



Piston Geometry Effects on Fuel-Air Mixture Preparation in a Light-Duty Optical Diesel Engine

Kan Zha^a, Stephen Busch^a, Xu He^b

^a Sandia National Laboratories

^b Beijing Institute of Technology

Acknowledgements:

Gurpreet Singh, Leo Breton (DOE)

Eric Kurtz (Ford)

Alok Warey, Dick Peterson (Ford)



Sandia National Laboratories

U.S. DEPARTMENT OF ENERGY
ENERGY EFFICIENCY & ENERGY
RESEARCH

Abstract

It is widely reported in the literature that for direct-injection Diesel engines, stepped-lip piston geometry exhibits fuel efficiency and emission advantages over re-entrant piston geometry at some injection timings. This observation is present both under low-load EGR-diluted Low-Temperature Combustion (LTC) and medium-load conventional diesel combustion regimes. However, the geometry-induced mechanisms for increased heat release rates and higher combustion and/or thermal efficiency is not fully understood. In order to understand the mechanism, experimental investigation of piston geometry effects on fuel-air mixture preparation is needed. This work utilizes a fuel tracer laser-induced fluorescence (LIF) technique to conduct non-intrusive near measurements of in-cylinder fuel distribution under non-combusting conditions inside a single-cylinder single-bore optical Diesel engine. In this study, two transparent piston bowls - adapting both re-entrant and stepped-lip geometry respectively - are compared. By taking area-averaged fuel fraction in a polar-coordinate fashion, the temporal and spatial trends show that stepped-lip geometry tends to reduce injected fuel on the lip shoulder, which promotes better bowl fuel stratification and may help prevent unburnt fuel from penetrating into the squish region by means of the squish flow. Further experimental and computational investigations such as high-speed imaging of in-cylinder soot natural luminance and turbulent mixing, speed/load/spray targeting sensitivities and spray targeting are needed to study the geometry-induced benefits for clean and efficient diesel combustion.

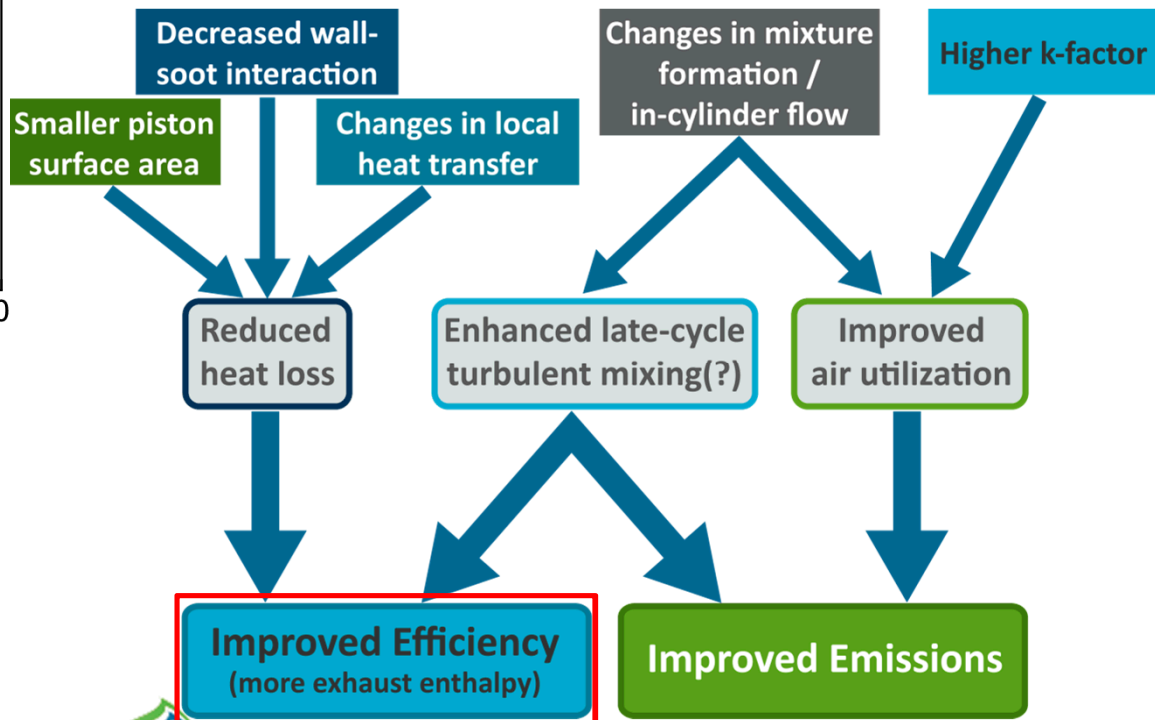
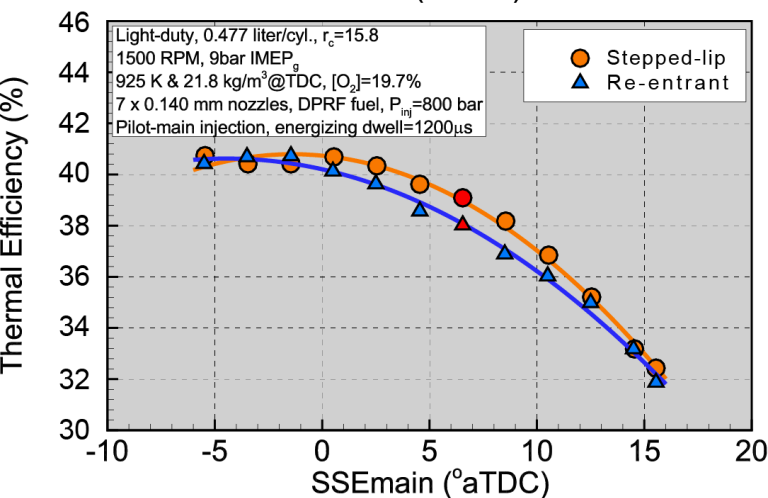
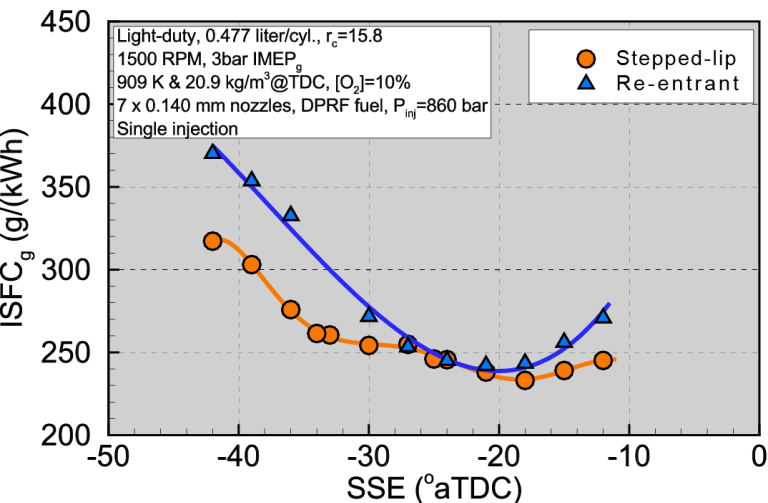


Outline

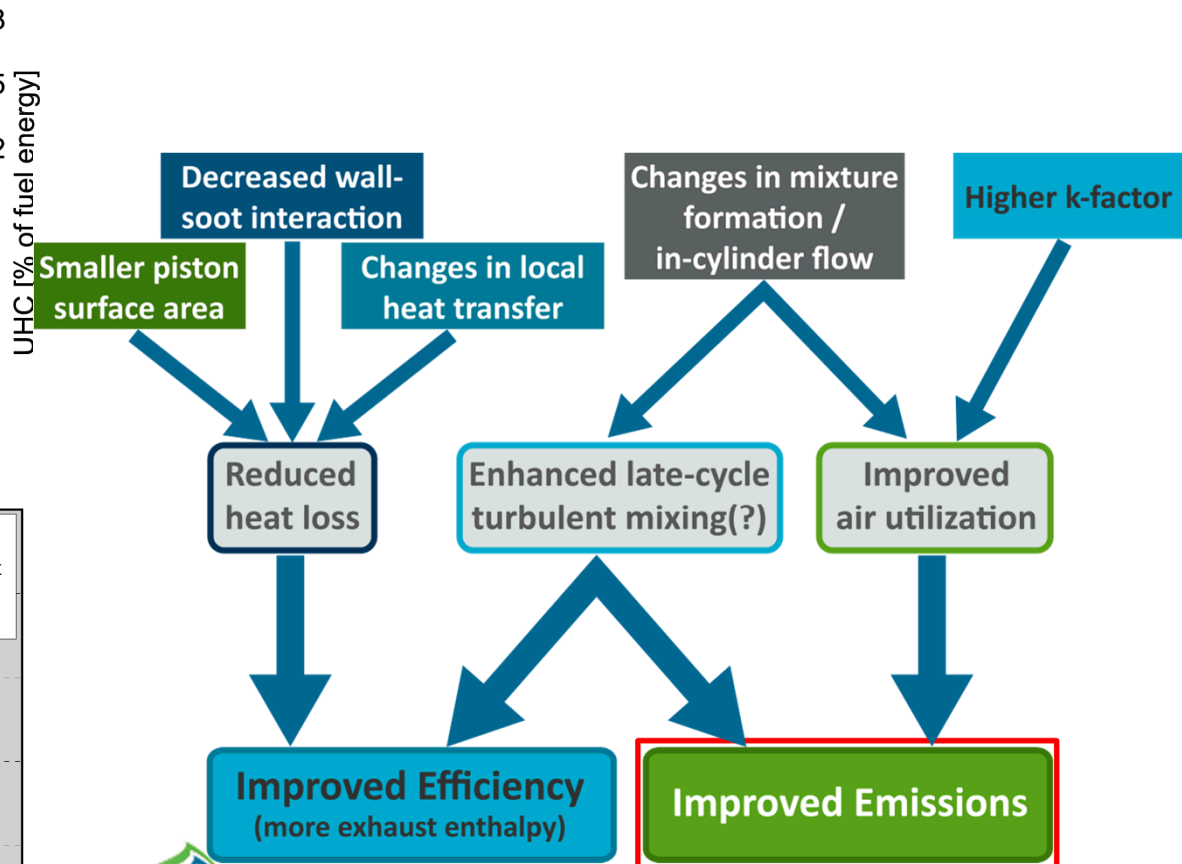
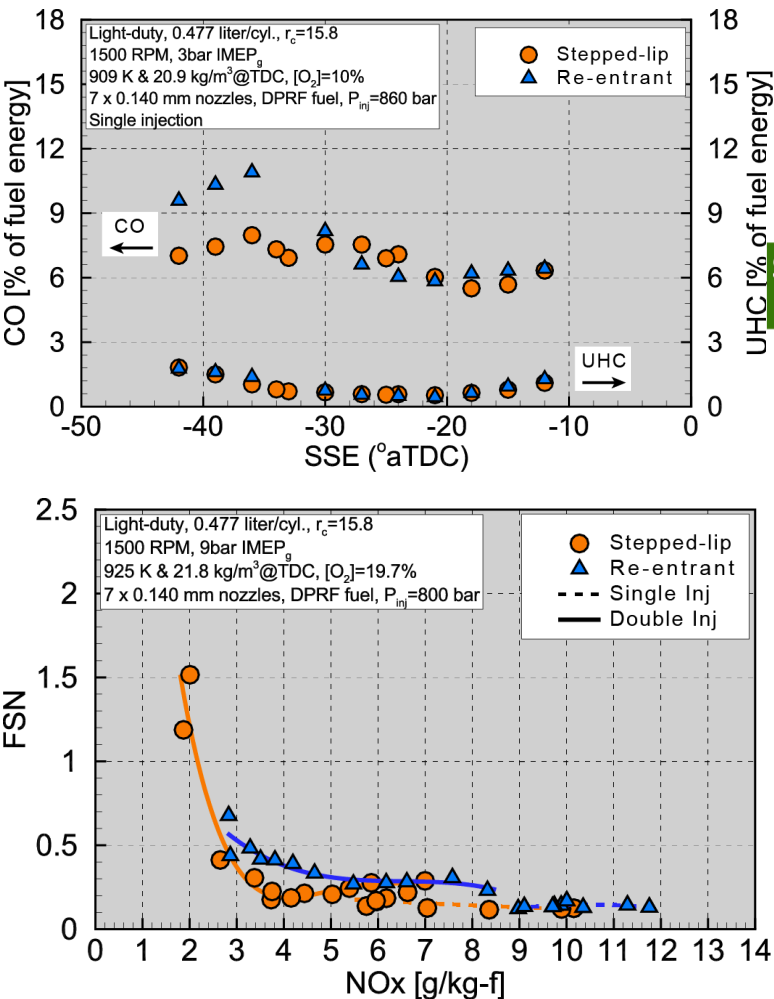
- Introduction and motivation
- PLIF experimental setup
 - SNL optical piston bowl geometries
- PLIF: data collection and processing
 - Uncertainties of PLIF measurements
- Area-averaged fuel mole fraction analysis
 - Single-injection, EGR-diluted LTC regime
 - Double-injection, conventional diesel combustion
- Conclusion



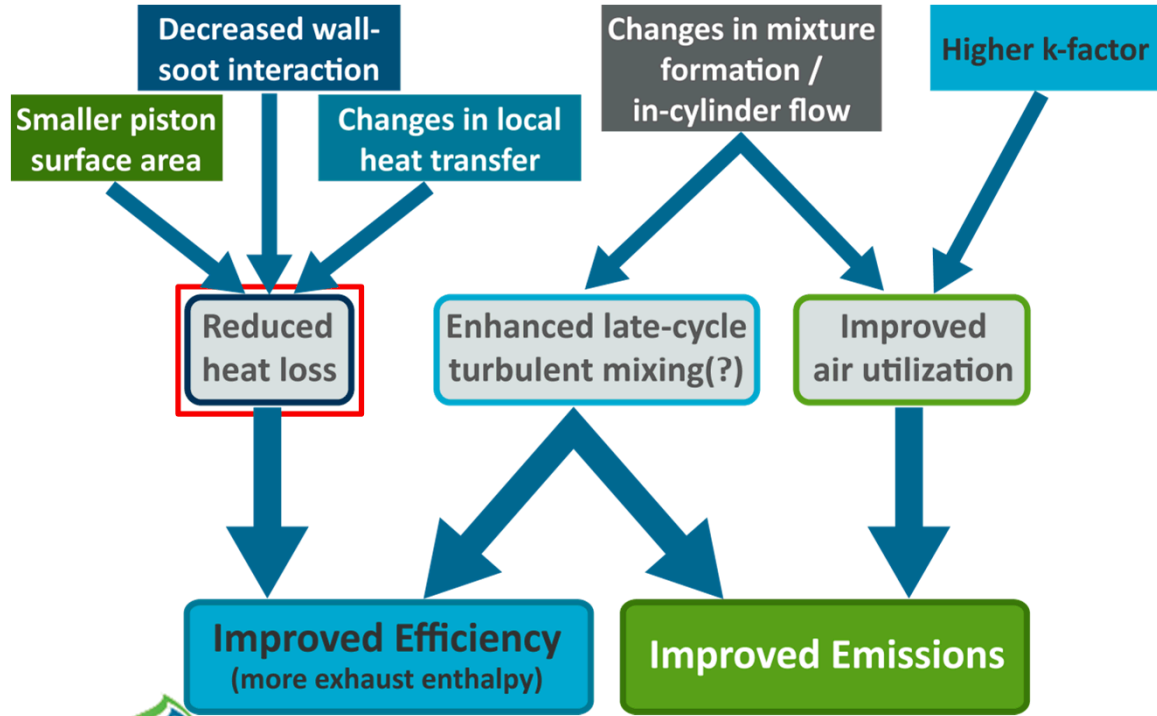
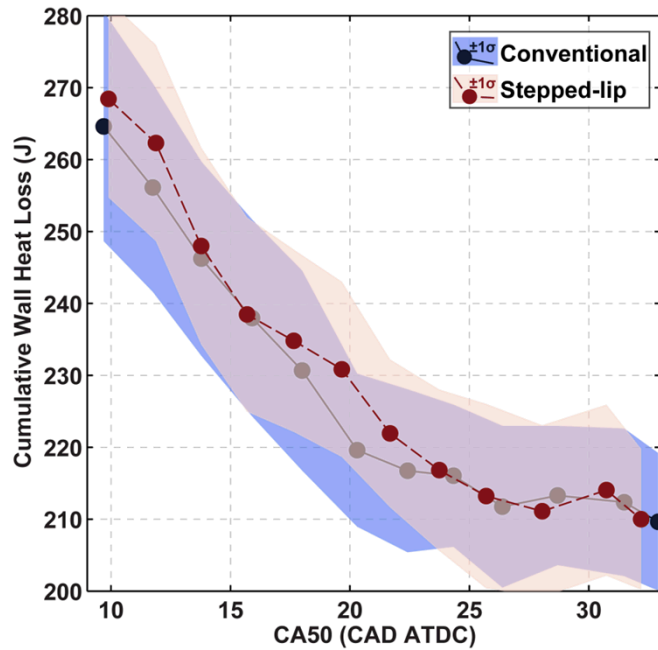
What makes the stepped-lip bowl more efficient than the conventional bowl?



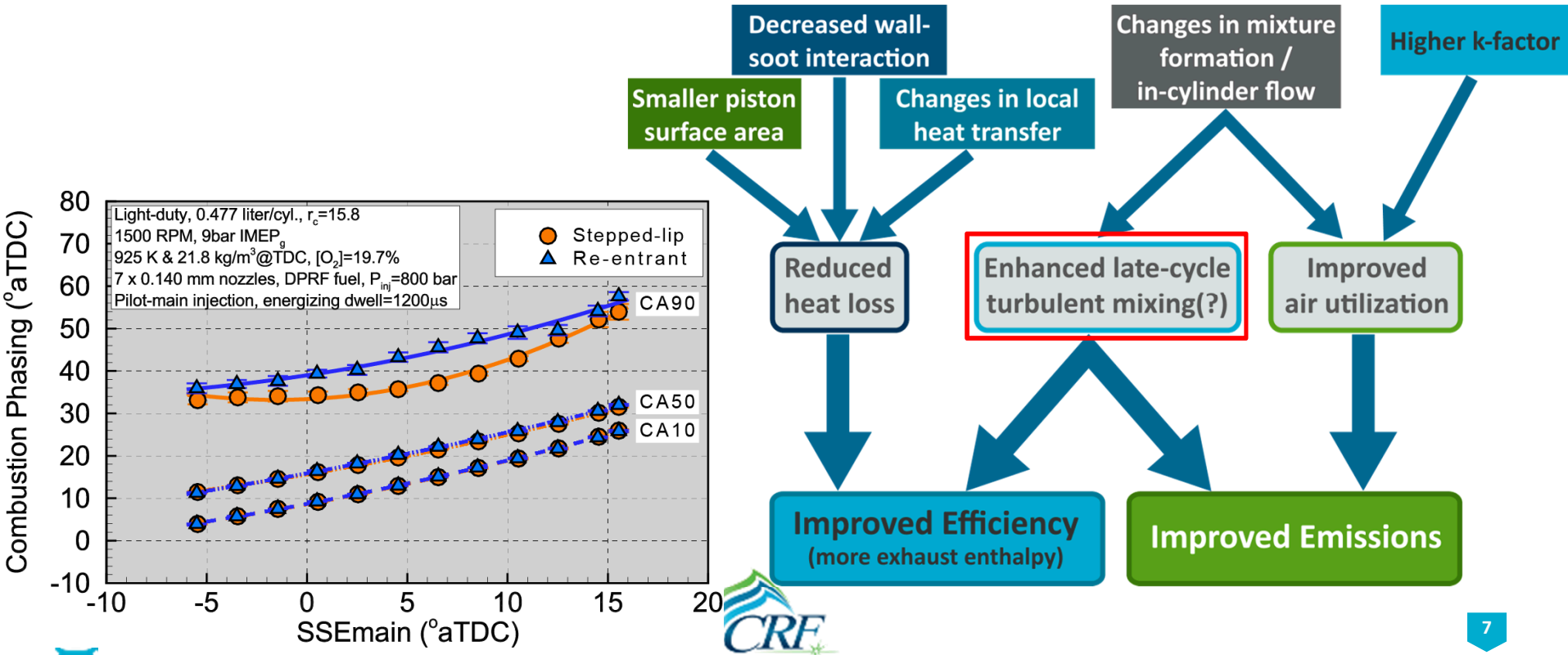
What makes the stepped-lip bowl more efficient than the conventional bowl?



“Cycle-resolved analyses do not suggest lower wall heat loss with the stepped-lip piston bowl geometry.”

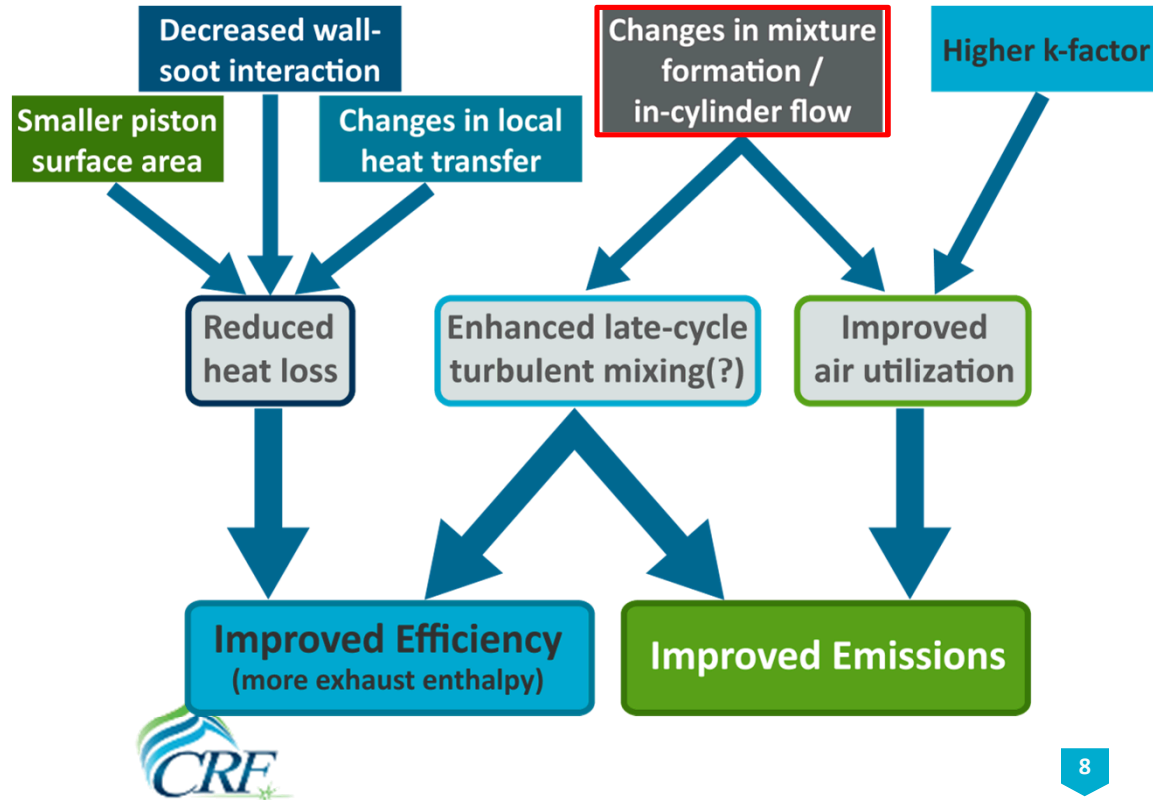


“Fuel conversion efficiency improvements with the stepped-lip piston are most closely related to enhanced late-cycle heat release rates.”



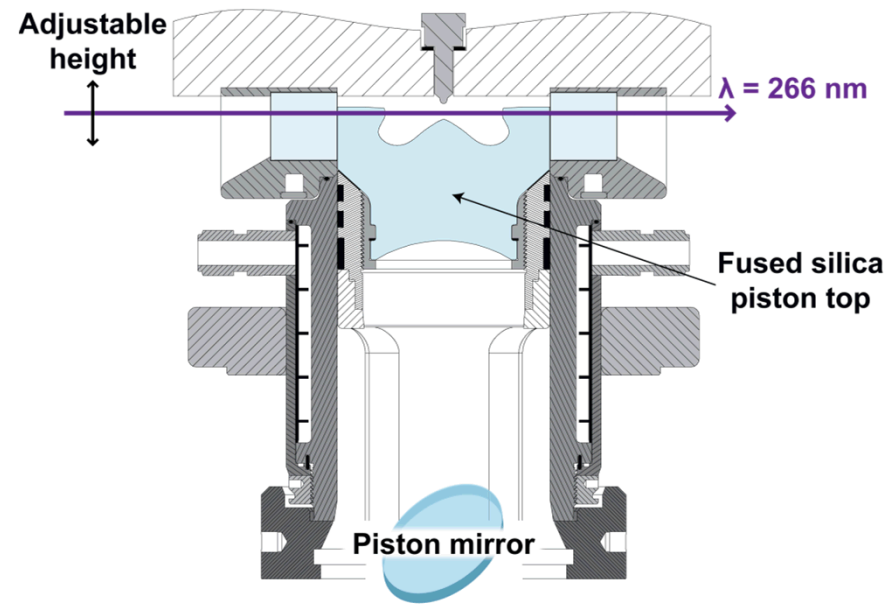
Does stepped-lip piston result in a mixture formation distribution more favorable for complete combustion and enhanced turbulent mixing?

- Does piston-induced changes in cold flow structure have big effects on mixture preparation?
- What is the role of squish flow?
- Spray-piston interaction?



PLIF Experiments in the SNL 0.48L light-duty single-cylinder optical engine

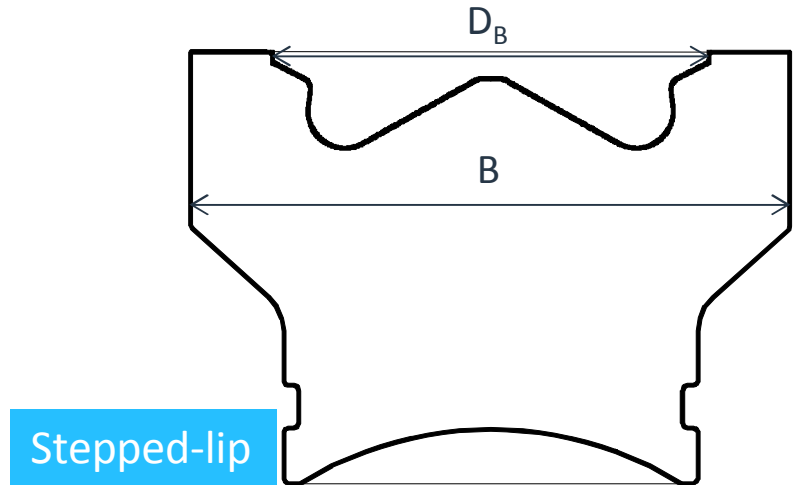
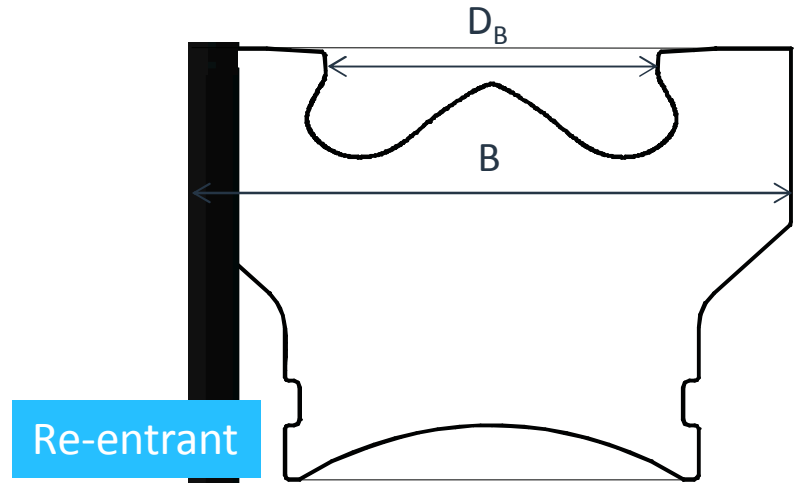
- Engine operation
 - 1500 rpm
 - Non-combusting, 0% O_2
 - Fuel: 42 vol% n-hexadecane + 58 vol% heptamethylnonane
 - Tracer: 0.5 weight% ethylhexyl naphthalene
 - Swirl ratio: 2.5
- Illumination
 - Laser: Nd:YAG Harmonic (266 nm)
 - Energy: 10 mJ/pulse (relative to full power, measured each shot)
 - Laser sheet thickness: 2 mm
- Imaging
 - Cameras: 4 ICCD cameras
 - Nikon UV-100
 - Wavelength: 266 nm



Bore x stroke	82 mm x 90.4 mm
Compression ratio	15.8:1
Valves	4
Injector type	Solenoid
Holes	7 x 139 μm
ks	1.5/86
Included Angle	149°

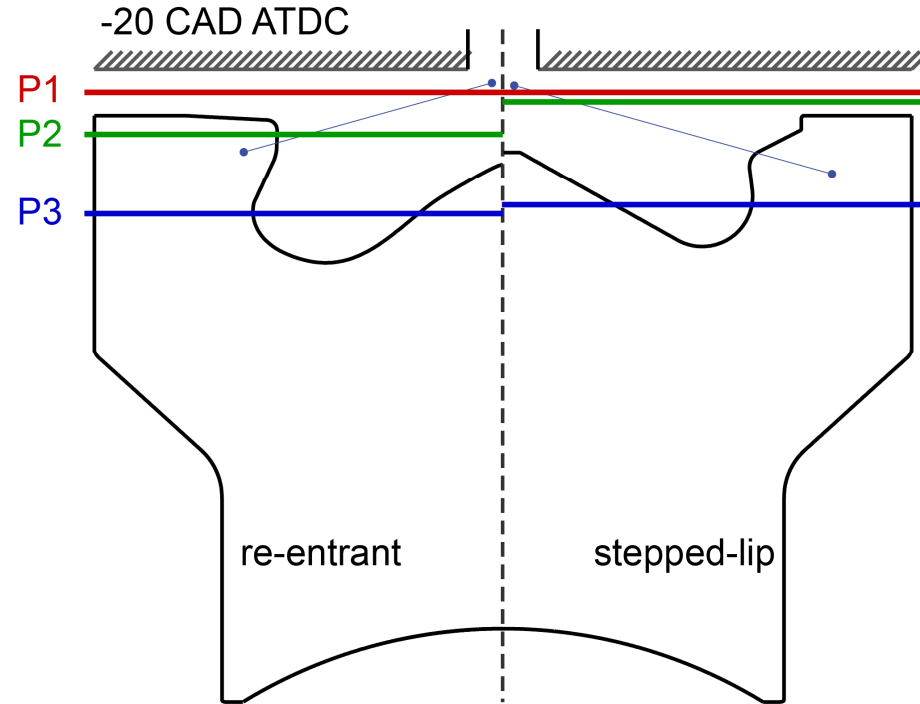
SNL optical piston bowl geometries

- Two quartz pistons have identical:
 - Bowl volume = 0.028 L
 - Squish height = 1.35 mm
 - Compression ratio = 15
 - No valve cut-outs
- Different bowl geometries result in different bowl-to-bore ratios
 - For stepped-lip: $D_B/B=0.55$
 - For re-entrant: $D_B/B=0.73$
- The surface area of stepped-lip bowl is 40% less than for re-entrant bowl
- Initial turbulence generation is sensitive on recommendations from designers



PLIF setup: laser plane locations

- Plane 1 (P1) is set half of squish height
- Plane 2 (P2) is empirically determined
 - Re-entrant: at rim of bowl where laser sheet passes through with minimum obstruction
 - Stepped-lip: 1.37 times the bowl height above the piston top
- Plane 3 (P3) is set deep within the bowl
 - Re-entrant: 9.88 mm below the piston top
 - Stepped-lip: 8.98 mm below the piston top
- P2 and P3 are adjusted with the piston crank angles.



PLIF: data collection and processing

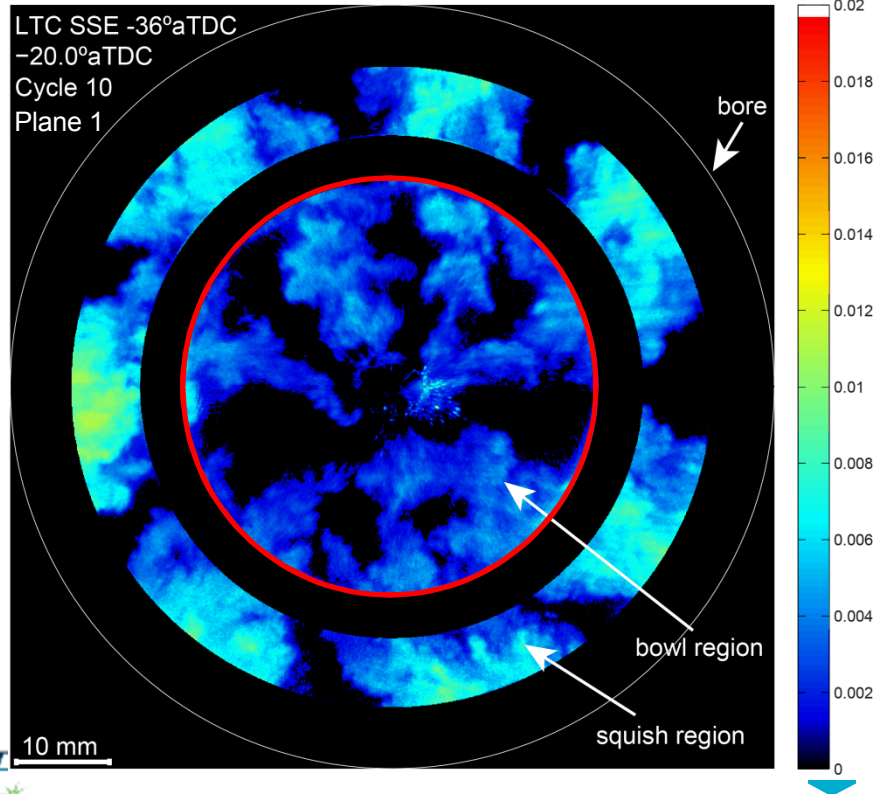
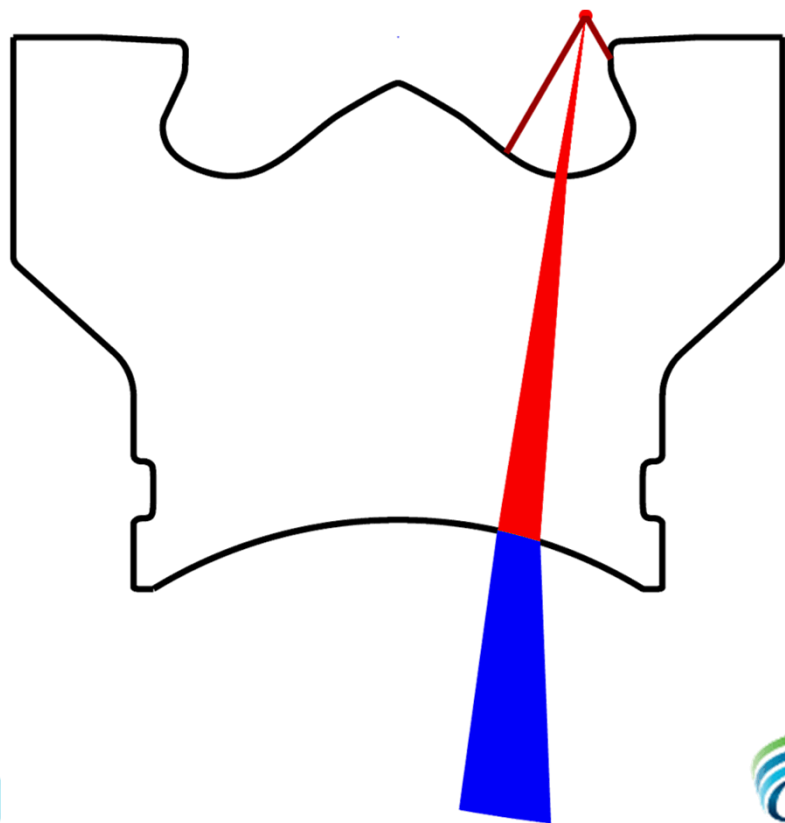
- Three sets of images for a given crank angle, plane, and operating point (51 images per set)
 - Background (no fuel injection)
 - Flat-field (6/8 injections in intake stroke)
 - Fuel injection image (desired operating point)
 - Fuel injection Image sets taken over range starting from injection ending prior to SOC.
- 9:15min's measurement schedule to maintain temperatures and pressures
- Distortion correction according to established ray-tracing routine

$$\chi_{fuel,d} = \chi_{fuel,cal} \frac{S_d}{S_{cal}} \frac{E_{cal}}{E_d} \frac{T_d}{T_{cal}} \frac{P_{cal}}{P_d} \frac{\sigma\eta(T_{cal})}{\sigma\eta(T_d)}$$

- $\chi_{fuel,d} = (\text{moles nC16H34} + \text{moles iC16H34} + \text{moles 1MN}) / (\text{total moles of CO}_2, \text{N}_2, \text{nC16H34, iC16H34, and 1MN}).$

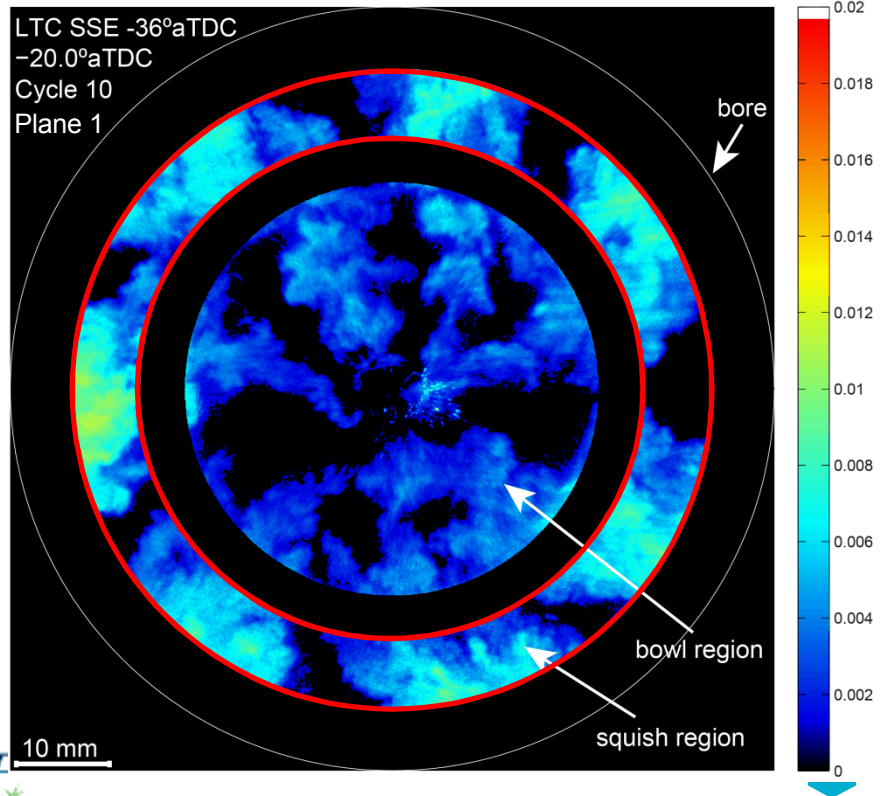
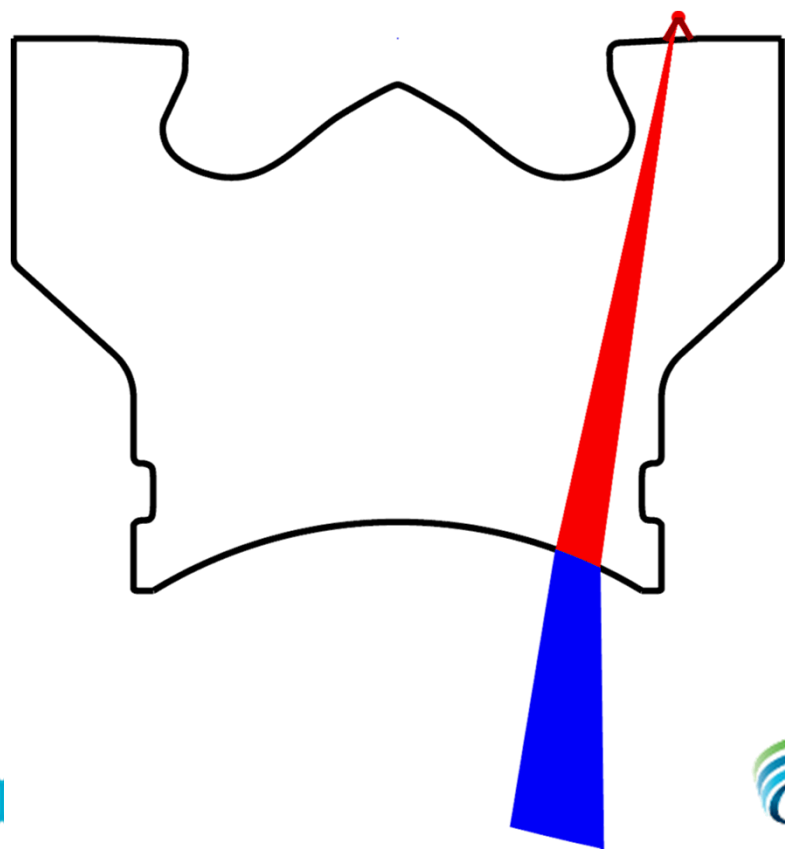
A sample of dewarped PLIF images with re-entrant geometry

Re-entrant Bowl

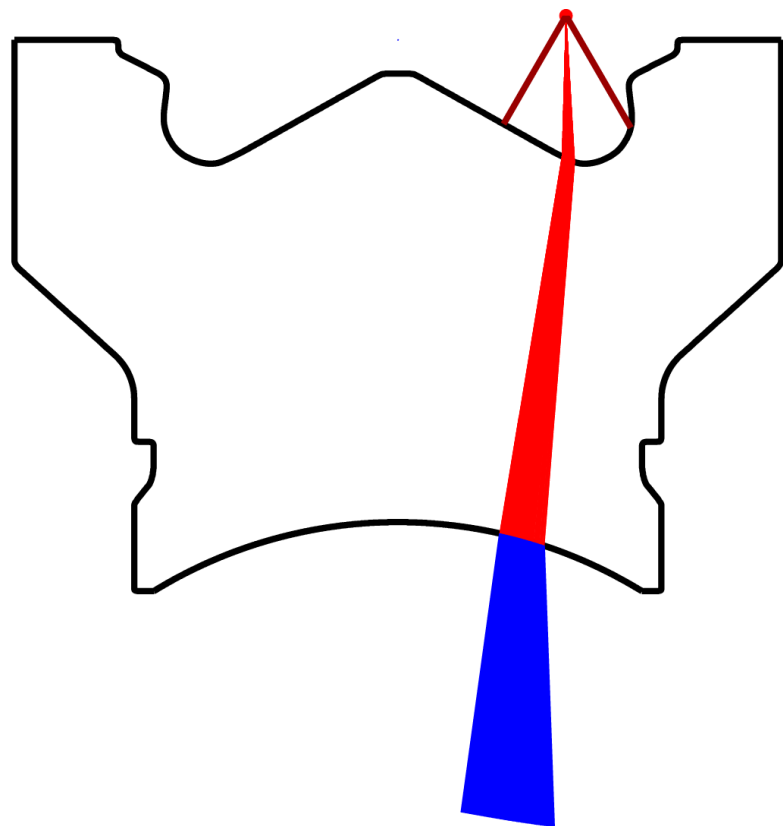


A sample of dewarped PLIF images with re-entrant geometry

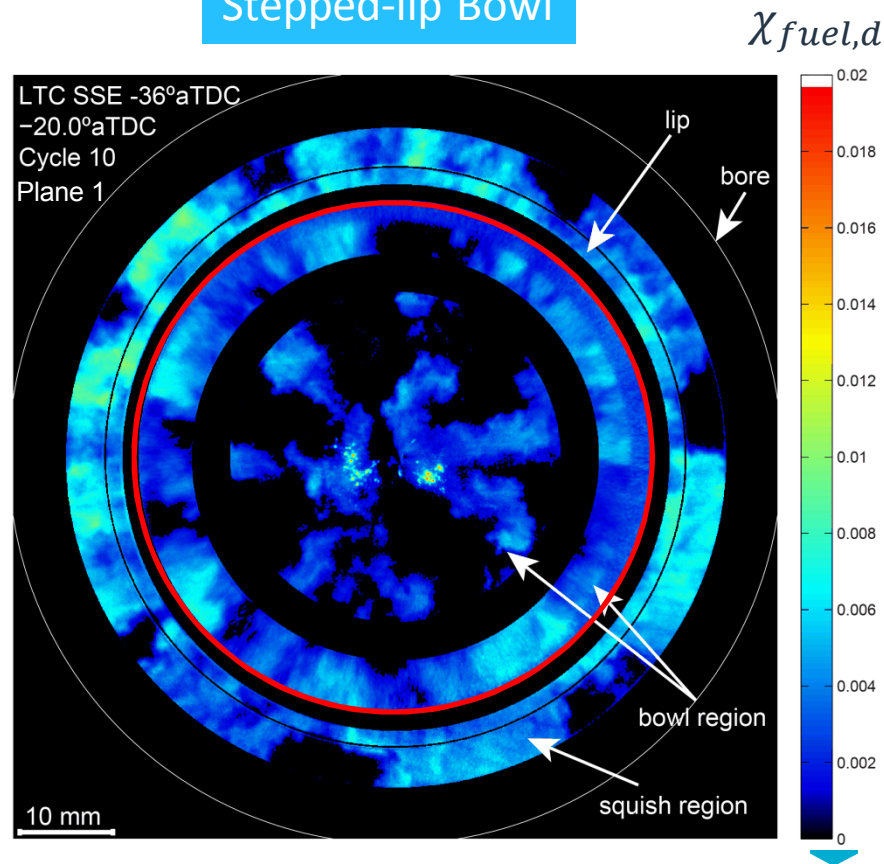
Re-entrant Bowl



A sample of dewarped PLIF images with stepped-lip geometry

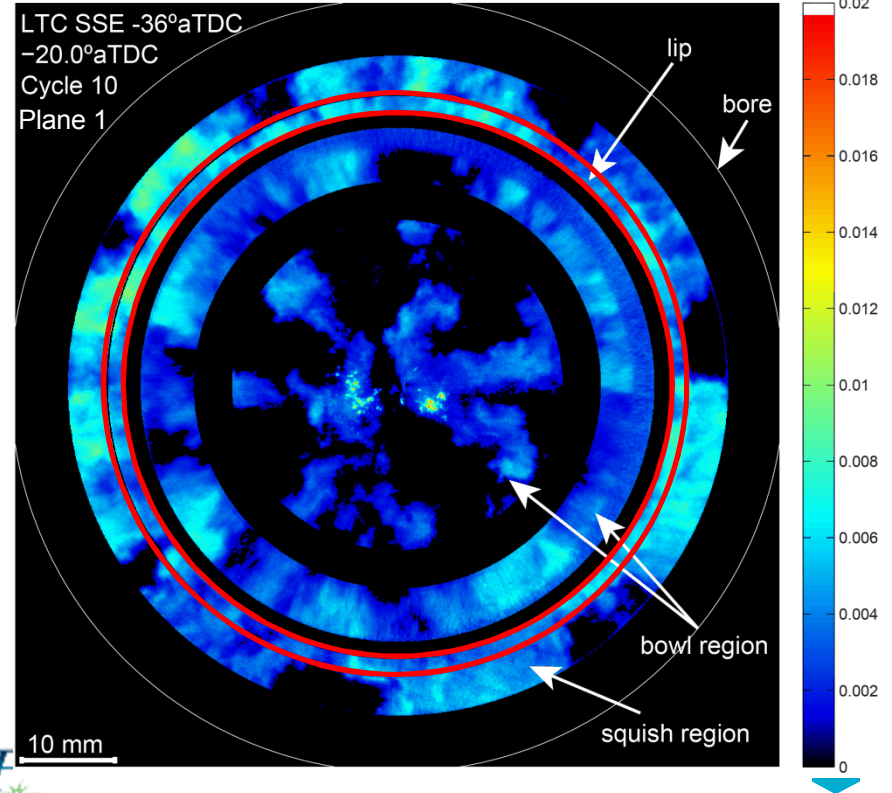
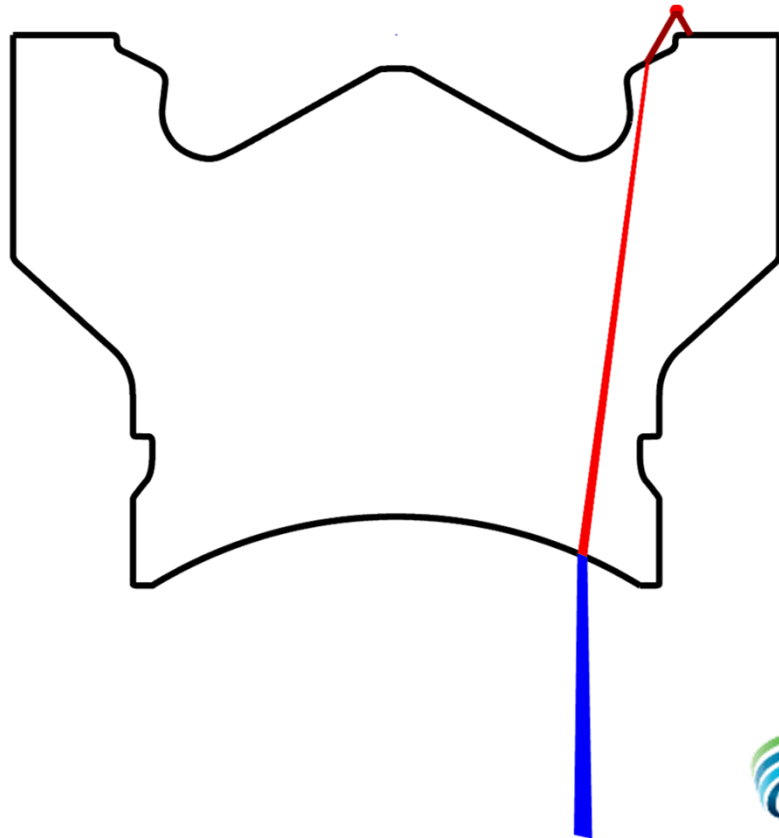


Stepped-lip Bowl



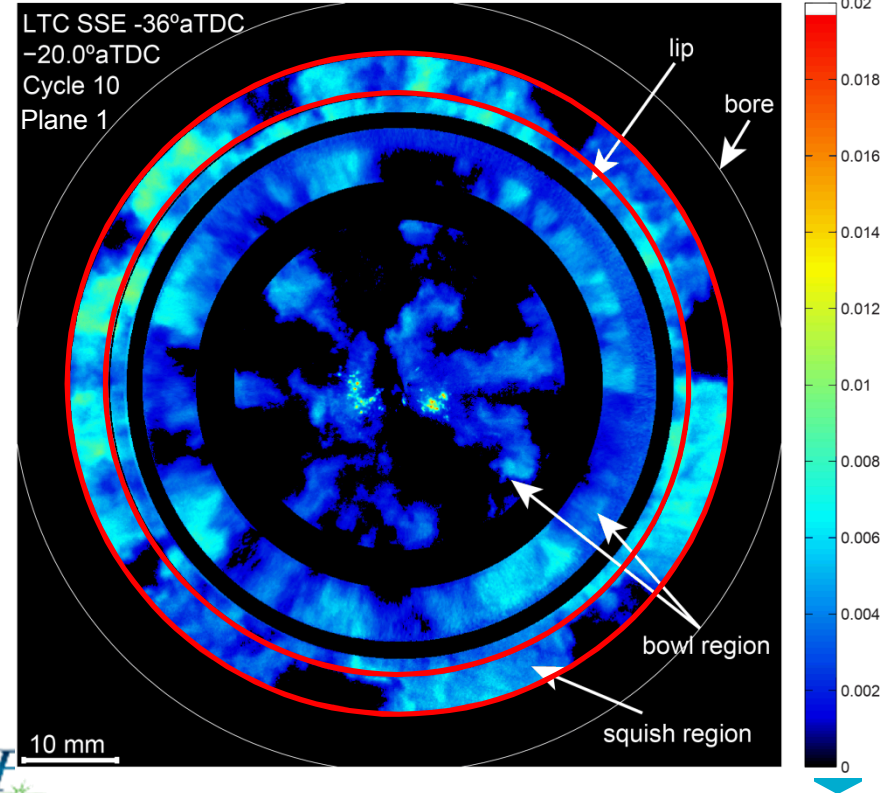
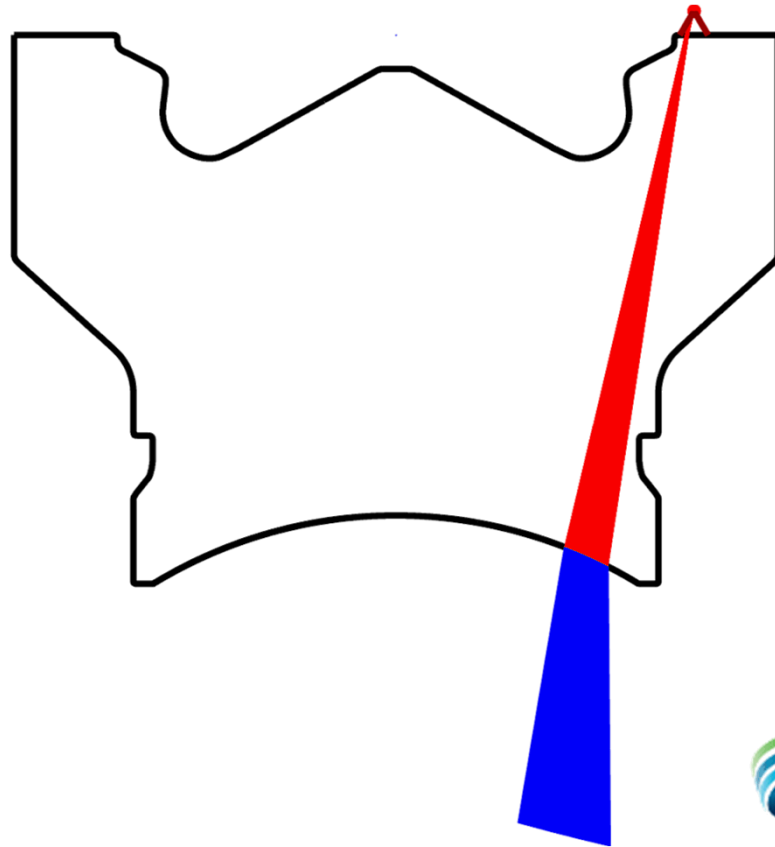
A sample of dewarped PLIF images with stepped-lip geometry

Stepped-lip Bowl



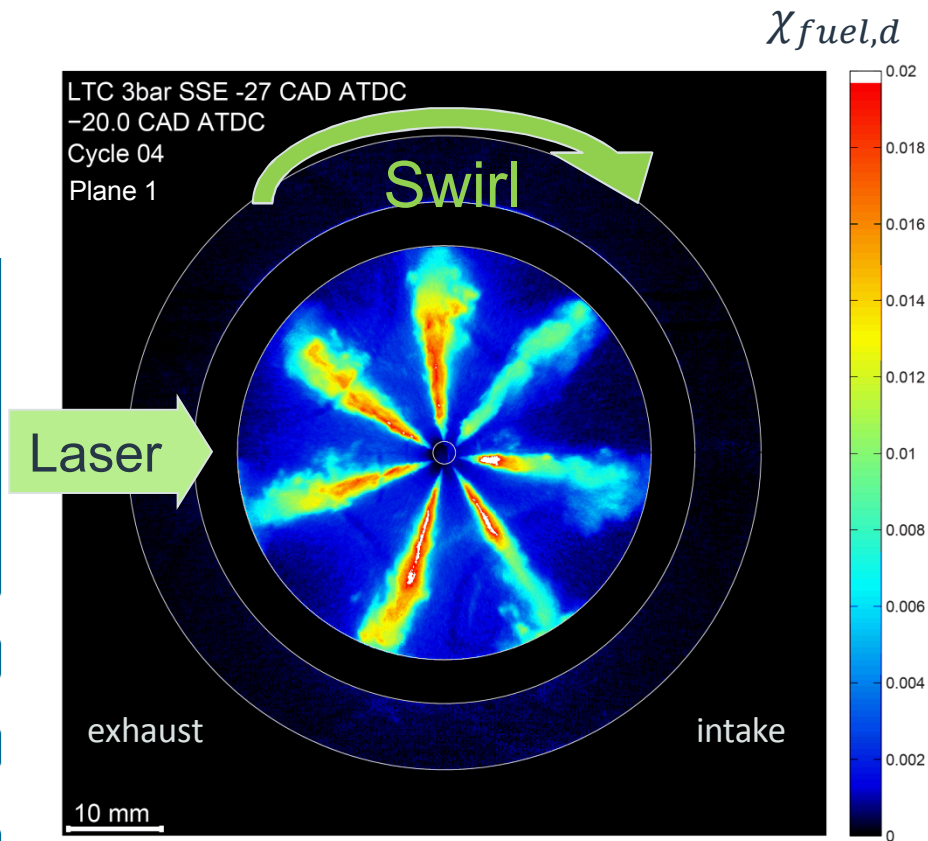
A sample of dewarped PLIF images with stepped-lip geometry

Stepped-lip Bowl



Uncertainties of PLIF measurements

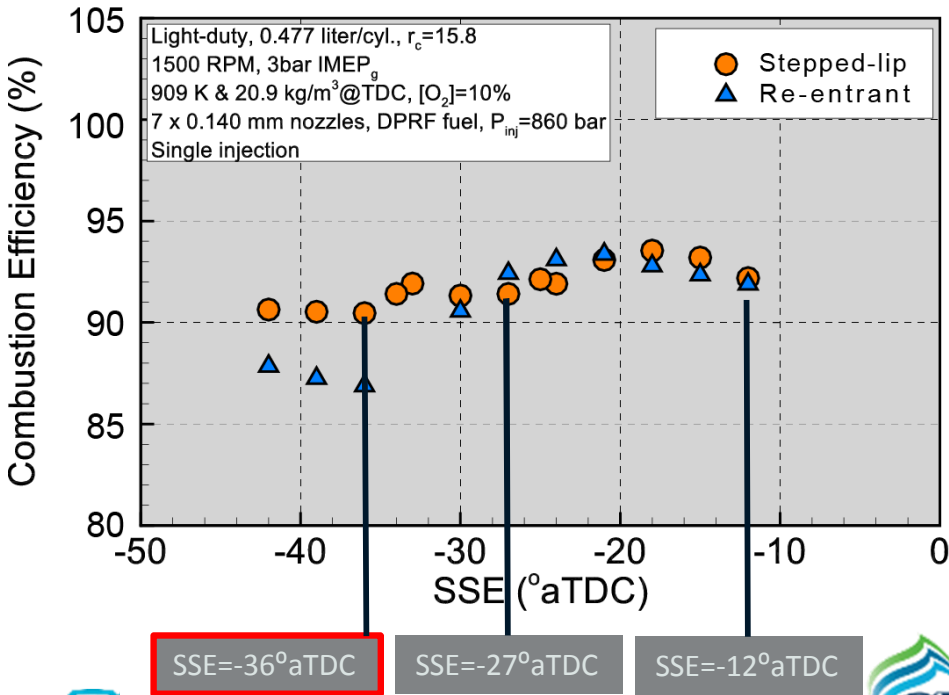
- Dewarping-induced error in radial locations: measurements near chamber center ($R \sim 7\text{mm}$) is not reliable.
- Camera nonlinearity at high intensities.
- Beam steering effects still show up in squish region when piston is in ± 15 CAD around TDC.
- Plumes facing incoming laser produce more measurements.
- Shadow caused by cylinder wall interference.
- Out-of-plane fluorescence from liquid brought by laser and background reflection.
- Fluorescence from light on chamber surface.



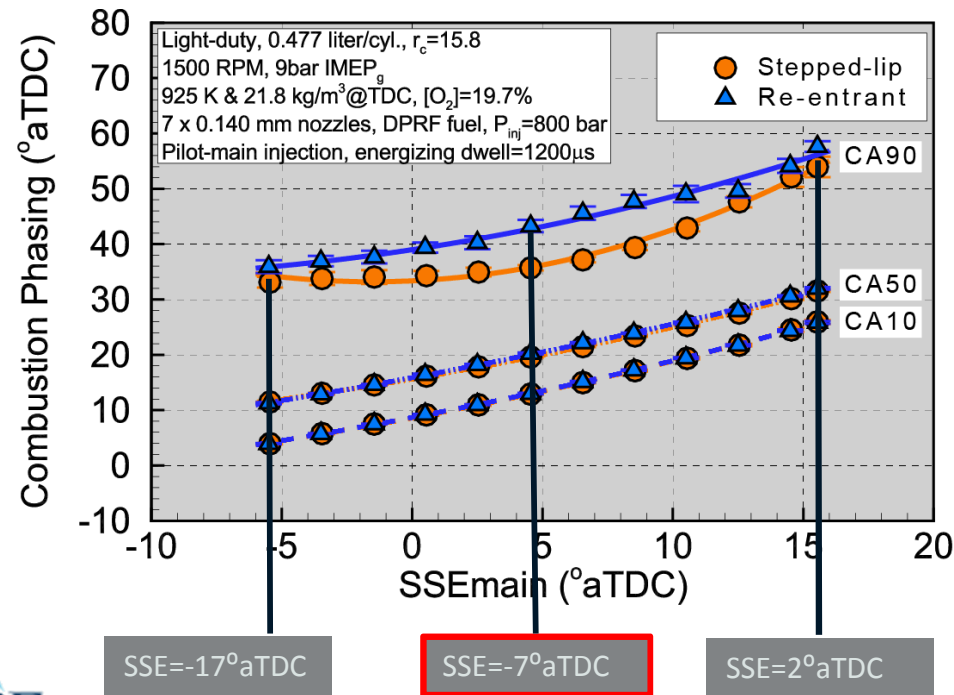
	CAD ATDC																							
	-26	-25	-24	-23	-22	-21	-20	-19	-18	-17	-16	-15	-14	-13	-12	-11	-10	-9	-8	-7	-6	-5	...	27
Images																								
Injection																								
Combustion																								

Points of interest for optical investigation

Single-injection, EGR-diluted LTC regime

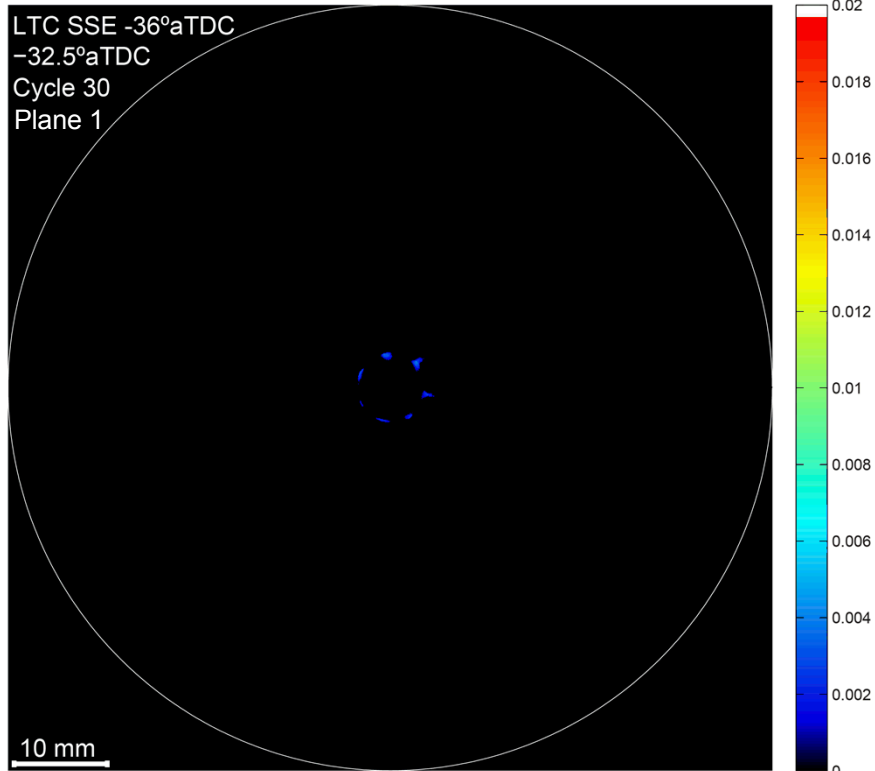


Double-injection, conventional combustion

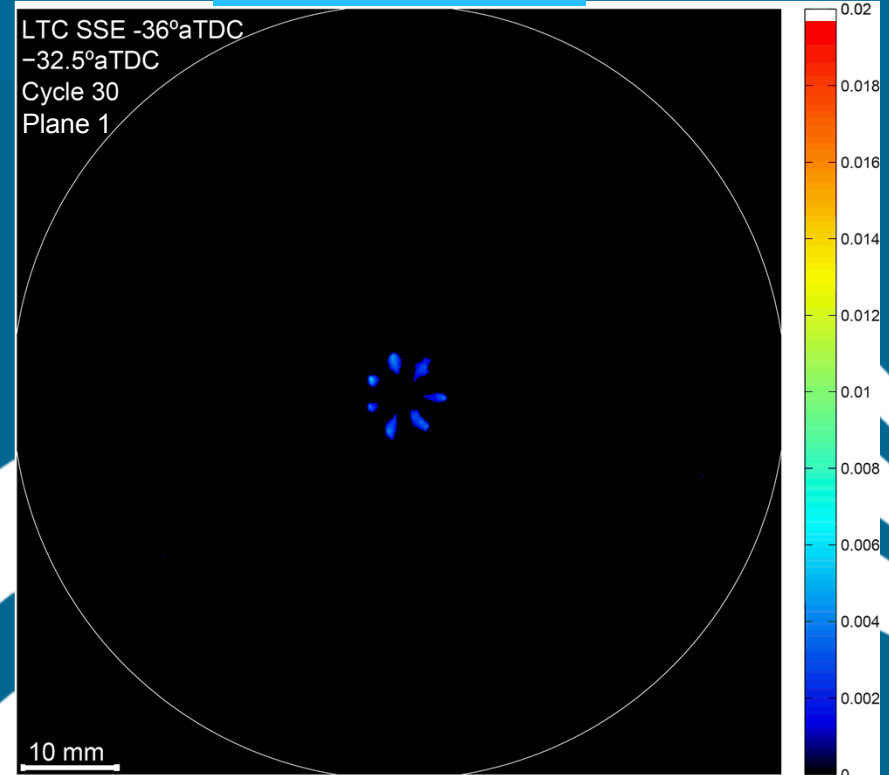


Is there a simple metric to quantify piston geometry impact on in-cylinder mixture preparation?

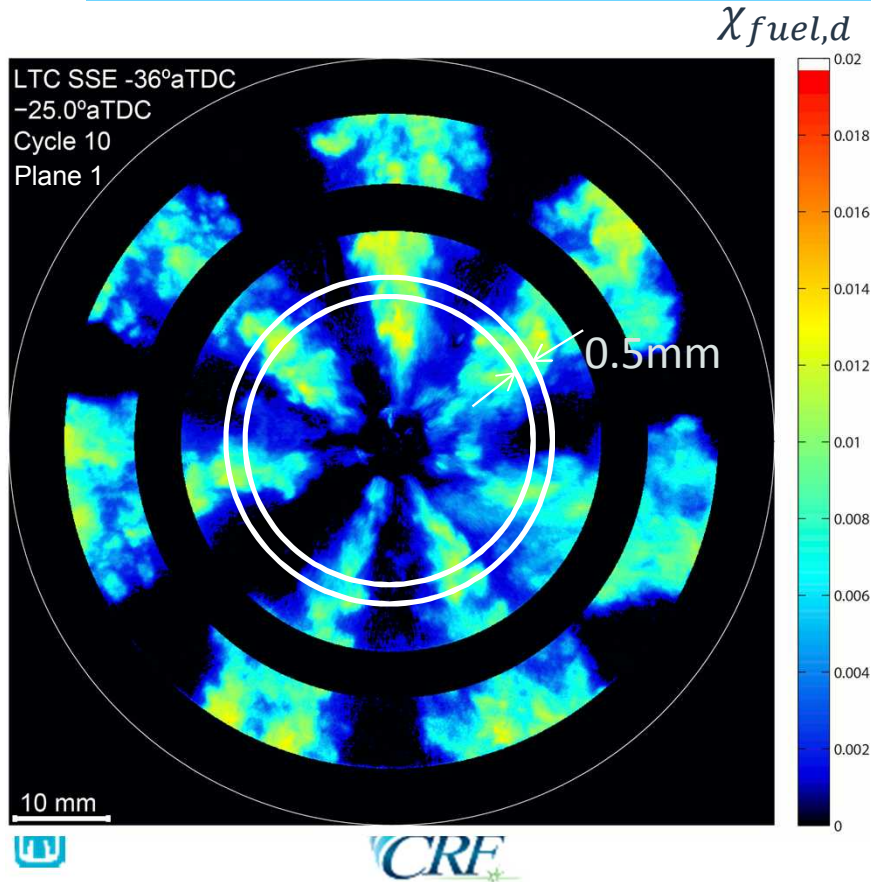
Re-entrant Bowl



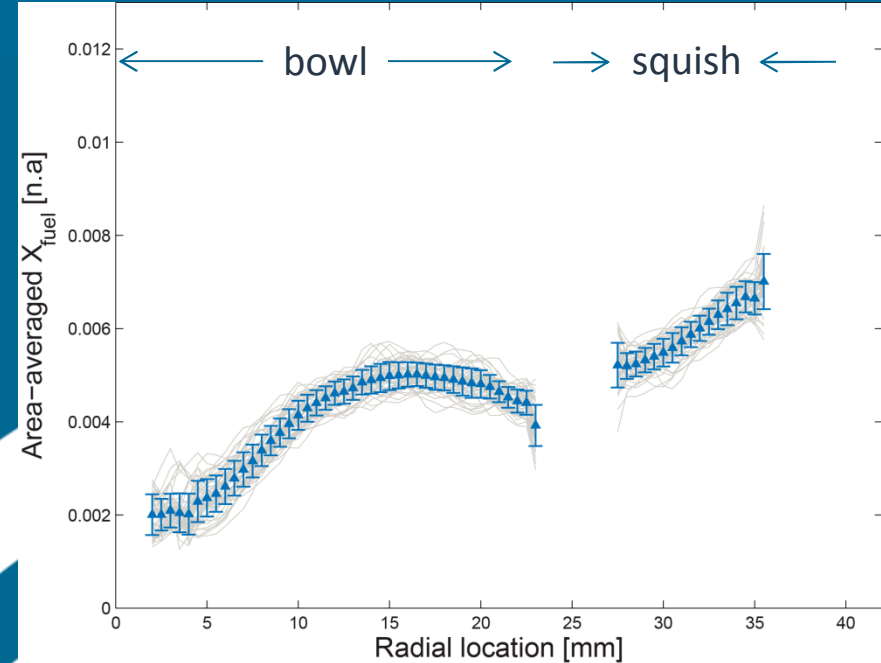
Stepped-lip Bowl



Area-averaged fuel mole fraction is calculated in polar coordinates to quantify spray-dominated mixture preparation pattern.



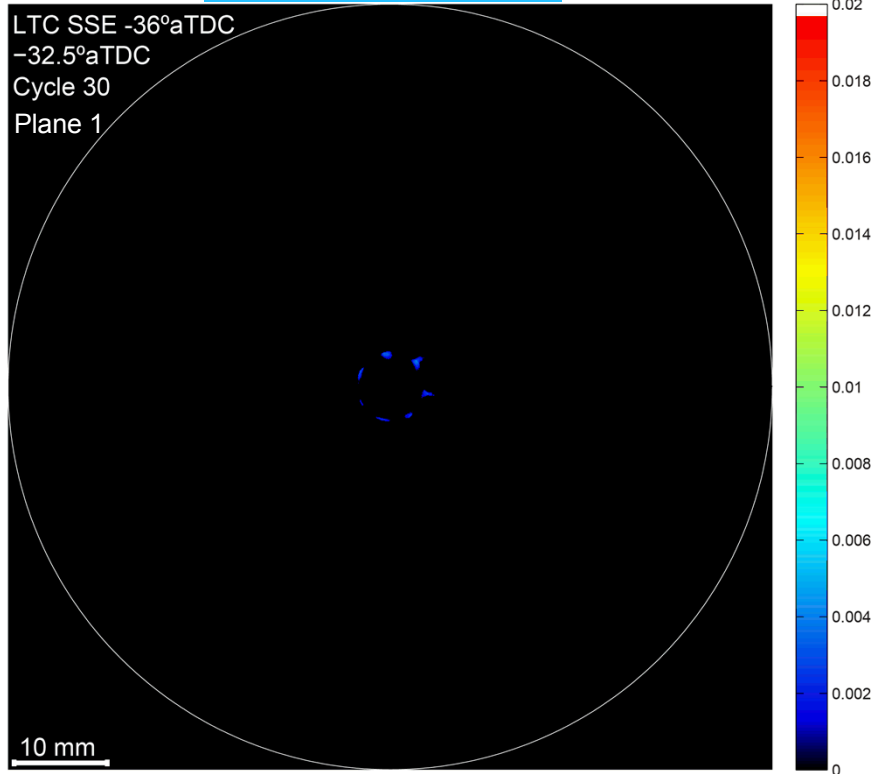
Area-averaged $\chi_{fuel,d}$



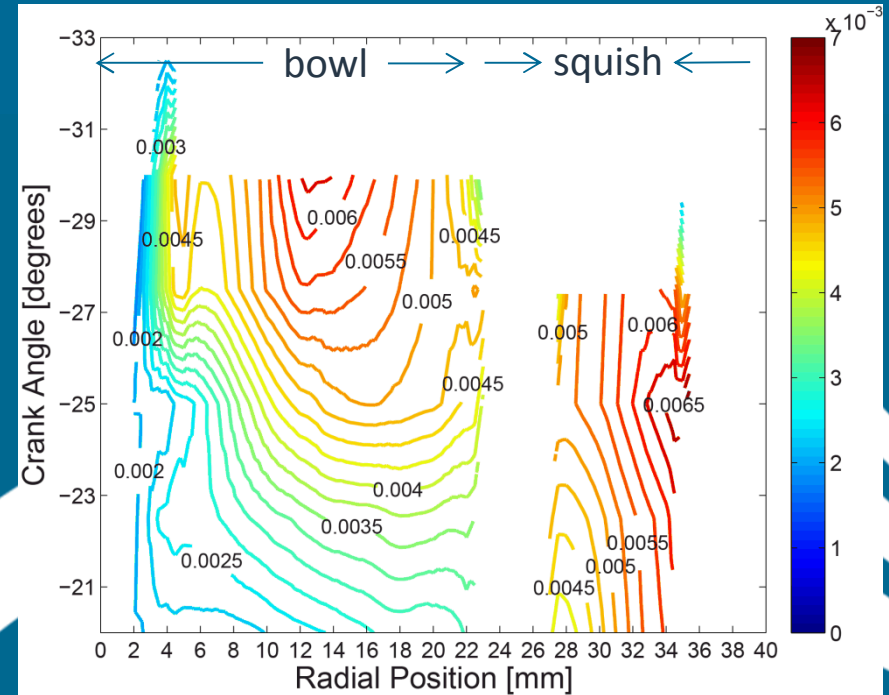
Error bar marks $\pm\sigma$ out of 50 realizations

Area-averaged fuel mole fraction with re-entrant bowl under LTC regime

Re-entrant Bowl

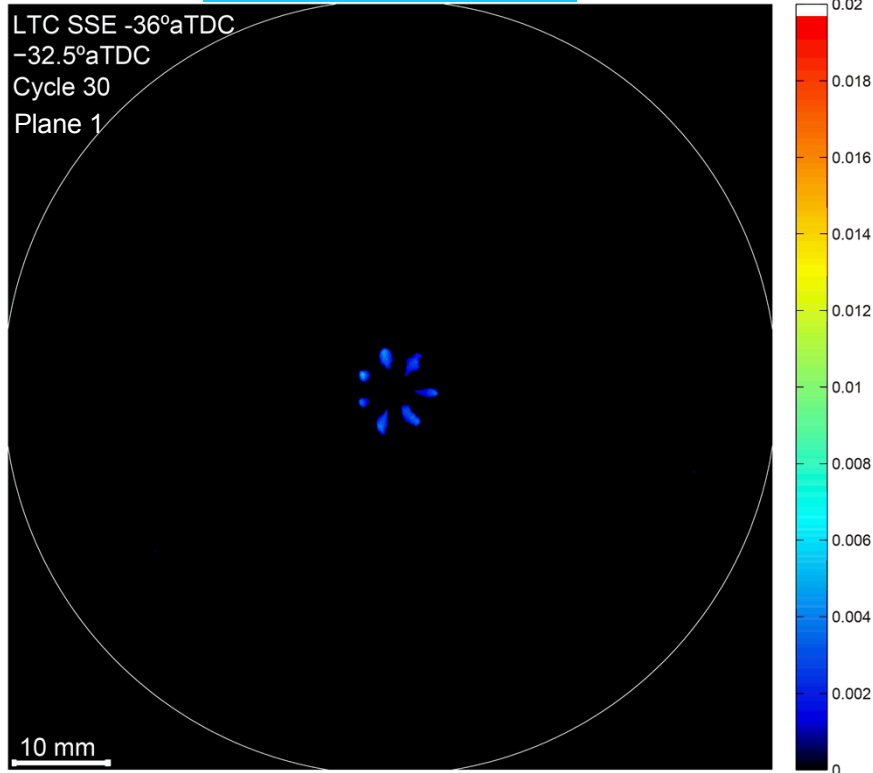


Area-averaged $\chi_{fuel,d}$

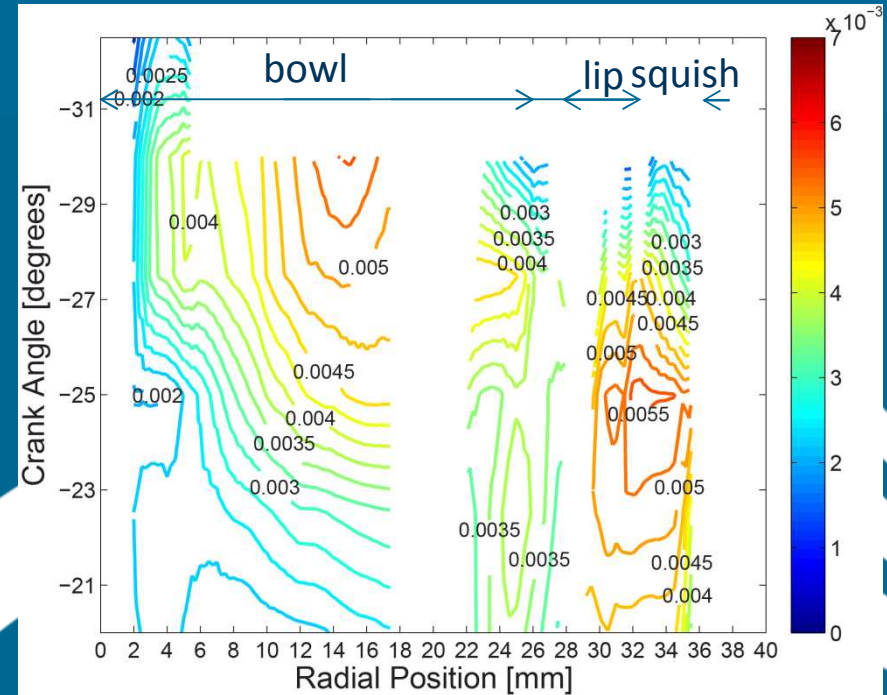


Area-averaged fuel mole fraction with stepped-lip bowl under LTC regime

Stepped-lip Bowl

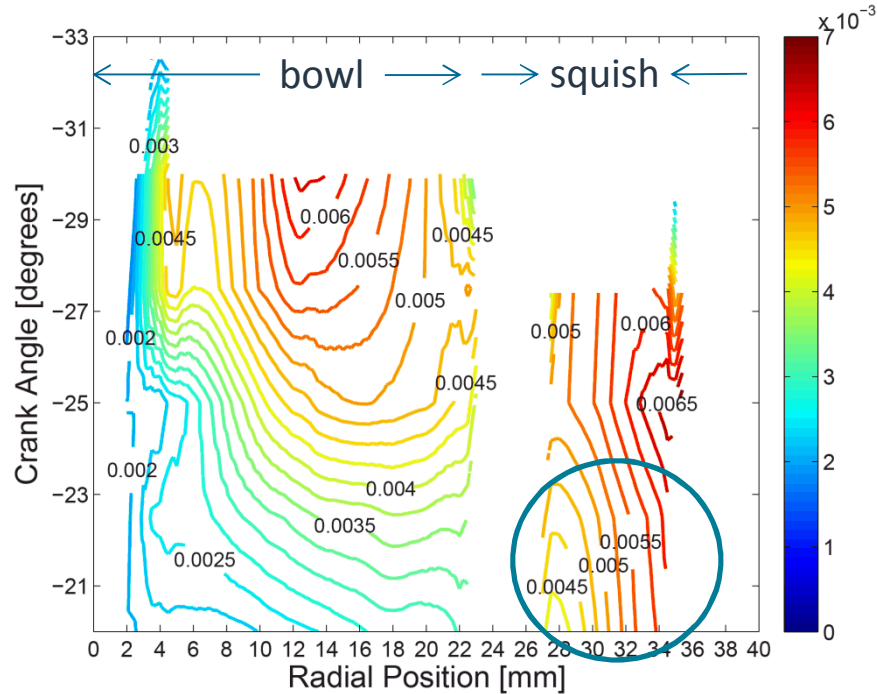


Area-averaged $\chi_{fuel,d}$

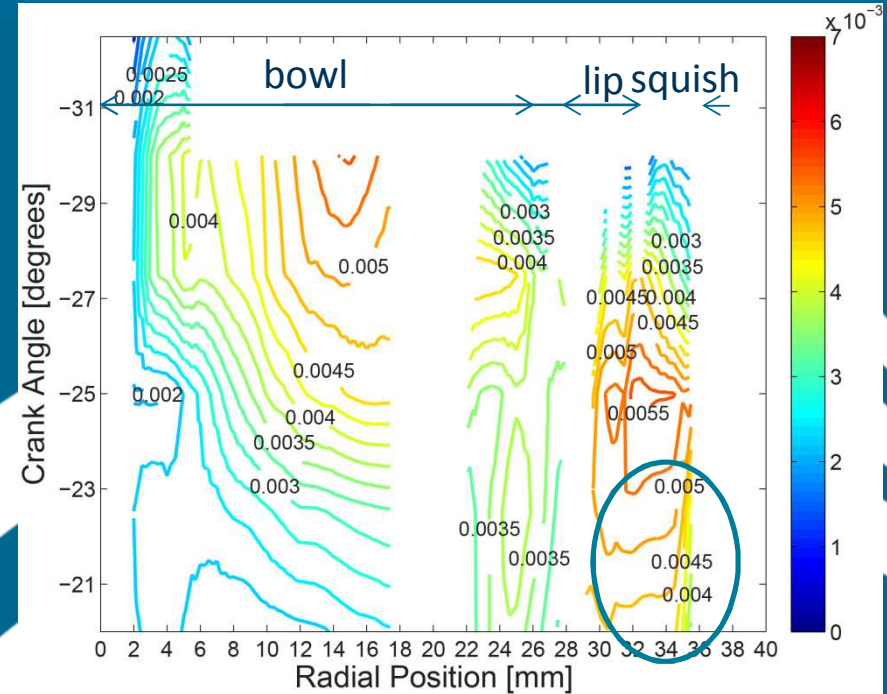


Stepped-lip piston exhibits leaner mixture formation in squish region under LTC regime.

Re-entrant Bowl

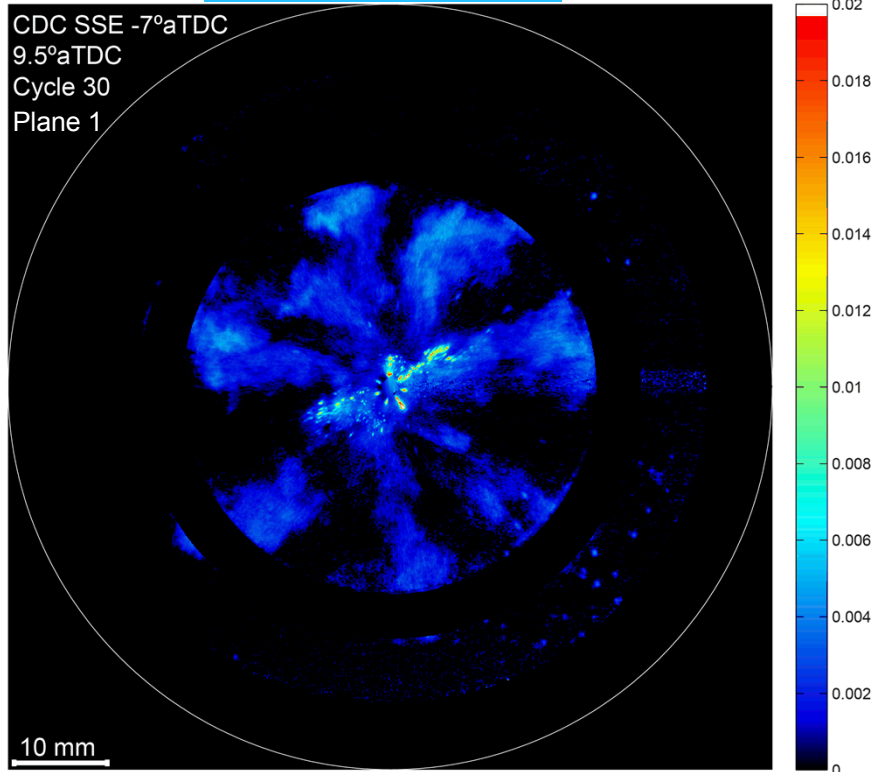


Stepped-lip Bowl

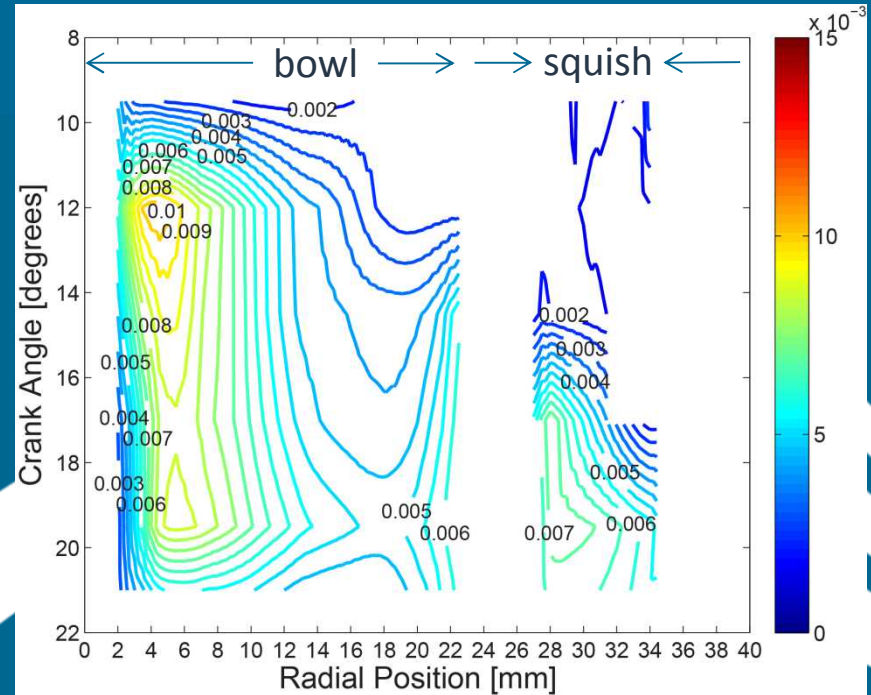


Area-averaged fuel mole fraction with re-entrant bowl under CDC regime

Re-entrant Bowl

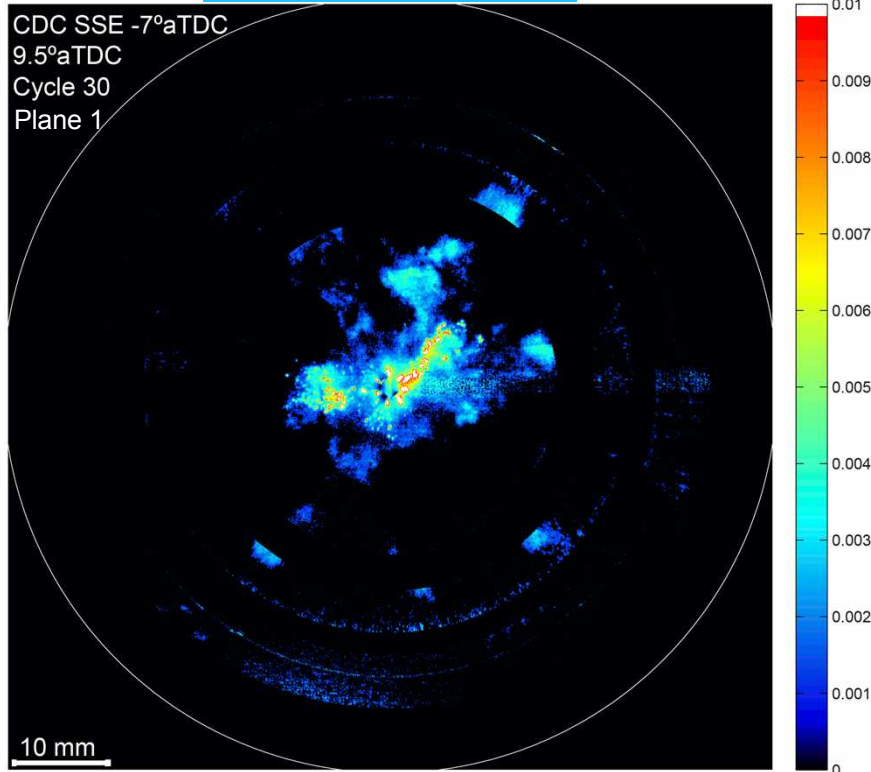


Area-averaged $\chi_{fuel,d}$

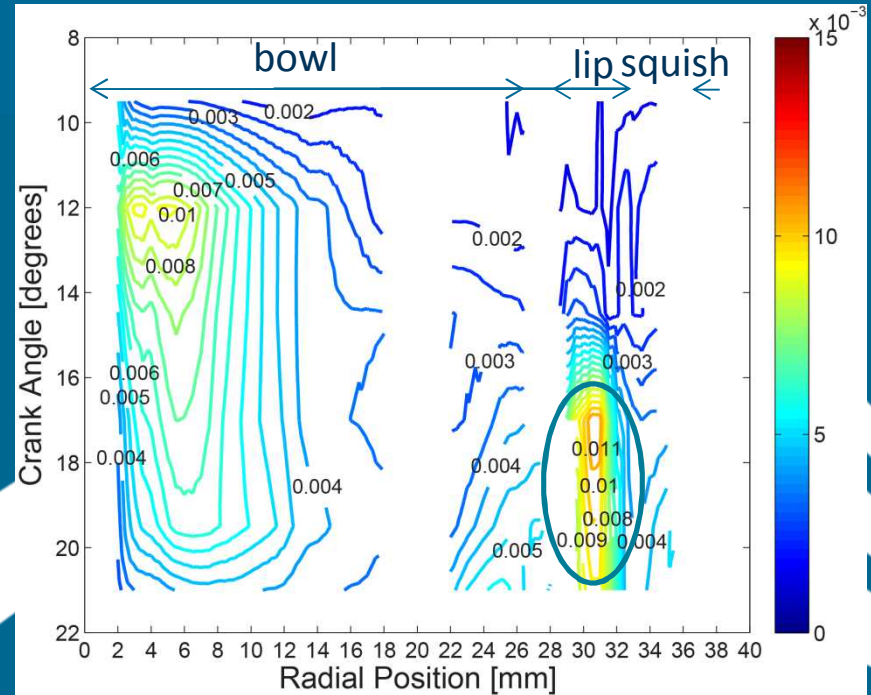


Area-averaged fuel mole fraction with stepped-lip bowl under CDC regime

Stepped-lip Bowl

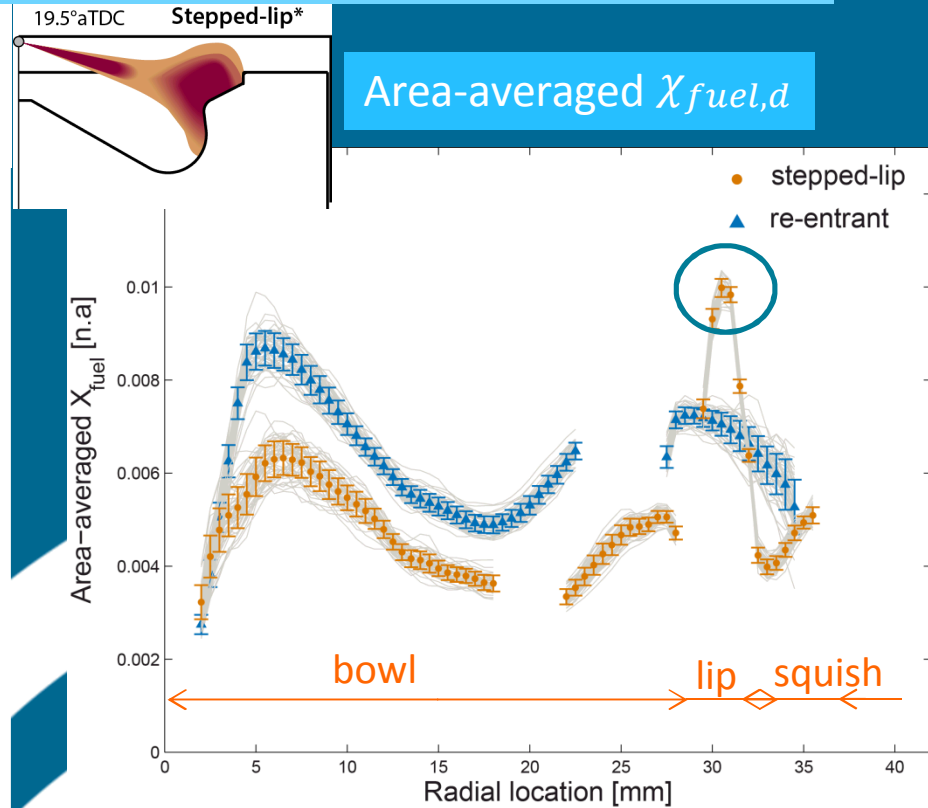
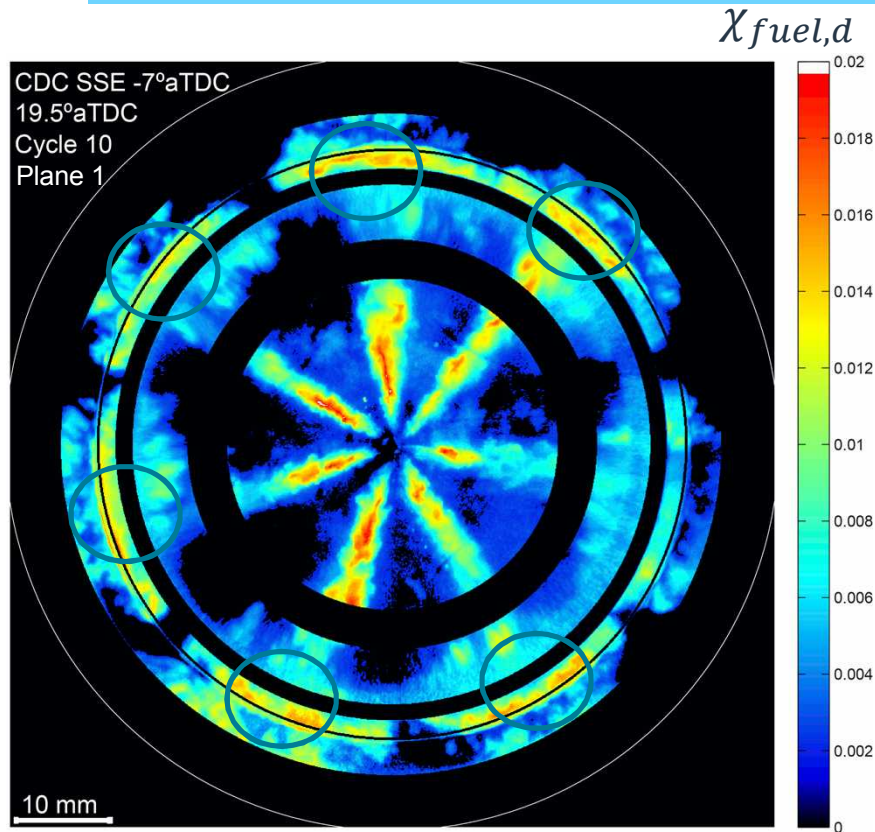


Area-averaged $\chi_{fuel,d}$



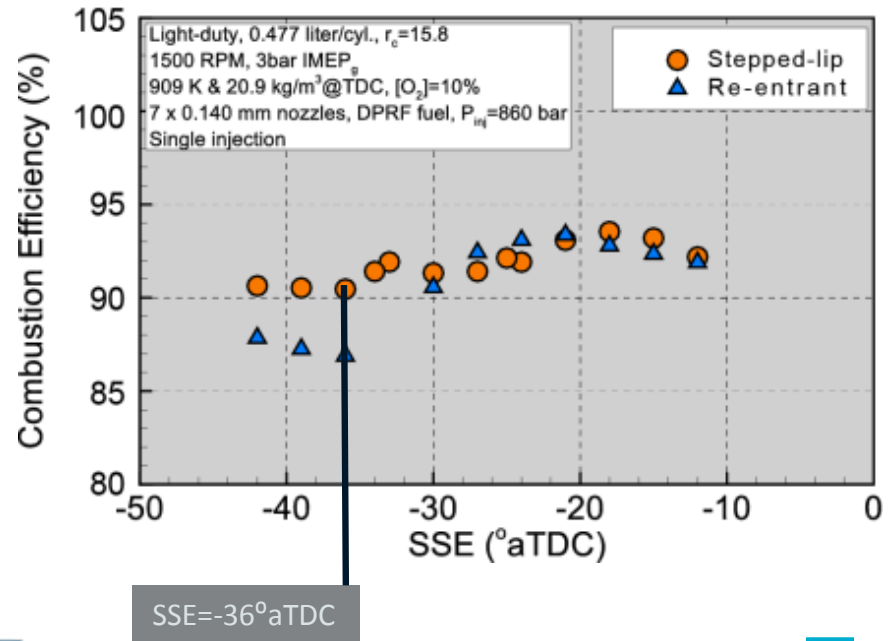
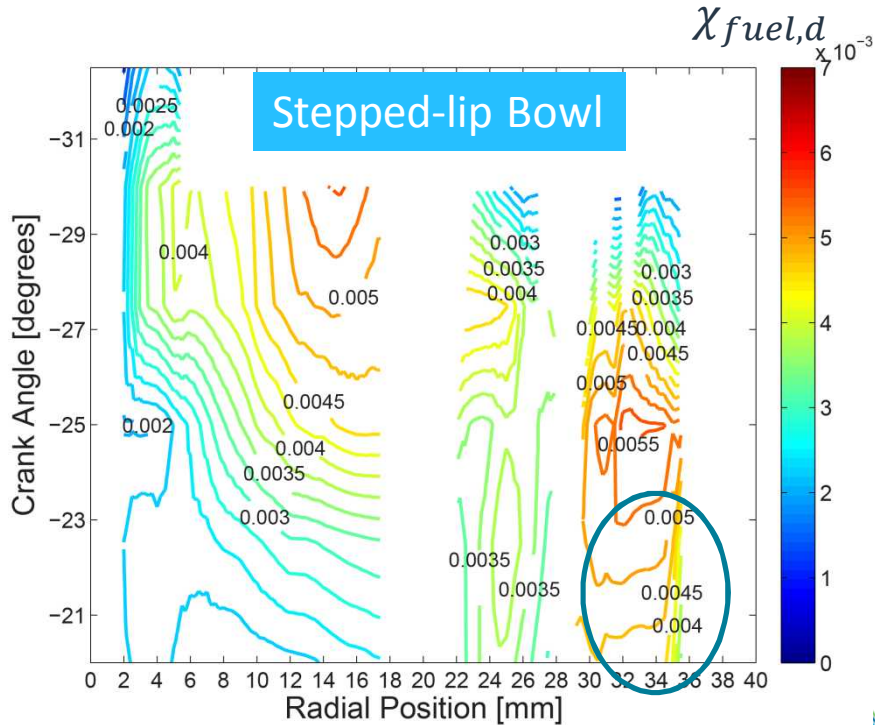
High $\chi_{fuel,d}$ is observed in lip region!

High $\chi_{fuel,d}$ observed in lip region implies better air utilization with stepped-lip piston geometry.

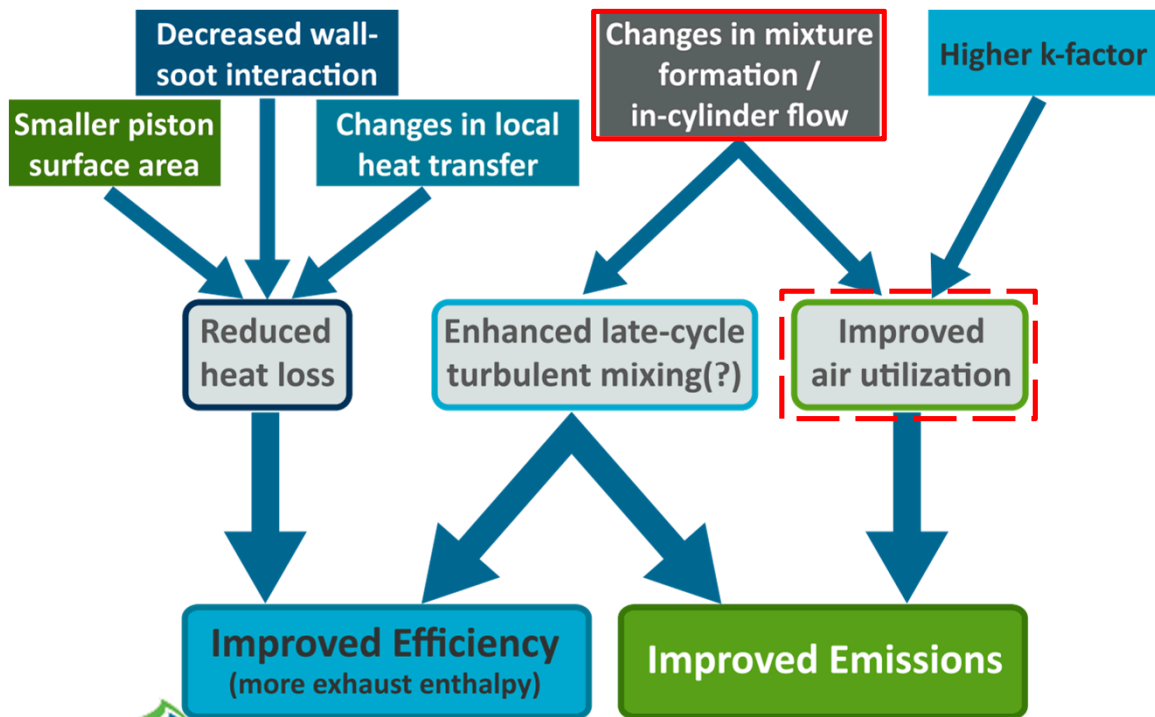
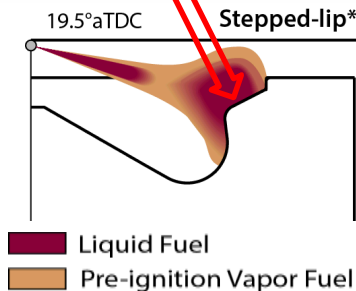
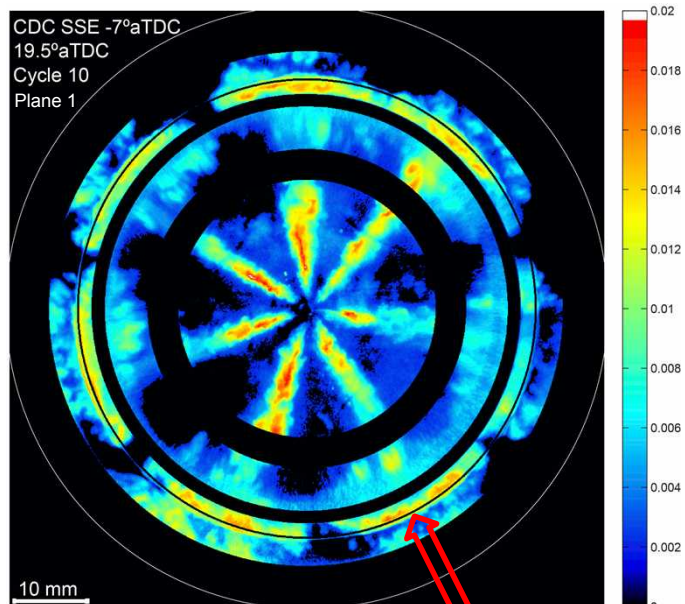


Error bar marks $\pm\sigma$ out of 50 realizations

Conclusion - Stepped-lip bowl exhibits less squish area. In EGR-diluted LTC region, this geometry results in less CO from squish-region lean mixtures. Therefore, higher combustion efficiency.

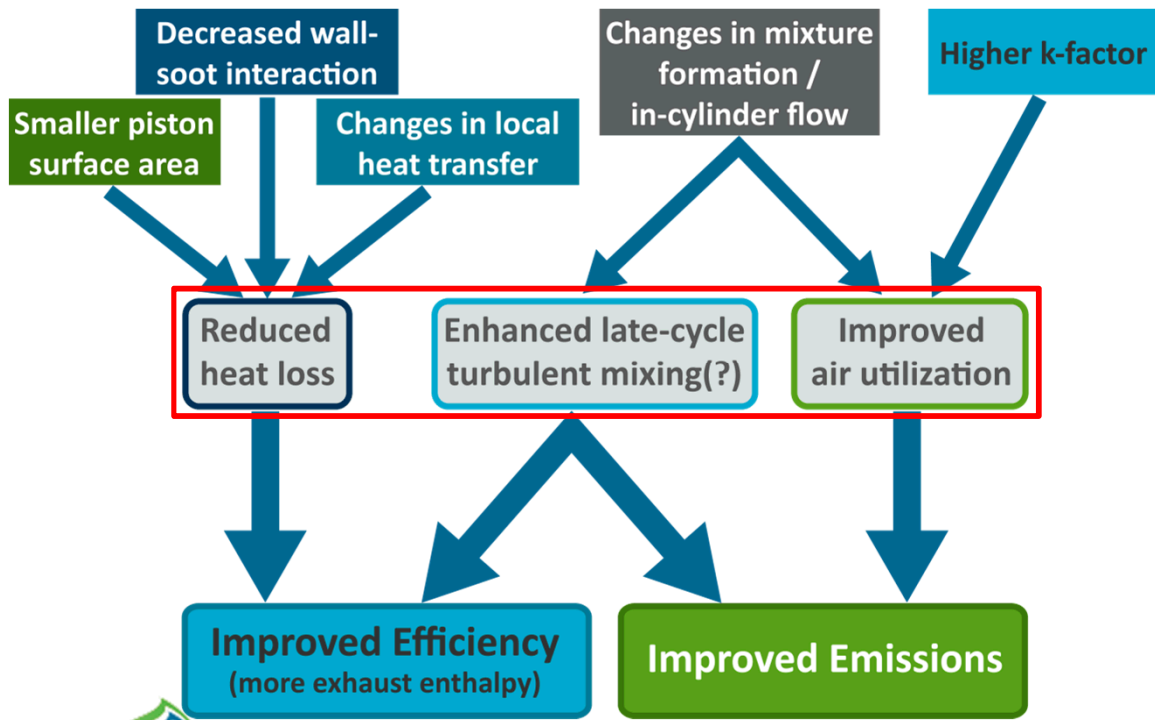


Conclusion - Stepped-lip geometry results in localized high fuel concentration on lip shoulder, which implies better air utilization.



Future work: Understanding the geometry-induced mechanisms for increased heat release rates and higher efficiency.

- Optical experiments: SNL
 - High-speed soot natural luminosity imaging
- Computational studies: UW
 - Bowl geometry, fuel injection, and combustion impact on in-cylinder flow
 - Speed / load / spray targeting sensitivities



Acknowledgement

- Federico Perini, Professor Rolf Reitz, UW-Madison ERC
- Tim Gilbertson, R&D Technologist, Sandia





Thank you for your attention!

Questions?



Sandia National Laboratories

U.S. DEPARTMENT OF ENERGY
ENERGY

PLIF: computation of fuel concentrations

- $\chi_{fuel,d} = \chi_{fuel,cal} \frac{S_d}{S_{cal}} \frac{E_{cal}}{E_d} \frac{T_d}{T_{cal}} \frac{P_{cal}}{P_d} \frac{\sigma\eta(T_{cal})}{\sigma\eta(T_d)}$
 - S : background-subtracted, distortion-corrected image intensity
 - E : measured laser pulse energy
 - T : bulk gas temperature from GT-Power model
 - P : cylinder pressure from GT-Power model
 - $\sigma\eta$: product of absorption cross section and quantum yield; function of temperature alone
- Calibration with homogeneous mixture of known concentration ($\chi_{fuel,cal}$)
 - “Flat-field” correction
- $\sigma\eta(T)$ is determined with separate measurements and analyses

PLIF temperature calibration

- $\sigma\eta(T)$ determined from flat-field images taken at various crank angles and for various intake temperatures
- Upper limit of possible flat-field fuel concentrations limited by wall-wetting
 - $\phi_{ff} \approx 0.3$
- Comparison with previous temperature calibration
 - Coefficients between 14-18% higher than previously determined values
 - The arbitrary normalization of the calibration curve is responsible for the majority of this discrepancy
- Future plans include expanded calibration dataset

