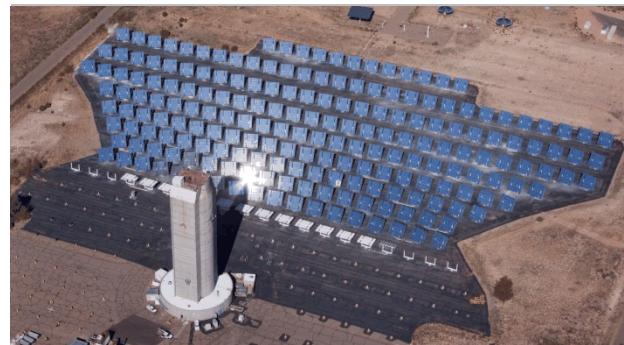
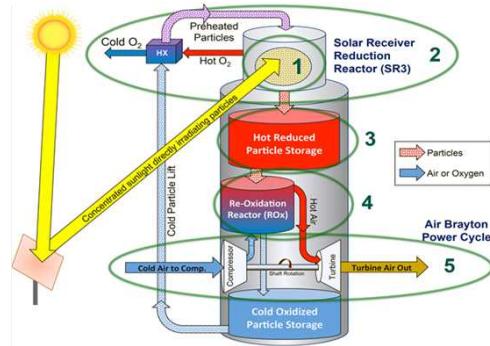
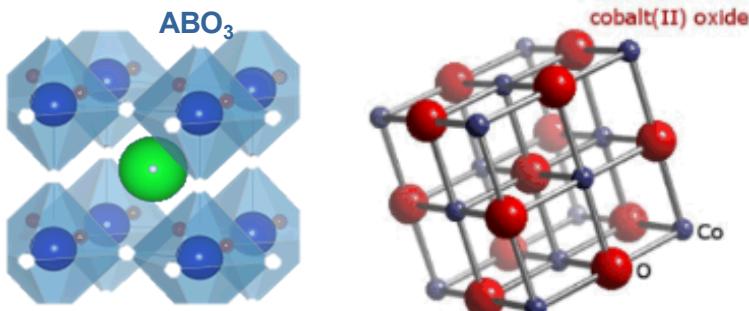


*Exceptional service in the national interest*



# Metal Oxides with Ionic-Electronic Conductivity for Thermochemical Energy Storage

Eric N. Coker, Sean M. Babiniec, Andrea Ambrosini, James E. Miller



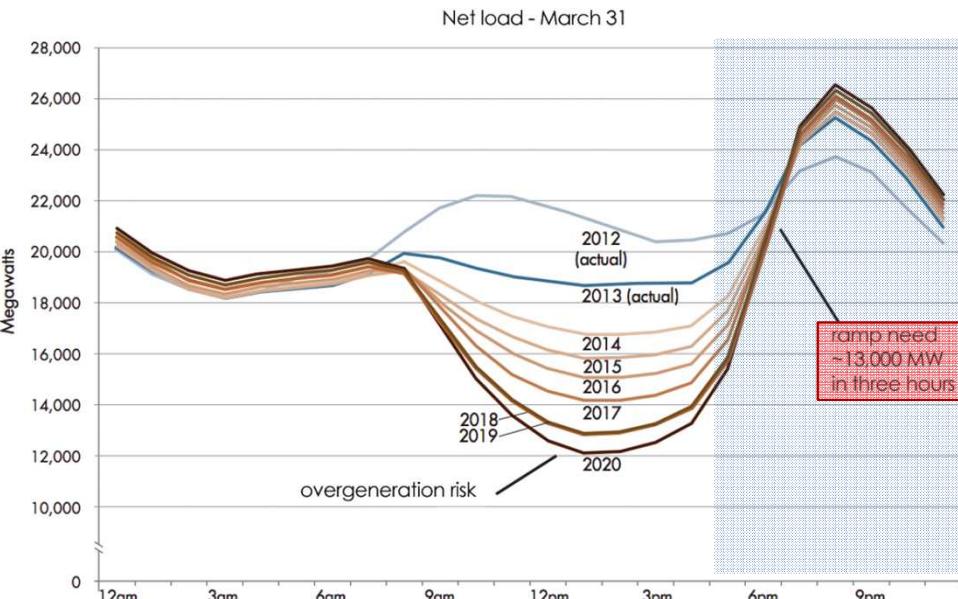
**ECI CO<sub>2</sub> Summit II: Technologies and Opportunities**  
 Santa Ana Pueblo, NM. April 10-14, 2016

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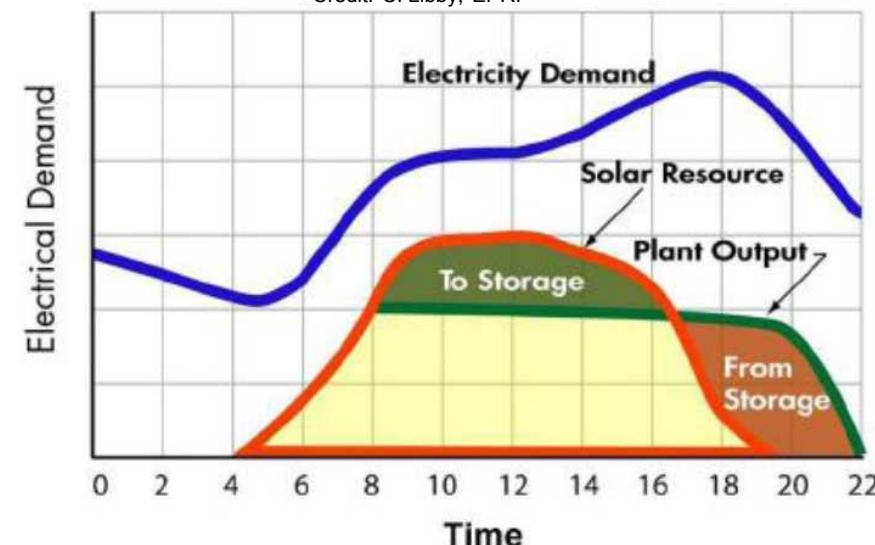
# Storage is critical for market penetration of solar energy into the grid

- Without storage, solar electricity is generated when least needed
- Shifting solar electricity generation to period of peak demand would have large implications on grid integration
- Decrease Levelized Cost of Electricity (LCOE) through better sizing/usage of power block

Credit: California Independent System Operator Corporation



Credit: C. Libby, EPRI

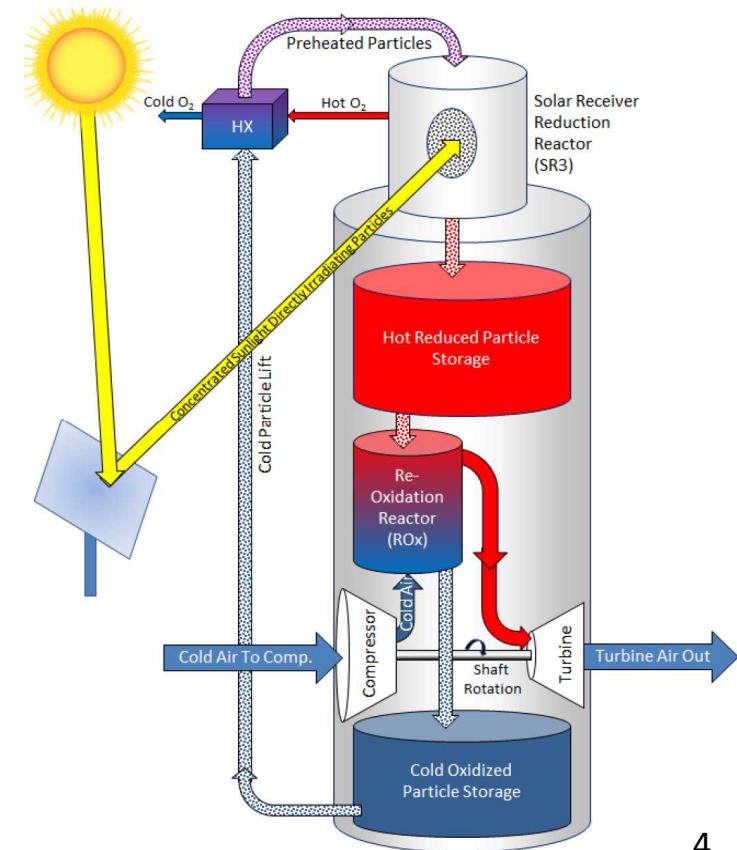


# Storage: Why thermal?

- Mechanical
  - Flywheels, compressed air, hydrostatic
    - ✓ High capacities (large scale)
    - ✗ Typically suffer from low efficiencies
- Electronic
  - Li-ion batteries
    - ✓ High efficiencies
    - ✗ Expensive materials, limited charge/discharge rates
  - Supercapacitors
    - ✓ Fast charge/discharge rates
    - ✗ Low energy densities
- Thermal
  - ✓ High efficiency
  - ✗ Temperatures high to support new power cycles (~1200 °C)
    - ❖ *Materials development crucial to feasibility of thermal storage at such temperatures*

Concentrating solar power (CSP) has unique ability to harness thermal storage

- Solar energy used to heat storage media, drive thermal engine
- Current molten-salt storage systems are limited
  - Sensible-only storage, low energy storage densities
  - Salt decomposition limits turbine operating temperatures ( $\sim 600$  °C, max.)
- Redox particle-based systems offer advantages
  - High storage densities *via* (sensible + reaction) enthalpy
    - Thermochemical energy storage (TCES)
  - Cycle not limited by low decomposition temperatures
  - Direct irradiation of thermal storage media
  - Re-oxidation reaction directly off compressor outlet, favorably shifting thermodynamics



# Materials requirements driven by Air-Brayton operating parameters



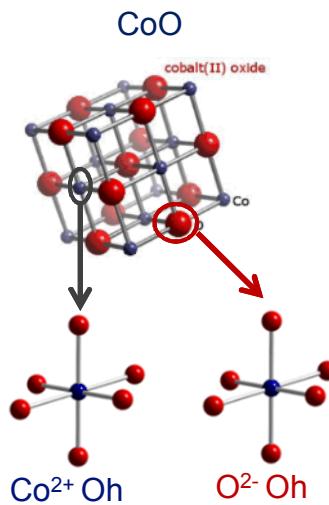
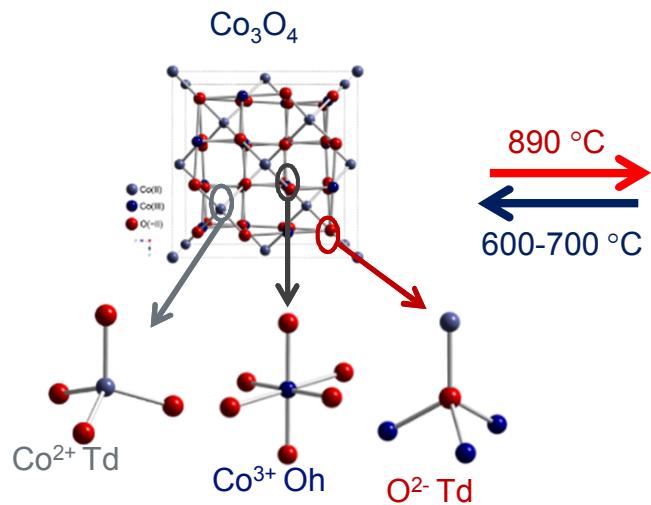
- High-efficiency Air-Brayton turbines are designed to operate at  $\sim 1200$  °C
- Such temperatures are problematic for existing oxide TCES materials

- State-of-the-art cobalt oxide redox couple:

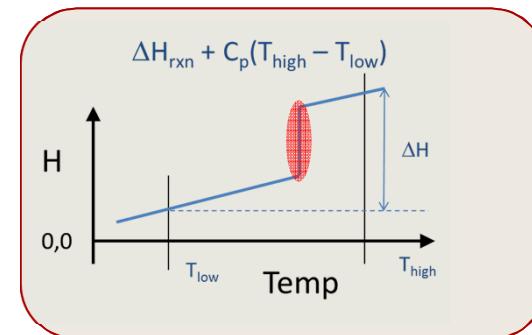


- High theoretical  $\Delta H$  occurring at one discrete transition
- Reduction/oxidation in air occurs near 885 °C
- Kinetics are slow at low temperatures
- Cobalt is expensive

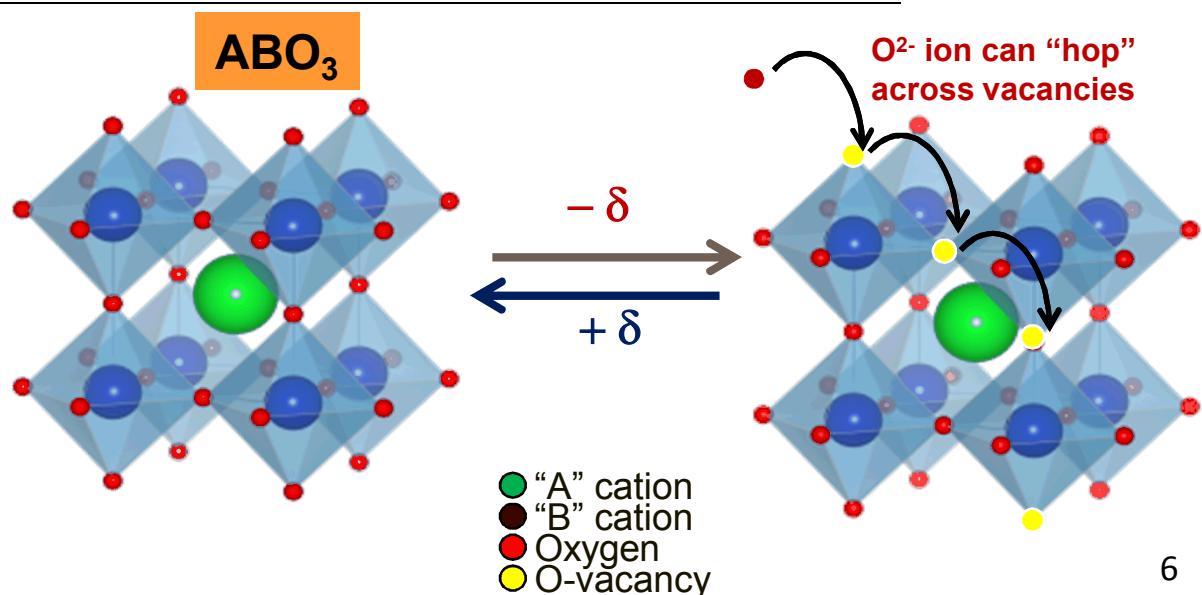
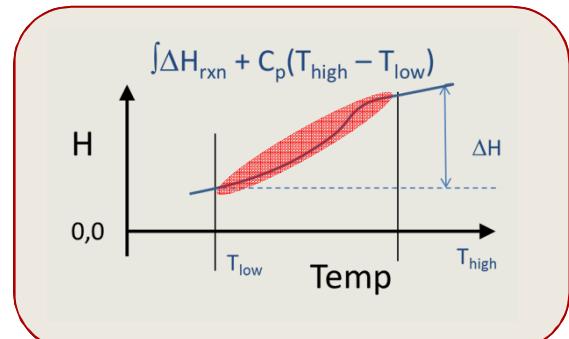
# Cobalt oxide vs. Perovskites ( $\text{ABO}_3$ )



- Energetic phase change
- No  $\text{O}^{2-}$  transport
- Oxidation exotherm typically recovered at lower temperature than reduction

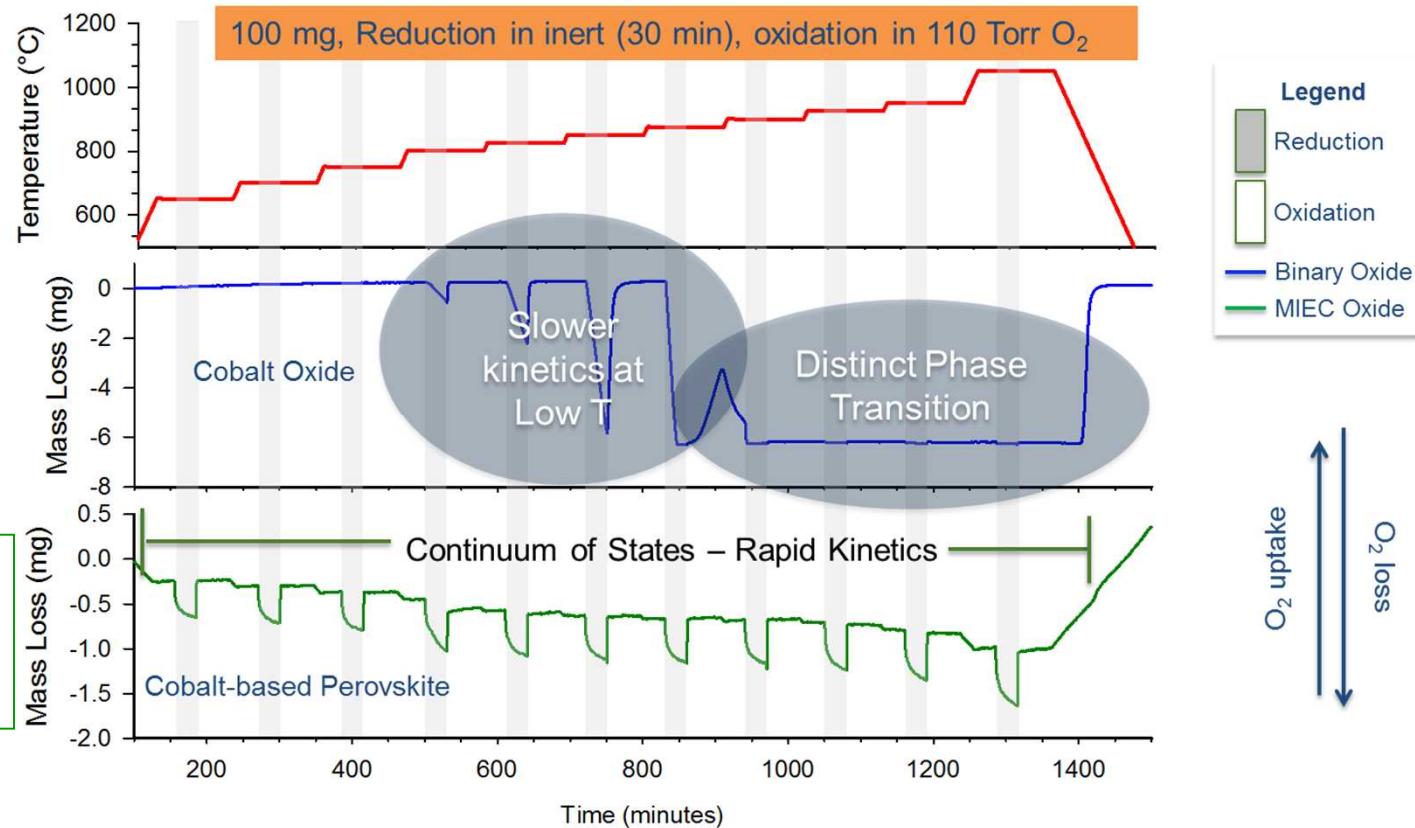


- No phase change occurs
- Vacancies facilitate  $\text{O}^{2-}$  transport
- Redox activity continuous over variety of T and  $\text{pO}_2$



# Perovskites offer a solution to increasing turbine inlet temperatures to $\geq 1200$ °C

- Continuous reduction behavior as opposed to discrete reaction



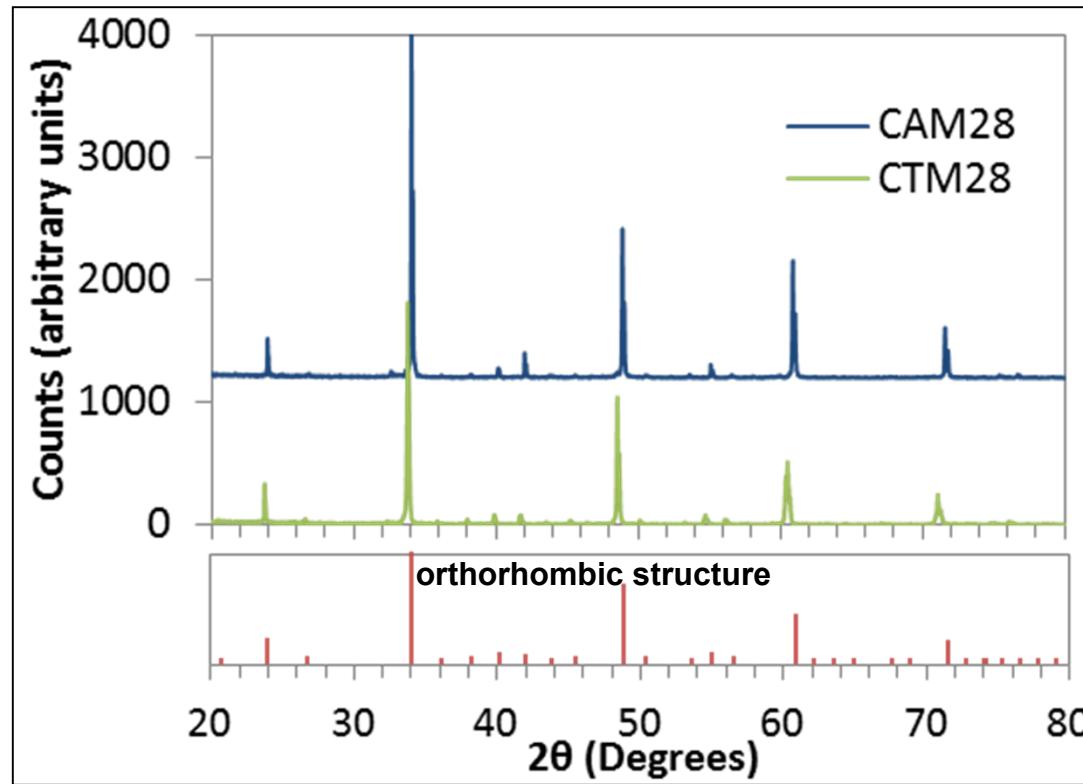
- Perovskites need to be engineered to increase capacity (mass loss) and reaction enthalpy

# Perovskite compositions

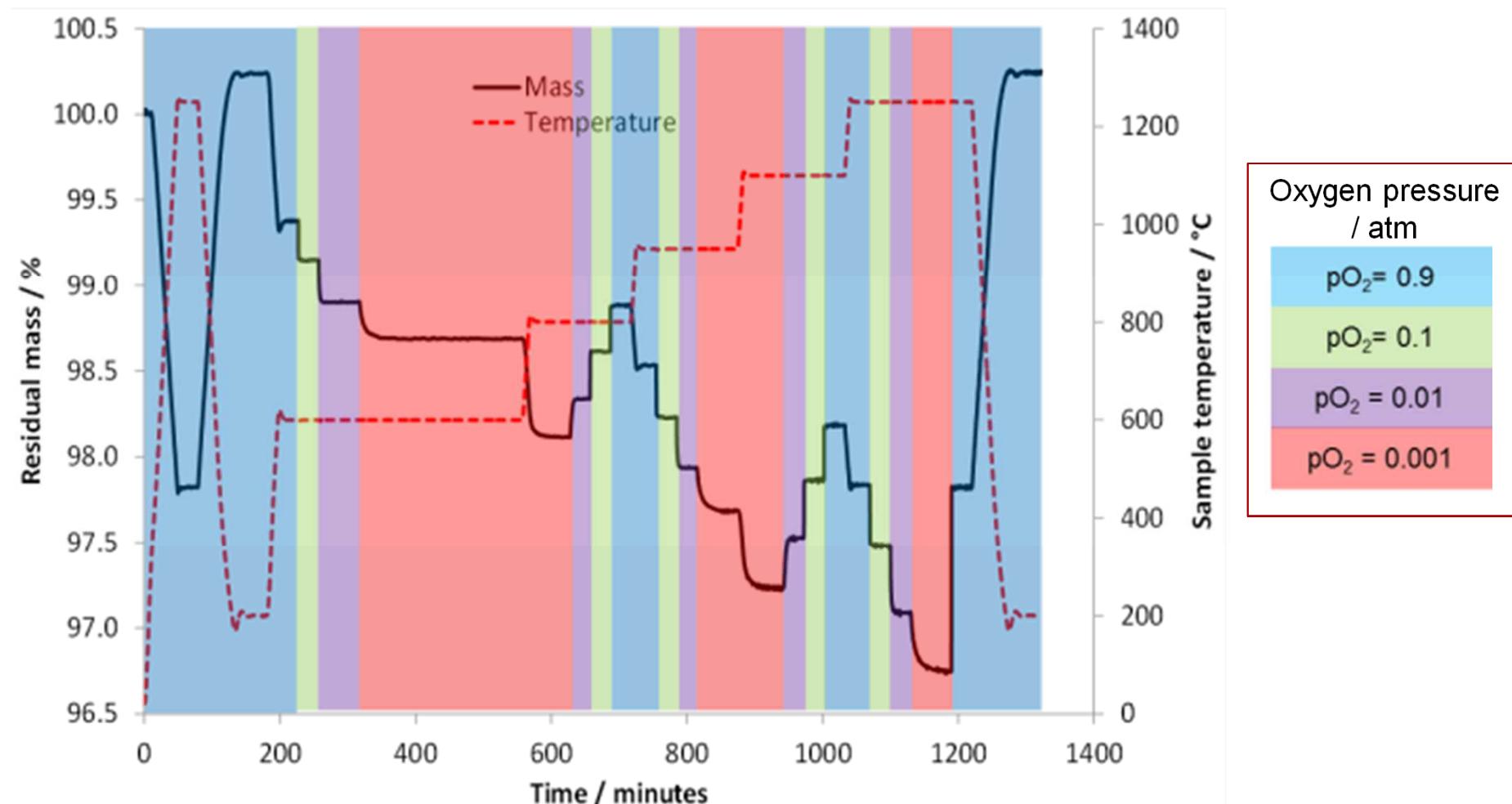
- $\text{ABO}_3 + \text{H} \leftrightarrow \text{ABO}_{3-\delta} + \delta/2 \text{ O}_{2(\text{g})}$ 
  - Gas species dominates entropy term (largest # degrees-of-freedom)
- At equilibrium (onset of reduction)  $\Delta G_{\text{red}} = 0 = \Delta H_{\text{red}} - T \Delta S_{\text{red}}$ ,
  - A change in reduction enthalpy necessitates a change in reduction temperature
- Previous studies focused on  $\text{La}_x\text{Sr}_{1-x}\text{Co}_y\text{M}_{1-y}\text{O}_{3-\delta}$ , with  $\text{M} = \text{Fe}, \text{Mn}$ 
  - High redox capacity ( $\delta$ ), but at low temperature (low reaction enthalpy)
- New materials aim to improve cost, reaction enthalpy:
  - Cost-effective, lightweight cations desired
  - A-site: Ca, B-site: Mn, Ti, Al

# Synthesis and phase characterization

- Materials synthesized using an aqueous (Pechini) method
- X-ray diffraction used for phase identification
- Compositions:
  - CAM28  $(\text{CaAl}_{0.2}\text{Mn}_{0.8}\text{O}_{3-\delta})$
  - CTM28  $(\text{CaTi}_{0.2}\text{Mn}_{0.8}\text{O}_{3-\delta})$

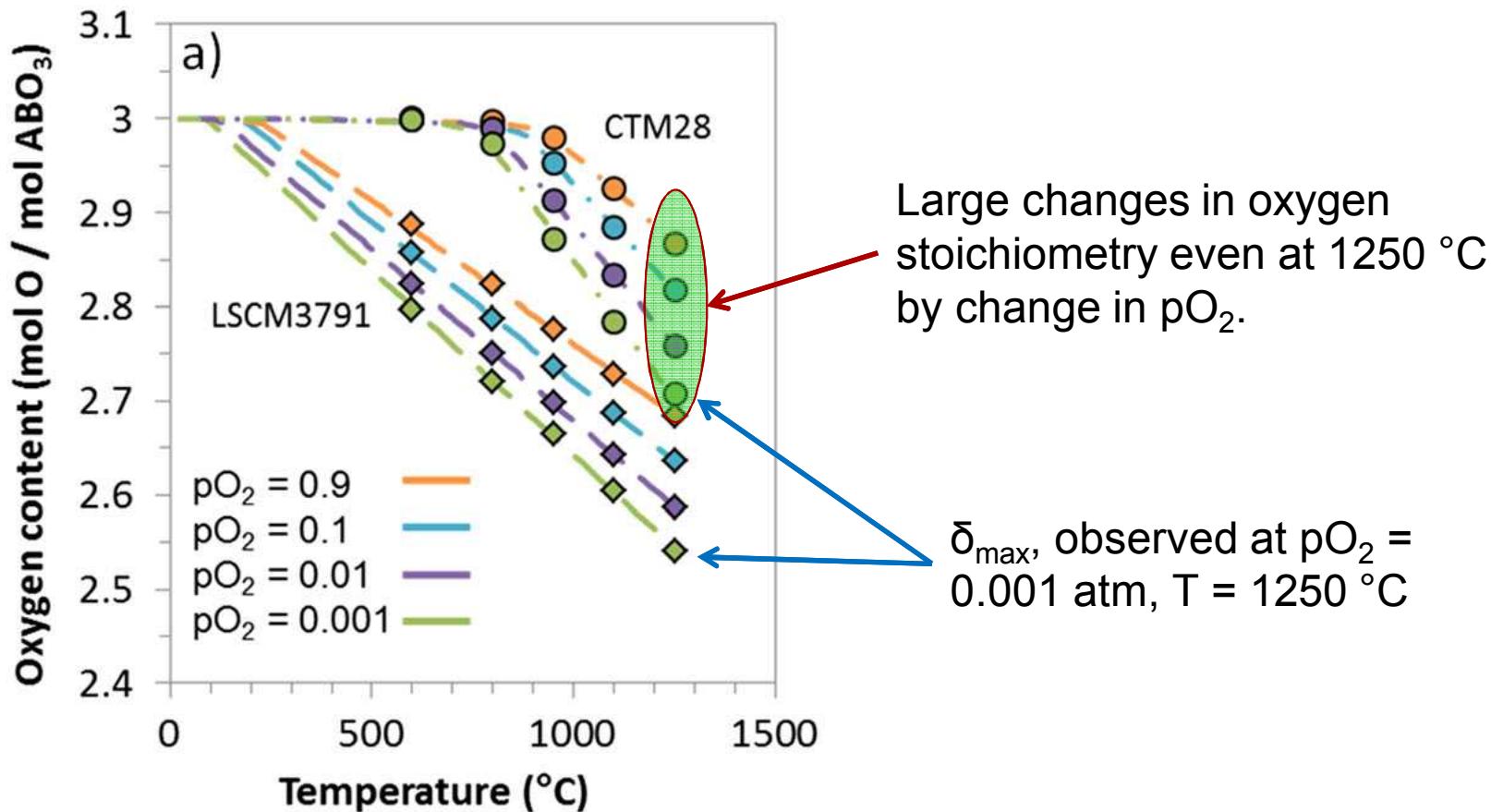


# Thermogravimetric data acquired over range of temperatures and oxygen partial pressures



Thermogravimetric Analysis = TGA

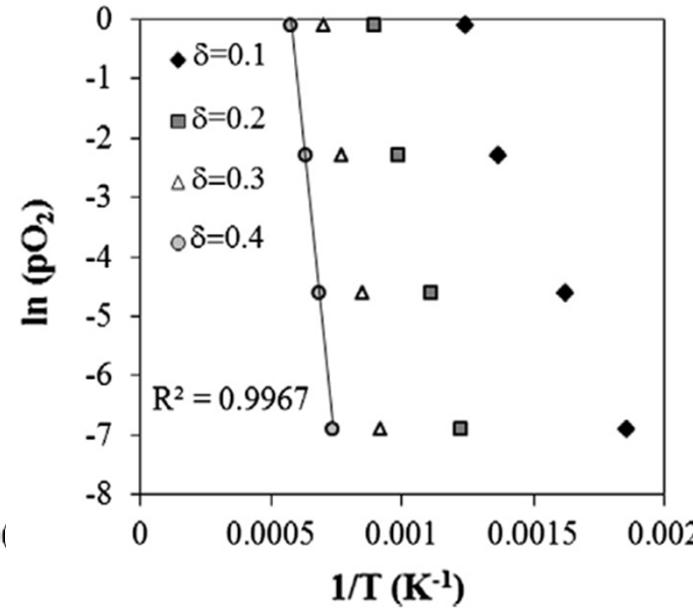
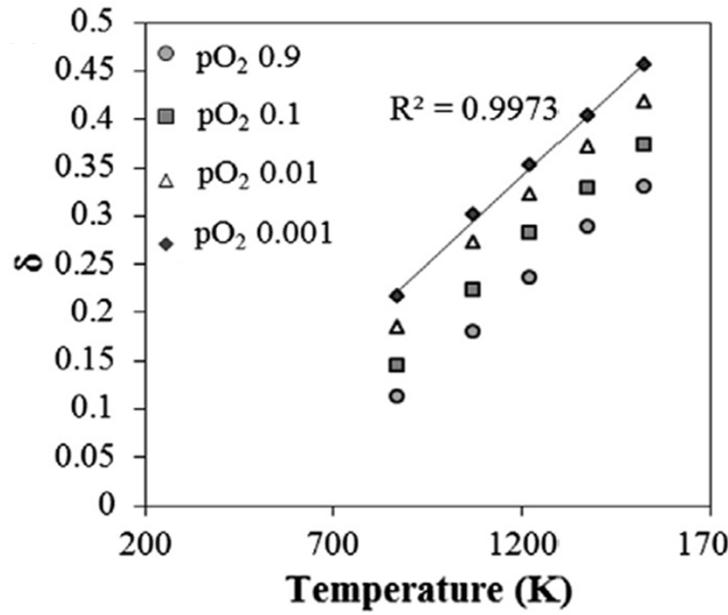
# Equilibrium data taken from TGA experiments



# Equilibrium TGA data used to estimate thermodynamic parameters

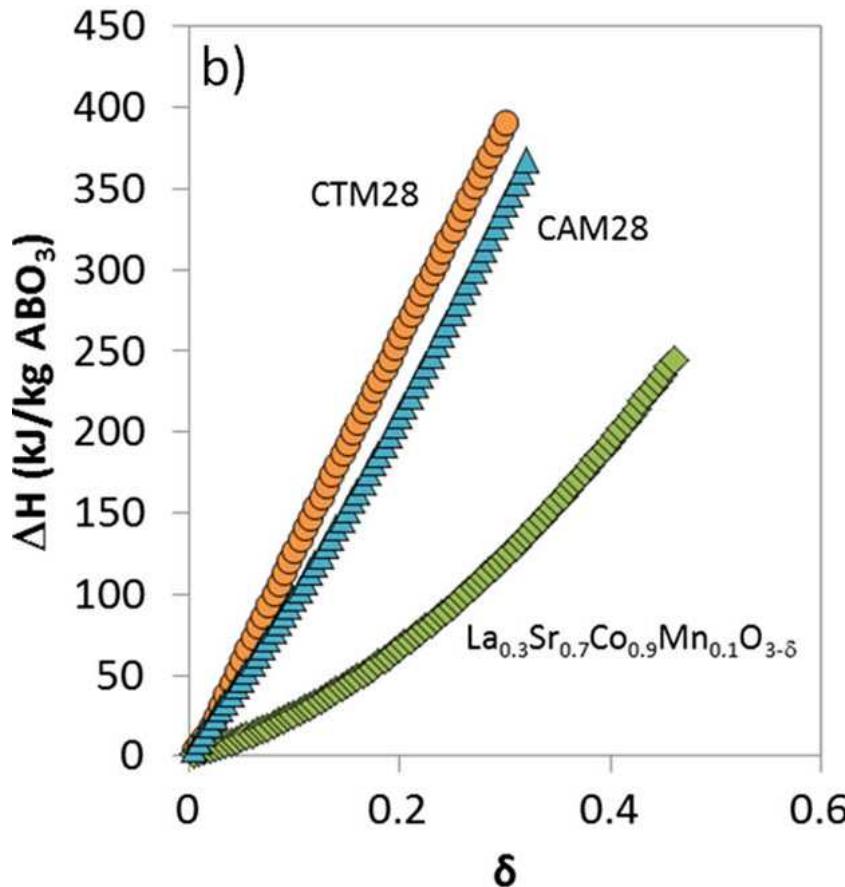
- Thermodynamic parameters extracted by van't Hoff approach:

- $K = \frac{[ABO_{3-\delta}]^{1/\delta} pO_2^{1/2}}{[ABO_3]^{1/\delta}}$ , assume ratio of solid activities is  $\approx$  unity
- $\ln(pO_2) = 2 \frac{-\Delta G_{rxn}}{RT} = 2 \left( \frac{1}{T} \cdot \frac{-\Delta H_{rxn}}{R} + \frac{\Delta S_{rxn}}{R} \right)$ 
  - Enthalpy determined by slope, entropy by intercept for each value of  $\delta$



# Enthalpies from van't Hoff are given for a specific oxygen non-stoichiometry

- Describe energy to remove a mole of  $O_2$  at a specific  $\delta$



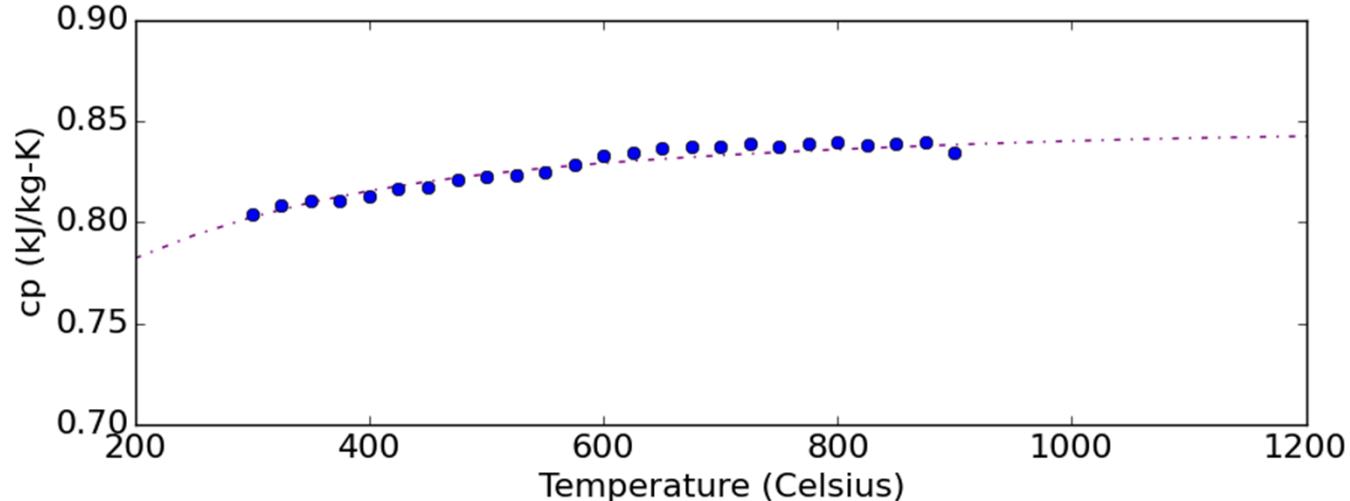
Material	Reduction onset ( $^{\circ}C$ )	Maximum $\delta$	Enthalpy at $\delta_{max}$ (kJ/kg)
LSCM3791	352	0.461	240 <sup>a</sup>
CTM28	901	0.293	390 <sup>b</sup>
CAM28	759	0.322	370 <sup>b</sup>

<sup>a</sup> S.M. Babiniec, et al., *Solar Energy*, **118**, 451–9, (2015).

<sup>b</sup> S.M. Babiniec, et al., *Int. J. Energy Res.*, **40**, 280–4, (2016).

# Heat capacity as a function of temperature is needed to calculate sensible heat

- Einstein heat capacity model used to fit data for CAM28, converted to polynomial fit for ease of integration
  - CTM28 expected to be similar due to same structure and similar molecular weight



$$c_p = a_5 * T^5 + a_4 * T^4 + a_3 * T^3 + a_2 * T^2 + a_1 * T + a_0$$

	$a_5$	$a_4$	$a_3$	$a_2$	$a_1$	$a_0$
CAM28	8.066E-18	-7.169E-14	2.455E-10	-4.070E-7	3.346E-4	7.329E-1

$$\Delta H_{sens} = \int_{T_1}^{T_2} C_p(T) dT = 871 \text{ kJ/kg between } 200 \text{ and } 1250 \text{ }^{\circ}\text{C}$$

$$\Delta H_{total} = \Delta H_{sens} + \Delta H_{reaction} = 871 + 370 = 1241 \text{ kJ/kg}$$

# Discussion/Conclusions

- CAM28 shows high storage enthalpy
  - Sensible + reaction enthalpy is over 1000 kJ/kg
  - Increase in reduction temperature results in larger reaction enthalpy
    - CTM28 and CAM28 show an increase in reaction enthalpy of over 60% compared to the previously studied  $\text{La}_{0.3}\text{Sr}_{0.7}\text{Co}_{0.9}\text{Mn}_{0.1}\text{O}_{3-\delta}$
  - The use of calcium in the A-site instead of lanthanum and strontium will result in significant cost savings

# Acknowledgements

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