



Piston Geometry Effects on Fuel-Air Mixture Preparation in a Light-Duty Optical Diesel Engine

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NETL

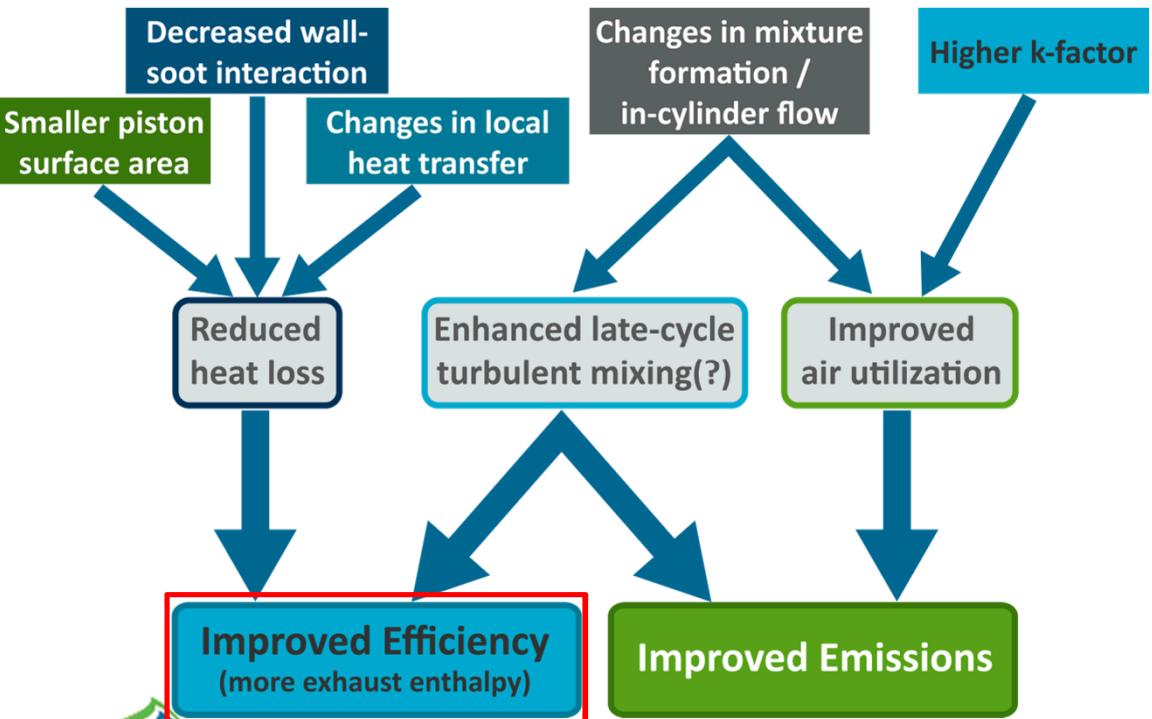
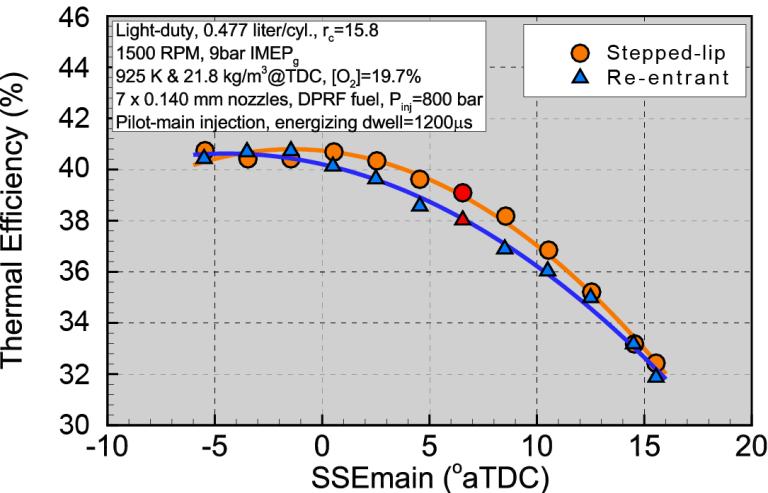
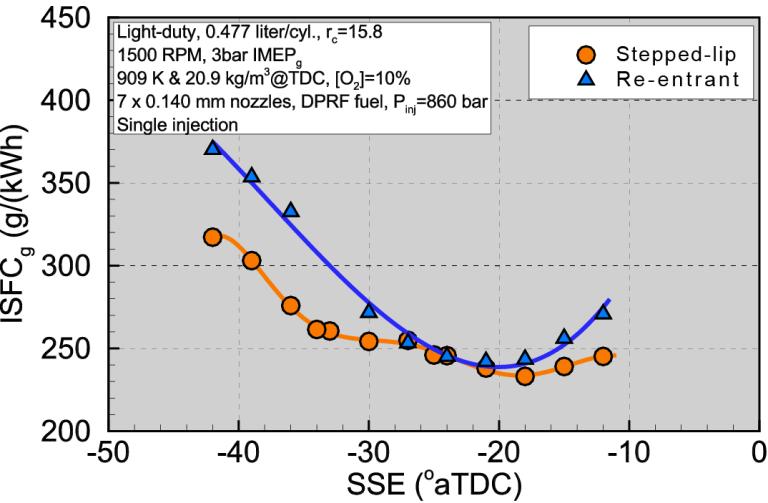
Abstract

It is widely reported in the literature that for direct-injection Diesel engines, stepped-lip piston geometry exhibits fuel efficiency and emission advantages over re-entrant piston geometry at some injection timings. This observation is present both under low-load EGR-diluted Low-Temperature Combustion (LTC) and medium-load conventional diesel combustion regimes. However, this geometry-induced mechanisms for increased heat release rates and higher combustion and/or thermal efficiency is not fully understood. In order to understand the mechanism, experimental investigation of piston geometry effects on fuel-air mixture preparation is needed. This work utilizes a fuel tracer laser-induced fluorescence (LIF) technique to conduct non-intrusive planar measurements of in-cylinder fuel distribution under non-combusting conditions inside a single-cylinder small-bore optical Diesel engine. In this study, two transparent piston bowls - adaptive bowl for re-entrant and stepped-lip geometry respectively - are compared. By taking area-averaged fuel mass fraction in a polar-coordinate fashion, the temporal and spatial trends show that stepped-lip geometry tends to deposit injected fuel on the lip shoulder, which promotes better boundary layer utilization and may help prevent unburnt fuel from penetrating into the squish region by creating a strong squish flow. Furthermore, experimental and computational investigations such as high-speed imaging, soot under soot natural conditions, and turbulent mixing, speed/load/spray targeting sensitivities and soot distributions are needed to study the underlying physical benefit of clean and efficient diesel combustion.

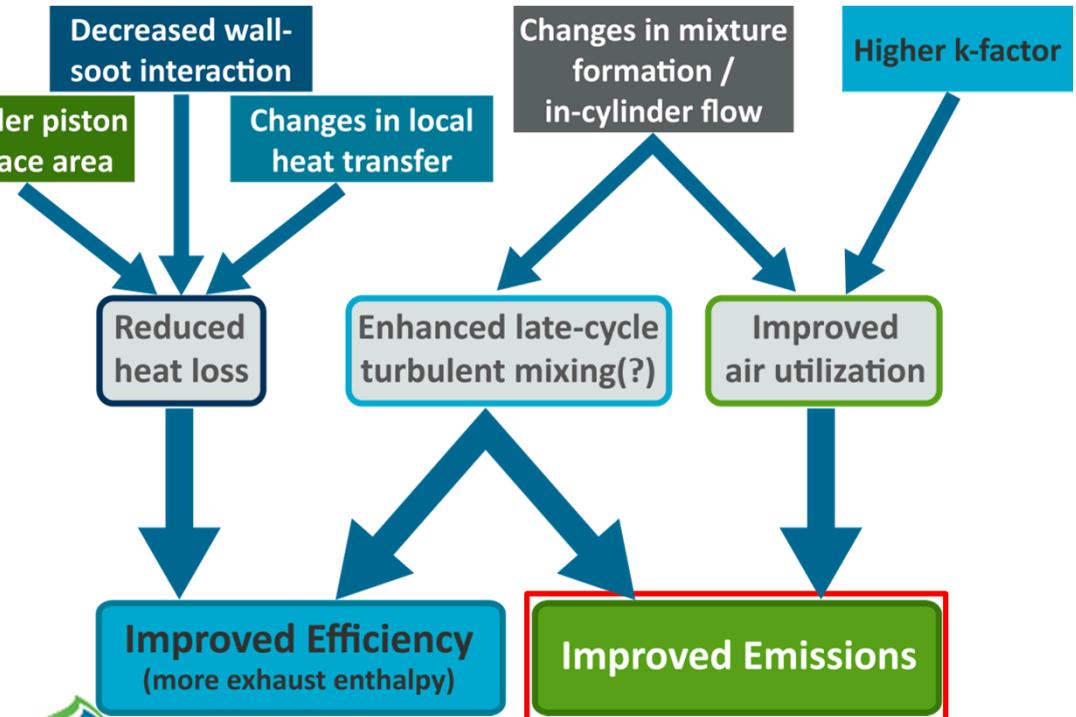
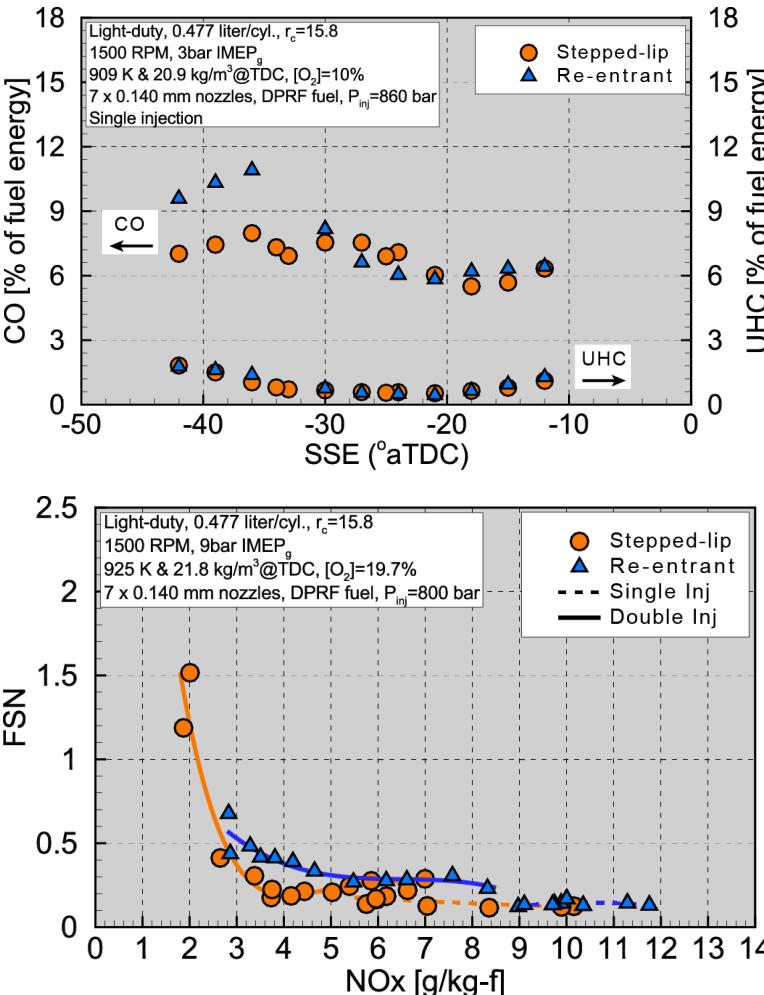
Outline

- Introduction and motivation
- PLIF experimental setup
 - SNL optical piston bowl geometries
- PLIF: data collection and processing
 - Uncertainties of PLIF measurements
- Area-averaged fuel mole fraction analysis
 - Single-injection, EGR-diluted LTC regime
 - Double-injection, conventional diesel con
- Conclusion

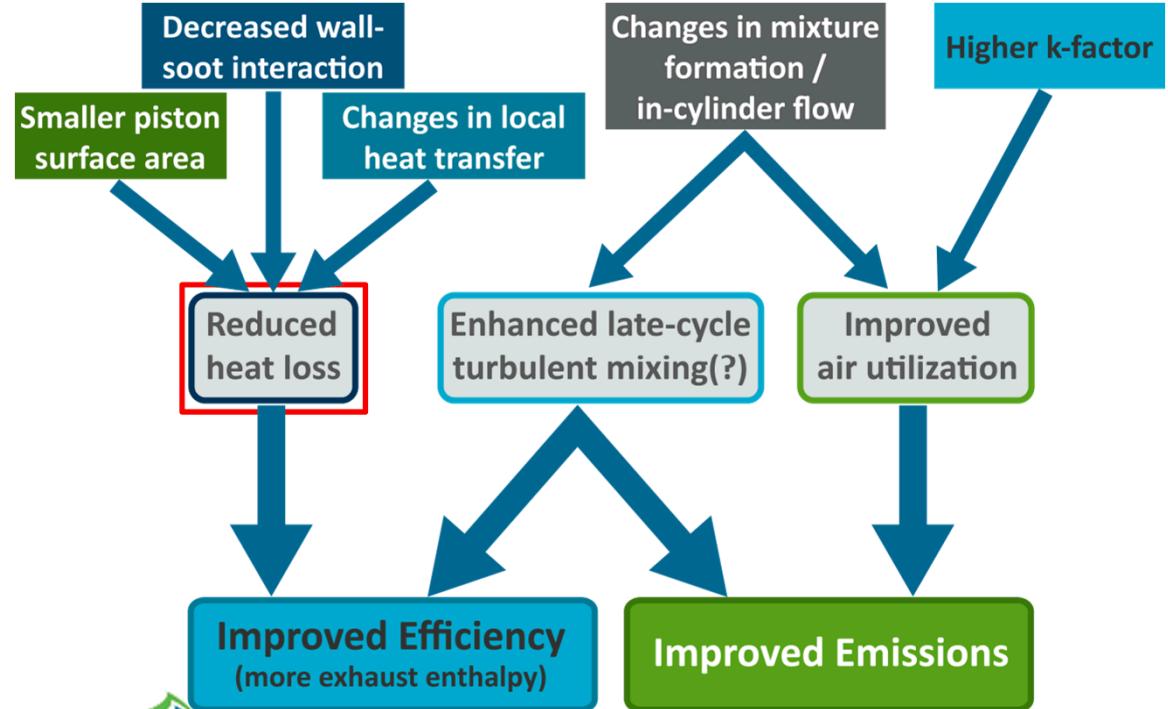
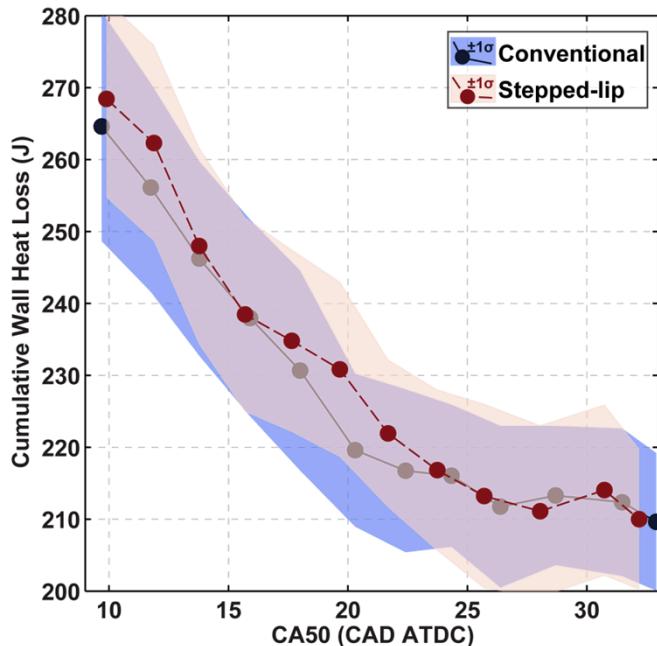
What makes the stepped-lip bowl more efficient than the conventional bowl?



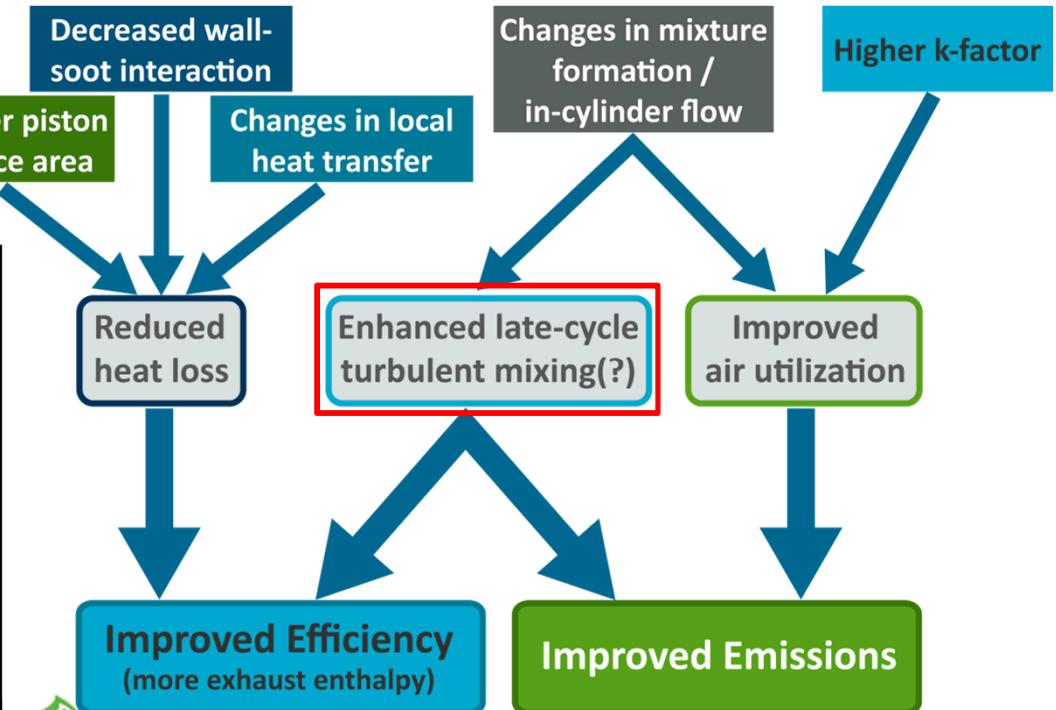
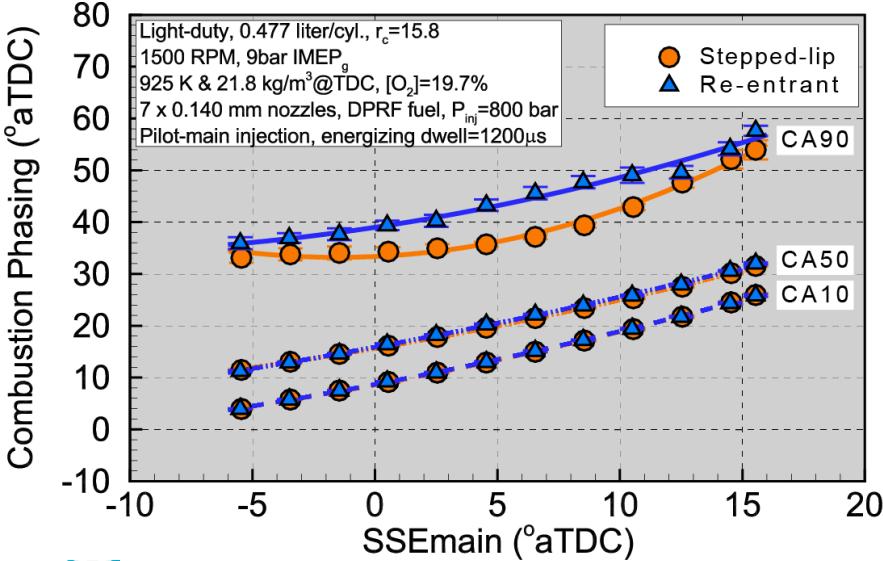
What makes the stepped-lip bowl more efficient than the conventional bowl?



“Cycle-resolved analyses do not suggest lower wall heat loss with the stepped-lip piston bowl geometry.”

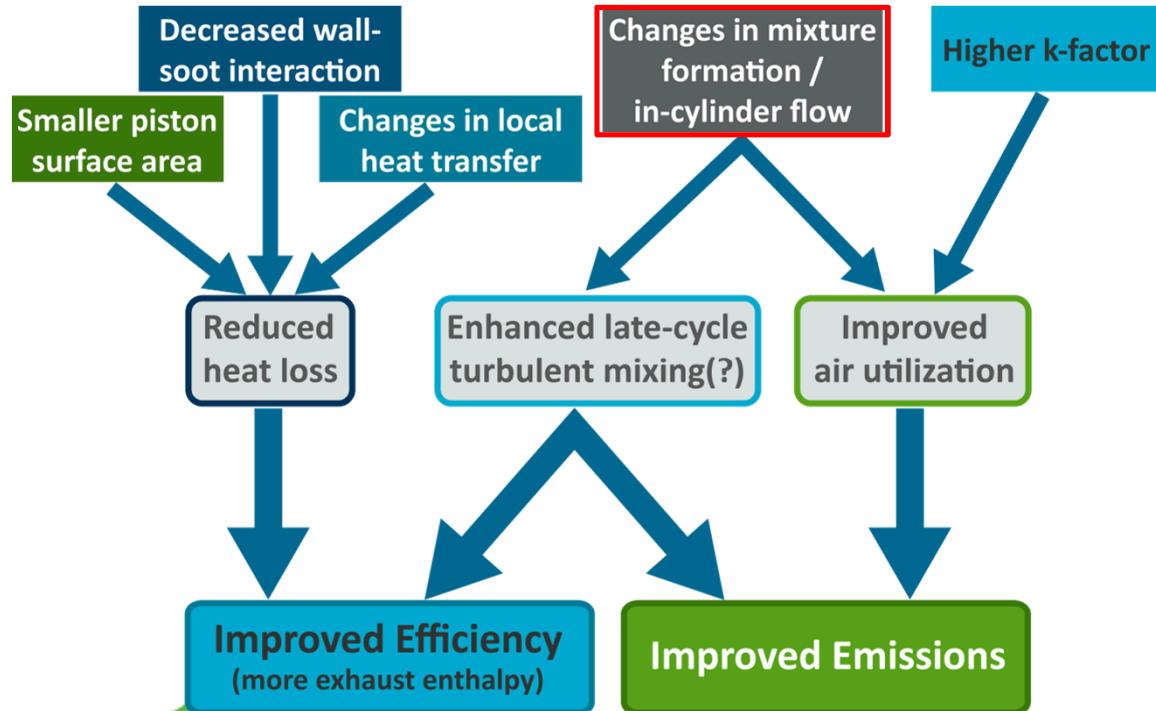


“Fuel conversion efficiency improvements with the stepped-lip piston are most closely related to enhanced late-cycle heat release rates.”



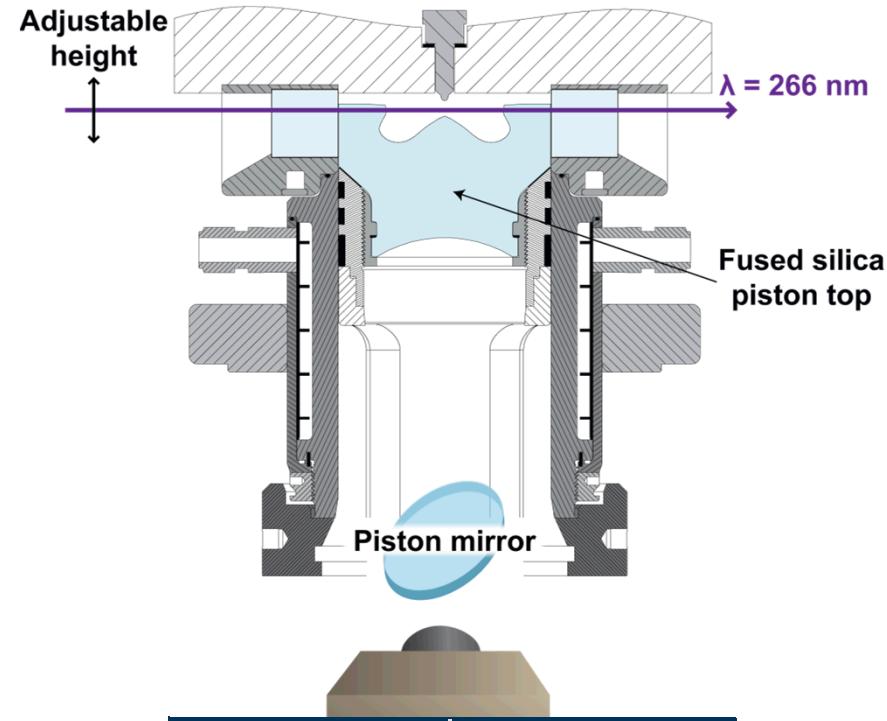
Does stepped-lip piston result in a mixture formation distribution more favorable for complete combustion and enhanced turbulent mixing?

- Does piston-induced changes in cold flow structure have big effects on mixture preparation?
- What is the role of squish flow?
- Spray-piston interaction?



PLIF Experiments in the SNL 0.48L light-duty single-cylinder optical engine

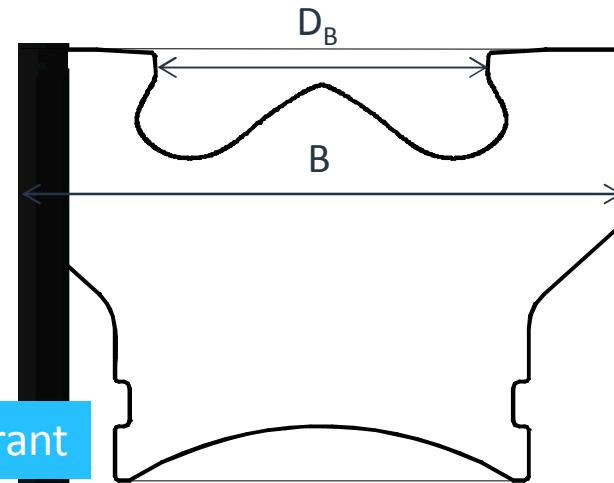
- Engine operation
 - 1500 rpm
 - Non-combusting, 0% O₂
 - Fuel: 42 vol% n-hexadecane + 58 vol% heptamethylnonane
 - Tracer: 0.5 weight% methylcyclohexane
 - Swirl ratio: 2.1
- Illumination
 - Laser: Nd:YAG harmonic (266 nm)
 - Energy: 100 mJ/pulse (relative energy measured each shot)
 - Laser sheet thickness: 1 mm
- Imaging
 - 1000x4 ICCD camera
 - Nikon UV-10 lens
 - WC filter



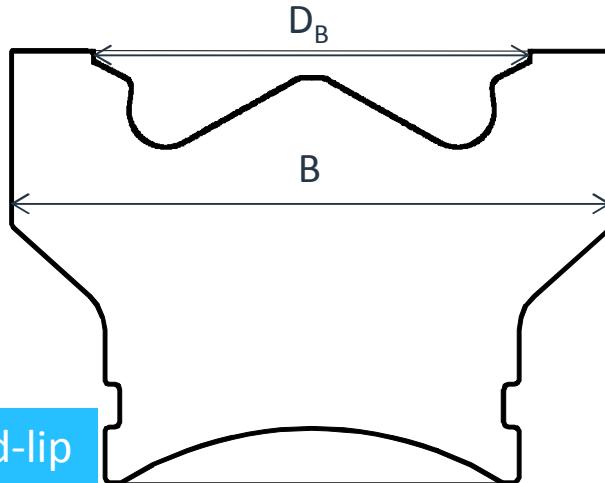
Bore x stroke	82 mm x 90.4 mm
Compression ratio	15.8:1
Valves	4
Injector type	Solenoid
Holes	7 x 139 µm
ks	1.5/86
Included Angle	149°

SNL optical piston bowl geometries

- Two quartz pistons have identical:
 - Bowl volume = 0.028 L
 - Squish height = 1.35 mm
 - Compression ratio = 15
 - No valve cut-outs
- Different bowl geometries result in different bowl-to-bore ratios
 - $D_B = 25.55 \text{ mm}$ and $B = 18.55 \text{ mm}$ $\therefore D_B/B = 0.73$
 - Surface area of stepped bowl is 10% less than for a conventional bowl
- Initial acceleration is reduced on account of reduced forces on the pistons



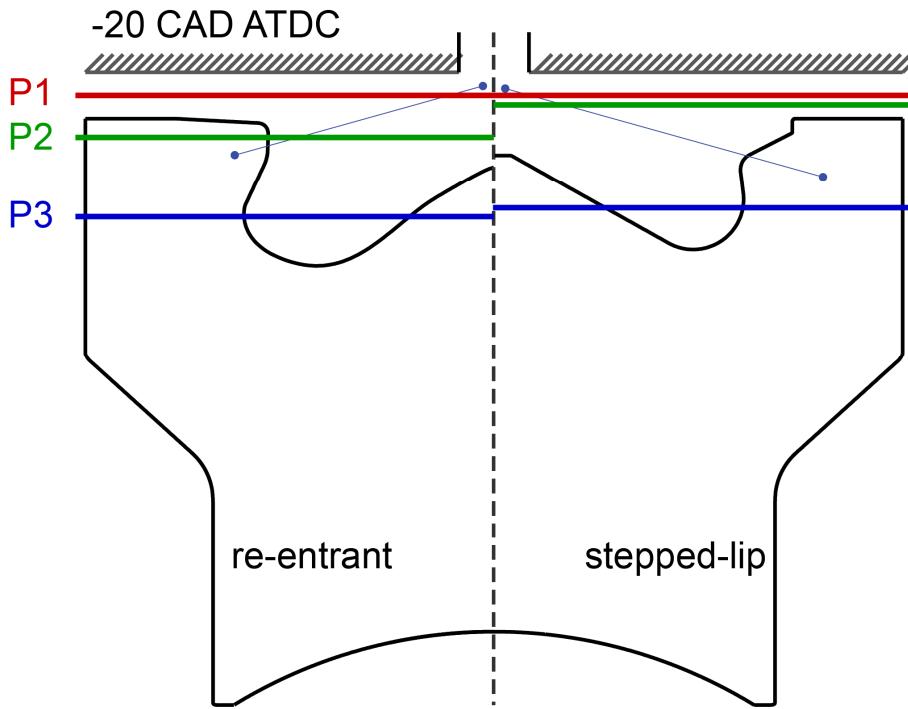
Re-entrant



Stepped-lip

PLIF setup: laser plane locations

- Plane 1 (P1) is set half of squish height
- Plane 2 (P2) is empirically determined
 - Re-entrant: at rim of bowl where laser sheet passes through with minimum deflection
 - Stepped-lip: 1.37 mm above the piston top
- Plane 3 (P3) is set deep within the bowl
 - Re-entrant: 9.88 mm below the piston top
 - Stepped-lip: 8.98 mm above the piston top
- P2 and P3 are aligned with the piston rank changes.



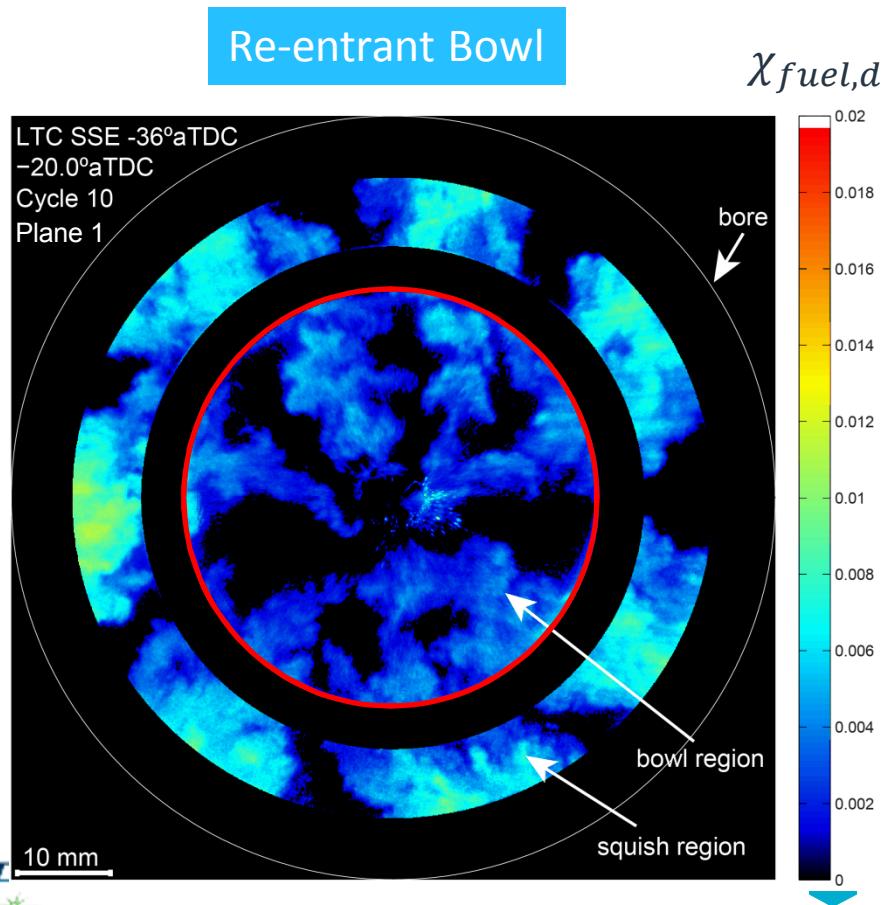
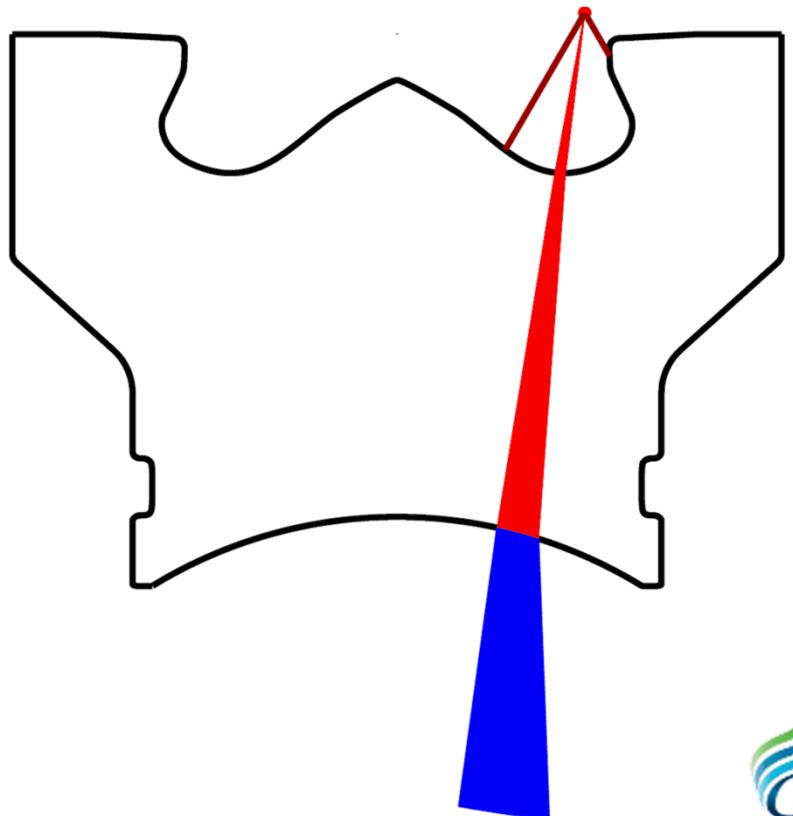
PLIF: data collection and processing

- Three sets of images for a given crank angle, plane, and operating point (51 images per set)
 - Background (no fuel injection)
 - Flat-field (6/8 injections in intake stroke)
 - Fuel injection image (desired operating point)
 - Fuel injection Image sets taken over range starting from injection ending prior to SOC.
- 9:15min's measurement schedule to maintain temperatures and pressures
- Distortion correction according to established ray-tracing routine

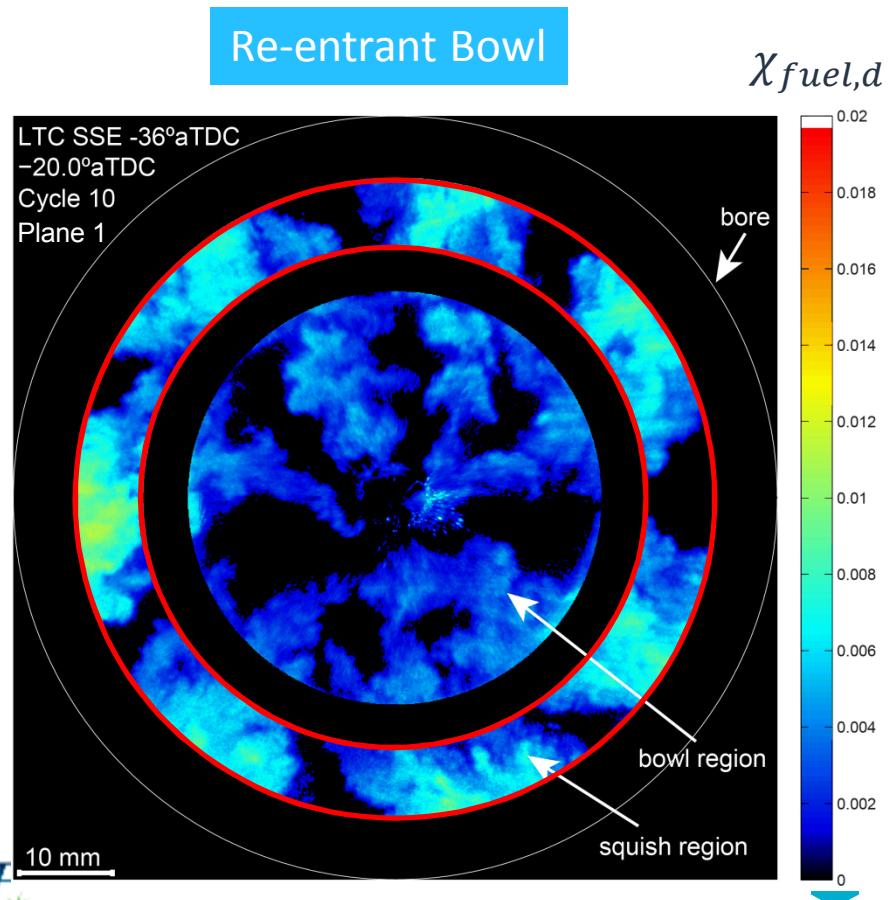
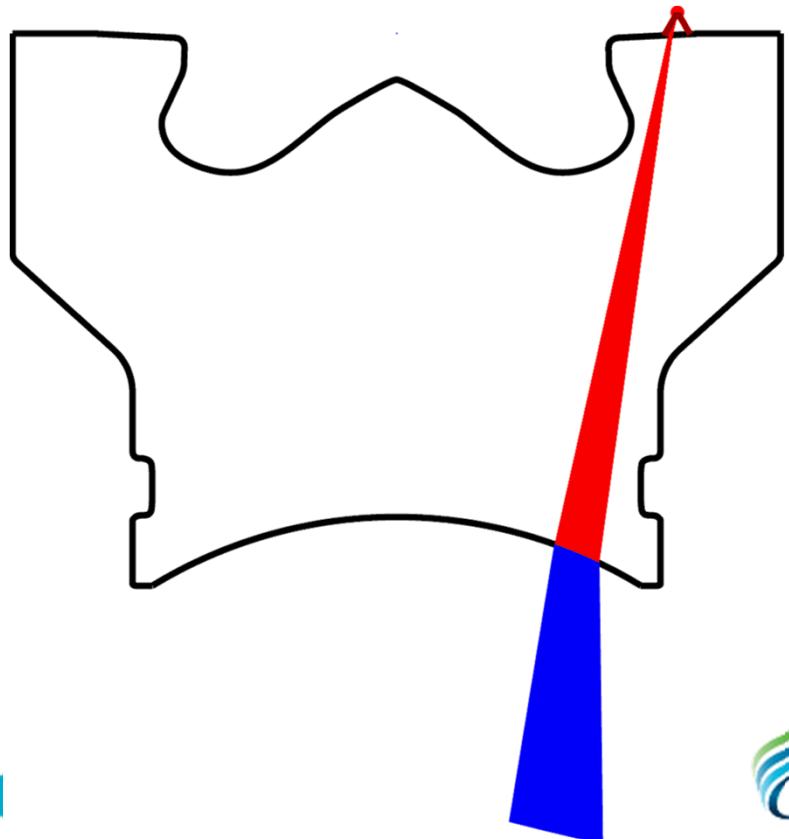
$$\chi_{fuel,d} = \chi_{fuel,cal} \frac{S_d}{S_{cal}} \frac{E_{cal}}{E_d} \frac{T_d}{T_{cal}} \frac{P_{cal}}{P_d} \frac{\sigma\eta(T_{cal})}{\sigma\eta(T_d)}$$

- $\chi_{fuel,d} = (\text{moles nC16H34} + \text{moles iC16H34} + \text{moles 1MN}) / (\text{total moles of CO}_2, \text{N}_2, \text{nC16H34, iC16H34, and 1MN}).$

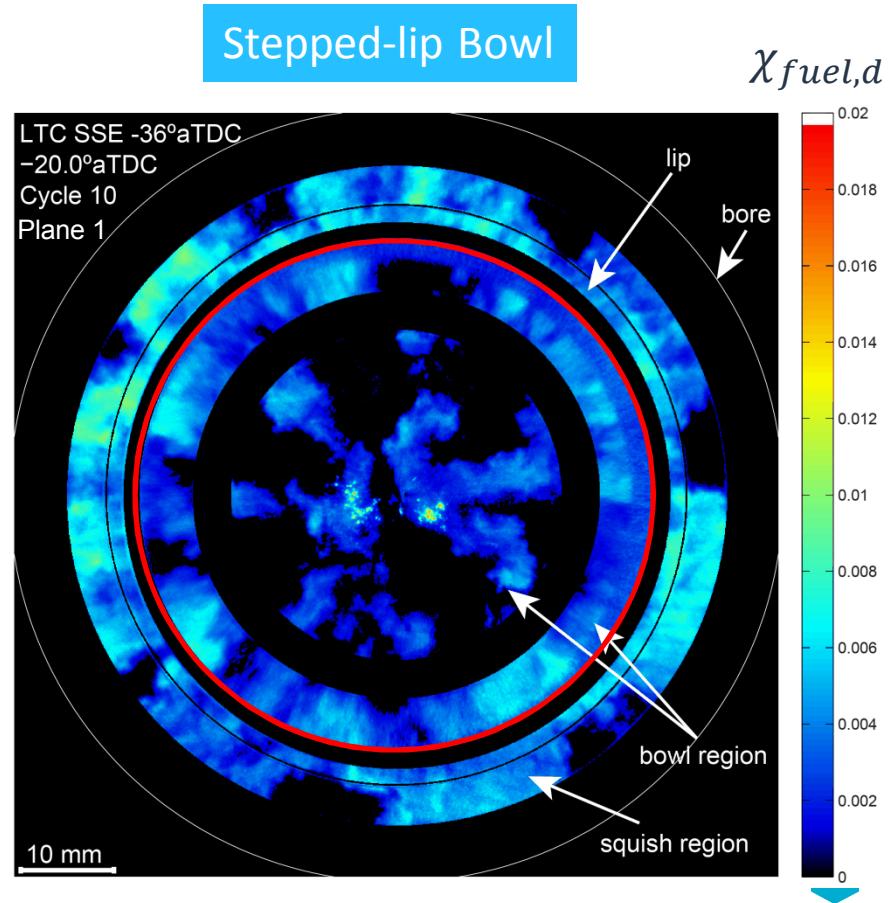
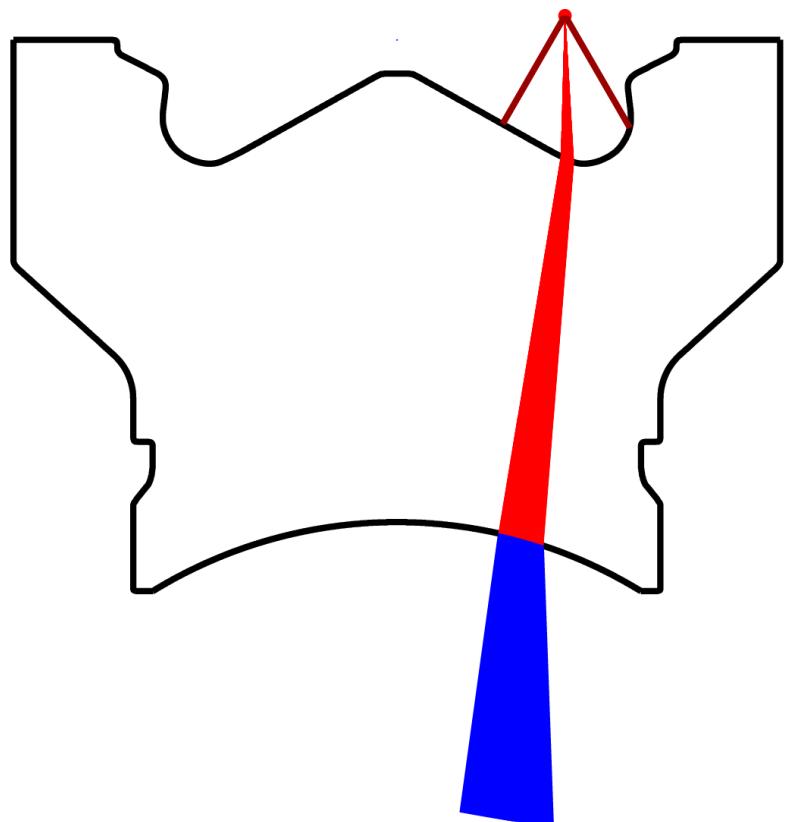
A sample of dewarped PLIF images with re-entrant geometry



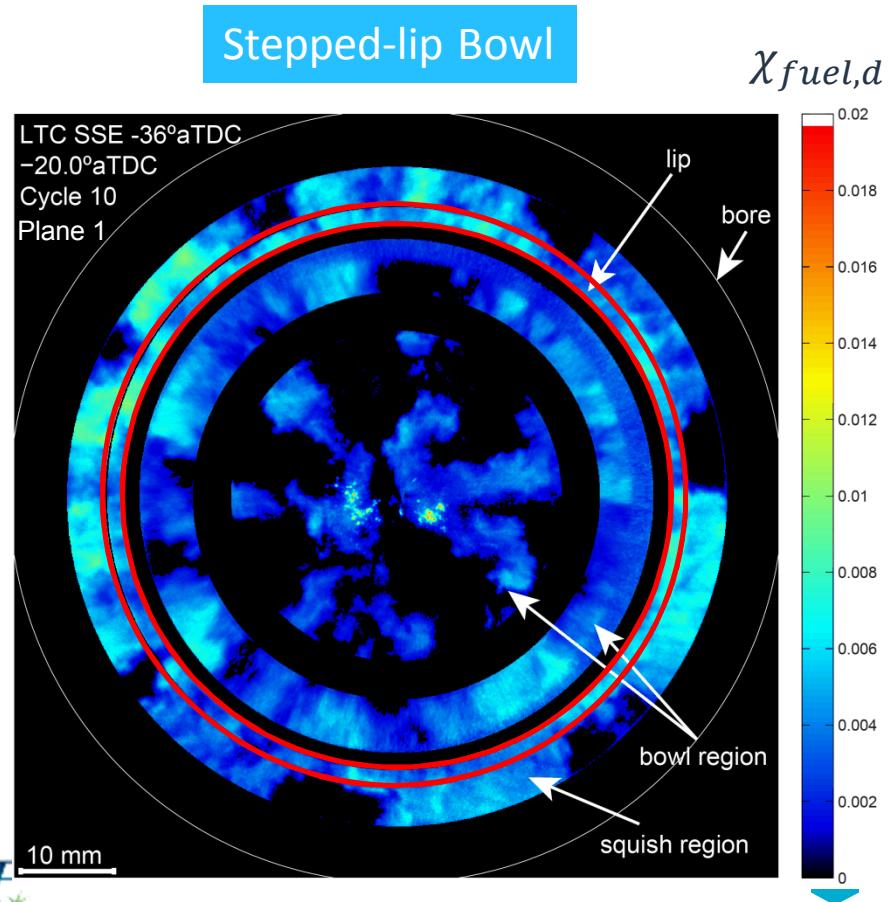
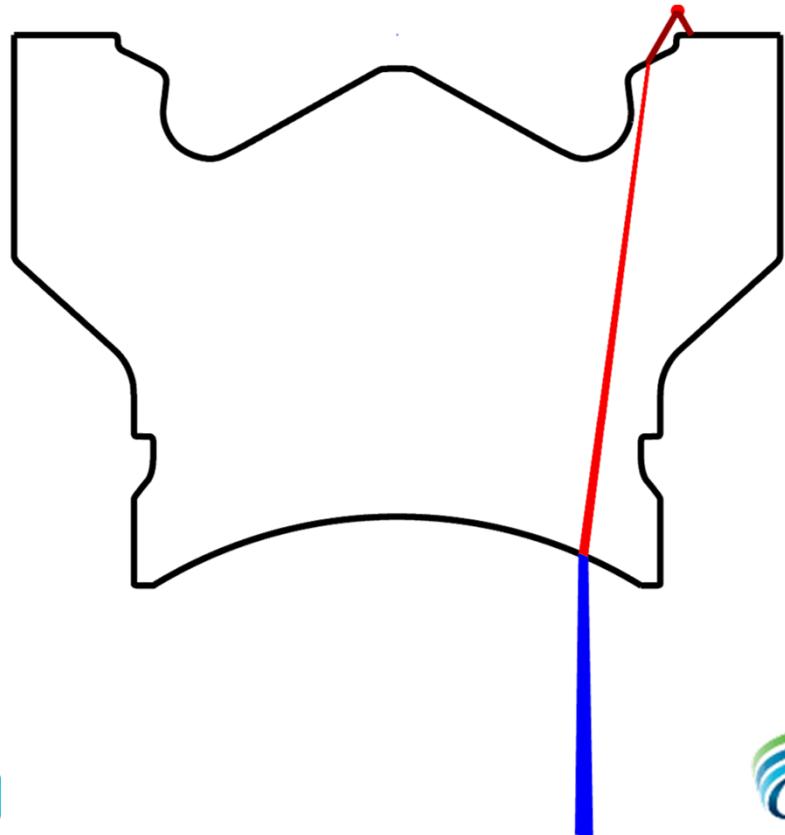
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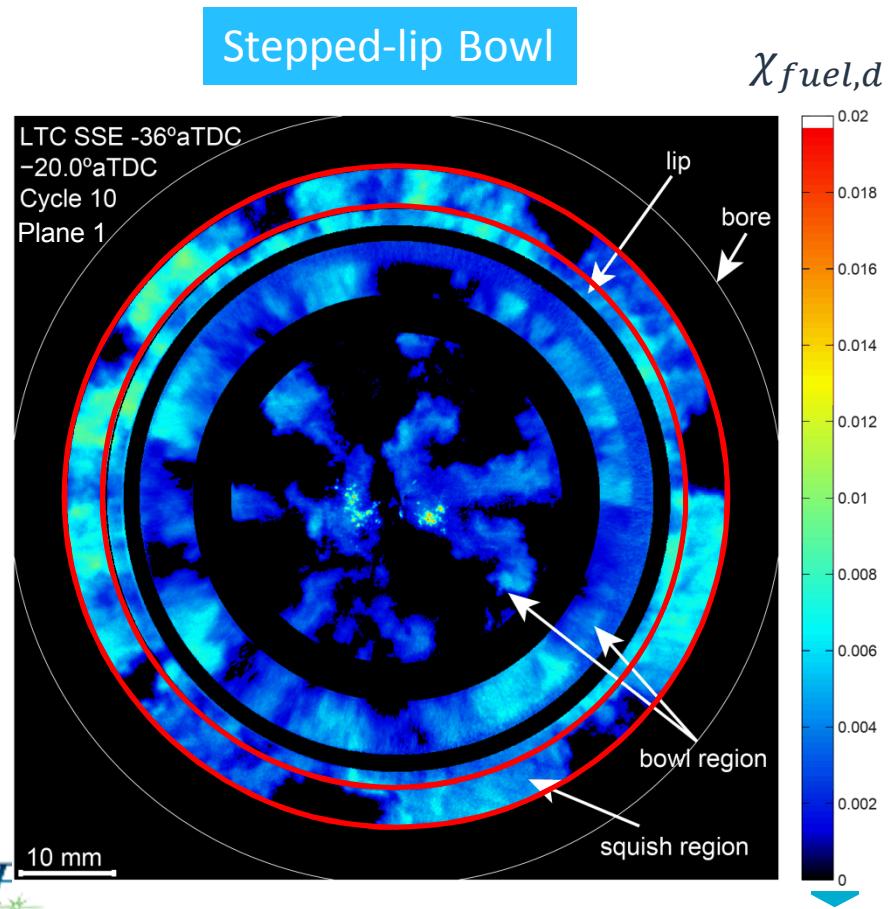
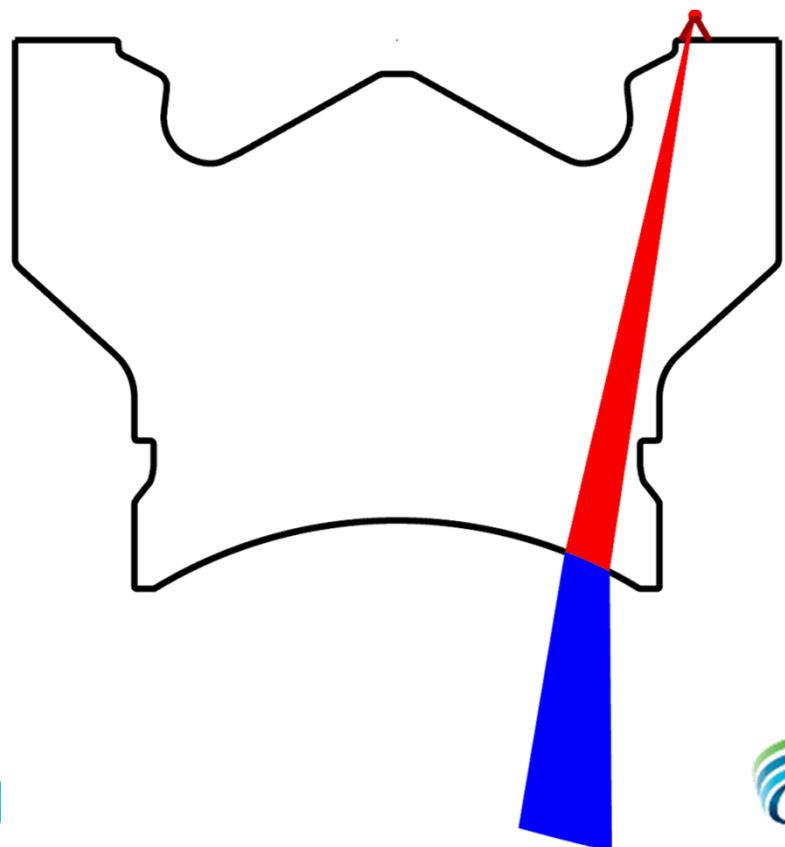
A sample of dewarped PLIF images with stepped-lip geometry



A sample of dewarped PLIF images with stepped-lip geometry



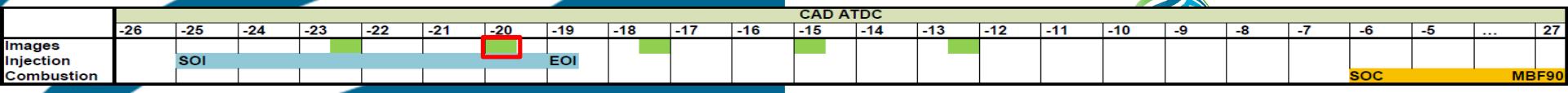
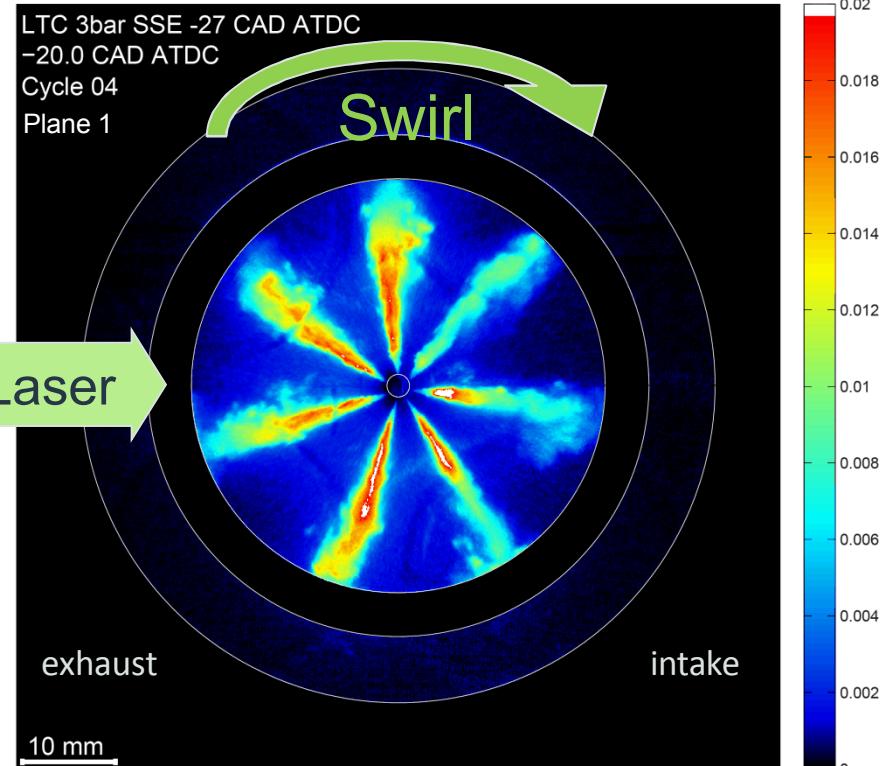
A sample of dewarped PLIF images with stepped-lip geometry



Uncertainties of PLIF measurements

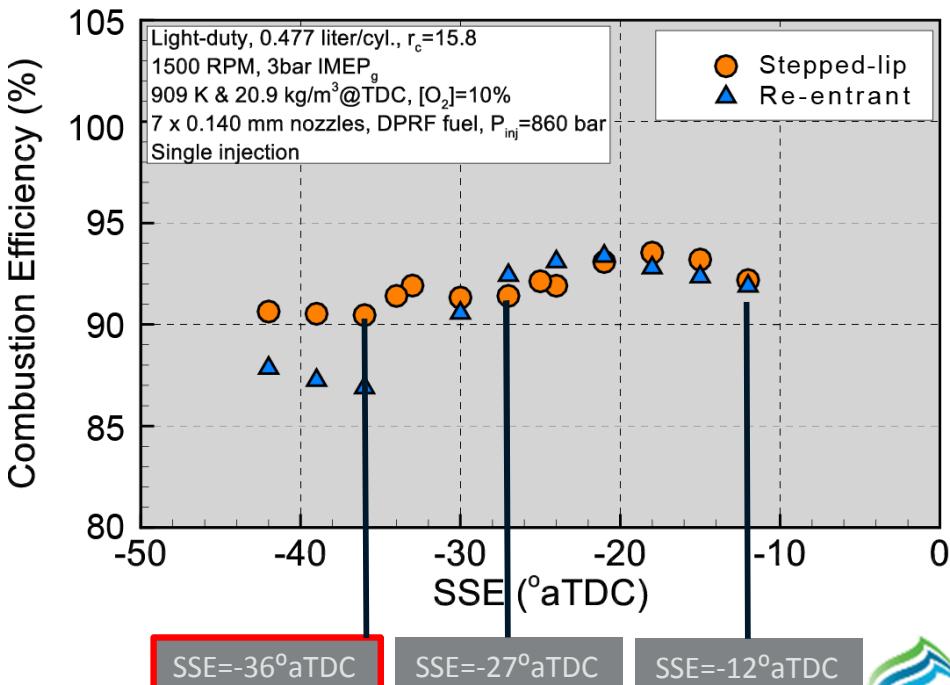
- Dewarping-induced error in radial locations: measurements near chamber center ($R < \sim 7\text{mm}$) is not reliable.
- Camera nonlinearity at high intensities.
- Beam steering effects start to show up in squish region when piston is within ± 15 CAD around TDC.
- Plumes facing the incoming laser produce more artifacts in measurements.

• Shadow caused by laser interference.
 • Out-of-plane fluorescence signal from liquid brought by laser beam and background reflection.
 • Fluorescence from ambient light
 • on chamber surface

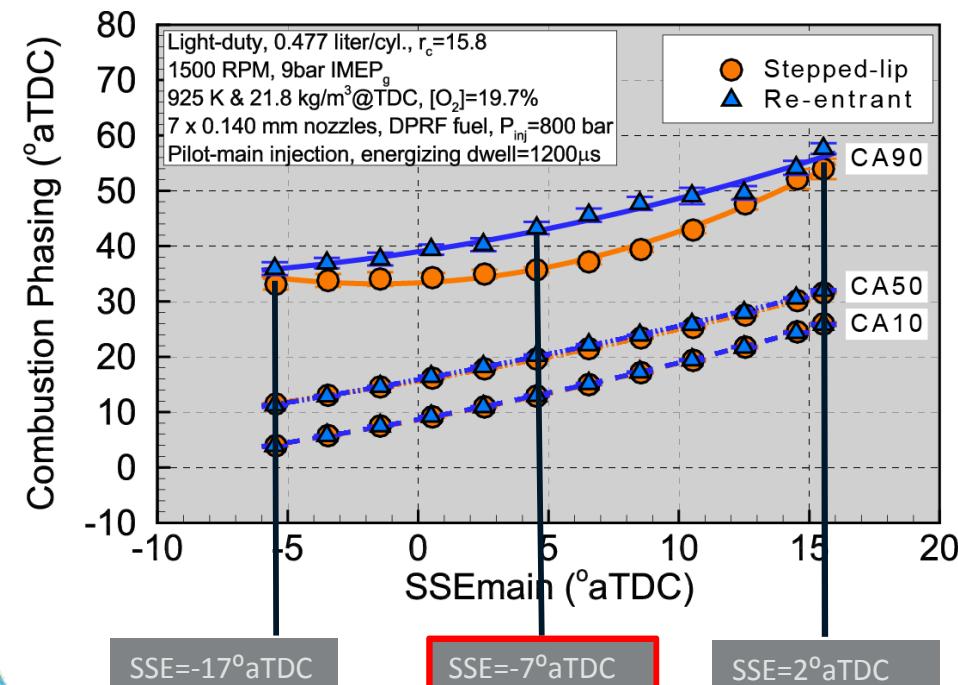


Points of interest for optical investigation

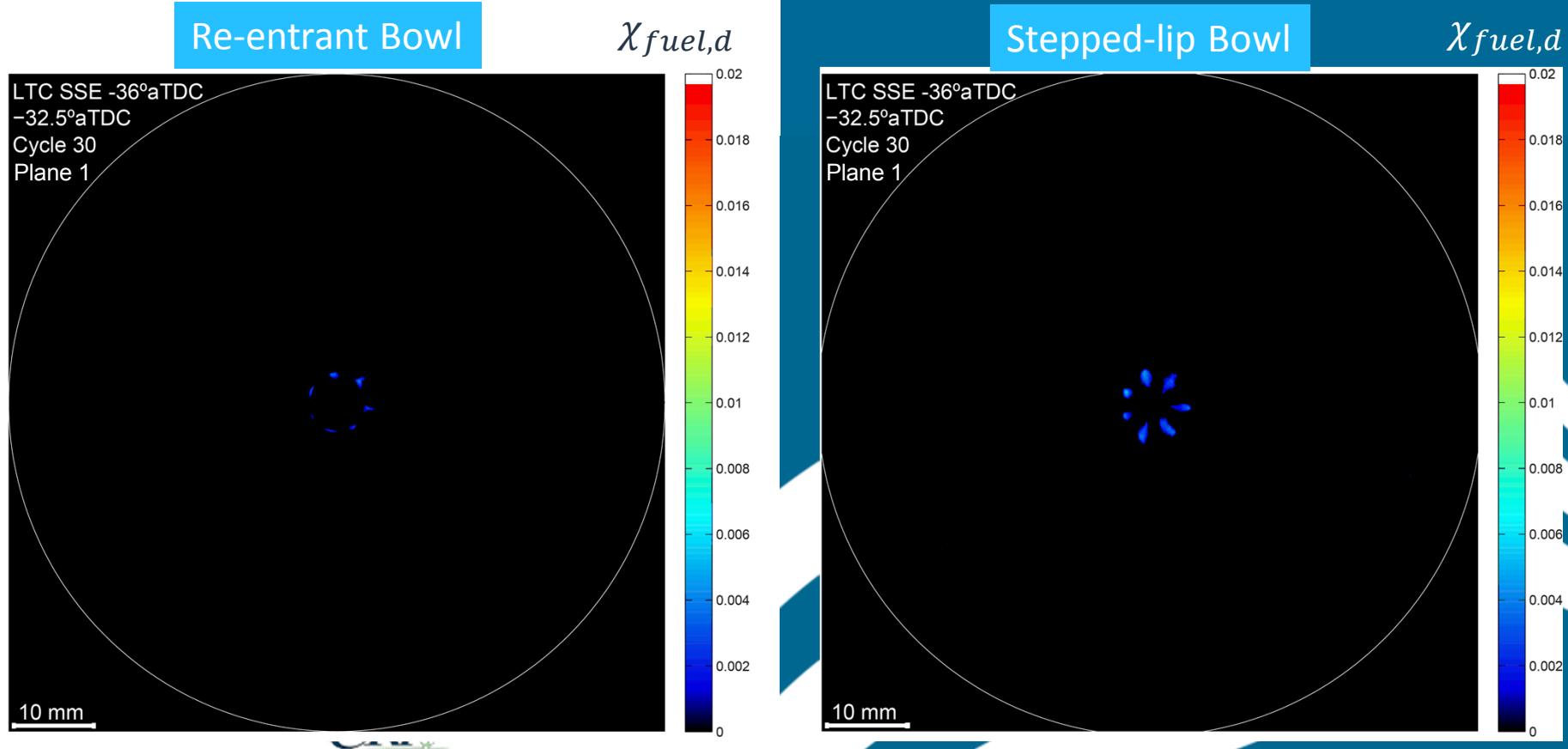
Single-injection, EGR-diluted LTC regime



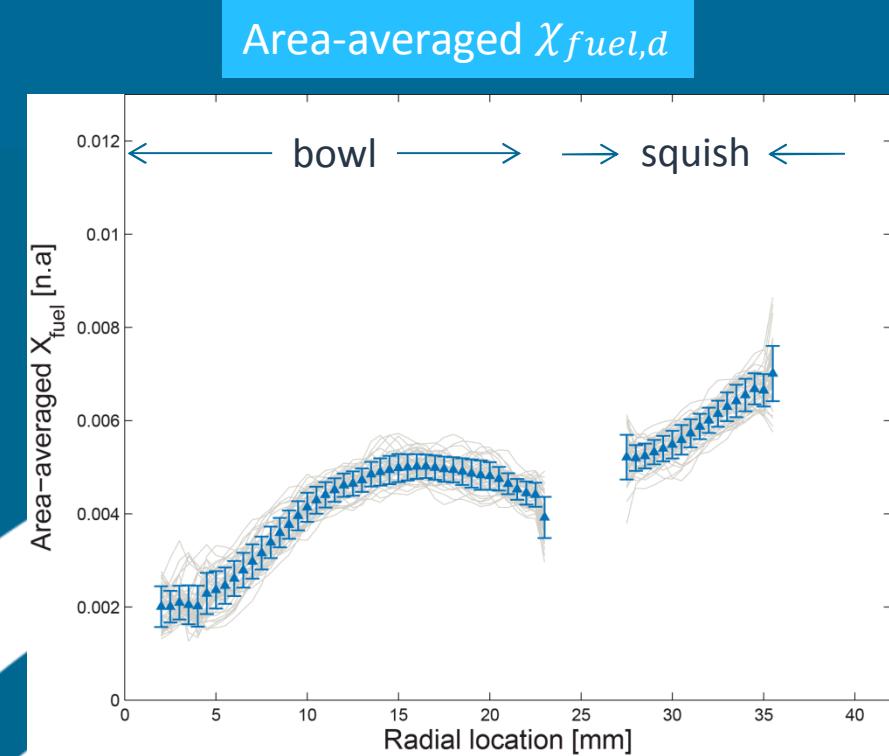
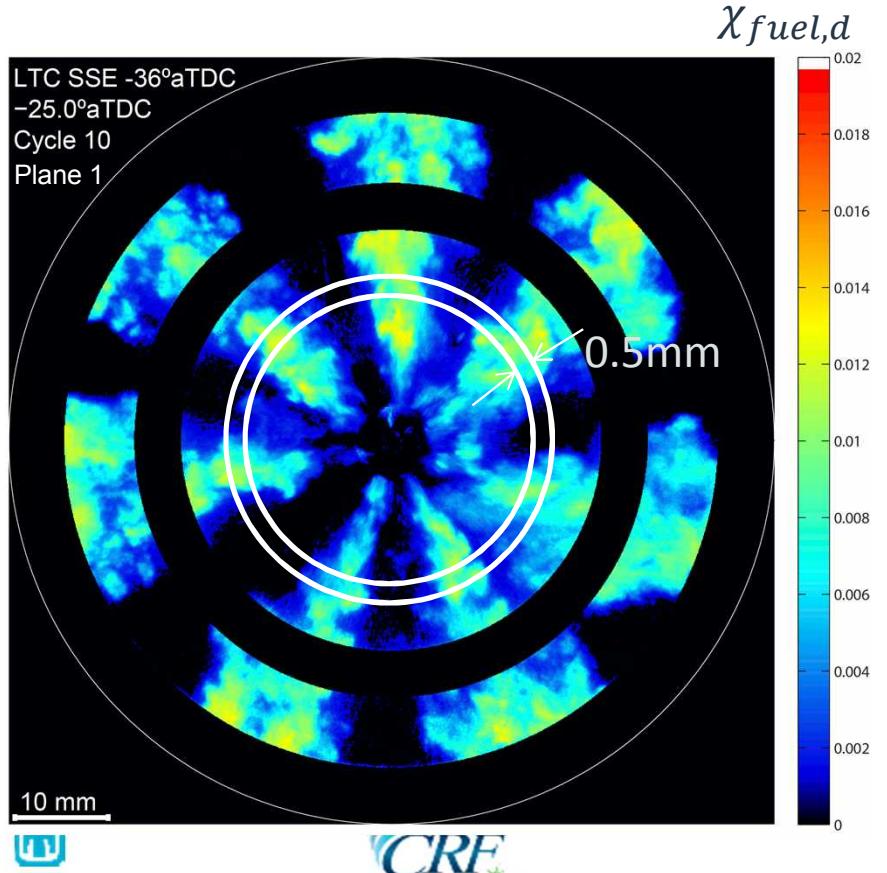
Double-injection, conventional combustion



Is there a simple metric to quantify piston geometry impact on in-cylinder mixture preparation?

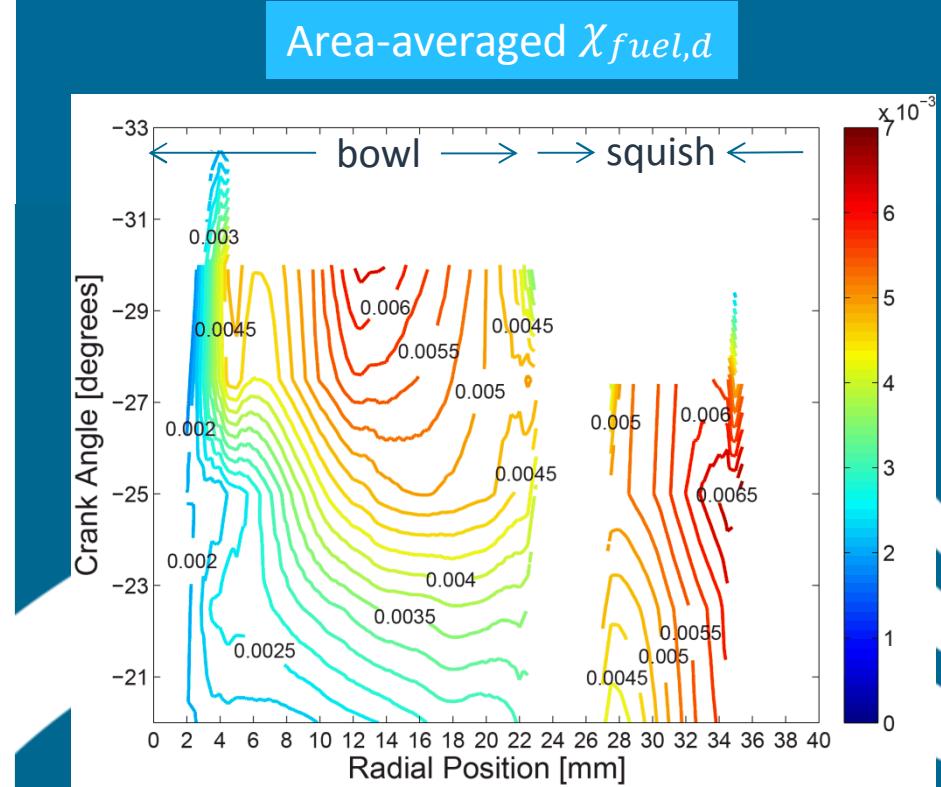
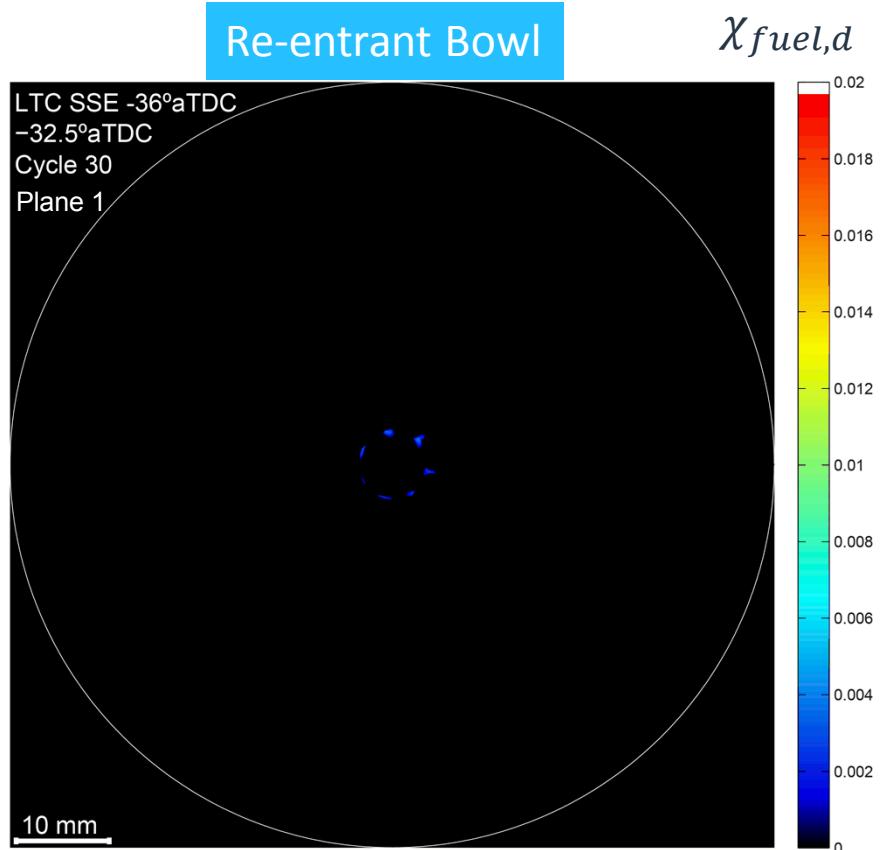


Area-averaged fuel mole fraction is calculated in polar coordinates to quantify spray-dominated mixture preparation pattern.

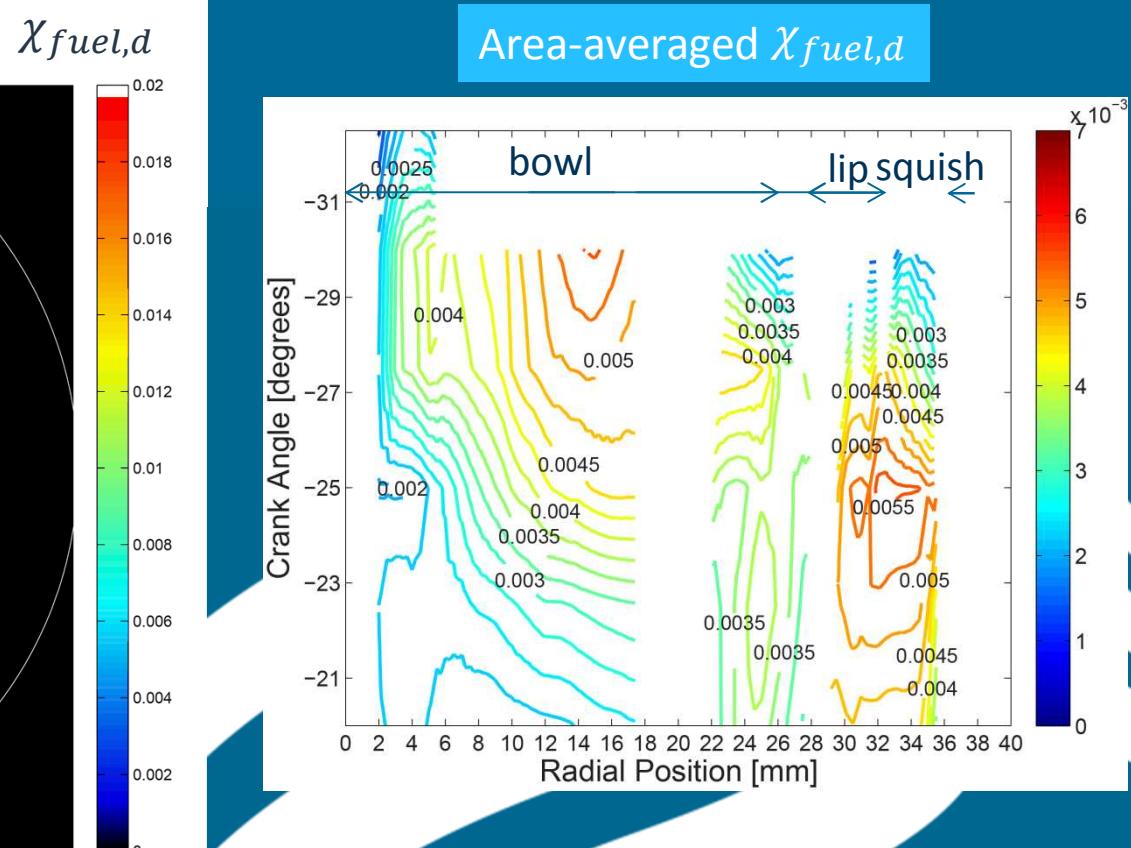
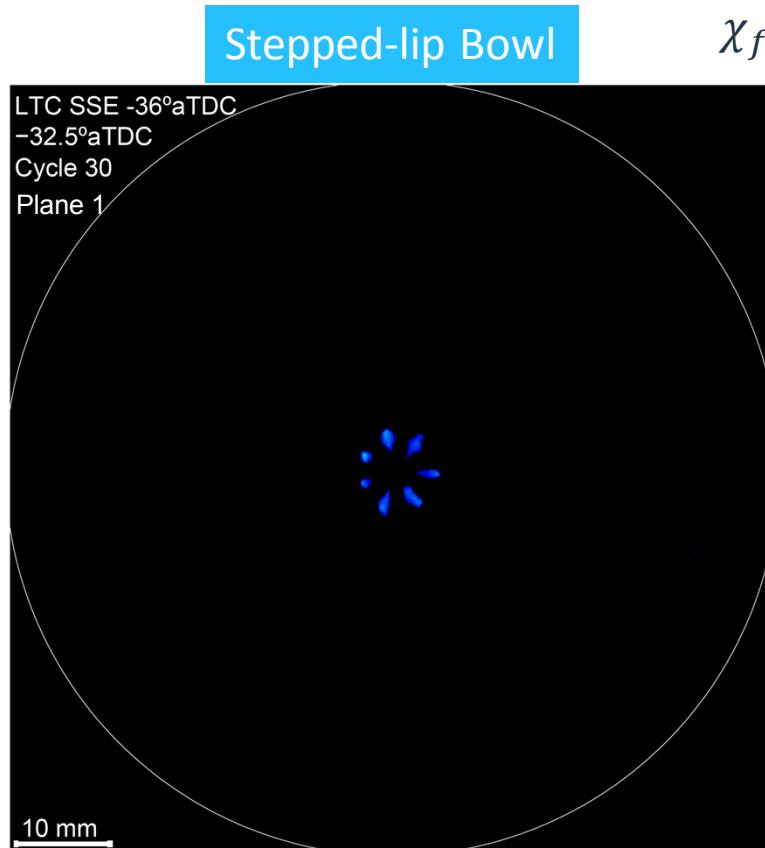


Error bar marks $\pm \sigma$ out of 50 realizations

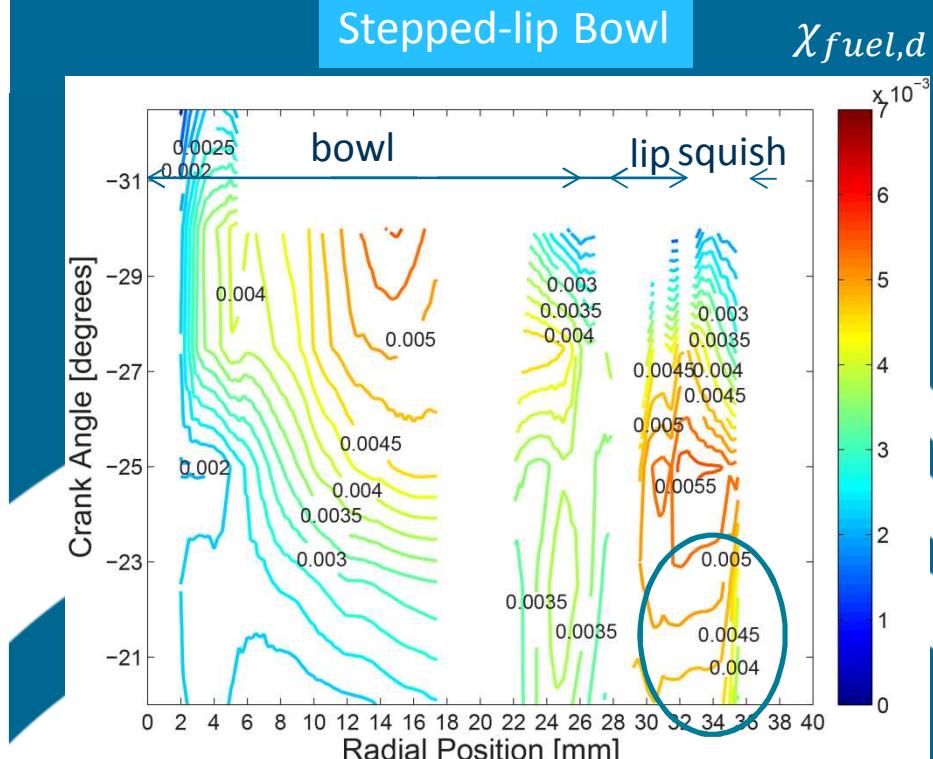
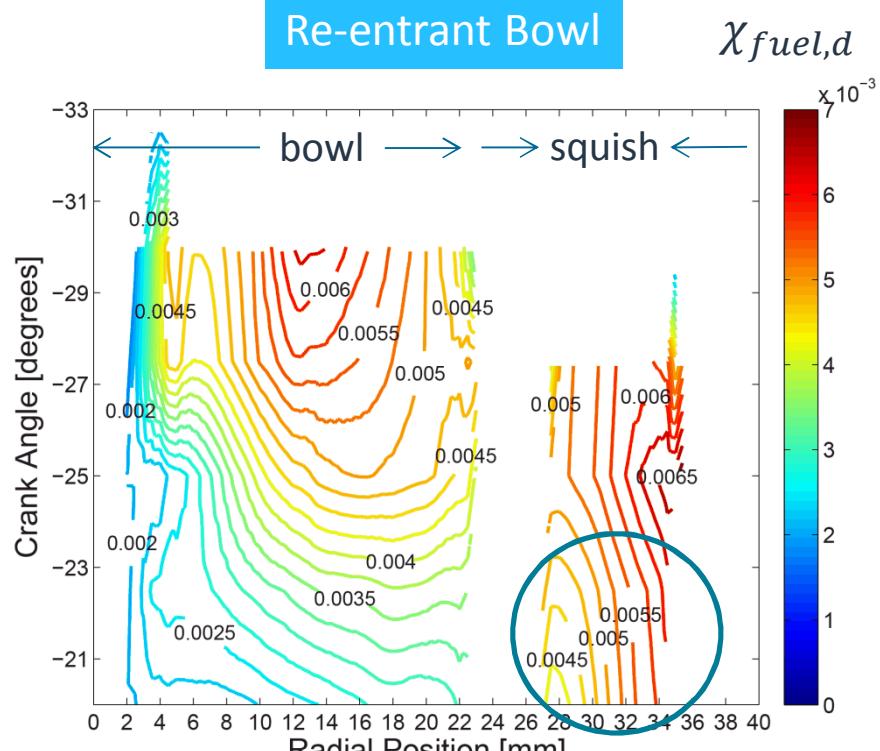
Area-averaged fuel mole fraction with re-entrant bowl under LTC regime



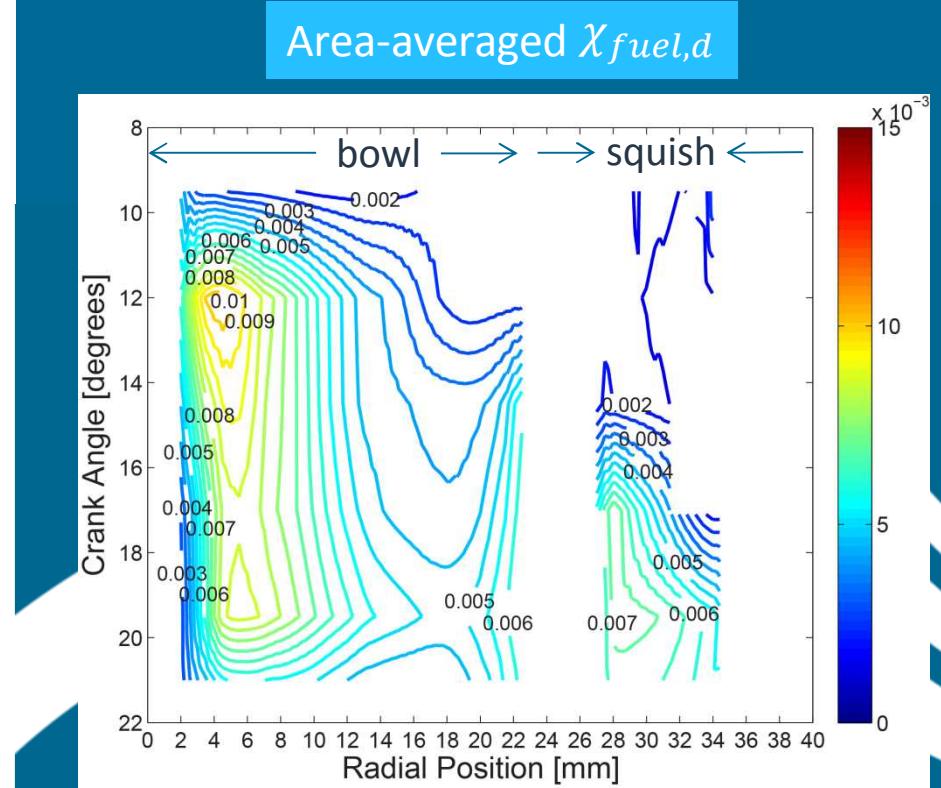
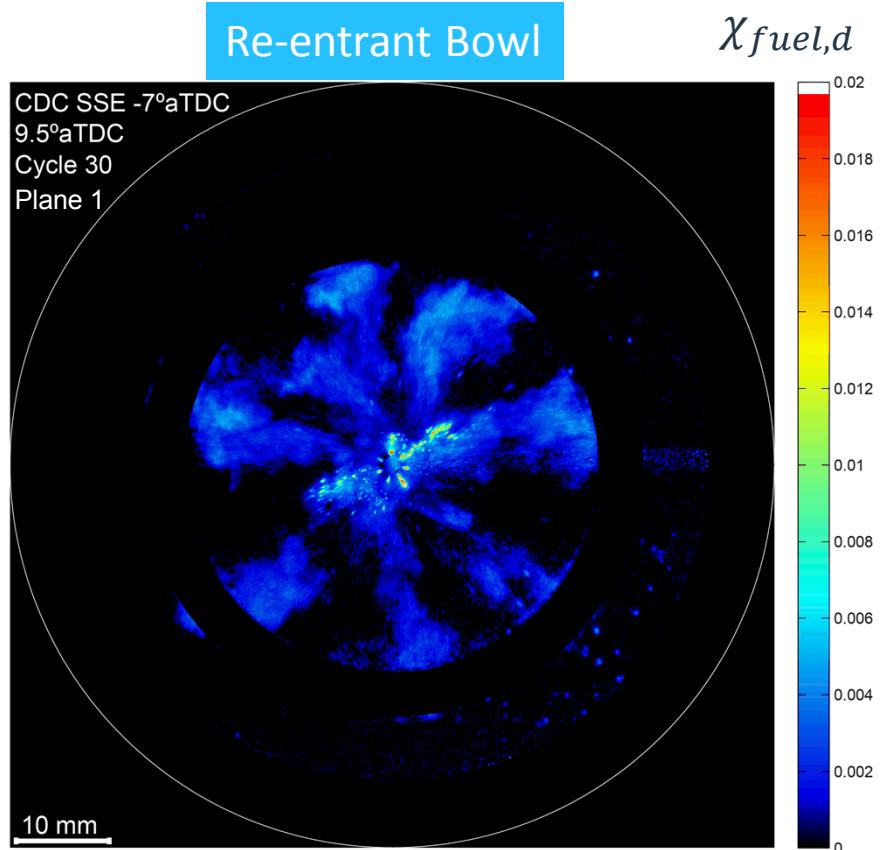
Area-averaged fuel mole fraction with stepped-lip bowl under LTC regime



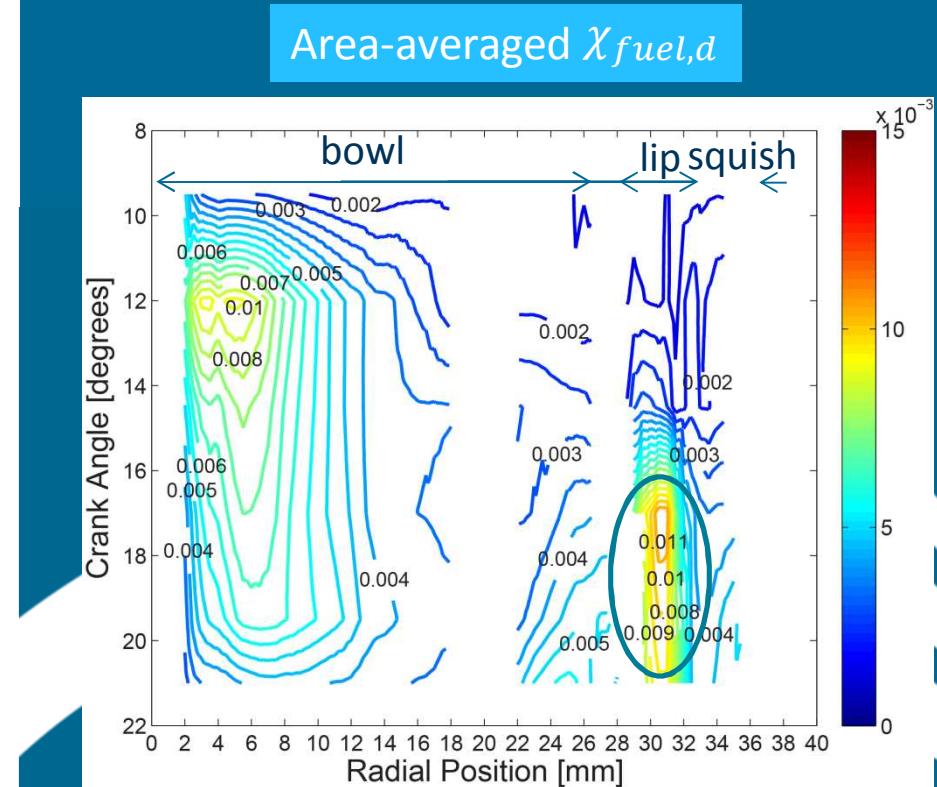
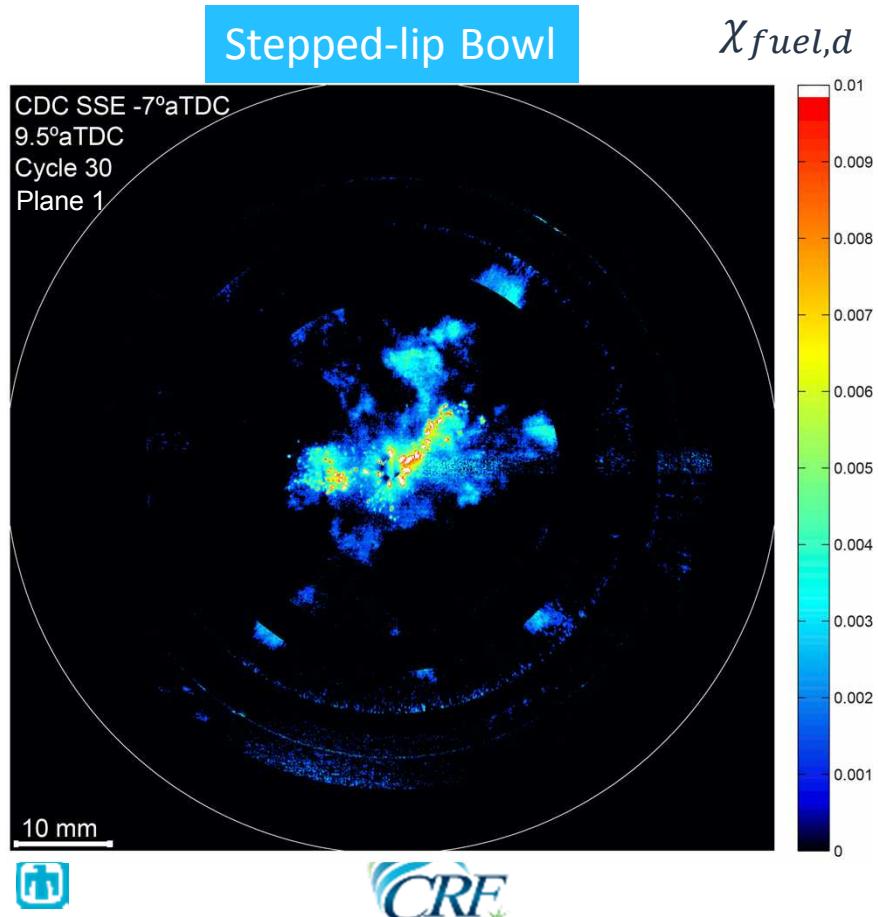
Stepped-lip piston exhibits leaner mixture formation in squish region under LTC regime.



Area-averaged fuel mole fraction with re-entrant bowl under CDC regime

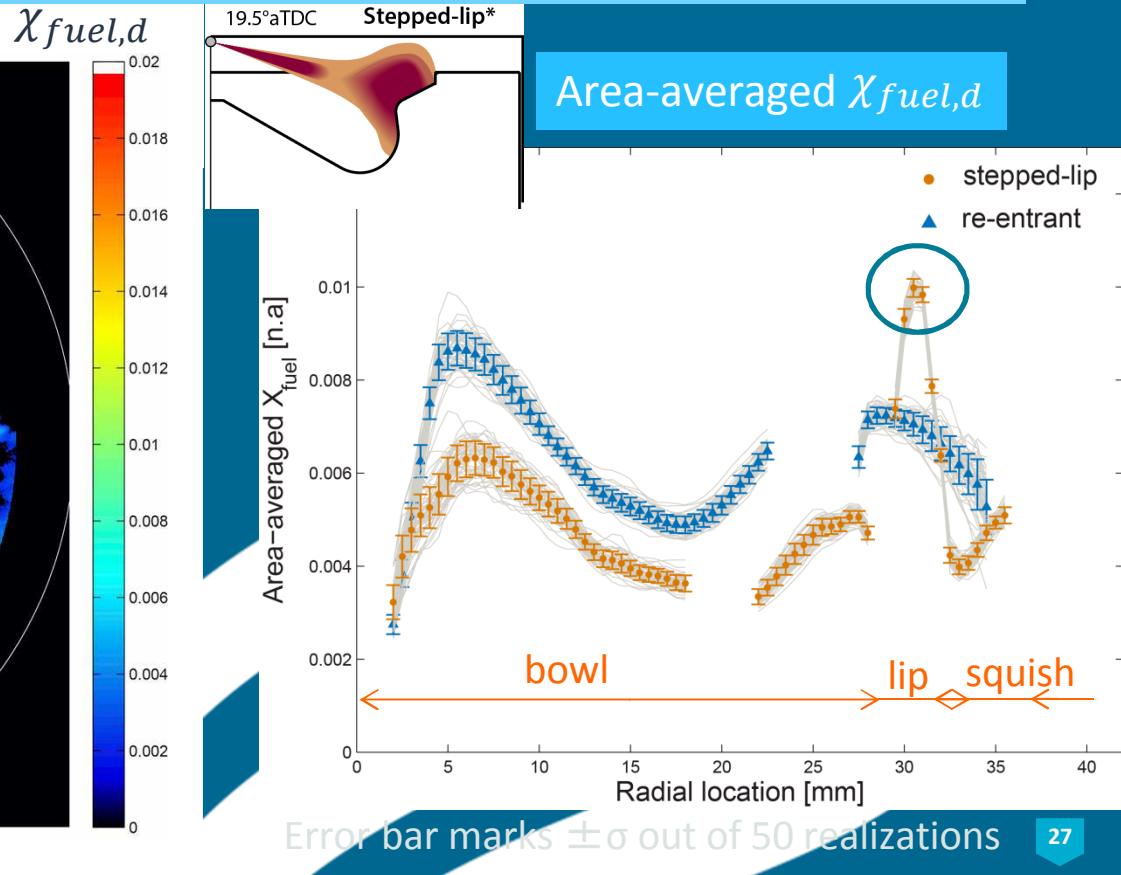
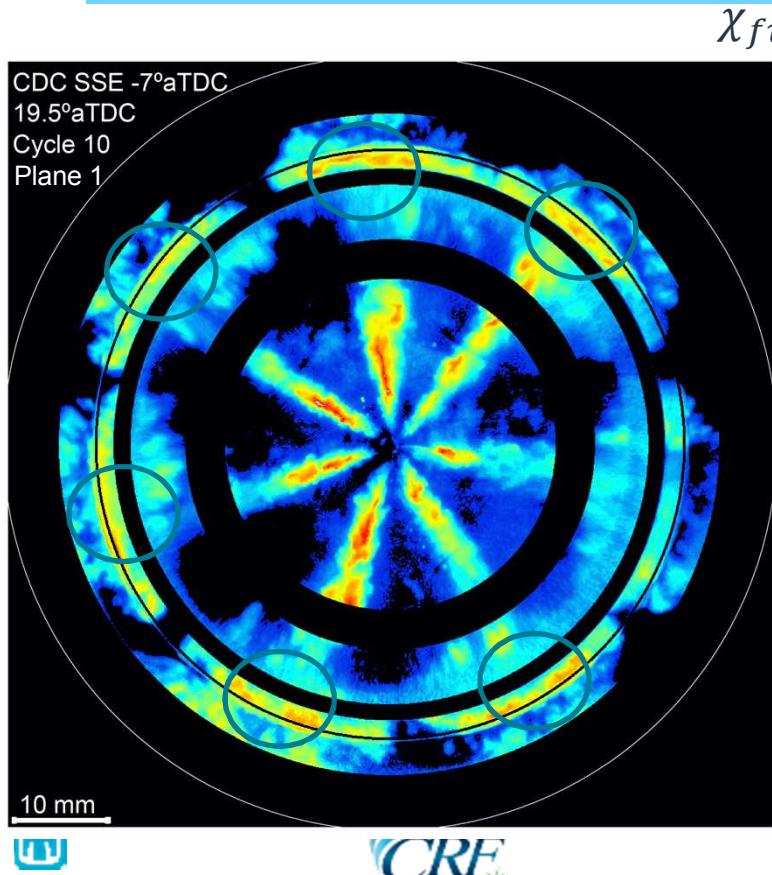


Area-averaged fuel mole fraction with stepped-lip bowl under CDC regime

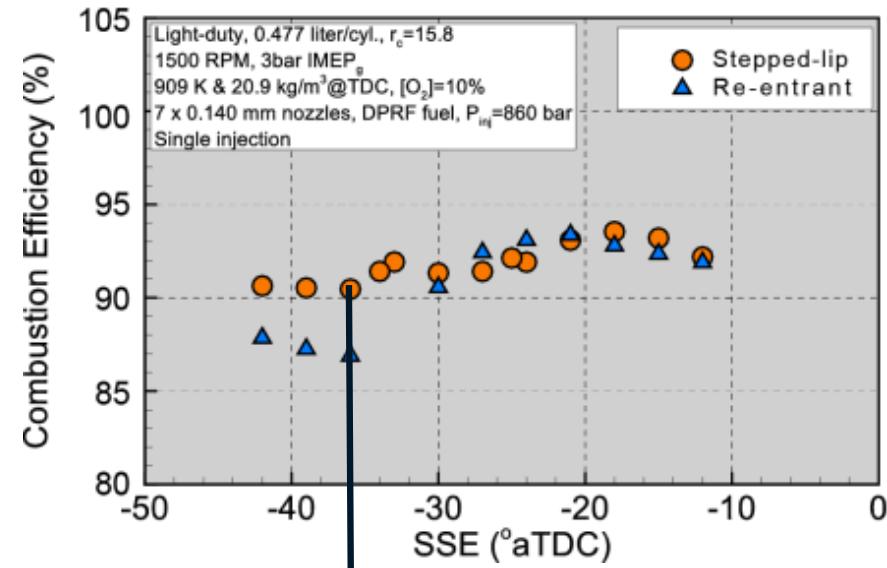
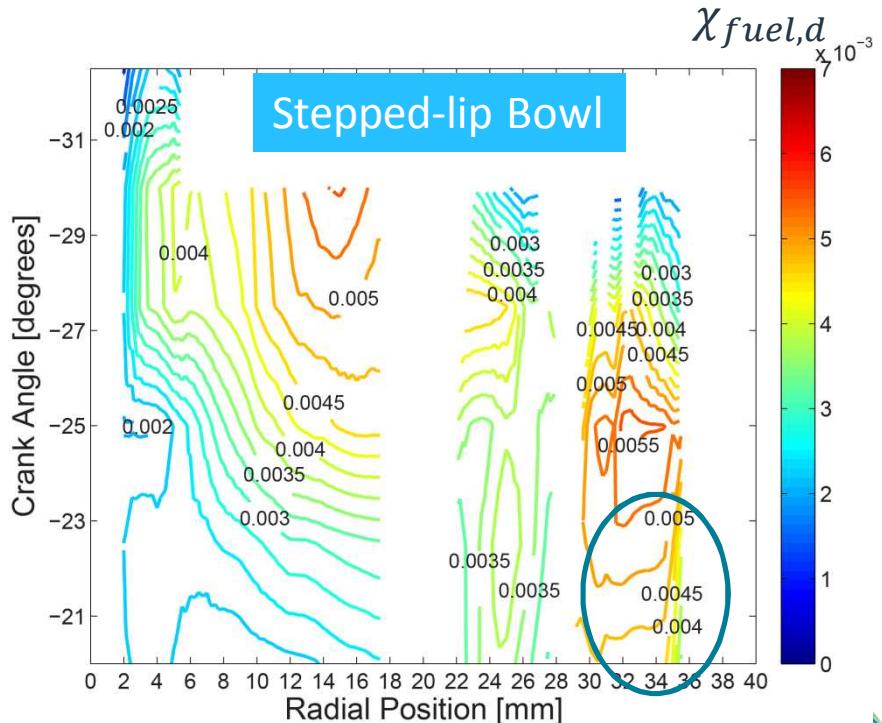


High $\chi_{fuel,d}$ is observed in lip region!

High $\chi_{fuel,d}$ observed in lip region implies better air utilization with stepped-lip piston geometry.

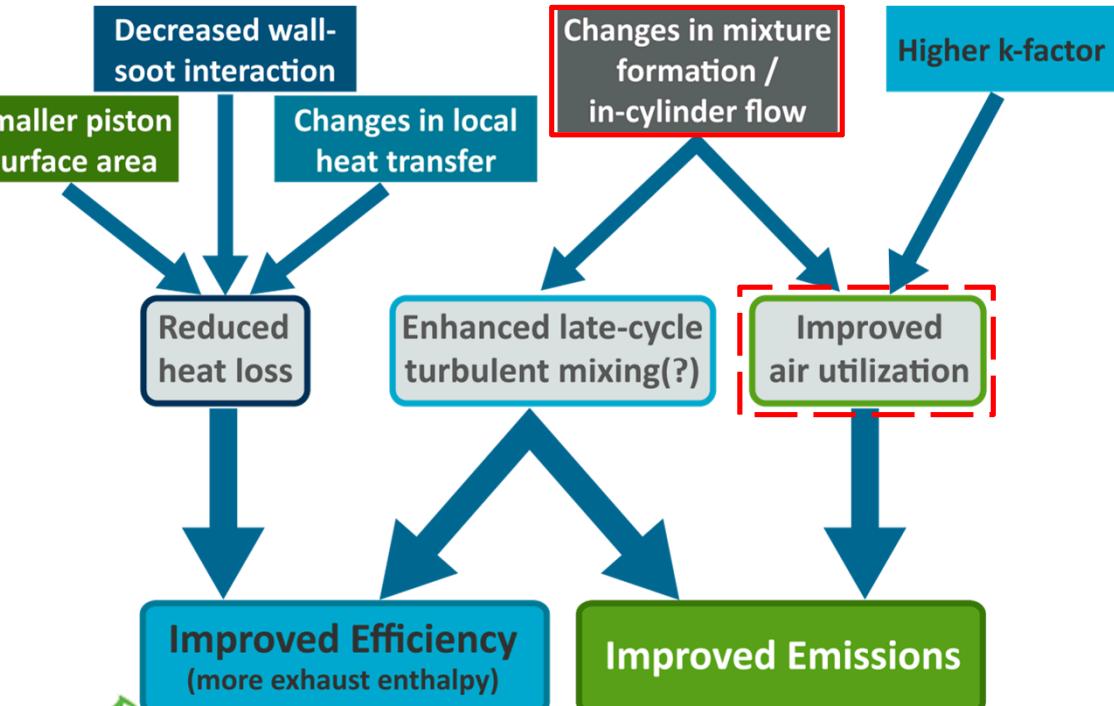
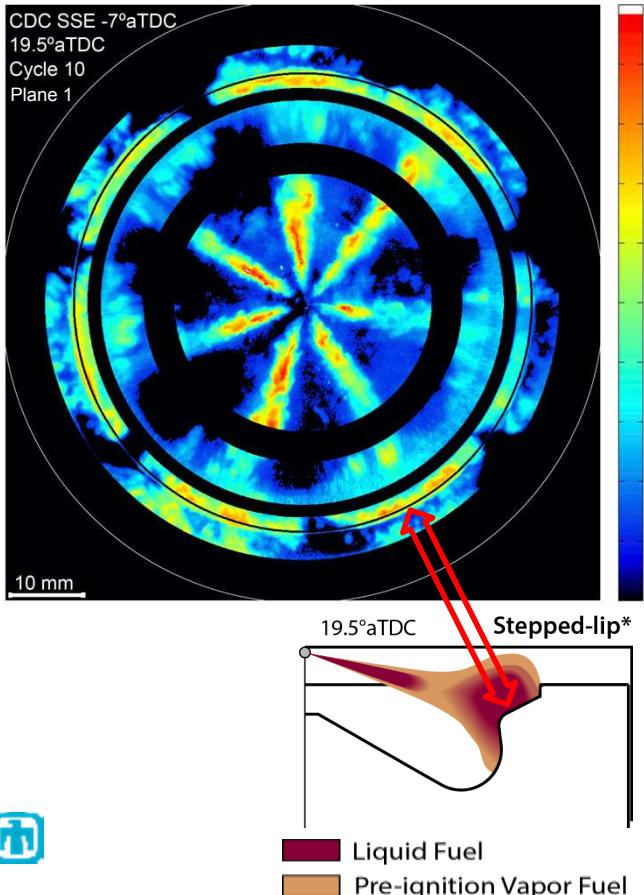


Conclusion - Stepped-lip bowl exhibits less squish area. In EGR-diluted LTC region, this geometry results in less CO from squish-region lean mixtures. Therefore, higher combustion efficiency.



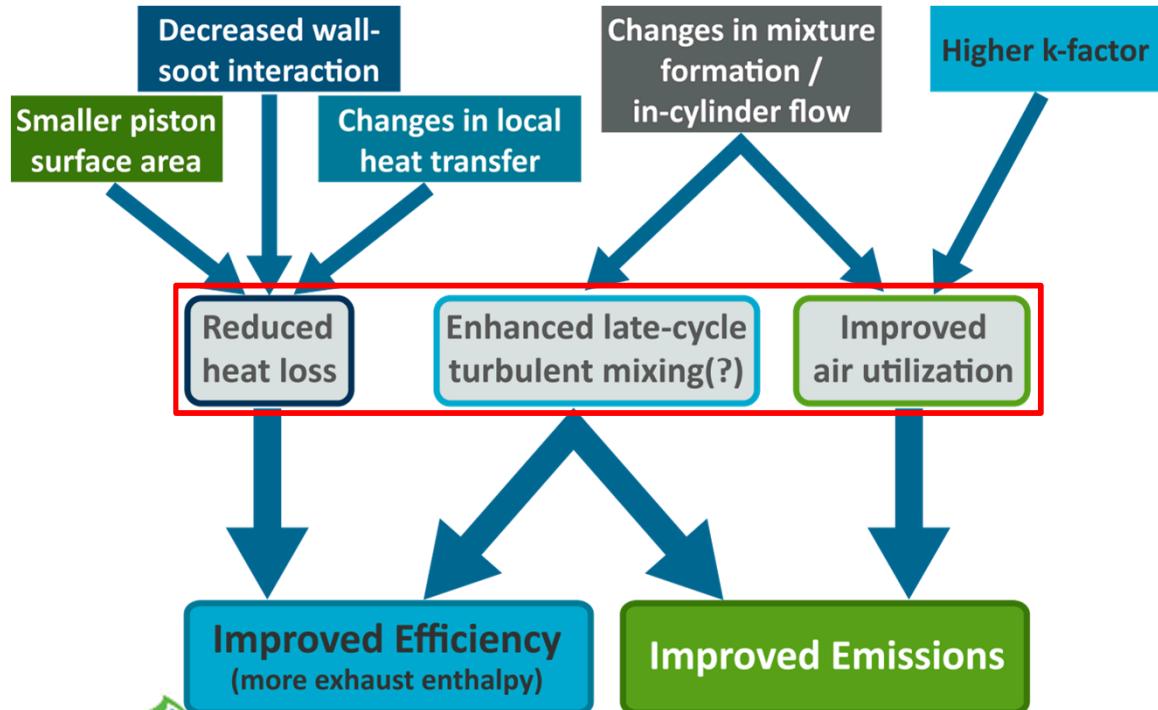
SSE=-36°aTDC

Conclusion - Stepped-lip geometry results in localized high fuel concentration on lip shoulder, which implies better air utilization.



Future work: Understanding the geometry-induced mechanisms for increased heat release rates and higher efficiency.

- Optical experiments: SNL
 - High-speed soot natural luminosity imaging
- Computational studies: UW
 - Bowl geometry, fuel injection, and combustion impact on in-cylinder flow
 - Speed / load /spray targeting sensitivities



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- Tim Gilbertson, R&D Technologist, Sandia



Thank you for your attention!

Questions?



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PLIF: computation of fuel concentrations

- $\chi_{fuel,d} = \chi_{fuel,cal} \frac{S_d}{S_{cal}} \frac{E_{cal}}{E_d} \frac{T_d}{T_{cal}} \frac{P_{cal}}{P_d} \frac{\sigma\eta(T_{cal})}{\sigma\eta(T_d)}$
 - S : background-subtracted, distortion-corrected image intensity
 - E : measured laser pulse energy
 - T : bulk gas temperature from GT-Power model
 - P : cylinder pressure from GT-Power model
 - $\sigma\eta$: product of absorption cross section and quantum yield; function of temperature alone
- Calibration with homogeneous mixture of known concentration ($\chi_{fuel,cal}$)
 - “Flat-field” correction
- $\sigma\eta(T)$ is determined with separate measurements and analyses

PLIF temperature calibration

- $\sigma\eta(T)$ determined from flat-field images taken at various crank angles and for various intake temperatures
- Upper limit of possible flat-field fuel concentrations limited by wall-wetting
 - $\phi_{ff} \approx 0.3$
- Comparison with previous temperature calibration
 - Coefficients between 14-18% higher than previously determined values
 - The arbitrary normalization of the calibration curve is responsible for the majority of this discrepancy
- Future plans include expanded calibration dataset

