

Fukushima Forensics: Combustible Gas Effects

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Presentation Overview

- Information available
- TEPCO Reports
- Explosion Characteristics
 - 1F1, 1F3, 1F4
- Videos of Events
- Insights for Plant Data
- Summary of Insights
- Recommendations

Forensic Information Obtained

Item	What/How Obtained	Data Available ¹
RB-3a	Photos/videos of damaged walls and structures (1F1)	A
RB-3b	Photos/videos of damaged walls and structures (1F3)	A
RB-3c	Photos/videos of damaged walls and structures (1F4)	A
RB-4	Photos/videos of damaged walls and components and radionuclide surveys (1F2)	A
RB-6	Radionuclide surveys and sampling of ventilation ducts (1F4)	NA
RB-7	Isotopic evaluations of obtained concrete samples (1F2)	NA
RB-9	DW Concrete Shield Radionuclide surveys (1F1, 1F2, and 1F3 - after debris removed in 1F1 and 1F3)	NA
	Photos/videos around mechanical seals and hatches and electrical penetration seals (as a means to classify whether joints were in compression or tension).	A
RB-10	Photos/videos of 1F1 (vacuum breaker), 1F1, 1F2, and 1F3 PCV leakage points (bellows and other penetrations).	A
RB-11	Photos/videos and available information on 1F1, 1F2, and 1F3 containment hardpipe venting pathway, standby gas treatment system and associated reactor building ventilation system	NA
RB-13	Photos/videos of 1F1, 1F2, and 1F3 main steam lines at locations outside the PCV.	A
PC-1	Tension, Torque, and Bolt Length Records (prior and during removal); Photos/videos of head, head seals, and sealing surfaces (1F1, 1F2, and 1F3).	NA
PC-3	c) If vessel failed, photos/video, RN surveys, and sampling of 1F1, 1F2, and 1F3 pedestal wall and floor.	NA
	d) If vessel failed, 1F2, and 1F3 concrete erosion profile; photos/videos and sample removal and examination	NA
PC-4	Photos/videos of 1F1, 1F2, and 1F3 recirculation lines and pumps	NA

Hydrogen Explosions



Containment Over-pressurization Led to Release of H₂ into Buildings

Unit 1 Hydrogen Explosion



Unit 3 Hydrogen Explosion



1F1 End State

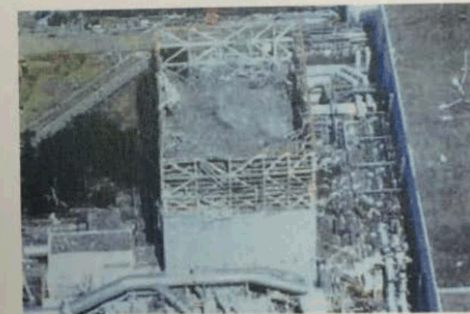
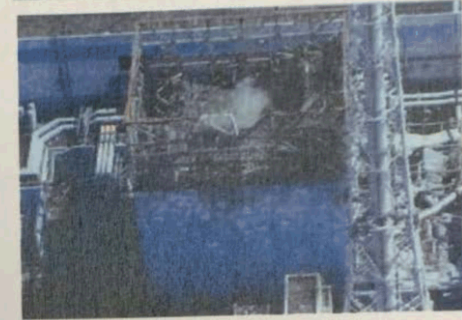
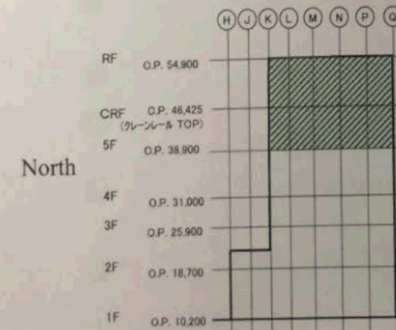
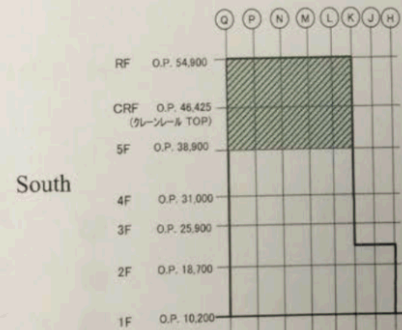
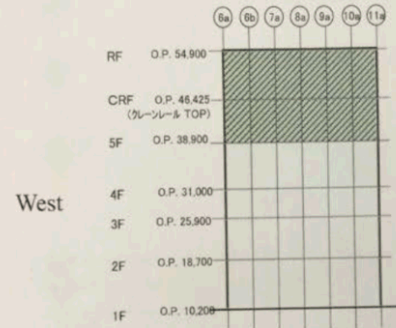
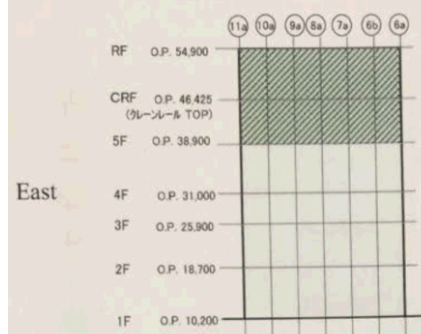
- Damage following explosion
- Shows all four sides of the building

Intact Portion

Damaged Portion

Damage on Outer Surface

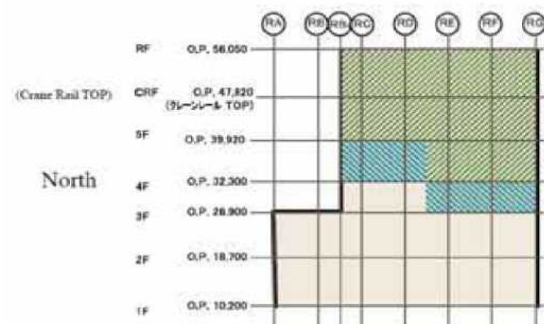
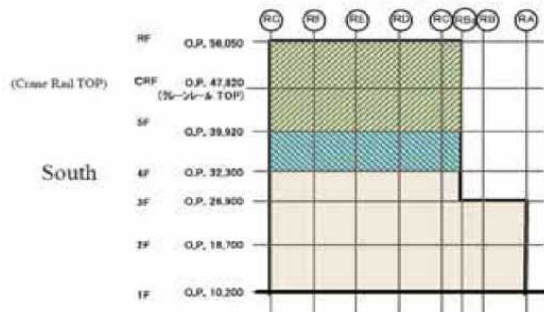
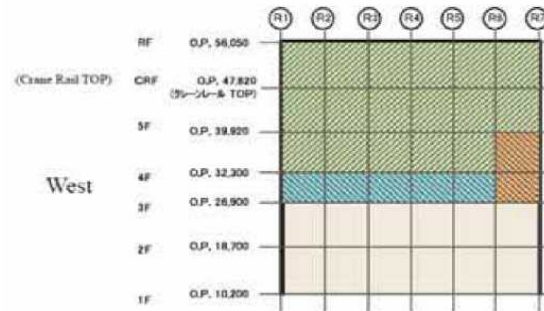
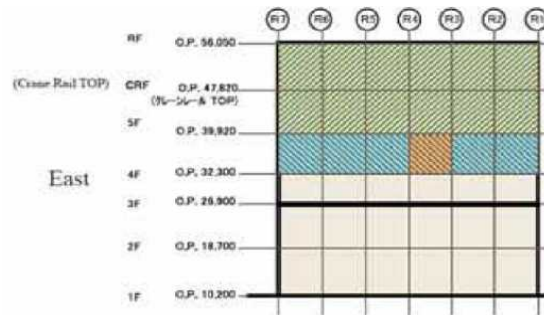
Wall Portion not Considered



1F3 End State

- Damage following explosion
- Shows all four sides of the building

Intact Portion
Damaged Portion
Damage on Outer Surface
Wall Portion not Considered



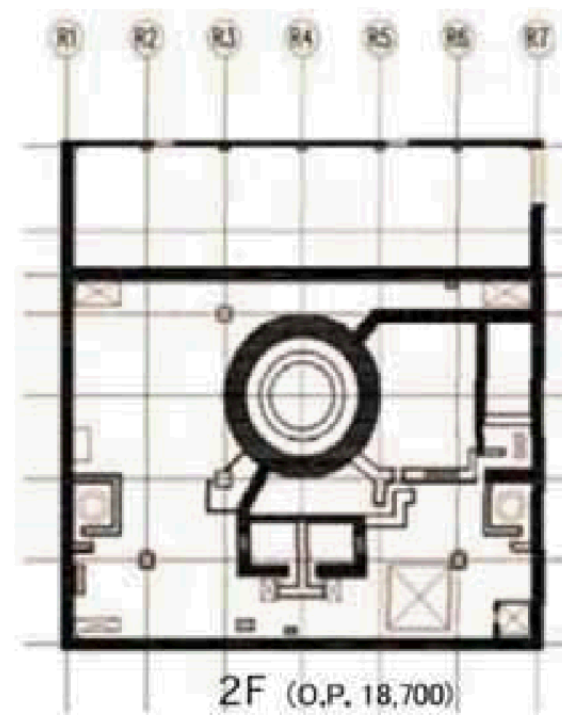
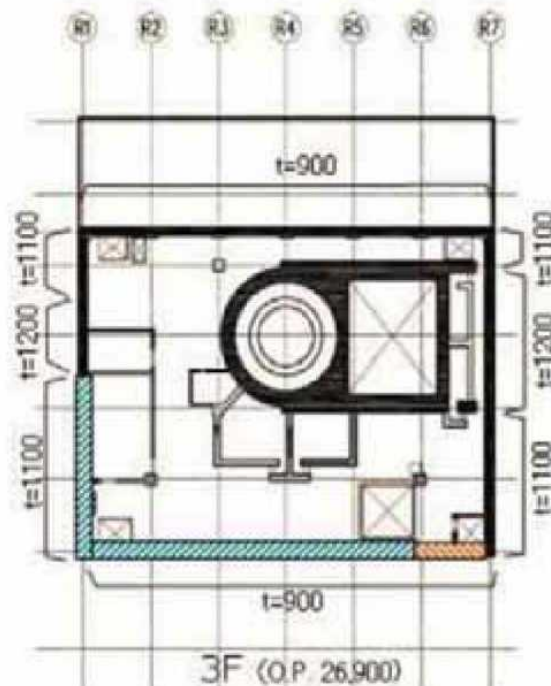
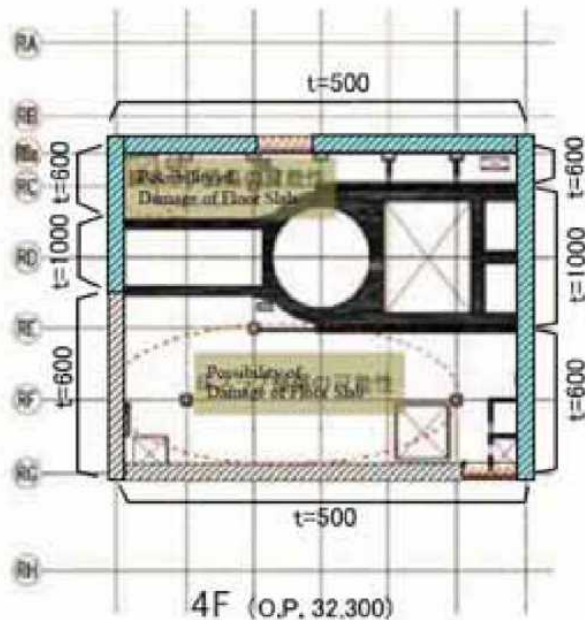
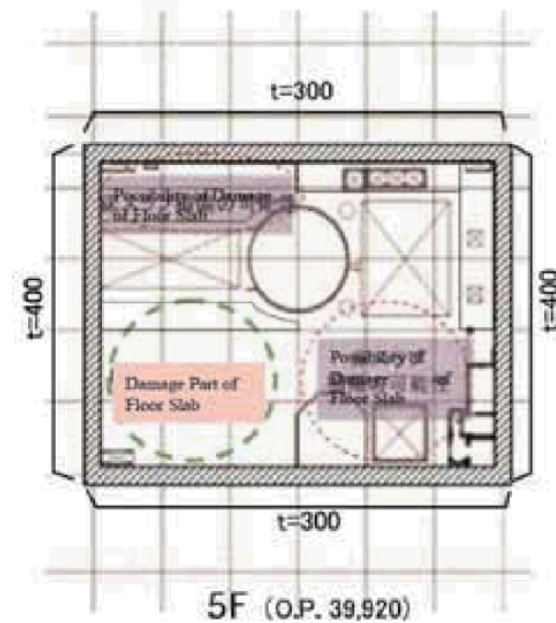
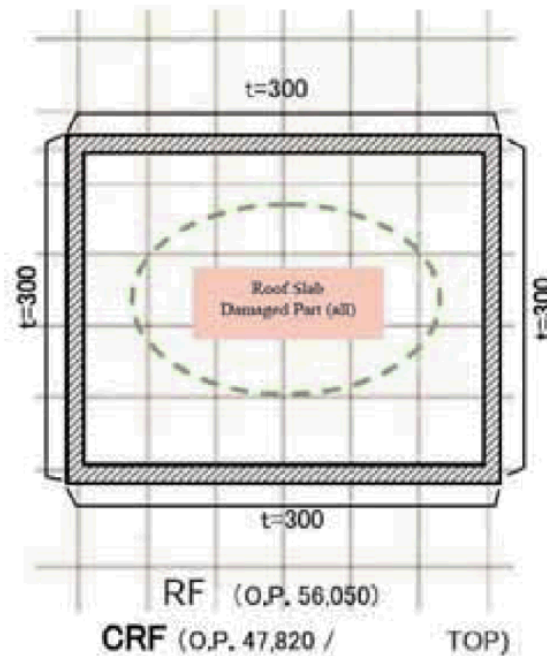
1F3 End State

- Floor plan

Damaged Portion

Damage on Outer Surface

Wall Portion not Considered



1F4 End State

- Damage following explosion
- Shows all four sides of the building

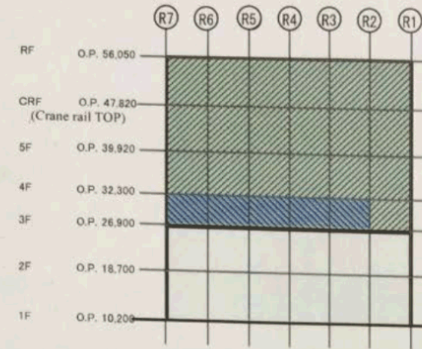
Intact Portion

Damaged Portion

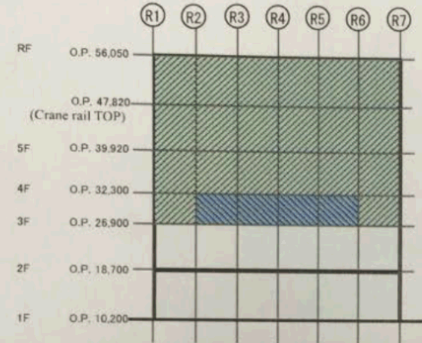
Damage on Outer Surface

Wall Portion not Considered

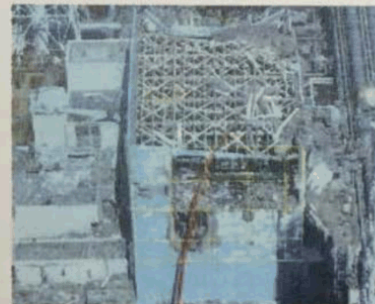
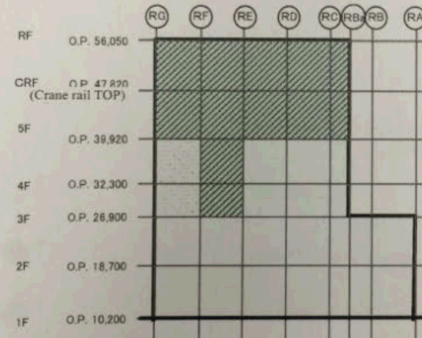
East
Side



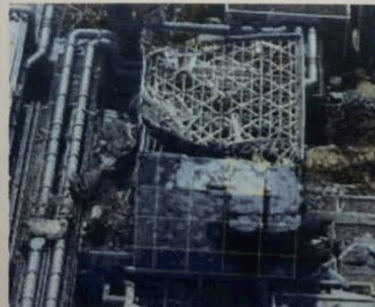
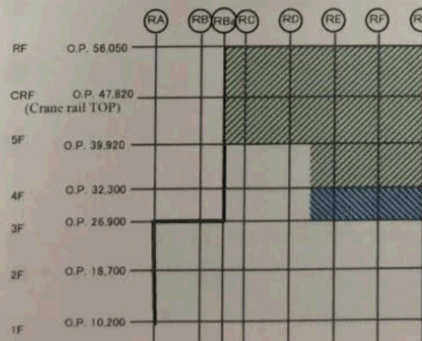
West
Side



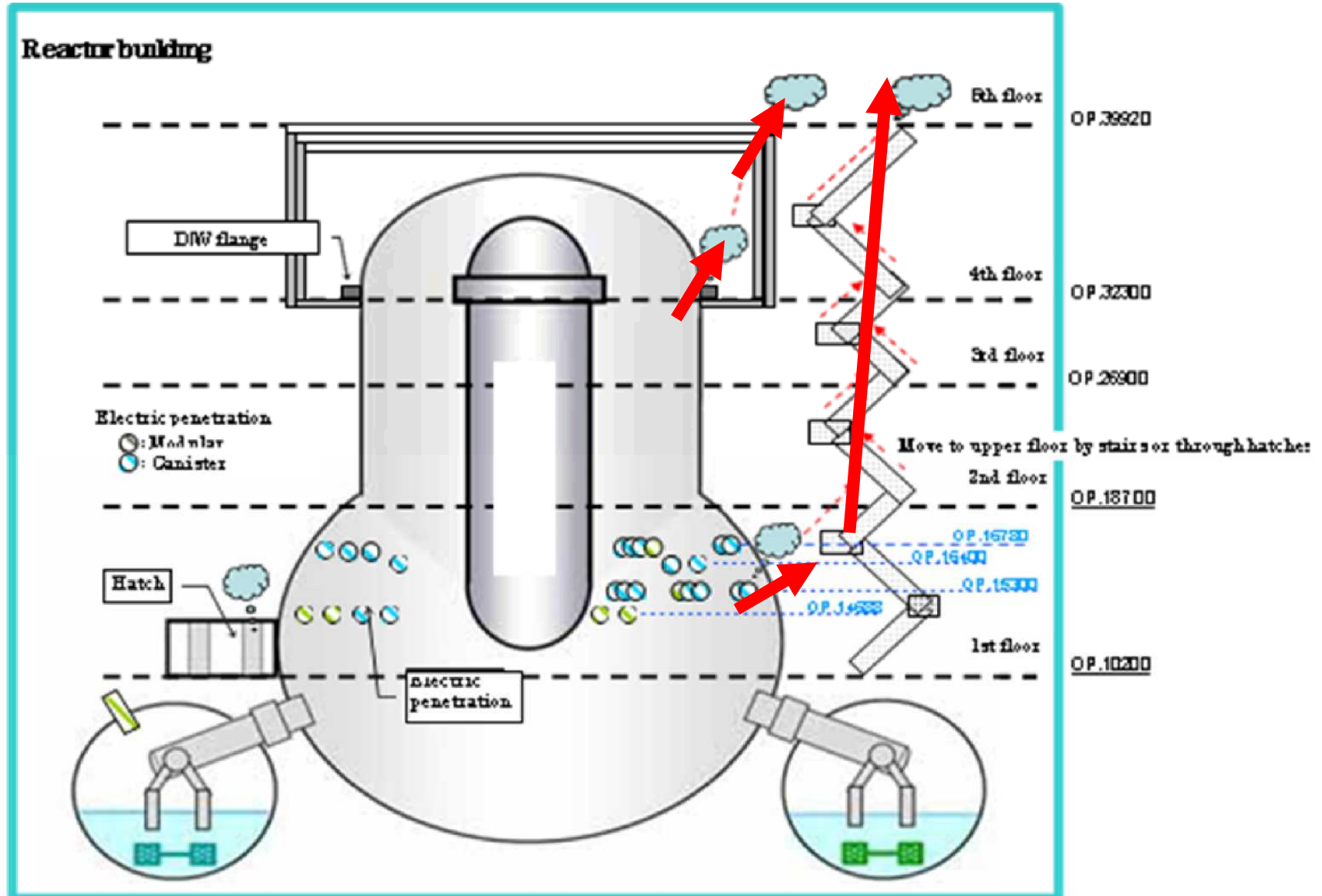
South
Side



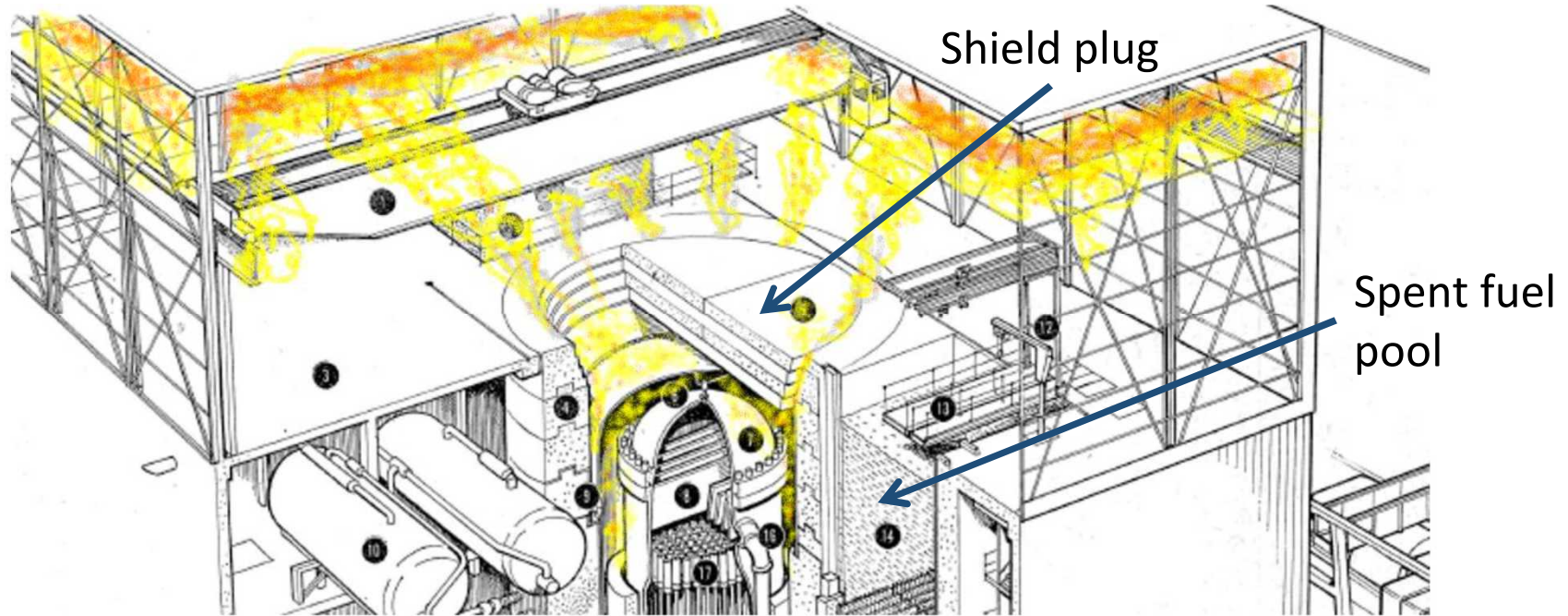
North
Side



1F1 Hydrogen Accumulation

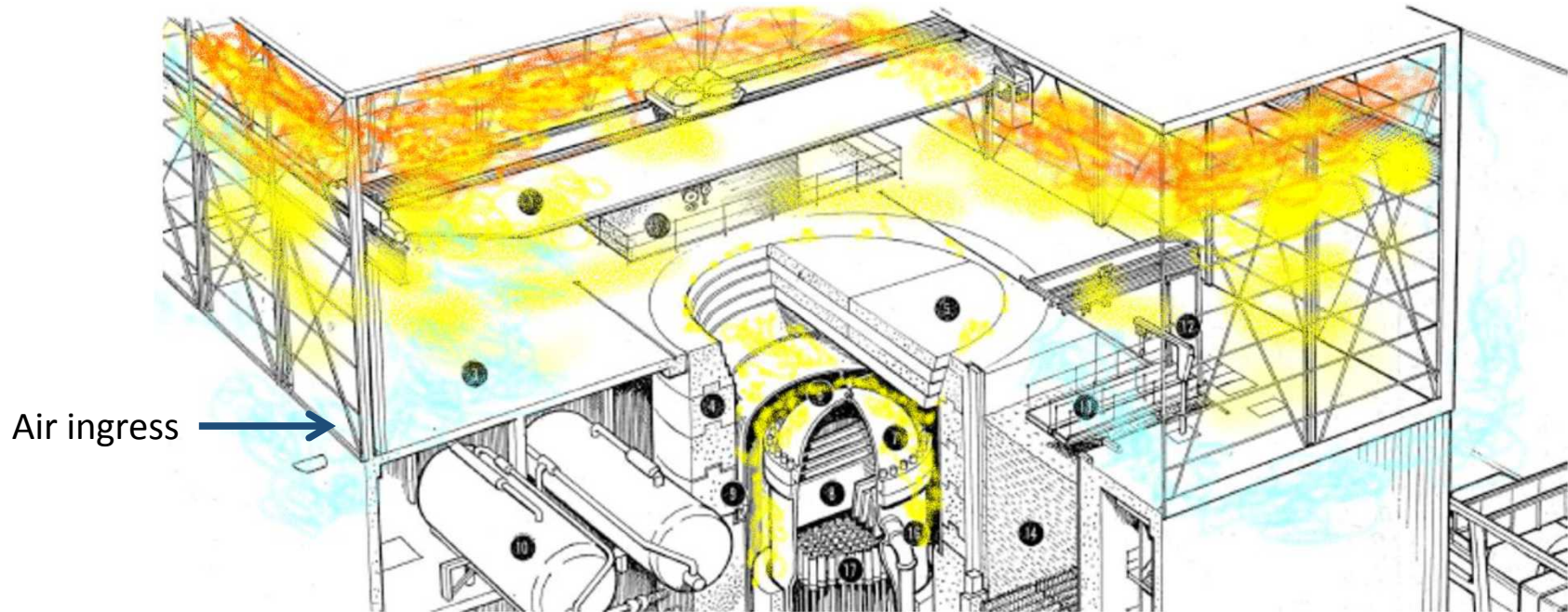


Hydrogen Accumulation in 1F1 – Alternative



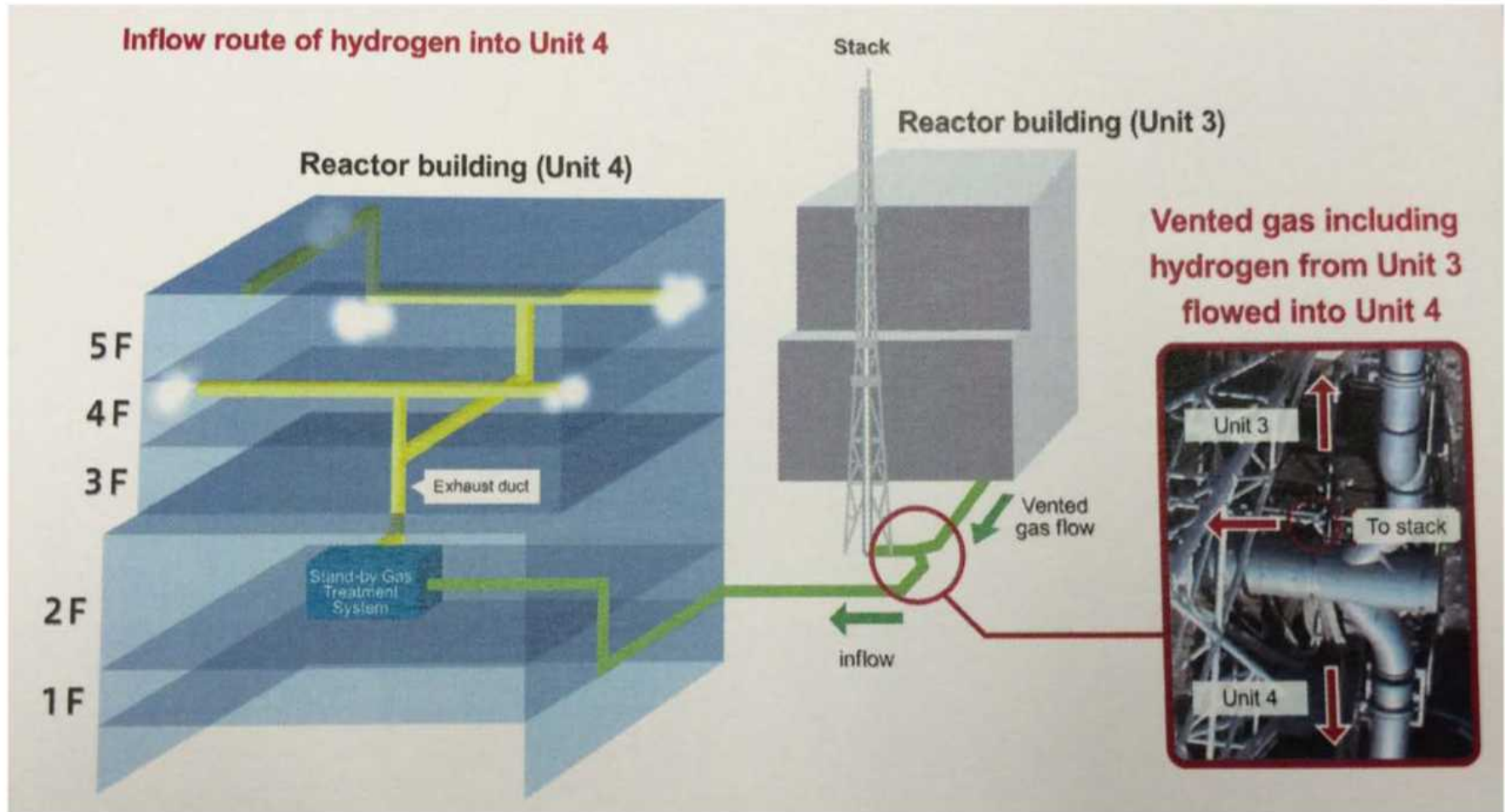
- Between ~12 hours and ~23 hours, steam and hydrogen leaks from drywell head flange and enters RB via shield plug seams
- Hydrogen, CO and steam rises to roof and spreads laterally
- Steam produced in MCCI and from emergency water injection
- Condensation in refueling bay depletes steam in hot layer and enriches hydrogen
- Mixture displaces air from building
- Steam mole fraction exceeds 50% - inert conditions prevent combustion

Combustible Conditions Follow PCV Venting in 1F1 - Alternative

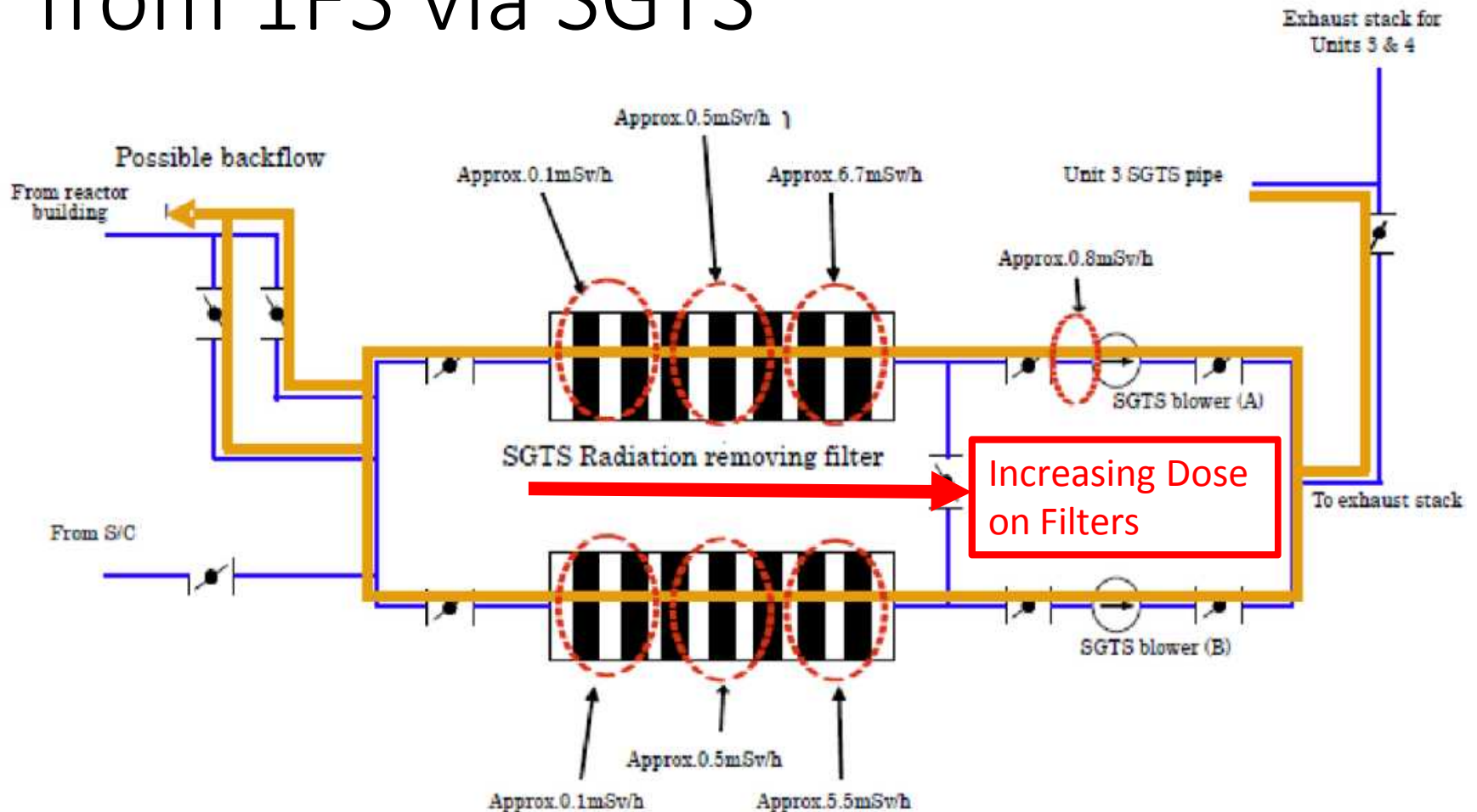


- At around ~23 hours, steam and hydrogen leakage from PCV greatly reduced
 - Water injection was stopped
 - PCV was depressurized by operator venting action
- Continuing condensation without steam source....
 - Reduces steam molar fraction to below 50% in refueling bay, and
 - Produces partial vacuum that draws in outside air
- Air ingress and steam condensation leads to conditions favoring combustion
- Hydrogen stratification produces flammable or detonable concentrations of H_2/O_2

Transfer of H₂ to 1F4 from 1F3 via SGTS

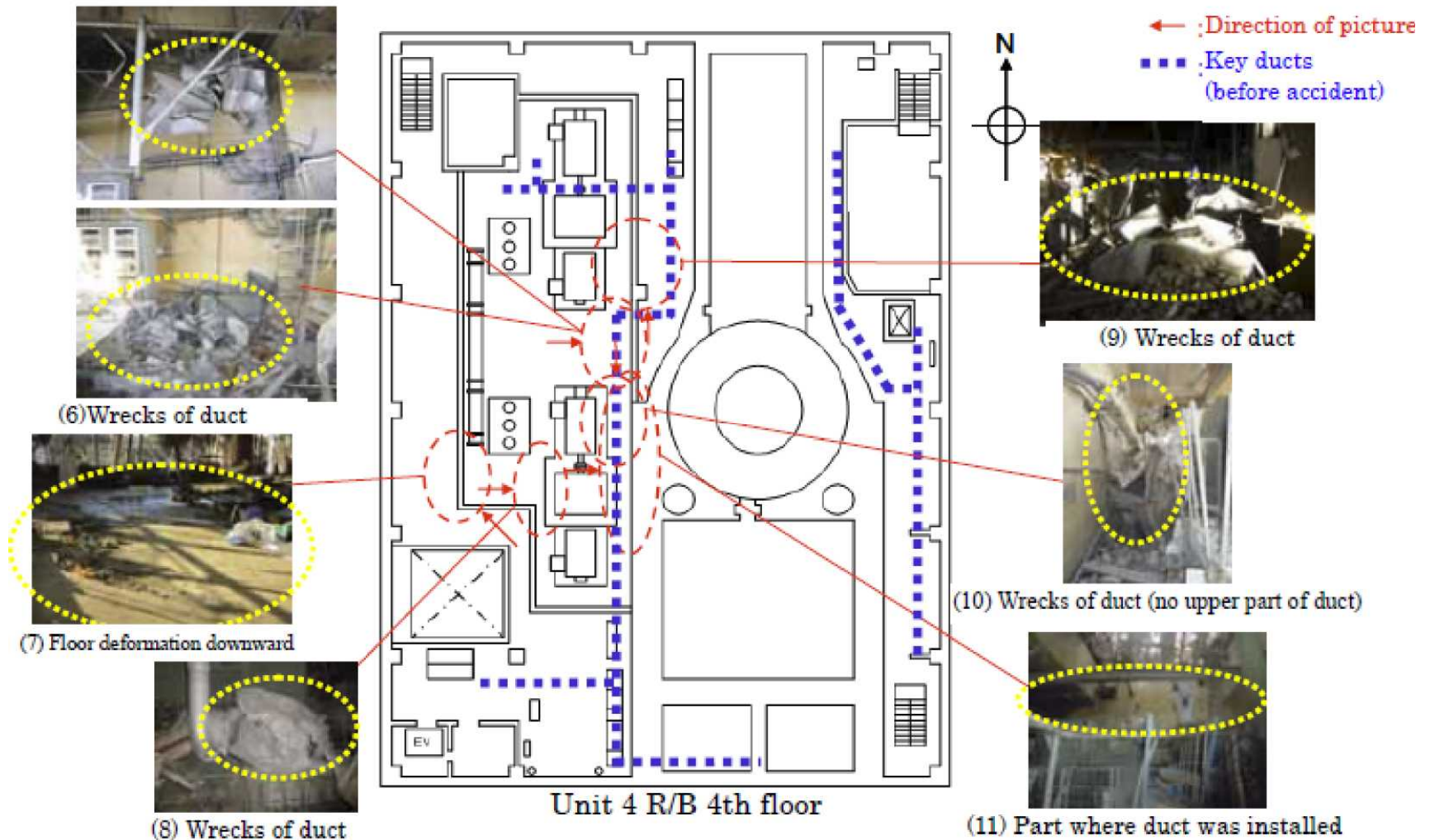


Transfer of H₂ to 1F4 from 1F3 via SGTS

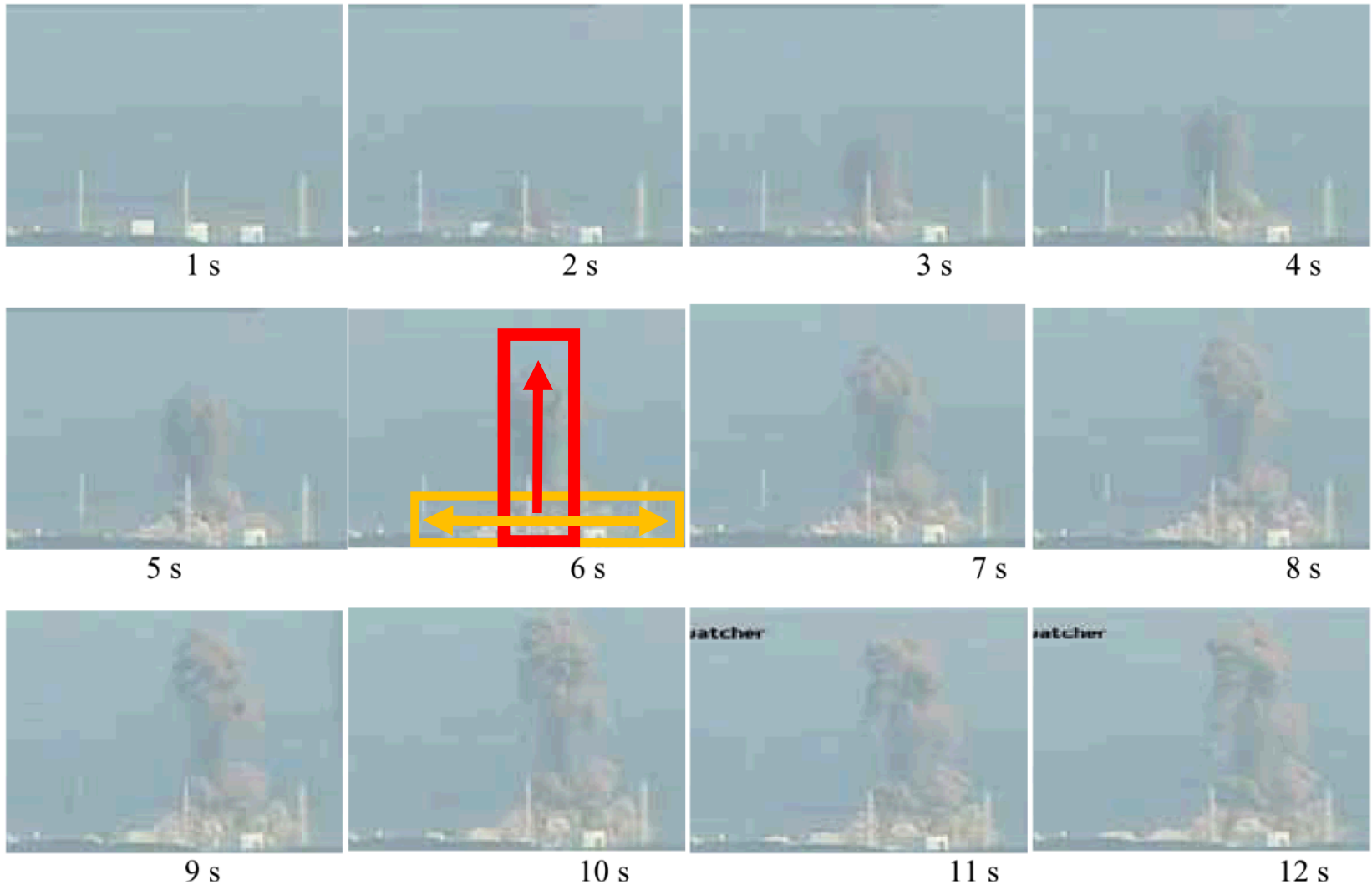


Results of measurement of amount of radiation in Unit 4 SGTS
(conducted on August 25, 2011)

1F4 Field Investigation



Two Separate Explosions at Unit 3



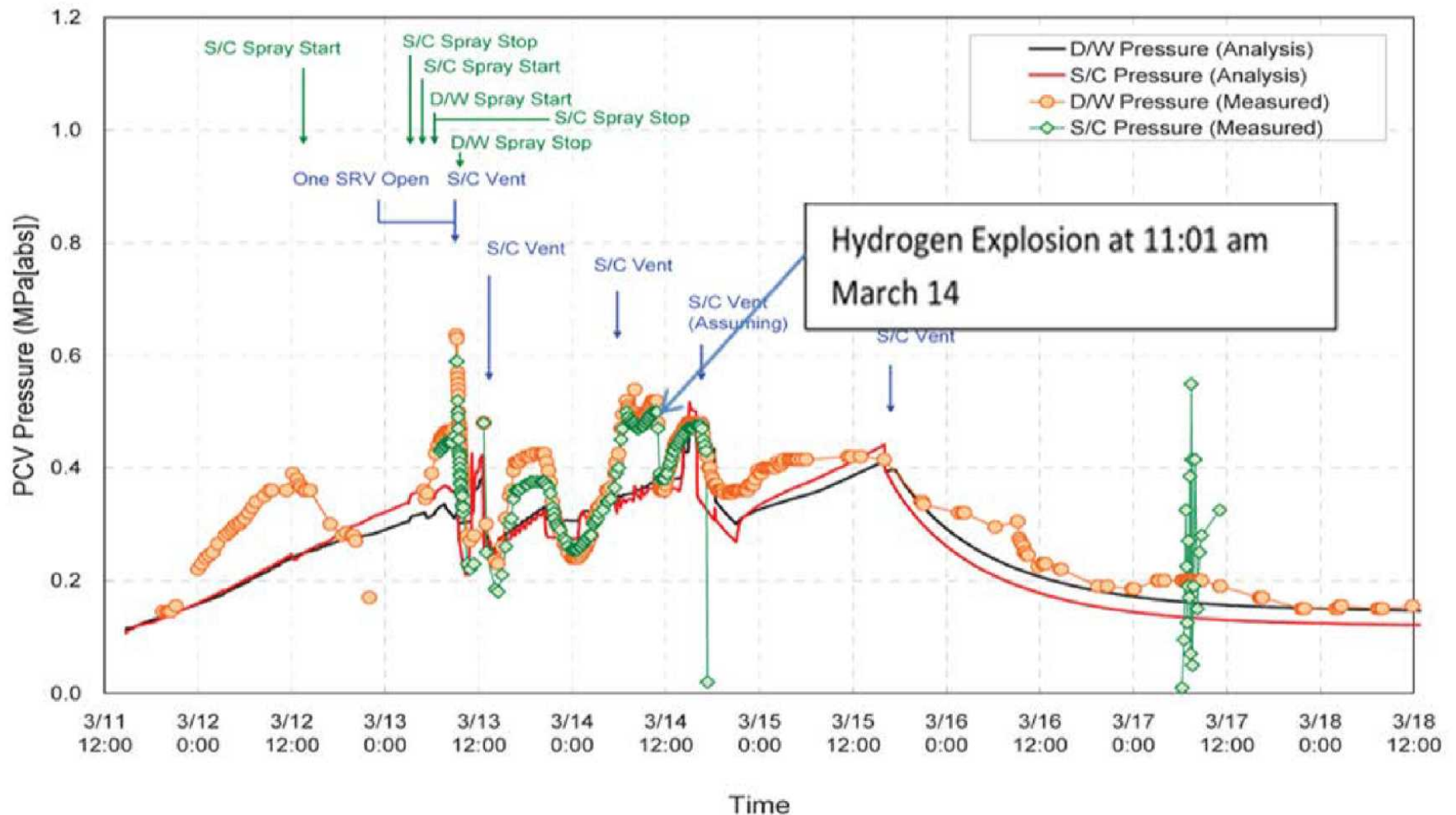
Two Separate Explosions at Unit 3

- There appeared to be at least two explosions
- First:
 - less energetic and directed horizontally (similar to that of 1F1)
 - The color of the explosion “smoke” appears white and orange
- Second:
 - Directed vertically with an almost perfect spherical fireball appearing above the building
 - Shooting up very high into the sky (about 3 times the vent stack height)
 - Large chunks of materials appeared to be carried with the fireball.
- 1F3 images indicate that concrete pillars on the building top floor were highly damaged
- Product gas of the explosion appears to be a darker color, raising questions:
 - Reactor building concrete dust was generated from the explosion?
 - If dust was generated within the drywell due to MCCI?

1F3 Plant Data

Primary containment failure before explosion

- DW head failure
- Bellows failure



Insight Summary

- **The 1F3 explosion was not a stand-alone randomly occurring event.**
 - The 1F3 explosion was most likely initiated by failure of the drywell upper head seal when it was at high PCV pressure of 0.53 MPa.
 - The released hot gas was likely the ignition source and became a source of fuel that supplied to the highly energetic fireball burning at and above the building.
 - The fireball was a dark color (rather than the white color of a water vapor condensation cloud), raising questions, such as whether a significant amount of reactor building concrete dust was generated from the explosion, or whether dust generated from within the drywell was due to MCCI.
- **The damage to the 1F3 building was more extensive compared to damage incurred at 1F1 and 1F4.**
 - To what extent was the damage caused by the energetic explosion as a consequence of drywell head seal failure at high PCV pressure and temperature is a question to be answered.
- **The shared vent stack between 1F3 and 1F4 allowed hydrogen that was vented from 1F3 to enter the 1F4 reactor building.**
 - Radionuclide surveys and examination information confirm that the shared vent stack was the reason for the explosion in the 1F4 reactor building.

Recommendation

- Limited knowledge regarding in-core damage progression can lead to significant differences in code predictions for hydrogen production
 - Differences between code predictions stem from a lack of experimental data that would clarify appropriate modeling assumptions regarding in-core melt progression behavior
 - As a result, the MAAP and MELCOR predict different amounts of in-core hydrogen generation
 - MAAP5 typically predicting lesser amounts of in-core hydrogen generation relative to MELCOR (See xWalk)
- Important consequences for the development of flammable conditions in the 1F1 and 1F3 reactor buildings

Recommendation 6.1:

To address this important knowledge gap in severe accident phenomena, evaluations of combustible gas phenomena should be continued to reduce uncertainties in MAAP and MELCOR predictions.

References – Taken from Report

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115. Tokyo Electric Power Company, the Report on the Investigation into the Current Seismic Safety and Reinforcement of the Reactors at Fukushima Daiichi Nuclear Station (No. 2)," July 13, 2011
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120. W. Luangdilok, E. van Heerden, P. McMinn, Calculation of the Probability of DDT during Severe Accidents, NURETH-16, Chicago, August 30 – September 4, 2015.
121. H. Yanagisawa, H. Takeuchi, M. Akinaga, S. Mizokami, T. Honda, and M. Watanabe, "The Accident Analysis for Unit 3 at Fukushima Daiichi Nuclear Power Station," *9th Int. Topical Meeting on Nuclear Thermal Hydraulics, Operation and Safety (NUTHOS-9)*, Kaohsiung, Taiwan, September 9-13 (2012).