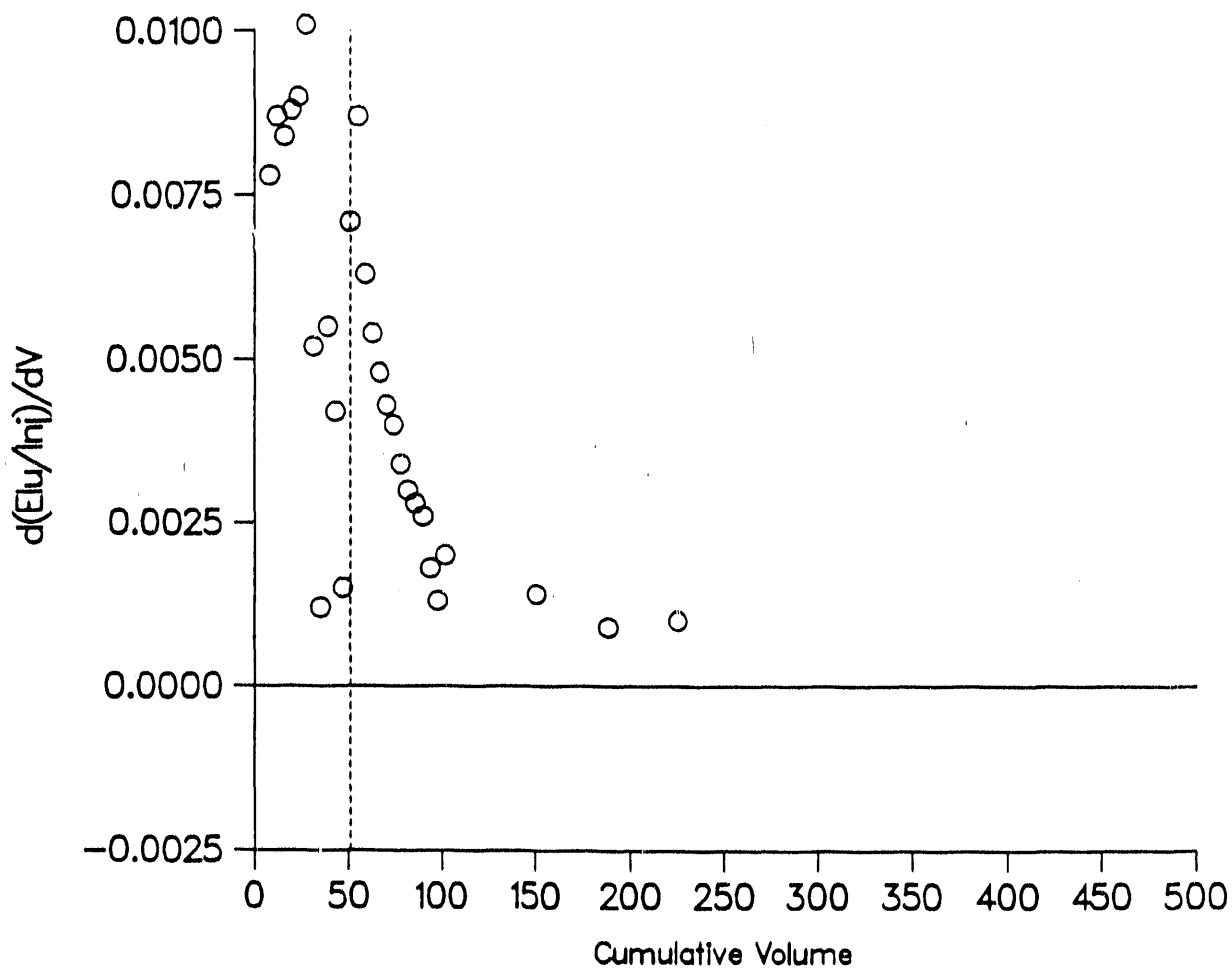


Fig. 17. Calculated rate of change for sum of relative eluted tracer from second run of HTO-spiked J-13 water in Topopah Spring Member fracture network column. Data shown in Fig. 11. Dashed line indicates change to unspiked J-13 water.

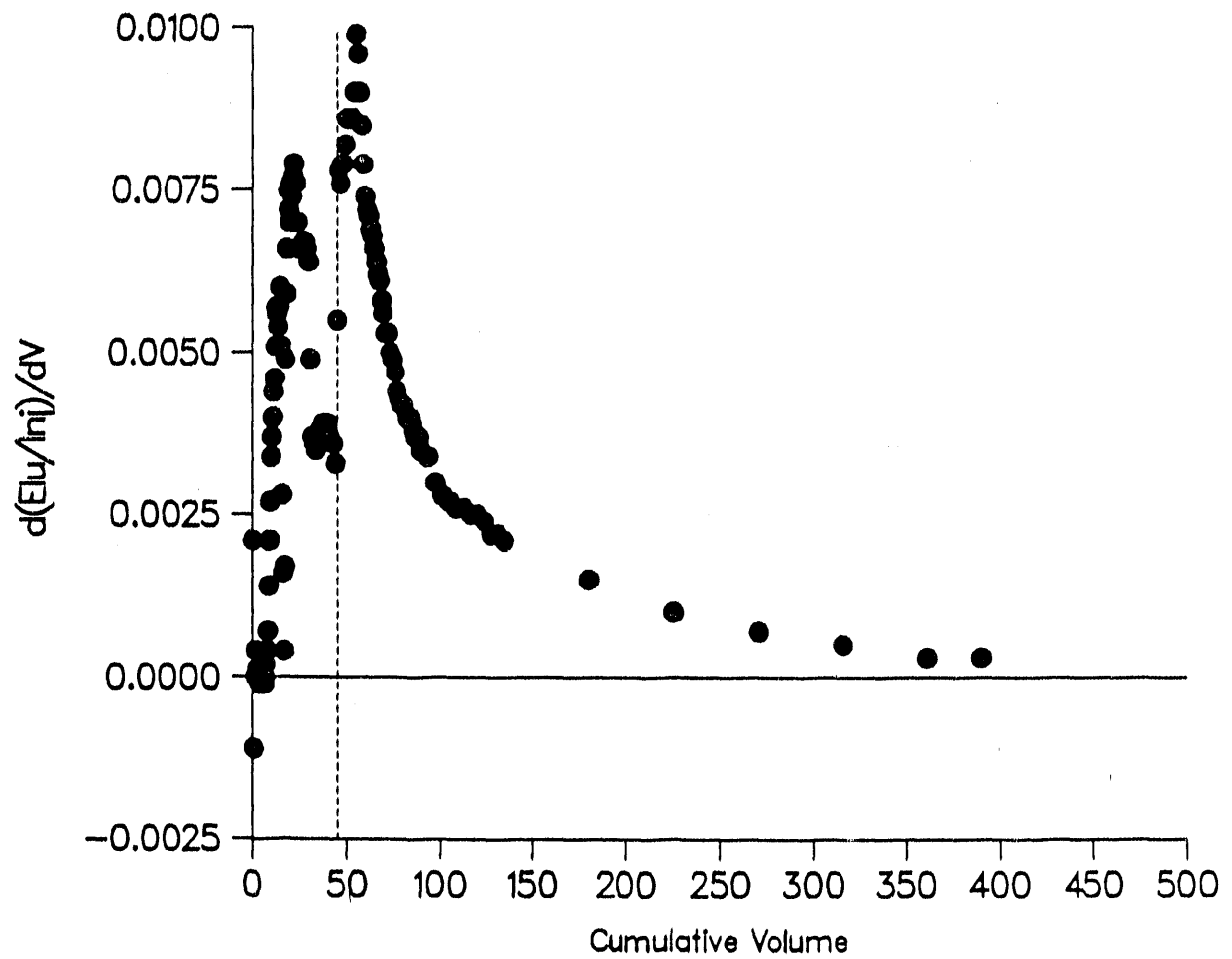


Fig. 18. Calculated rate of change for sum of relative eluted tracer from first run of pertechnetate-spiked J-13 water in Topopah Spring Member fracture network column. Data shown in Fig. 12. Dashed line indicates change to unspiked J-13 water.

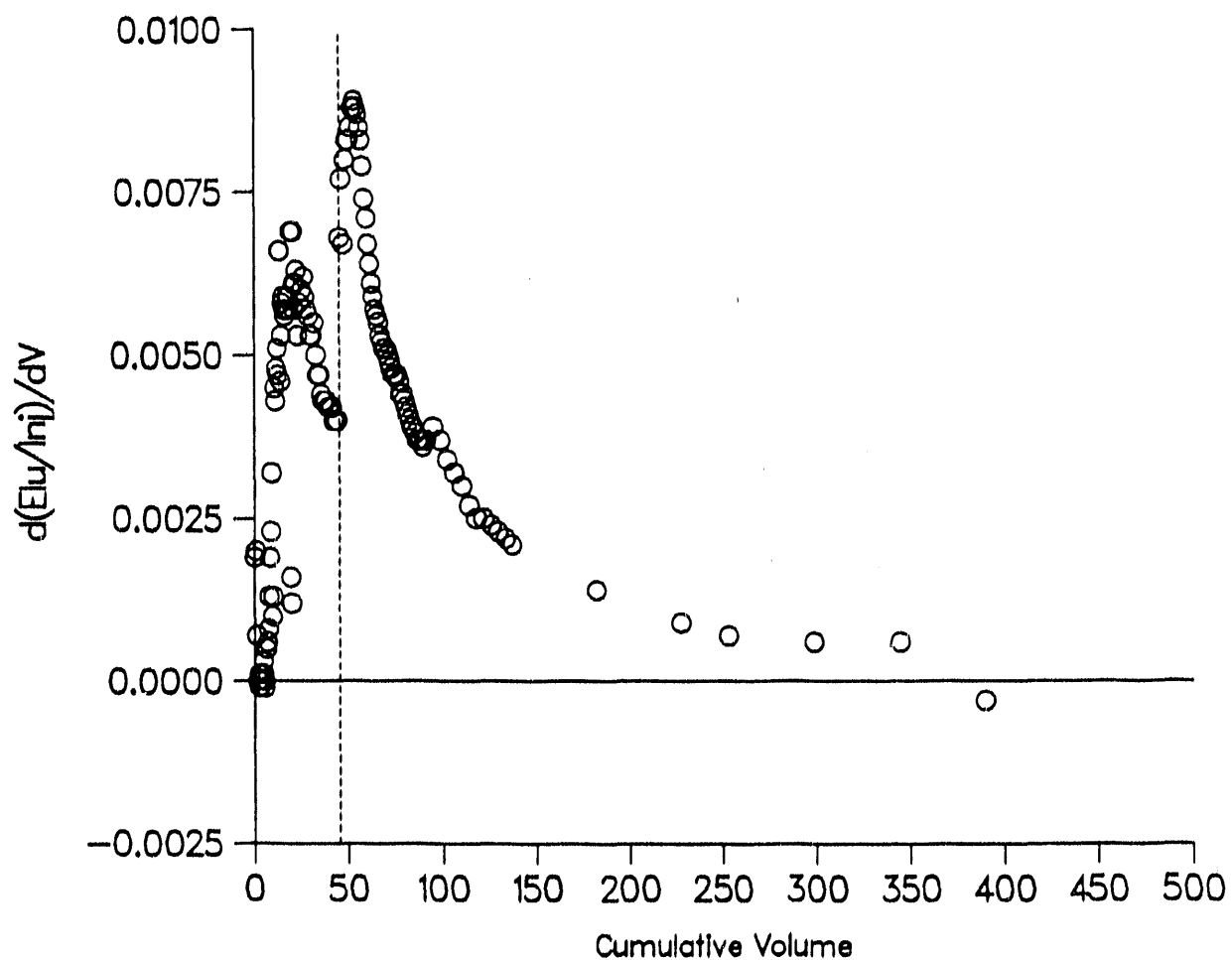


Fig. 19. Calculated rate of change for sum of relative eluted tracer from second run of pertechnetate-spiked J-13 water in Topopah Spring Member fracture network column. Data shown in Fig. 13. Dashed line indicates change to unspiked J-13 water.

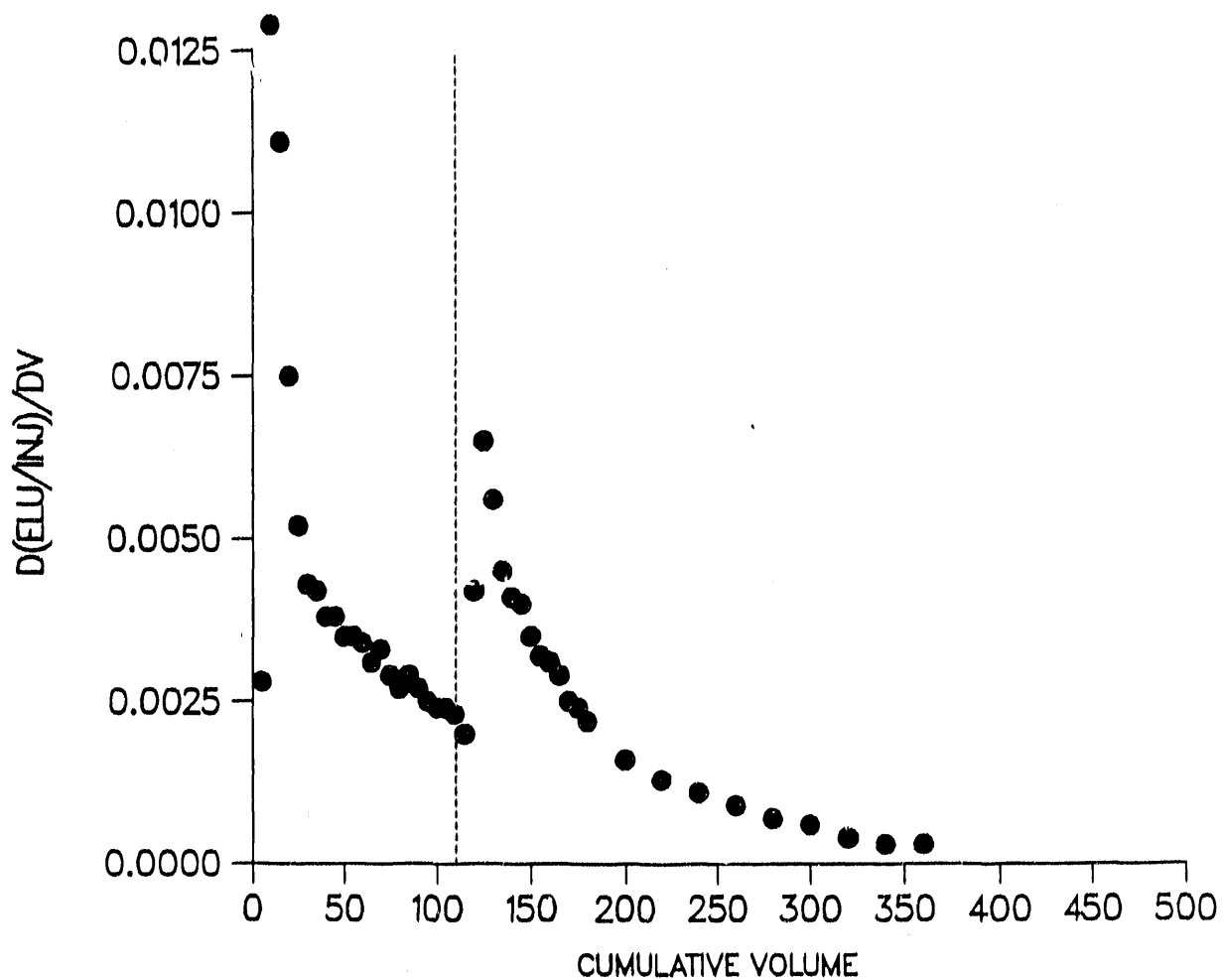


Fig. 20. Calculated rate of change for sum of relative eluted tracer from run of sulforhodamine B dye-spiked J-13 water in Topopah Spring Member fracture network column. Data shown in Fig. 14. Dashed line indicates change to unspiked J-13 water.

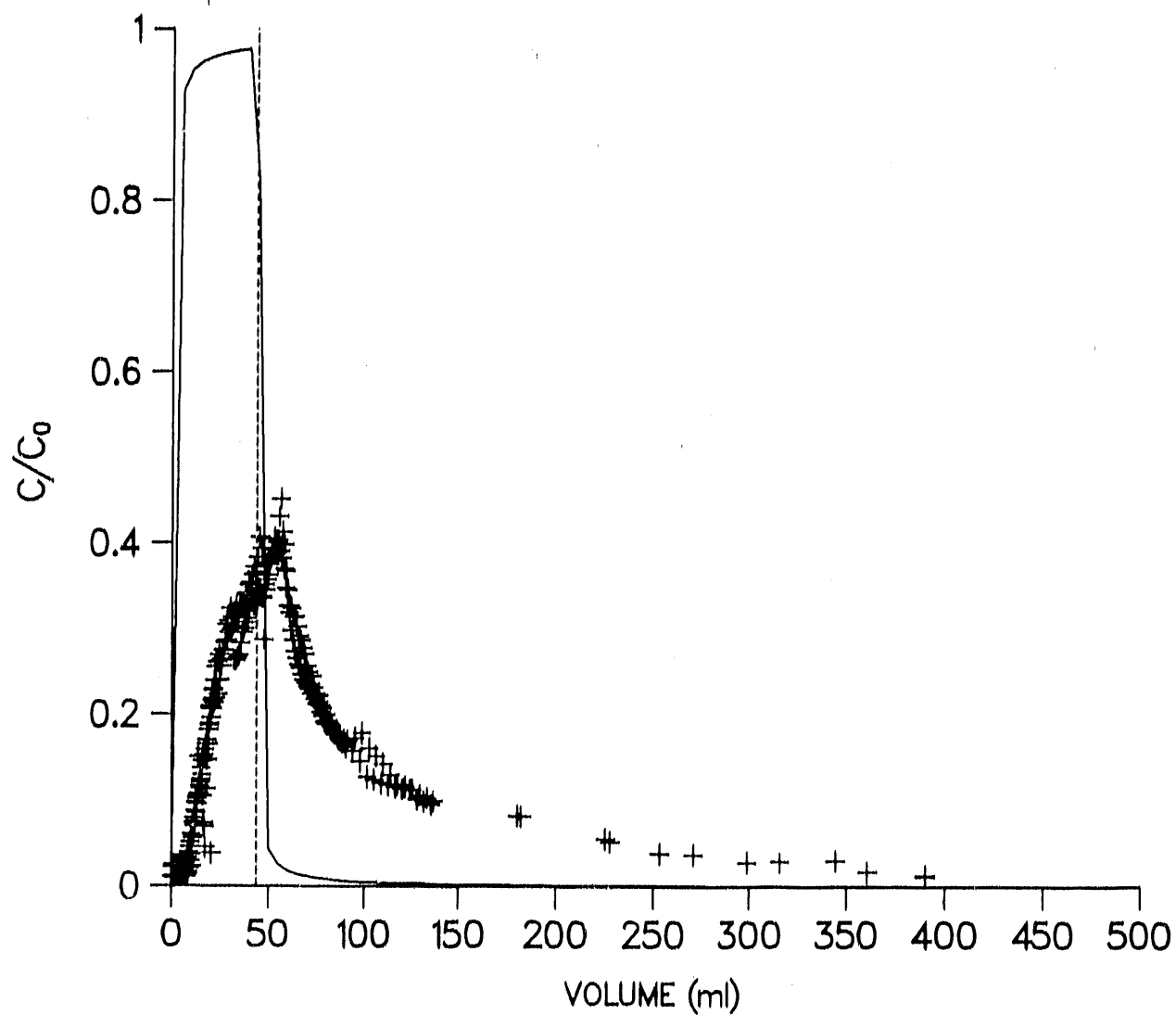


Fig. 21. Model for pertechnetate tracer elution through a single parallel-sided fracture in a porous medium uses the parameters for model 0 in Table II. Fracture aperture of 0.00592 cm was determined from head and flow rate measurements. Compare to experimental elution curves in Figs. 6 and 7. Dashed line indicates change to unspiked J-13 water.

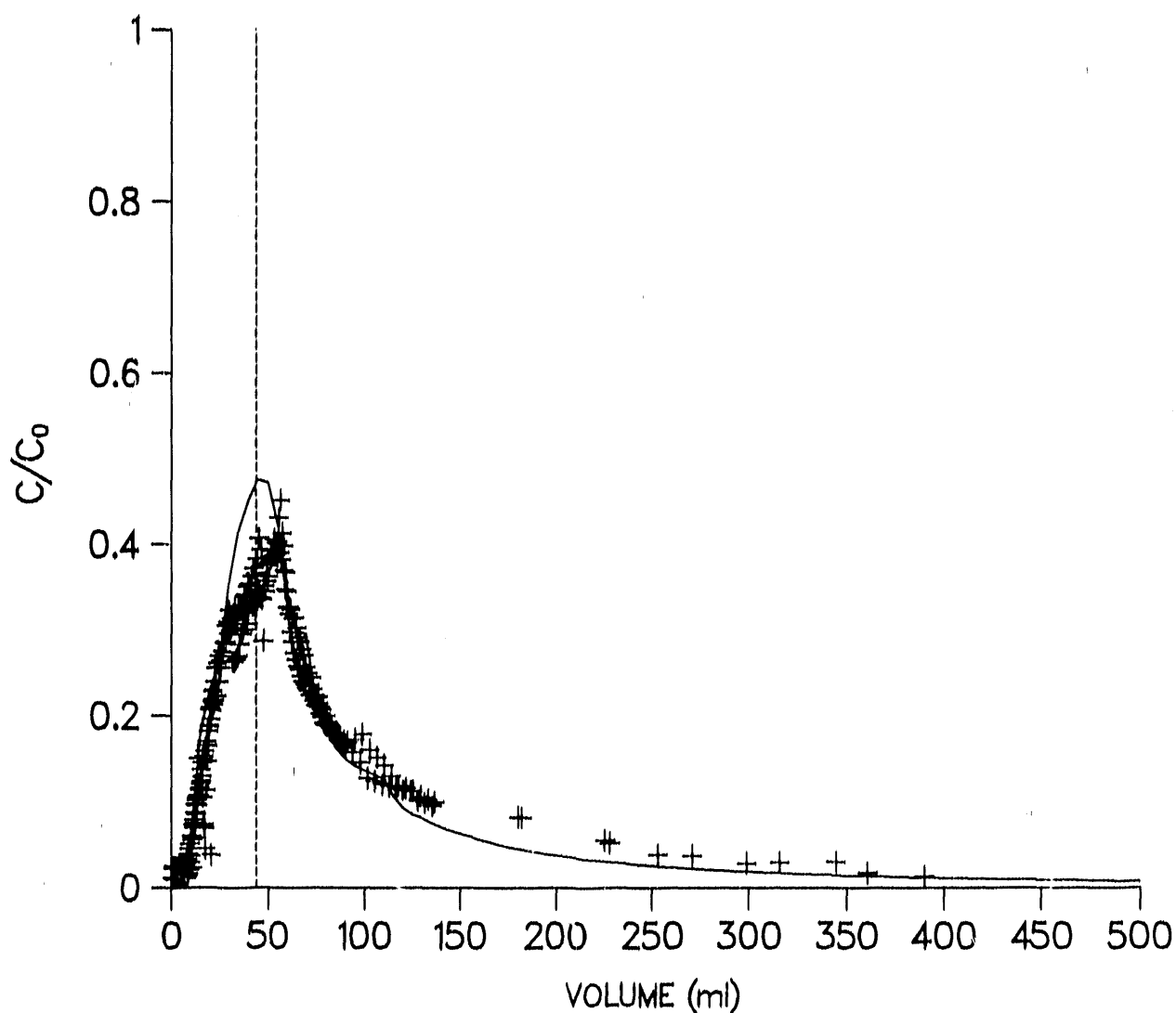


Fig. 22. Model for pertechnetate tracer elution through a single parallel-sided fracture in a porous medium uses the parameters for model 1 in Table II. Fracture aperture was set to 0.1 cm to achieve reasonable fit to experimental data (Figs. 6 and 7); compare to Fig. 21. Dashed line indicates change to unspiked J-13 water. Irregularities in elution curve shapes in these models are probably caused by inaccuracies in the numerical integration scheme used in the computer code. (Information received from R. Rundberg, Los Alamos National Laboratory, 1987.)

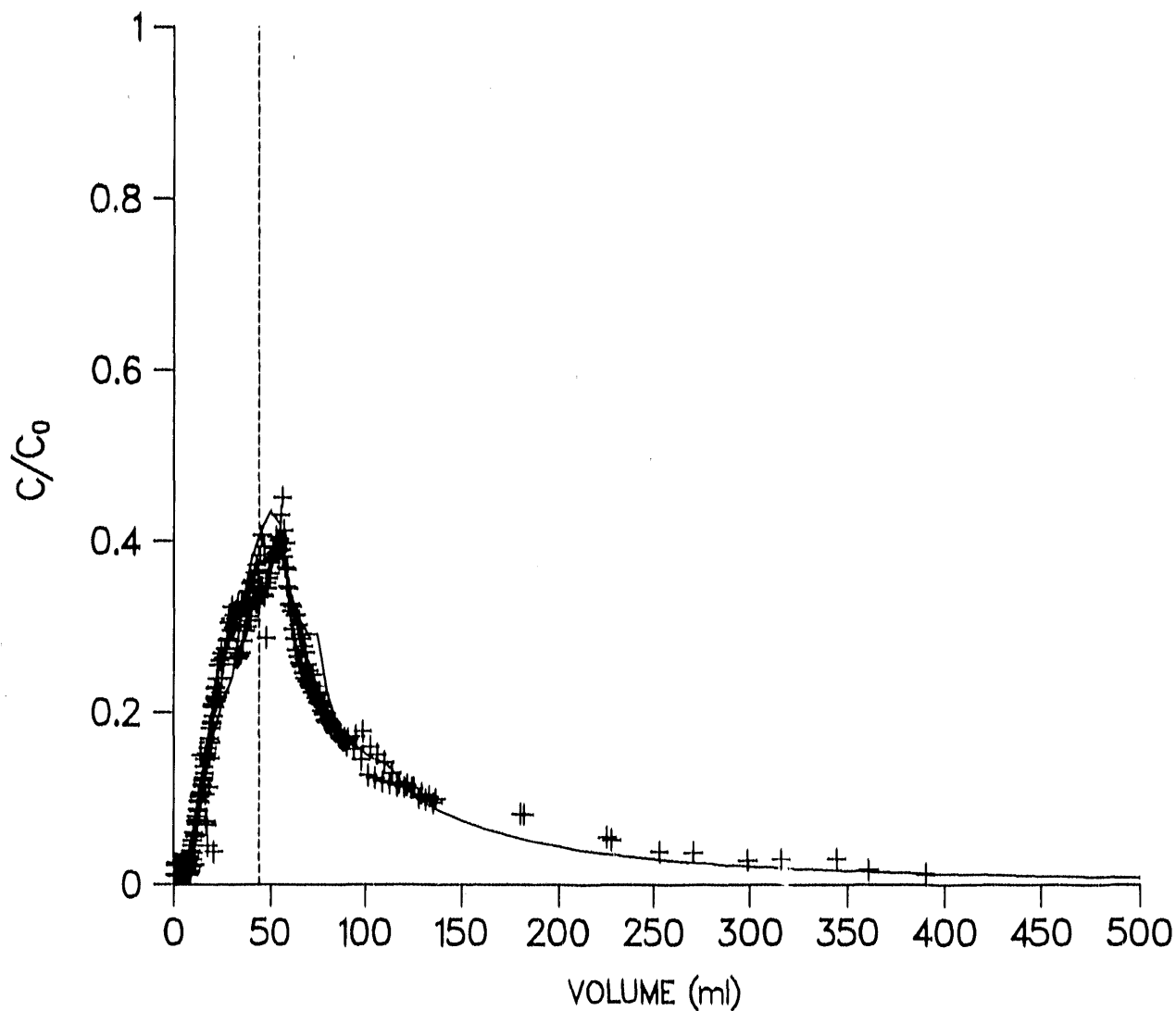


Fig. 23. Model for pertechnetate tracer elution through a single parallel-sided fracture in a porous medium uses the parameters for model 2 in Table II. Fracture aperture was set to 0.1 cm, as in Fig. 22, and dispersivity decreased from 0.003 to 0.002 to fit more closely to the experimental data (Figs. 6 and 9); compare to Fig. 21. Dashed line indicates change to unspiked J-13 water. Irregularities in elution curve shapes in these models are probably caused by inaccuracies in the numerical integration scheme used in the computer code. (Information received from R. Rundberg, Los Alamos National Laboratory, 1987.)

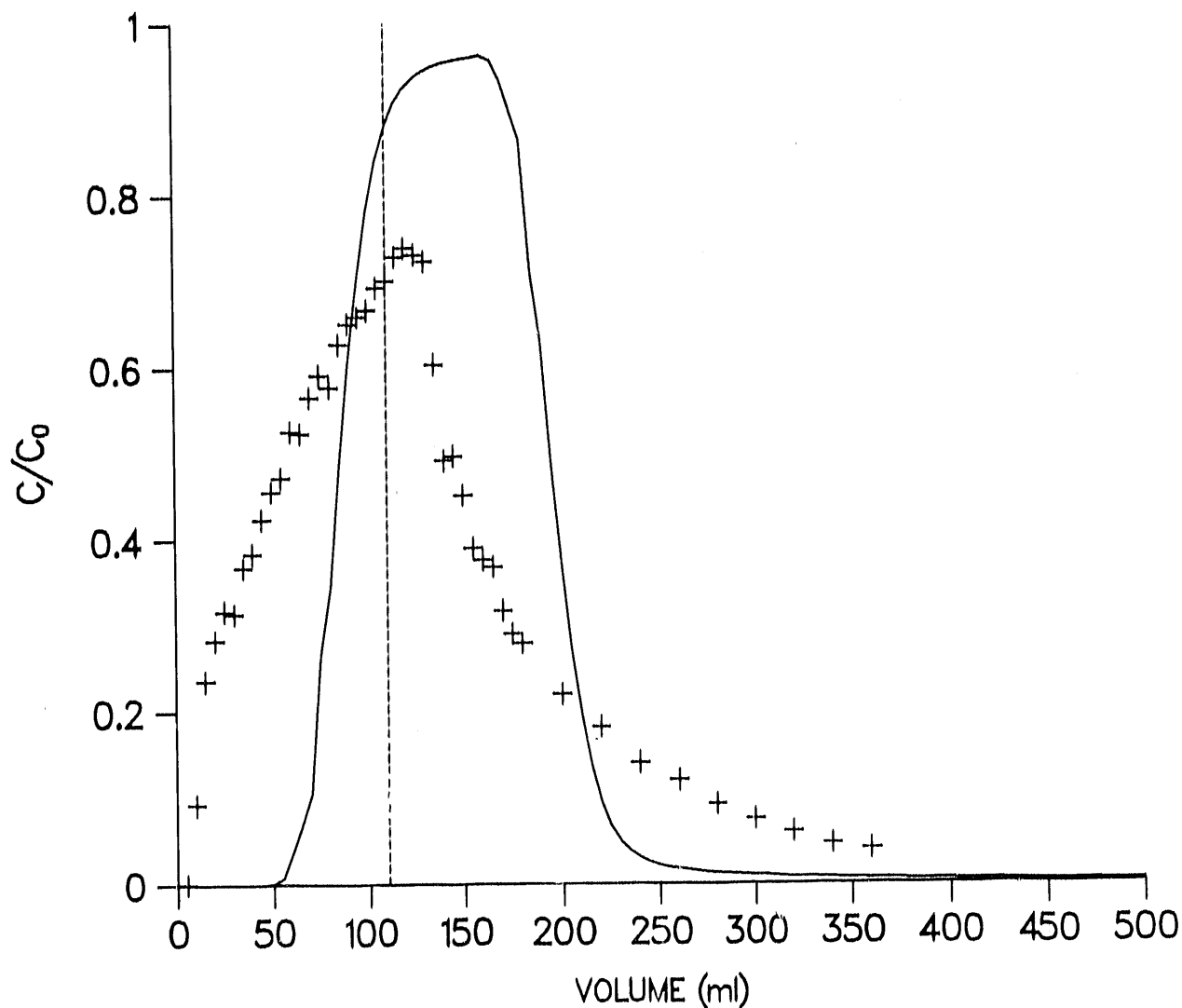


Fig. 24. Model for sulforhodamine B dye tracer elution through a single parallel-sided fracture in a porous medium uses the parameters for model 3 in Table II. Rock and fracture parameters are identical to those used in Fig. 23. Flow rate and tracer injection volume were changed to match experimental conditions (Table I and Fig. 8). Dashed line indicates change to unspiked J-13 water. Irregularities in elution curve shapes in these models are probably caused by inaccuracies in the numerical integration scheme used in the computer code. (Information received from R. Rundberg, Los Alamos National Laboratory, 1987.)

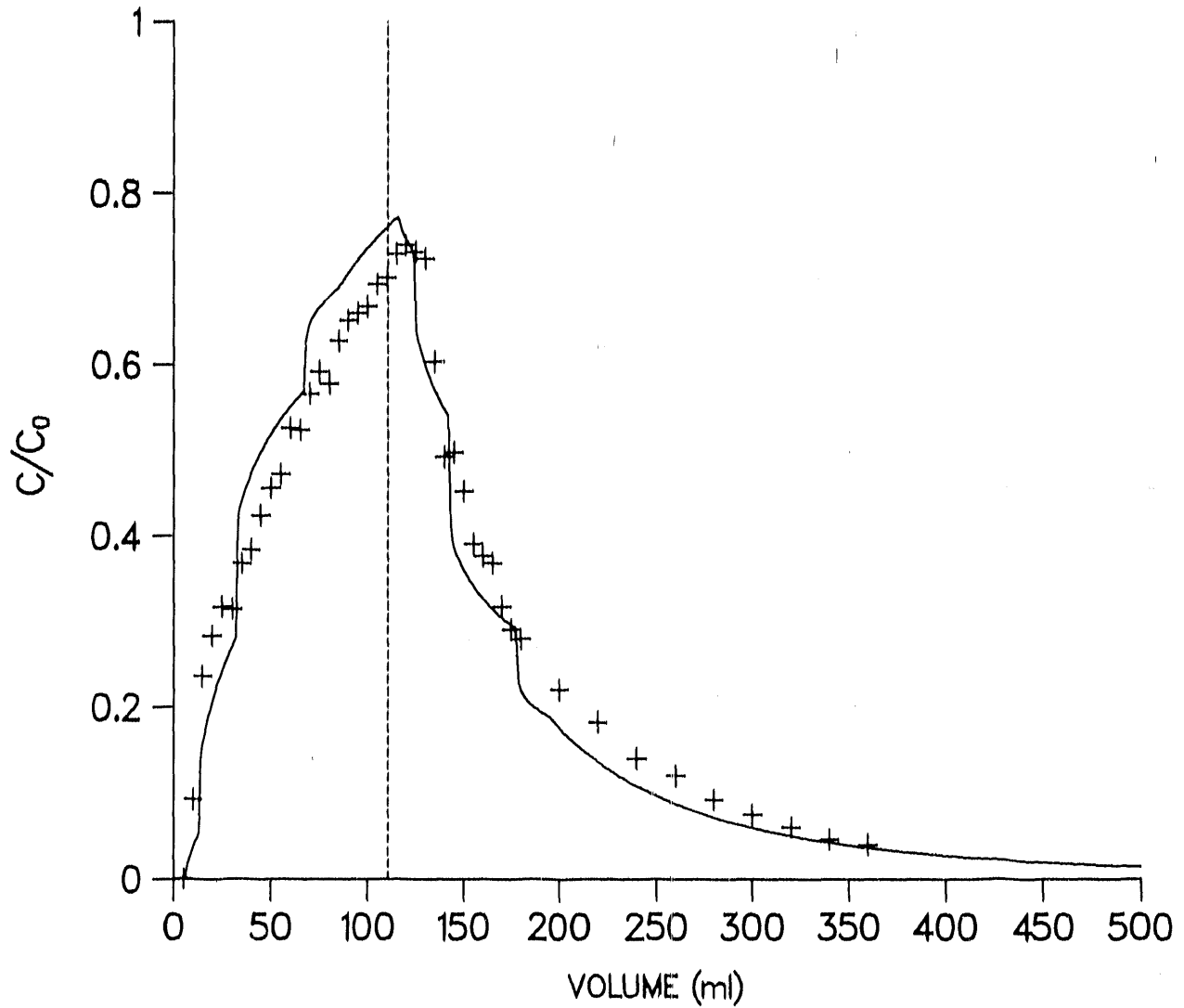


Fig. 25. Model for sulforhodamine B dye tracer elution through a single parallel-sided fracture in a porous medium uses the parameters for model 4 in Table II. Model parameters are identical to those used for Fig. 24 except that dispersivity was increased by a factor of 60 to compensate for increased flow rate; longitudinal dispersivity (Tang, 1981) is constant. Dashed line indicates change to unspiked J-13 water. Irregularities in elution curve shapes in these models are probably caused by inaccuracies in the numerical integration scheme used in the computer code. (Information received from R. Rundberg, Los Alamos National Laboratory, 1987.)

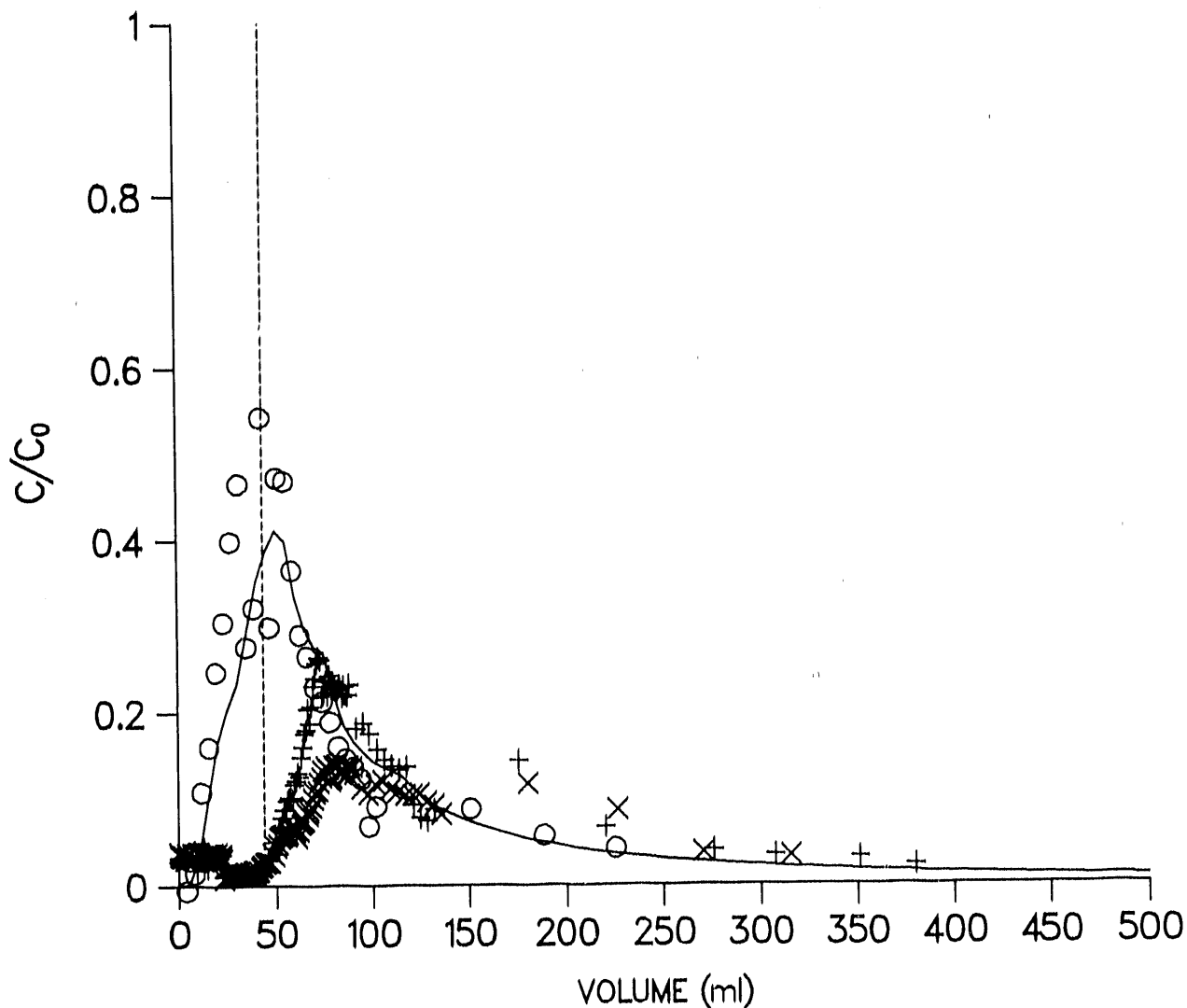


Fig. 26. Model for HTO tracer elution through a single parallel-sided fracture in a porous medium uses the parameters for model 5 in Table II. Model parameters are identical to those used for Fig. 23 except tracer diffusivity was changed to that of HTO. Dashed line indicates change to unspiked J-13 water. Irregularities in elution curve shapes in these models are probably caused by inaccuracies in the numerical integration scheme used in the computer code. (Information received from R. Rundberg, Los Alamos National Laboratory, 1987.)

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