

Fatigue Crack Growth Relationships for Cr-Mo Steels in H₂ Gas: Optimizing Measurements and Implications for Vessel Design Life

SAND2015-5846C

Brian Somerday

Sandia National Laboratories
Livermore CA, USA

Paolo Bortot

Tenaris-Dalmine R&D
Dalmine, Italy

John Felbaum

FIBA Technologies
Millbury MA, USA

ASME 2015 Pressure Vessels & Piping Conference
Boston MA, USA
July 23, 2015



Sandia is a multiprogram laboratory operated by Sandia Corporation, a Lockheed Martin Company, for the United States Department of Energy under contract DE-AC04-94AL85000



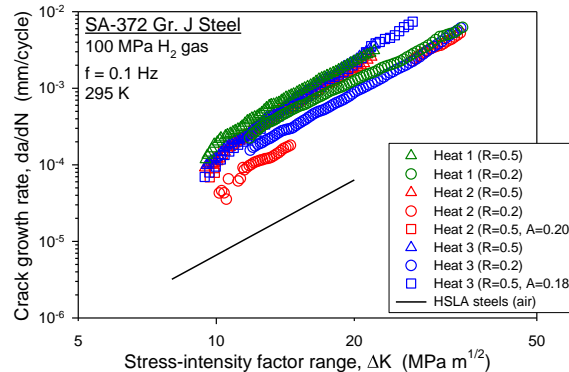
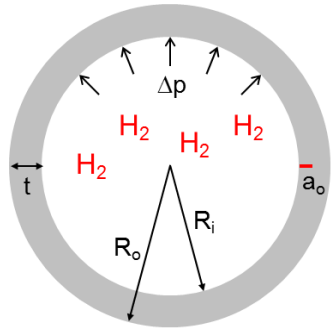
Steel pressure vessels store high-pressure compressed hydrogen at refueling stations



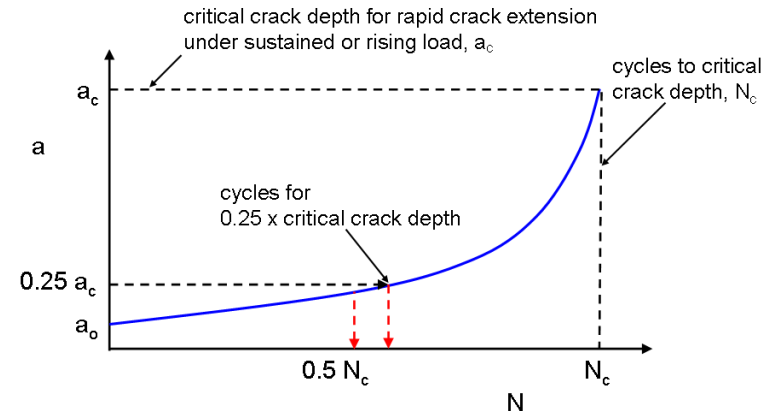
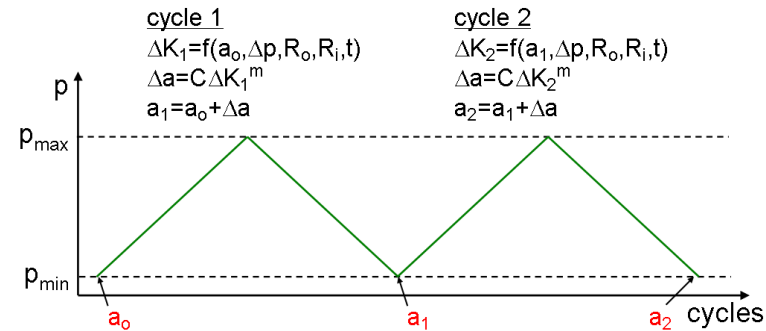
- ASME developed Article KD-10 in Section VIII-3 of Boiler and Pressure Vessel code for high-pressure H_2 vessel design
 - “Special Requirements for Vessels in High Pressure Gaseous Hydrogen Service”
 - Mandatory for seamless vessels with H_2 pressure > 41 MPa and welded vessels with H_2 pressure > 17 MPa (upper limit 100 MPa)

KD-10 requires fracture mechanics measurements on containment materials in high-pressure H_2 gas

Design life analysis in ASME Article KD-10 employs damage-tolerance principles



=

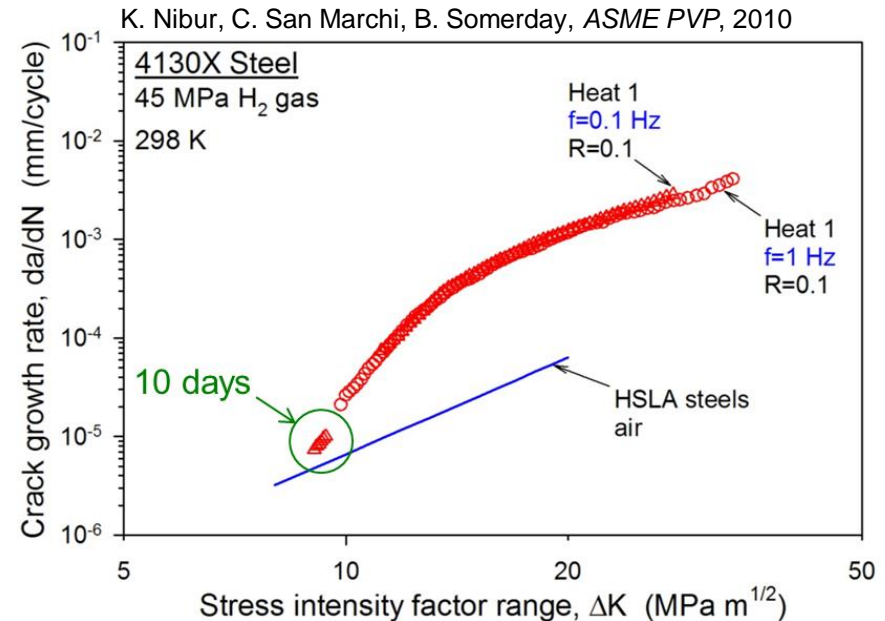
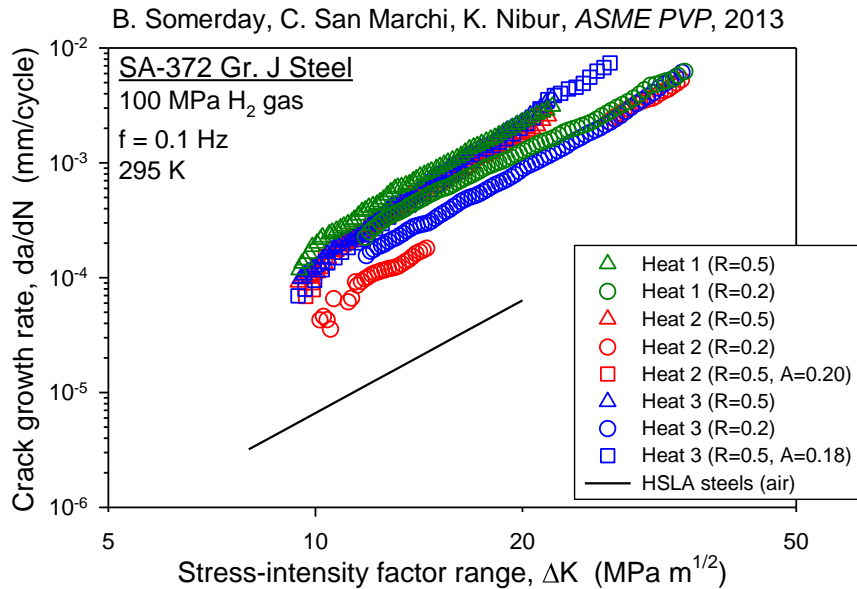


$$\Delta K = \Delta p [f(a, t, R_o, R_i)]$$

$$da/dN = C \Delta K^m$$

Need efficient and reliable measurements of fatigue crack growth relationships in H_2 gas

Measurements on SA-372 Gr. J steel for 1000 bar H₂ vessel design revealed non-optimum test procedures



- Load-cycle frequency prescribed in ASME KD-10 (0.1 Hz) led to compromise in measurements to limit the duration of each test
 - Impractical test durations can arise from test frequency of 0.1 Hz
 - Test durations curtailed by initiating tests at higher ΔK , but extrapolations to lower ΔK excessively inflate da/dN
- **Goal: explore modified procedure that shortens test duration while maintaining data value**

Fatigue crack growth relationships measured for two Cr-Mo steels in high-pressure H₂ gas

• Materials

- SA-372 Grade J ($S_y = 760$ MPa, $S_u = 890$ MPa)
- 34CrMo4 ($S_y = 950$ MPa, $S_u = 1045$ MPa)

• Instrumentation

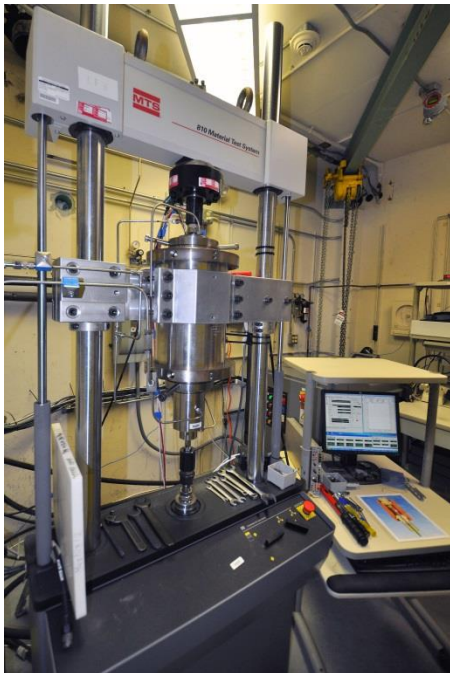
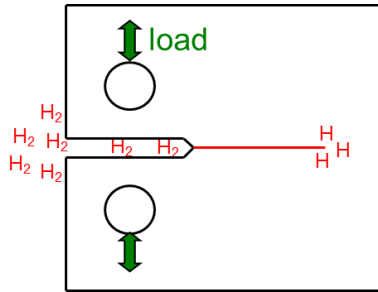
- Internal load cell in feedback loop
- Crack-opening displacement measured internally using LVDT
- Crack length calculated from compliance

• Mechanical loading

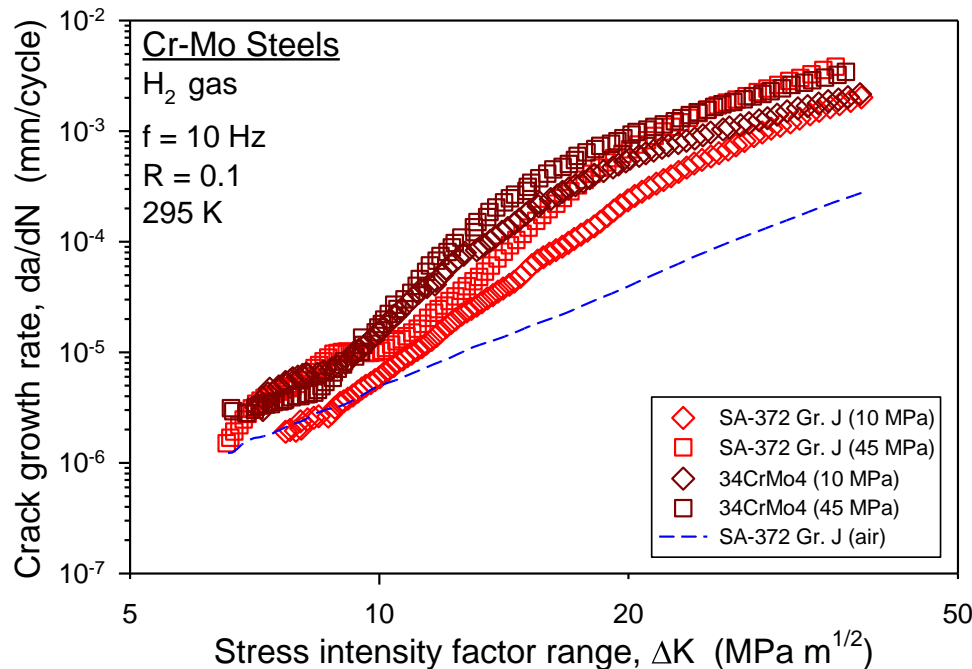
- Triangular load-cycle waveform, frequency range 0.002 to 10 Hz
- Constant load amplitude or constant ΔK

• Environment

- 99.9999% H₂ supply gas
- Pressures = 10, 45, and 100 MPa
- Room temperature

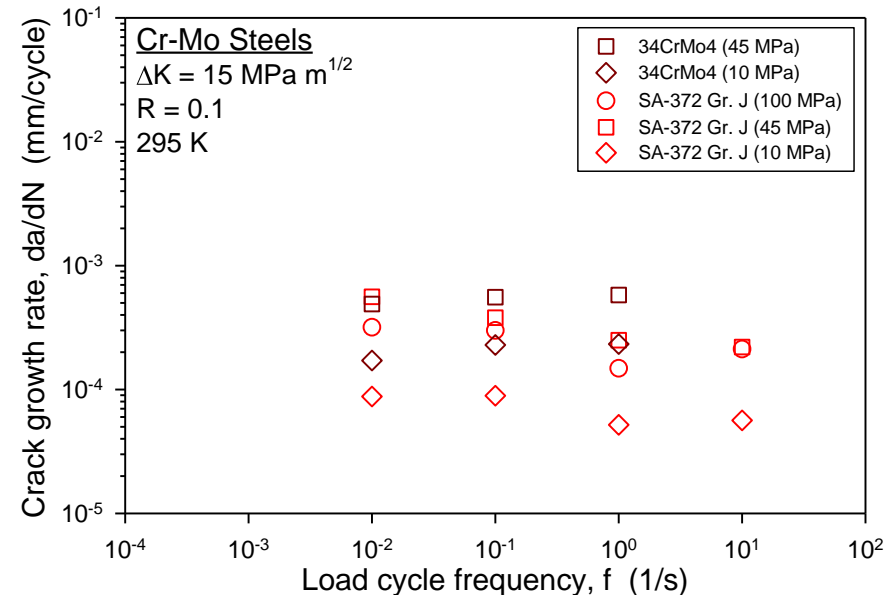
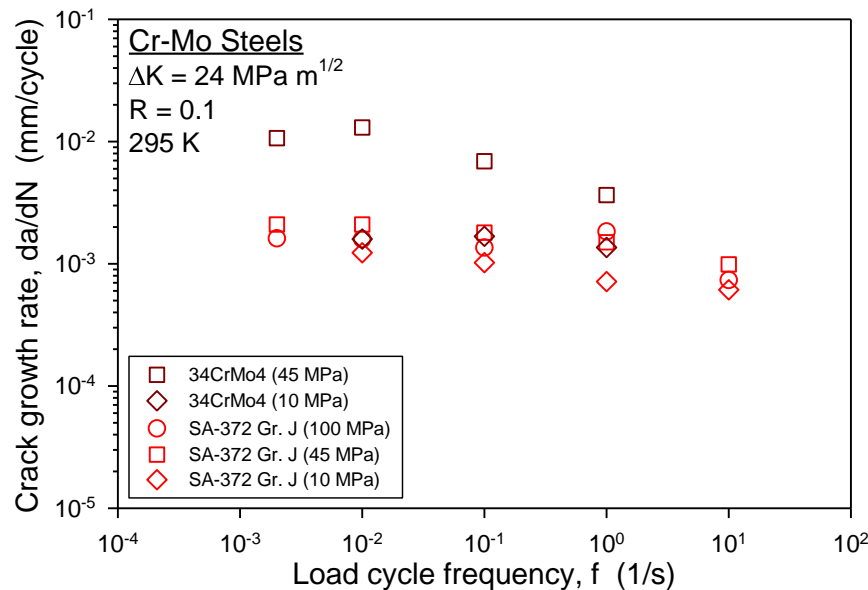


Baseline fatigue crack growth relationships (da/dN vs. ΔK) measured at 10 Hz for two steels



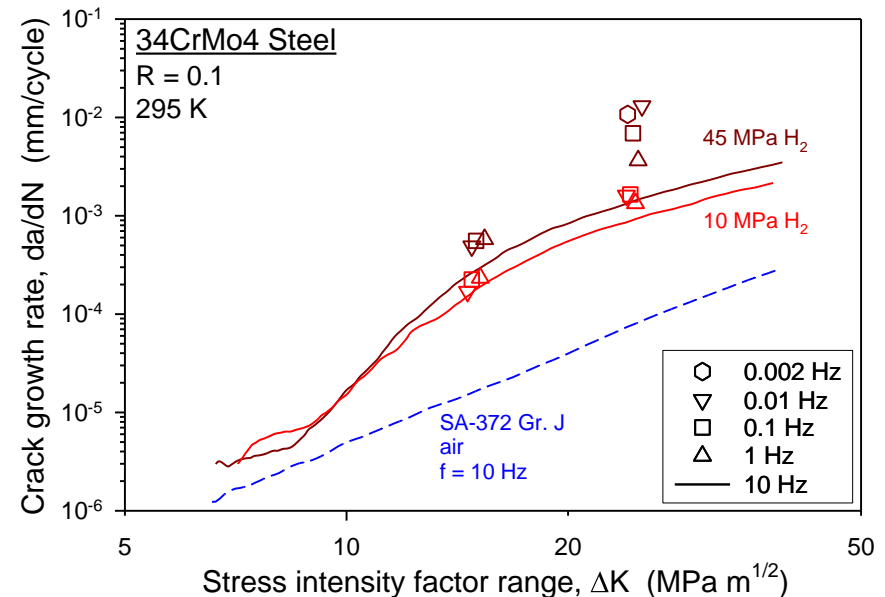
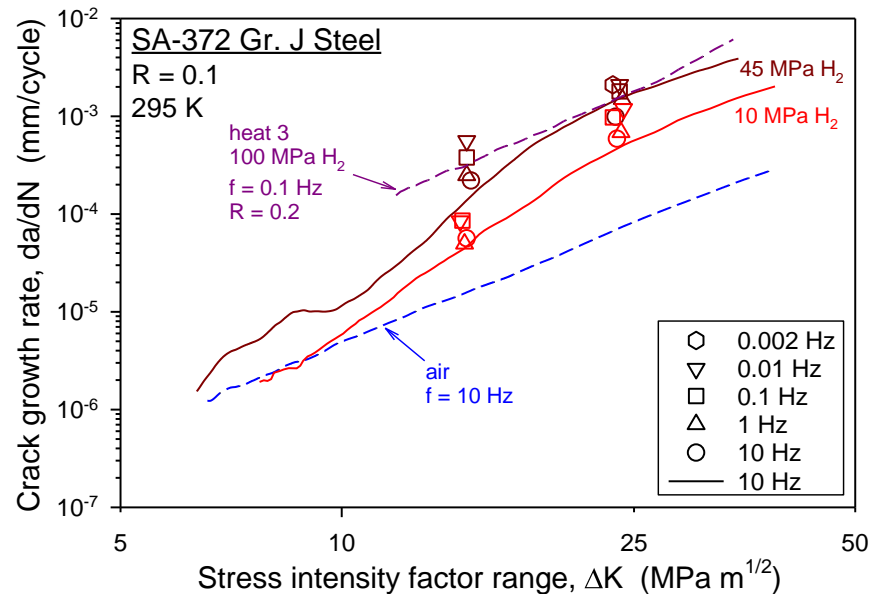
- At higher ΔK , fatigue crack growth rates in H_2 gas $\sim 10\times$ higher than air
- At lower ΔK , fatigue crack growth rates in H_2 gas approach rates in air
 - Measurements at 10 Hz capture essential lower- ΔK data without prolonged testing times
 - *Crack growth rates measured at 10 Hz may not represent upper-bound behavior*

Measurement of da/dN vs. frequency indicates that crack growth rates at 10 Hz are not upper bounds



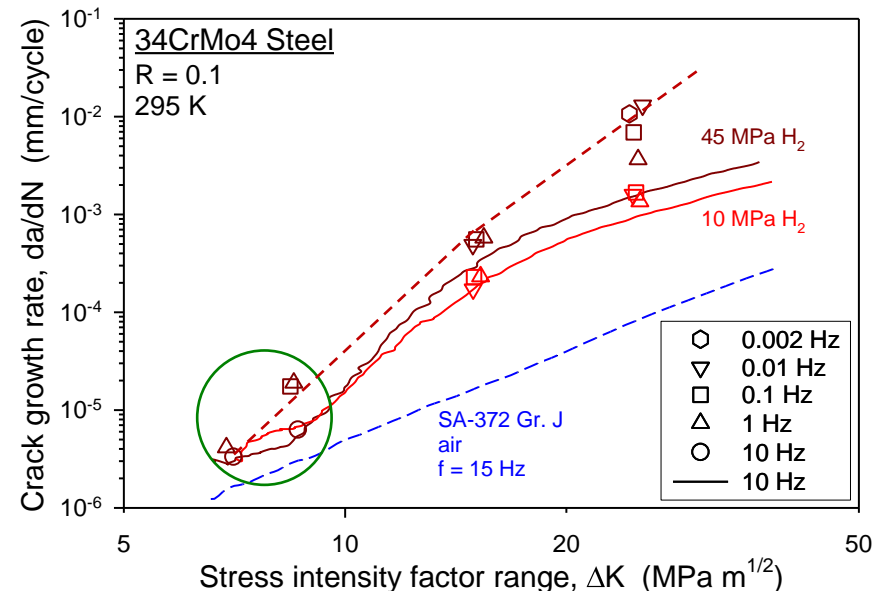
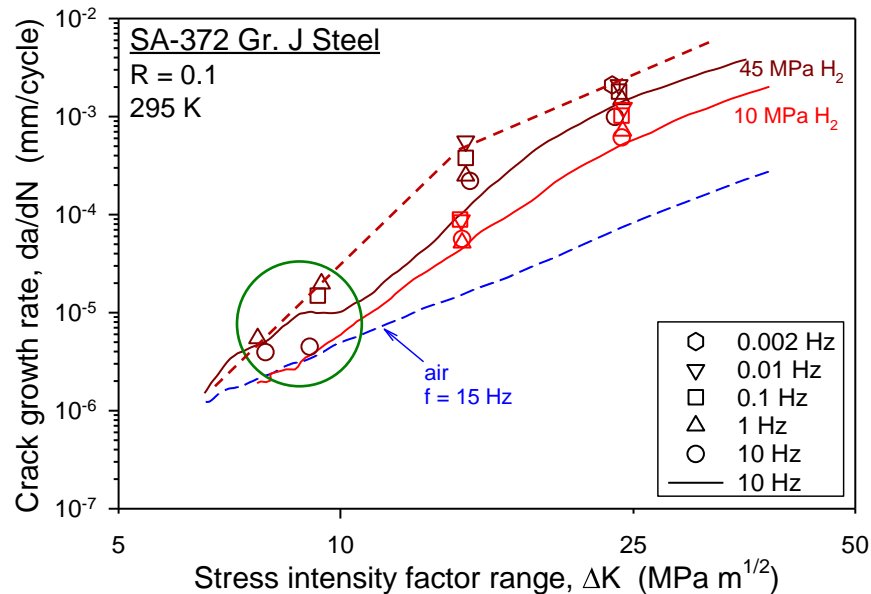
- **General trend: da/dN increases as frequency decreases, then reaches plateau value**
 - Most pronounced for 34CrMo4 steel in 45 MPa H_2 gas at $\Delta K = 24 \text{ MPa m}^{1/2}$
- da/dN vs. f data reveal effects of material and environmental variables
 - Higher-strength 34CrMo4 steel generally more susceptible to hydrogen-accelerated fatigue crack growth than lower-strength SA-372 Gr. J steel
 - Crack growth rates for SA-372 Gr. J steel equal at 45 and 100 MPa H_2 pressure

Possible modified approach: measure da/dN vs. ΔK at 10 Hz, correct data based on da/dN vs. frequency



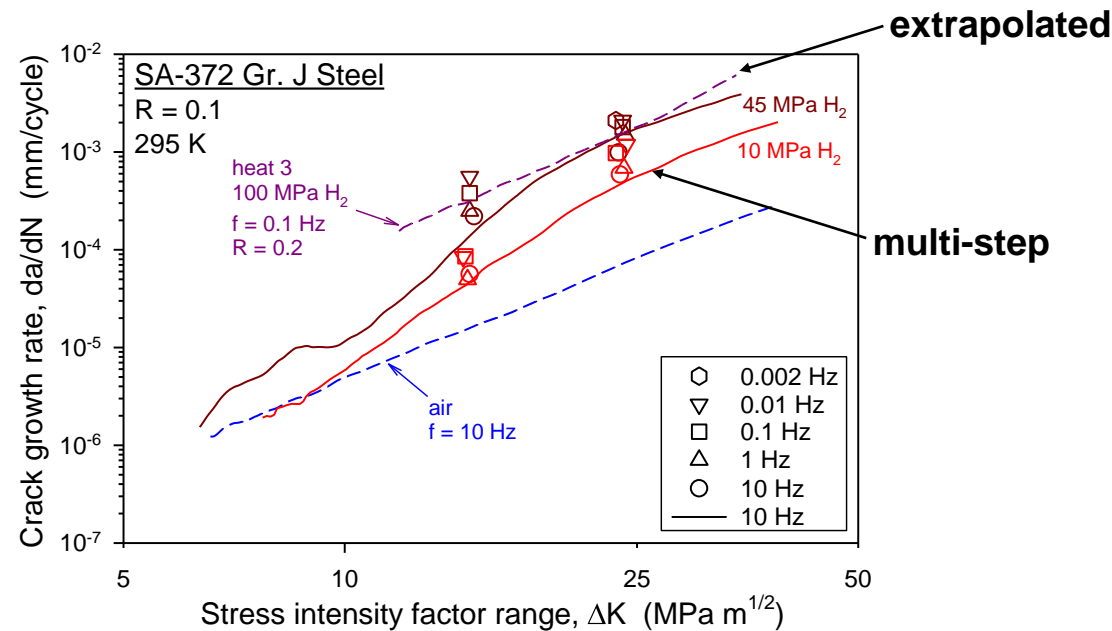
- Baseline da/dN vs. ΔK relationships measured efficiently at 10 Hz, indicate essential regimes that must be represented
 - Baseline relationships reveal that da/dN in H₂ gas approaches da/dN in air
- Since da/dN vs. ΔK relationships are non-conservative at 10 Hz, da/dN vs. f measured at constant ΔK serve as correction to baseline
 - *da/dN vs. f must be measured at multiple ΔK levels to provide most reliable correction → are $\Delta K = 15$ and $24 \text{ MPa m}^{1/2}$ sufficient?*

Additional da/dN vs. frequency measurements at lower ΔK clarify onset of H₂-accelerated crack growth



- Crack growth rate (da/dN) vs. frequency data at lower ΔK verify that da/dN measurements at 10 Hz may not represent upper-bound values
- Corrected da/dN vs. ΔK relationship must reflect onset of H₂-accelerated crack growth at lower ΔK relative to da/dN vs. ΔK curve at 10 Hz
- **Reliable correction to da/dN vs. ΔK relationship measured at 10 Hz must include da/dN vs. frequency data sets measured at lower ΔK**

Fatigue-life analysis for manufactured vessel: consider extrapolated and multi-step FCG relationships



- Double-neck cylinder designed according to EN-1964-1 + 2010/35/EU (TPED qualification)
 - 220 x 9.1 mm (OD x WT min)
 - **MAWP = 28 MPa**
 - Fabricated from 34CrMo4 steel (S_y min = 600 MPa, $780 < S_u < 890$ MPa): not ASME-qualified, but cylinder thickness compliant with Section VIII-2
 - **For fatigue-life calculations, assume SA-372 Gr. J steel**

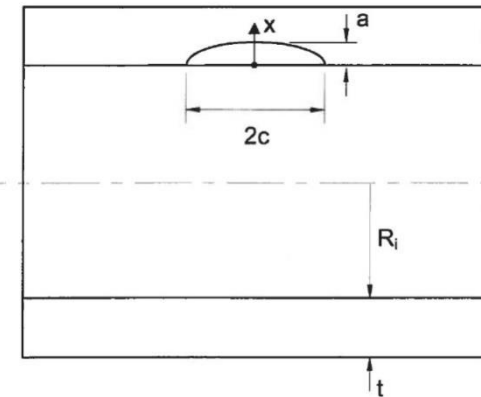
Fatigue-life analysis follows fracture mechanics approach using K solutions from API579-1 / ASME FFS1

Applied K solution for internally pressurized cylinder with longitudinal-oriented, semi-elliptical surface crack

$$K_I = \frac{pR_0^2}{R_0^2 - R_i^2} \left[2G_0 - 2G_1 \left(\frac{a}{R_i} \right) + 3G_2 \left(\frac{a}{R_i} \right)^2 - 4G_3 \left(\frac{a}{R_i} \right)^3 + 5G_4 \left(\frac{a}{R_i} \right)^4 \right] \cdot \sqrt{\frac{\pi a}{Q}}$$

Semi-elliptical defect size and shape:

- Depth: $a = 0.455$ mm (5% min WT)
- Length: $c = 1.365$ mm ($a/2c = 1/3$, as specified in KD-4)



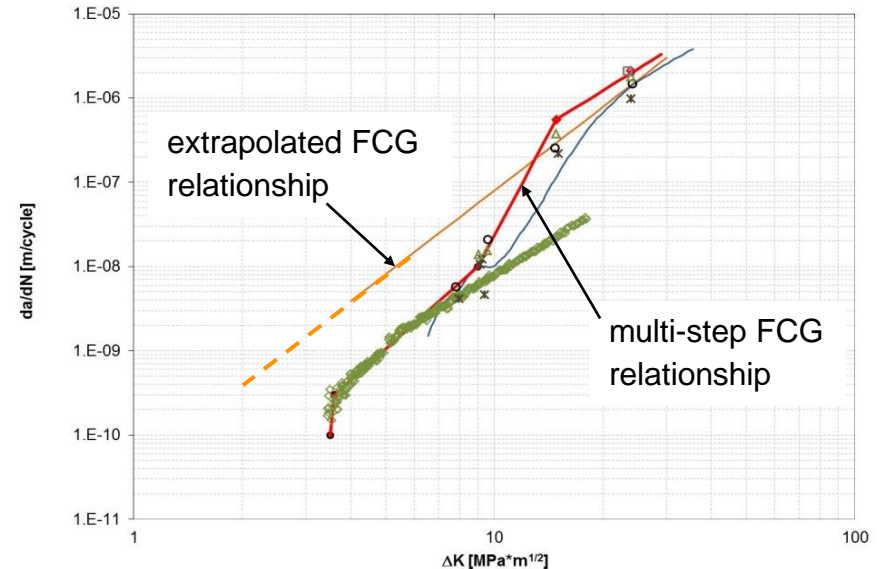
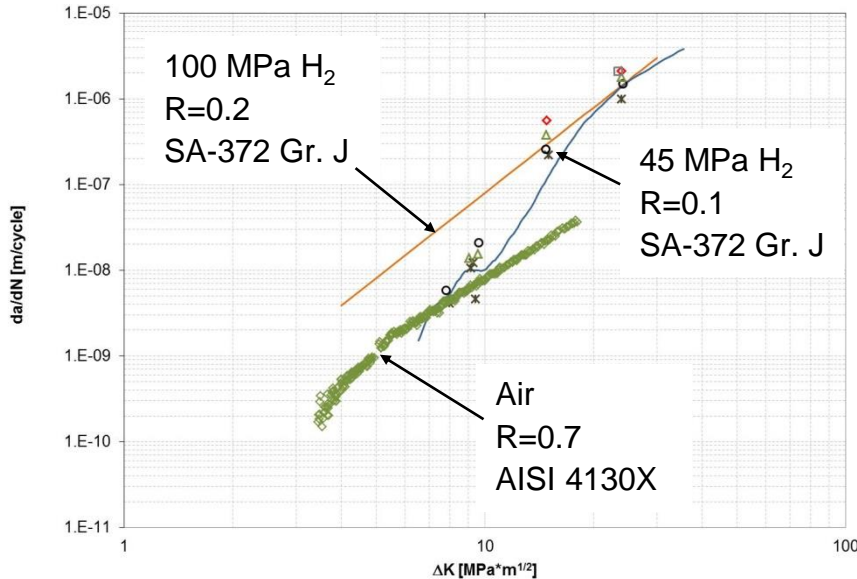
Crack depth (a) vs. number of cycles (N) calculated from two different fatigue crack growth relationships:

$$\frac{da}{dN} = C \Delta K^m$$

Extrapolated: single power-law relationship fit only to high- ΔK data

Multi-step: multiple power-law relationships fit to data in low-, intermediate-, and high- ΔK ranges

Extrapolated and multi-step FCG relationships formulated from multiple data sets



- Extrapolated FCG relationship: SA-372 Gr. J at 100 MPa H₂ and 0.1 Hz
 - Crack growth rates do not vary with H₂ pressure above 45 MPa
- Multi-step FCG relationship: SA-372 Gr. J at 45 MPa H₂ and 4130X in air
 - At intermediate and high ΔK , curve fit to upper-bound crack growth rates
- Assumption: relative differences between extrapolated and multi-step FCG relationships maintained at higher R ratios (i.e., R = 0.5 and 0.7)

Fatigue crack growth relationship has prominent effect on calculated pressure vessel design life

Δp	FCG relationship	Allowable # cycles
14 – 28 MPa (50% MAWP)	extrapolated	36,000
	multi-step	179,000
19.6 – 28 MPa (30% MAWP)	extrapolated	194,000
	multi-step	∞

Developing test procedures that allow construction of reliable multi-step FCG relationship has significant impact

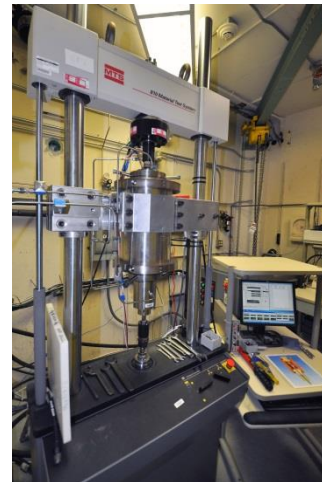
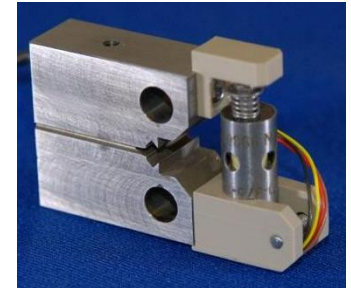
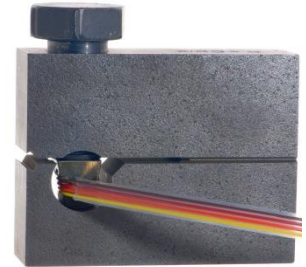
Summary

- Fatigue crack growth rates measured for Cr-Mo pressure vessel steels SA-372 Grade J and 34CrMo4 in H₂ gas as function of ΔK , f , and pressure
- da/dN vs. ΔK relationships measured in H₂ gas at 10 Hz suggest that capturing data at lower ΔK benefits design-life analyses
 - At lower ΔK , crack growth rates in H₂ gas approach rates in air
- da/dN vs. f data measured in H₂ gas at selected constant- ΔK levels demonstrate that crack growth rates at 10 Hz are not upper bounds
 - da/dN vs. ΔK relationships at 10 Hz not reliable inputs for design-life analyses
- Hybrid approach: measure the da/dN vs. ΔK relationship at 10 Hz, apply correction based on da/dN vs. f data
 - Possible approach to efficiently establish fatigue crack growth relationship in H₂ gas without compromising data quality
- Fatigue-life analysis of industrial cylinder demonstrates advantage of multi-step FCG relationship formulated from hybrid data

Back-up Slides

SNL core capability in hydrogen embrittlement features Hydrogen Effects on Materials Lab

- Static-loading crack-growth system
 - Wedge opening load (WOL) and double cantilever beam (DCB) specimens
 - H₂ pressure up to 200 MPa
 - Temperature -70 to 170 °C
- Dynamic-loading crack-growth system
 - Compact tension (CT) and single edge notch (SEN) specimens
 - H₂ pressure up to 138 MPa
 - New pressure vessel design with target temperatures -100 to 200 °C



Materials testing in H₂ supports technology development in several mission areas