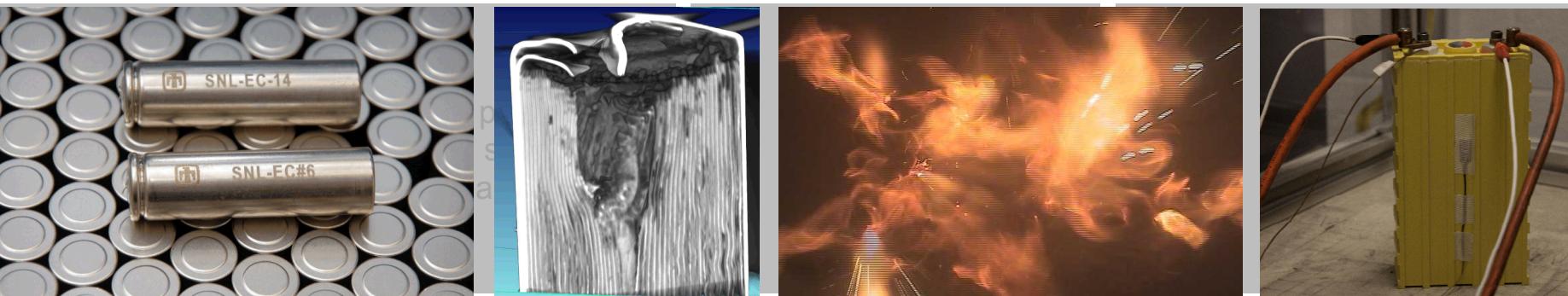


Exceptional service in the national interest



Battery Safety and Abuse Testing at Sandia National Laboratories

Joshua Lamb

January 19, 2016



Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000. SAND NO. 2011-XXXX

INTRODUCTION TO THE BATTERY ABUSE TESTING LABORATORY (BATLAB)

Capabilities and Infrastructure



- ***Battery Abuse Testing Laboratory (BATLab)***
- ***Cell Prototype Facility***
- ***Battery Calorimetry***
- ***Modeling and Simulations***
- ***Materials Development R&D***
- ***Thermal Test Complex (TTC)***
- ***Burn Site, Laurence Canyon***



Thermal Test Complex (TTC)

Understanding Battery Safety



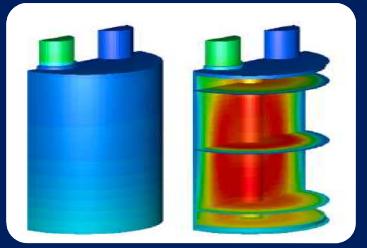
Materials R&D

- Non-flammable electrolytes
- Electrolyte salts
- Coated active materials
- Thermally stable materials



Testing

- Electrical, thermal, mechanical abuse testing
- Failure propagation testing on batteries/systems
- Large scale thermal and fire testing (TTC)
- Development for DOE Vehicle Technologies and USABC



Simulations and Modeling

- Multi-scale models for understanding thermal runaway
- Validating vehicle crash and failure propagation models
- Fire Simulations to predict the size, scope, and consequences of battery fires



Procedures, Policy, and Regulation

- USABC Abuse Testing Manual (SAND 2005-3123)
- SAE/UL procedures and standards
- R&D programs with NHTSA/DOT to inform best practices, policies, and requirements

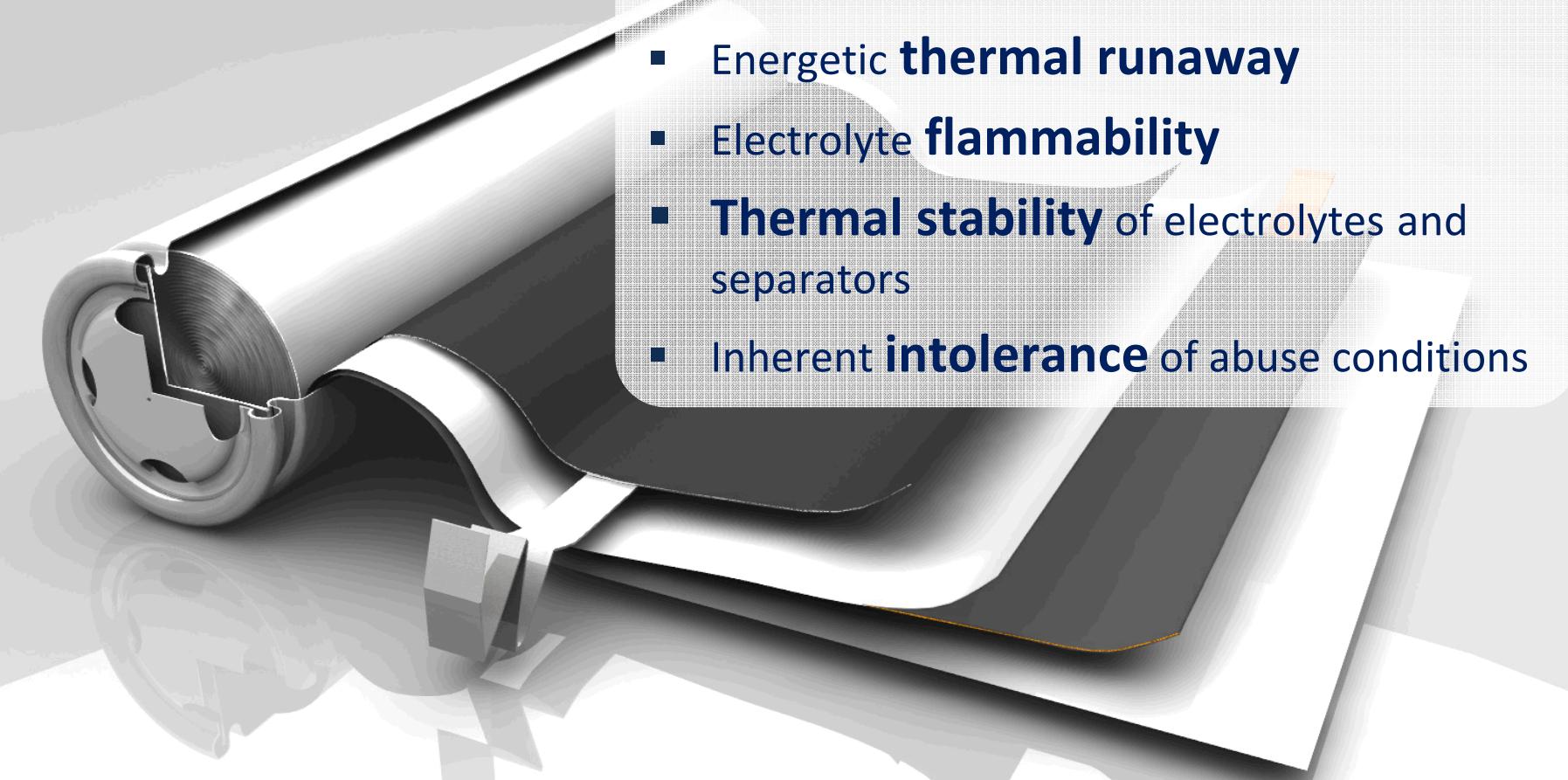
Program Support & Collaborations



Challenges with Lithium-ion Materials

Lithium-ion Materials Issues:

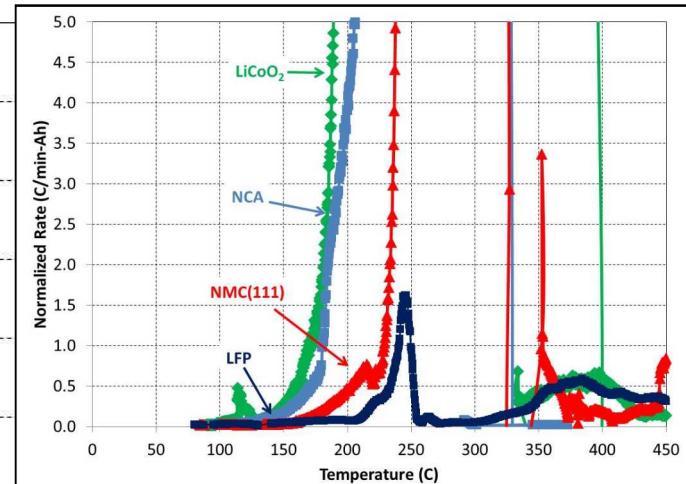
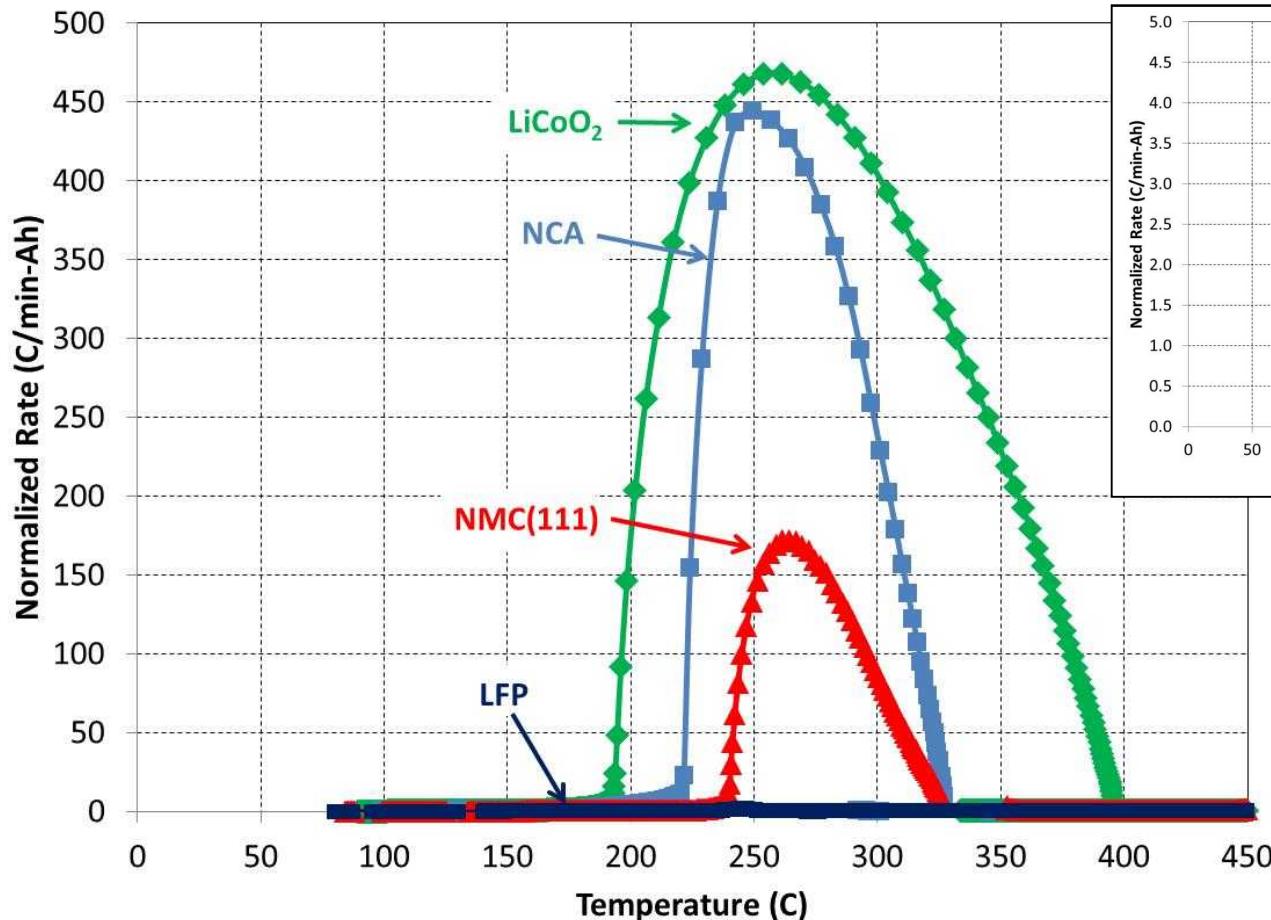
- Energetic **thermal runaway**
- Electrolyte **flammability**
- **Thermal stability** of electrolytes and separators
- Inherent **intolerance** of abuse conditions



Materials choices and interfacial chemistry can impact these safety challenges

Calorimetry of Lithium-ion Cells

Understanding the Thermal Runaway Response of Materials in Cells



High Rate Runaway	
Cathode	$\Delta H_{\text{runaway}}$ (kJ/Ah)
LiCoO ₂	15.9
NCA	9.8
NMC111	8.3
LFP	2.4

*Can high energy cathodes behave like LFP during thermal runaway?
Where do high capacity Si/C anodes fit on this plot?*

MECHANICAL TESTING OF ELECTROCHEMICAL CELLS AND BATTERIES

Lamb, J. and C. J. Orendorff (2014). "Evaluation of mechanical abuse techniques in lithium ion batteries." Journal of Power Sources **247**(0): 189-196.

Field failure vs. abuse failure

Field failure

- Random
- Often the result of manufacturing defects that are difficult to predict or recreate
- Historically the greater concern to battery manufacturers

Abuse failure

- Caused by an external stimulus that pushes a cell outside its safe operating conditions
- Can generally be grouped as: Thermal, Electrical and Mechanical abuse
- Traditionally a laboratory curiosity – performed due to convenience rather than accurate recreation of conditions



Internal Shorts and Mechanical Testing

- Internal short circuit is still the primary cause of field failure in cells
- Nail penetration is the traditional test used due to the lack of an accepted method to create internal short circuits
 - Often approached simply as a test that must be passed
- Few systemic evaluations of mechanical testing exist

Mechanical ISC techniques

Blunt rod- first used by UL and NASA

Nail penetration

Crush

Motorola/ORNL – spherical pinch

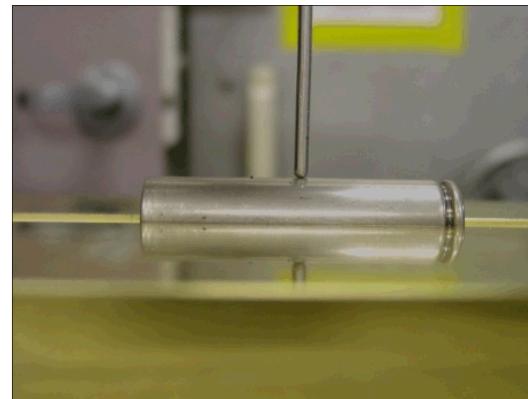
SAE J2464 (ISC test omitted)

Internal short triggers

TIAX – internal defect w/cycling

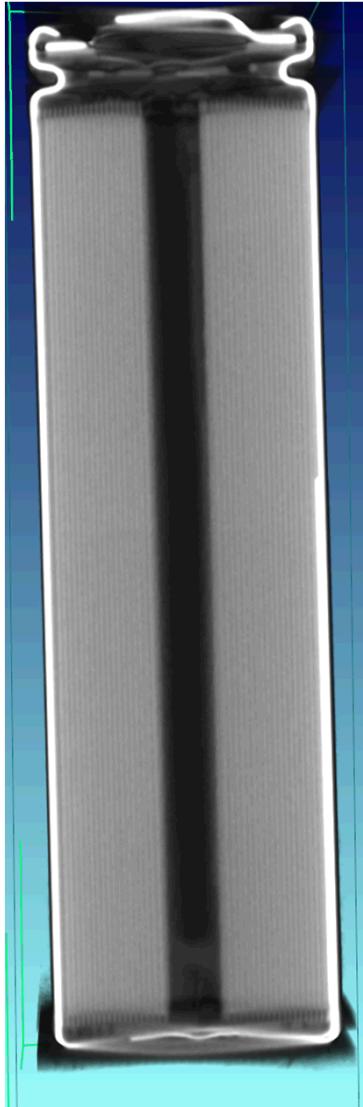
SNL – low melting point metal

Saft – internal heater



DOE testing programs have a vested interest in evaluation of various ISC testing methods. Historically, the SNL viewpoint is that mechanical techniques are not representative of ISC, but may be useful as a runaway trigger

Testing methods



Differences in basic cell construction may lead to differing responses to abuse conditions

- Presence/absence of center rod
- Dead space in can
- Differing size/position of negative tab

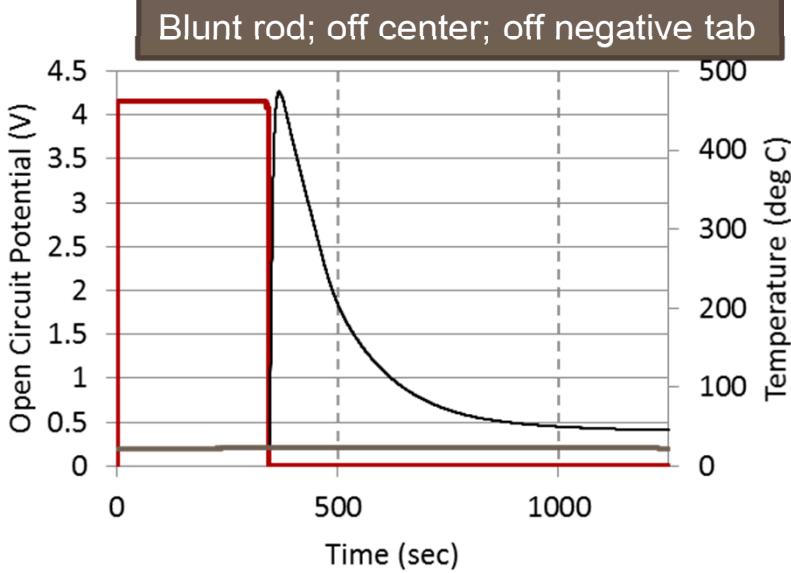
Test conditions		
Speed	2 mm/min	
Construction	316 SS	
Nail Tip	5 mm	
Temperature	RT	60C
	100 mV	20 mm
End Conditions	drop	penetration

Cell type A

Cell type B

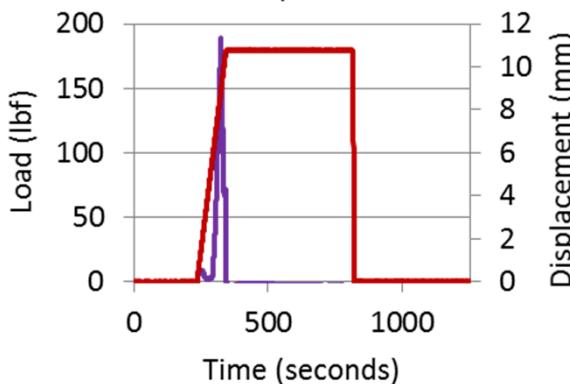


Results: Axial Loading



— Open Circuit Potential — Cell Temp

— Ambient Temp



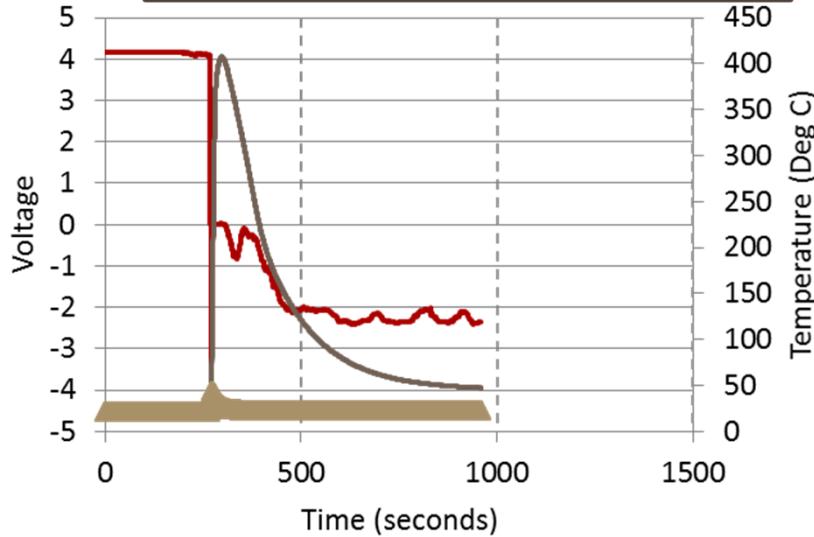
— Load — Displacement



- Resulted in hard short with high temperature and sharp drop in voltage
- Not shown: crush directly on center difficult to fully short as rod passed through empty center

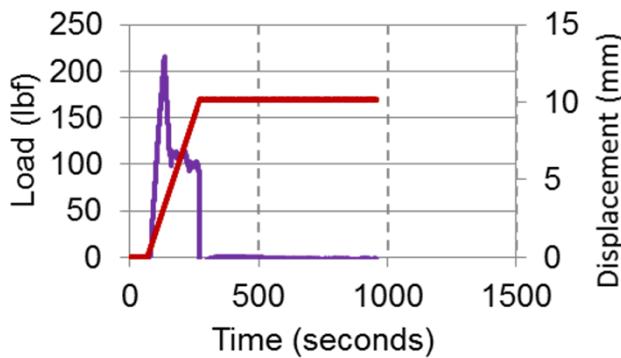
Results: Axial Loading

Blunt rod; off center; on negative tab

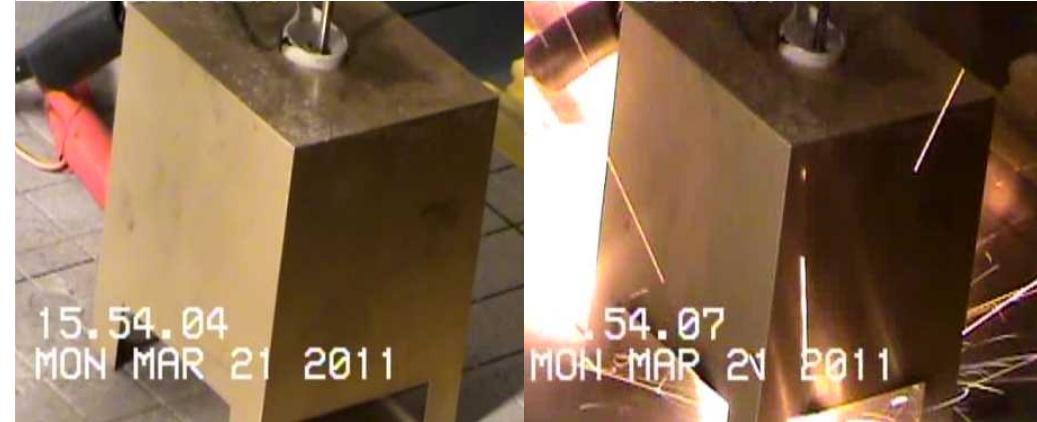


— Open Circuit Potential — Cell Temp

▲ Ambient Temp



— Load — Displacement



- Noisier voltage curve after short
- Hard short occurs shortly after penetration

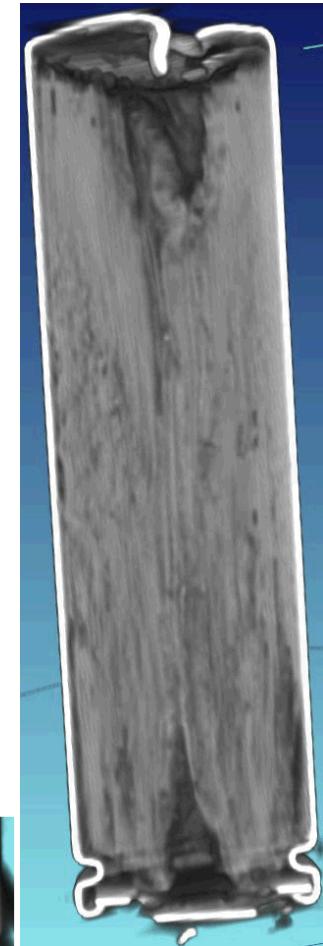
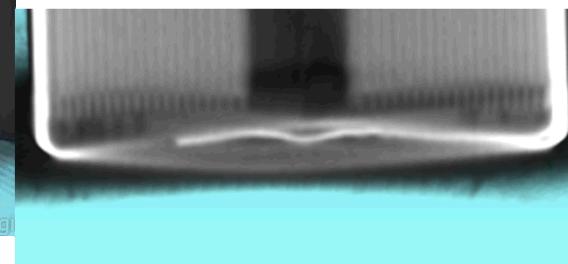
Internal damage – Axial load

Blunt rod; off center; off negative tab

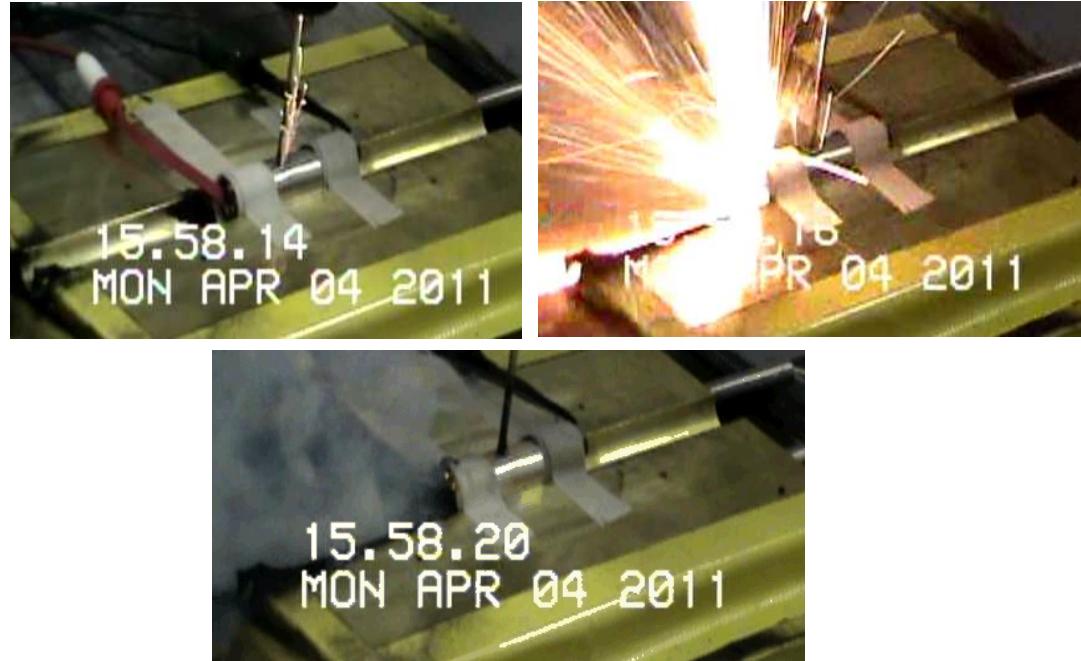
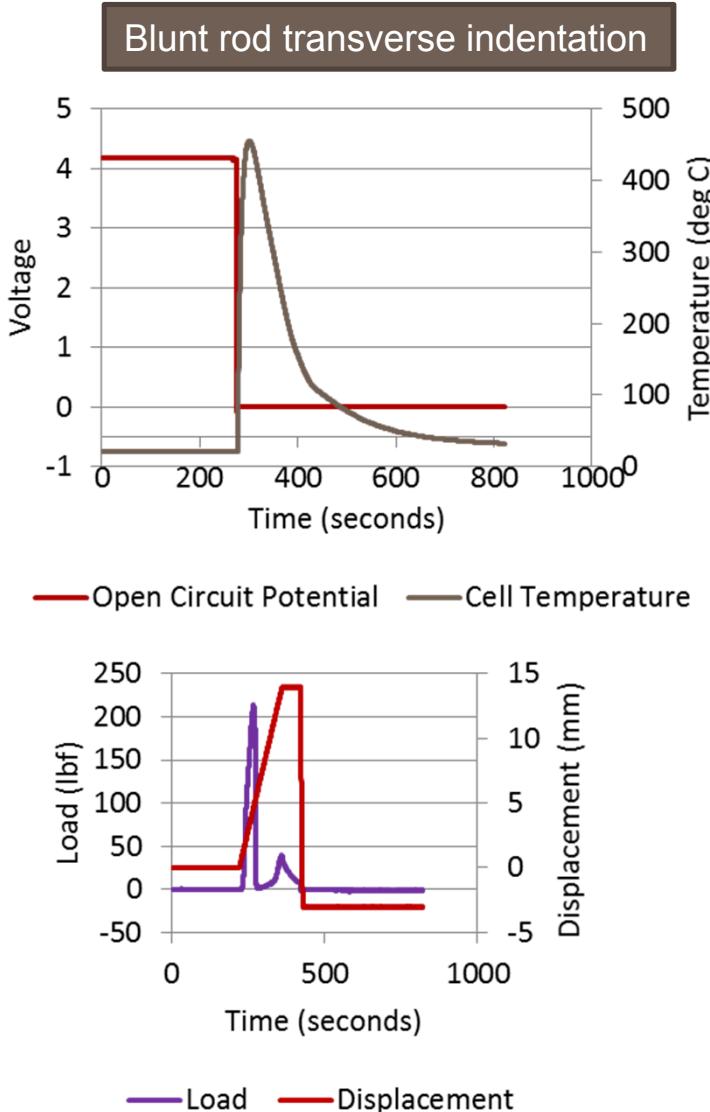


Short location

- Propagation of short through cell towards vent. Damage becomes more extensive near vent from flow of escaping gas
- Large gap between can and electrodes prevent contact without cell puncture
- Limited use for internal short circuit due to large degree of cell damage before short, but reliable runaway initiation

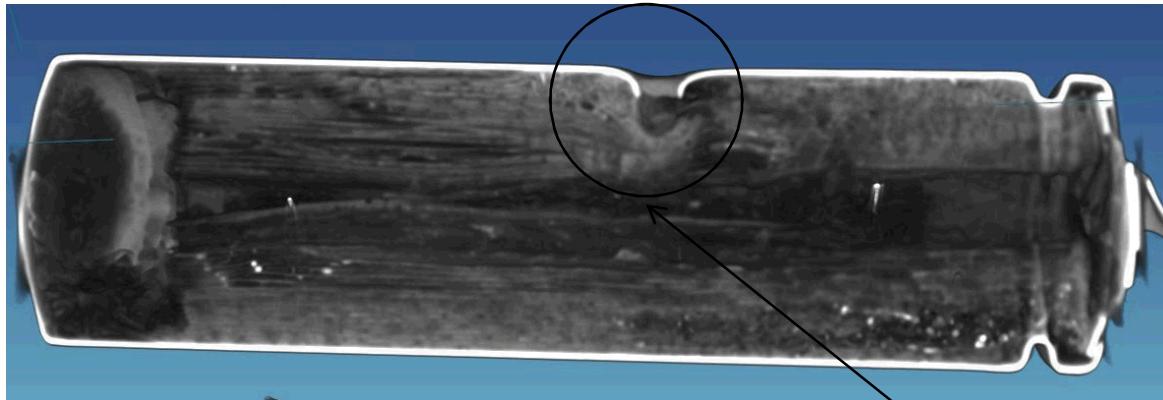


Results: Transverse load

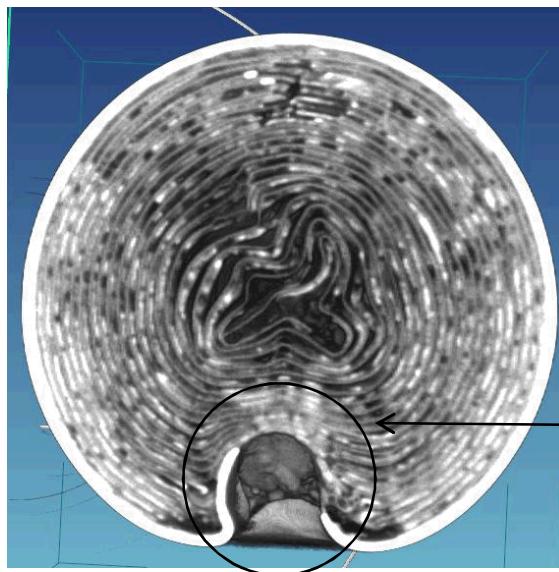


- Cell type A: no internal core
- Catastrophic cell failure; all escaping gas comes through puncture or vent

Catastrophic short failure

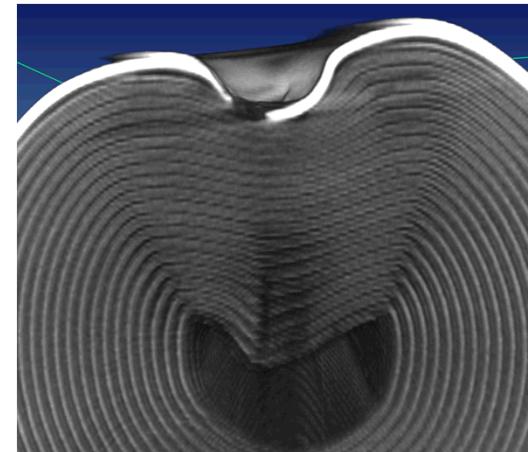
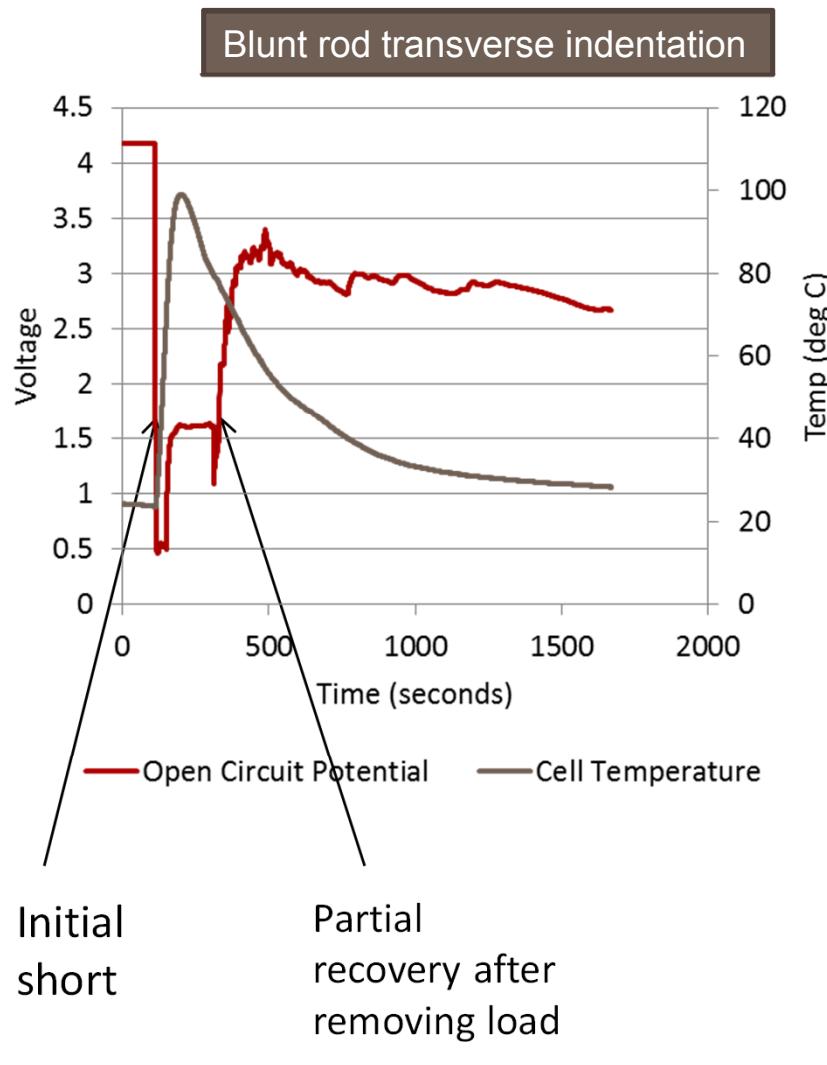


Propagation of failure through cell

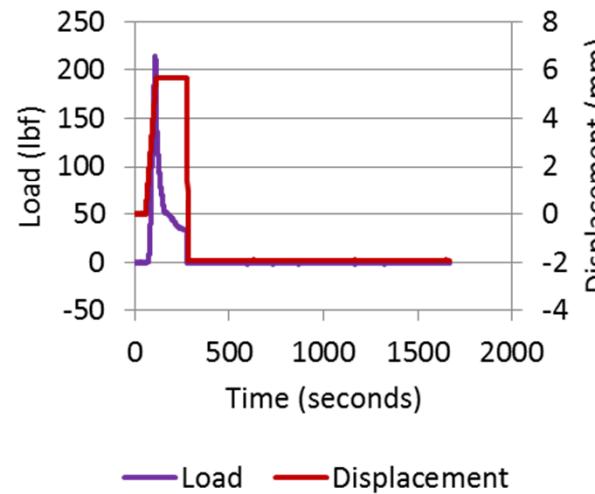


Short location – electrode collapses into core and escaping gas through vent forces jelly roll up towards vent

Failure: Soft short with partial recovery

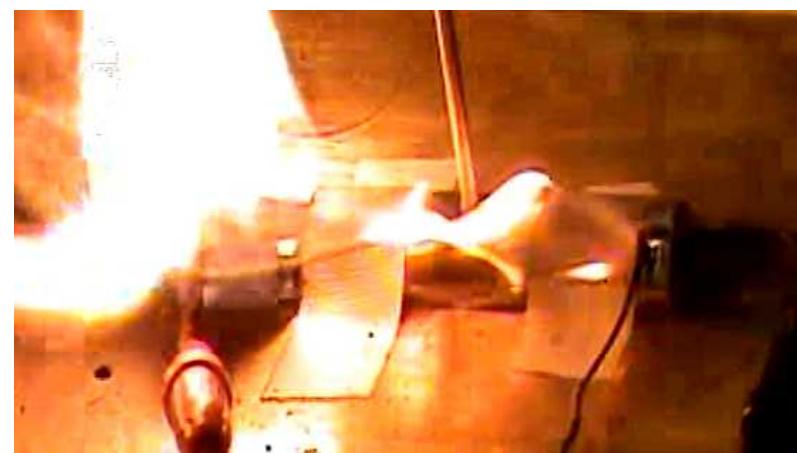
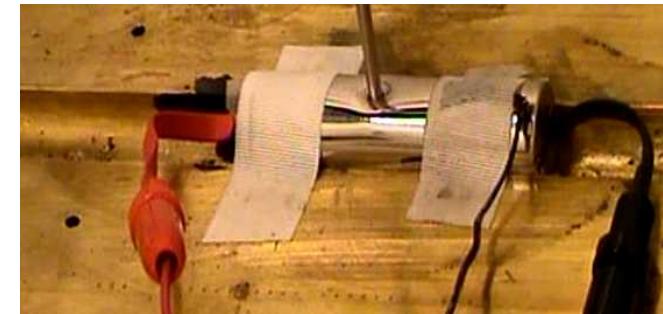
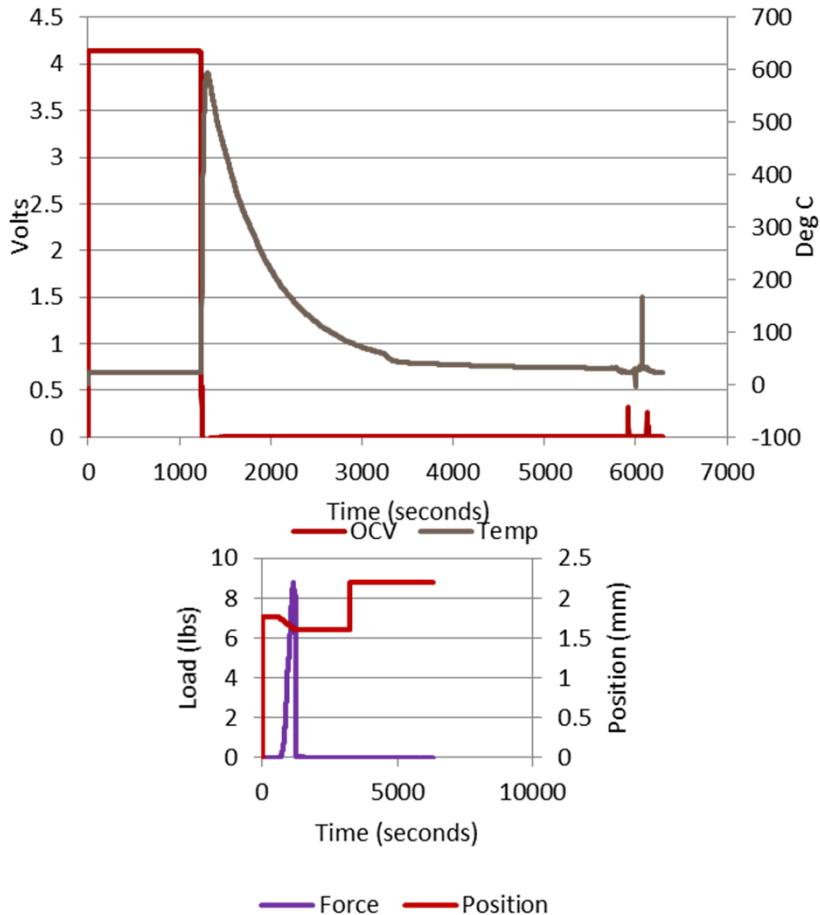


Cell shorting between layers. Electrode is able to deform and collapse into open space in core of cell.



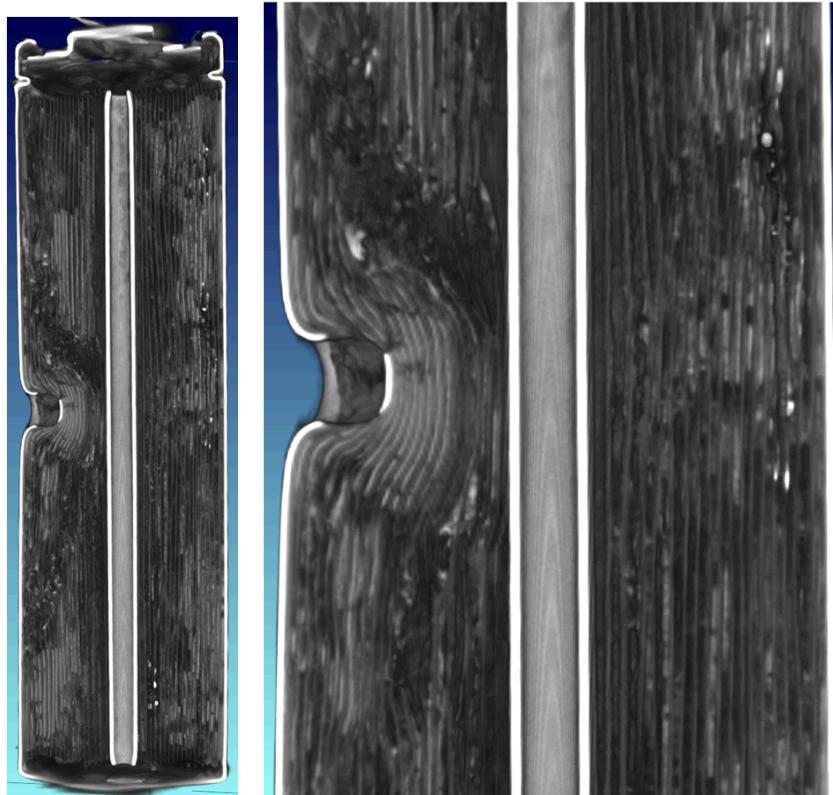
Effect of Cell construction: Cell type B

Blunt rod transverse indentation

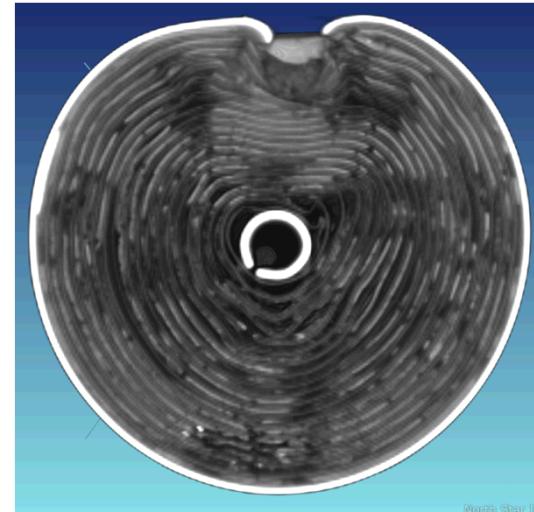


- Catastrophic failure readily seen
- Very high temperatures and self ignition

Cell type B continued

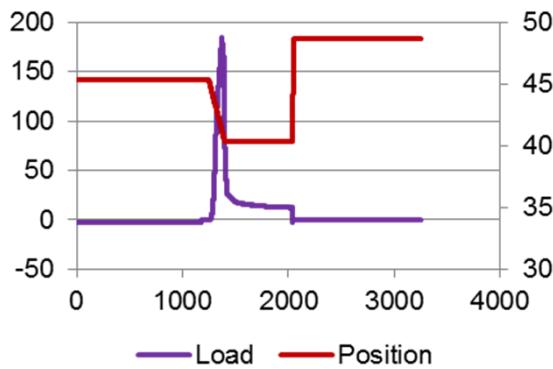
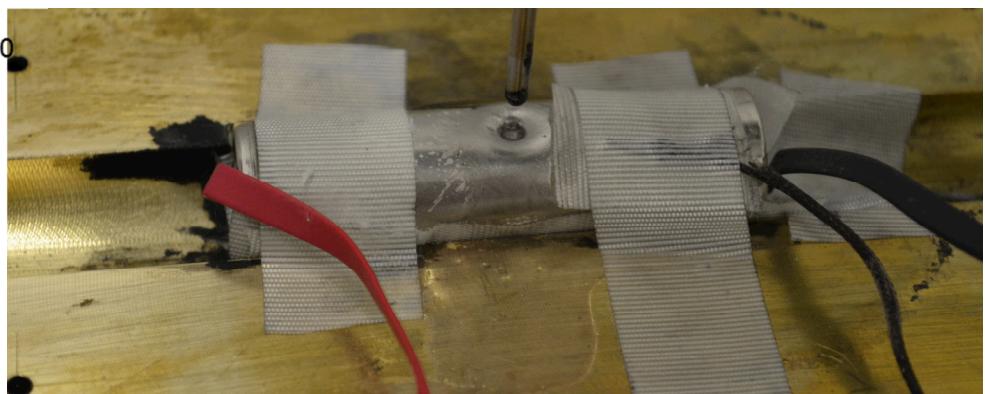
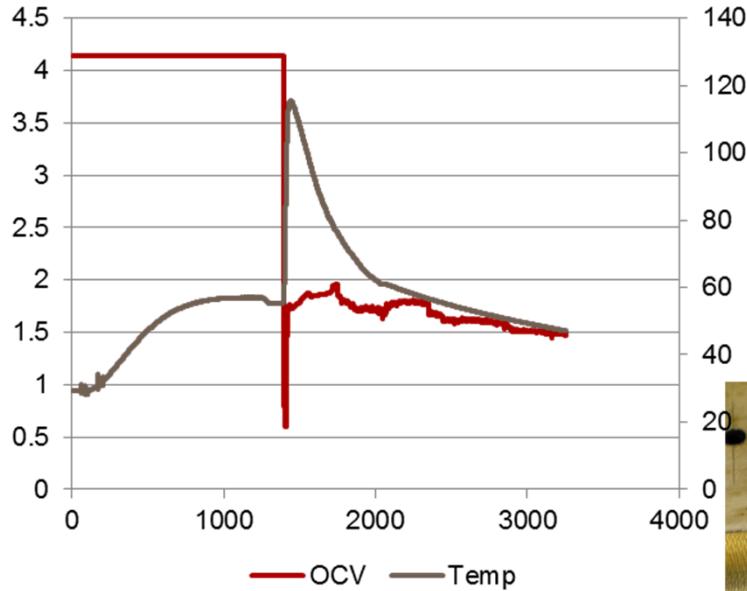


- Center core restricts contents during catastrophic failure
- Creates an effective “backing plate” allowing the electrode to be sandwiched between blunt rod and core



Elevated temperature - Cell type A

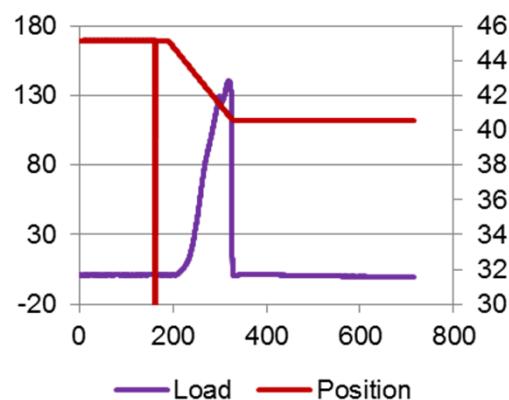
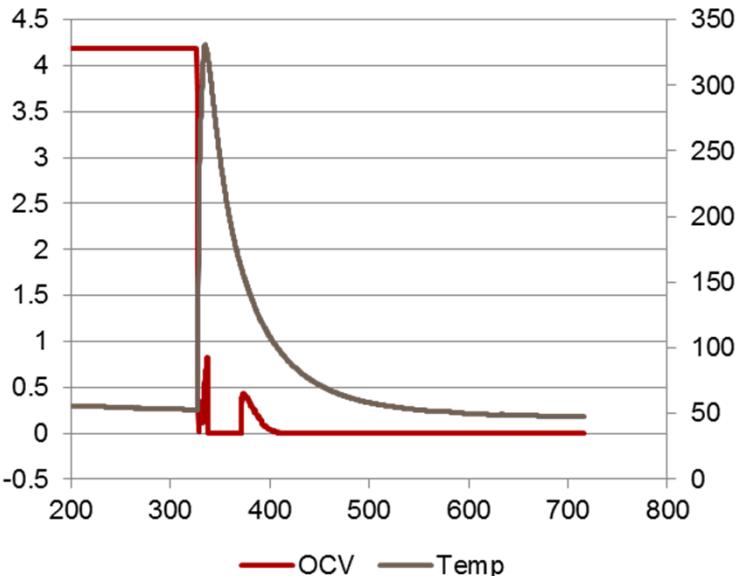
Blunt rod transverse indentation, 50 °C



- Full short observed, but no catastrophic failure
- Repeatedly observe 100 mV drop before catastrophic failure occurs

Elevated temperature – Cell type B

Blunt rod transverse indentation, 50 °C

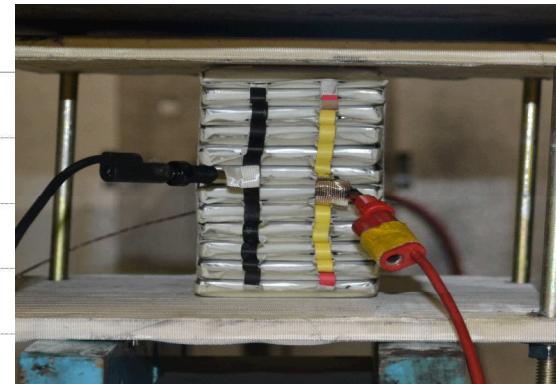
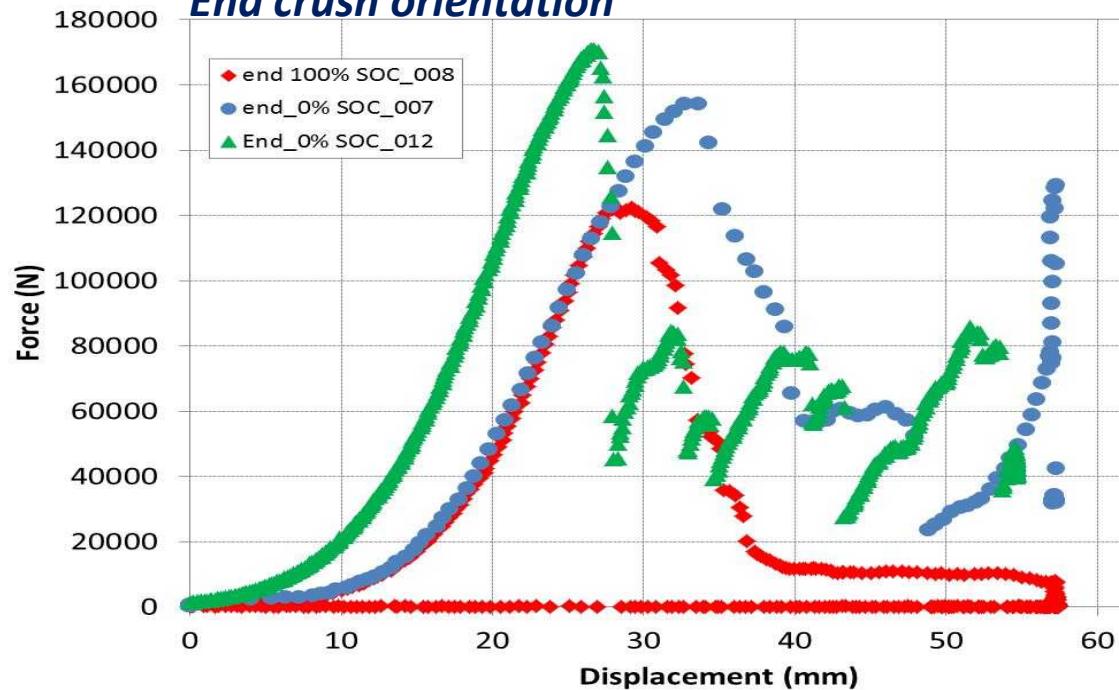


- Very catastrophic failure
- Rupture of can
- Ejection of cell contents

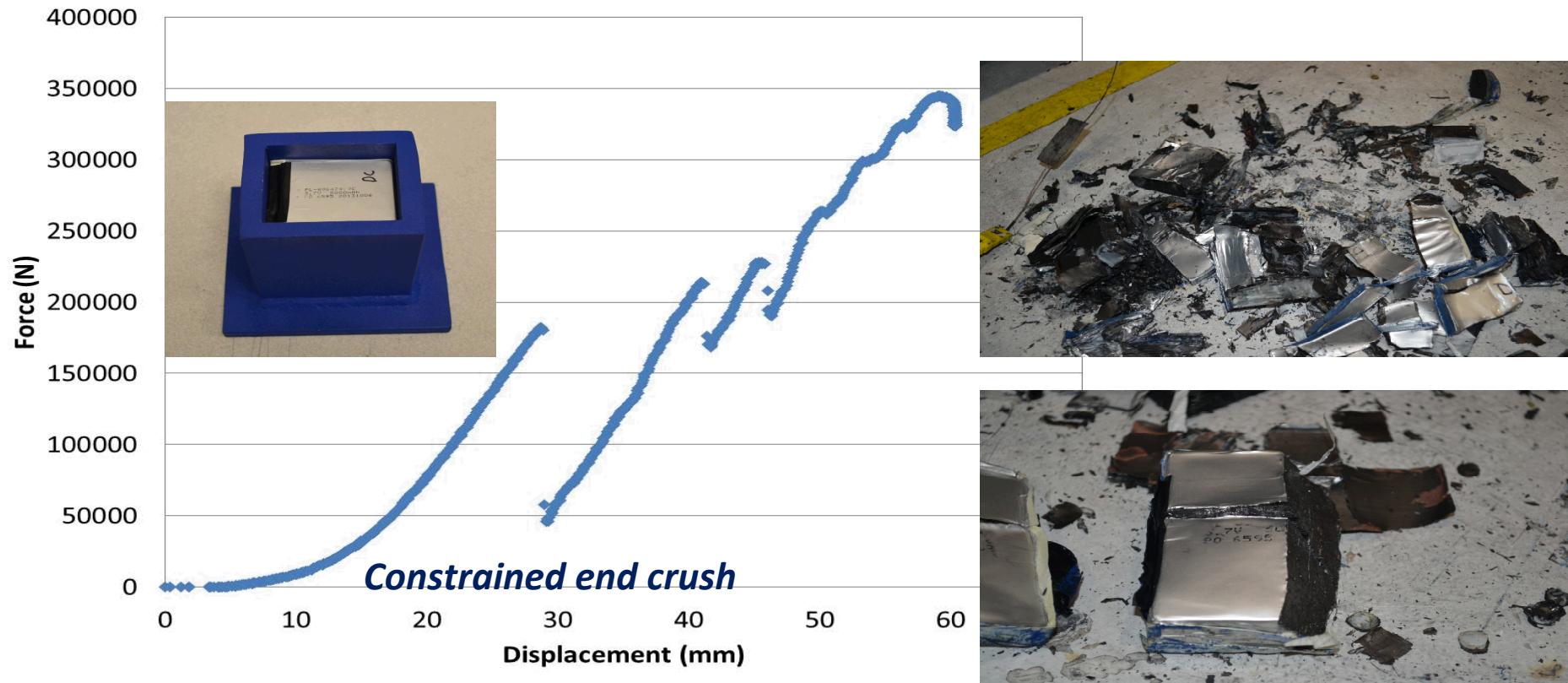
Battery Crash Worthiness

Mechanical testing support of battery mechanical model development

End crush orientation



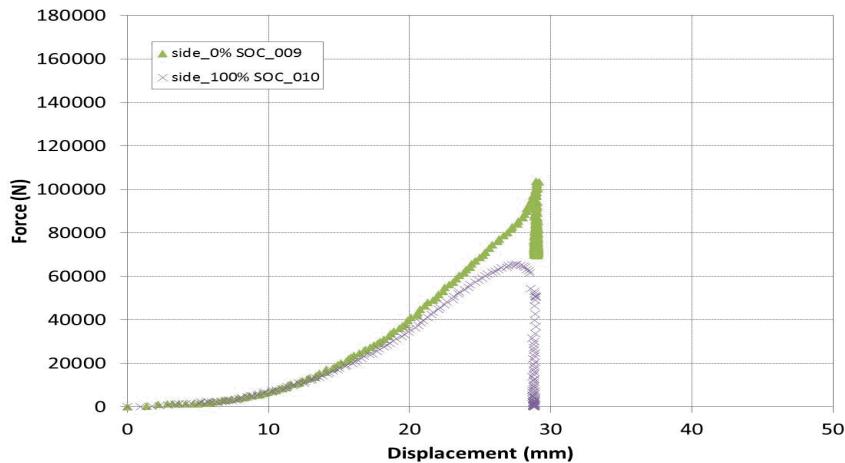
Crash Safety



Fully constrained 12 cell pack (0% SOC) crushed along the longest dimension.

Crash Safety

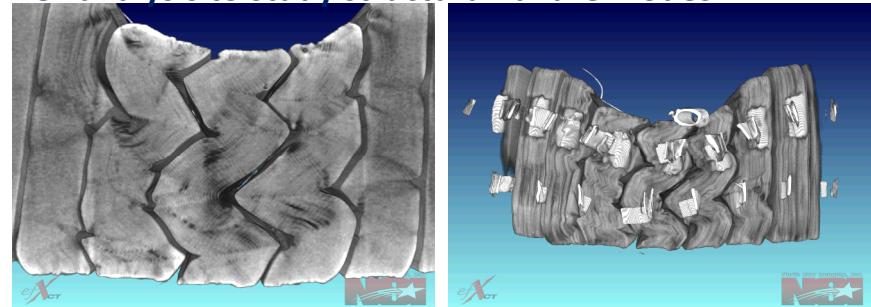
Mechanical behavior under compression



Analog “pole test” of a battery

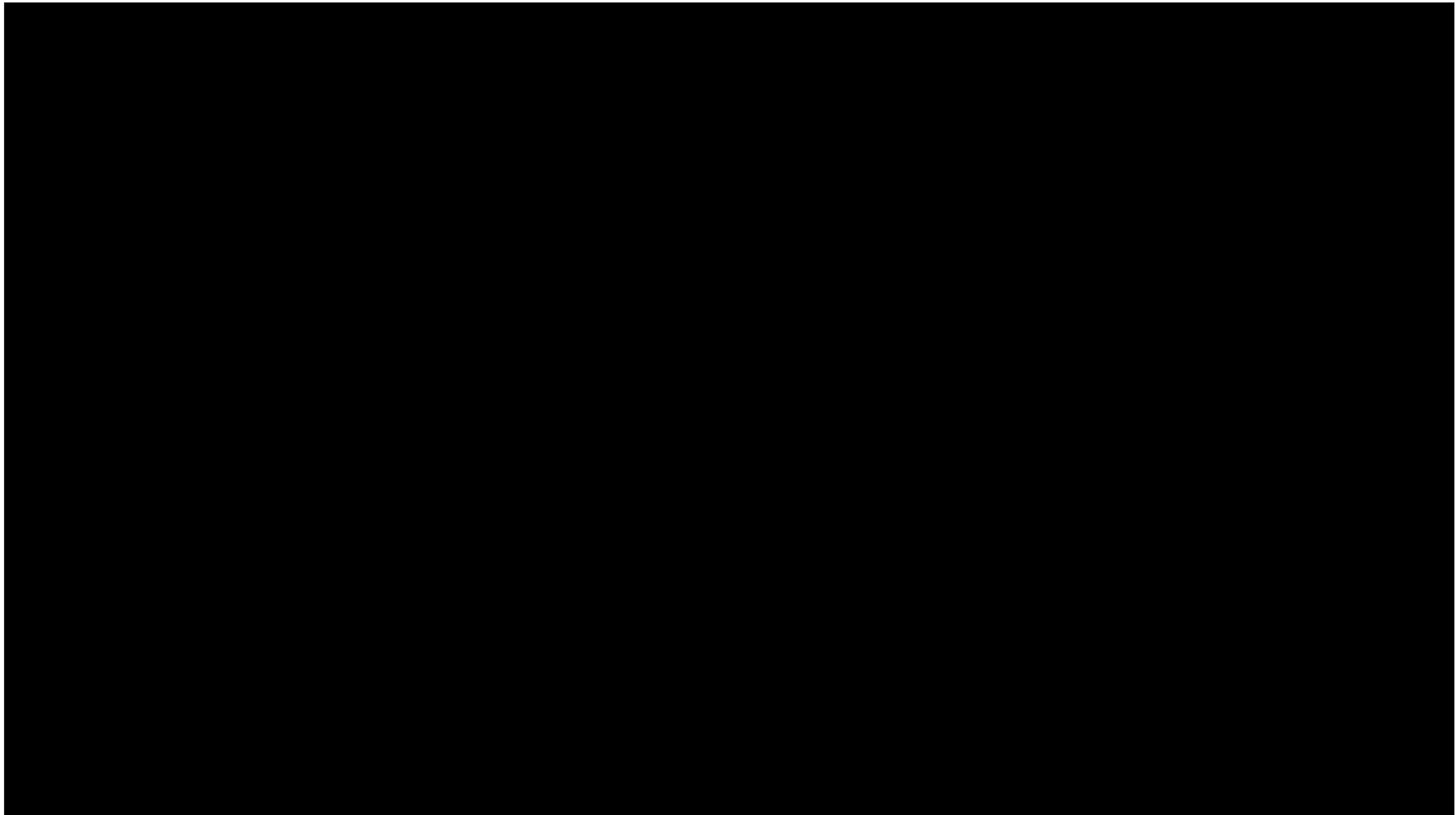


CT analysis to study structural failure modes



*Determining baseline mechanical behavior of batteries during crush/impact testing
Testing support to validate mechanical models for batteries during a crash scenario*

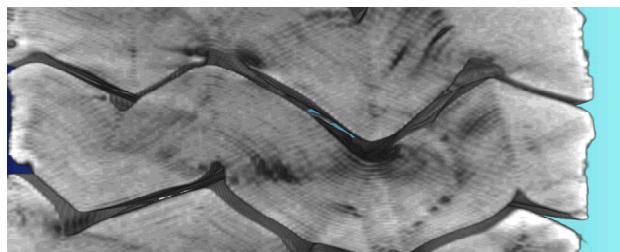
Crush of 1S12P battery



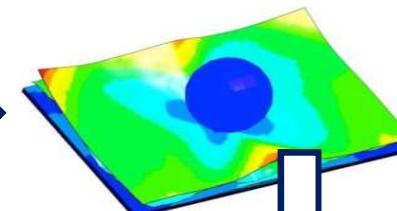
Crash Safety Modeling

Computer Aided Engineering for Batteries (CAEBAT) DOE VTO and NREL

Battery Crush Experiment (SNL, USCAR)



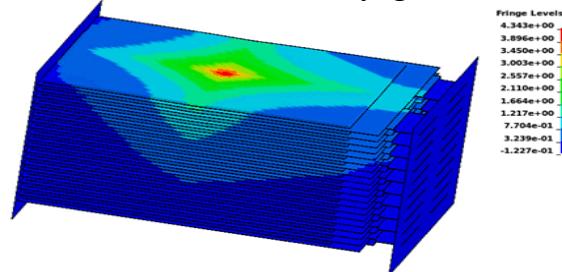
Cell-level Mechanical Model (MIT)



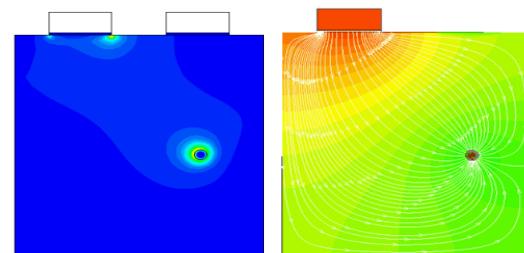
Current density
contour and vector

Integrated Thermoelectrochemical & Mechanical Model (NREL)

Thermal Cell-to-Cell Propagation Model



Thermoelectrochemical Model



- Use battery crush data to validate the integrated model
- Develop a predictive capability for battery thermal runaway response to mechanical insult

Summary and Conclusions

- Repeatability of mechanical testing dependent heavily on cell construction
 - Differences in manufacture designs can have an effect on results
 - Level of uniformity of manufactured cells may contribute to results
 - Central core restricts expansion of cell contents during catastrophic failure
- Reproducible runaway with axial penetration
 - Candidate technique for propagation through multi cell packs
- Prismatic pouch cells show similar rates of failure
 - More detail on pouch cells in JPS article
- Crush testing of 1S12P shows shearing failure in long direction, buckling failures in shorter directions
- CT scans show how buckling may lead to internal shorting

Acknowledgements

- Technical team
 - Christopher Orendorff
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 - Dave Howell
 - Brian Cunningham
 - Peter Faguy
- DOT- NHTSA
 - Phil Gorney

THANK YOU

Timeline of notable safety events

- 2006- Dell recalls 4.1 million laptops due to fire risk
 - Manufacturing defect in LIB cited as cause
- 2007- Apple laptop fire originating from battery
 - Ultimately leads to 1.8 million unit recall
- 2011 Zotye Electric taxi catches fire
 - Investigation links fire to defective battery
- 2011 – Chevrolet Volt spontaneously ignites 3 weeks after crash testing
 - Cause thought to be leaking coolant from the battery system that ultimately shorted the battery
 - Illustrates the stranded energy problem
- 2011 Fisker Automotive recalls 239 vehicles due to fire risk
 - Risk tied to potential coolant leak
- 2012 BYD e6 electric taxi ignites after being struck at high speed
 - Investigators link fire to high voltage line damage
- 2012 Fisker Karma cited as cause of a garage fire that spread to the attached home
 - A good deal of controversy surrounds this event. The fire inspector cited the vehicle as the origin, however the car was not plugged in and the battery pack remained intact
- 2012 1 Toyota Prius and 16 Fisker Karmas caught fire after being submerged in seawater for an extended period as a result of Hurricane Sandy
 - In both cases damage to the electrical system was cited as the cause of the fires
- 2013 Boeing 787 Dreamliner grounded ~4 months following multiple LIB incidents
 - Cause of battery failures still undetermined