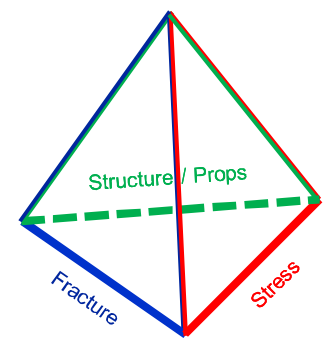
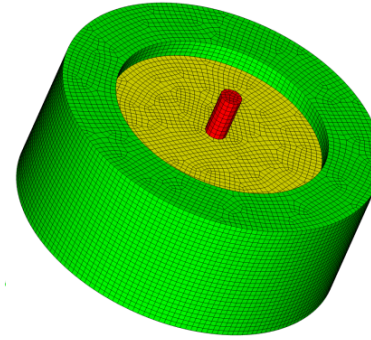
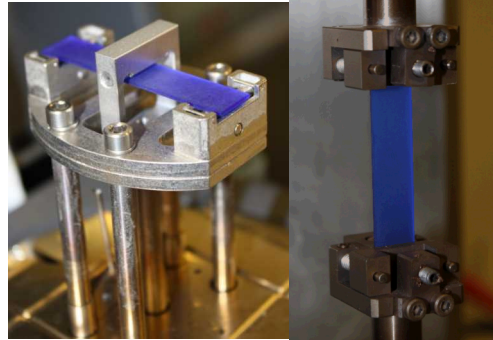
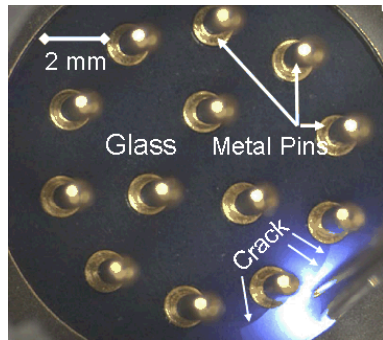


Exceptional service in the national interest



Characterizing and Predicting Stress and Structural Relaxation in Glass

^aKevin T. Strong Jr, ^bBrenton Elisberg, ^bRyan D Jamison,
and ^cKevin G Ewsuk

Glass and Optical Materials Division Meeting

May 24, 2016

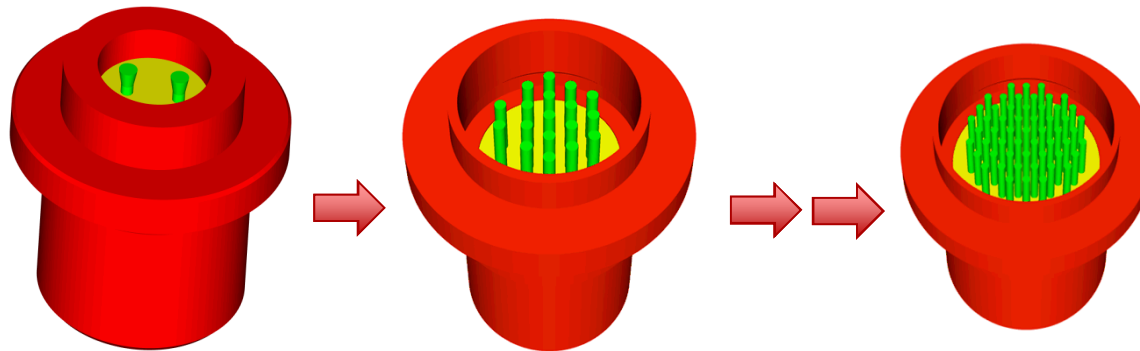
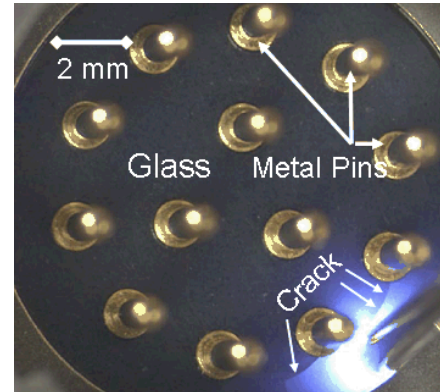
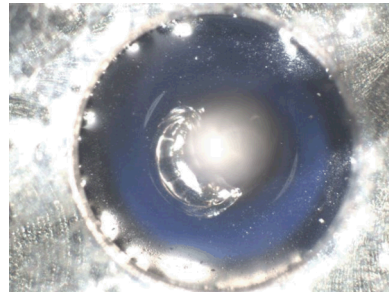
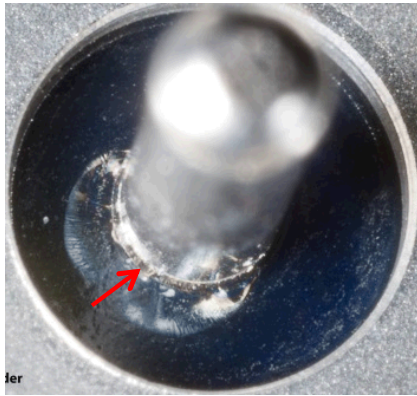


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Outline

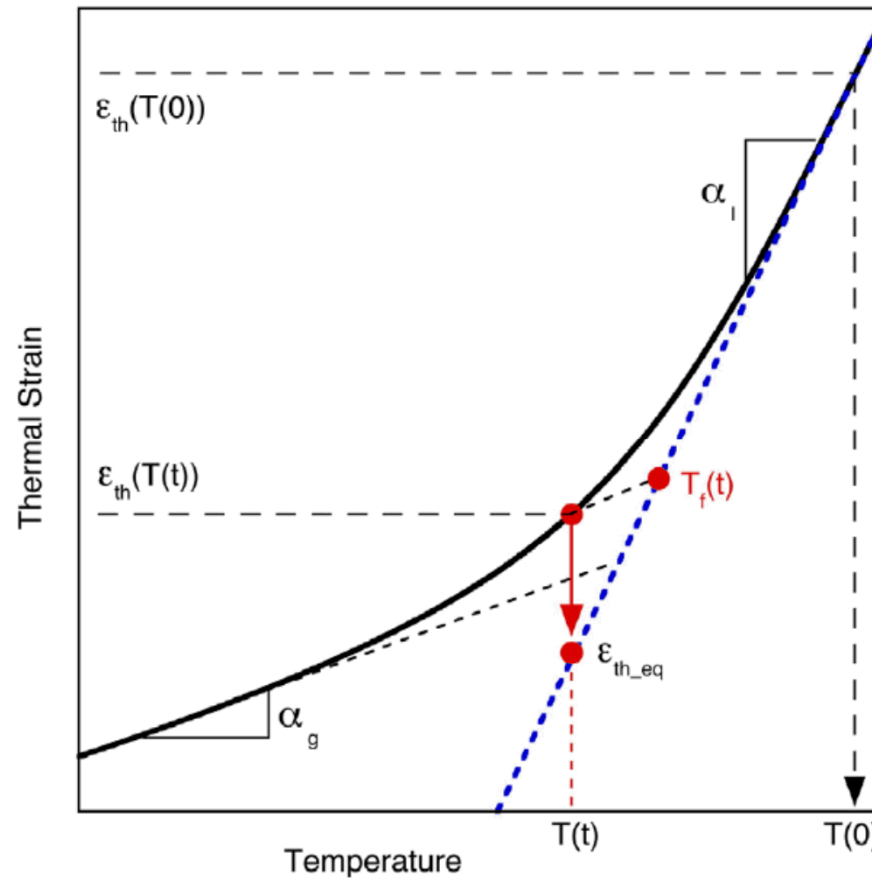
- Motivation
- Approach
- Model Calibration Experiments
- Model Validation
- Current Applications
- Conclusions

Motivation – Glass to Metal Seals

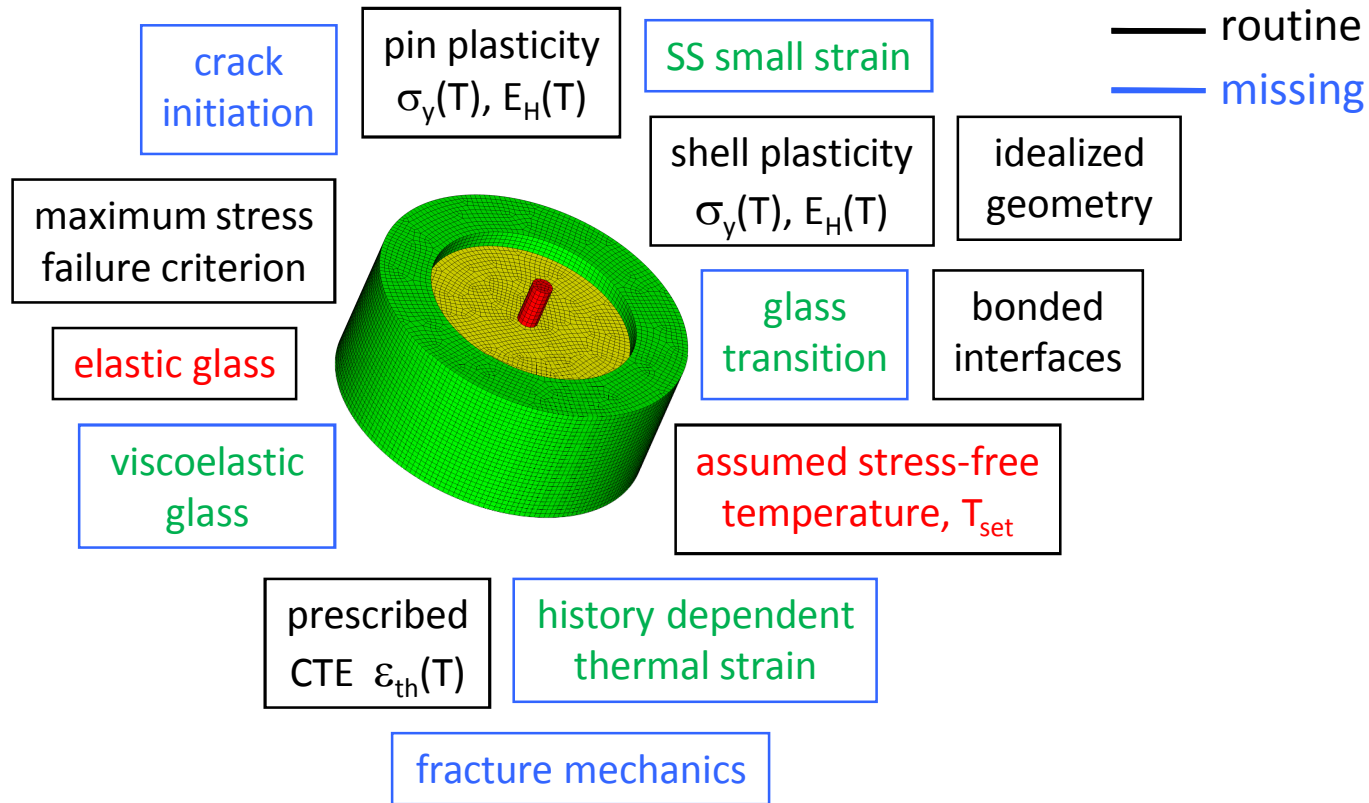


Higher fidelity stress modeling is needed to address shrinking performance margin in more complex designs

Background – Structural Relaxation



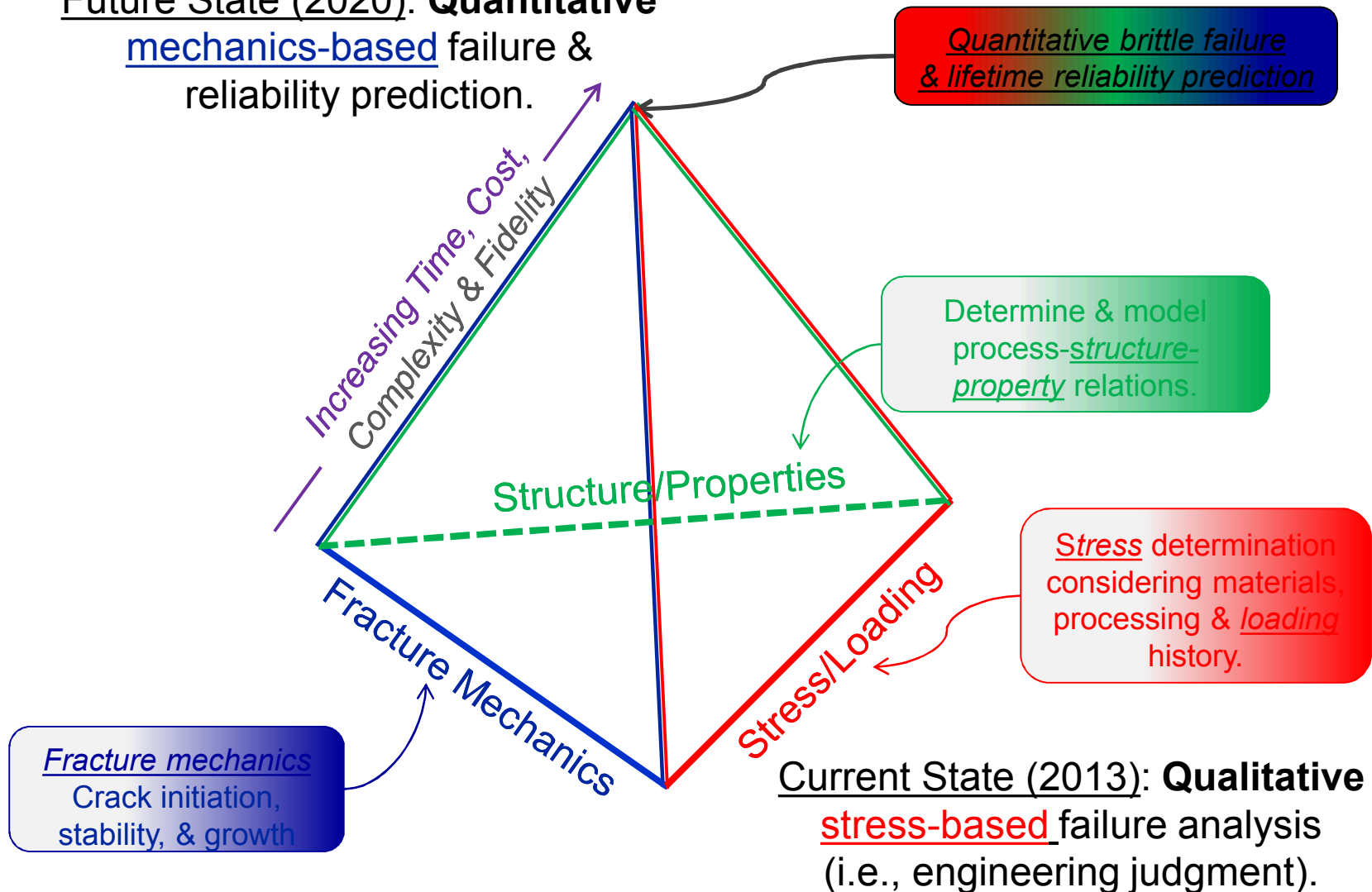
Finite Element (FE) Modeling Predicts Residual Stress In Glass-to-Metal Seals



Higher fidelity stress modeling is possible with improved materials behavior models

BrittMAPP – Brittle Materials Assurance Predictability Program

Future State (2020): **Quantitative**
mechanics-based failure &
reliability prediction.



Simplified Potential Energy Clock (SPEC) Model

Journal of Non-Crystalline Solids 432 (2016) 545–555



Contents lists available at [ScienceDirect](#)

Journal of Non-Crystalline Solids

journal homepage: www.elsevier.com/locate/jnoncrysol



Characterization and calibration of a viscoelastic simplified potential energy clock model for inorganic glasses



Robert S. Chambers^{a,*}, Rajan Tandon^b, Mark E. Stavig^c

^a Engineering Sciences Center, Sandia National Laboratories, Albuquerque, NM 87185–0346

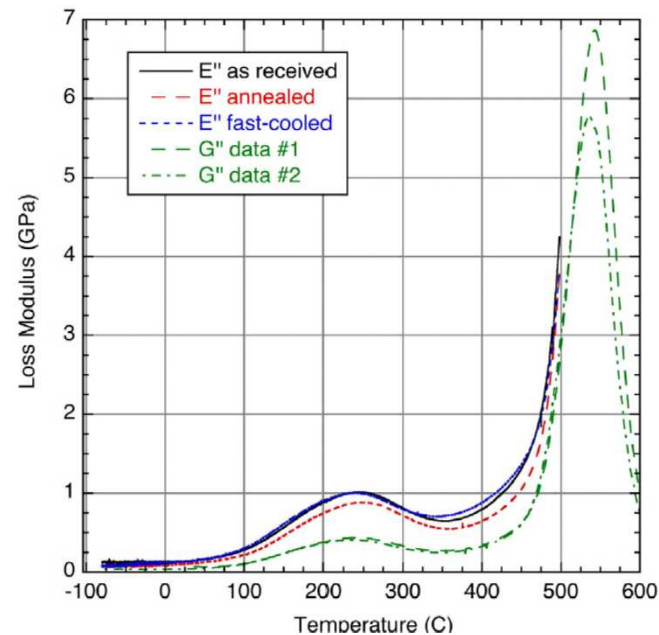
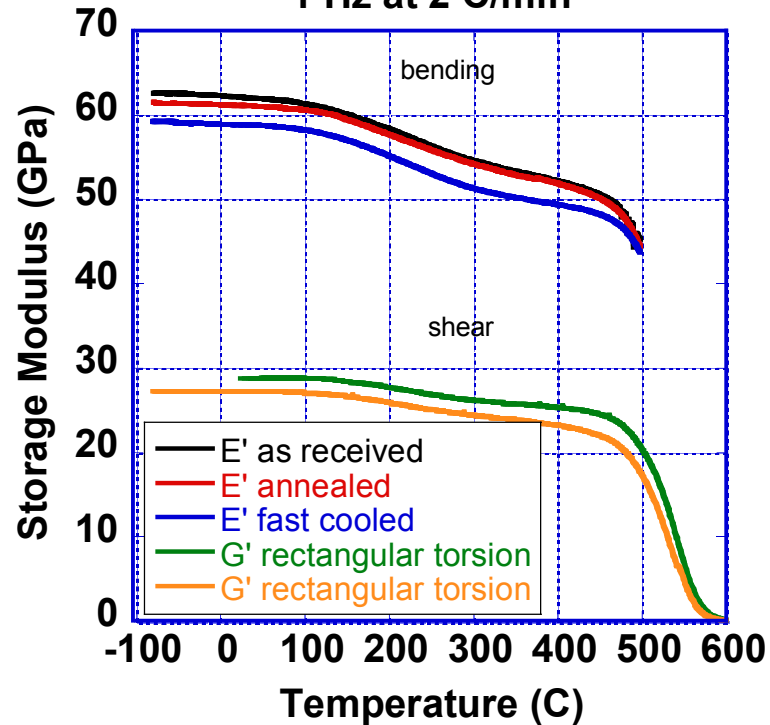
^b Analytical Technologies Department, Sandia National Laboratories, Albuquerque, NM 87185–0871

^c Materials Science and Engineering Center, Sandia National Laboratories, Albuquerque, NM 87185–0958

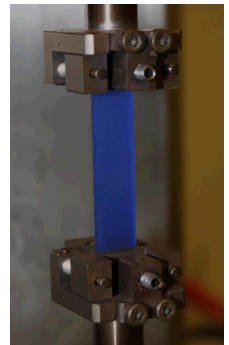
Dynamic Mechanical Analysis

Temperature Sweep

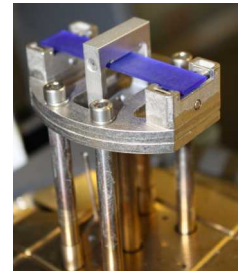
S8061 Temperature Sweep
1 Hz at 2 C/min



TA ARES
Rheometer

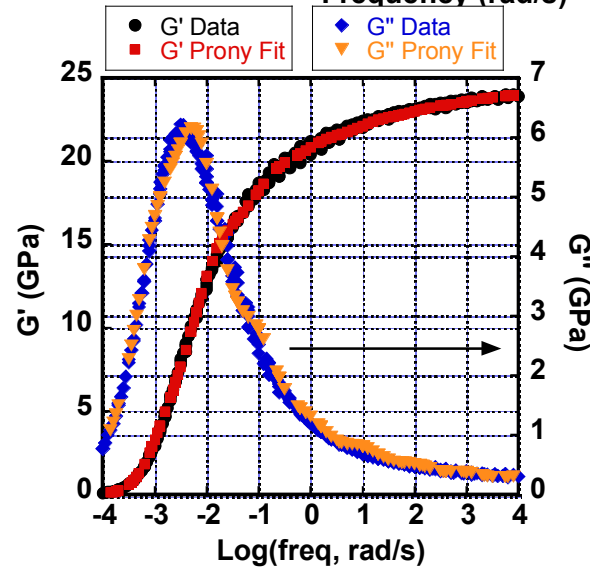
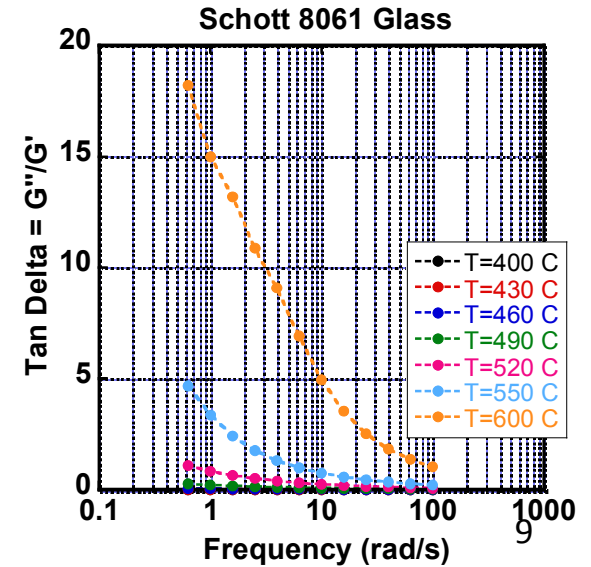
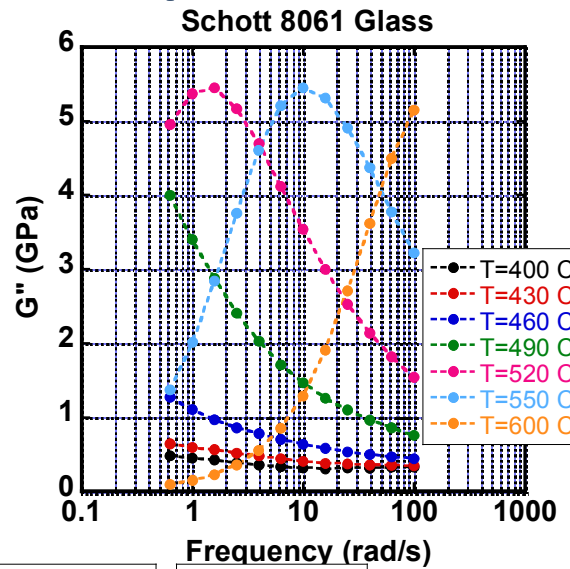
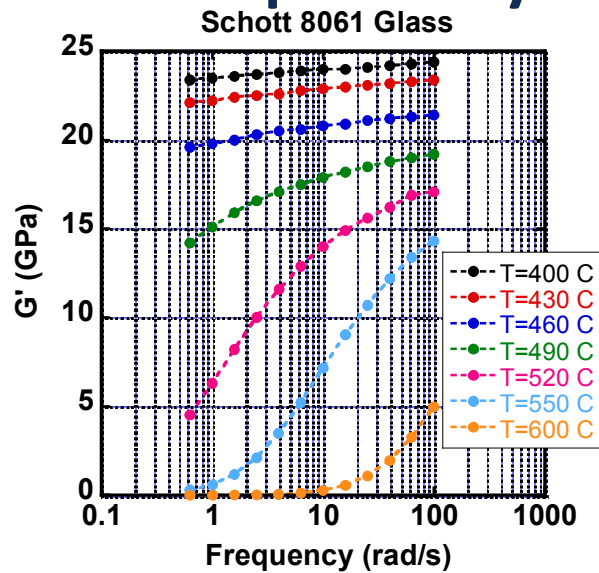


TA Q800 DMA

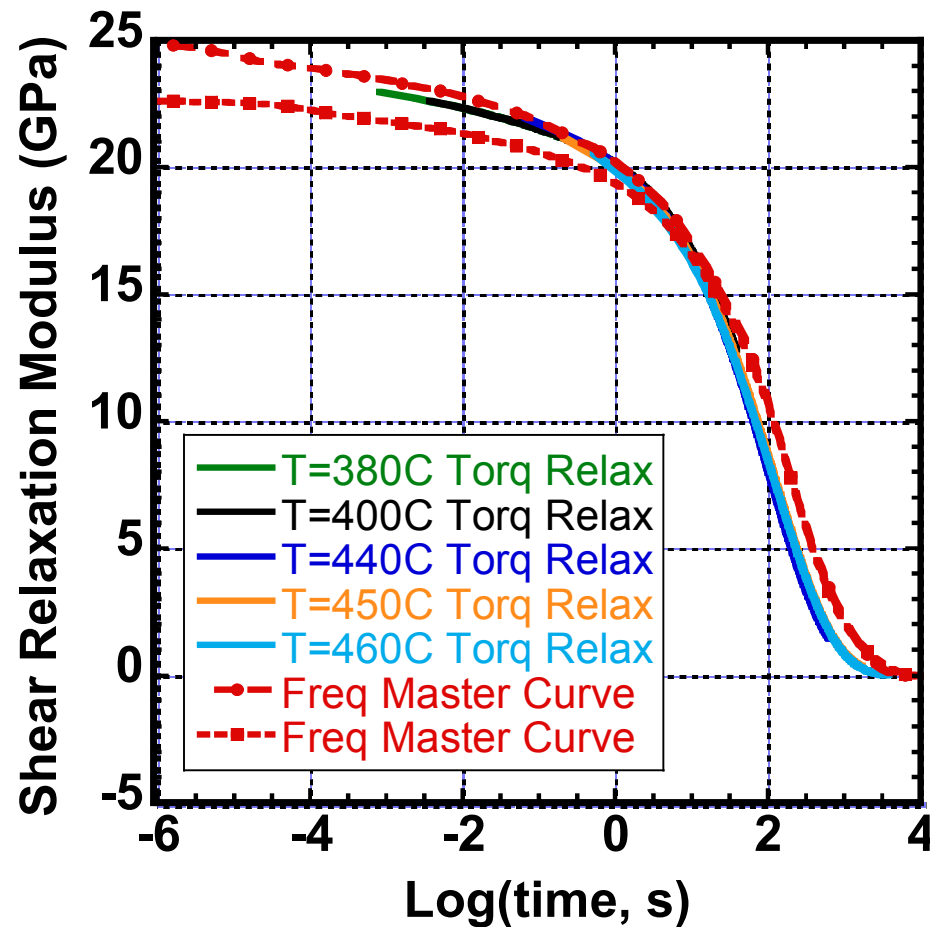


Dynamic Mechanical Analysis

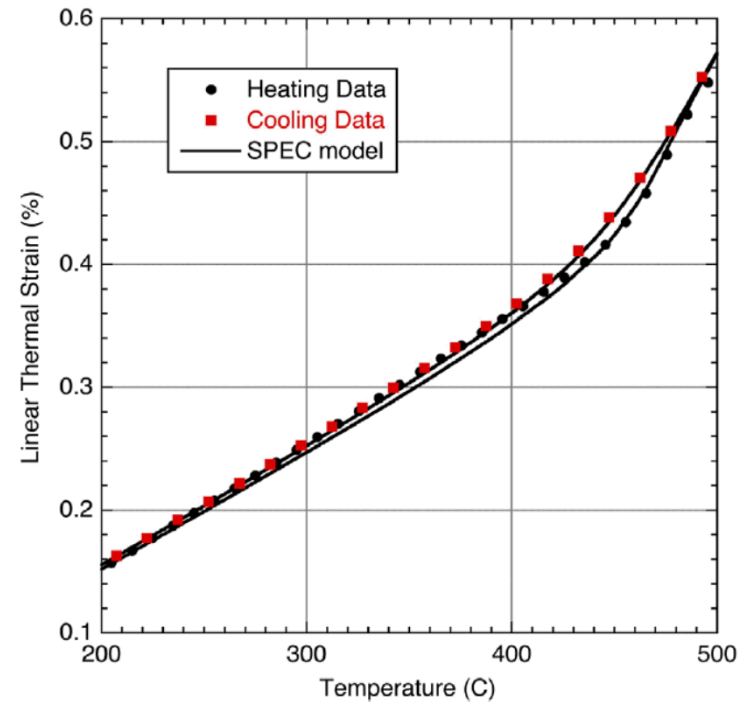
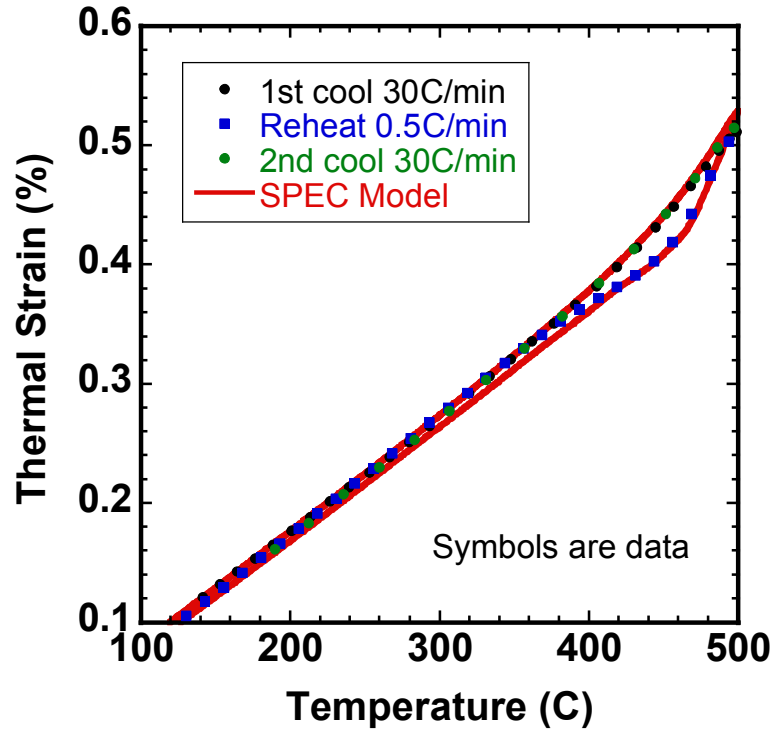
Frequency Sweep



Constructing time based master curve

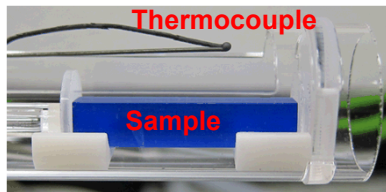
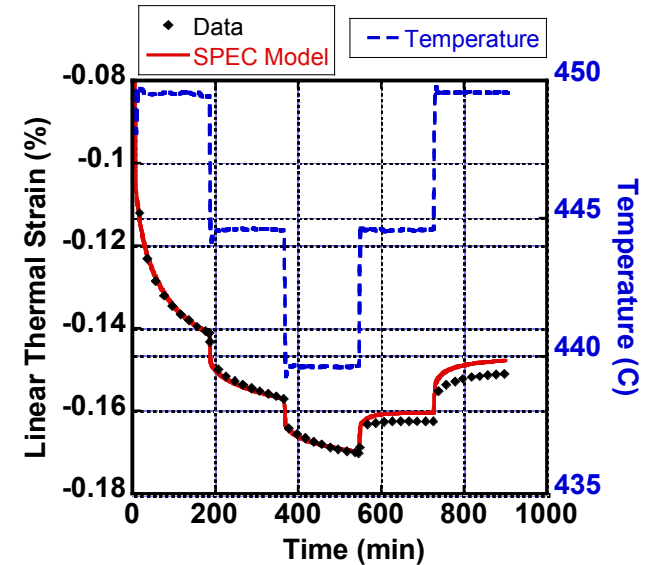
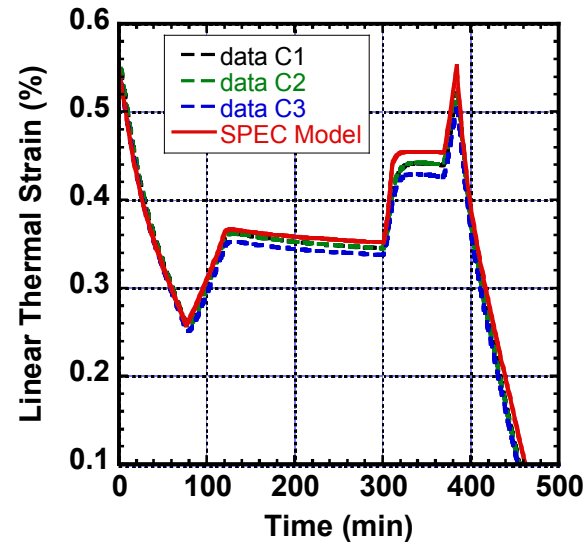
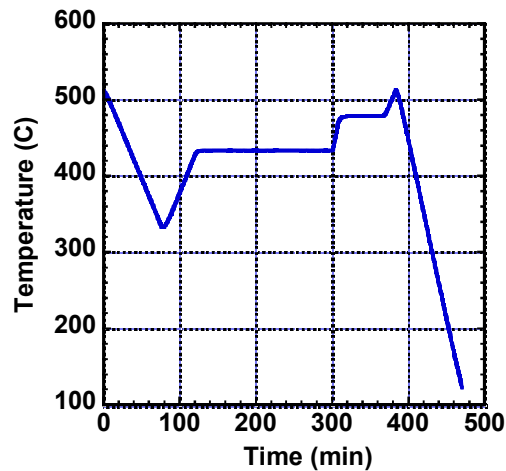


Model Calibration



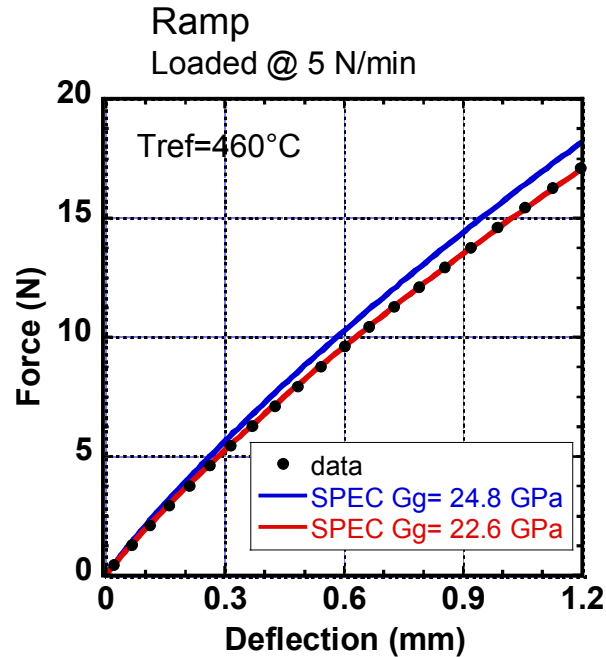
SPEC Model volume response adapted and calibrated to measure glass thermal strain

Model Validation – Complex Thermal History



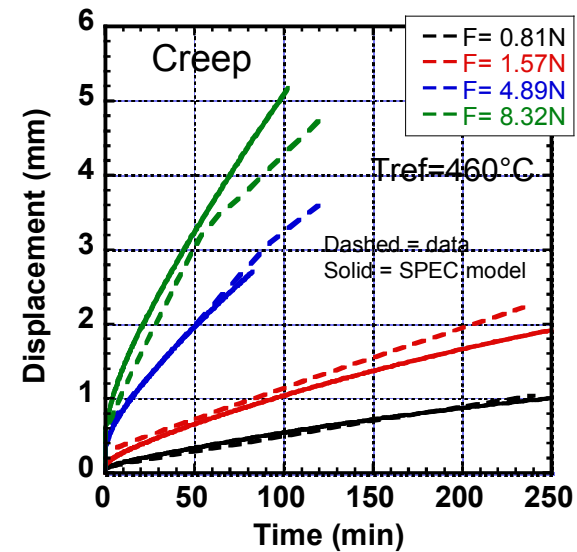
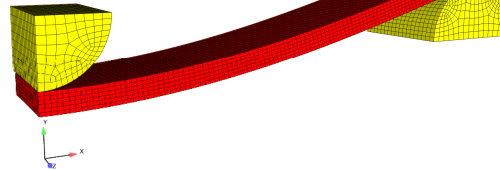
Netzsch Dilatometer

Model Validation – 3 – point bending



3-Pnt Bending Tests at T_g

55mm x 11mm x 1.1mm
beam

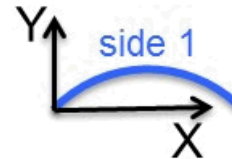


Characterizing Low Temp Creep

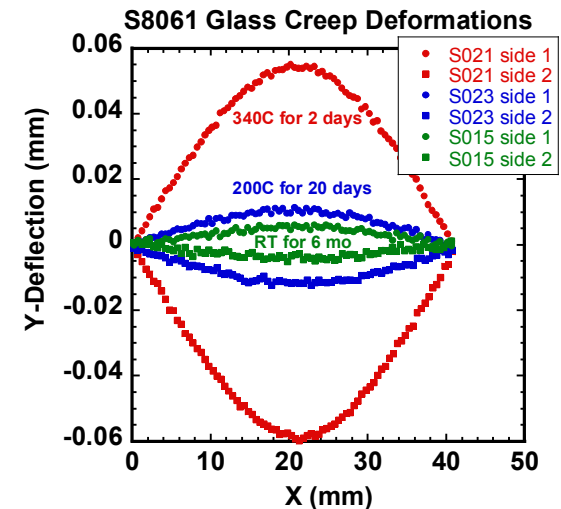
Three-point bend testing



T (°C)	Stress (psi)
340	4220
200	4220
20	4720

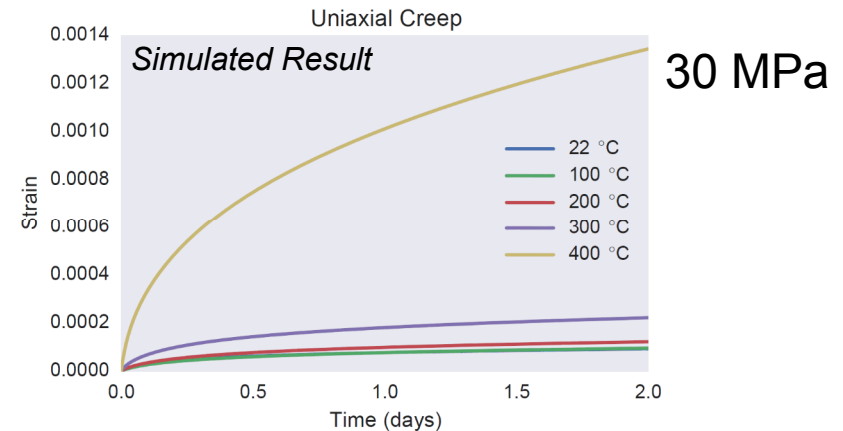
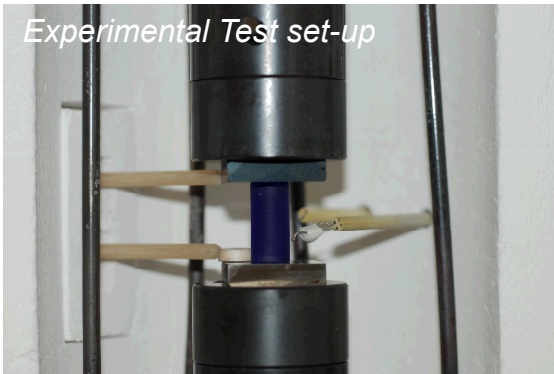


... Measurable creep 440°C
below Glass Transition

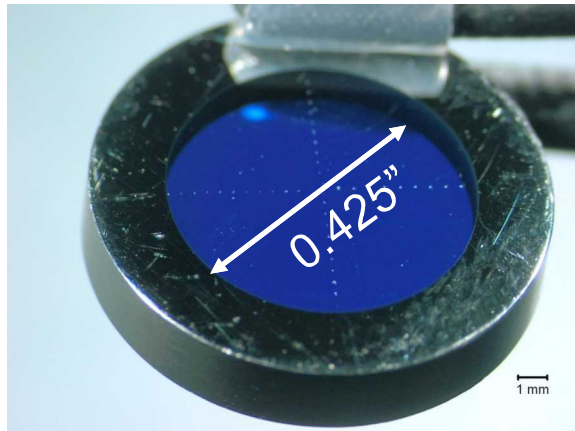


Compression creep testing

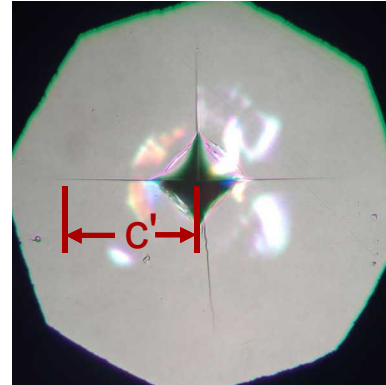
Experimental Test set-up



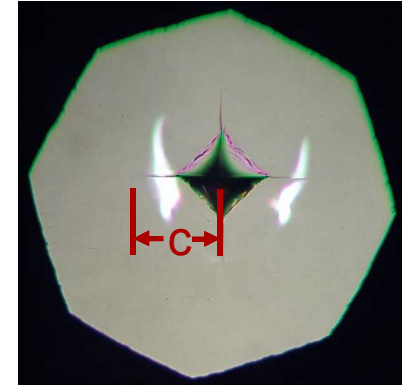
Model Validation: stress mapping by indentation crack measurements



GtoM seal test geometry



Polished Annealed Block
avg. $c \approx 92 \mu\text{m}$



Indent on test geometry
glass (not near SS shell)
avg. $c \approx 55 \mu\text{m}$

$$K_{IC}' = \chi P/c^{3/2}$$

stressed
glass

unstressed
glass

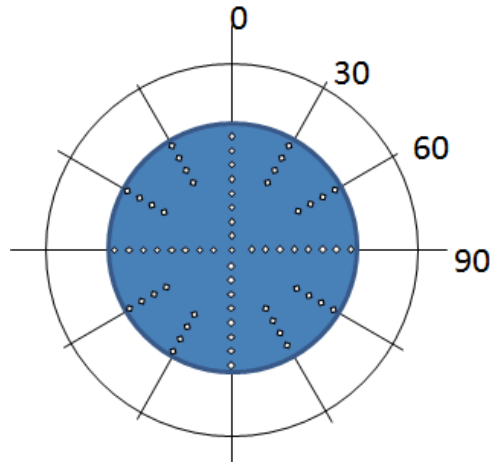
$$\sigma_r = \frac{-(K_I - K_{IC}')}{1.12 \pi c^{1/2}}$$

*Derived from indentation fracture
mechanics concepts*

e.g. Lawn Fracture of Brittle Solids (1993)

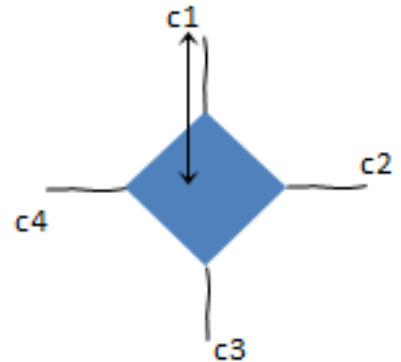
Model Validation: stress mapping by indentation crack measurements

Indentation
locations



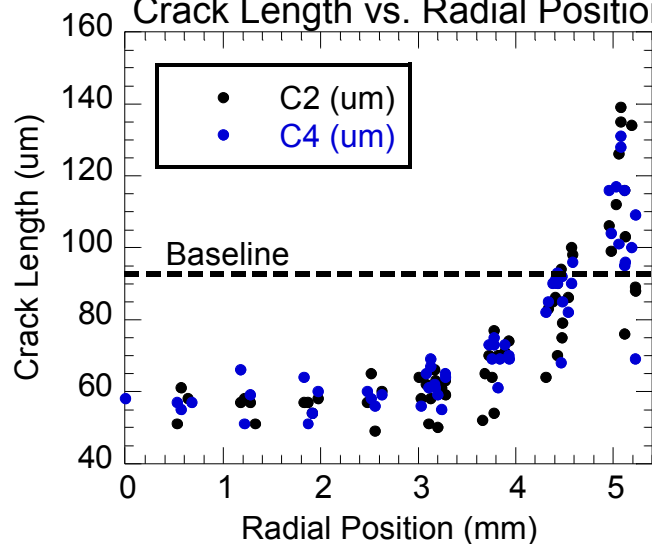
Radial Component
c1 and c3

Tangential Component
c2 and c4



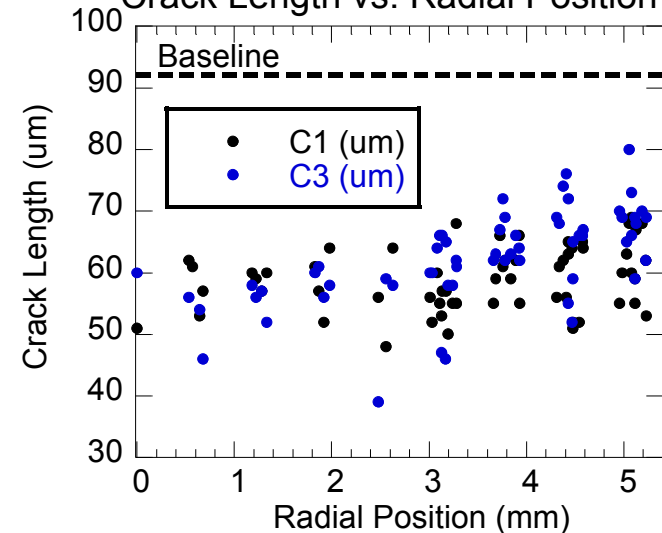
Radial Component

Crack Length vs. Radial Position

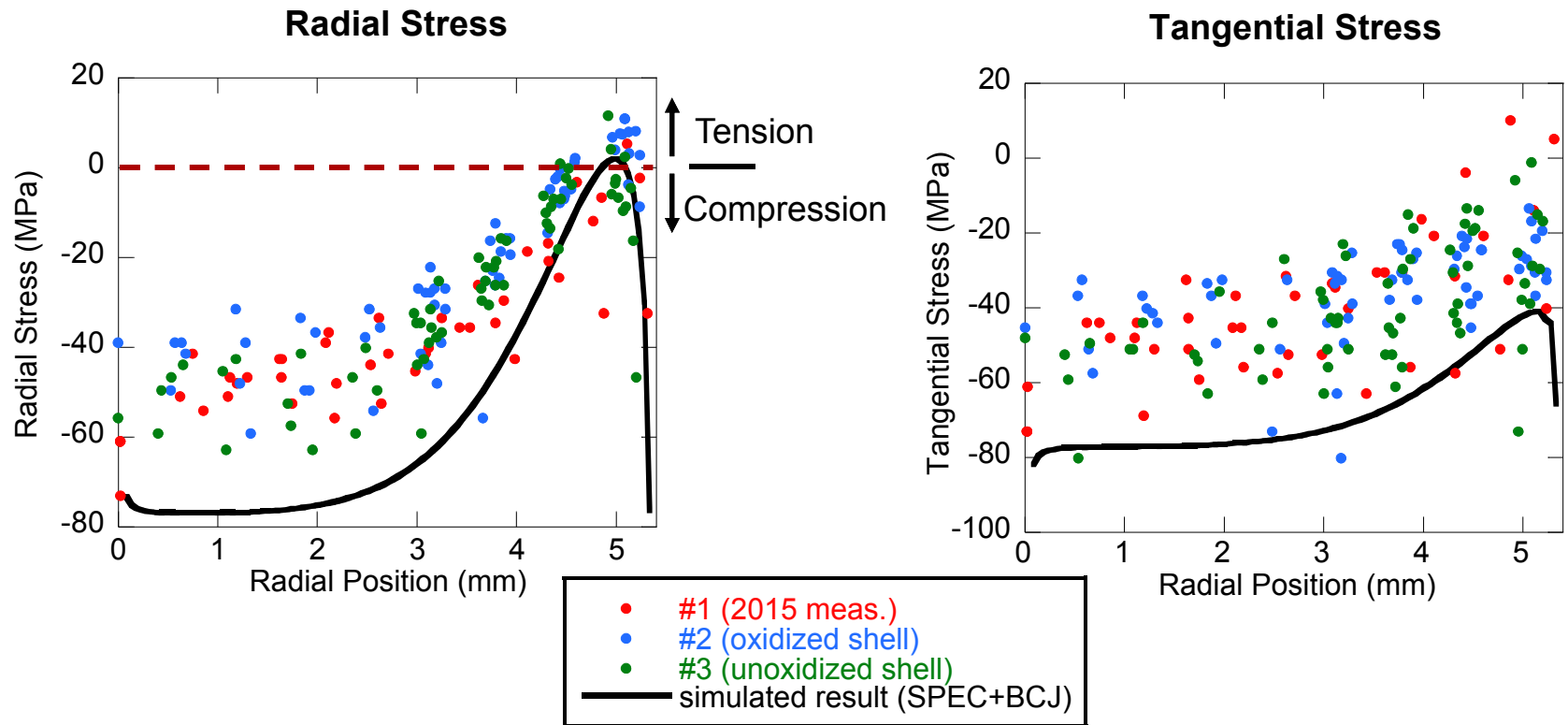


Tangential Component

Crack Length vs. Radial Position



Model Validation: stress mapping by indentation crack measurements

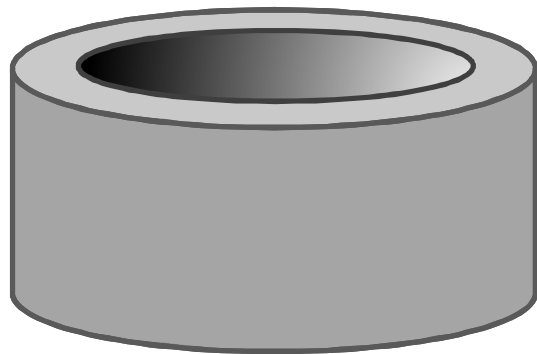


Model Validation: capturing dimensional changes in a glass to metal seal geometry

Tall cylinder geometry

OD= 0.635 ± 0.002 "

ID= 0.425 ± 0.0005 "



0.415 ± 0.005 "

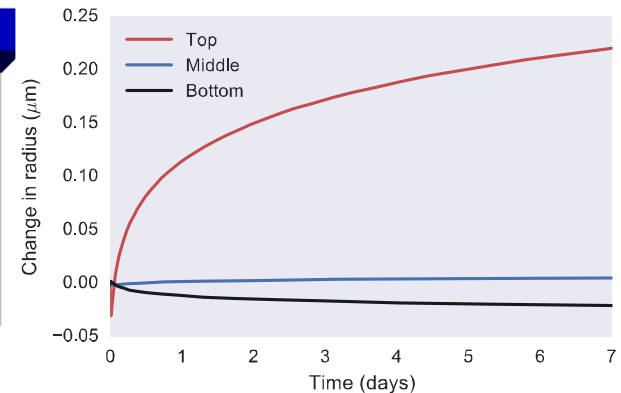
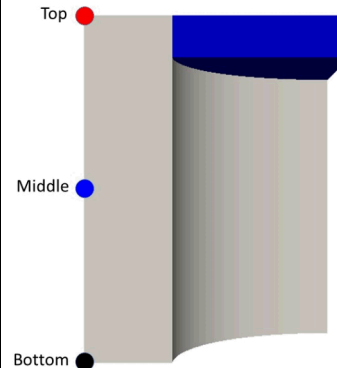
Mat'l: 304 L SS

0.050 ± 0.0005 "

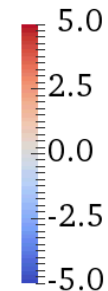
Material: Schott 8061 Glass

Seal at top of cylinder

A simulated result



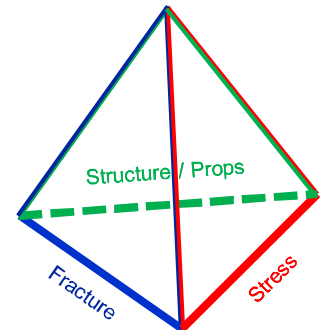
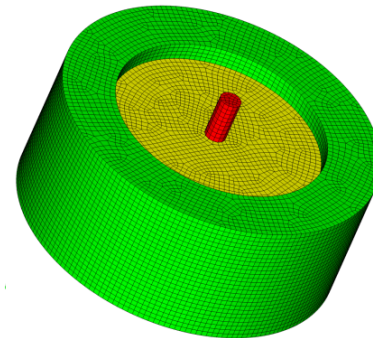
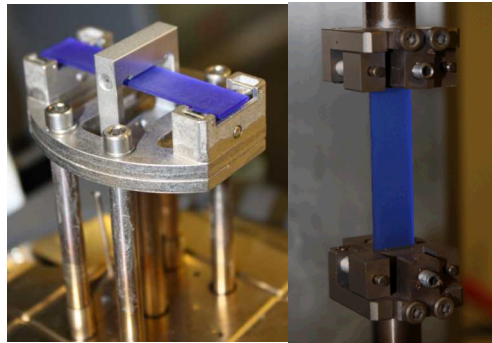
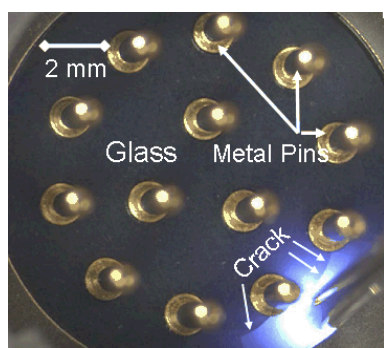
Max Principal Stress (MPa)



A geometry which can exaggerate dimensional changes due to the sealing process

Conclusions

- SPEC model can predict glass response with engineering accuracy
- Currently applying the model to realistic components to predict long term reliability



Acknowledgements

- Thomas Buchheit
- Clay Newton
- Raj Tandon
- Bob Chambers
- Mark Stavig
- Scott Reedy

