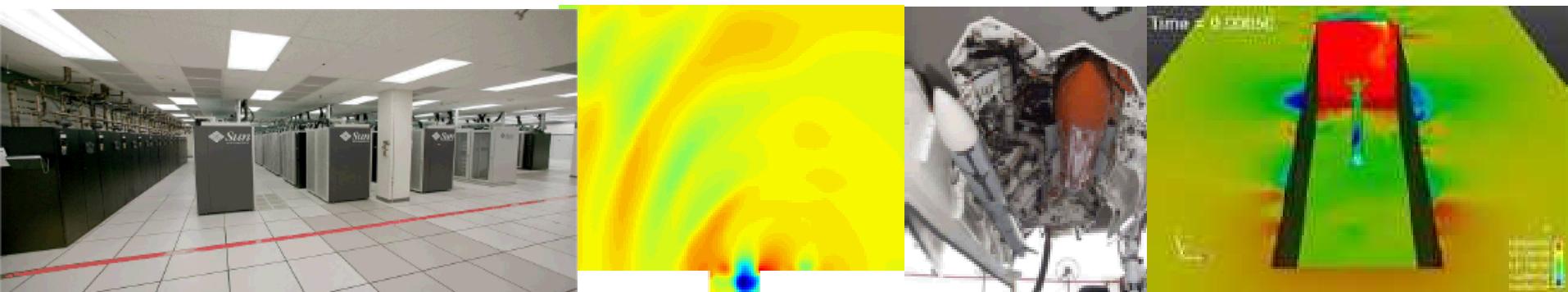


*Exceptional service in the national interest*



## A minimal subspace rotation approach for obtaining stable & accurate low-order projection-based reduced order models for nonlinear compressible flow

Irina Tezaur<sup>1</sup>, Maciej Balajewicz<sup>2</sup>

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# Outline

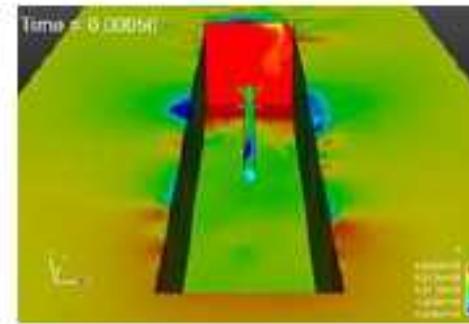
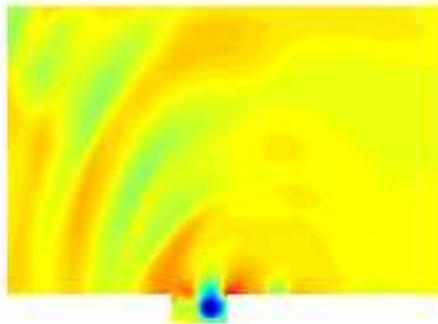
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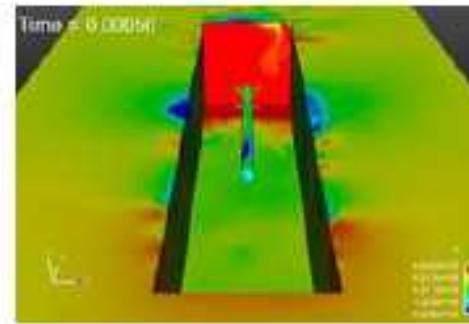
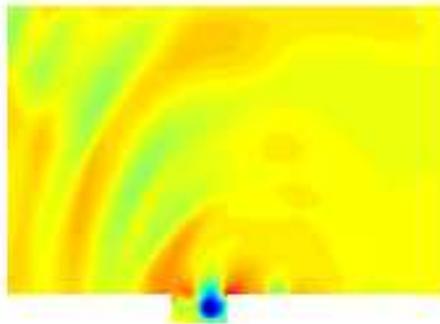
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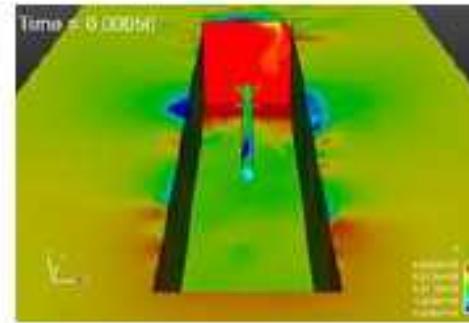
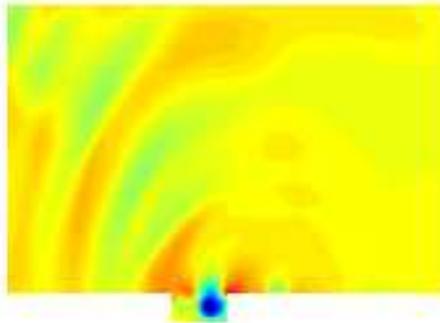
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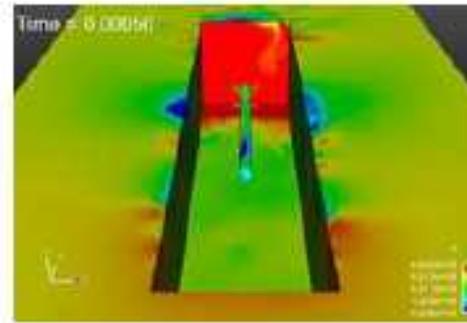
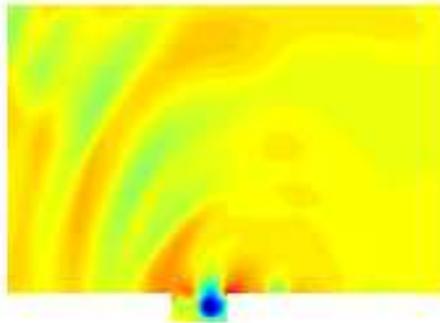
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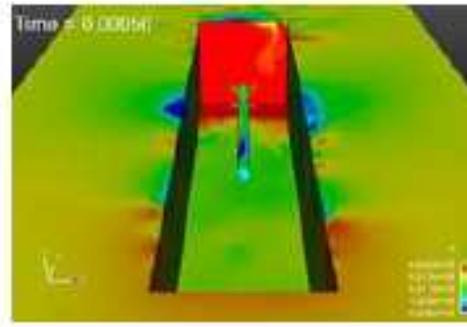
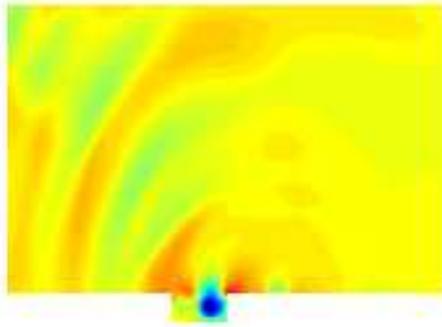
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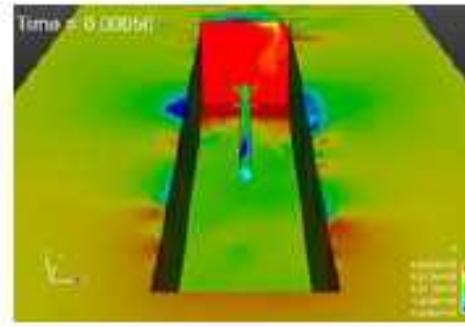
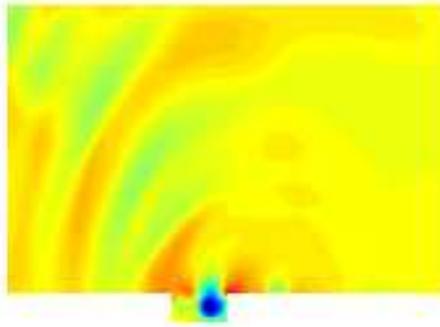
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**MOR for nonlinear, compressible fluid flows is still in its infancy!**

# Projection-based model order reduction

## Governing equations

- 3D compressible Navier-Stokes equations in primitive specific volume form:

[PDEs]

$$\begin{aligned}\zeta_{,t} + \zeta_{,j} u_j - \zeta u_{j,j} &= 0 \\ u_{i,t} + u_{i,j} u_j + \zeta p_{,i} - \frac{1}{Re} \zeta \tau_{ij,j} &= 0 \\ p_{,t} + u_j p_{,j} + \gamma u_{j,j} p - \left( \frac{\gamma}{PrRe} \right) (\kappa(p\zeta)_{,j})_{,j} - \left( \frac{\gamma-1}{Re} \right) u_{i,j} \tau_{ij} &= 0\end{aligned}\tag{1}$$

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[PDEs]

- Spectral discretization\* ( $\mathbf{q}(\mathbf{x}, t) \approx \sum_{i=1}^n a_i(t) \mathbf{U}_i(\mathbf{x})$ ) + Galerkin projection applied to (1) yields a system of  $n$  coupled quadratic ODEs:

[ROM]

$$\frac{d\mathbf{a}}{dt} = \mathbf{C} + \mathbf{L}\mathbf{a} + [\mathbf{a}^T \mathbf{Q}^{(1)} \mathbf{a} + \mathbf{a}^T \mathbf{Q}^{(2)} \mathbf{a} + \cdots + \mathbf{a}^T \mathbf{Q}^{(n)} \mathbf{a}] \quad (2)$$

where  $\mathbf{C} \in \mathbb{R}^n$ ,  $\mathbf{L} \in \mathbb{R}^{n \times n}$  and  $\mathbf{Q}^{(i)} \in \mathbb{R}^{n \times n}$  for all  $i = 1, \dots, n$ .

\* Here we use a Proper Orthogonal Decomposition (POD) basis  $\mathbf{U}_i(\mathbf{x})$ .

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**Turbulence Modeling**  
(traditional approach)

**Subspace Rotation**  
(our approach)

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## Traditional linear eddy-viscosity approach

- Dissipative dynamics of truncated higher-order modes are modeled using an additional linear term:

$$\frac{d\mathbf{a}}{dt} = \mathbf{C} + \mathbf{L}\mathbf{a} + [\mathbf{a}^T \mathbf{Q}^{(1)} \mathbf{a} + \mathbf{a}^T \mathbf{Q}^{(2)} \mathbf{a} + \cdots + \mathbf{a}^T \mathbf{Q}^{(n)} \mathbf{a}]^T$$

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- Disadvantages of this approach:
  1. Additional term destroys consistency between ROM and Navier-Stokes equations.
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  3. Inherently a linear model → cannot be expected to perform well for all classes of problems (e.g., nonlinear).

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### Illustrative example

- Standard approach: retain only the most energetic POD modes, i.e.,  $\mathbf{U}_1, \mathbf{U}_2, \mathbf{U}_3, \mathbf{U}_4, \dots$
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- Proposed approach: choose some higher order basis modes to increase dissipation, i.e.,  $\mathbf{U}_1, \mathbf{U}_2, \mathbf{U}_6, \mathbf{U}_8, \dots$
- More generally: approximate the solution using a linear superposition of  $n + p$  (with  $p > 0$ ) most energetic modes:

$$\tilde{\mathbf{U}}_i = \sum_{j=1}^{n+p} X_{ij} \mathbf{U}_j, \quad i = 1, \dots, n, \quad (3)$$

where  $\mathbf{X} \in \mathbb{R}^{(n+p) \times n}$  is an orthonormal ( $\mathbf{X}^T \mathbf{X} = \mathbf{I}_{n \times n}$ ) “rotation” matrix.

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 → ensure appropriate balance between energy production and energy dissipation.

- Once  $\mathbf{X}$  is found, the result is a system of the form (2) with:

$$Q^{(i)}_{jk} \leftarrow \sum_{s,q,r=1}^{n+p} X_{si} Q^{(s)}_{qr} X_{qr} X_{rk}, \quad \mathbf{L} \leftarrow \mathbf{X}^T \mathbf{L} \mathbf{X}, \quad \mathbf{C} \leftarrow \mathbf{X}^T \mathbf{C}^*$$

# Accounting for modal truncation

**Minimal subspace rotation:** trace minimization on Stiefel manifold

$$\begin{aligned}
 & \text{minimize}_{\mathbf{X} \in \mathcal{V}_{(n+p),n}} - \text{tr}(\mathbf{X}^T \mathbf{I}_{(n+p) \times n}) \\
 & \text{subject to} \quad \text{tr}(\mathbf{X}^T \mathbf{L} \mathbf{X}) = \eta
 \end{aligned} \tag{9}$$

- $\mathcal{V}_{(n+p),n} \in \{\mathbf{X} \in \mathbb{R}^{(n+p) \times n} : \mathbf{X}^T \mathbf{X} = \mathbf{I}_n, p > 0\}$  is the Stiefel manifold.
- Constraint is traditional linear eddy-viscosity closure model ansatz → involves overall balance between linear energy production and dissipation / vanishing of averaged total power ( $= \text{tr}(\mathbf{X}^T \mathbf{L} \mathbf{X}) + \text{energy transfer}$ ).
  - $\eta \in \mathbb{R}$ : proxy for the balance between linear energy production and energy dissipation (calculated iteratively using modal energy).
- Equation (9) is solved efficiently offline using the method of Lagrange multipliers (Manopt MATLAB toolbox).
- See (Balajewicz, Tezaur, Dowell, 2016) and Appendix slide for Algorithm.

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  2. Stability cannot be proven like for incompressible case.

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# Applications

## Channel driven cavity: low Reynolds number case

Flow over square cavity at Mach 0.6,  $Re = 1453.9$ ,  $Pr = 0.72$   
 $\Rightarrow n = 4$  ROM (91% snapshot energy).

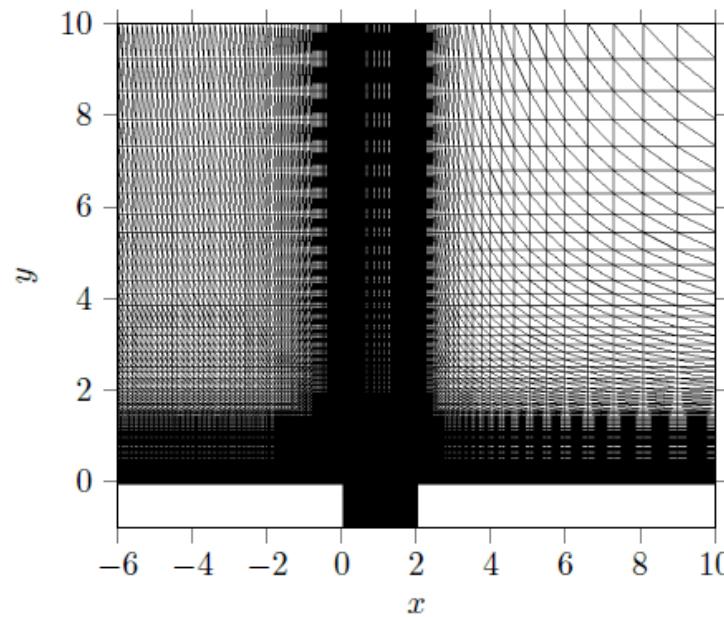


Figure 1: Domain and mesh for viscous channel driven cavity problem.

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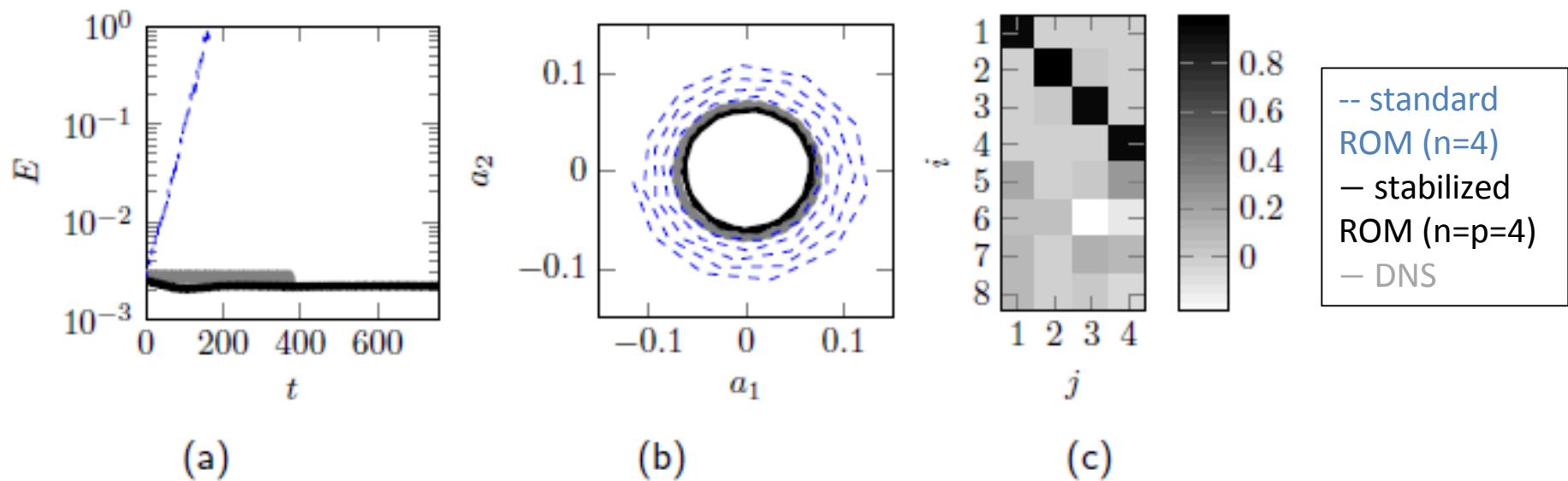


Figure 2: (a) evolution of modal energy, (b) phase plot of first and second temporal basis  $a_1(t)$  and  $a_2(t)$ , (c) illustration of stabilizing rotation showing that rotation is small:  

$$\frac{\|X - I_{(n+p),n}\|_F}{n} = 0.188, X \approx I_{(n+p),n}$$

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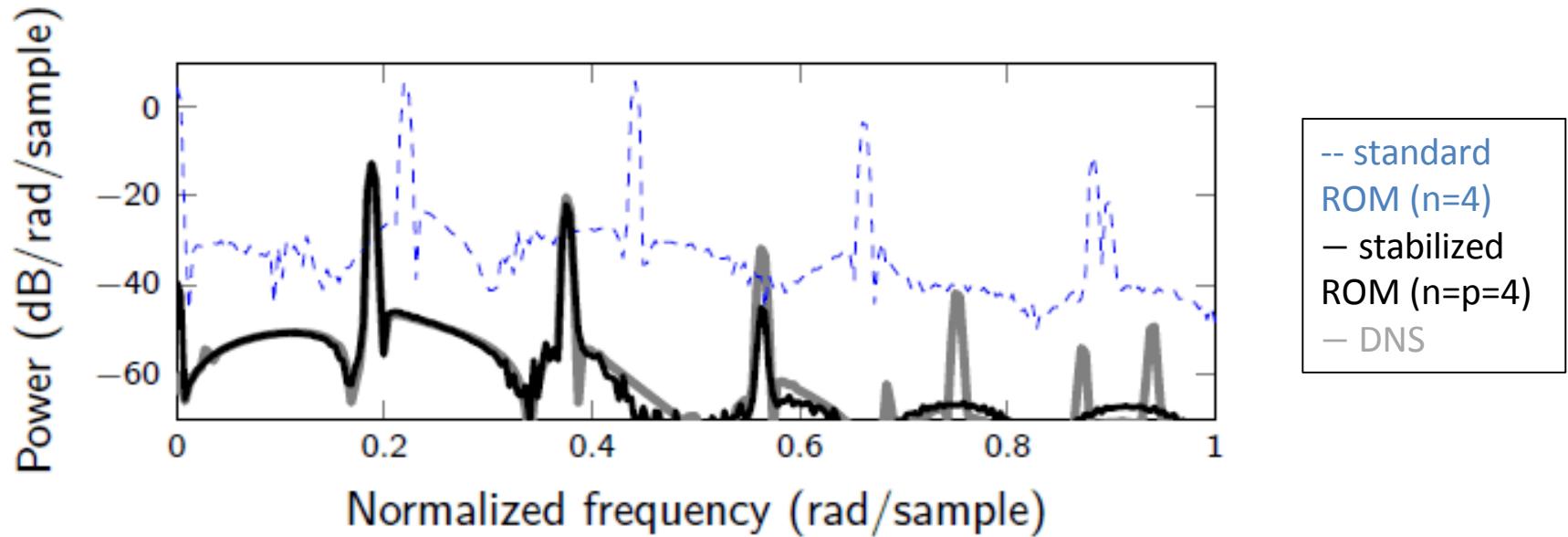


Figure 3: Pressure power spectral density (PSD) at location  $x = (2, -1)$ ; stabilized ROM minimizes subspace rotation.

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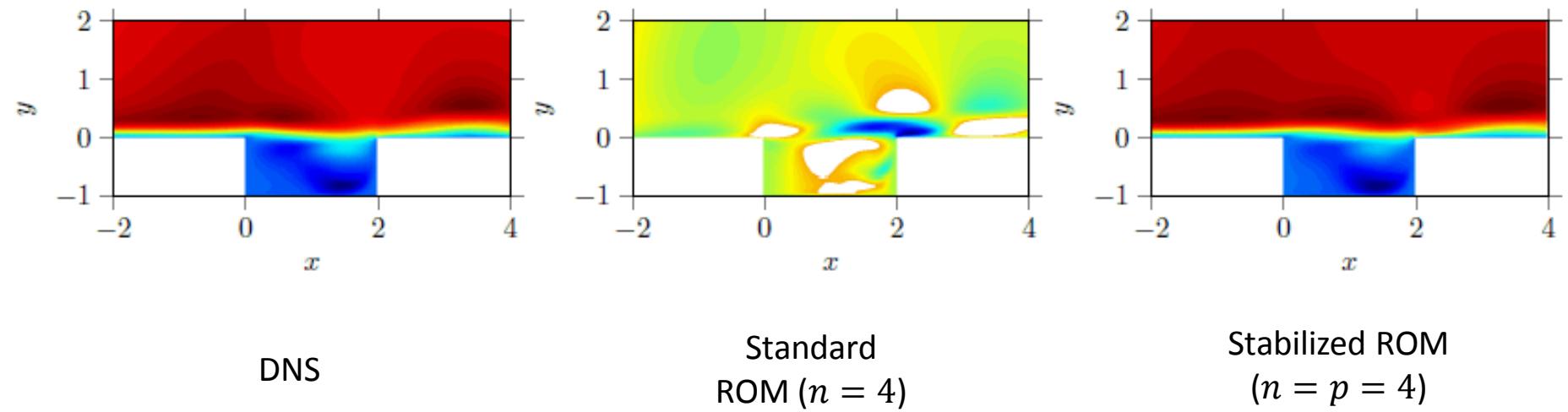


Figure 4: Channel driven cavity  $\text{Re} \approx 1500$  contours of  $u$ -velocity at time of final snapshot.

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# Applications

## Channel driven cavity: moderate Reynolds number case

Flow over square cavity at Mach 0.6,  $Re = 5452.1$ ,  $Pr = 0.72$   
 $\Rightarrow n = 20$  ROM (71.8% snapshot energy).

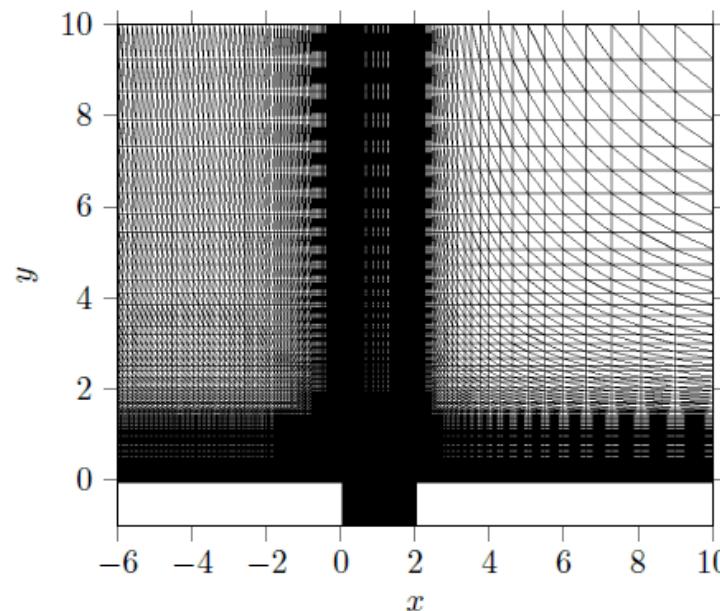
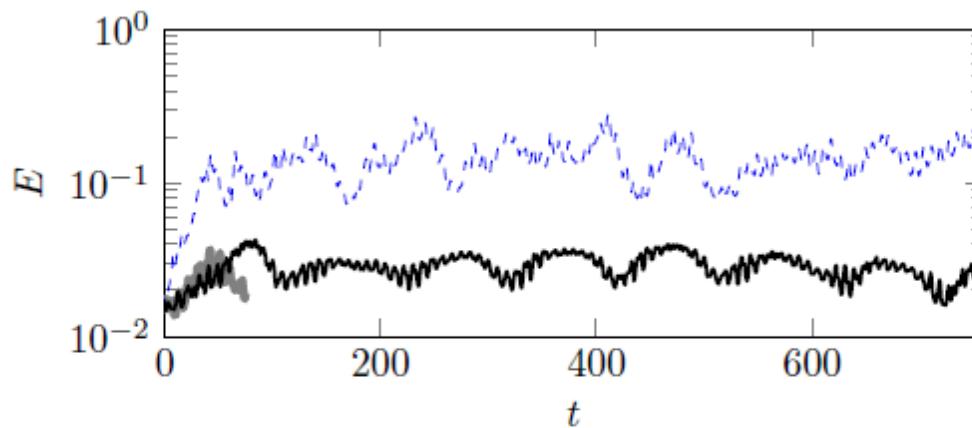


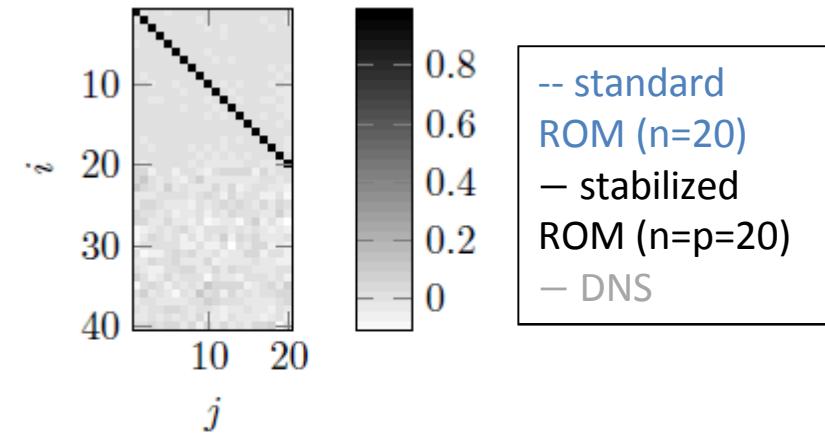
Figure 5: Domain and mesh for viscous channel driven cavity problem.

# Applications

## Channel driven cavity: moderate Reynolds number case



(a)



(b)

Figure 6: (a) evolution of modal energy, (b) illustration of stabilizing rotation showing that rotation is small:  $\frac{\|X - I_{(n+p),n}\|_F}{n} = 0.038, X \approx I_{(n+p),n}$

# Applications

## Channel driven cavity: moderate Reynolds number case

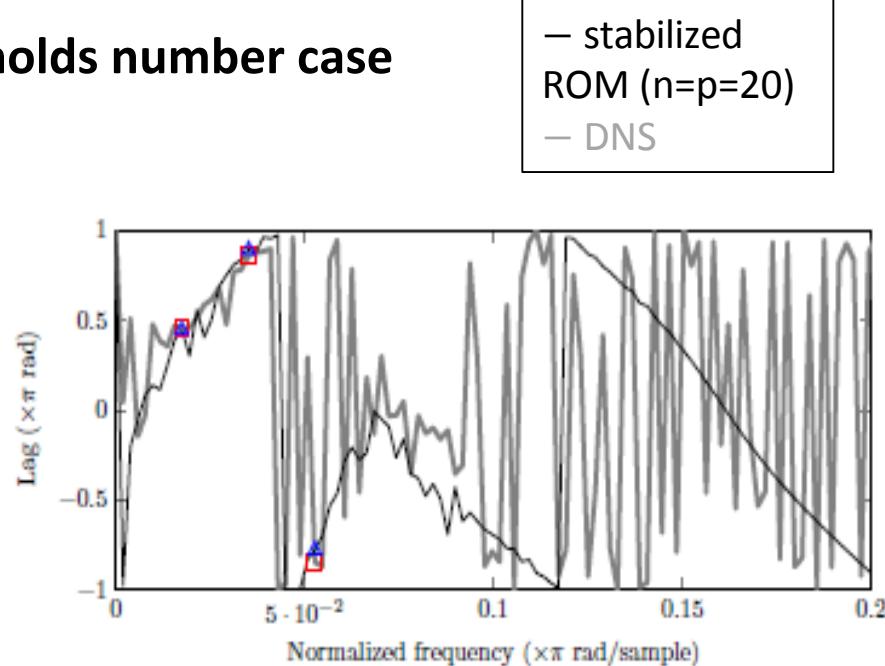
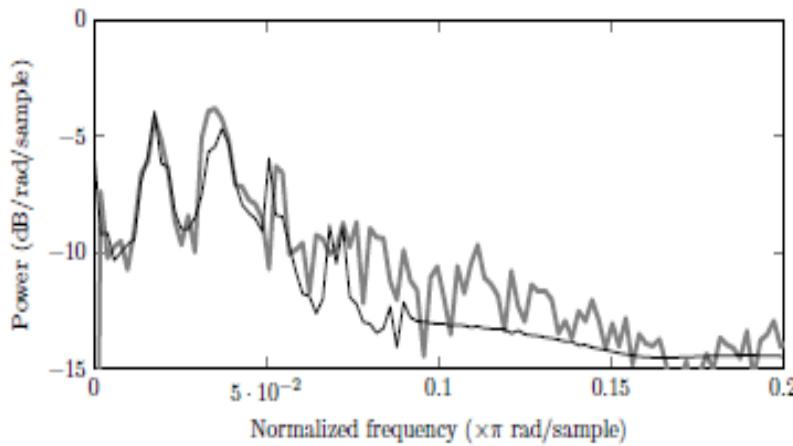


Figure 7: Pressure cross PSD of  $p(\mathbf{x}_1, t)$  and  $p(\mathbf{x}_2, t)$  where  $\mathbf{x}_1 = (2, -0.5)$ ,  $\mathbf{x}_2 = (0, -0.5)$

Power and phase lag at fundamental frequency, and first two super harmonics are predicted accurately using the fine-tuned ROM ( $\Delta$  = stabilized ROM,  $\square$  = DNS)

# Applications

## Channel driven cavity: moderate Reynolds number case

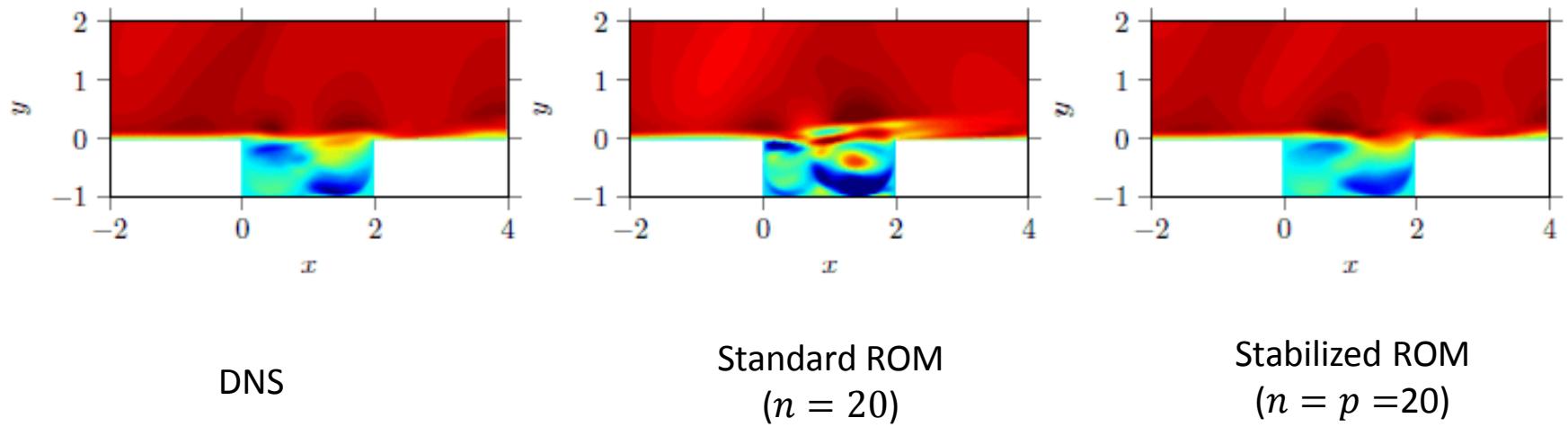


Figure 8: Channel driven cavity  $\text{Re} \approx 5500$  contours of  $u$ -velocity at time of final snapshot.

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# Summary

- We have developed a non-intrusive approach for stabilizing and fine-tuning projection-based ROMs for compressible flows.
- The standard POD modes are “rotated” into a more dissipative regime to account for the dynamics in the higher order modes truncated by the standard POD method.
- The new approach is consistent and does not require the addition of empirical turbulence model terms unlike traditional approaches.
- Mathematically, the approach is formulated as a quadratic matrix program on the Stiefel manifold.
- The constrained minimization problem is solved offline and small enough to be solved in MATLAB.
- The method is demonstrated on several compressible flow problems and shown to deliver stable and accurate ROMs.

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# Future work

- Application to higher Reynolds number problems.
- Extension of the proposed approach to problems with generic nonlinearities, where the ROM involves some form of hyper-reduction (e.g., DEIM, gappy POD).
- Extension of the method to minimal-residual-based nonlinear ROMs.
- Extension of the method to predictive applications, e.g., problems with varying Reynolds number and/or Mach number.
- Selecting different goal-oriented objectives and constraints in our optimization problem:

$$\begin{aligned} & \text{minimize}_{\mathbf{X} \in \mathcal{V}_{(n+p),n}} f(\mathbf{X}) \\ & \text{subject to } g(\mathbf{X}, \mathbf{L}) = 0 \end{aligned}$$

e.g.,

- Maximize parametric robustness:

$$f = \sum_{i=1}^k \beta_i \|\mathbf{U}^*(\mu_i)\mathbf{X} - \mathbf{U}^*(\mu_i)\|_F.$$

- ODE constraints:  $g = \|\mathbf{a}(t) - \mathbf{a}^*(t)\|.$

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# Appendix: Accounting for modal truncation

**Stabilization algorithm:** returns stabilizing rotation matrix  $\mathbf{X}$ .

**Inputs:** Initial guess  $\eta^{(0)} = \text{tr}(L(1 : n, 1 : n))$  ( $\mathbf{X} = \mathbf{I}_{(n+p) \times n}$ ), ROM size  $n$  and  $p \geq 1$ , ROM matrices associated with the first  $n + p$  most energetic POD modes, convergence tolerance  $TOL$ , maximum number of iterations  $k_{\max}$ .

for  $k = 0, \dots, k_{\max}$

Solve constrained optimization problem on Stiefel manifold:

$$\begin{aligned} & \underset{\mathbf{X}^{(k)} \in \mathcal{V}_{(n+p),n}}{\text{minimize}} && -\text{tr}(\mathbf{X}^{(k)\text{T}} \mathbf{I}_{(n+p) \times n}) \\ & \text{subject to} && \text{tr}(\mathbf{X}^{(k)\text{T}} \mathbf{L} \mathbf{X}^{(k)}) = \eta^{(k)}. \end{aligned}$$

Construct new Galerkin matrices using (4).

Integrate numerically new Galerkin system.

Calculate "modal energy"  $E(t)^{(k)} = \sum_i^n (a(t)_i^{(k)})^2$ .

Perform linear fit of temporal data  $E(t)^{(k)} \approx c_1^{(k)} t + c_0^{(k)}$ , where  $c_1^{(k)}$  =energy growth.

Calculate  $\epsilon$  such that  $c_1^{(k)}(\epsilon) = 0$  (no energy growth) using root-finding algorithm.

Perform update  $\eta^{(k+1)} = \eta^{(k)} + \epsilon$ .

if  $\|c_1^{(k)}\| < TOL$

$\mathbf{X} := \mathbf{X}^{(k)}$ .

  terminate the algorithm.

end

end

# Applications

## CPU times (CPU-hours) for offline and online computations

	Procedure	Low Re Cavity	Moderate Re Cavity
offline	FOM # of DOF	288,250	243,750
	Time-integration of FOM	72 hrs	179 hrs
	Basis construction (size $n + p$ ROM)	0.88 hrs	3.44 hrs
	Galerkin projection (size $n + p$ ROM)	5.44 hrs	14.8 hrs
	Stabilization	14 sec	170 sec
online	ROM # of DOF	4	20
	Time-integration of ROM	0.16 sec	0.83 sec
	Online computational speed-up	1.6e6	7.8e5

- Stabilization is fast ( $O(\text{sec})$  or  $O(\text{min})$ ).
- Significant online computational speed-up!