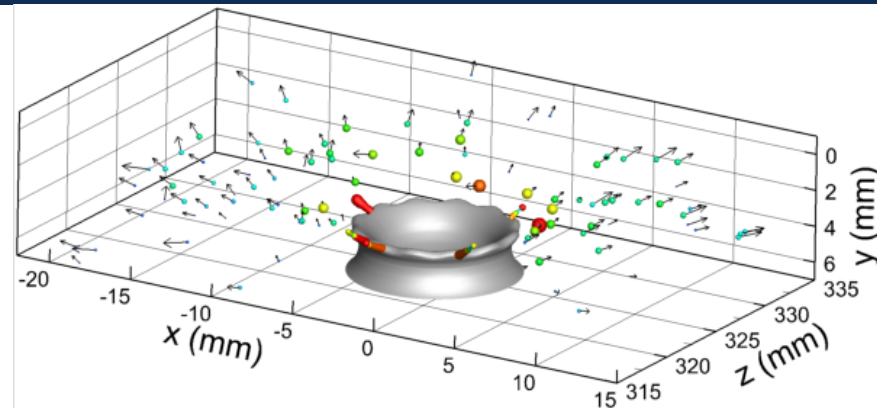
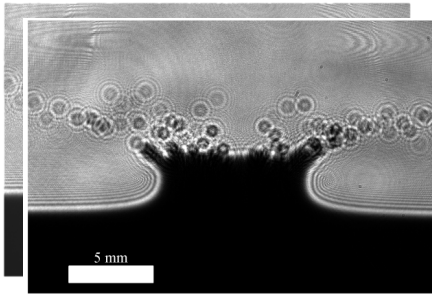


Exceptional service in the national interest



Digital In-line Holography (DIH) for 3D Quantification of Inert and Reacting Particle Fields

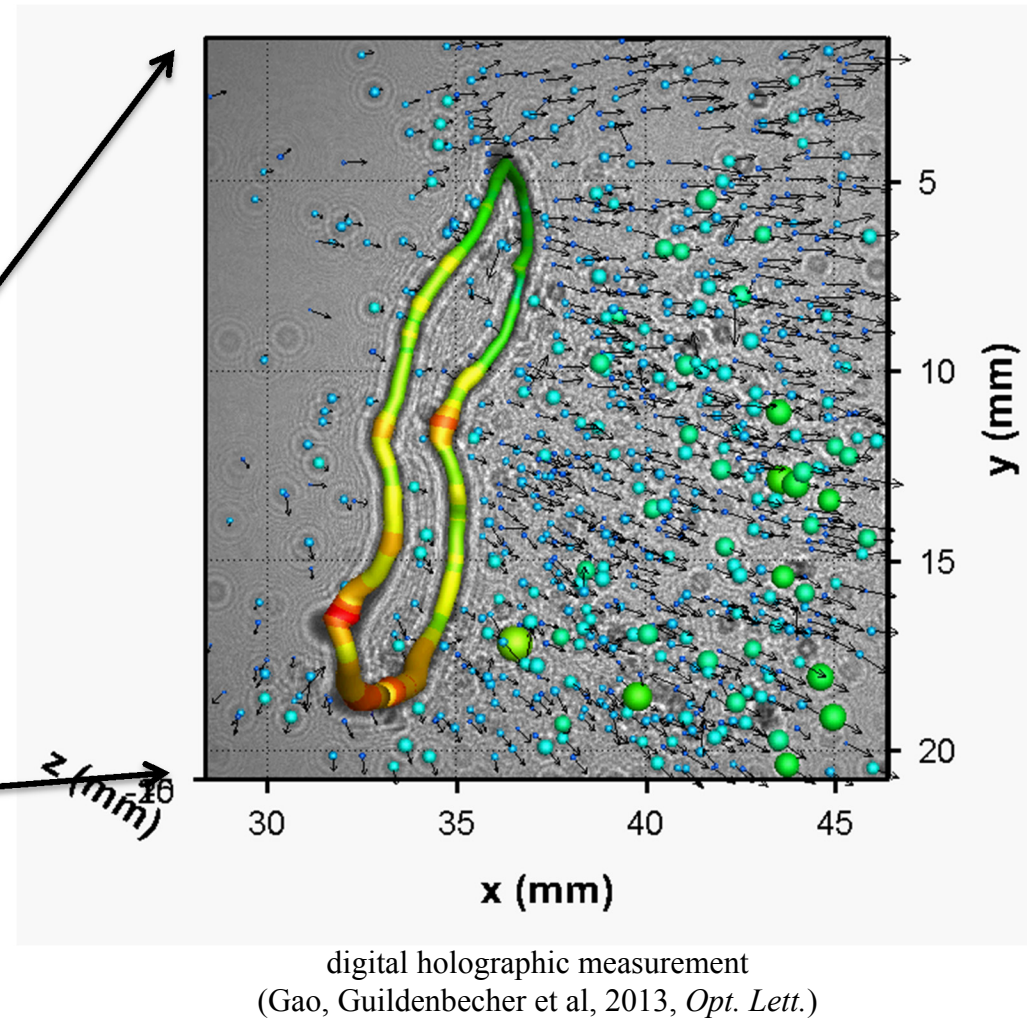
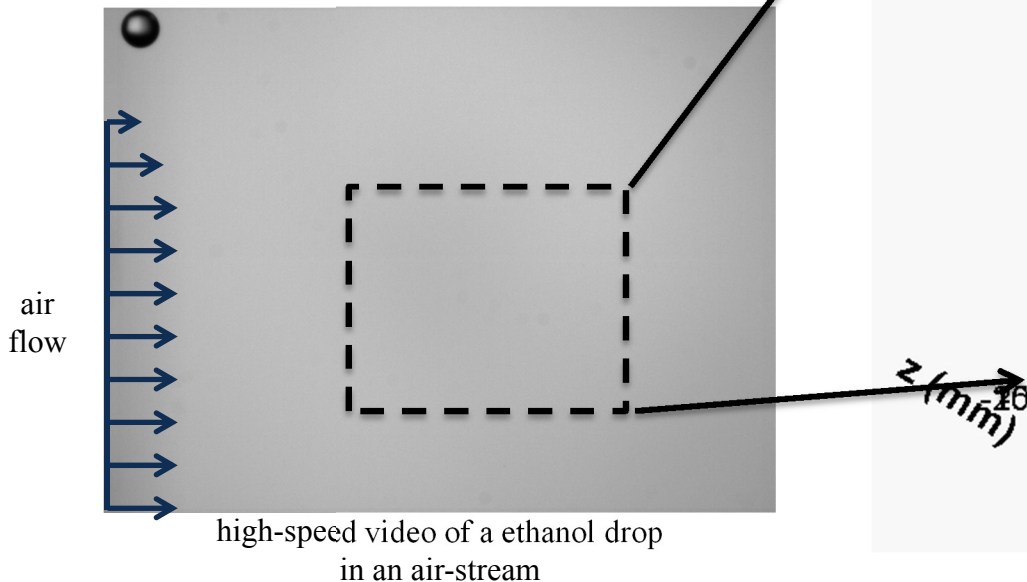
Daniel R. Guildenbecher

May 19, 2015

Motivation: 3D imaging for a 3D world

Widely available 2D imaging or point-wise measurement techniques are often insufficient to resolve 3D flow phenomena

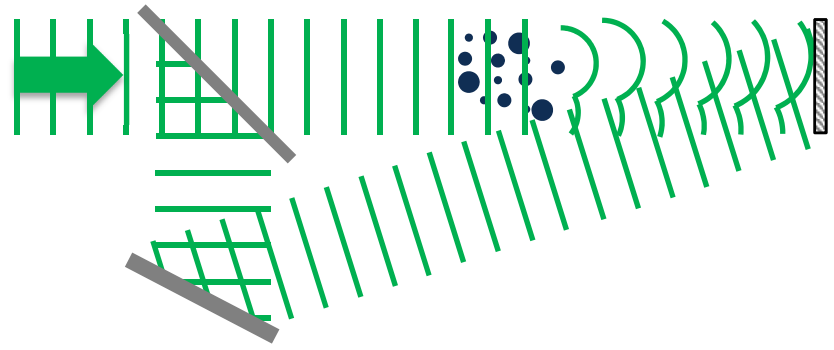
- Repetition needed to capture spatial statistics



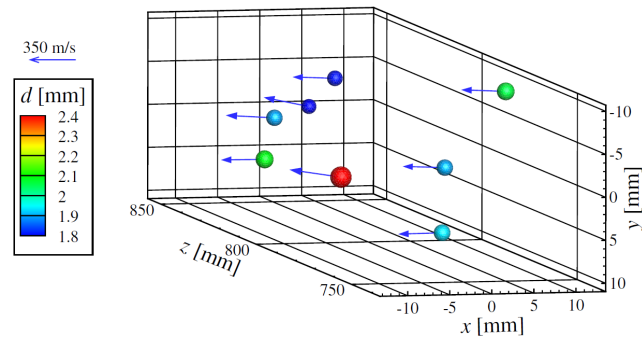
Holography is an optical technique to record and reconstruct a 3D light field

Outline for talk

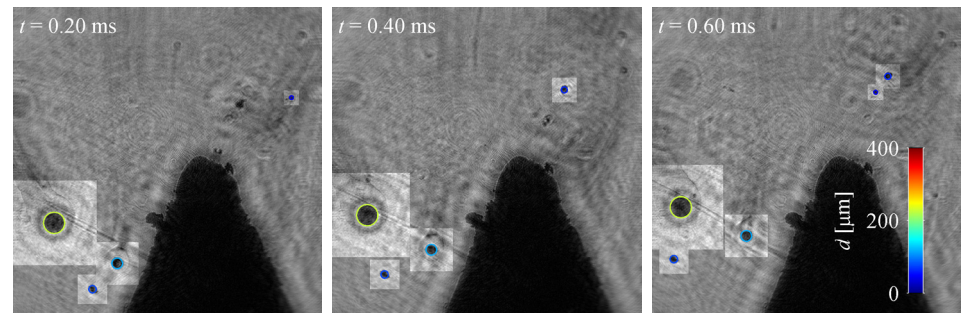
Introduction to holography and
the “digital revolution”



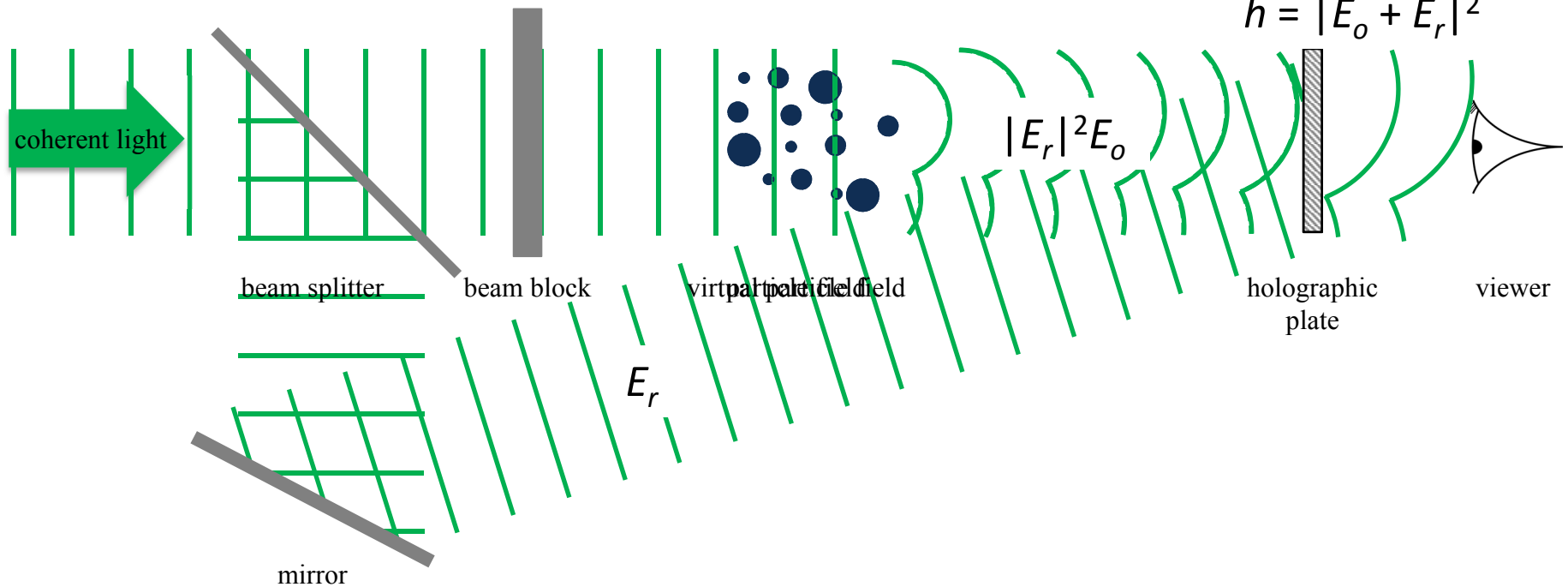
Particle measurements



Recent advancements



What is holography?



Optical method first proposed by Gabor in 1948

1. Coherent light diffracted by particle field forms the object wave, E_o
2. Interference with a reference wave, E_r , forms the hologram: $h = |E_o + E_r|^2$
3. Reconstruction with E_r forms virtual images at original particle locations

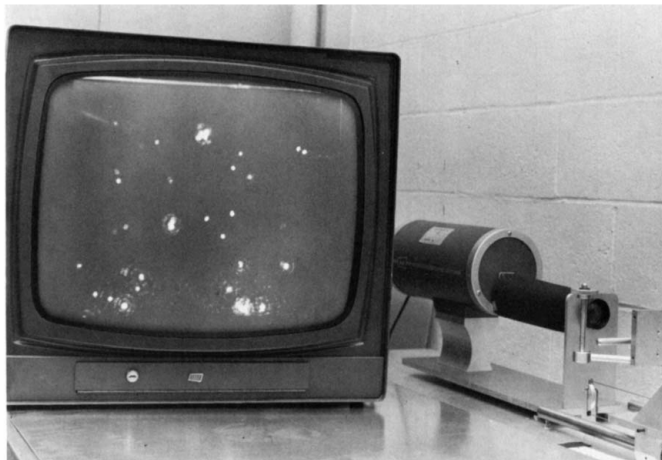
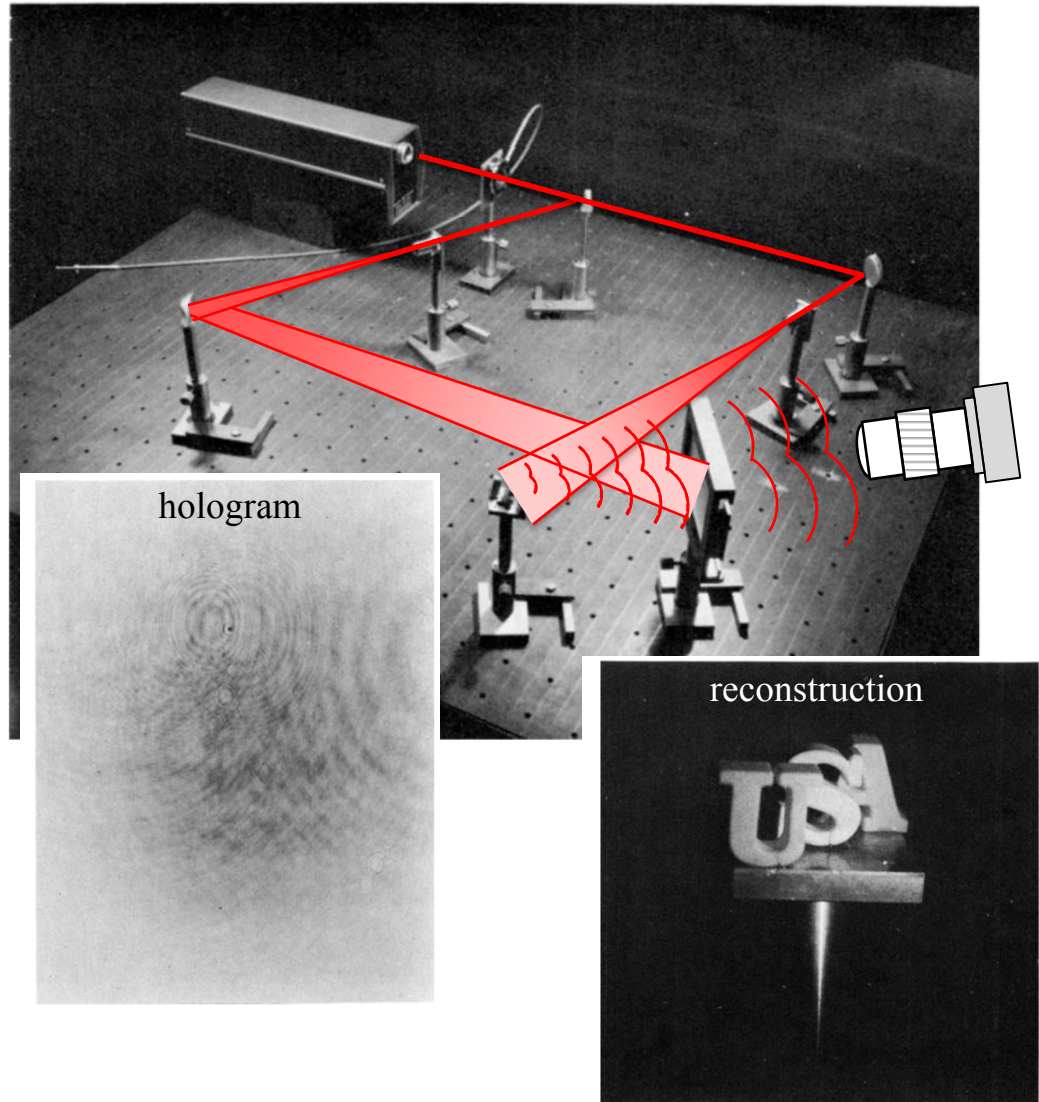
$$h \cdot E_r = \underbrace{(|E_o|^2 + |E_r|^2)E_r}_{\text{DC term}} + \underbrace{|E_r|^2 E_o}_{\text{virtual image}} + \underbrace{E_r^2 E_o^*}_{\text{real image}}$$

Analog holography

Applications of holography took off with invention of the laser in 1960

Challenges:

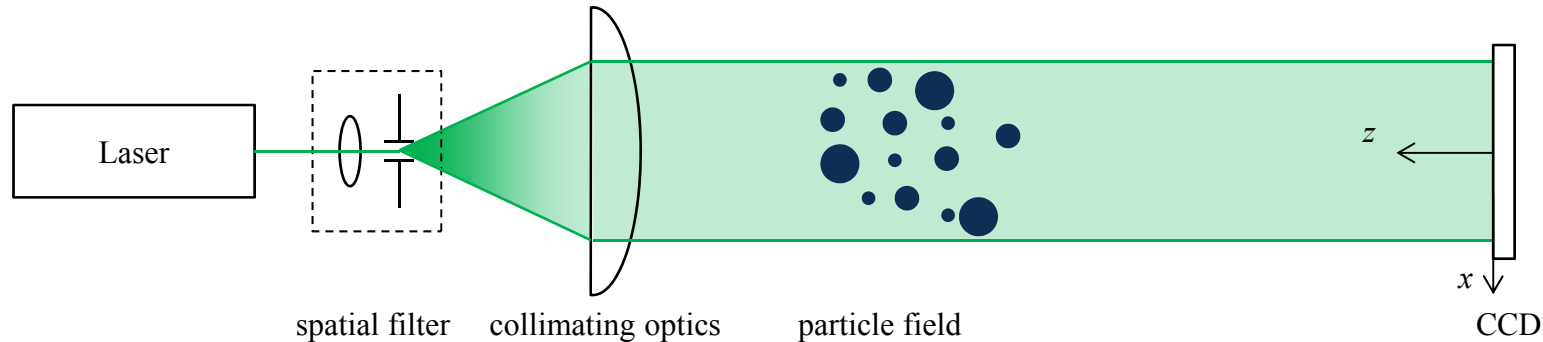
- Darkroom needed to process the hologram
- Limited temporal resolution
- Manual post processing



Thompson et al, 1967, *Appl. Opt.*

Collier et al, 1971, *Optical Holography*

Digital in-line holography (DIH)



Holographic plate and wet-chemical processing replaced with digital sensor

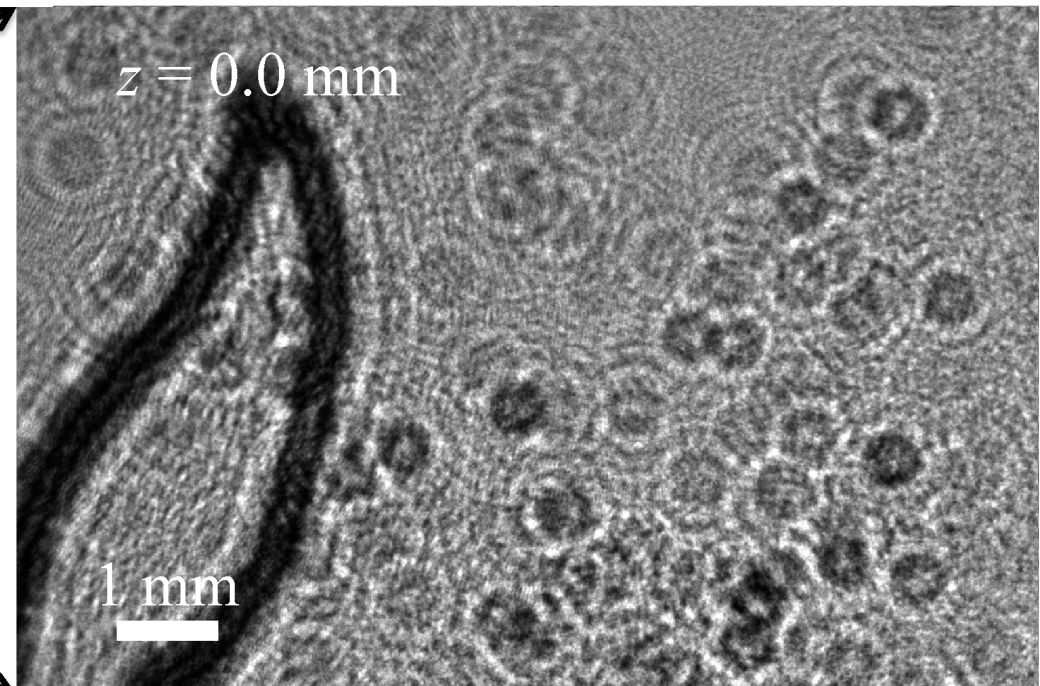
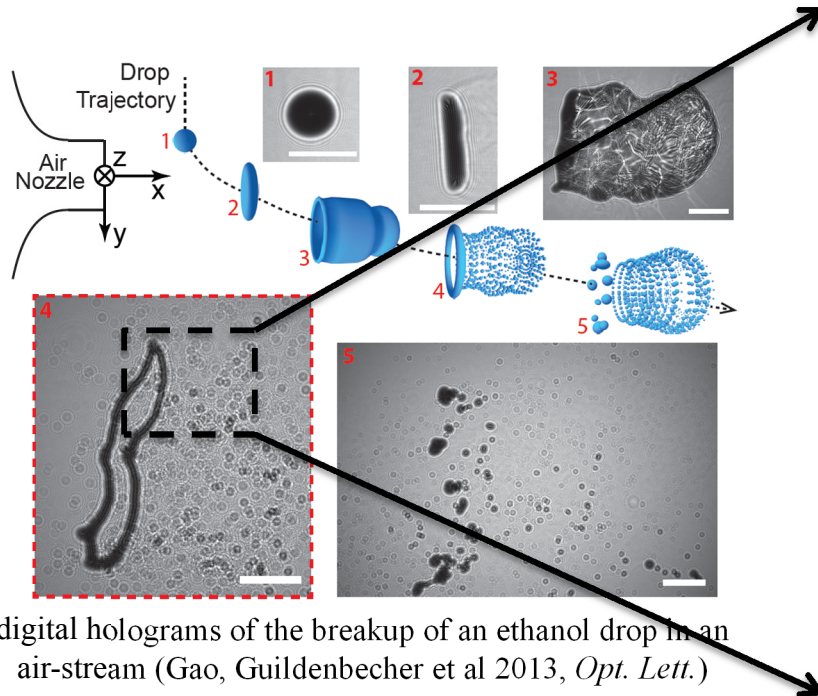
- First proposed by Schnars and Jüptner in '90s
- Advantages: (1) no darkroom, (2) temporal resolution is straight forward, (3) results can be numerically refocused and post-processed
- Challenge: Resolution of digital sensors (order 100 line pairs/mm) is much less than resolution of photographic emulsions (order 5,000 line pairs/mm)
 - For suitable off axis angles, θ , the fringe frequency, f , is typically too large to resolve with digital sensors ($f = 2\sin(\theta/2)/\lambda$)
 - Rather, the in-line configuration ($\theta = 0$) is typically utilized

Numerical refocusing

Light propagation in a non-absorbing, constant index of refraction medium is described by the diffraction integral equation:

$$E(x, y, z) = \frac{1}{\lambda} \iint E(\xi, \eta, z=0) \frac{e^{-jkr}}{r} d\xi d\eta \quad \text{where: } r = \sqrt{(\xi - x)^2 + (\eta - y)^2 + z^2}$$

- $E(\xi, \eta, 0) \equiv$ complex amplitude at hologram plane = $h(\xi, \eta) \cdot E_r^*$
- $E(x, y, z) \equiv$ refocused complex amplitude at optical depth z

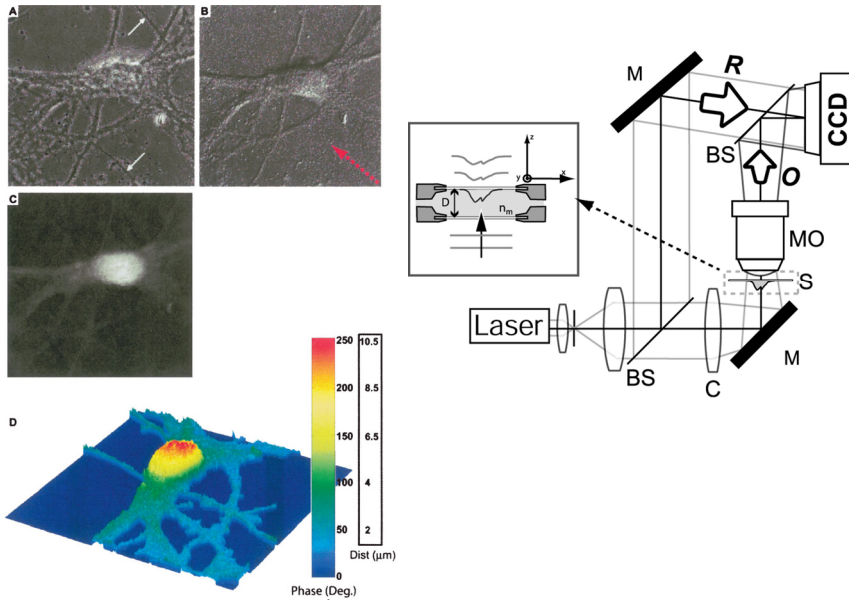


reconstructed digital hologram at optical depth, z

digital holograms of the breakup of an ethanol drop in an air-stream (Gao, Guildenbecher et al 2013, *Opt. Lett.*)

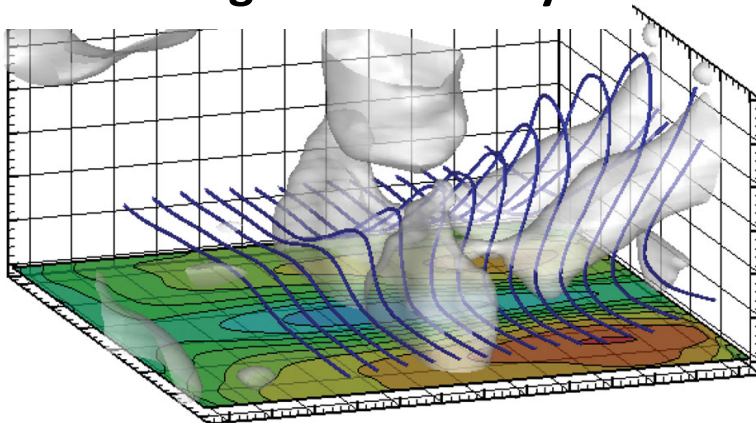
DIH in the literature

Microscopy



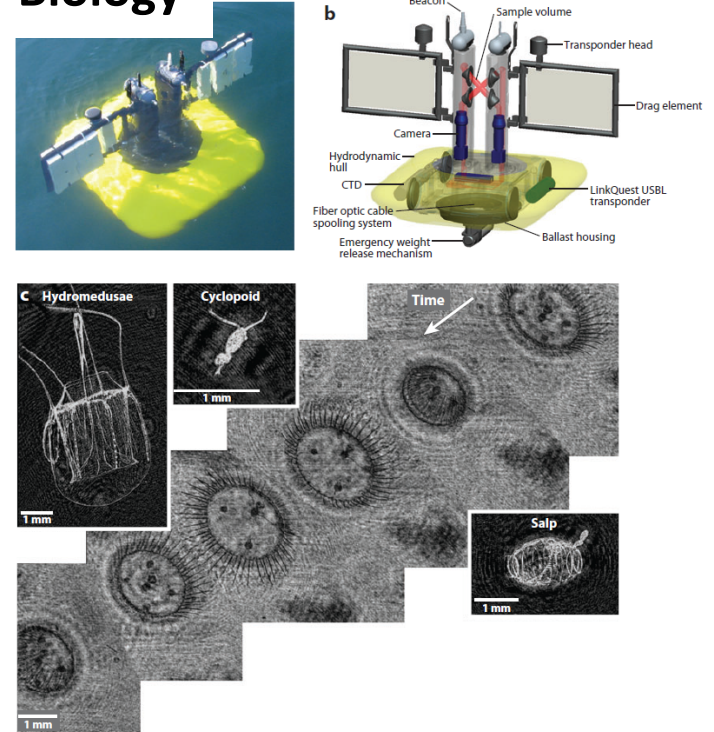
Marquet et al 2005, *Opt. Lett.*

Particle Image Velocimetry



Sheng et al 2009, *J. Fluid Mech.*

Biology

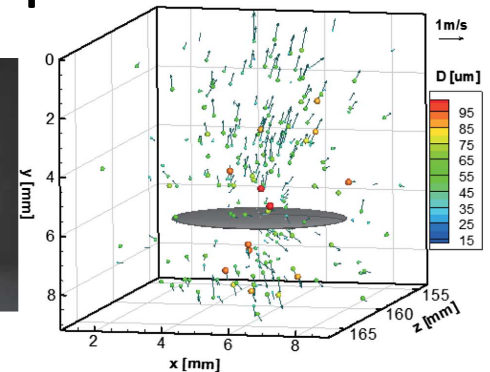


Katz and Sheng 2010, *Annu. Rev. Fluid Mech.*

Multiphase Flows



Yao et al 2015, *Appl Opt.*



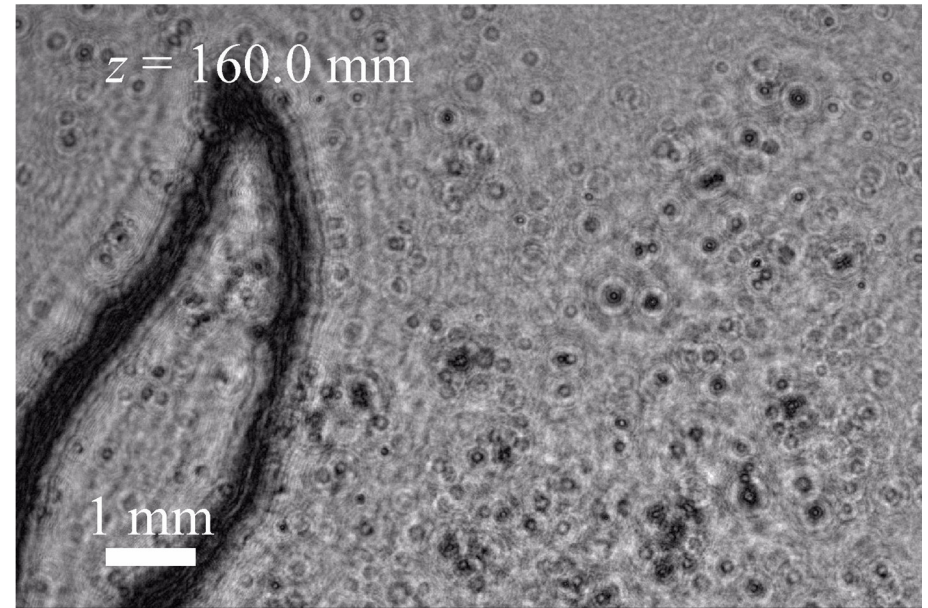
Particle measurements

Data processing

Acquisition and refocusing of a digital hologram is relatively straightforward.

However...

For quantitative measurements, methods are required to locate and measure particles.



Challenge: depth-of-focus problem

The spatial extent of the diffraction pattern limits the angular aperture, Ω , from which a particle is effectively reconstructed (Meng et al, 2004, *Meas. Sci. Technol.*)

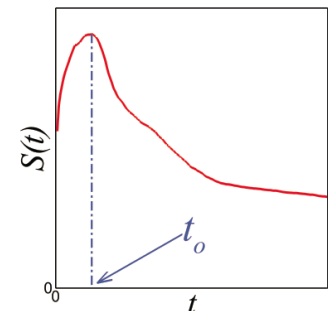
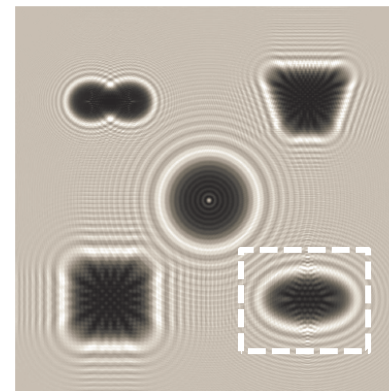
- From the central diffraction lobe $\rightarrow \Omega \approx 2\lambda/d$
- Using the traditional definition of depth-of-focus, δ , based on change of intensity within the particle center $\rightarrow \delta \approx 4\lambda/\Omega^2$
- Therefore: for in-line holography, $\delta \approx d^2/\lambda$
 - Example: $d = 300 \mu\text{m}$, $\lambda = 532 \text{ nm} \rightarrow \delta \approx 170 \text{ mm!}$

Literature contains two basic methods to find the focal plane:

1. Fit a model to the observed diffraction patterns (inverse method)
 - Generally accurate with small depth uncertainty
 - Limited to objects with known diffraction patterns (spheres)
2. Reconstruct the amplitude (or intensity) throughout depth and apply a focus metric to find “in-focus” objects
 - No *a-priori* knowledge of particle shape required
 - Accuracy is a strong function of the chosen focus metric

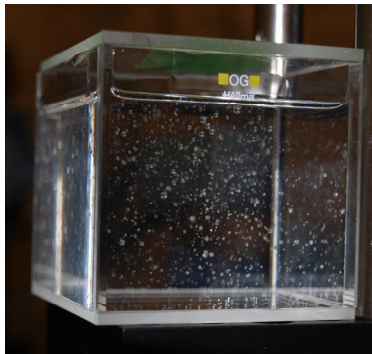
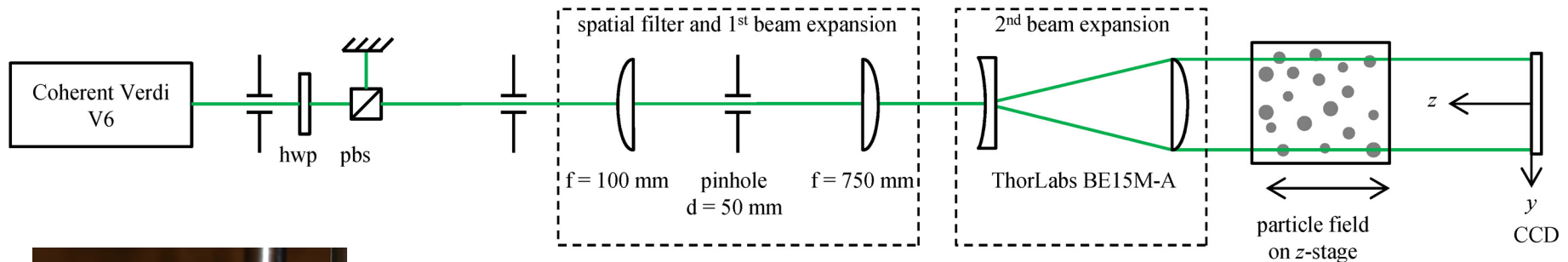
Hybrid method:

- Focus metric is a combination of amplitude minimization and edge sharpness maximization
 - Details in Guildenbecher et al 2013, *Appl. Opt.*; Gao et al 2013, *Opt. Express*; Gao et al 2014, *Appl. Opt.*



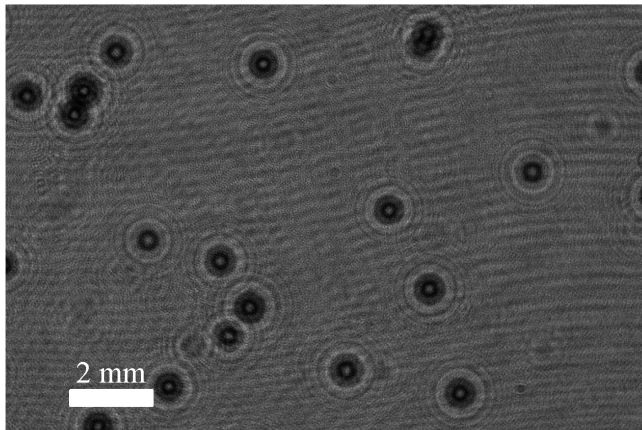
Gao et al 2014, *Appl. Opt.*

Experimental validation

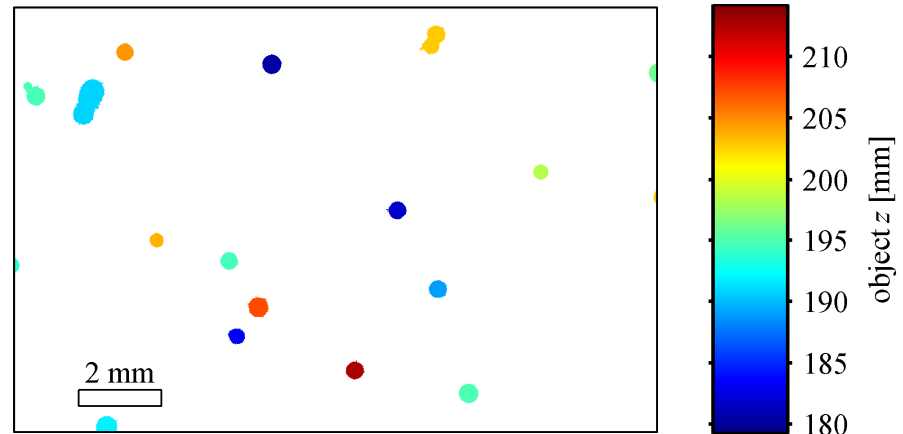


particle field

- Quasi-stationary particle field
 - Polystyrene beads ($\bar{d} \approx 465 \mu\text{m}$) in 10,000 cSt silicone oil
 - Settling velocity $\approx 0.8 \mu\text{m/s}$
- Multiple holograms recorded, displacing the particle field 2 mm in the z-direction between each acquisition

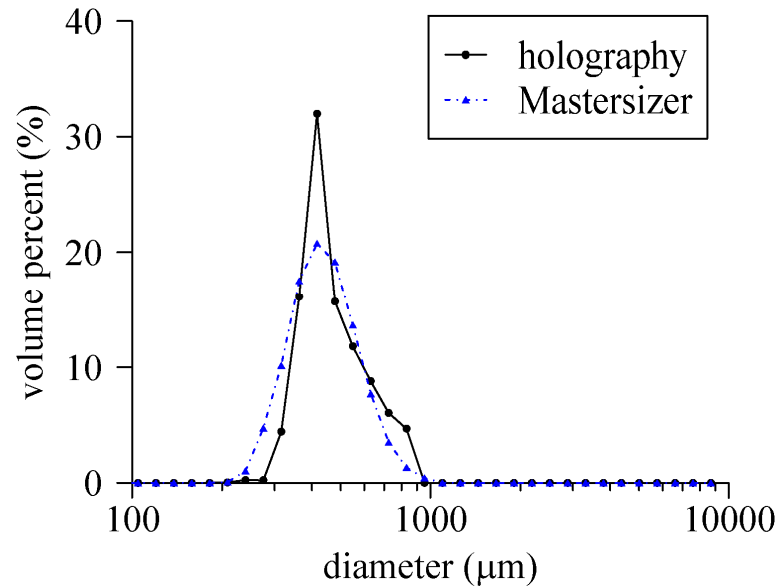


hologram



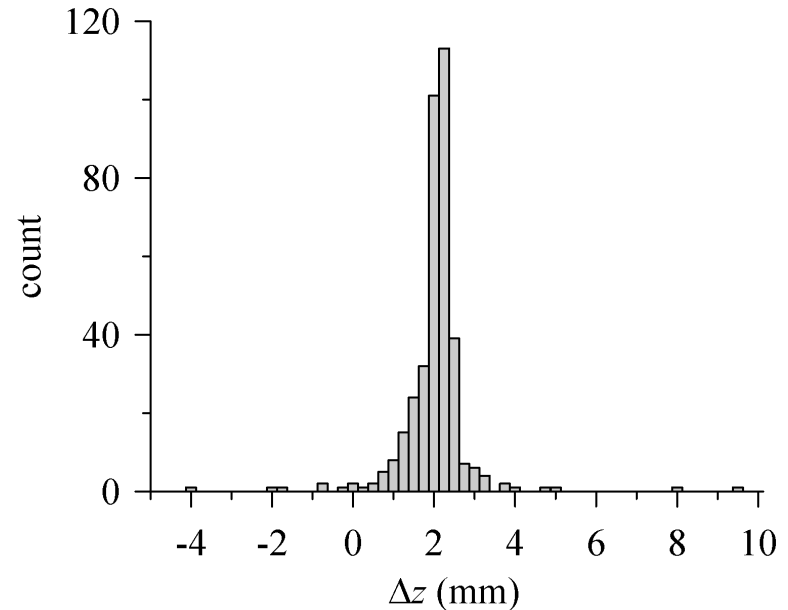
Detected objects colored by z-position

Experimental validation



Diameter measured from area of the detected 2D morphology

- Actual mass median diameter = 465 μm
- Measured mass median diameter = 474 μm
 - Error of 2.0% with respect to actual value



Displacement found by particle matching between successive holograms

- Actual displacement = 2.0 mm
- Mean detected displacement = 1.91 mm \pm 0.81 mm
 - Standard deviation of 1.74 times mean diameter

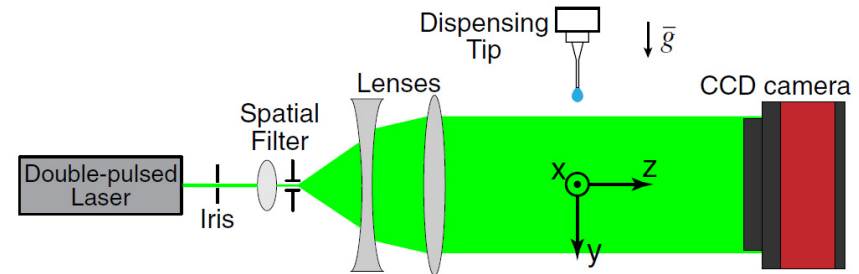
Aerodynamic drop fragmentation

Experimental configuration: Double-pulsed laser and imaging hardware as typically used in PIV

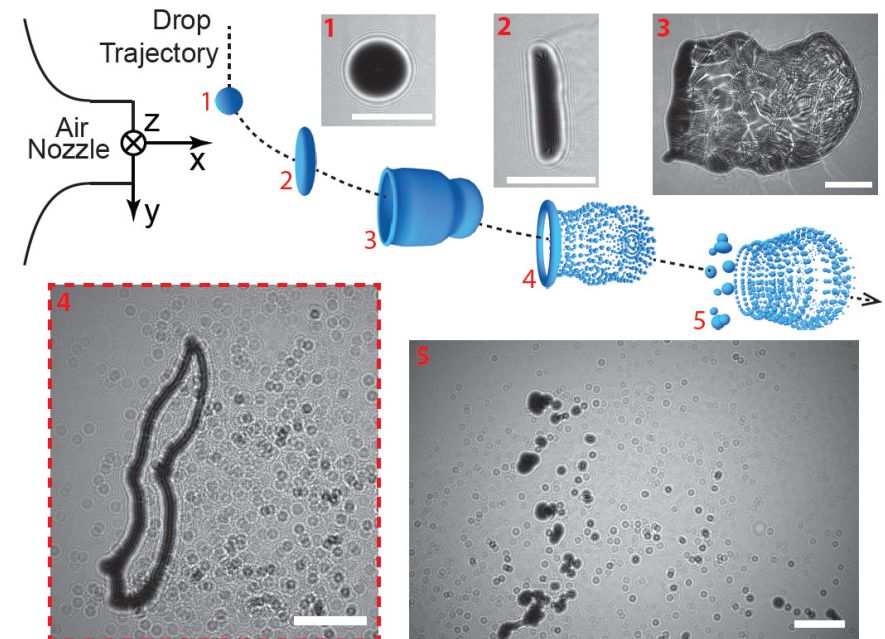
- $\lambda = 532 \text{ nm}$, 5 ns pulsewidth
- Interline transfer CCD (4008 × 2672, 9 μm pixel pitch)
- Temporal separation, $\Delta t = 62 \mu\text{s}$, determined by laser timing

Note: without a separate reference wave, coherence length requirements in DIH are greatly relaxed.

- Expensive injection seeders are not always needed
- Faster lasers (ps or fs) can be used with some advantages (e.g. Nicolas et al 2007, *Opt. Express*)



Optical configuration (Gao, Guildenbecher et al 2013, *Opt. Lett.*)

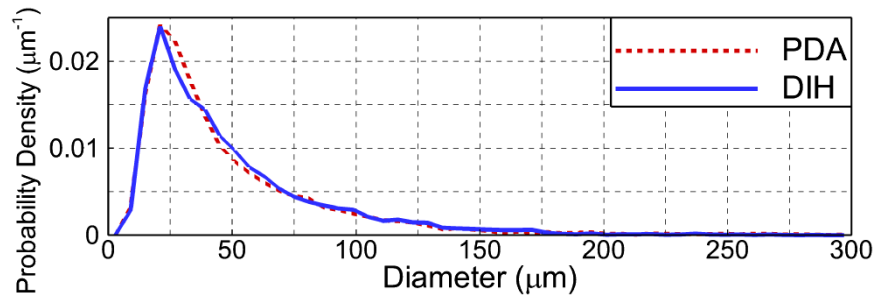


digital holograms of the breakup of an ethanol drop in an air-stream (Gao, Guildenbecher et al 2013, *Opt. Lett.*)

Aerodynamic drop fragmentation

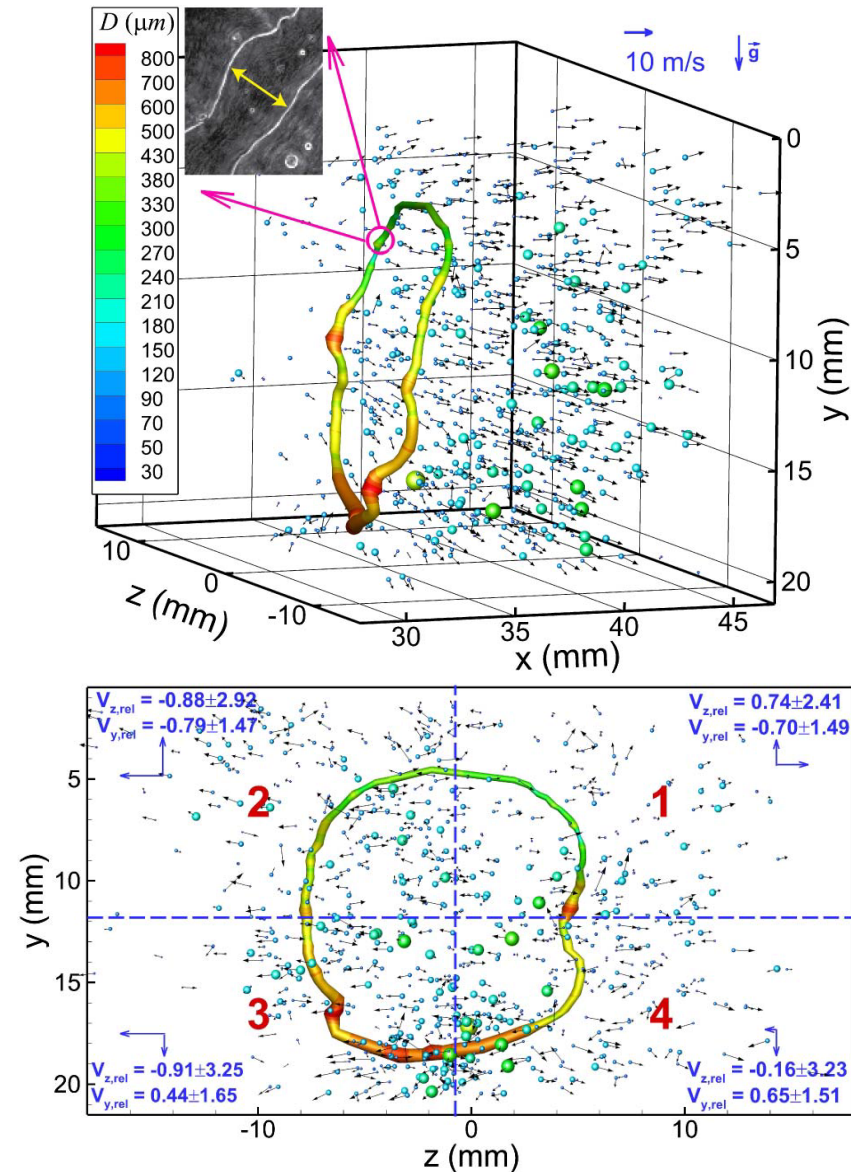
Secondary drop sizes/positions extracted by the hybrid method

- Comparison with phase Doppler anemometer (PDA) data confirms accuracy of measured sizes



Ring measured from z-location of maximum image gradient

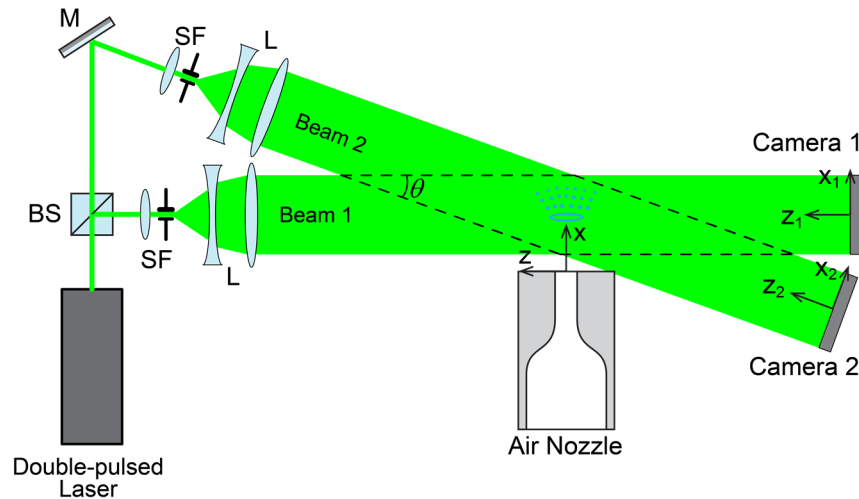
- Total volume of ring + secondary drops is within 2.2% of the initial volume



Aerodynamic drop fragmentation

Velocimetry suffers from uncertainty in the out-of-plane (z) position

- A stereo-view configuration is one solution

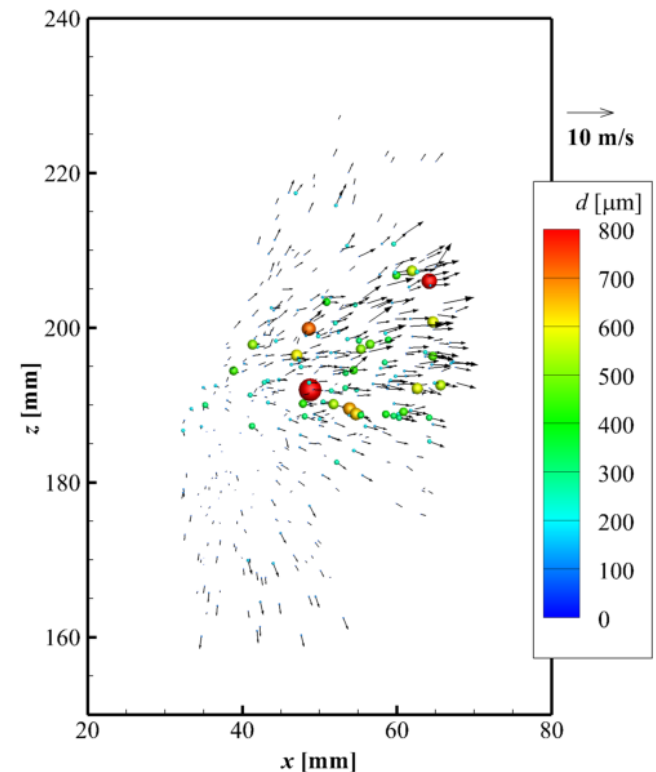
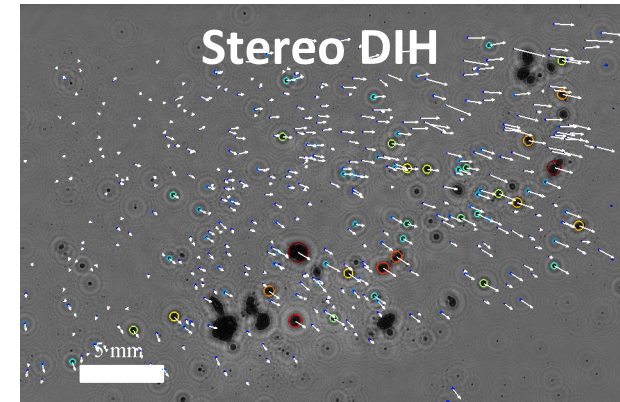


Advantages:

- Improved z -uncertainty
- Eliminates false particle size and position measurements

Challenges:

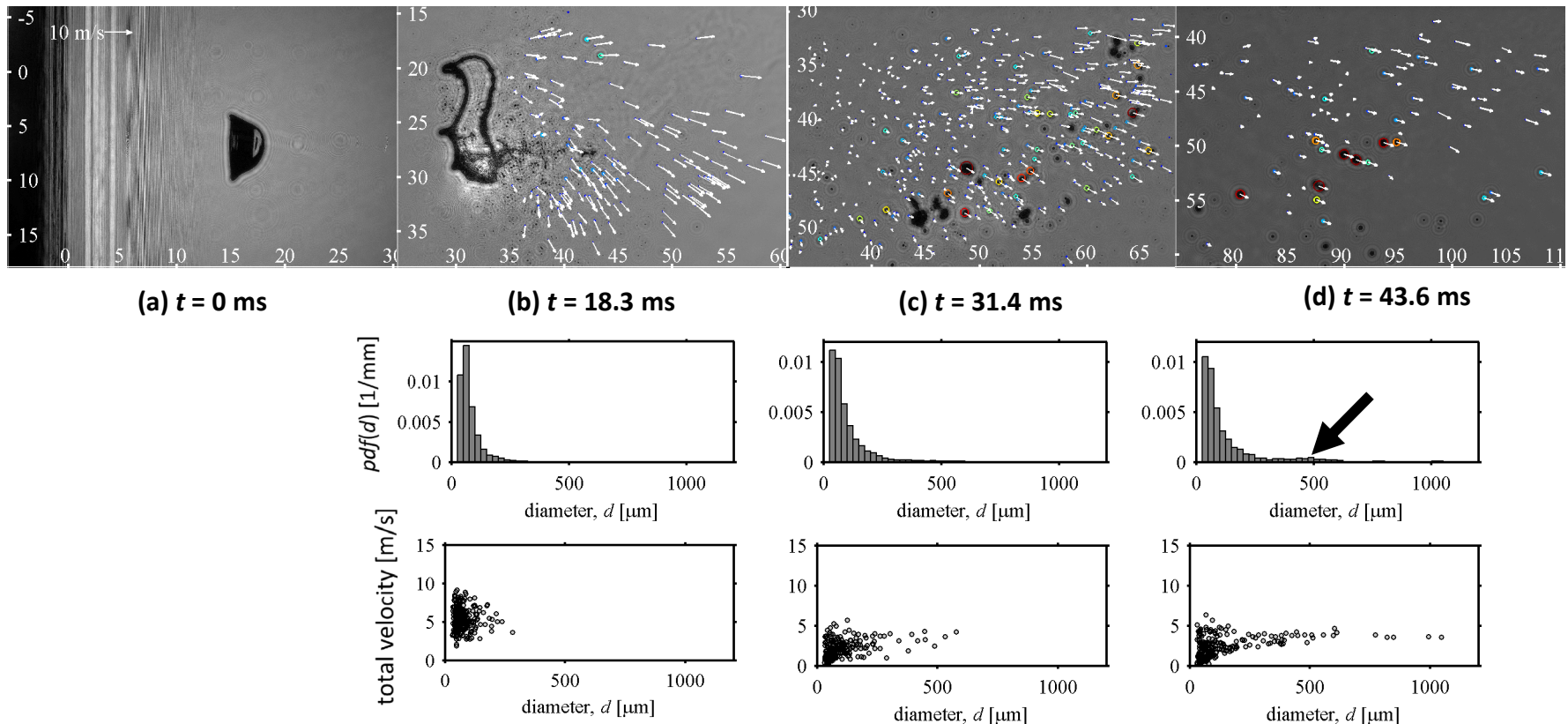
- Increased experimental complexity
- Careful calibration required



Aerodynamic drop fragmentation

Ensemble averaging of 44 realizations at each condition

- Roughly 10,000 individual drops measured per condition



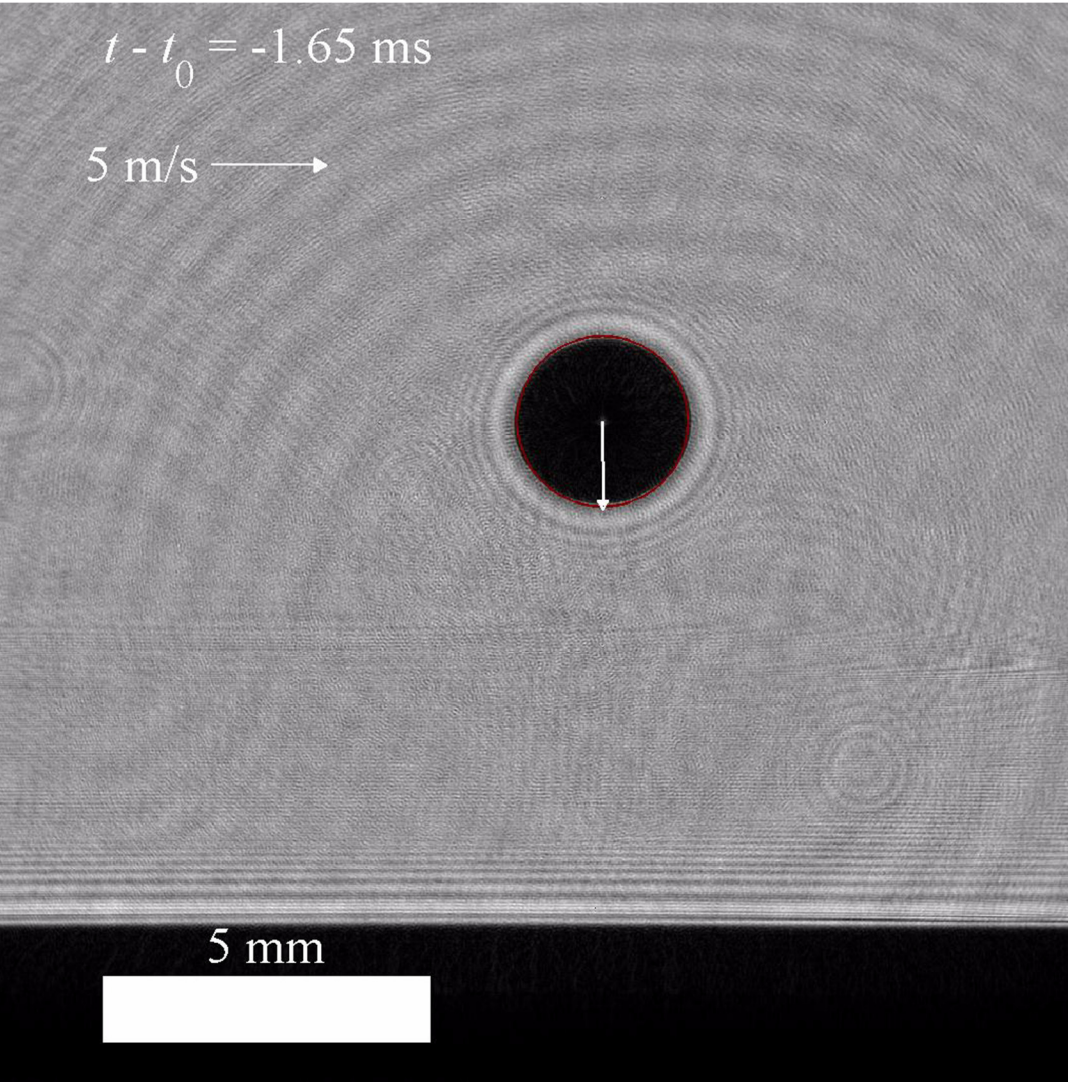
DIH is particularly advantageous for rapid quantification of particle statistics

New concepts and opportunities

High-speed (kHz) DIH

$t - t_0 = -1.65 \text{ ms}$

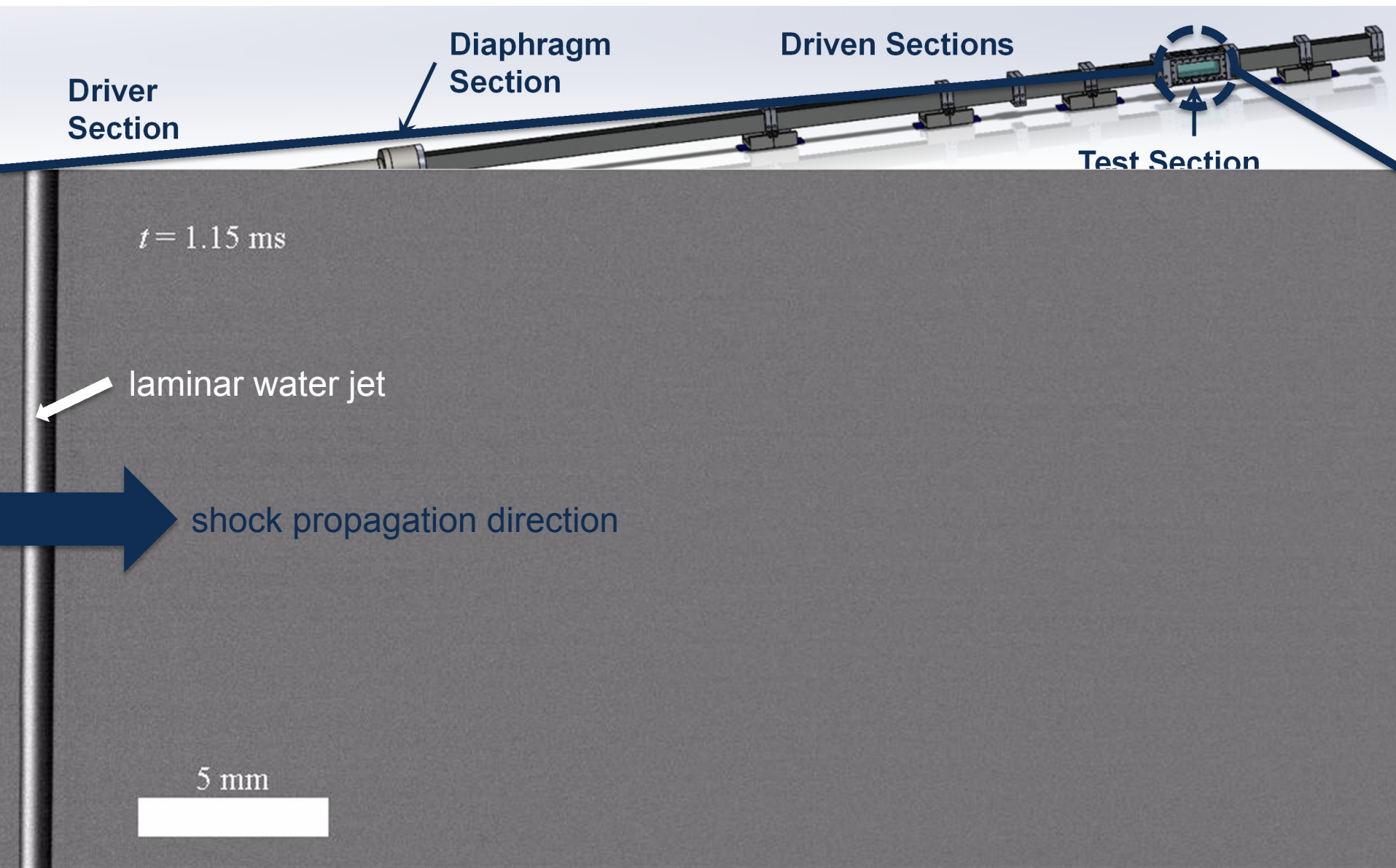
5 m/s \longrightarrow



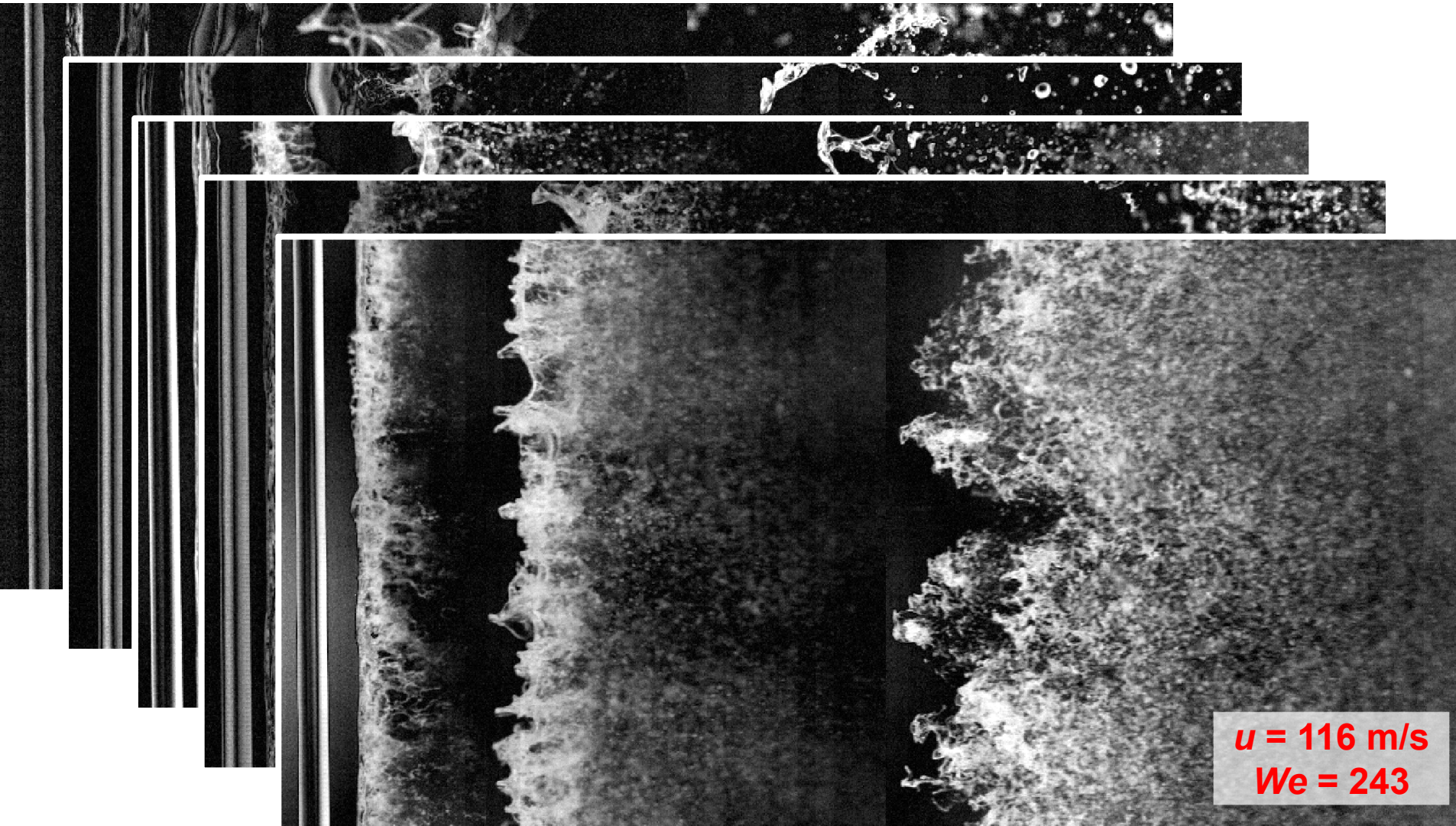
5 mm

Regression based Multi-frame Tracking (RMT) allows for 3D-3C temporal measurements (Guildenbecher *et al.*, 2016, *Appl. Opt.*)

Breakup of a water jet in a shock-tube

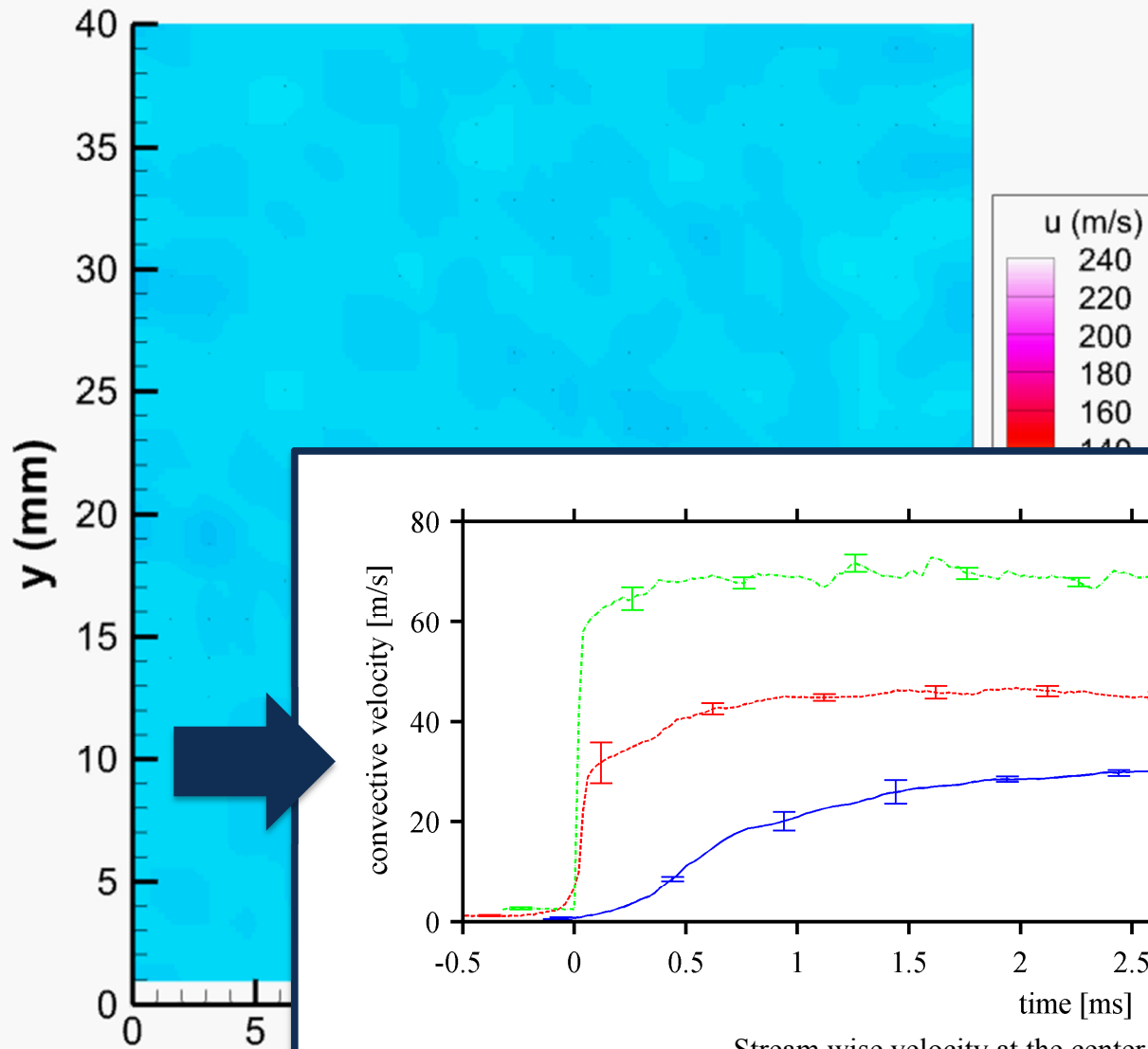


Observed breakup morphologies



Breakup morphologies similar to those observed for isolated drops

Well characterized boundary conditions



Pulse-burst PIV provides detailed characterization of the empty shock tube at 50 kHz

- Wagner et al. AIAA-2016-0791.

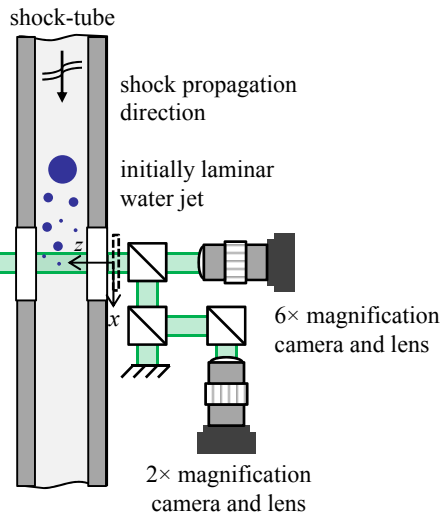
DIH recorded at 100,000 fps

recorded hologram at $t = 1.16$ ms

1 mm

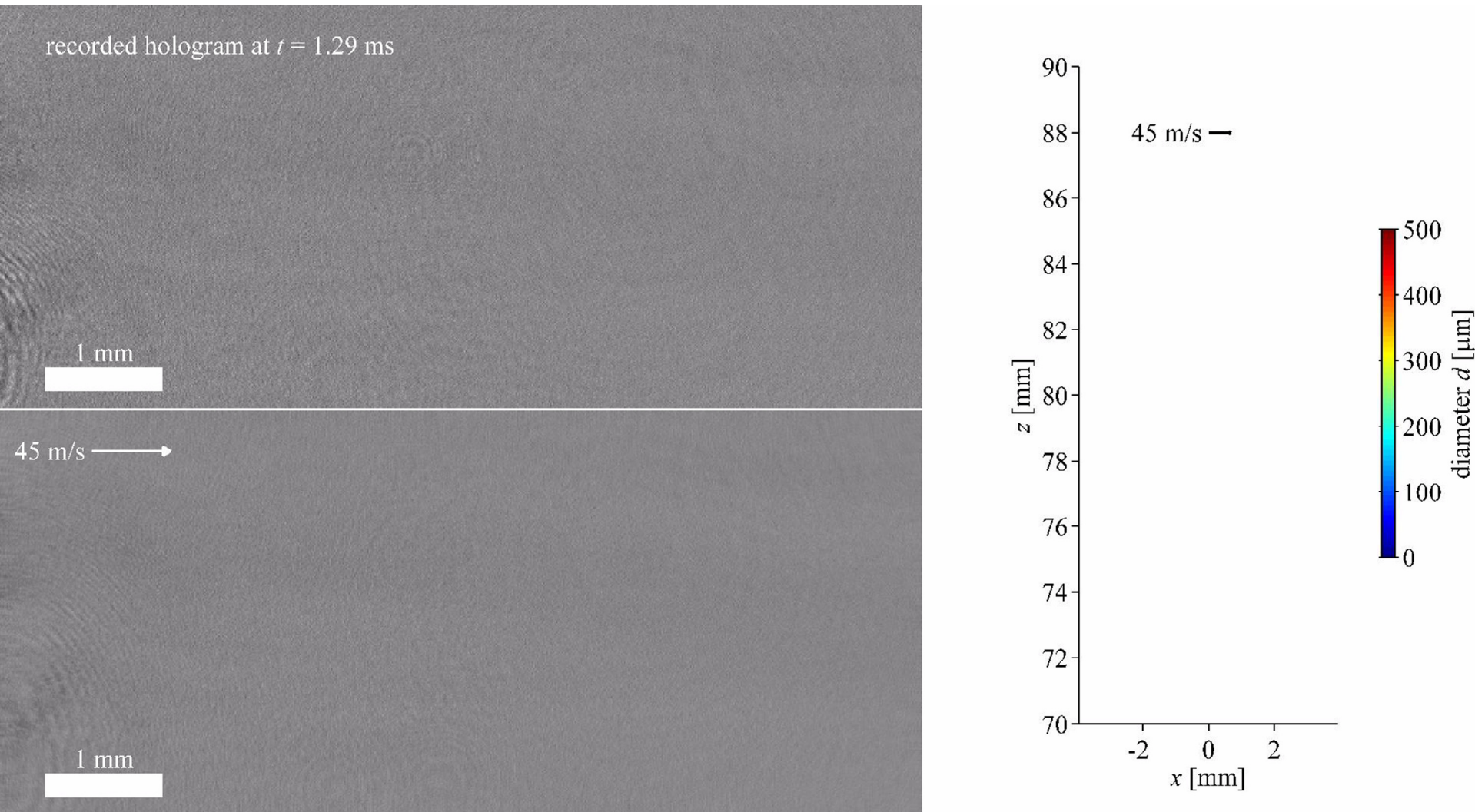
refocused to $z = 80$ mm

1 mm

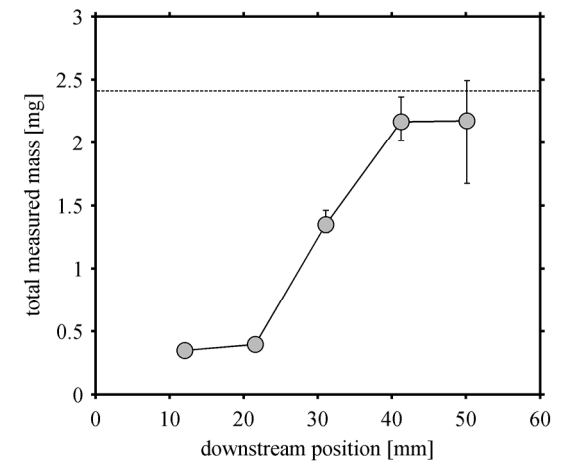
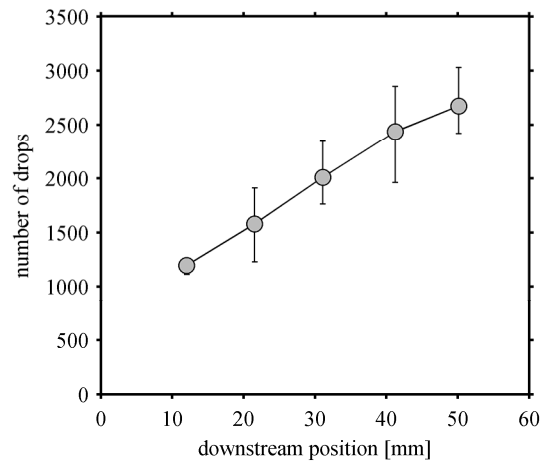
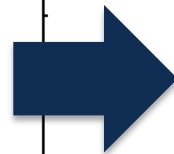
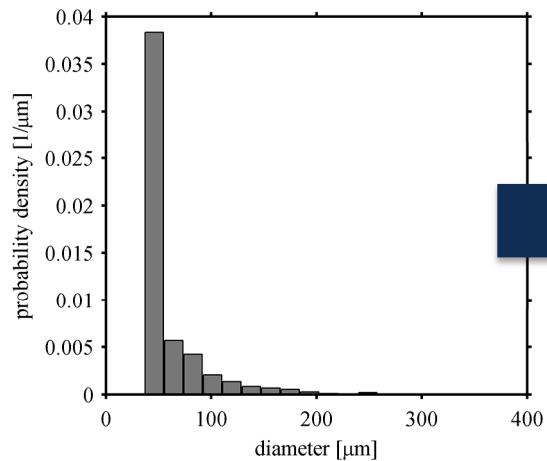
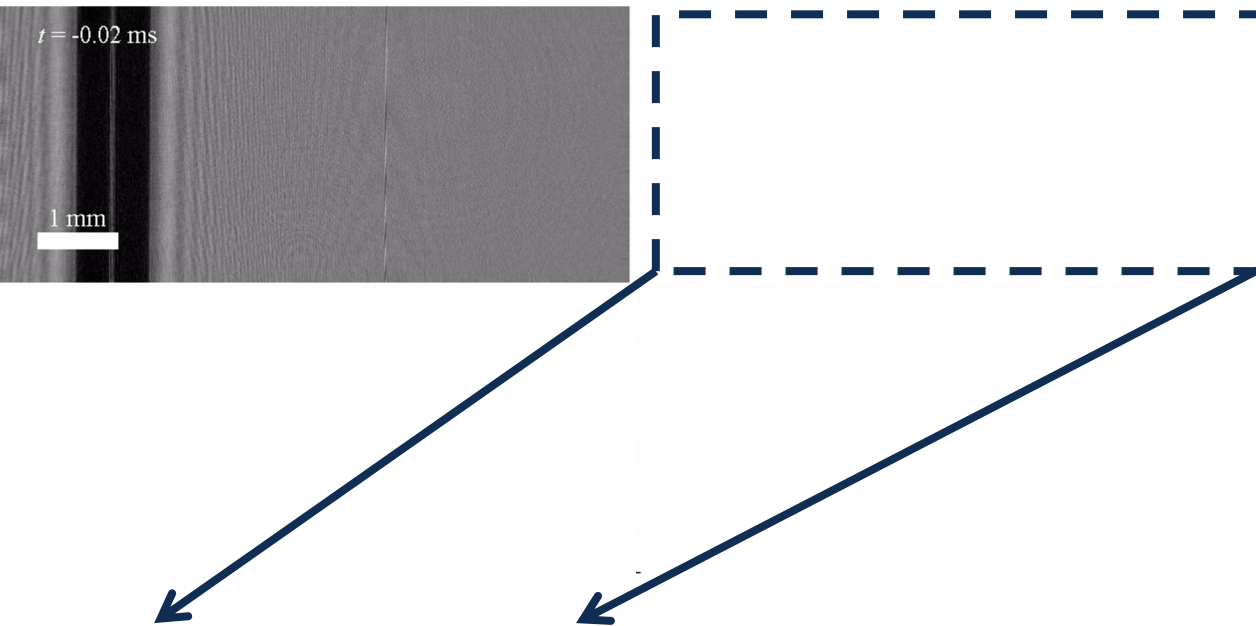


Temporally resolved, 3D particle field

Data processing similar to drop impact experiment



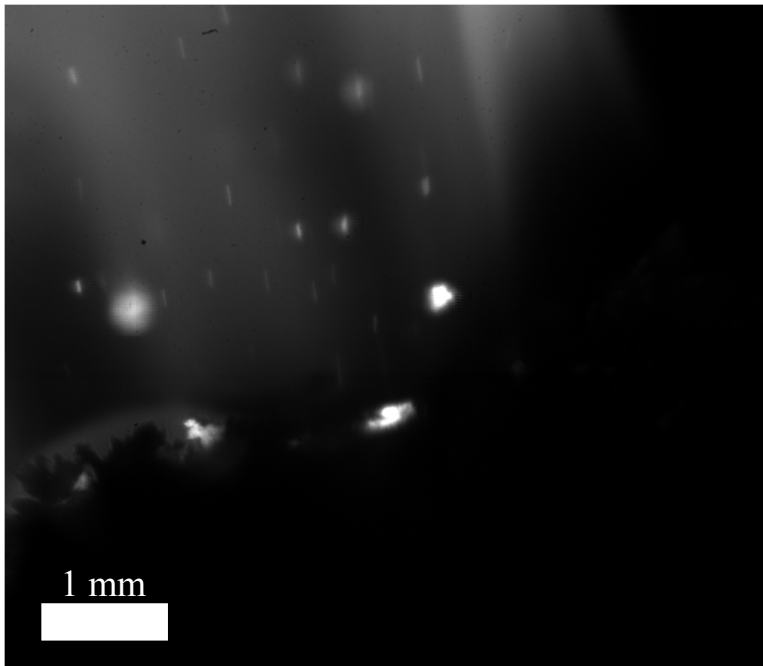
Multiple downstream fields of view



Aluminum drop combustion in propellants

Motivation: rocket failures can lead to propellant fires

- Sandia Laboratories is interested in predicting the response of objects in this environment



high-speed video of a burning propellant

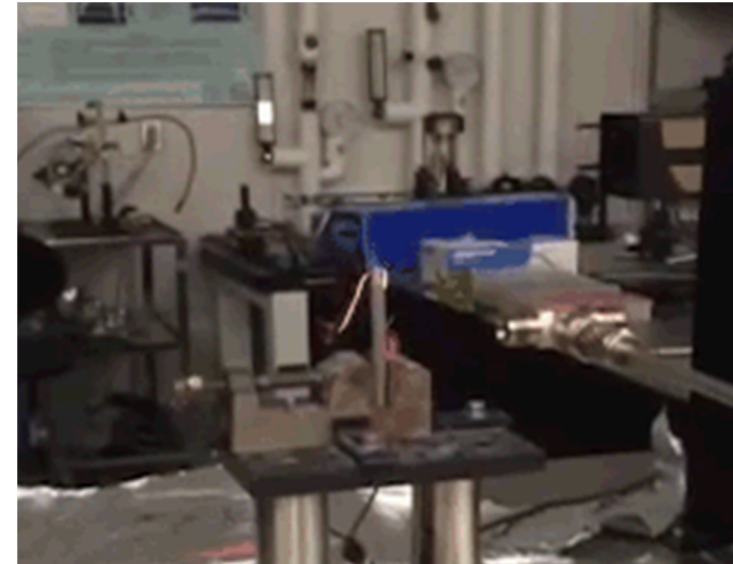
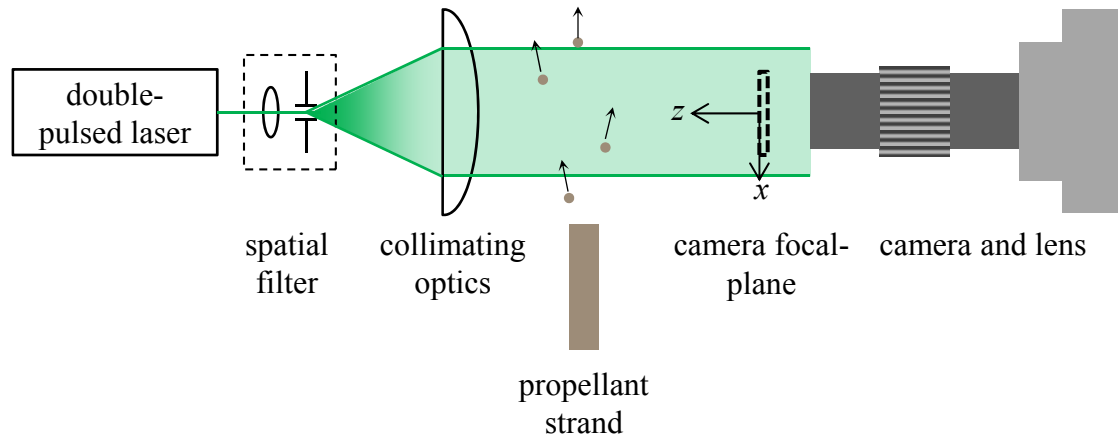


<http://www.cbsnews.com/news/rocket-crash-no-immediate-threat-to-station-but-cause-is-unknown/>

Aluminum agglomeration at the surface yields large reacting drops with high damage potential

- Prediction requires knowledge of particle *size, velocity, and temperature*

Aluminum drop combustion in propellants



propellant in the text fixture

Propellant: solid-rocket propellant pressed into a pencil size strand

- Combusts from the top surface down, ejecting molten aluminum particles traveling a few m/s

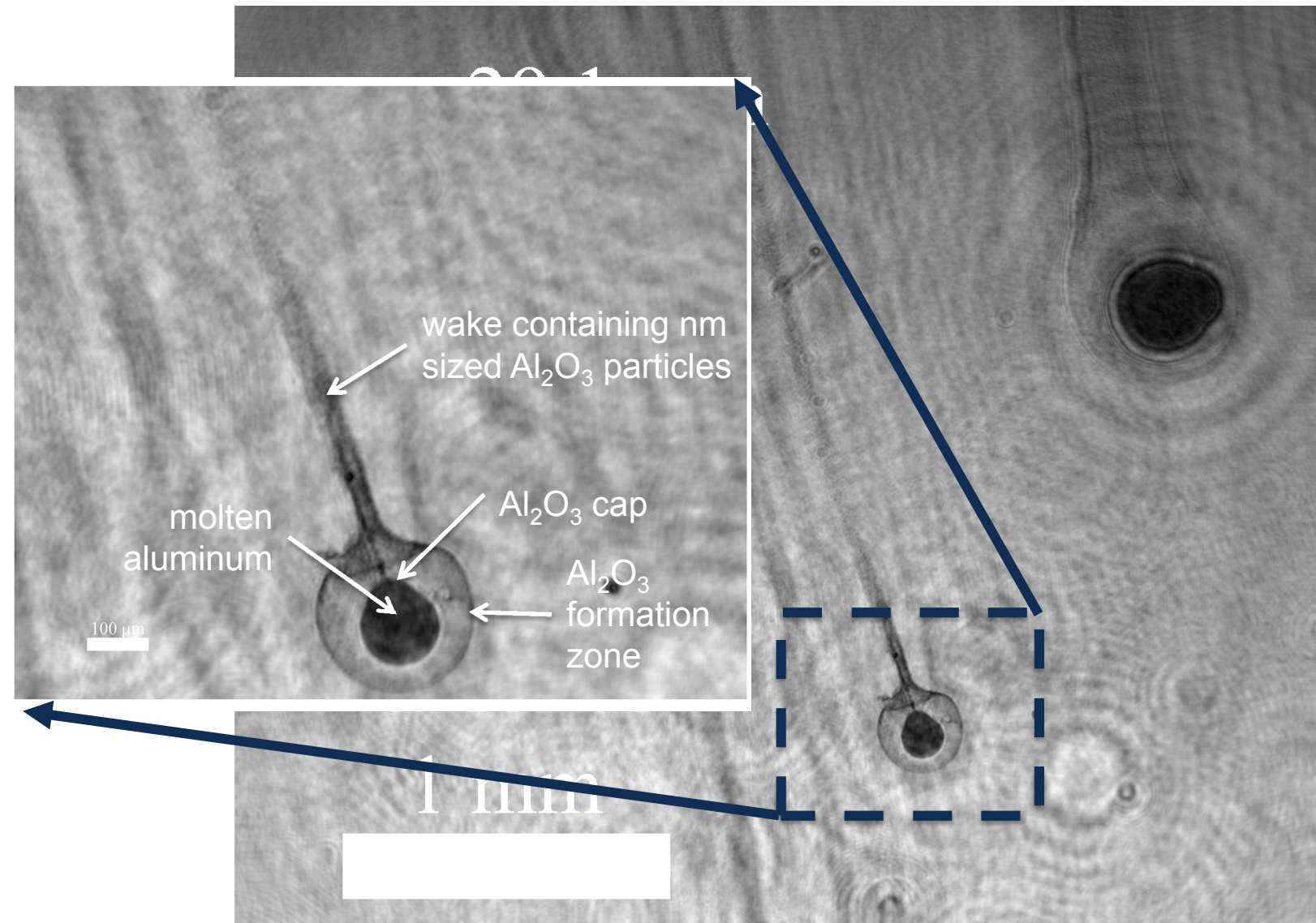
Laser: Continuum Minilite Nd:YAG, 532 nm wavelength, 5 ns pulse duration

Camera: sCMOS from LaVision at 15Hz

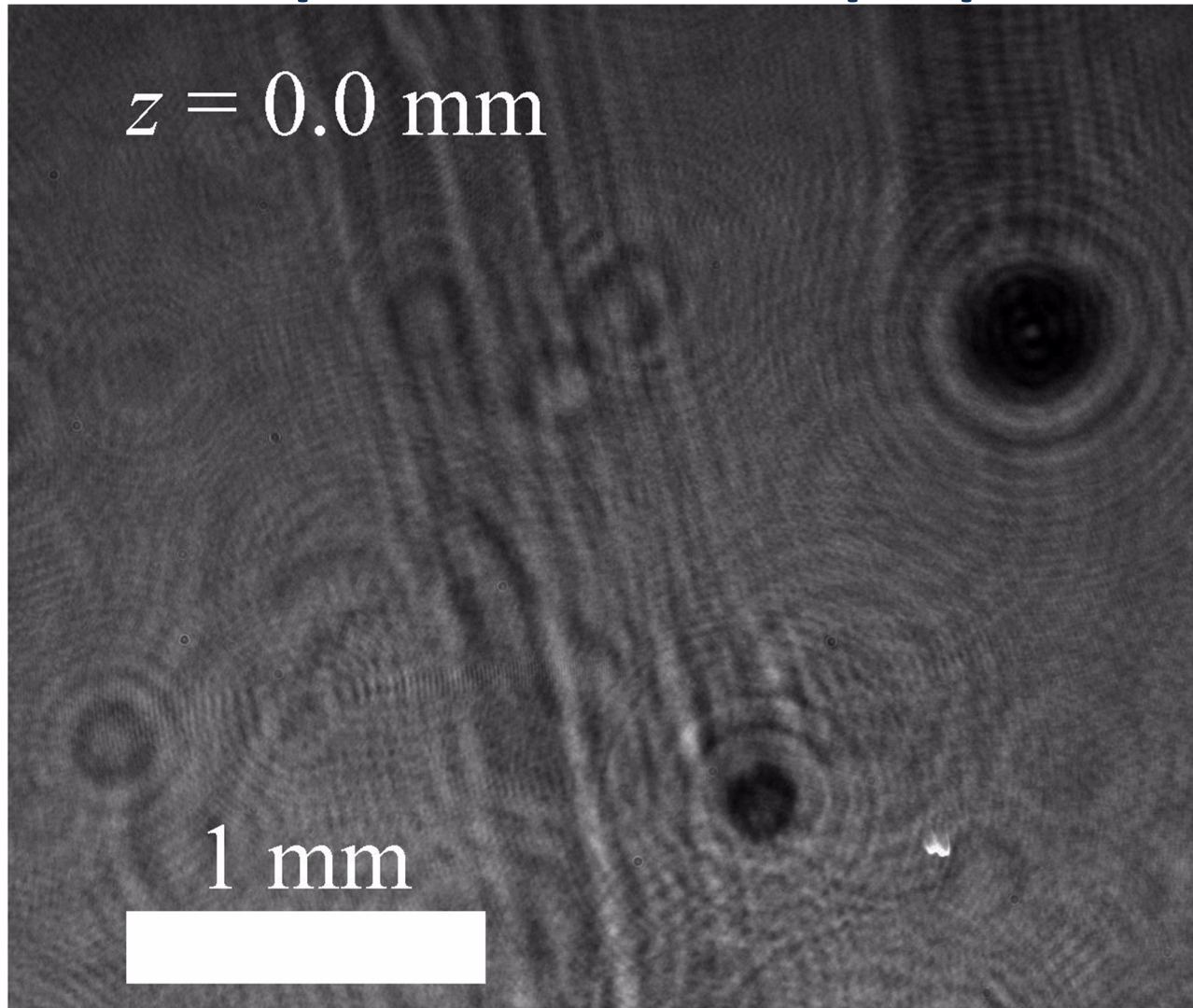
Lens: Infinity K2 long distance microscope with CF-4 objective

- ~ 6X magnification

Aluminum drop combustion in propellants



Aluminum drop combustion in propellants



Algorithms automatically measure unique features of burning aluminum

Aluminum drop combustion in propellants

Three strand burns → 5594 images
and 17496 measured drops

- Main peak due to agglomerated particulates
- Peak at 50 μm due to non-agglomerated particulate

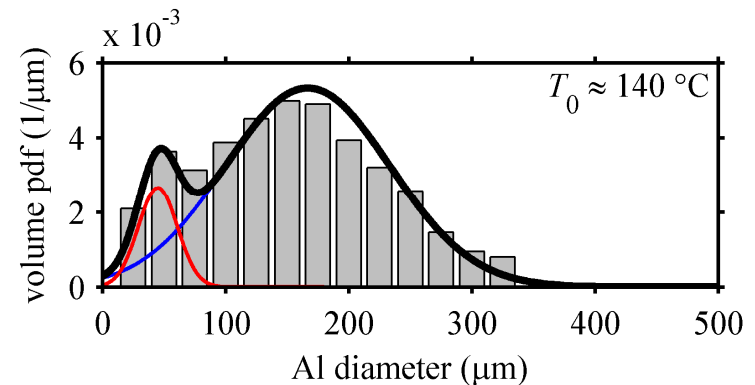
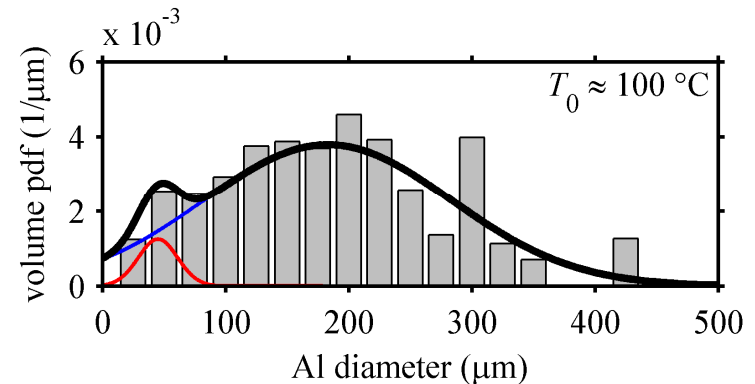
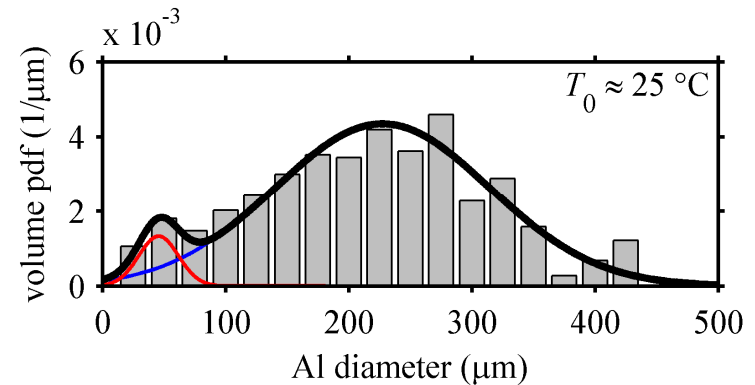
Experiments repeated at higher initial temperature (faster burn rate)

- Main peak is reduced due to decreased residence time for agglomeration

- Peak at 50 μm remains

Trend is consistent at still higher initial temperatures

- Main peak reduced further
- Peak at 50 μm remains



Recorded at
20,000 fps

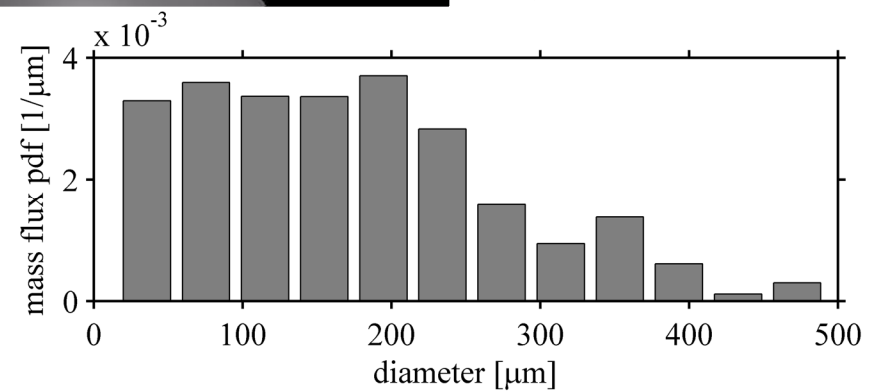
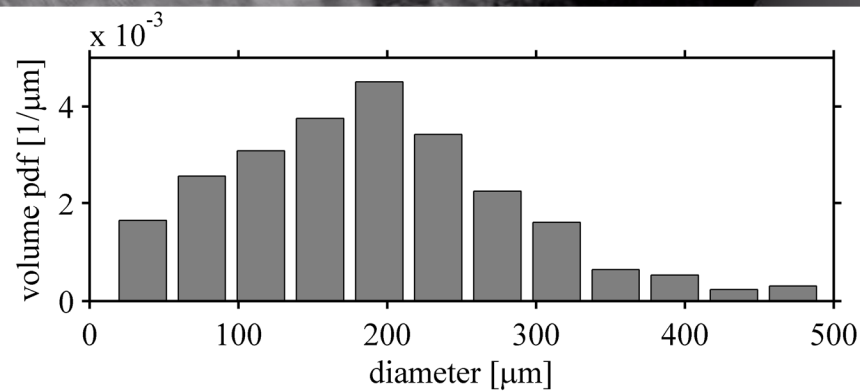
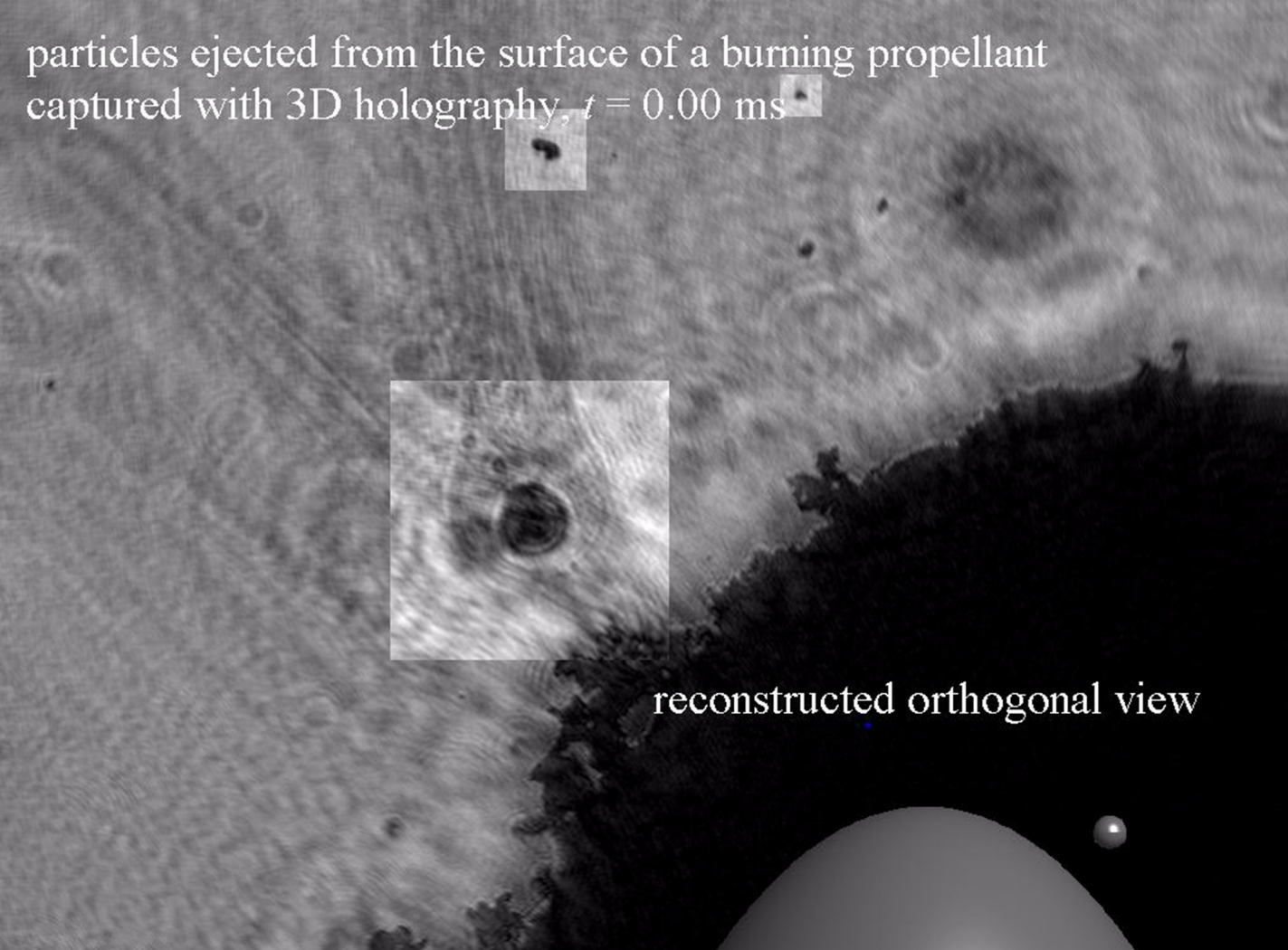
Camera: Photron SA-
Z

Laser: Coherent
Verdi V6

43,684 frames →

- 15,991 drops
- mass flux =
0.24 mg/s·mm²

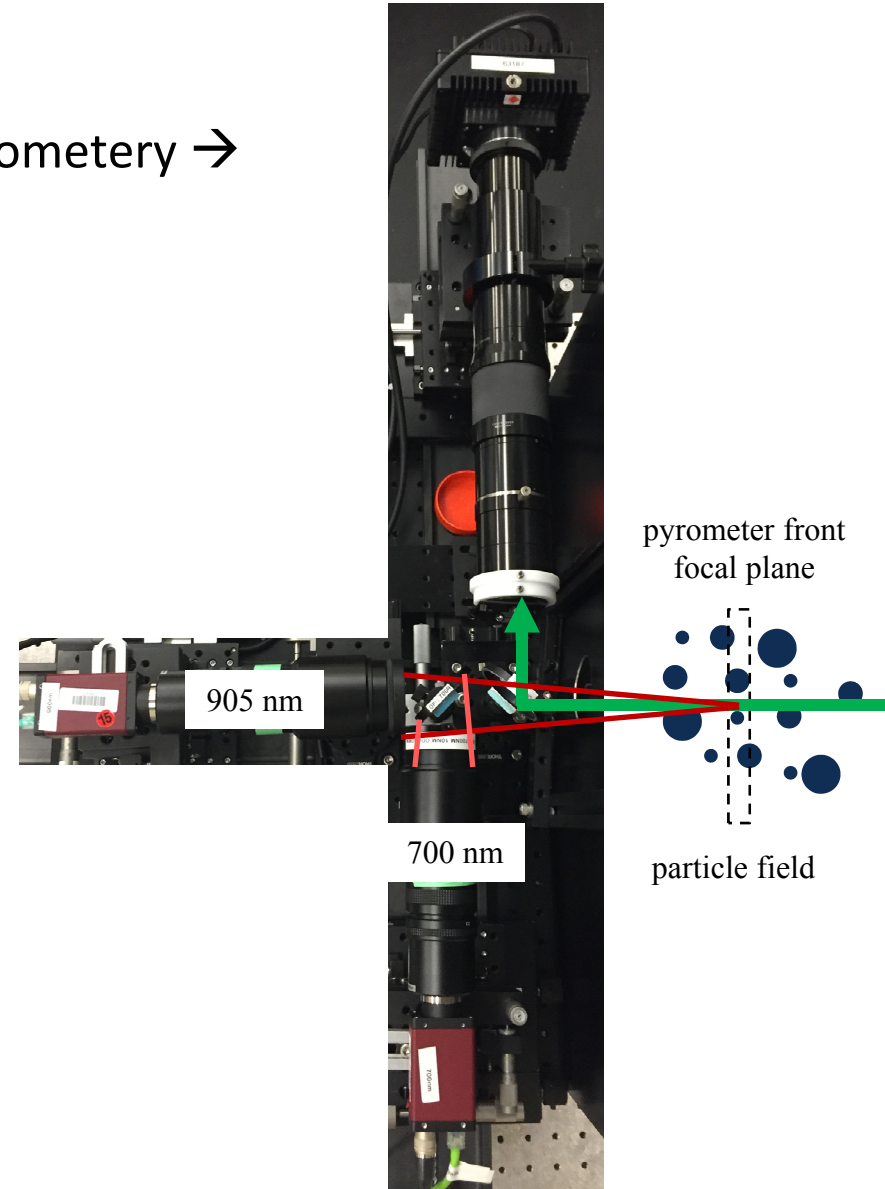
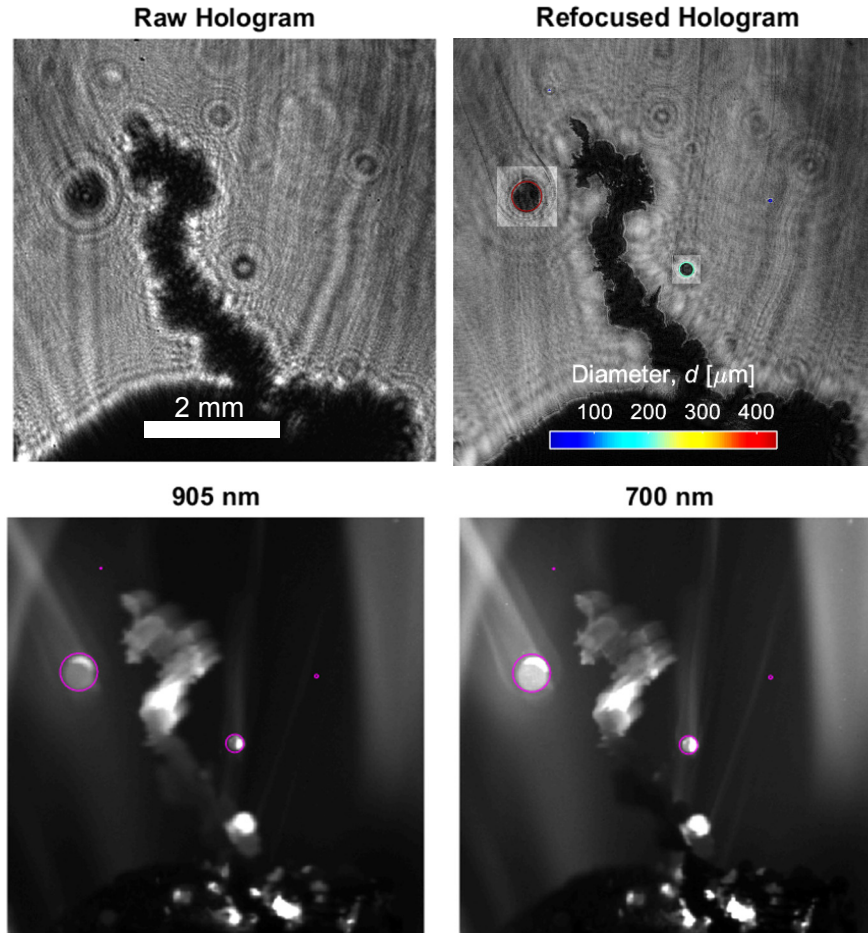
From burn rate and
known composition,
expected mass flux is



Particle temperature measurements

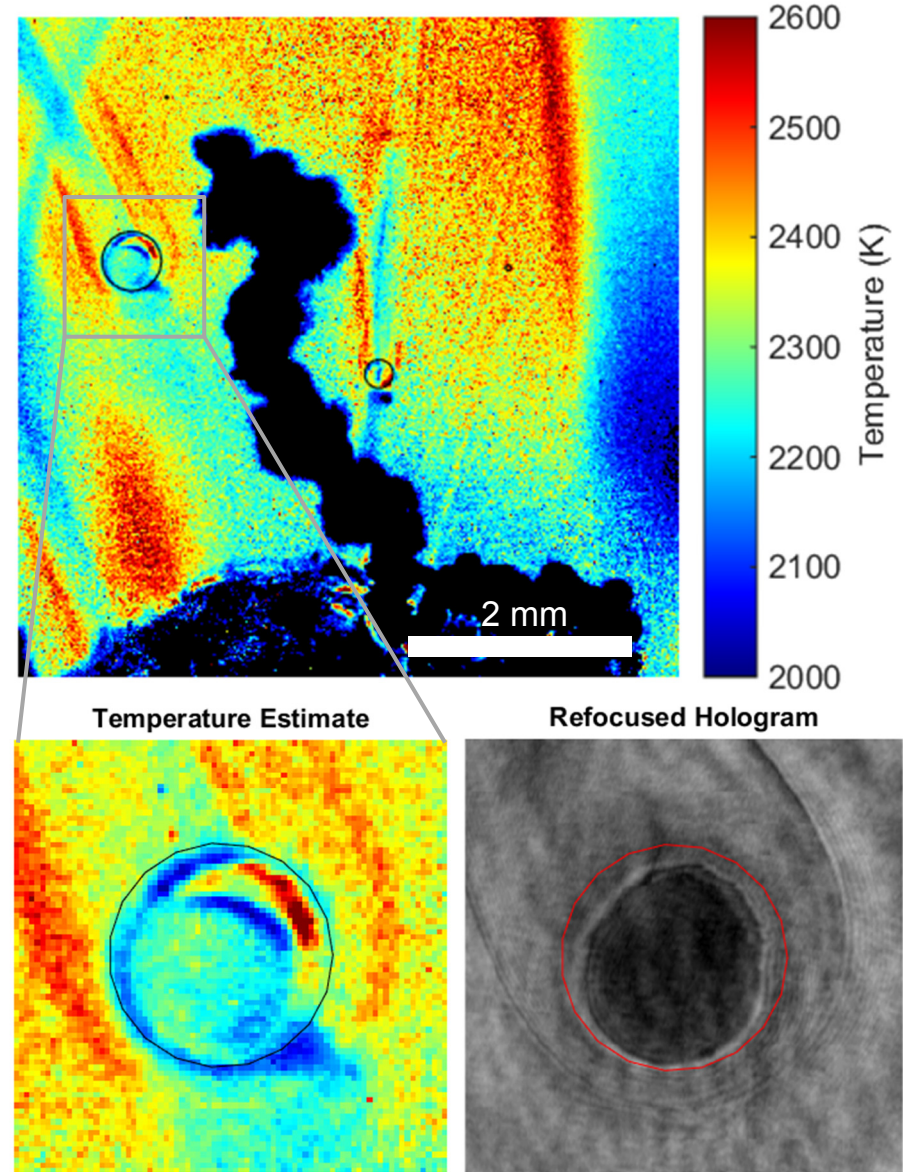
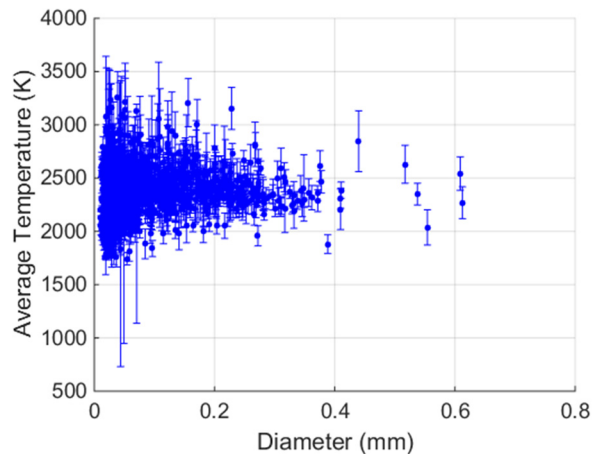
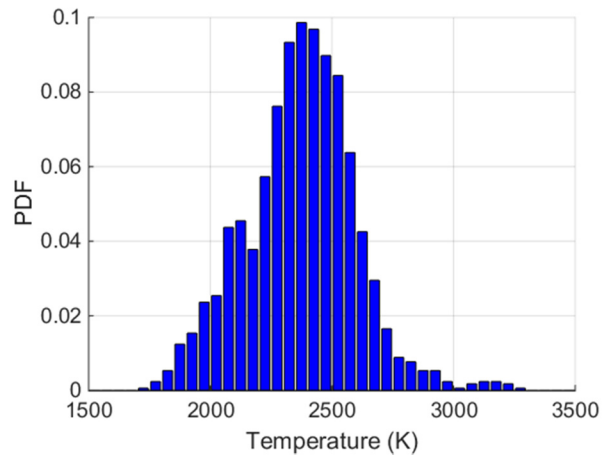
We also need to quantify heat transfer

- Combination of DIH and two-color pyrometry → particle size + velocity + *temperature*



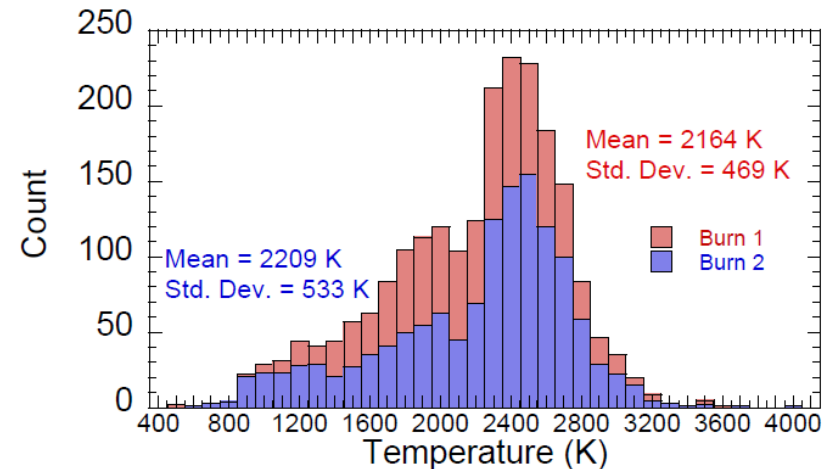
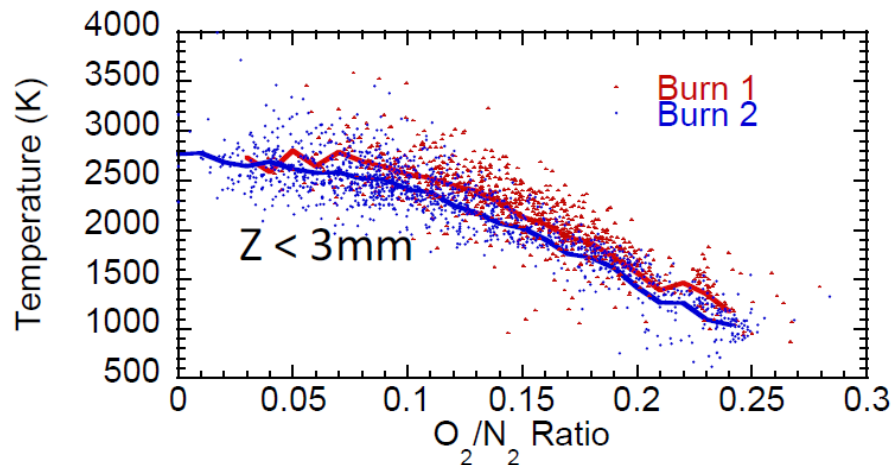
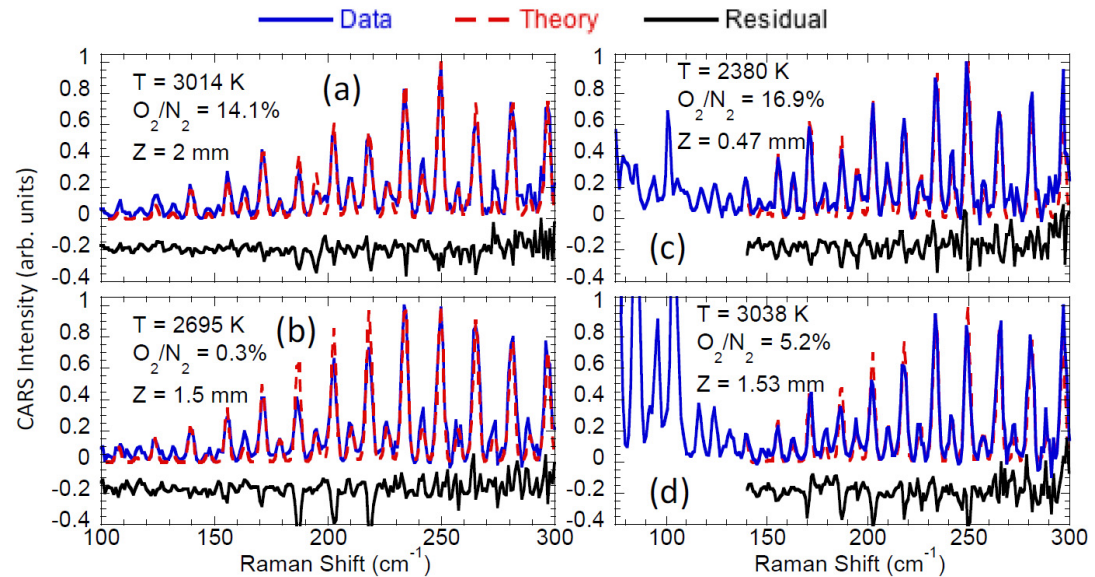
Particle temperature measurements

Assuming graybody emission, calibrated ratio imaging gives an estimate of particle temperatures



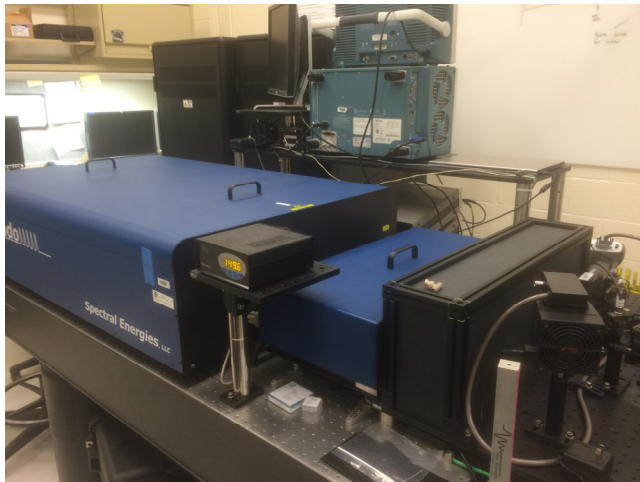
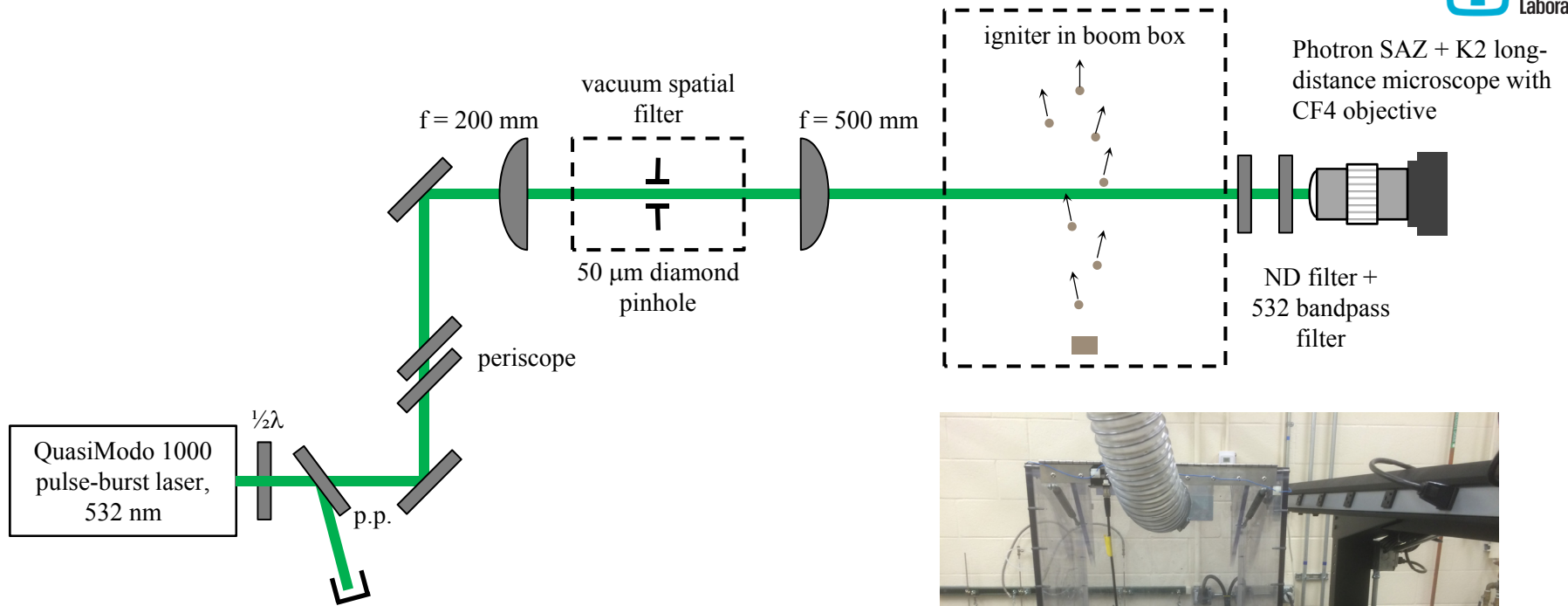
Gas-phase temperatures with CARS

S. Kearney is measuring gas-phase temperatures using fs/ps CARS

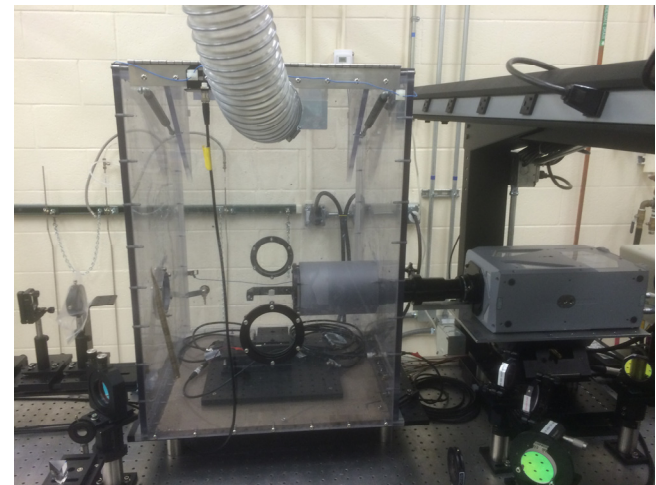


Kearney and Guildenbecher, 2016, *Appl. Opt.*

Pulse-burst DIH

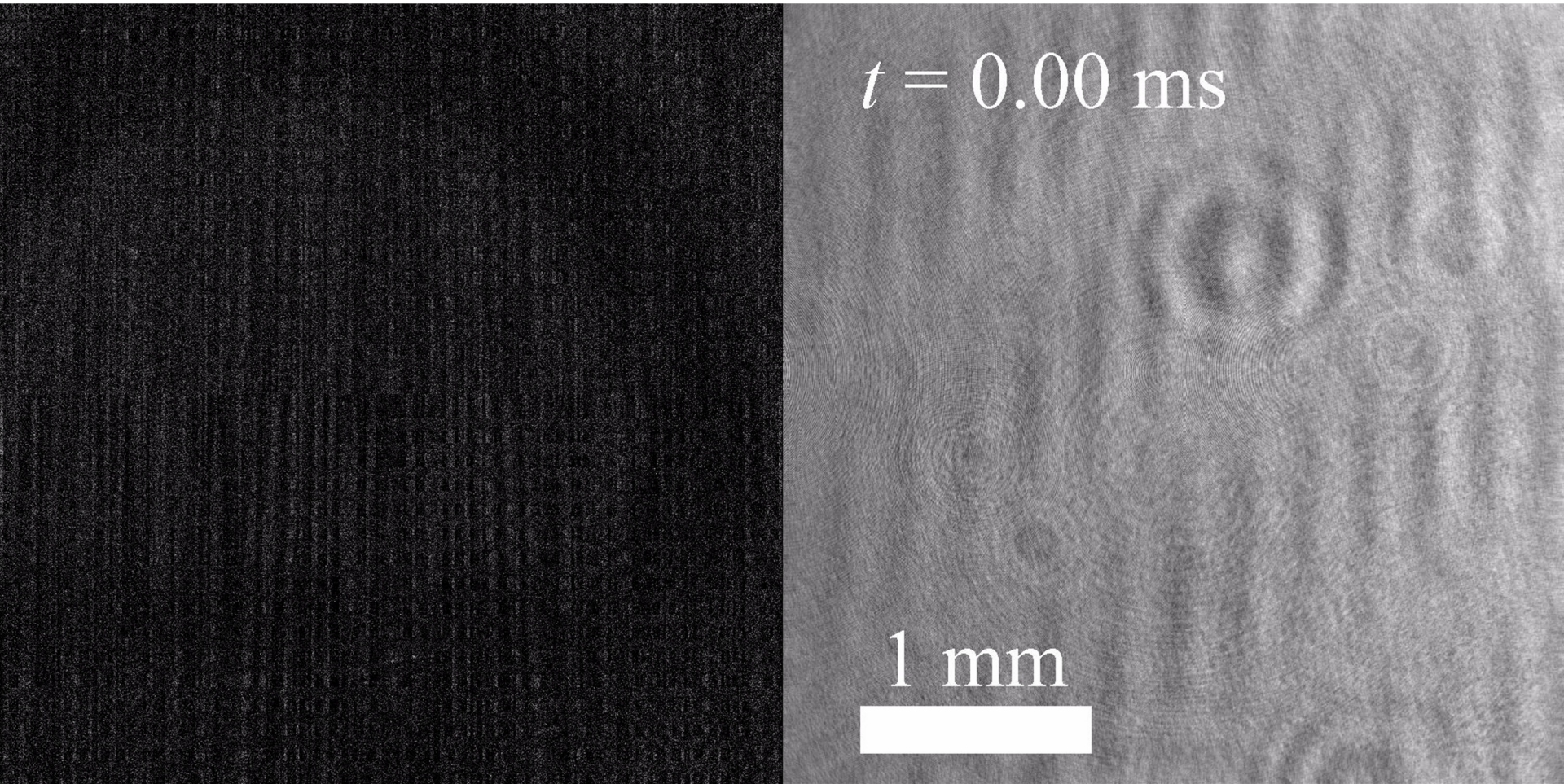


Spectral Energies pulse-burst laser



boom-box and high-speed DIH imager

Pulse-burst DIH

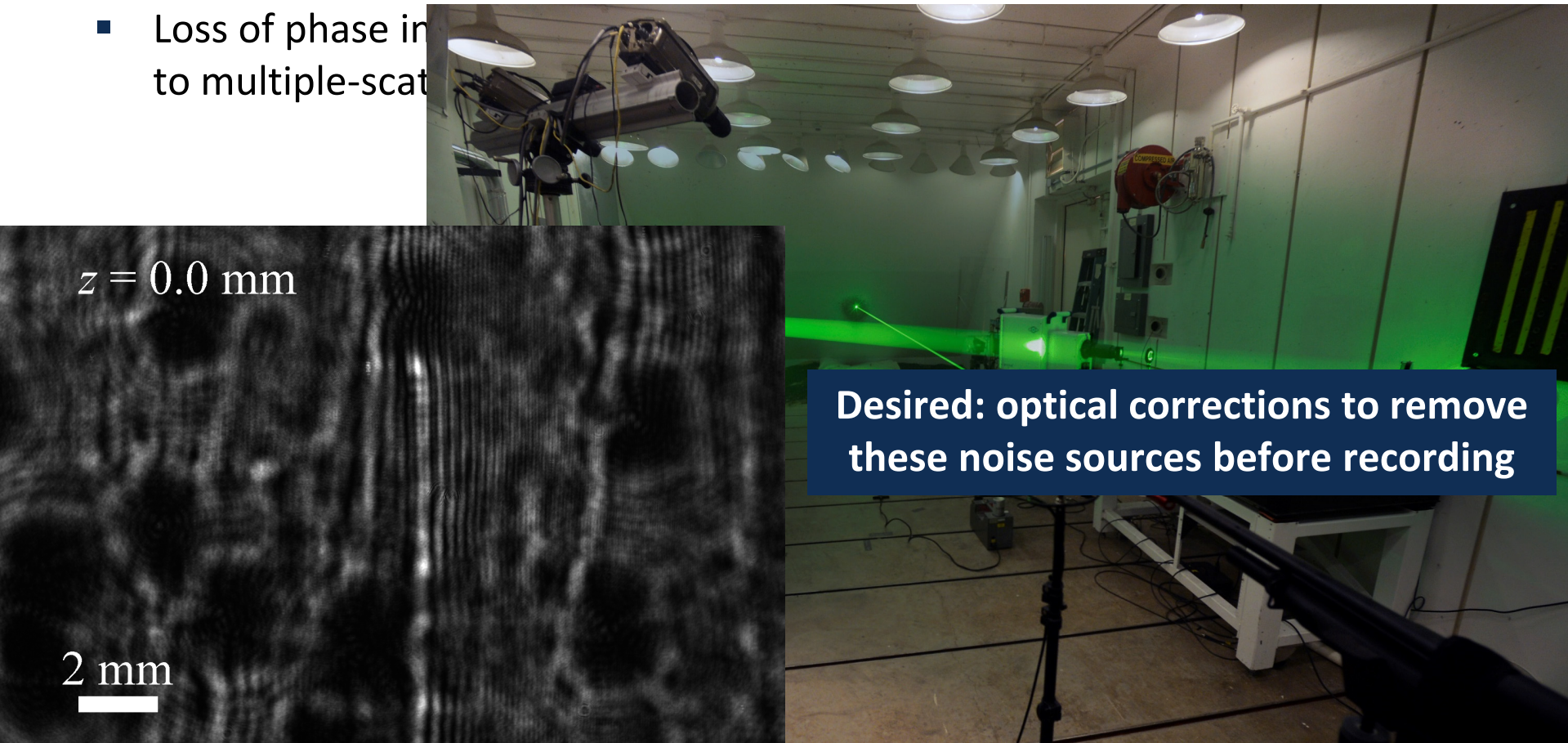


- Beam quality is sufficient for DIH
- Freezes high-speed particles and penetrates through flash and smoke
- Noise due to soot and index-of-refraction gradients

Optical challenges in DIH

Coherent imaging is susceptible to:

- Image distortion through index of refraction gradients
- Loss of phase information due to multiple-scattering

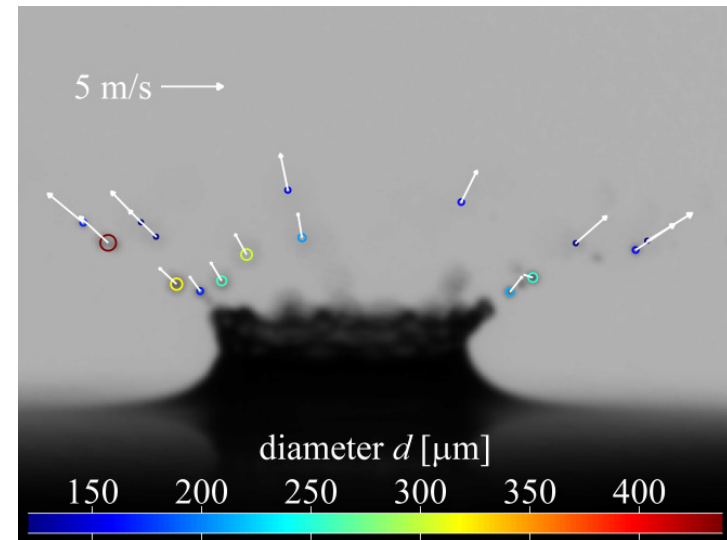
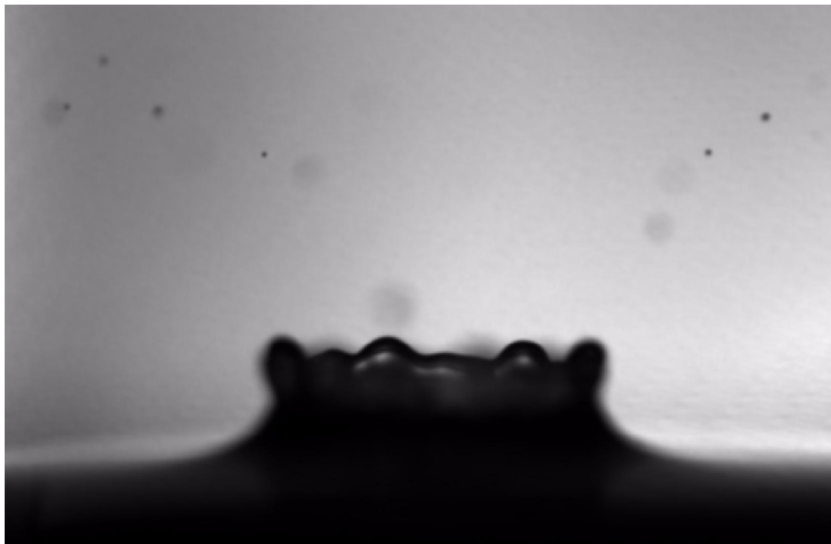
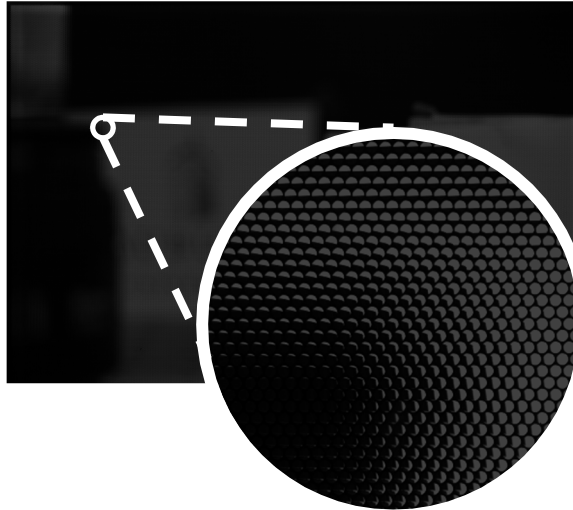


Reconstructed amplitude throughout depth, z

Holography configuration for shotgun investigations

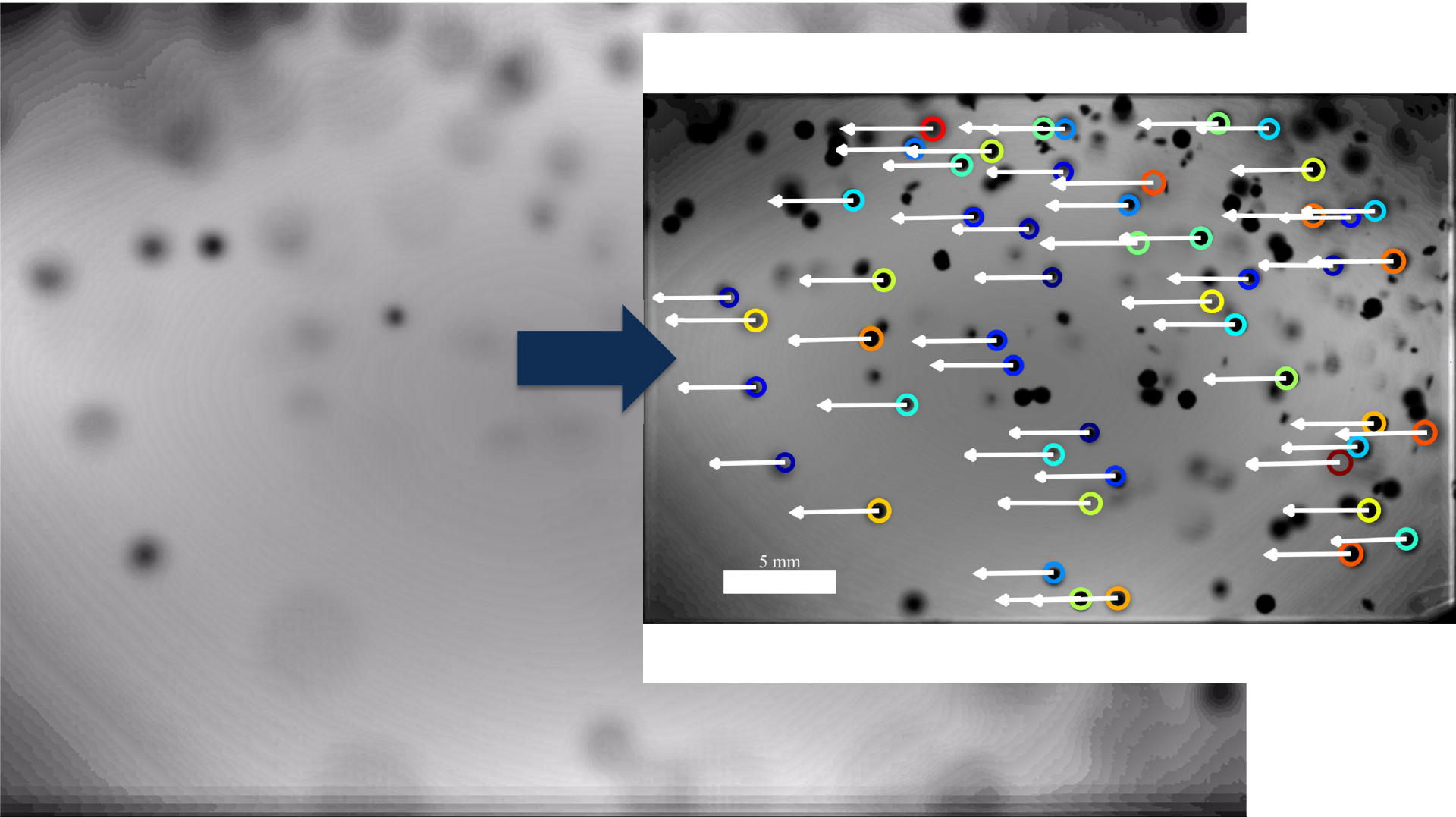
Alternative 3D measurements

Plenoptic cameras use micro-lens arrays and white light to create a 3D image



Alternative 3D measurements

Plenoptic imaging of a shotgun

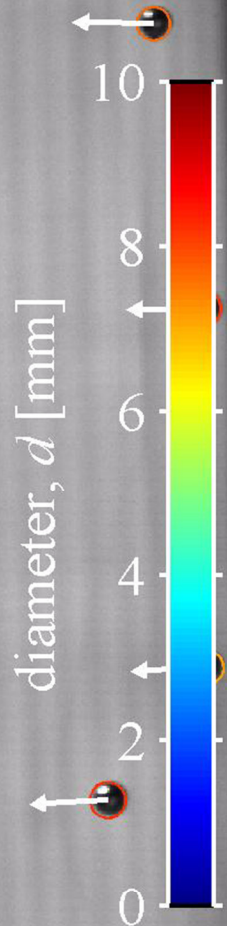


Particle tracking methods are versatile...

$t = 3.00 \text{ ms}$

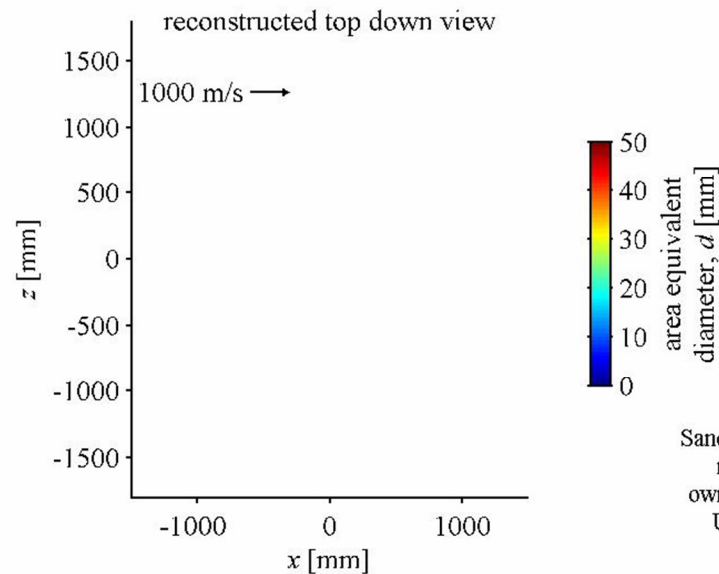
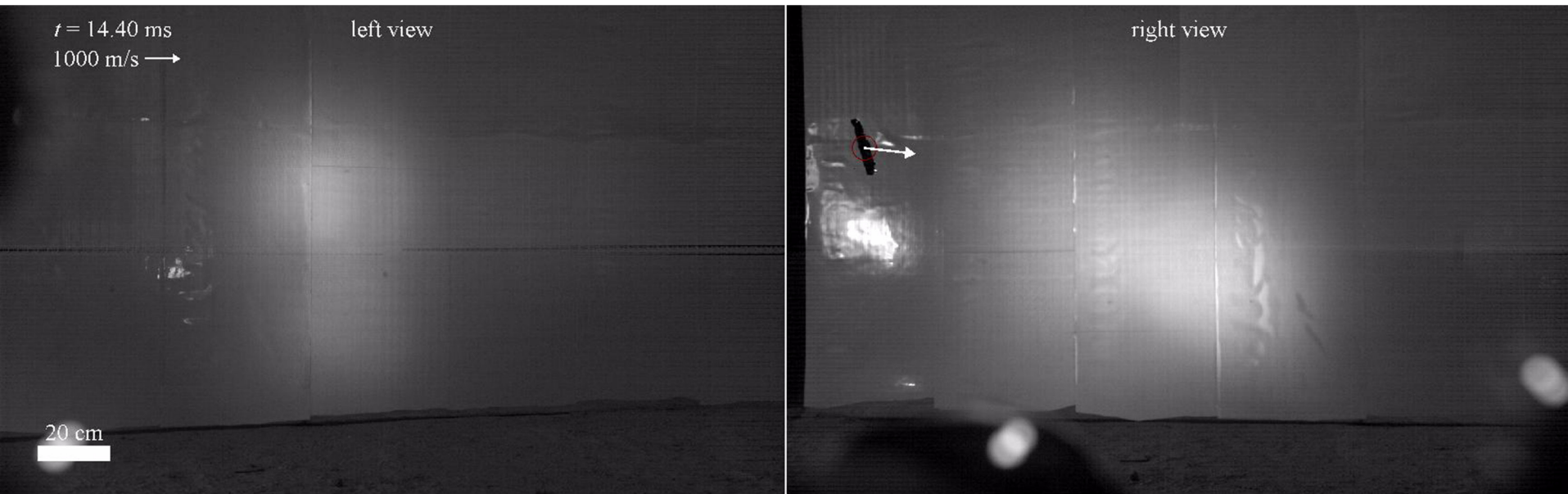
350 m/s \rightarrow

5 cm



Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.

... including large-scale munitions testing



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DIH has many advantages:

- 3D-3C measurement
- Rapid quantification of statistics
- Simple optical configuration

... and opportunities for research:

- Depth-of-focus problem
- Data processing
- Optical improvements

Acknowledgements:

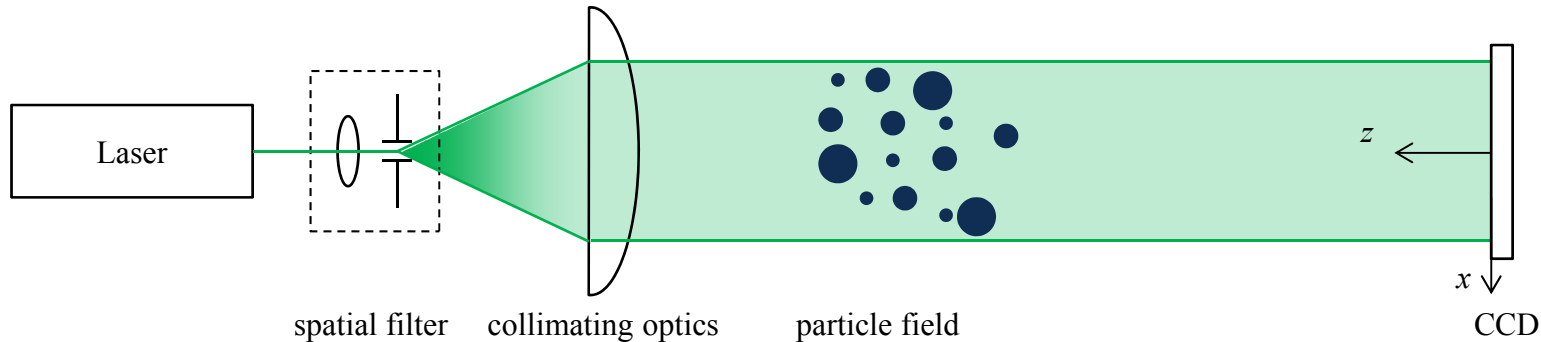
This work was supported by the Laboratory Directed Research and Development and the Weapons Systems Engineering Assessment Technology program at Sandia National Laboratories (SNL)

Many thanks to all of my excellent collaborators: *Jian Gao* (Johns Hopkins University), *Phillip L. Reu* (SNL), *Jun Chen* (Purdue University), *Sean P. Kearney* (SNL), *Kathryn G. Hoffmeister* (SNL), *Paul E. Sojka* (Purdue University), *Thomas W. Grasser* (SNL), *H. Lee Stauffacher* (SNL), *Marcia A. Cooper* (SNL), *Luke Engvall* (University of Colorado), *Justin L. Wager* (SNL), *Thomas A. Reichardt* (SNL), *Paul A. Farias* (SNL), *Joseph D. Olles* (SNL), *Ellen Y. Chen* (SNL), *Brian S. Thurow* (Auburn University), *Elise D. Munz* (Auburn University), *Timothy J. Miller* (SNL), and many others....

Questions

Backup slides

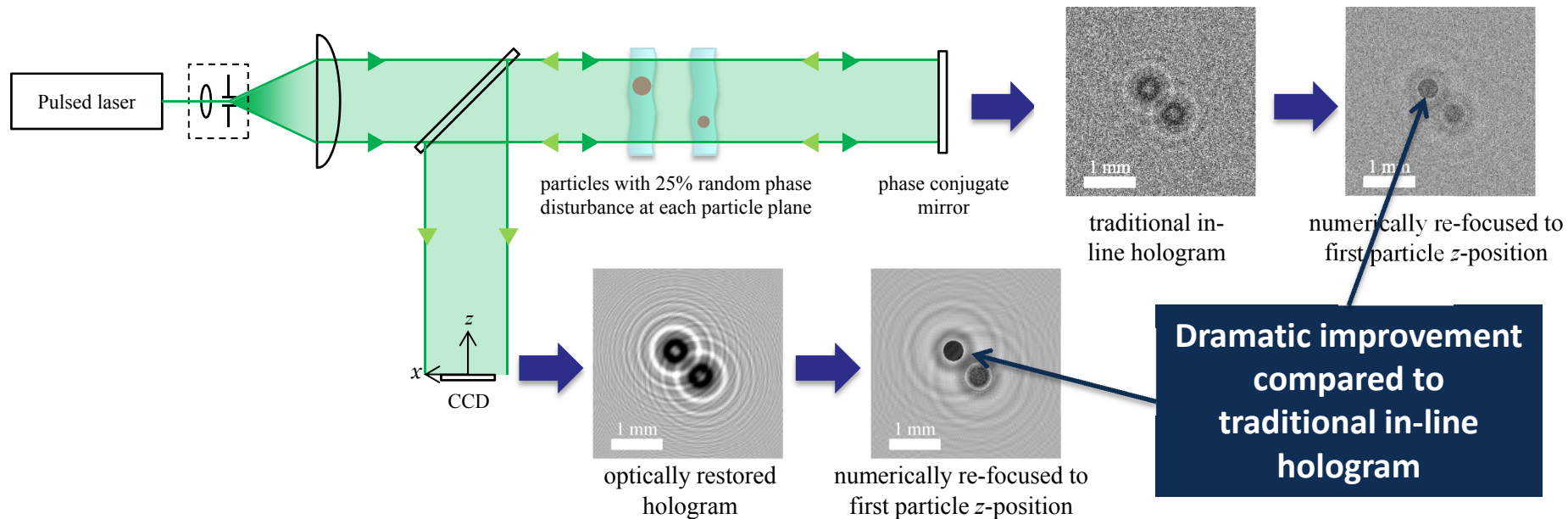
Where is the reference wave?



Hologram is the combination of object and reference waves: $h = |E_o + E_r|^2$

- Reconstruction with E_r gives: $h \cdot E_r = \underbrace{(|E_o|^2 + |E_r|^2)E_r}_{\text{DC term}} + \underbrace{|E_r|^2 E_o}_{\text{virtual image}} + \underbrace{E_r^2 E_o^*}_{\text{real image}}$
 - In off-axis holography, these terms are spatially separated as we attempt to reconstruct the original object wave, E_o
 - In in-line holography, we actually want to reconstruct the combination of the reference wave and object wave, $E_o + E_r$
 - Rearranging: $h \cdot E_r = \underbrace{|E_o|^2 E_r}_{\text{DC term}} + \underbrace{|E_r|^2 (E_o + E_r)}_{\text{virtual image}} + \underbrace{E_r^2 E_o^*}_{\text{real image}}$

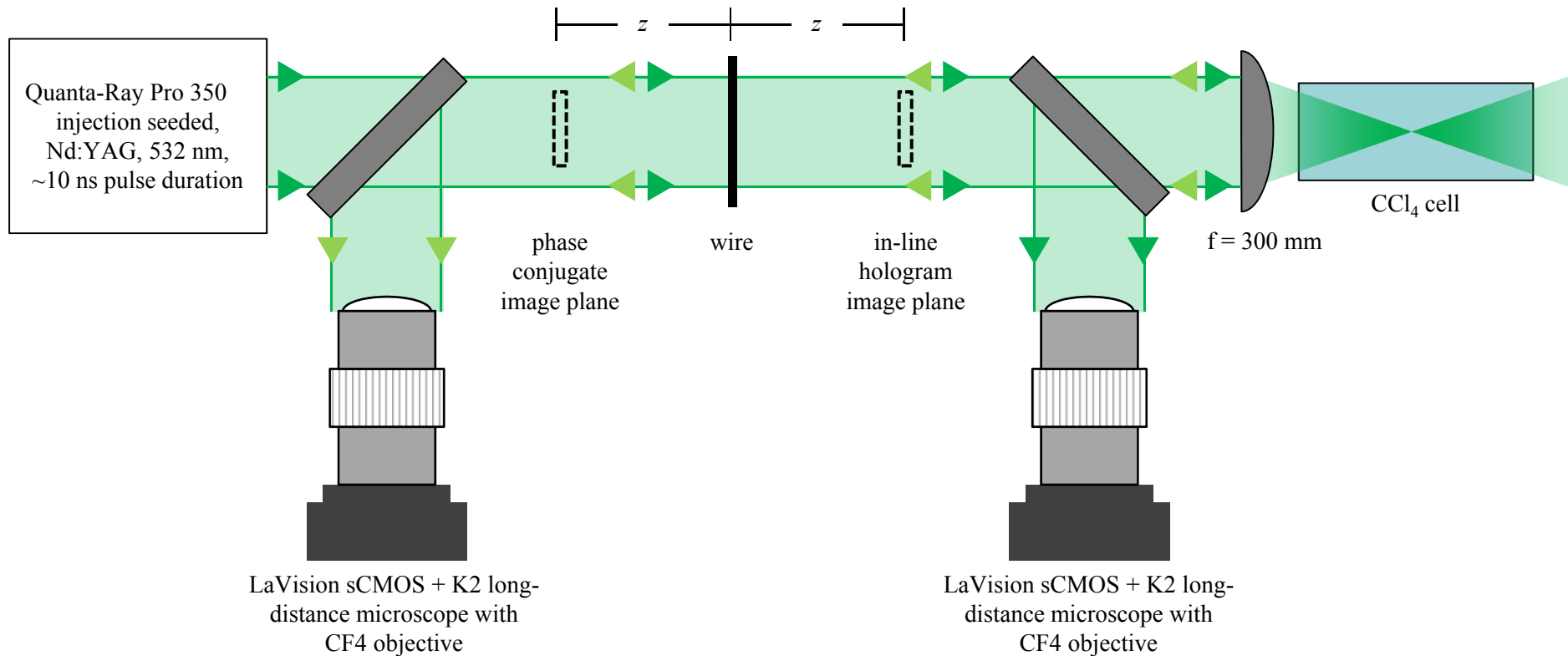
Phase-conjugate DIH theory



- Phase-conjugate mirror reflects the incoming wave with opposite phase
 - Non-linear optical effect achieved through passive means (stimulated Brillouin scattering) or active means (degenerate four-wave mixing)
- After double passing, the phase disturbance is canceled

SBS phase-conjugate DIH

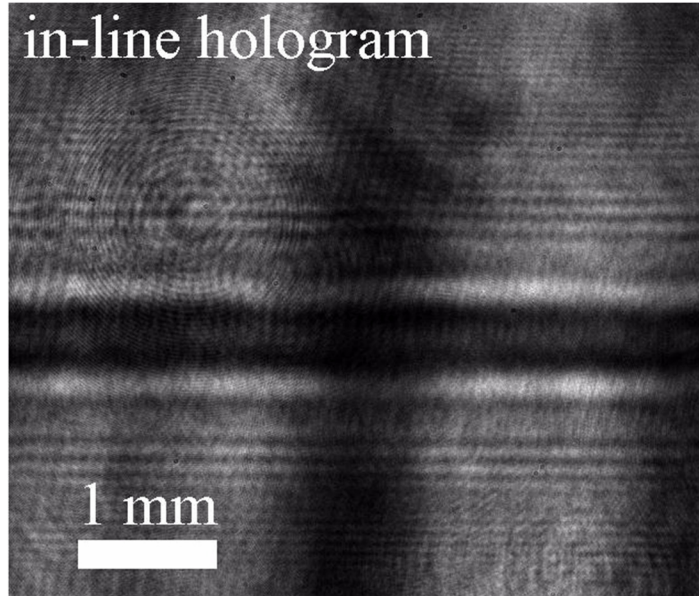
A focused beam in a non-linear medium induces phase conjugation via stimulated Brillouin scattering (SBS)



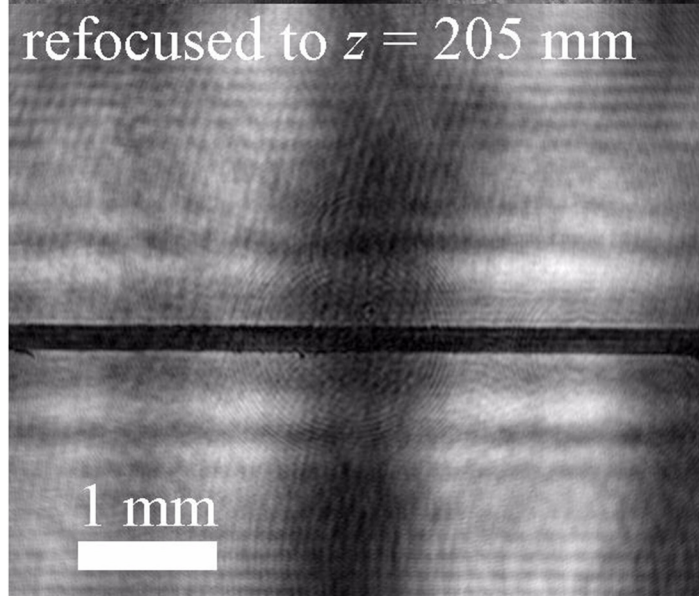
SBS phase-conjugate DIH

Without a
disturbance
both views give
similar results

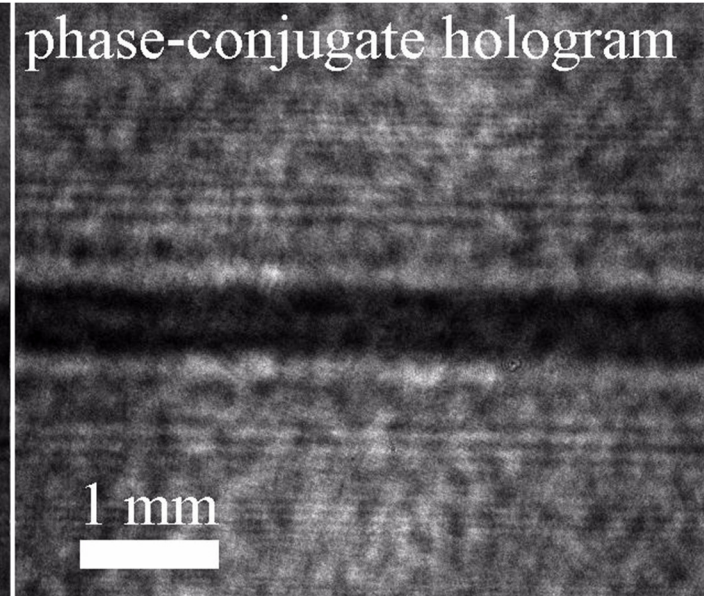
in-line hologram



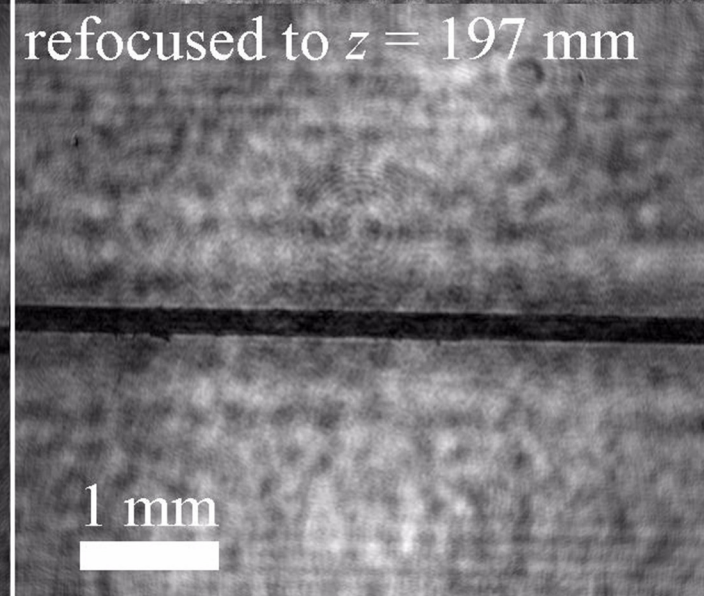
refocused to $z = 205$ mm



phase-conjugate hologram



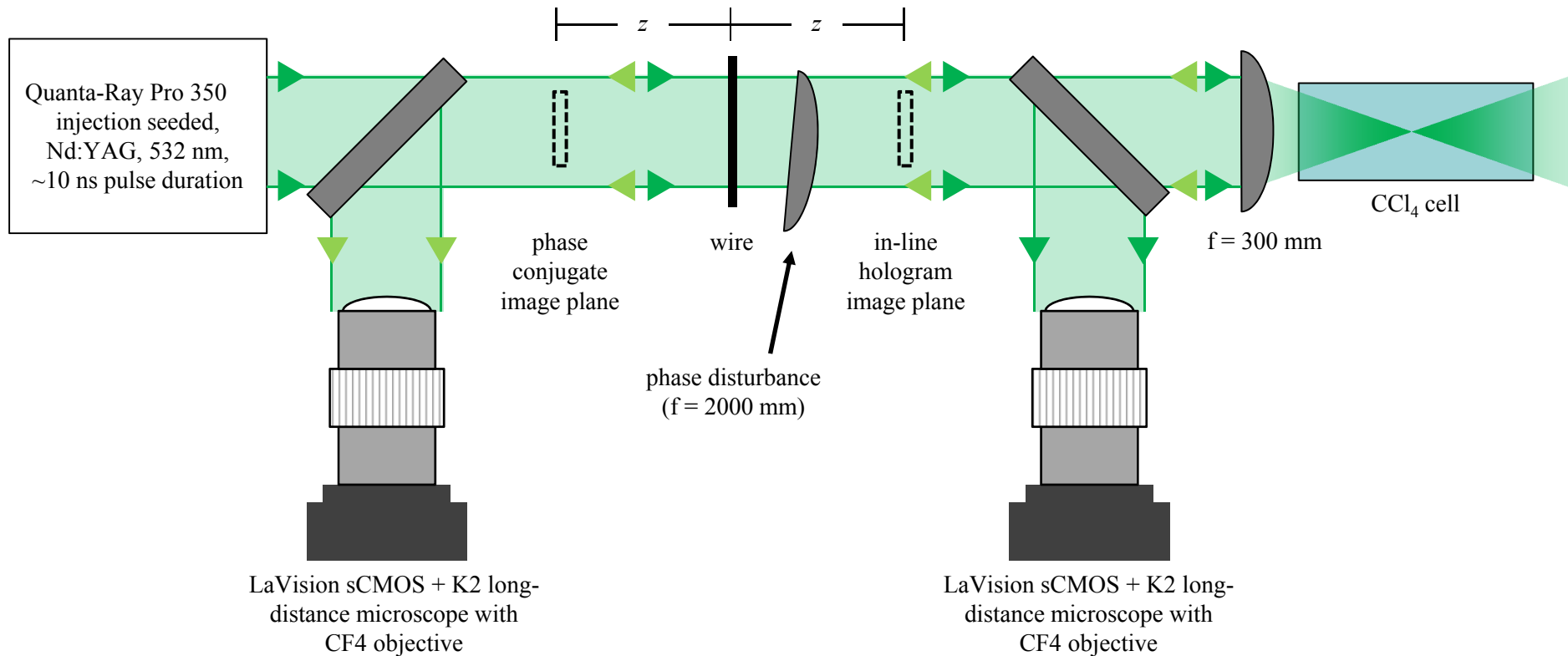
refocused to $z = 197$ mm



SBS phase-conjugate DIH

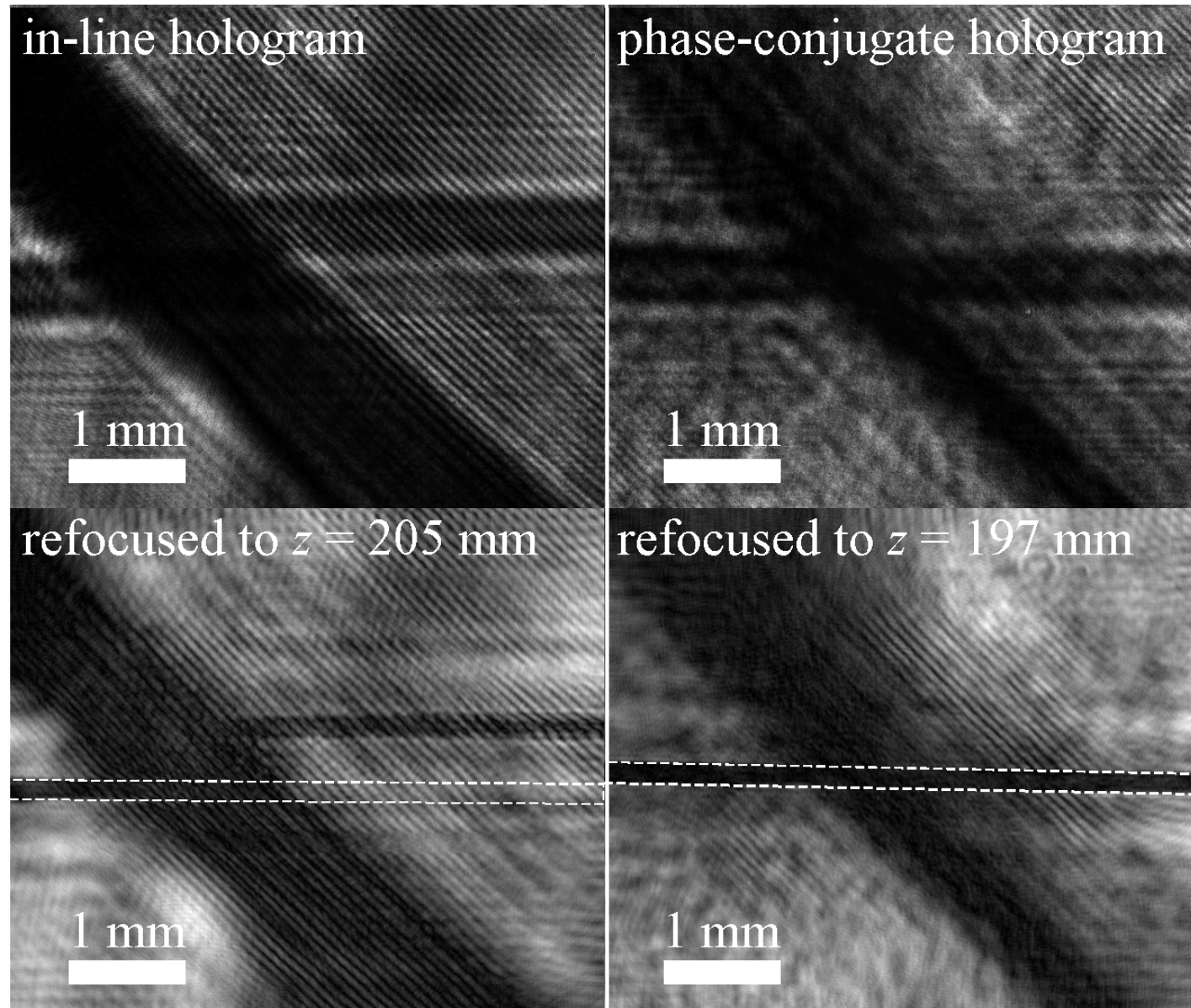
A focused beam in a non-linear medium induces phase conjugation via stimulated Brillouin scattering (SBS)

- A misaligned lens in the beam path causes a phase disturbance



SBS phase-conjugate DIH

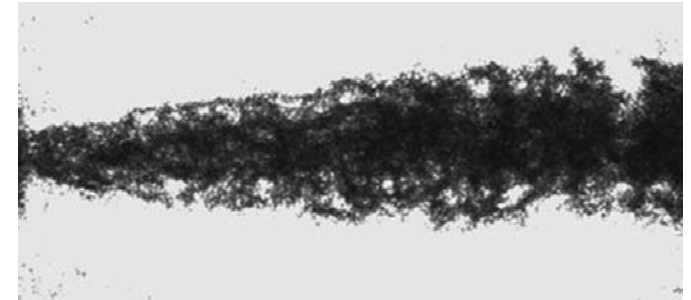
Phase
conjugation
corrects image
distortion



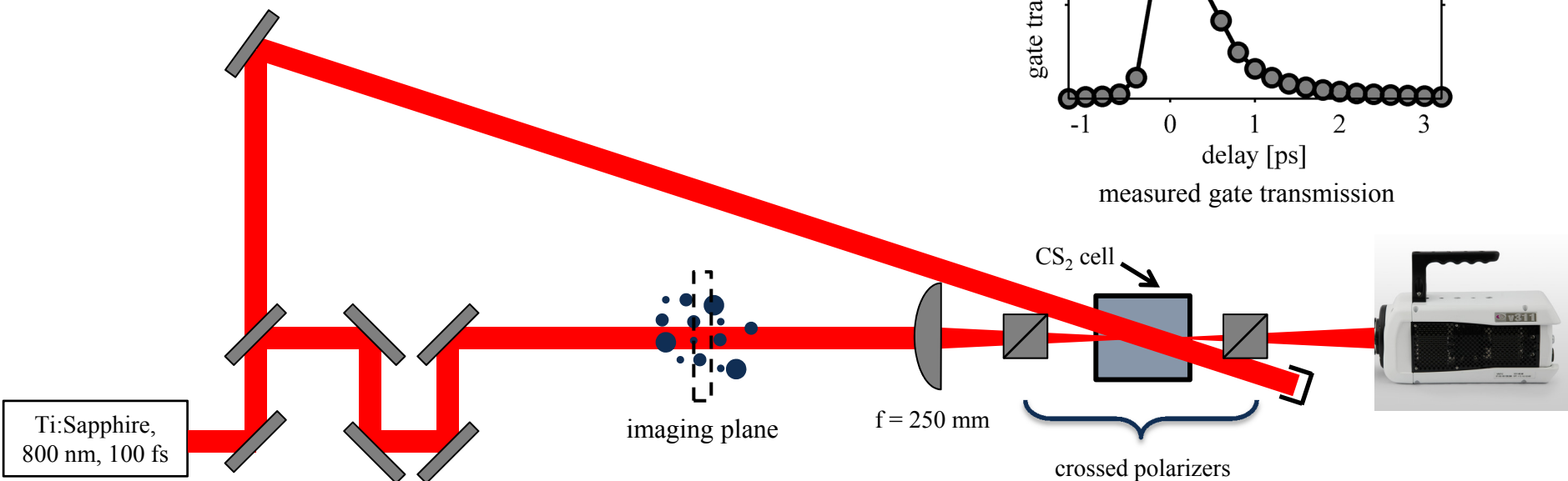
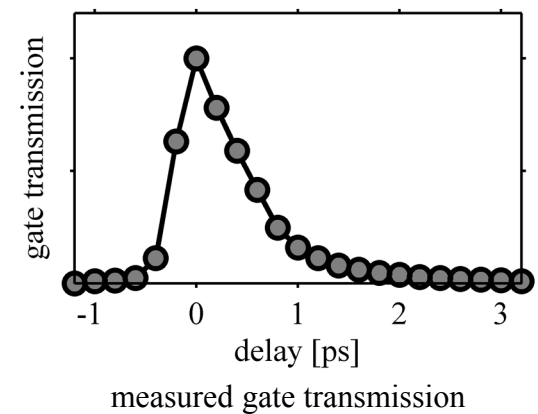
Ballistic DIH

Multiple scattering can be reduced through ps time gating

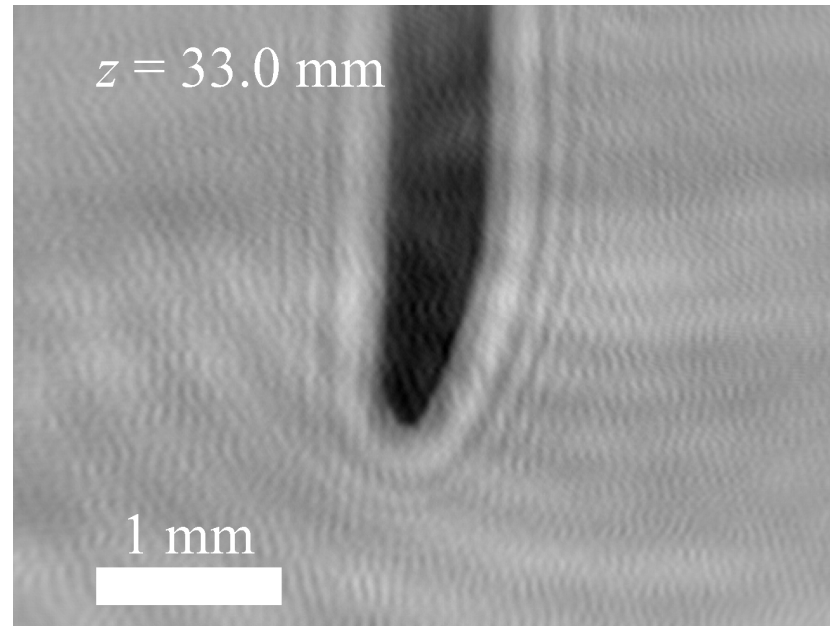
- Combination with DIH might enable scatter free 3D imaging through optically dense media
 - First proposed by: Trolinger et al 2011, *International Journal of Spray and Combustion Dynamics*



ballistic image of a diesel spray
(Linne et al 2006, *Exp. Fluids*)



DIH imaging through a Kerr gate (no scatter sources)

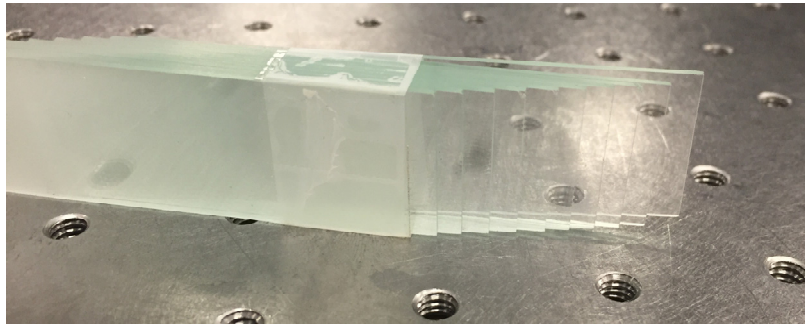
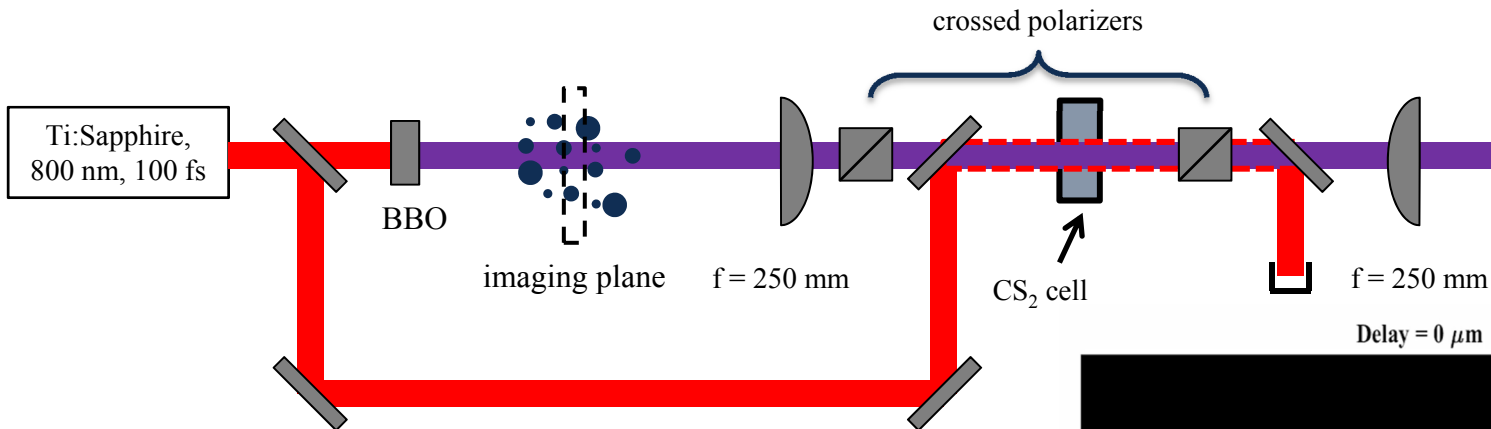


DIH image of a needle recorded with the ballistic configuration (1.6 ps switch delay)

Next step: Explore ballistic DIH through dense scattering sources

- Challenge: *Can we retain sufficient image fidelity and coherence to resolve 3D phenomena?*

Two-color, in-line ballistic imaging



stepped glass wedge