

High Resolution Silicon Arrayed Waveguide Gratings for Photonic Signal Processing Applications

Michael Gehl, Doug Trotter, Andrew Starbuck, Andrew Pomerene, Anthony Lentine, Christopher DeRose

Outline

- Introduction to Arrayed Waveguide Gratings
- Design & Fabrication
- Characterization by Swept Source Interferometry
- Phase Optimization
- Application
- Conclusion

Arrayed Waveguide Grating

Functionality of an Arrayed Waveguide Grating



- Arrayed waveguide gratings provided integrated spectral filtering
- Bending optical path creates highly compact devices
- Applications
 - RF signal processing
 - Wavelength division multiplexing
 - Spectral and Temporal Pulse Shaping

Arrayed Waveguide Grating

Functionality of an Arrayed Waveguide Grating



- State-of-the-art
 - 1GHz, 16 Channel Silica on Silicon – $A \sim 44 \text{ cm}^2$ [K. Takada, et. al. *J. Lightwave Tech.* **20**, 850 (2002)]
 - 25GHz, 512 Channel SOI – $A \sim 1.8 \text{ cm}^2$ [S. Cheung, et. al. *J. Sel. Top. Quant. Electronics* **20**, 8202207 (2014)]
 - 10GHz, 100 Channel InP – $A \sim 10 \text{ cm}^2$ [F. M. Soares, et. al. *Photonics J.* **3**, 975 (2011)]
 - 25GHz, 400 Channel Silica – $A \sim 80 \text{ cm}^2$ [Y. Hida, et. al. *Proc. Opt. Fiber Comm. Conf.* **3**, WB2-1 (2001)]
- Cutting-Edge Result (this work):
 - **1GHz, 11 Channel SOI – $A \sim 1.1 \text{ cm}^2$** [M. Gehl, et. al. *Opt. Express* **25**, pp. 6320-6334 (2017)]

Optical Phase Errors

Functionality of an Arrayed Waveguide Grating



- Fabrication imperfections create random phase perturbations
 - Perturbations in waveguide width (δw)
 - Perturbations in material index (δn)
- Phase uncertainty increases with waveguide length and index contrast
$$\sigma^2(\delta\phi) = L^2(A \cdot \Delta^3 \cdot \sigma^2(\delta w) + B \cdot \sigma^2(\delta n))$$
$$\Delta = \frac{(n_{core}^2 - n_{clad}^2)}{2n_{core}^2}$$
- Light no longer “focuses” to a single waveguide
 - Increased insertion loss
 - Increased cross-talk

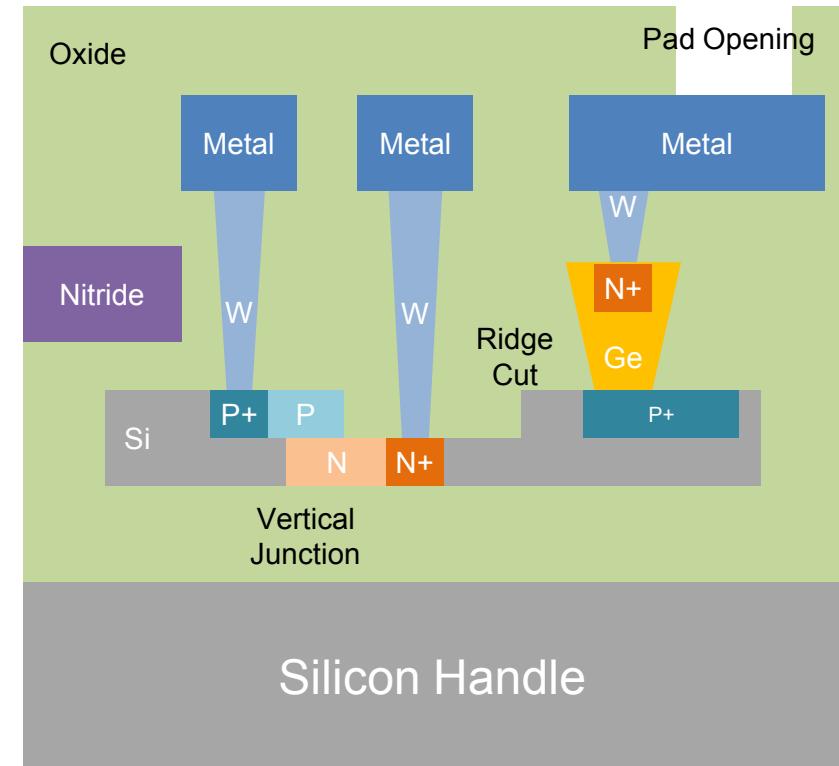
Methods of Phase Correction

- Passive Methods
 - Static Phase Correction
 - Benefit – No power required to maintain correction
 - Disadvantage – Irreversible, Challenging implementation
 - UV Irradiation [K. Takada, et. al. *Electron. Lett.* **36**, 60 (2000)]
 - Photo-Elastic Effect [H. Yamada, et. al. *Electron. Lett.* **32**, 1581 (1996)]
 - Phase Compensating Plate [H. Yamada, et. al. *Electron. Lett.* **33**, 1698 (1997)]
- Active Methods
 - Dynamically Applied Phase Correction
 - Benefit – Reversible, Allows active tuning and spectral shaping
 - Disadvantage – Requires constant power
 - Electro-Optic [W. Jiang, et. al. *Laser & Electro-Optics Society*, p. 52 (2008)]
 - Thermo-Optic [H. Yamada, et. al. *Electron. Lett.* **31**, 360 (1995)], [This Work]

Silicon Photonics Platform

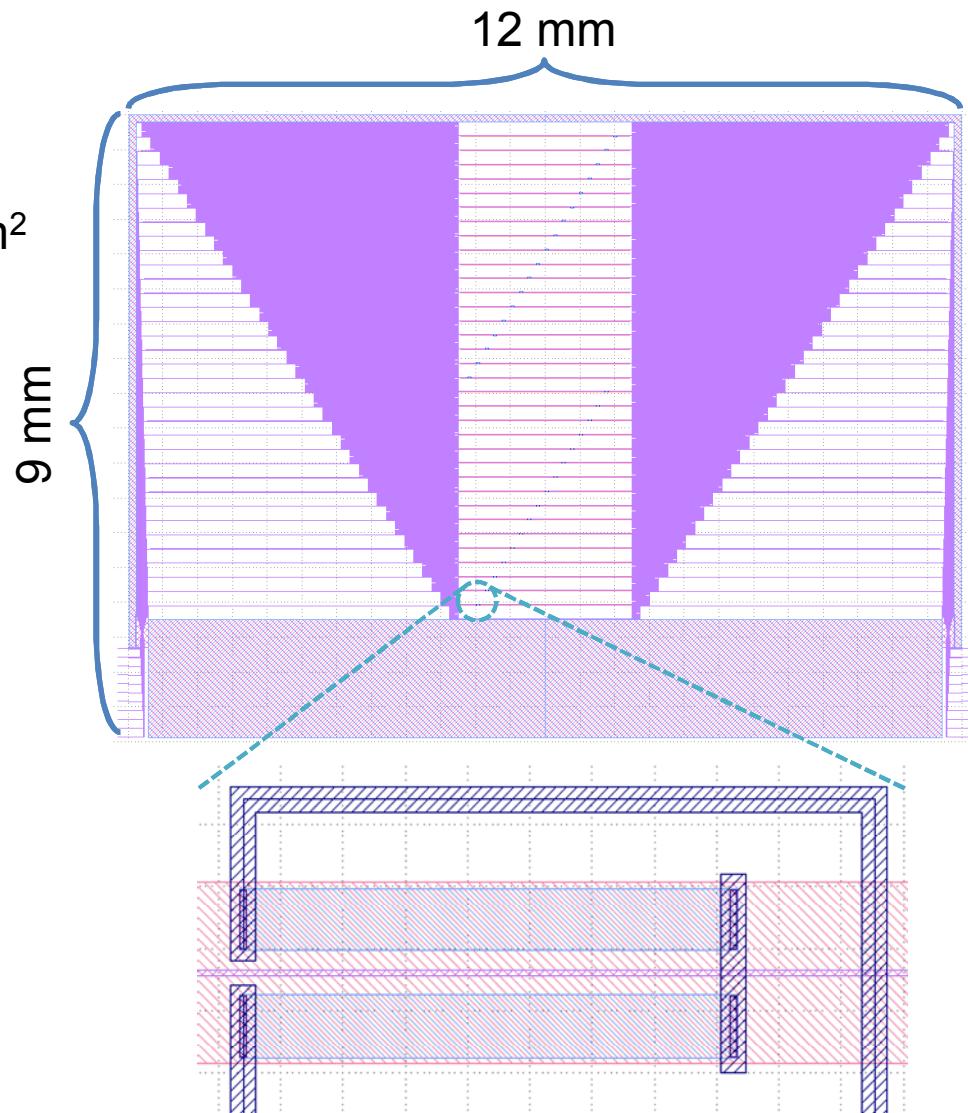
Silicon Photonic Process at the MESA Facility

- 6 in. SOI wafers, 250nm device layer, 3 μ m buried oxide layer
- Fully or partially etched silicon for rib or ridge waveguides
- 225nm low loss silicon nitride waveguide layer
- Selective area germanium epitaxy for photodiodes
- 4-6 ion implantation steps
- 1-2 aluminum metal layers

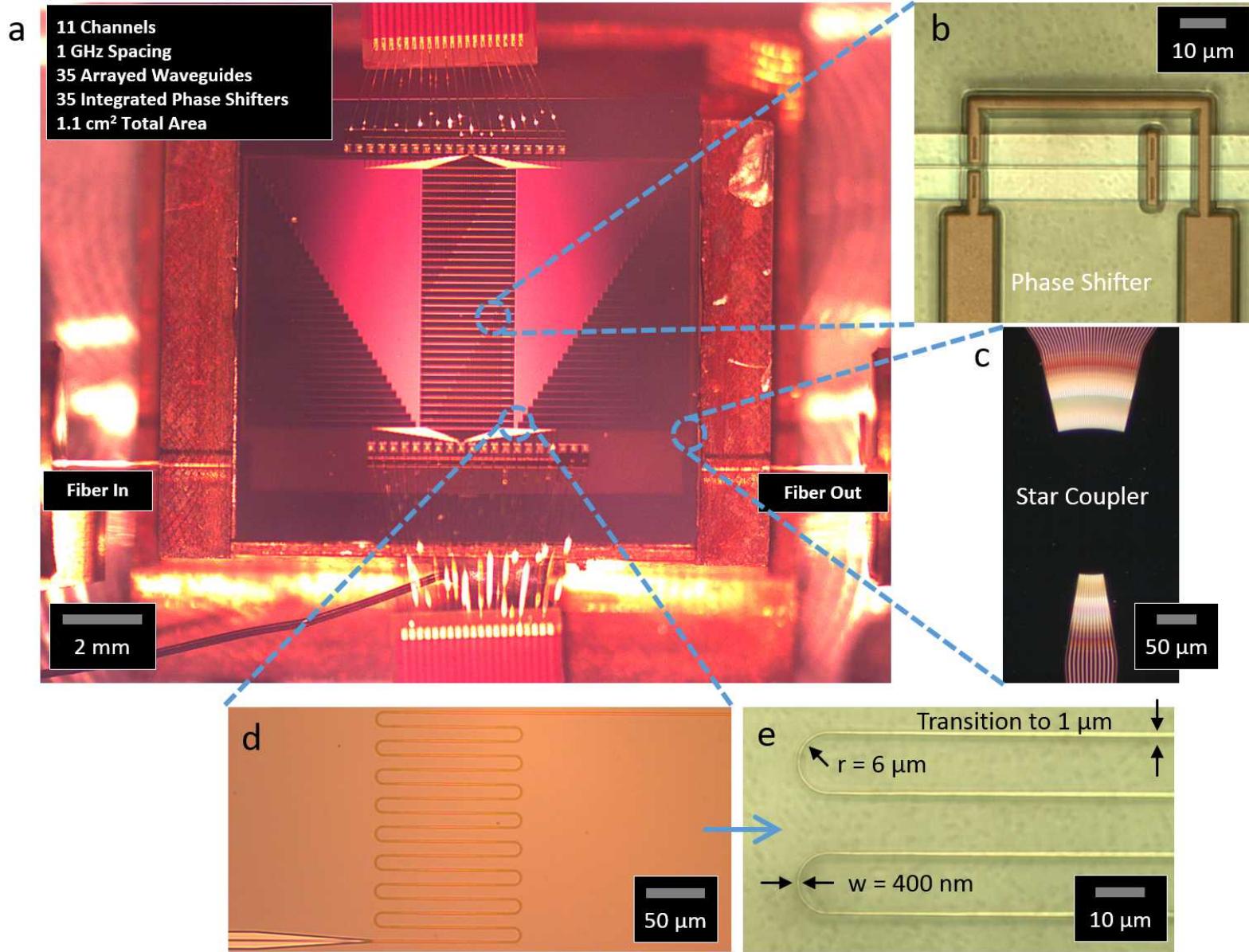


AWG Design

- Serpentine waveguides for compactness
 - Largest – $12 \text{ mm} \times 9 \text{ mm} = 1.1 \text{ cm}^2$
- 35 Arrayed waveguides
- 1, 10 & 50 GHz channel spacing
- Resistive thermal phase shifter for each waveguide
 - Thermo-optic effect changes effective path length of the waveguide
 - Phase shift approximately proportional to applied power

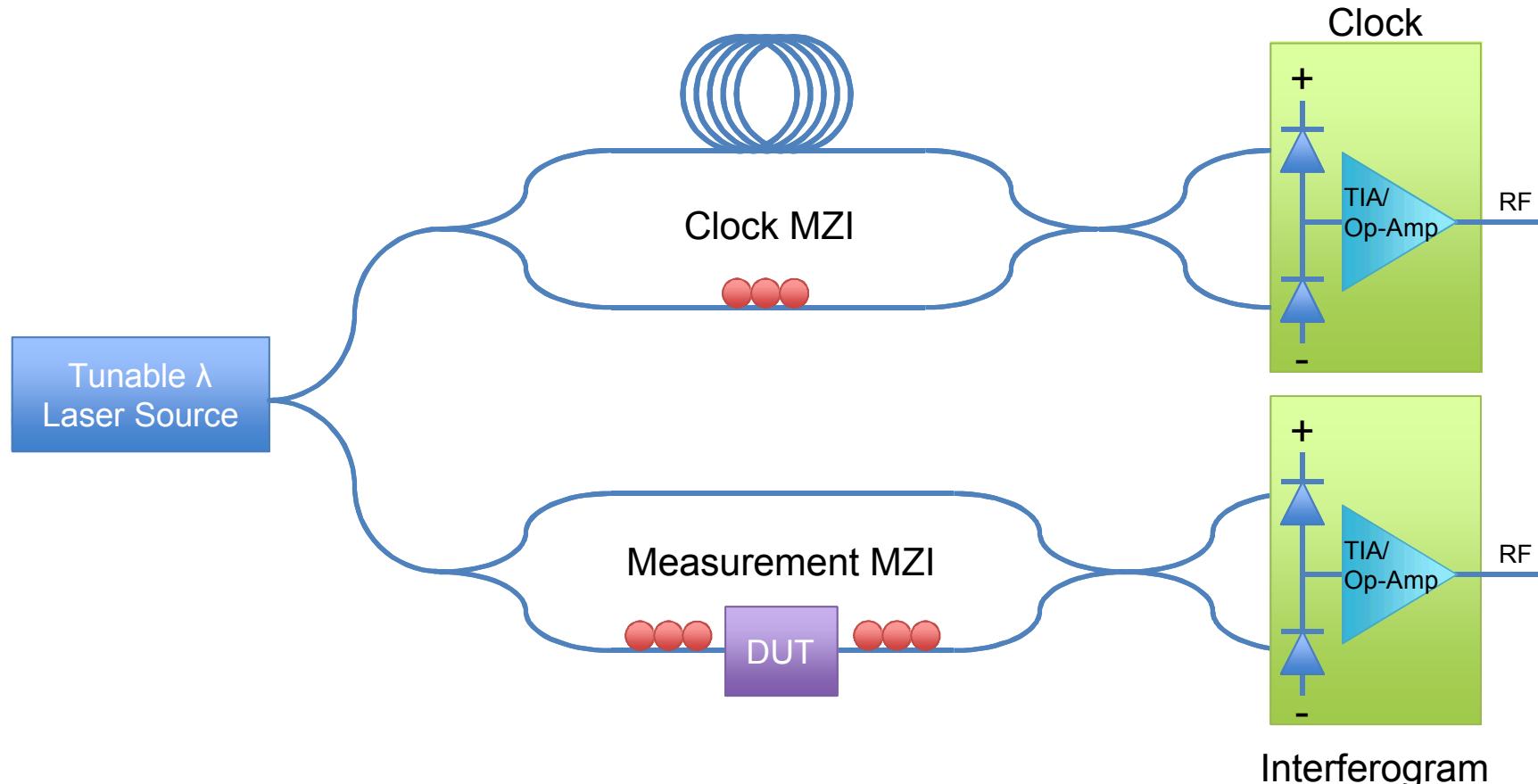


Device Fabrication & Packaging



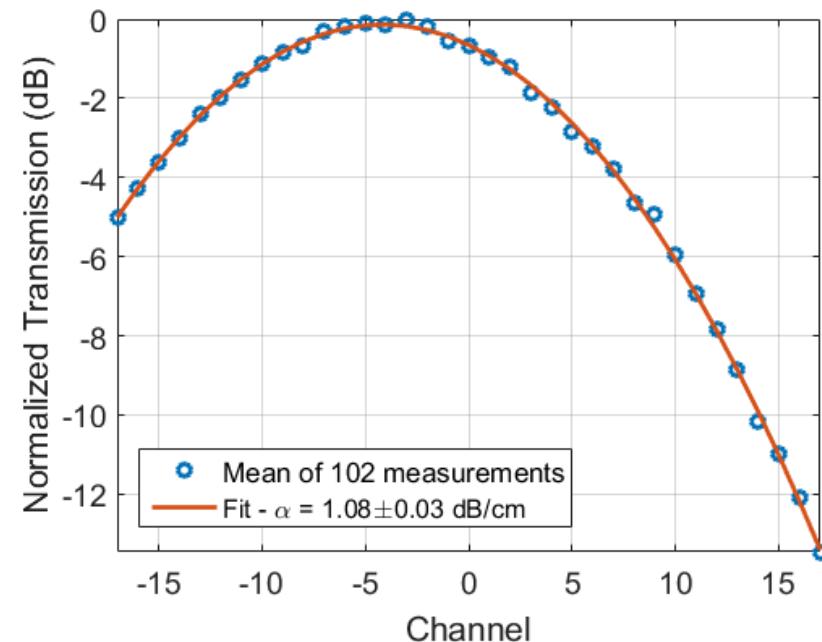
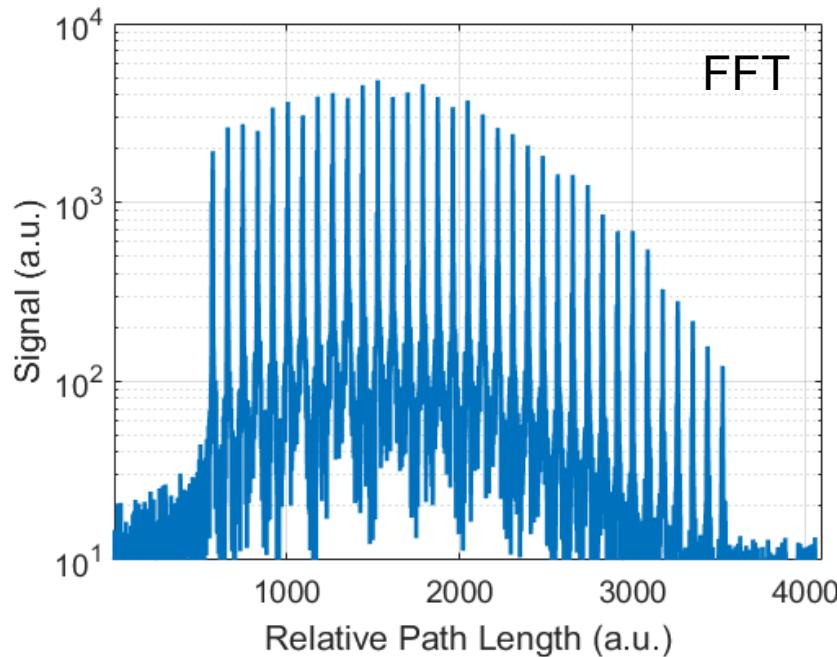
Interferometric Characterization

- Swept source interferometer
- Reference MZI to trigger data acquisition
 - $\Delta\lambda \approx 11.278 \text{ fm} \rightarrow \Delta\nu \approx 1.406 \text{ MHz}$



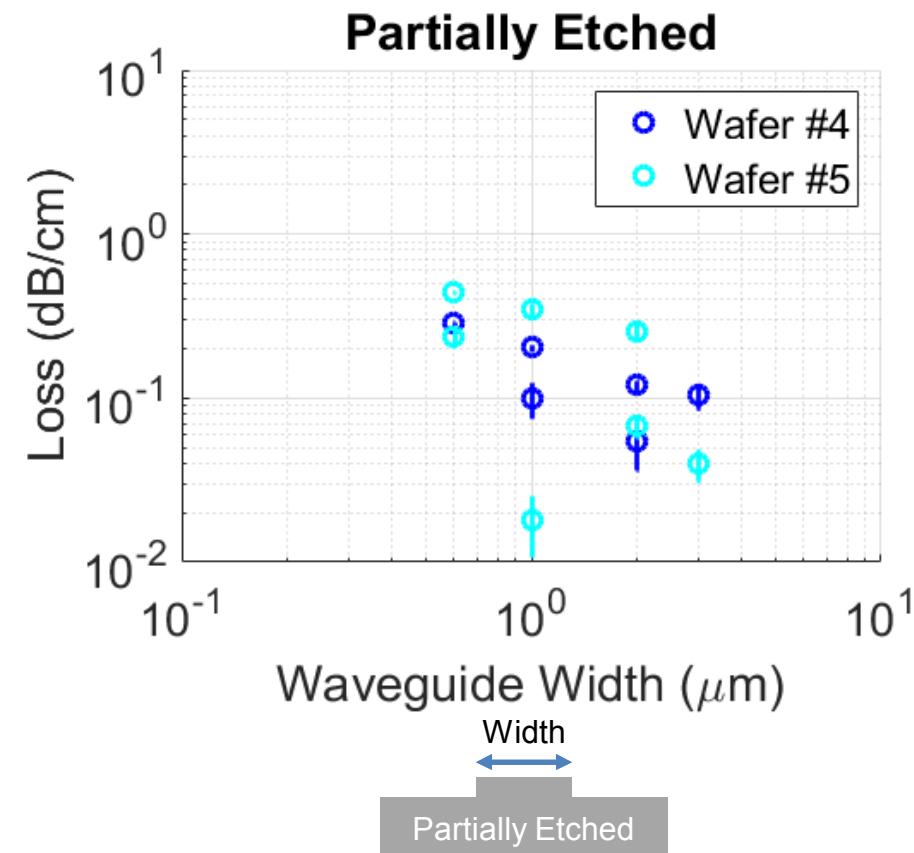
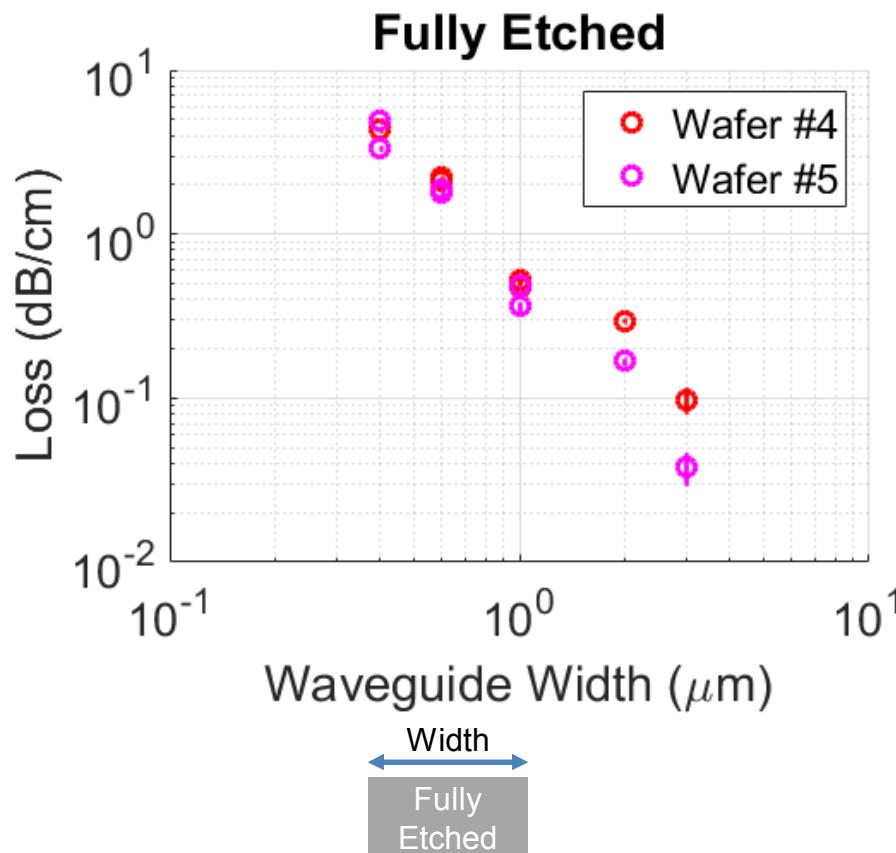
Interferometric Characterization

- FFT of interferogram provides phase and amplitude transmission of each optical path through device



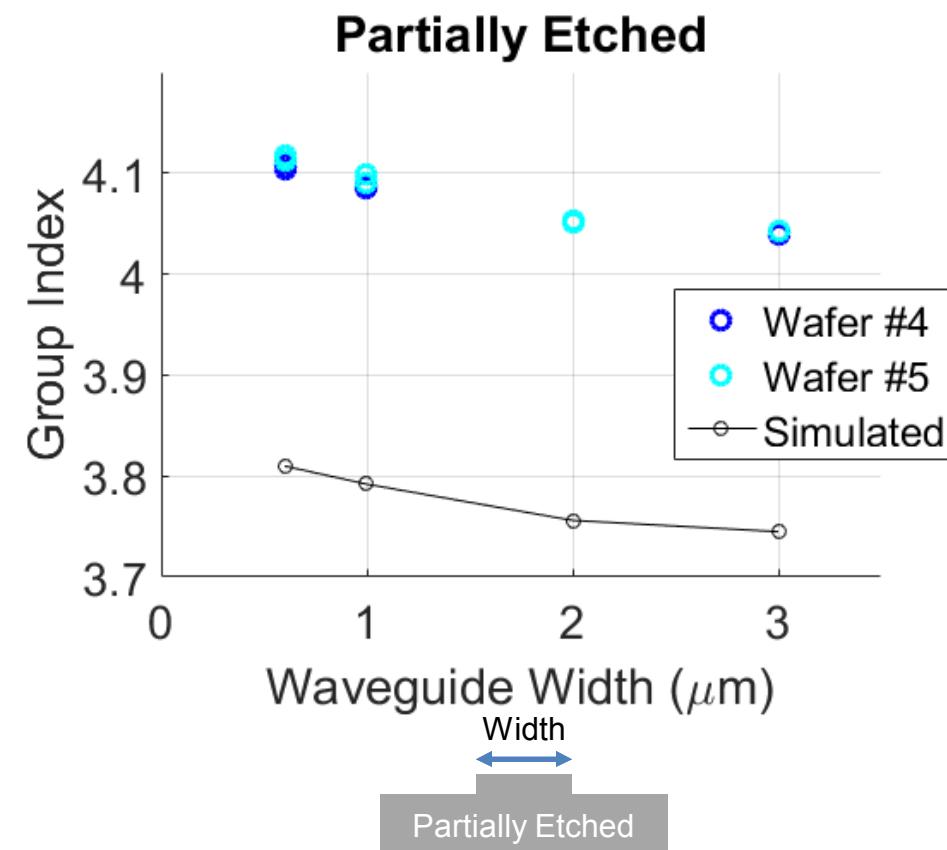
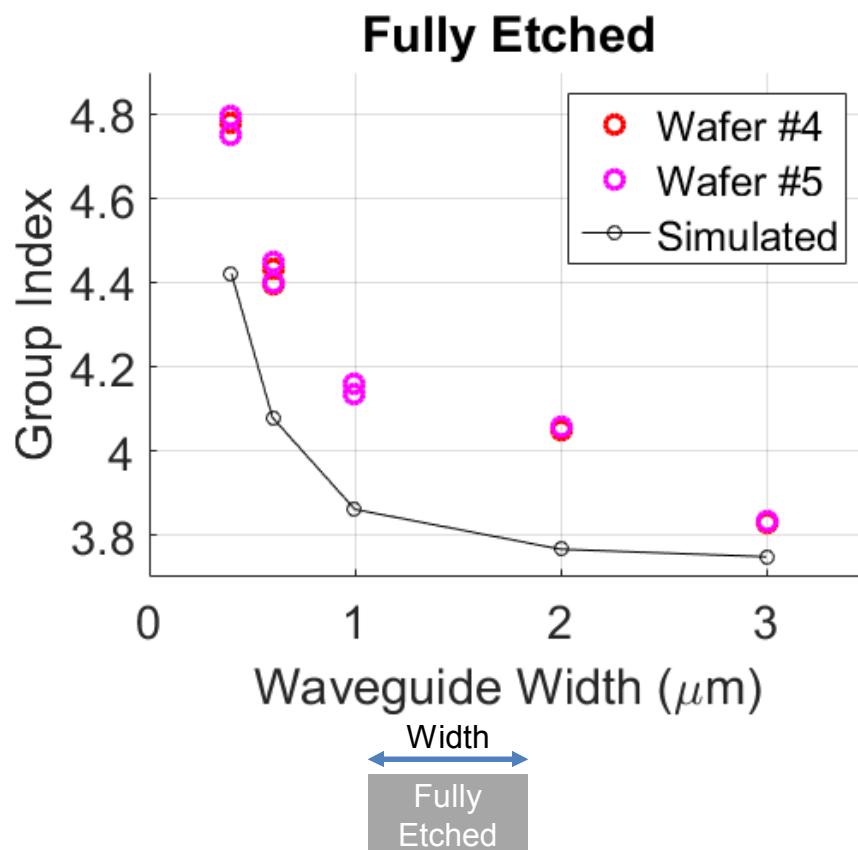
Interferometric Characterization

- From this we can accurately extract waveguide loss and group index



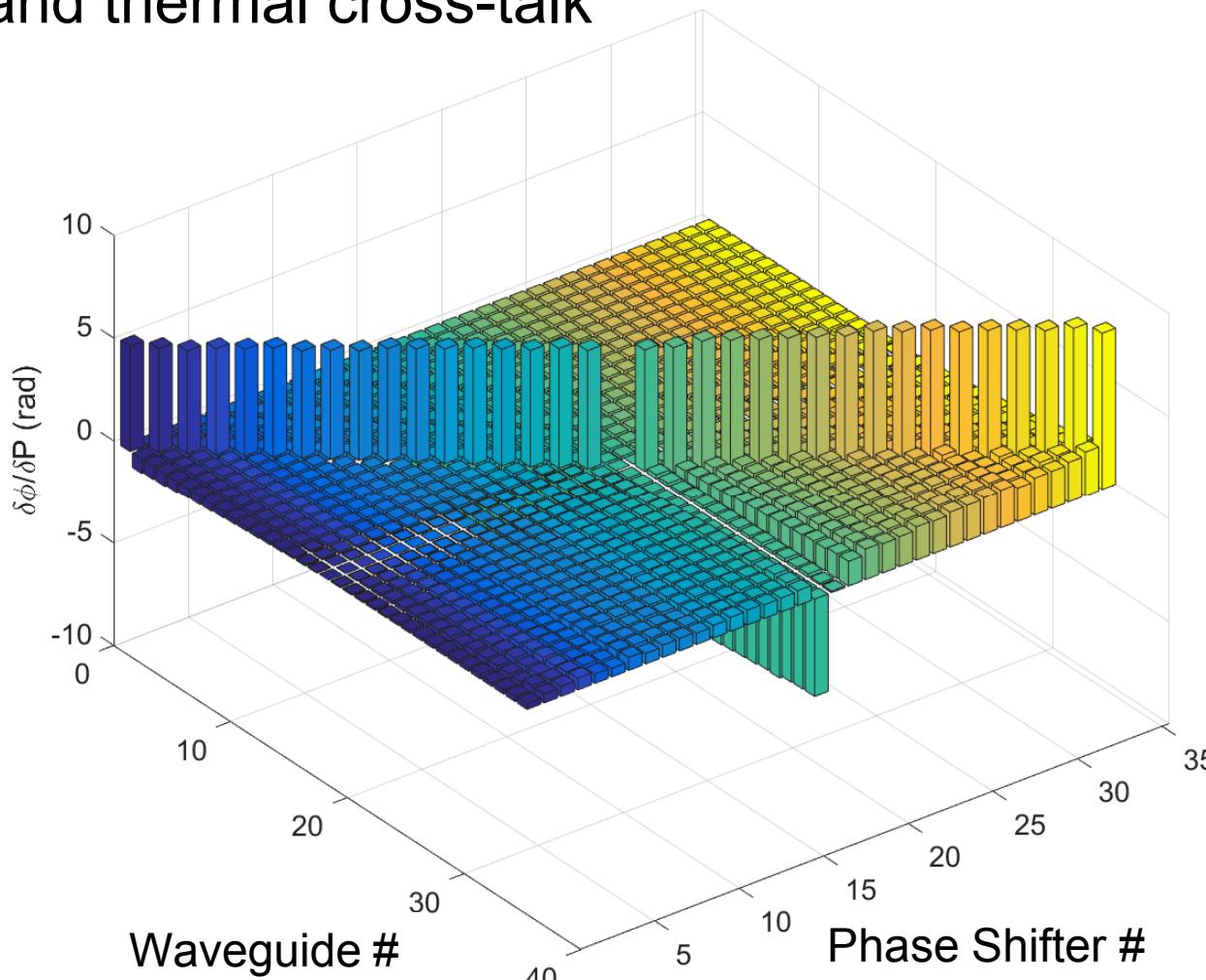
Interferometric Characterization

- From this we can accurately extract waveguide loss and group index



Interferometric Characterization

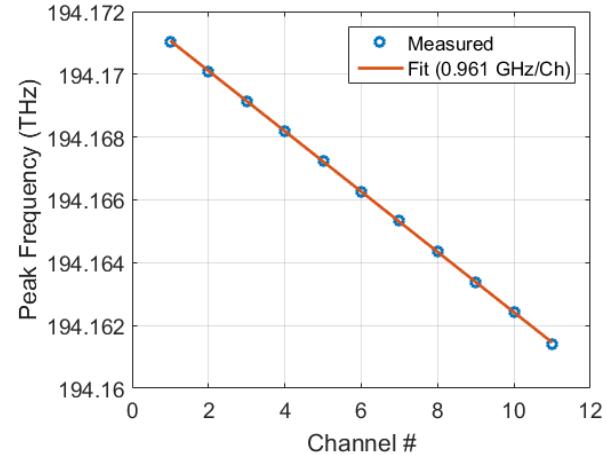
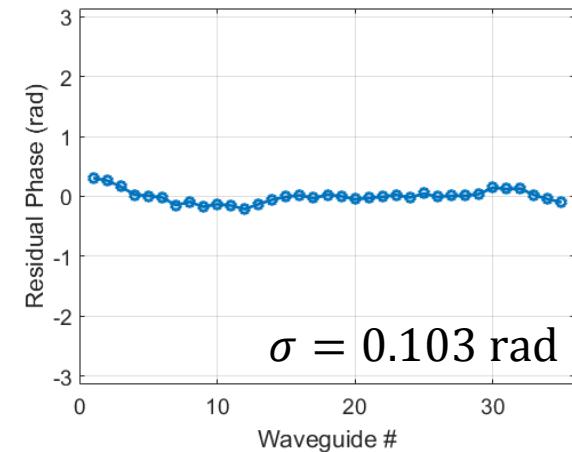
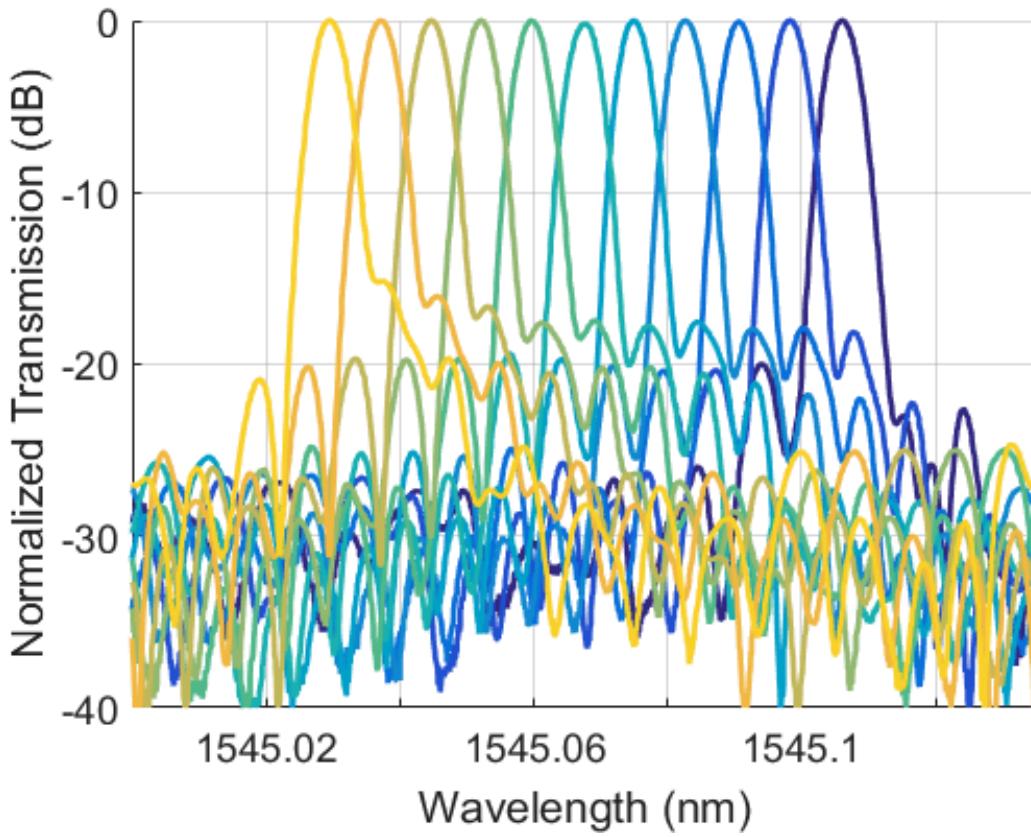
- Phase information provides accurate calibration of phase shifters and thermal cross-talk



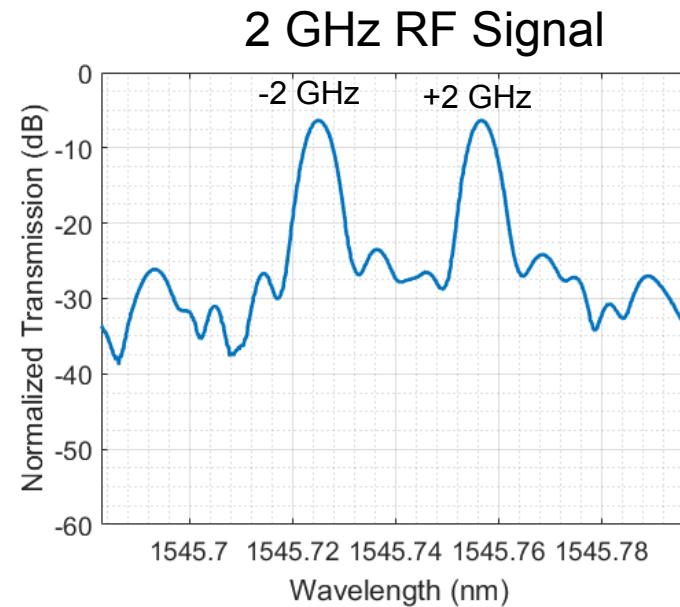
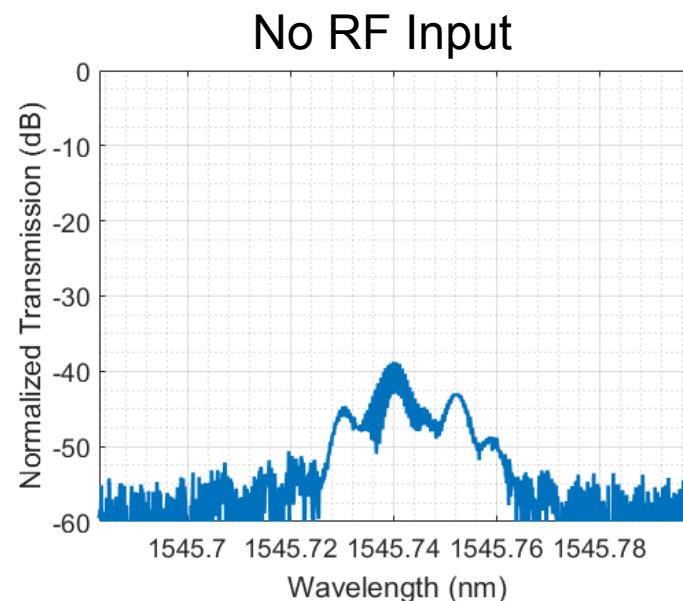
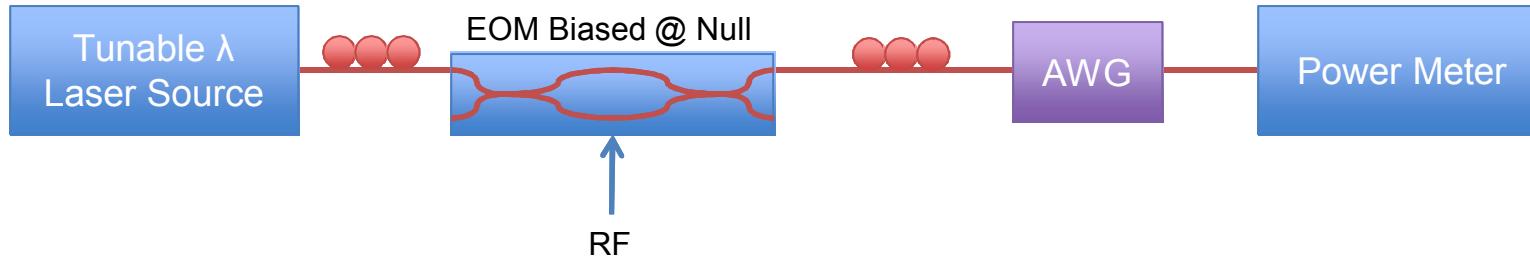
*Phases relative to waveguide #18

Optimization & Performance

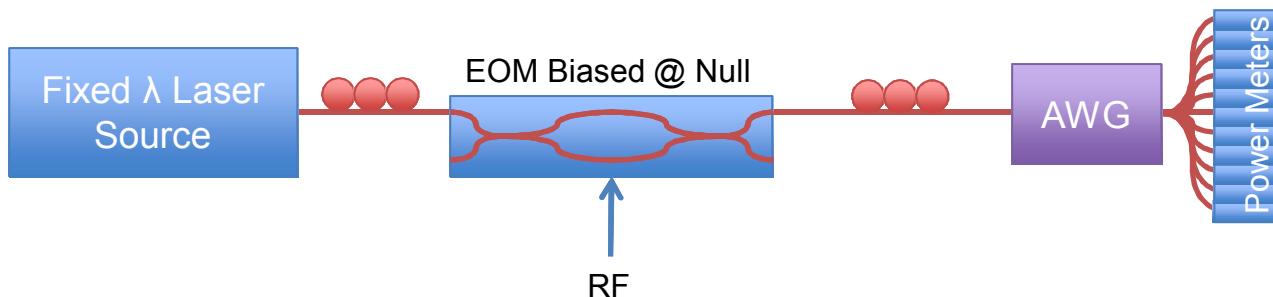
1 GHz Channel Spacing



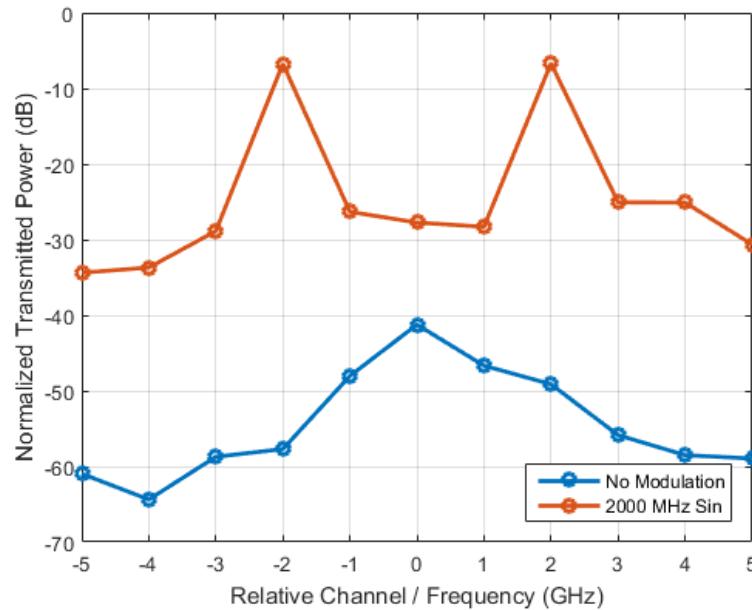
Applications – RF Signal Processing



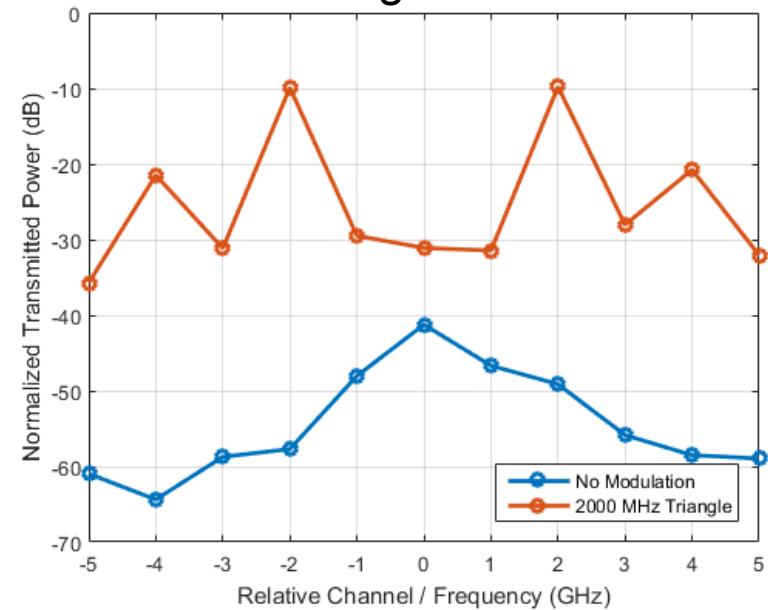
Applications – RF Signal Processing



2 GHz Sinusoidal Modulation

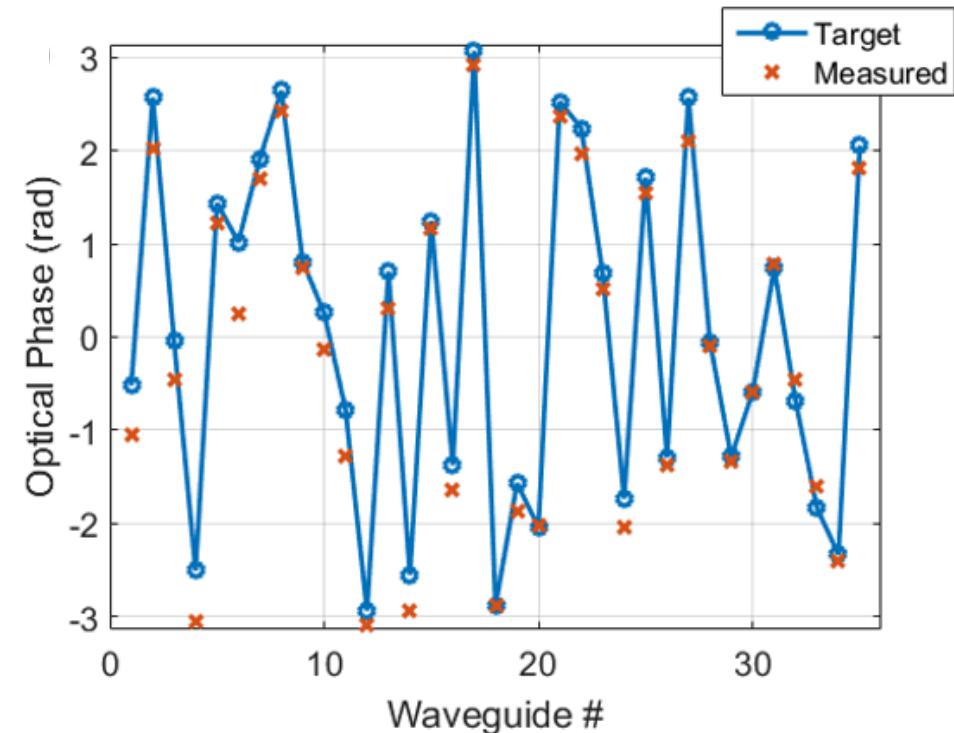
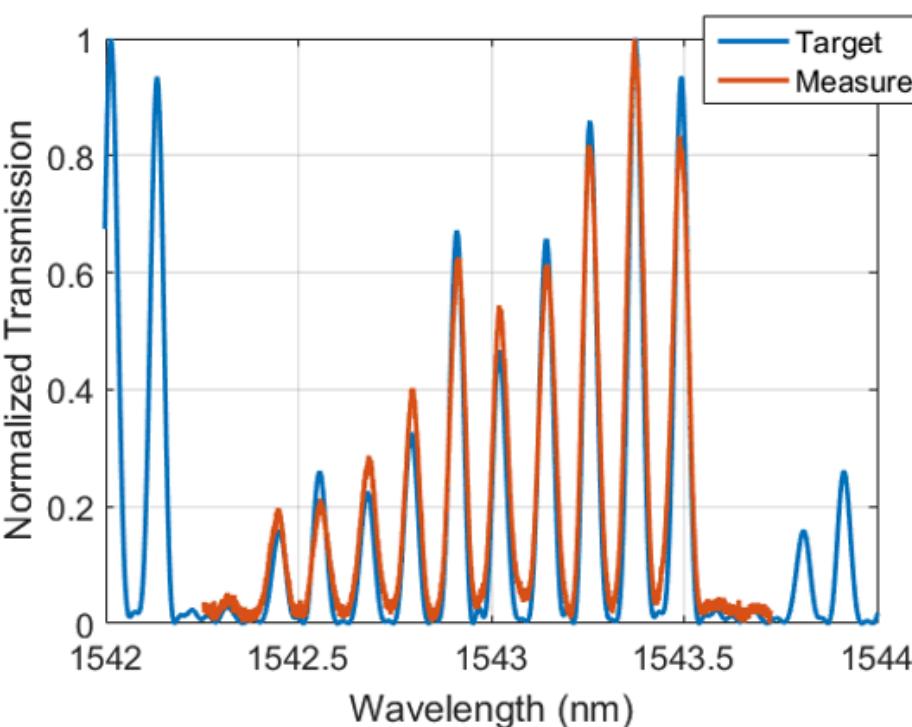


2 GHz Triangular Modulation



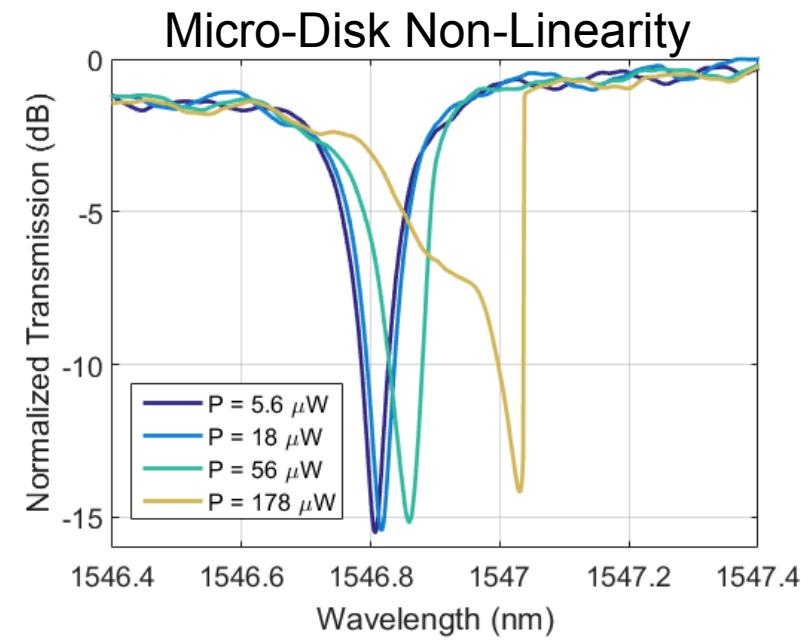
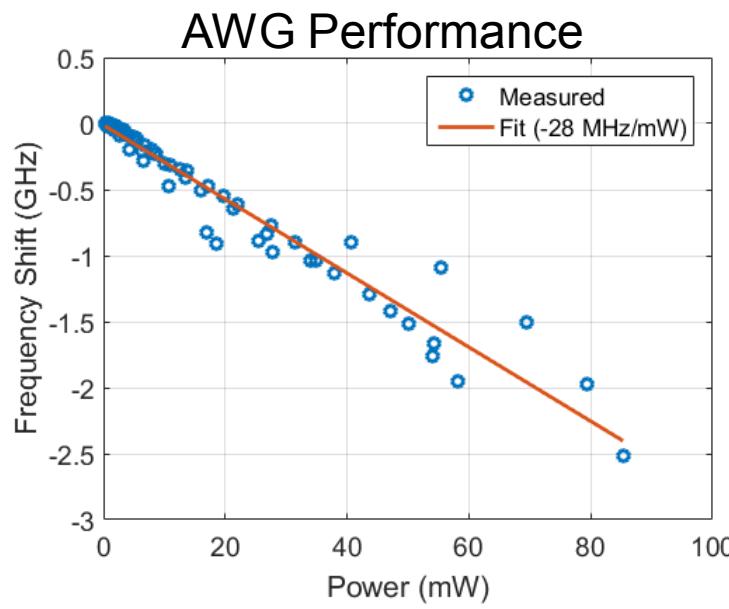
Applications – Spectral Shaping

- Gerchberg-Saxton Algorithm can be used to modify spectral transmission
 - Iterative algorithm which provides a target phase offset for each waveguide
 - Possible shapes limited by number of arrayed waveguides



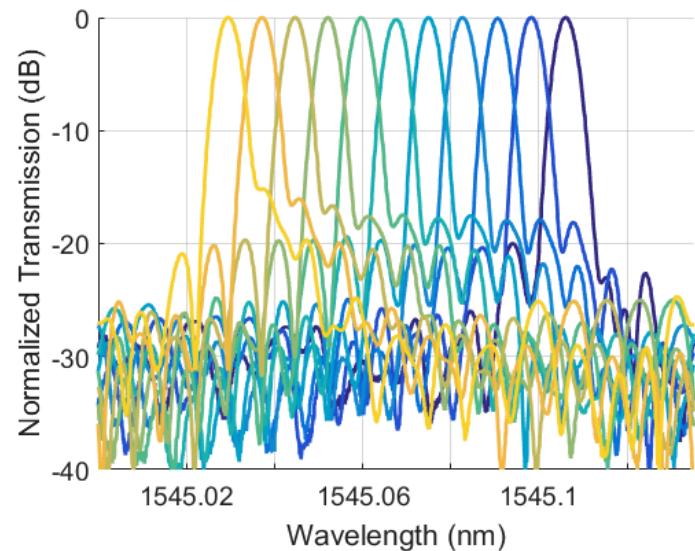
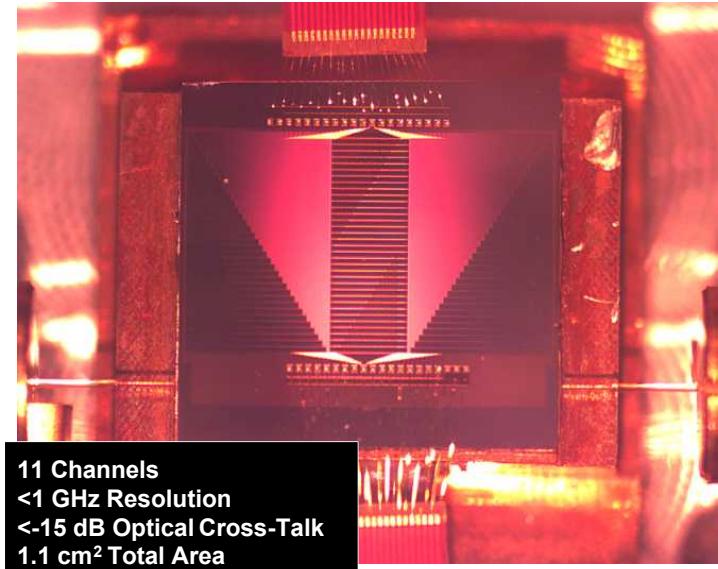
Applications – High Power Handling

- Resonant structures (i.e. micro-disks) have power limitations due to enhanced non-linearity
- AWG is non-resonant and can handle high powers
 - Observed shift of 28 MHz/mW
 - Could be compensated for by a temperature shift of only 0.003°C/mW



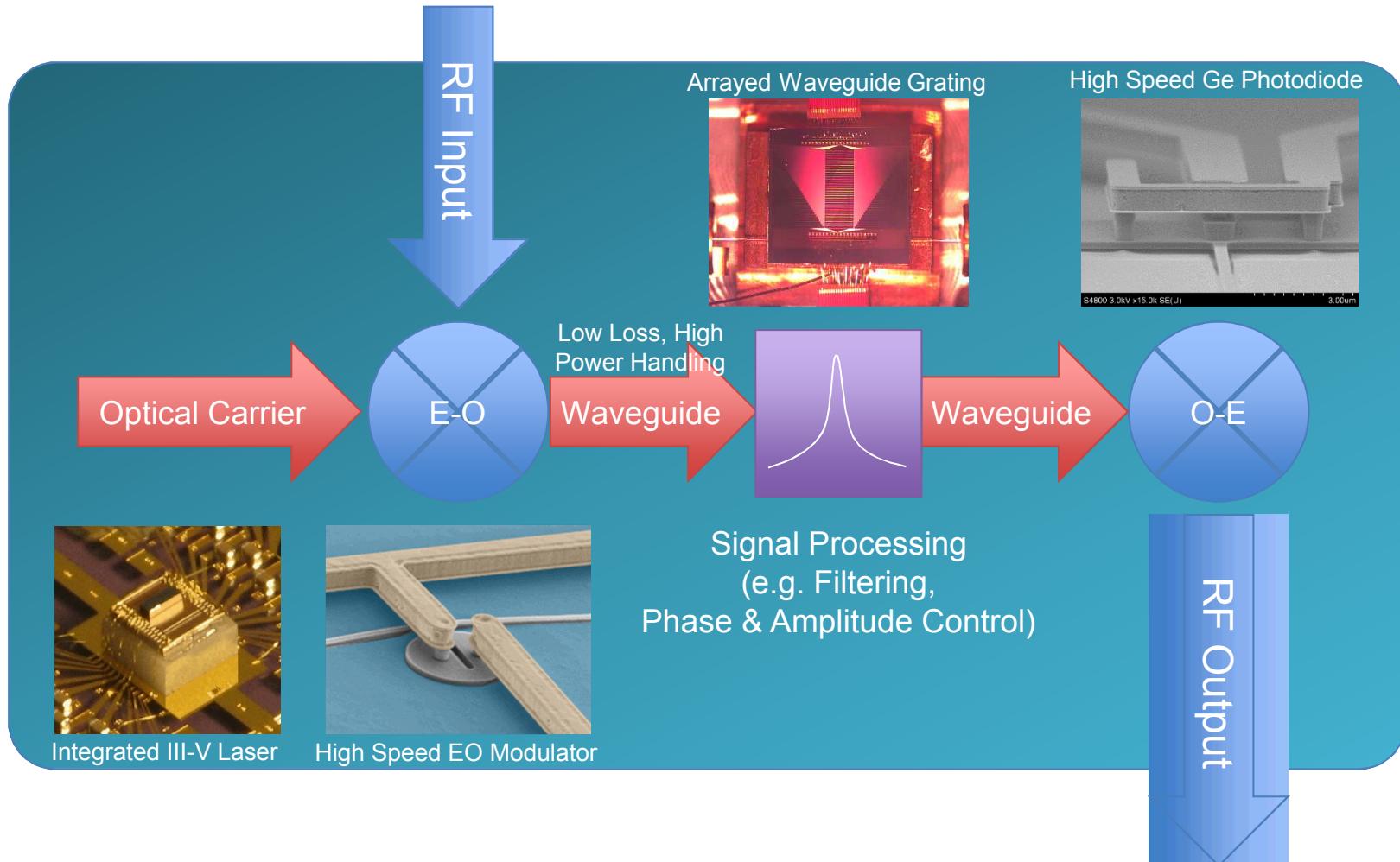
Conclusion

- Silicon photonic arrayed waveguide gratings provide compact and high resolution spectral filtering
- We have demonstrated <1GHz resolution through active thermo-optic phase tuning
- Demonstrated RF Channelization and Spectral Shaping
- Improvement of thermal isolation and phase shifter efficiency will improve performance



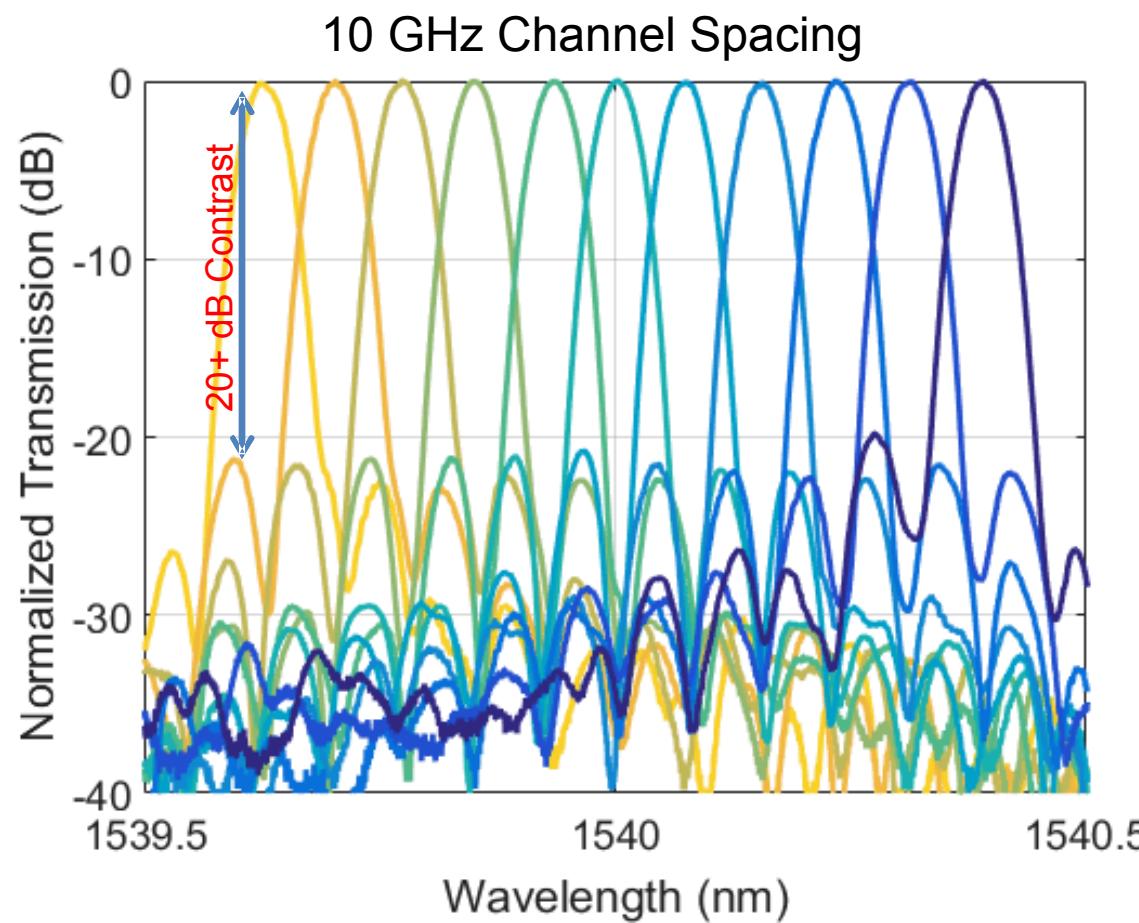
Silicon Photonics for RF Processing

Integrated Photonic Chip for Reduced SWaP-C



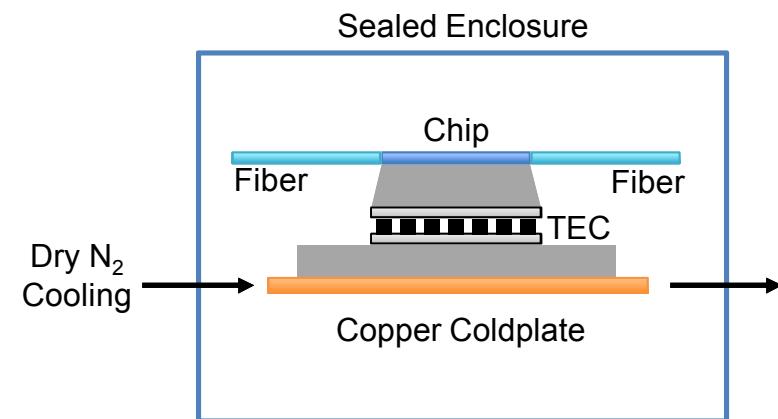
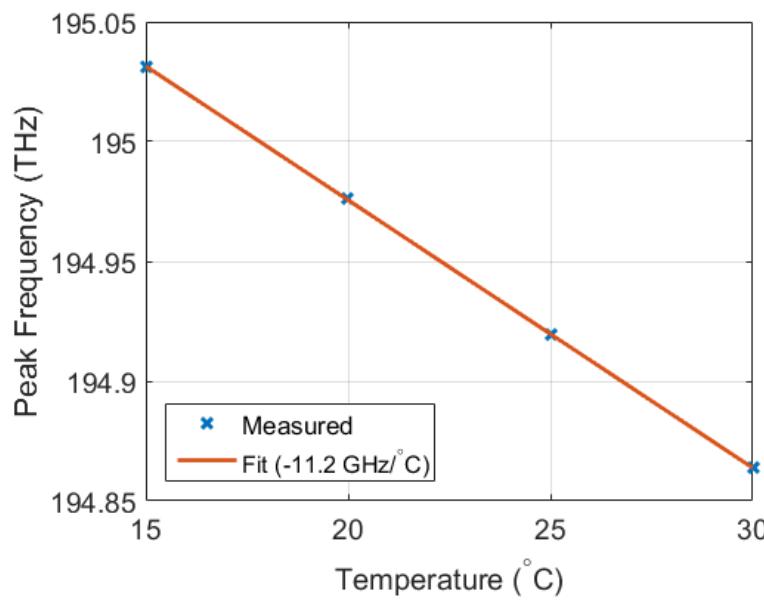
Optimization & Performance

- Iterative optimization necessary to account for thermal cross-talk



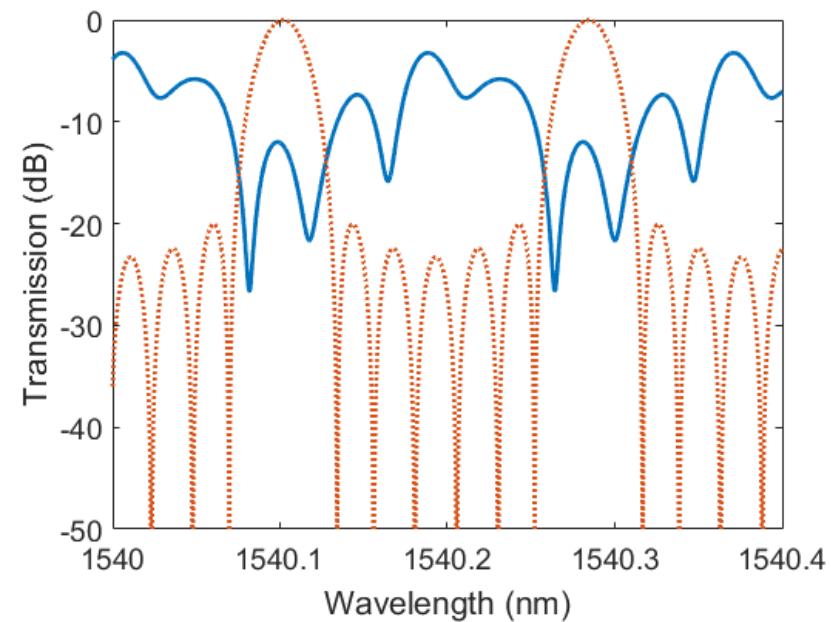
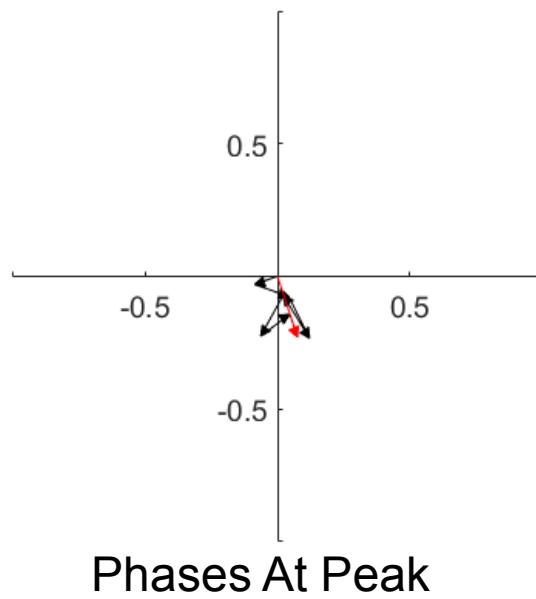
Thermal Considerations

- Temperature change creates a linear phase shift across each waveguide
 - Results in a shift in the peak transmission of $11 \text{ GHz}/^\circ\text{C}$
- Initial phase optimization requires demanding stability
 - Can be avoided with more advanced signal processing
- Significant phase shifter heat ($>1.5 \text{ W}$) which needs to be removed



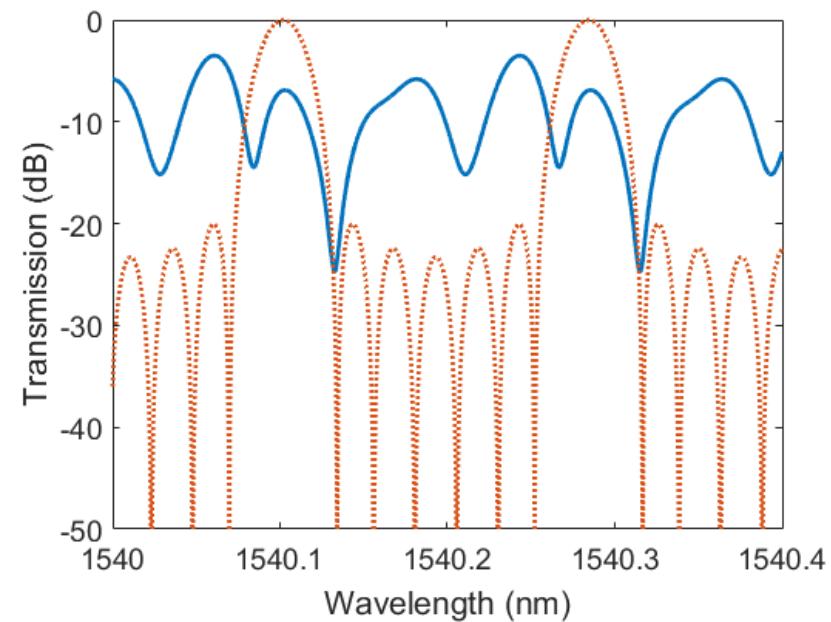
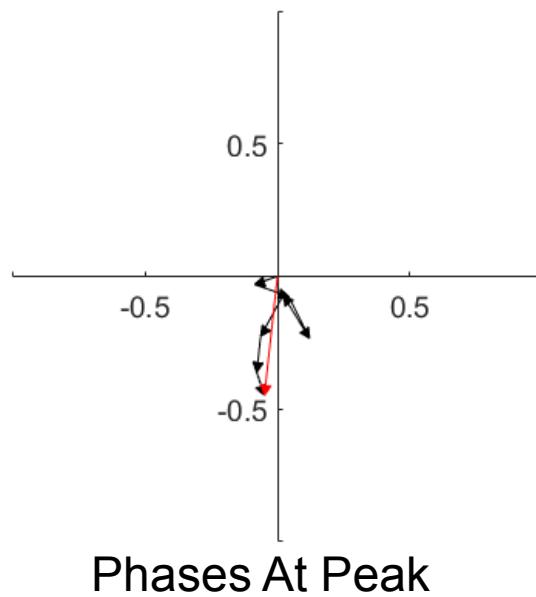
Optimization – Brute Force

- Output intensity at a fixed wavelength can be pictured as phasor addition of each arrayed waveguide
- Phase errors cause random walk in phasor addition
- Rotating a single waveguide phase by 2π causes a sinusoidal variation in the output power
- Choosing the phase which maximizes output power for each waveguide individually will straighten out the random walk



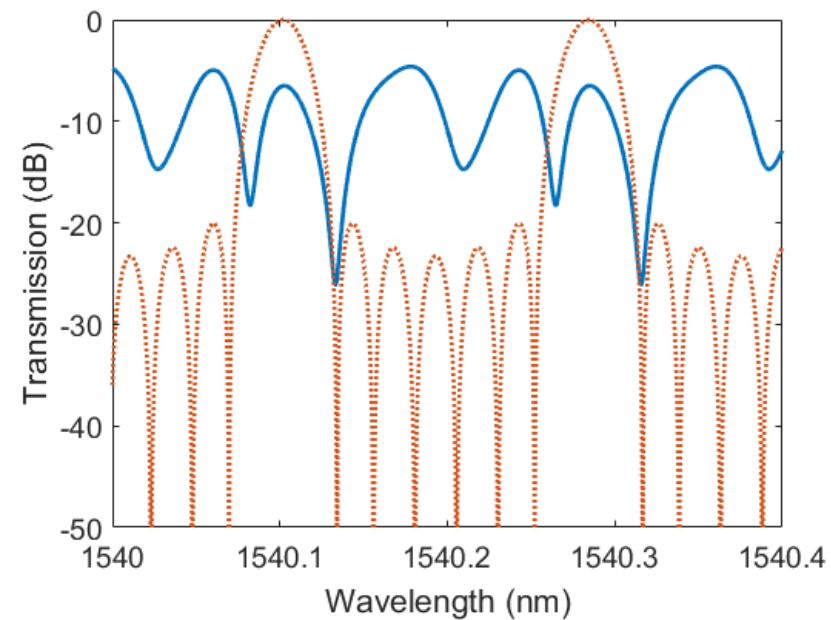
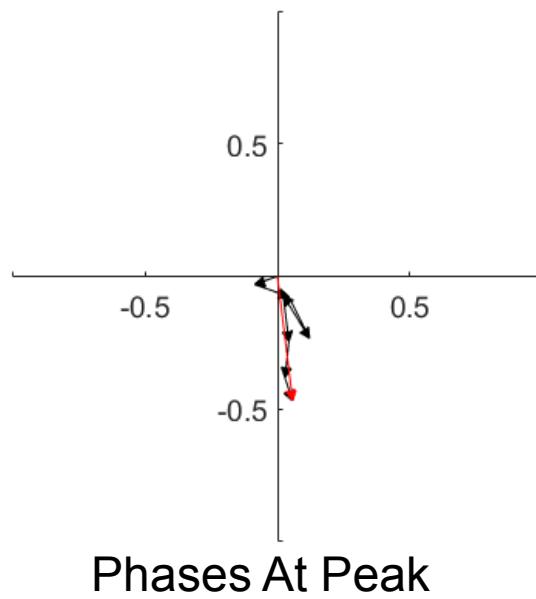
Optimization – Brute Force

- Output intensity at a fixed wavelength can be pictured as phasor addition of each arrayed waveguide
- Phase errors cause random walk in phasor addition
- Rotating a single waveguide phase by 2π causes a sinusoidal variation in the output power
- Choosing the phase which maximizes output power for each waveguide individually will straighten out the random walk



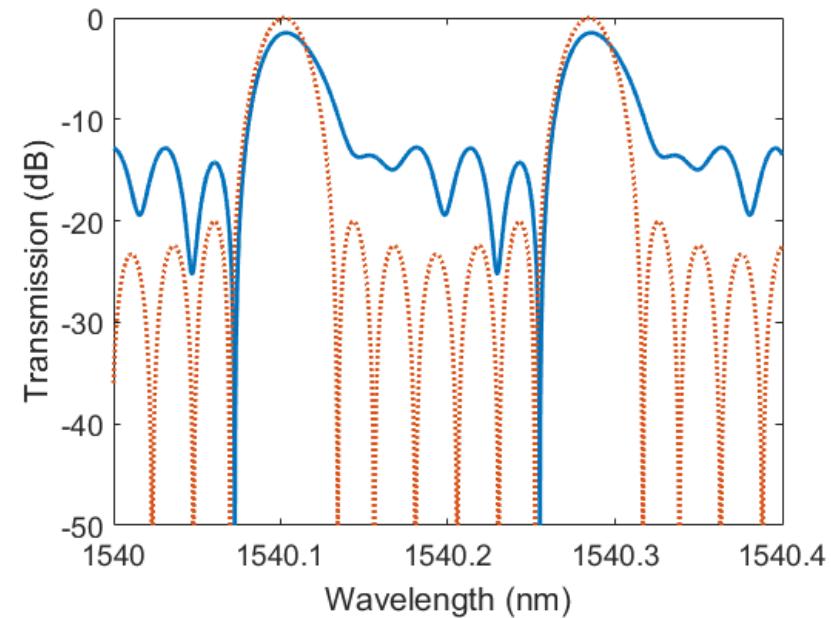
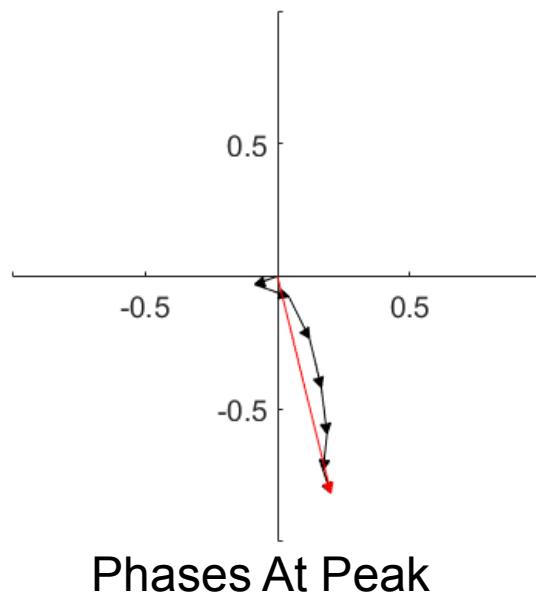
Optimization – Brute Force

- Output intensity at a fixed wavelength can be pictured as phasor addition of each arrayed waveguide
- Phase errors cause random walk in phasor addition
- Rotating a single waveguide phase by 2π causes a sinusoidal variation in the output power
- Choosing the phase which maximizes output power for each waveguide individually will straighten out the random walk



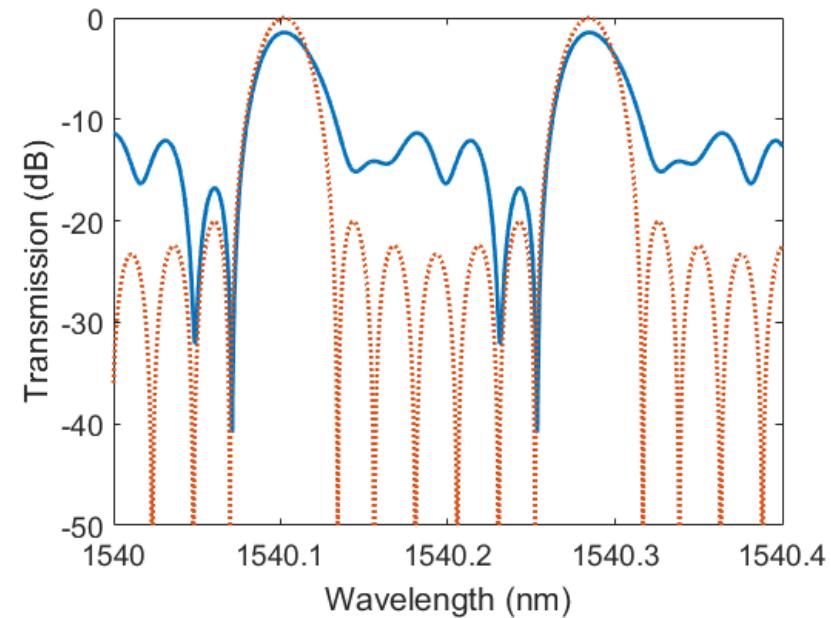
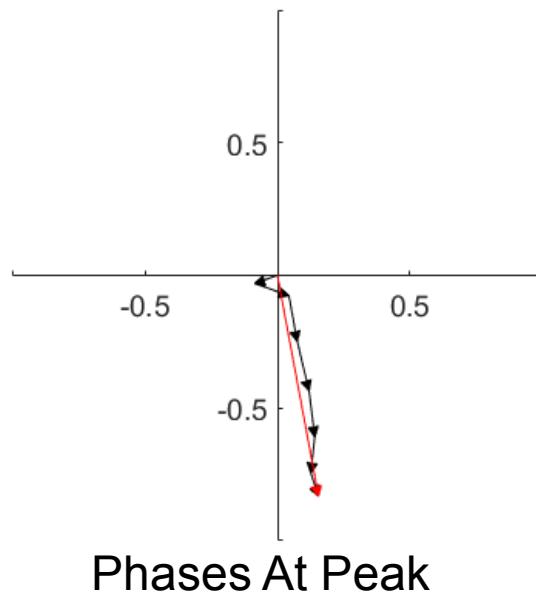
Optimization – Brute Force

- Output intensity at a fixed wavelength can be pictured as phasor addition of each arrayed waveguide
- Phase errors cause random walk in phasor addition
- Rotating a single waveguide phase by 2π causes a sinusoidal variation in the output power
- Choosing the phase which maximizes output power for each waveguide individually will straighten out the random walk



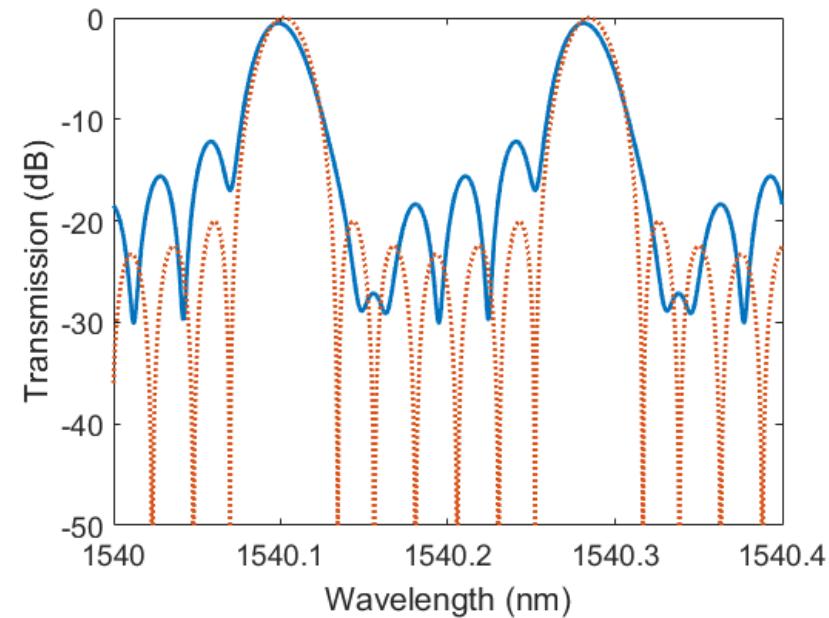
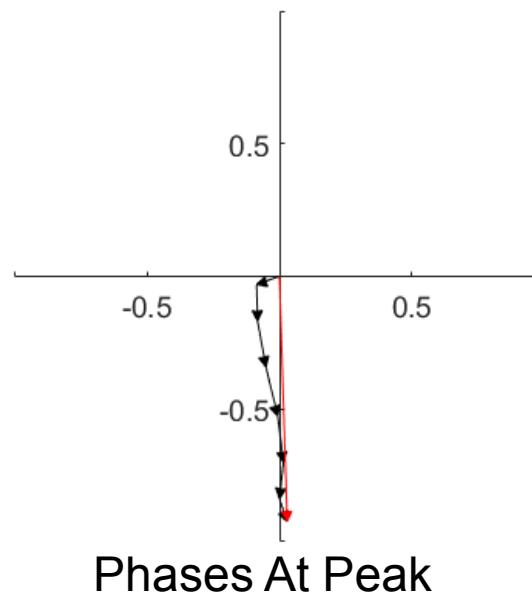
Optimization – Brute Force

- Output intensity at a fixed wavelength can be pictured as phasor addition of each arrayed waveguide
- Phase errors cause random walk in phasor addition
- Rotating a single waveguide phase by 2π causes a sinusoidal variation in the output power
- Choosing the phase which maximizes output power for each waveguide individually will straighten out the random walk



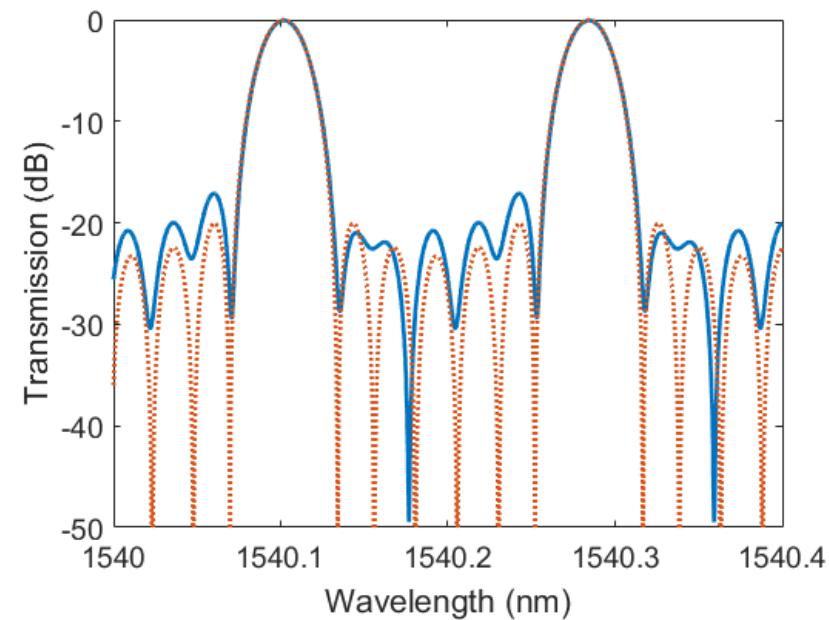
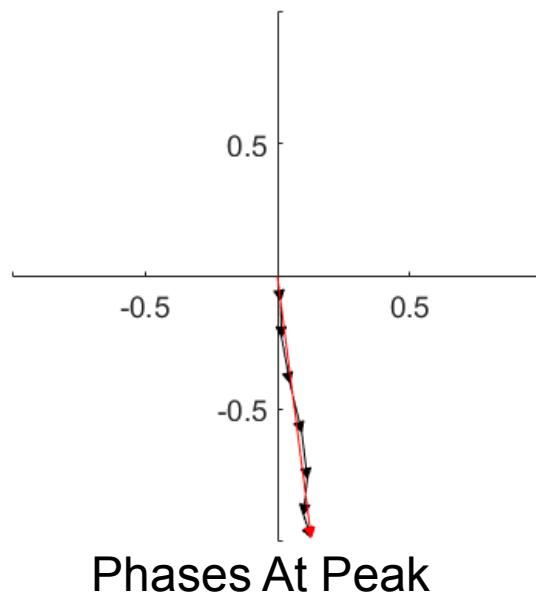
Optimization – Brute Force

- Output intensity at a fixed wavelength can be pictured as phasor addition of each arrayed waveguide
- Phase errors cause random walk in phasor addition
- Rotating a single waveguide phase by 2π causes a sinusoidal variation in the output power
- Choosing the phase which maximizes output power for each waveguide individually will straighten out the random walk



Optimization – Brute Force

- Output intensity at a fixed wavelength can be pictured as phasor addition of each arrayed waveguide
- Phase errors cause random walk in phasor addition
- Rotating a single waveguide phase by 2π causes a sinusoidal variation in the output power
- Choosing the phase which maximizes output power for each waveguide individually will straighten out the random walk



Optimization – Brute Force

- Benefits
 - Simple Implementation – Single fixed wavelength laser and power meter
 - High Contrast Ratio
 - Easy to shift peak wavelength
- Challenges
 - Intensity oscillation amplitude is less than $1/(\# \text{ of channels})$
 - Thermal cross-talk complicates simple phasor addition picture

