

# Project 3: Quantification of Uncertainty in Lap Joints

SAND2015-6044D



- **Students:**

Matthew S Bonney – University of Wisconsin

Brett A Robertson – Arizona State University

Fabian Schempp – University of Stuttgart

- **Mentors:**

Matthew Brake – Sandia National Labs

Marc Mignolet – Arizona State University

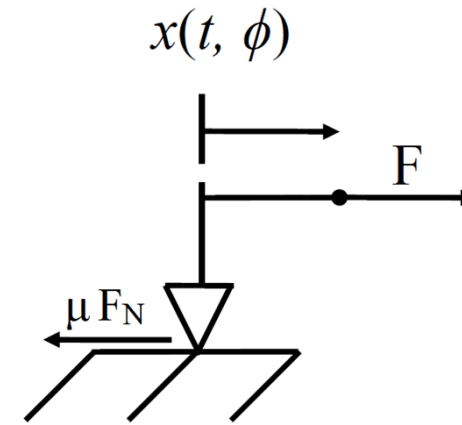
Matt Allen – University of Wisconsin

# Motivation

- The dynamics in physical joints is still mostly unknown; However, joints have a great influence on the energy dissipation and vibration characteristics of structures.
- Great effort has been put into creating models which capture the dynamic behavior in joints accurately.
- The scope of this project within the summer research institute is to deduce parameters for those models from experimental results and to quantify the uncertainty.
- The system used is the Brake-Reuß beam, which contains a lap joint fixed together by three bolts.
- Friction models that are investigated: Coulomb friction, Jenkins element, and Iwan friction model.

# Coulomb Friction

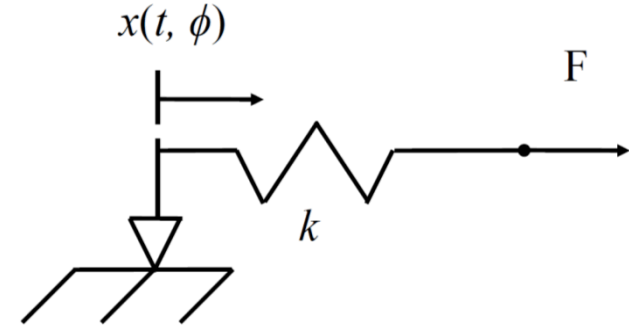
- Parameters:  $\mu$
- The coulomb friction model describes the relation between tangential force and the applied normal force as a function of displacement.
- $\mu$  may have different values for static and dynamic friction.
- Assumptions: Amontons' friction laws and Coulomb's friction law



$$F_f = \mu F_N$$

# Jenkins Element

- Parameters:  $k$  ,  $\mu$
- $\phi$  is the maximum distance the spring can elongate without the slider slipping.
- For a force equal to  $\mu F_N$ , the coulomb element will slip.
- Located at a single point.
- Fundamental element for Iwan and other friction models.
- Assumptions: Coulomb Friction, Linear spring



$$F(t) = \begin{cases} k x(t, \phi) & \text{Stick} \\ \mu F_N & \text{Slip} \end{cases}$$

# Iwan Element

- The Iwan model is a parallel connection of multiple Jenkins elements with different slip thresholds.
- Distribution of sliders given by:

$$\rho(\phi) = \mathbf{R} \phi^\chi [H(\phi) - H(\phi - \phi_{\max})] + \mathbf{S} \delta(\phi - \phi_{\max})$$

Converted to physical  
parameters

$$\{R, \chi, \phi_{\max}, S\} \longrightarrow \{F_s, K_t, \chi, \beta\}$$

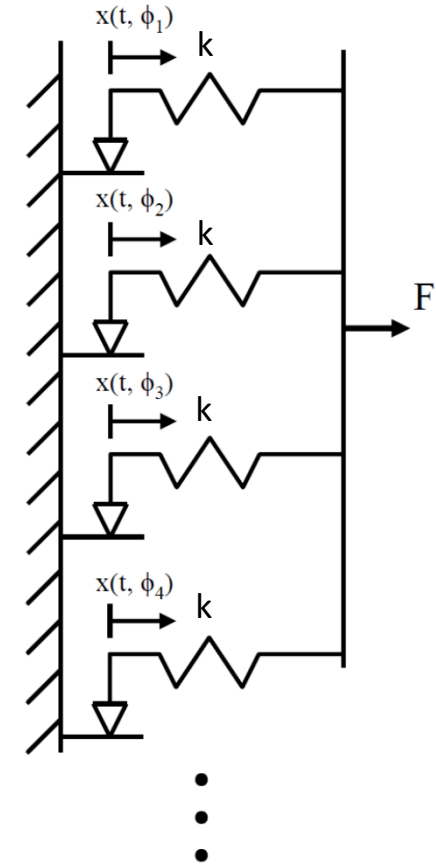
- Parameters:

$F_s$ : Force where macroslip first occurs

$K_t$ : Interface stiffness

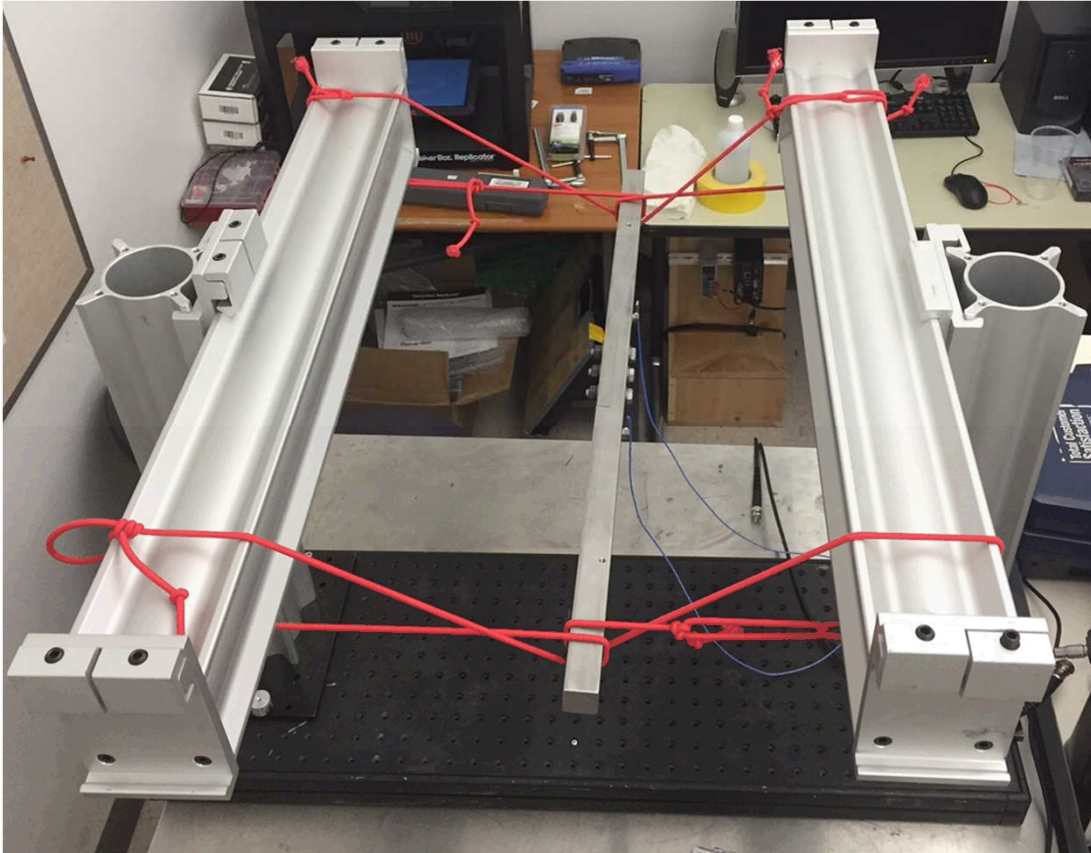
$\chi$ : Power law exponent

$\beta$ : Mathematical correction factor



$$F(t) = \int_0^\infty \rho(\tilde{\phi}) k [x(t) - \tilde{x}(t, \tilde{\phi})] d\tilde{\phi}$$

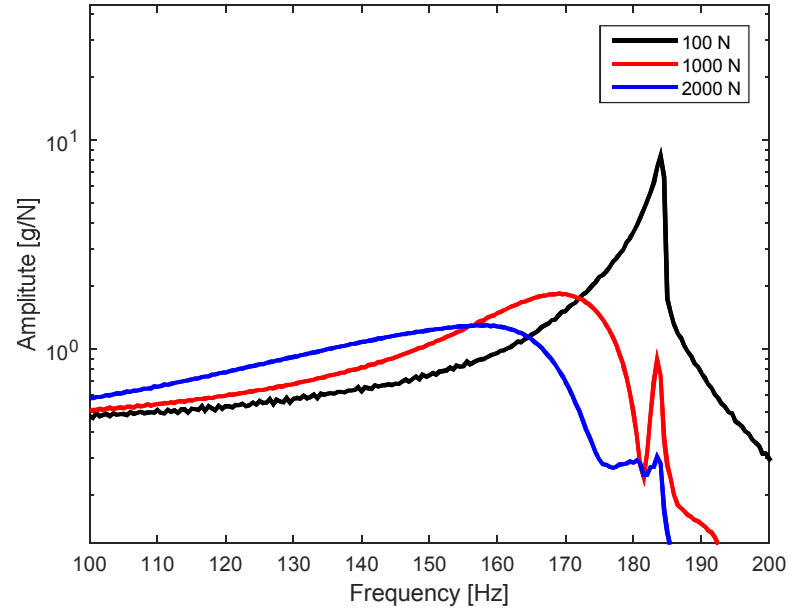
# Experimental Setup



- Test Parameters:
  - Beam Interface Finish (Rough -> Mirror)
  - Bolt Torque (3, 5, 7, 10, 15 N-m)
  - Impact Level (100, 1000, 2000, 4000, >8000 N)
- 4 total bungee loops used to hold beam in place, while also simulating free-free boundary conditions.

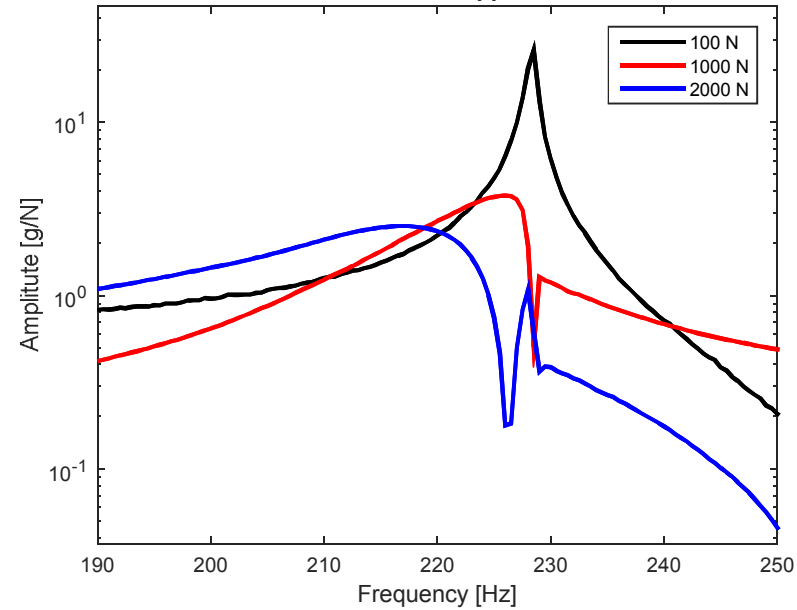
# FRF for Varying Load Level

Beam 5 at Varied Applied Load



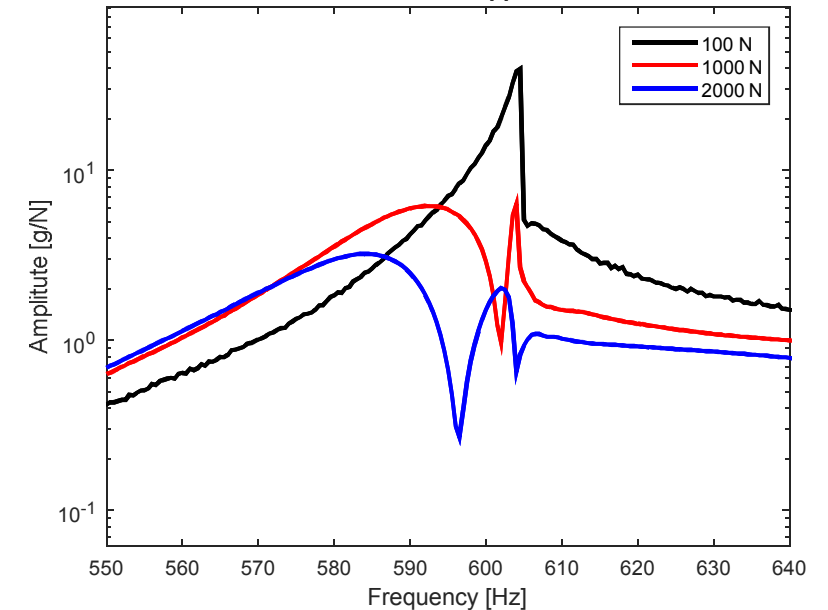
Mode 1

Beam 5 at Varied Applied Load



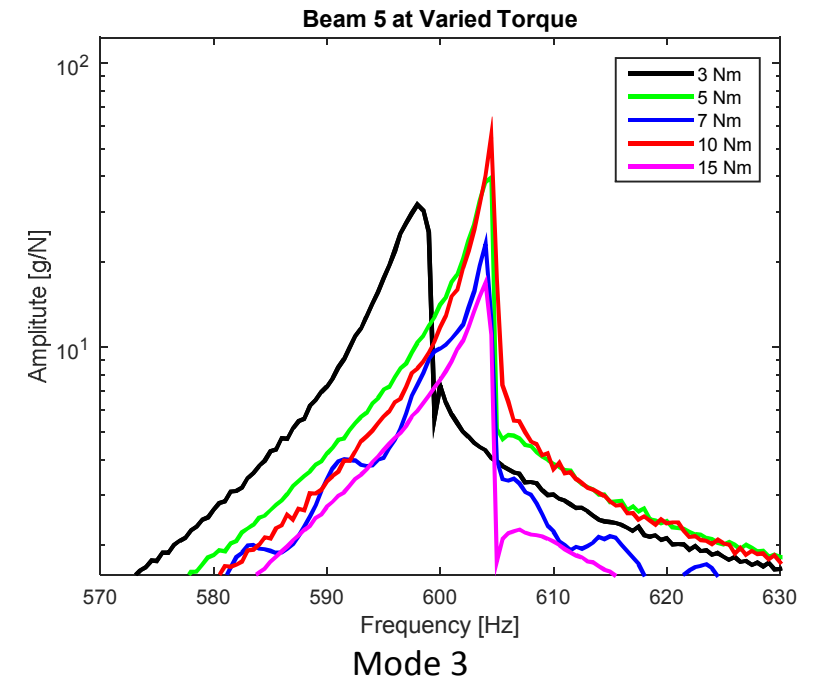
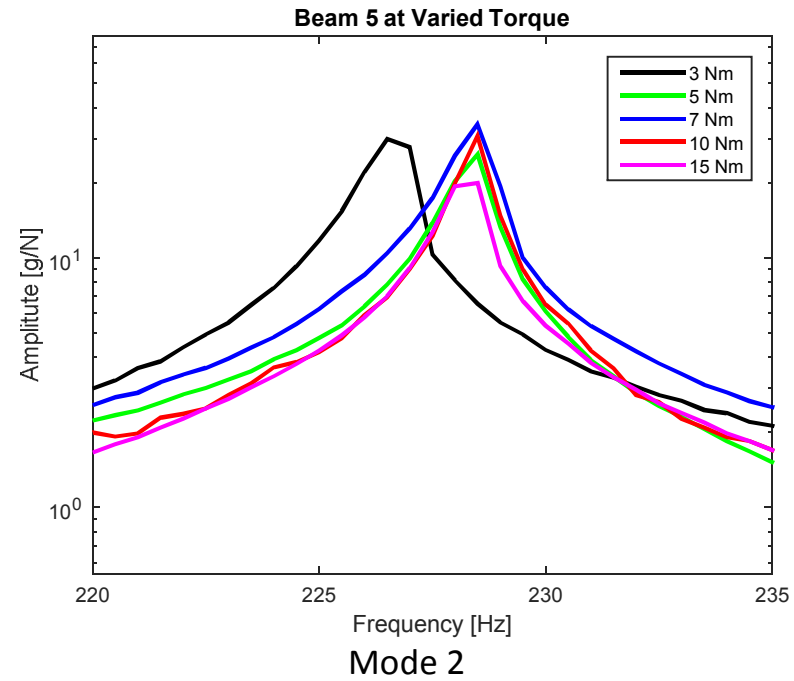
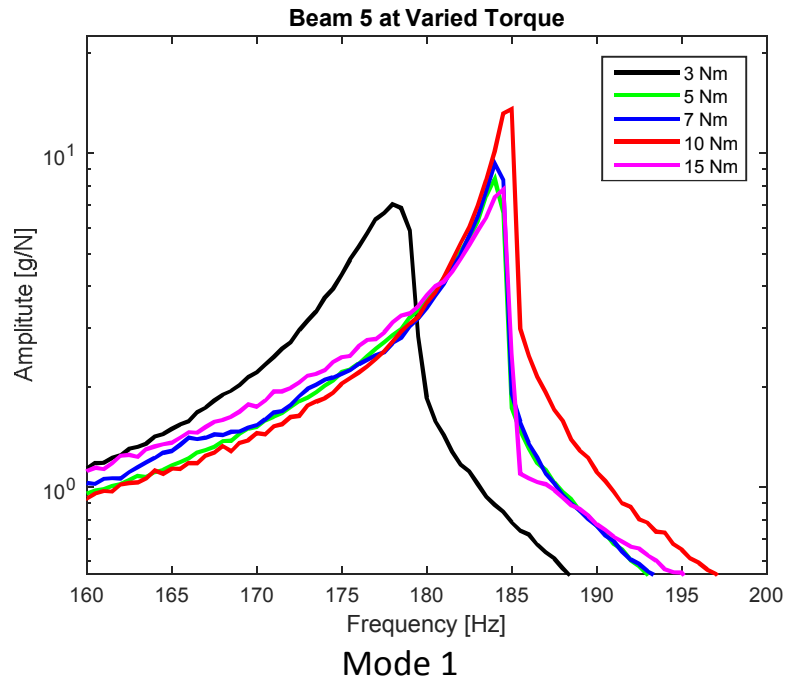
Mode 2

Beam 5 at Varied Applied Load



Mode 3

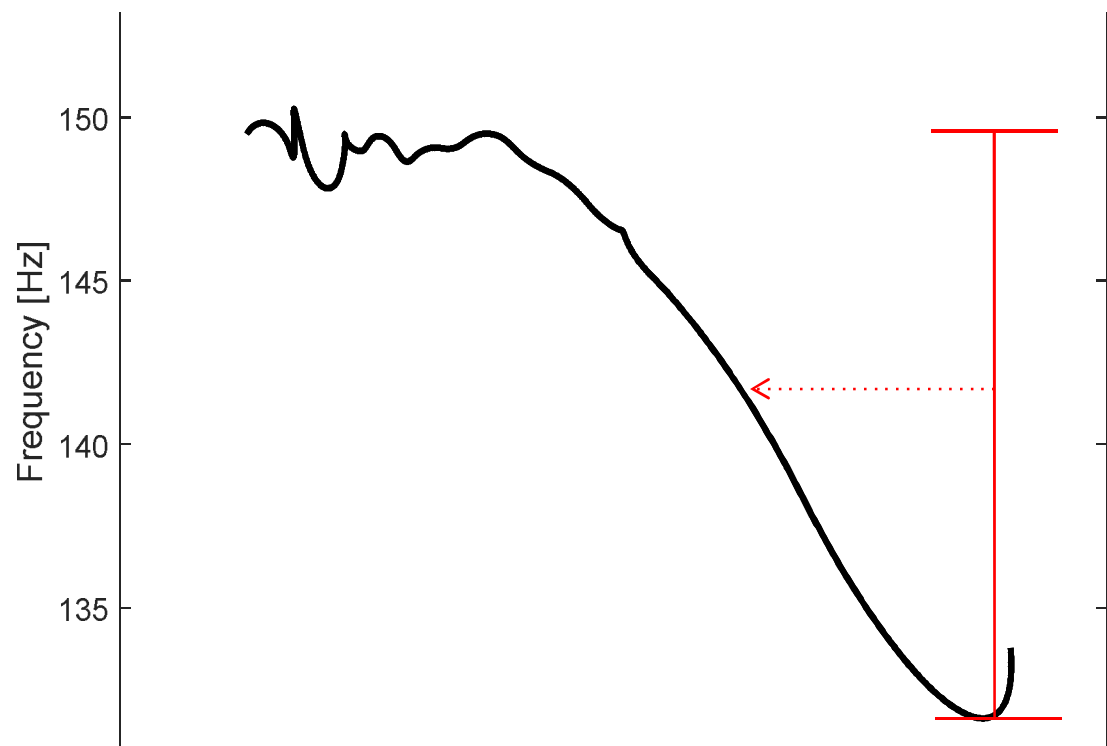
# FRF for Varying Torque Level



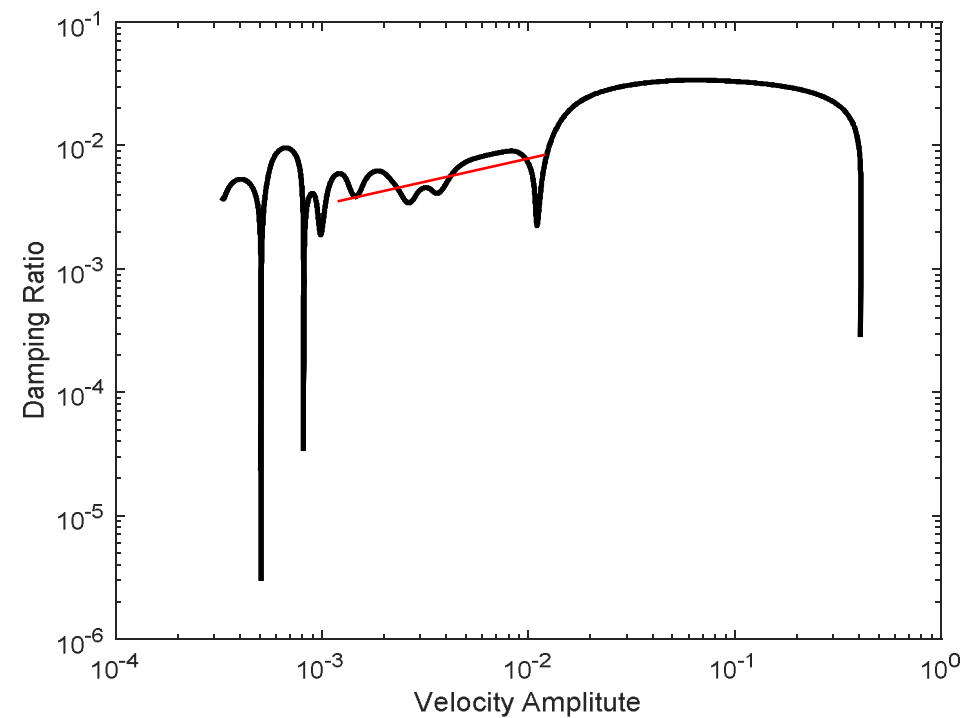


# Deducing Iwan Parameters

- Hilbert Transform of time history
  - Get frequency, damping, and velocity amplitudes
- Choose linear fit of damping vs. velocity amplitude - Slope =  $\chi$ 
  - Also obtain standard error of  $\chi$
- Determine  $K_t$  by difference in linear frequency and macroslip saturation frequency (using frequency vs. velocity amplitude plot)
- Determine  $\Phi_{\max}$  by choosing half the difference between linear and macroslip frequencies and obtaining velocity at that point, then transferring into displacement by dividing by  $\omega$
- Assume a distribution for  $\beta$
- Use sampling methods to determine distribution of  $F_s$  using all other parameters found

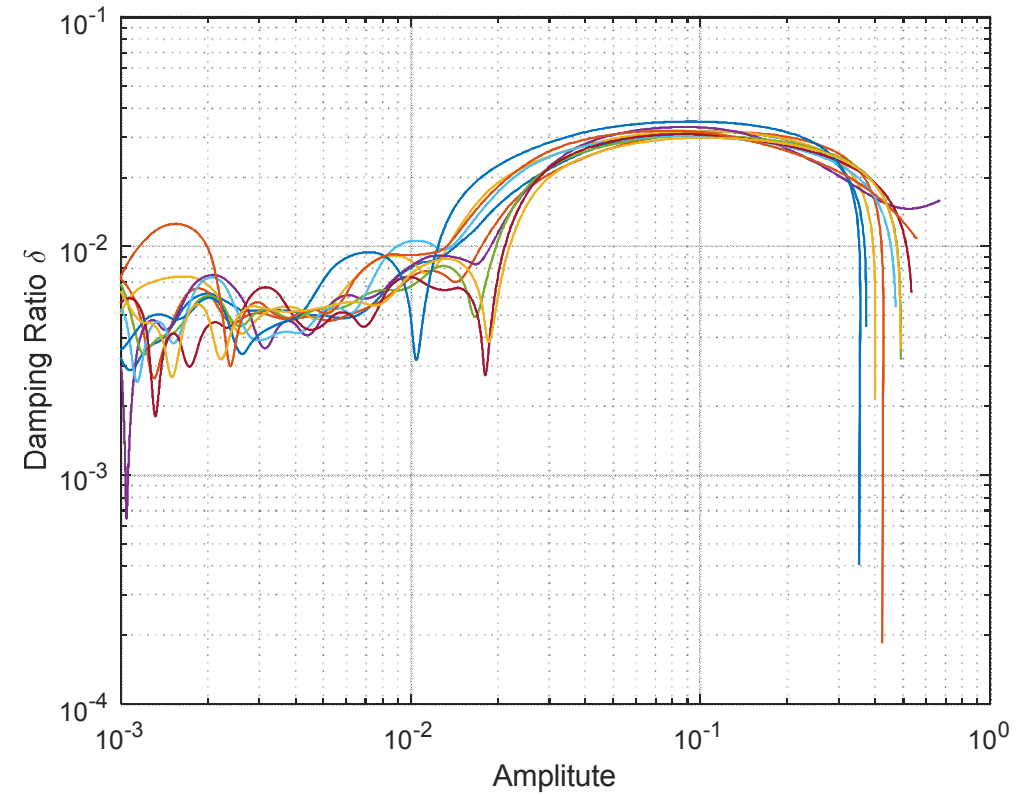
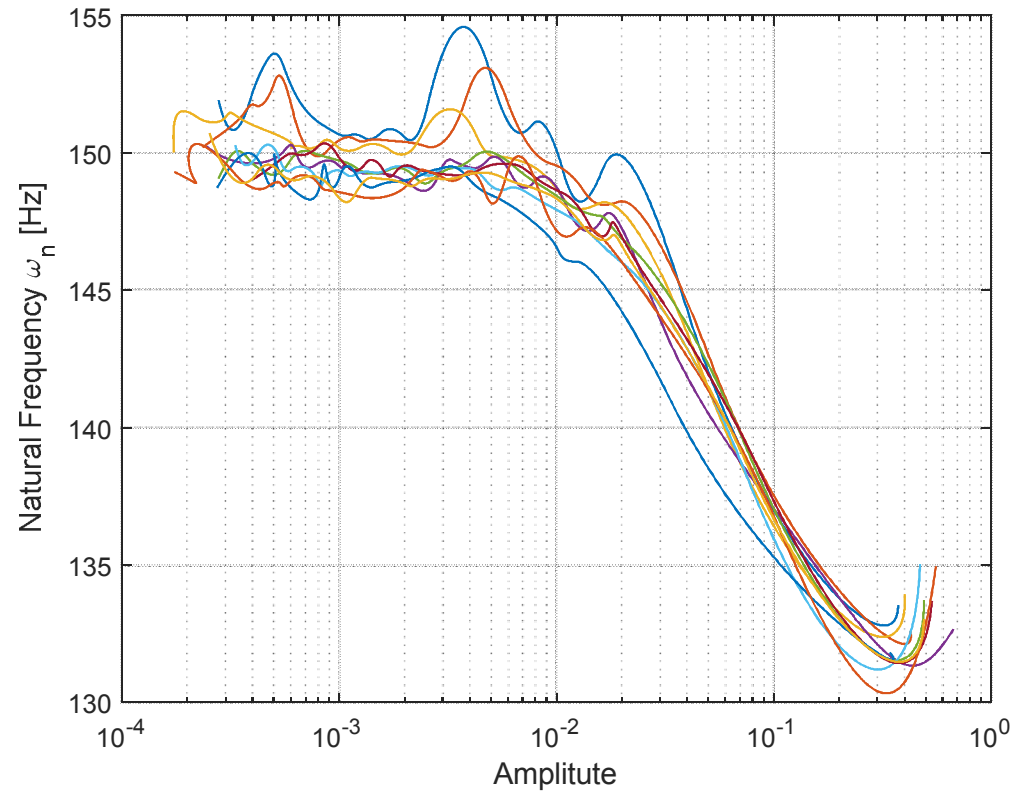


Frequency vs. Amplitude

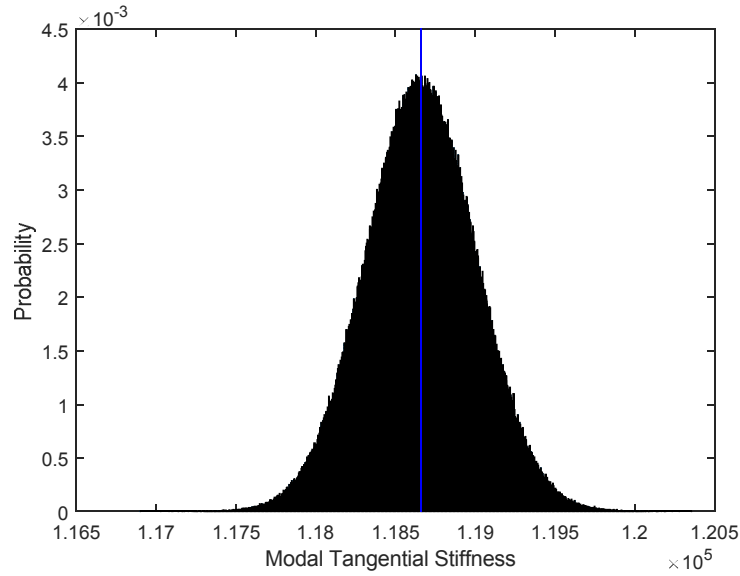


Damping Ratio vs. Amplitude

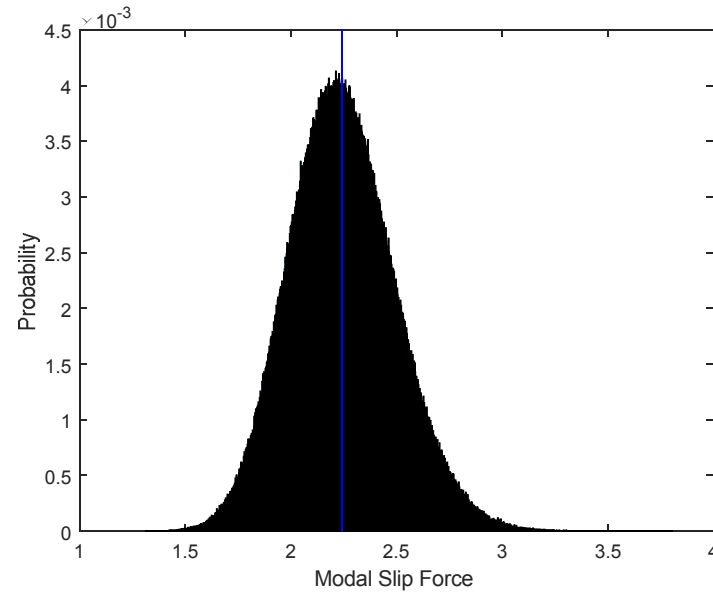
# Hilbert Transform of Data (Forcing Level > 8000 N)



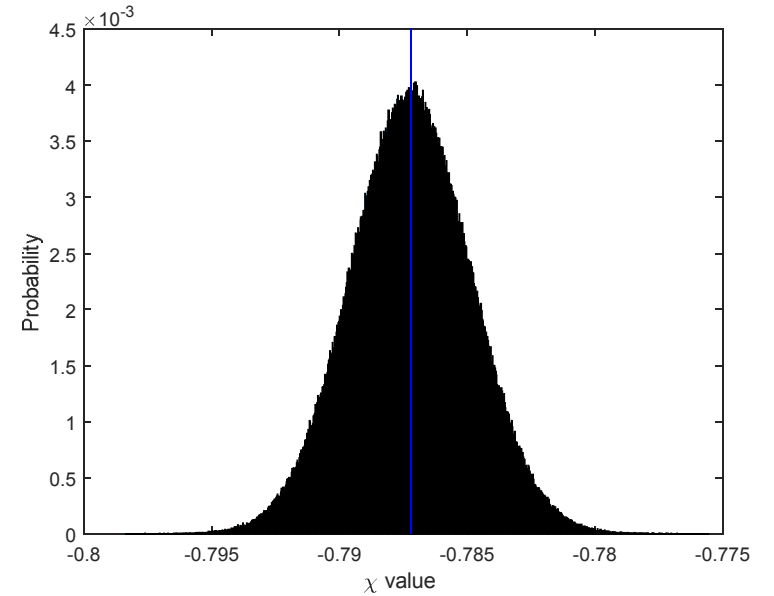
# Iwan Parameter Distributions (Beam 1, Torque 15 N-m, Mode 1)



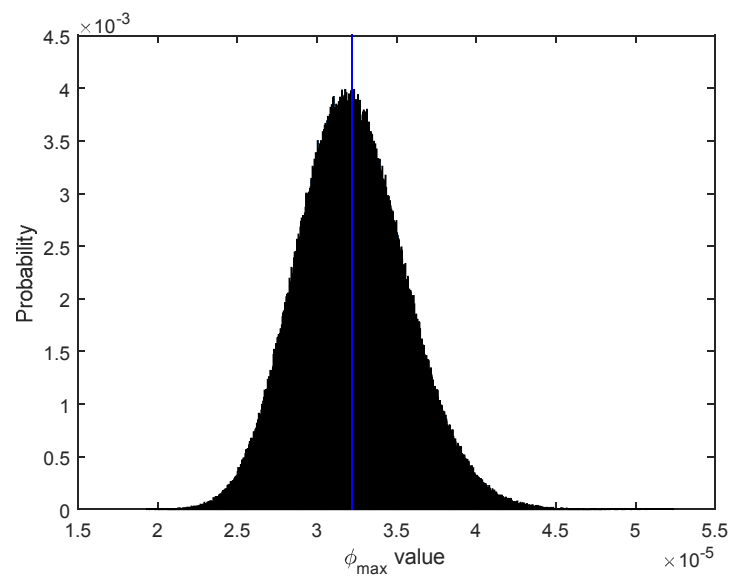
$$K_T \sim \Gamma(\alpha_K, 1)$$



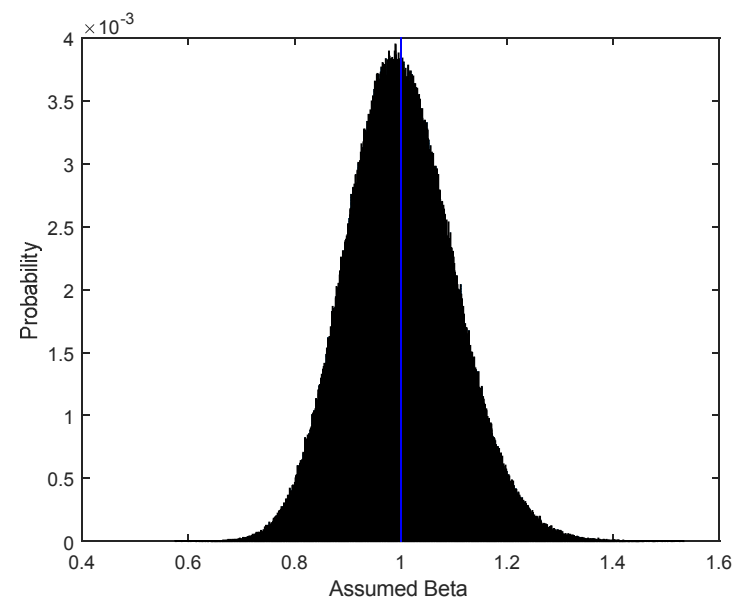
$$F_S \sim \Gamma(\alpha_F, \beta_F)$$



$$\chi \sim \beta(\alpha_\chi, \beta_\chi) - 1$$



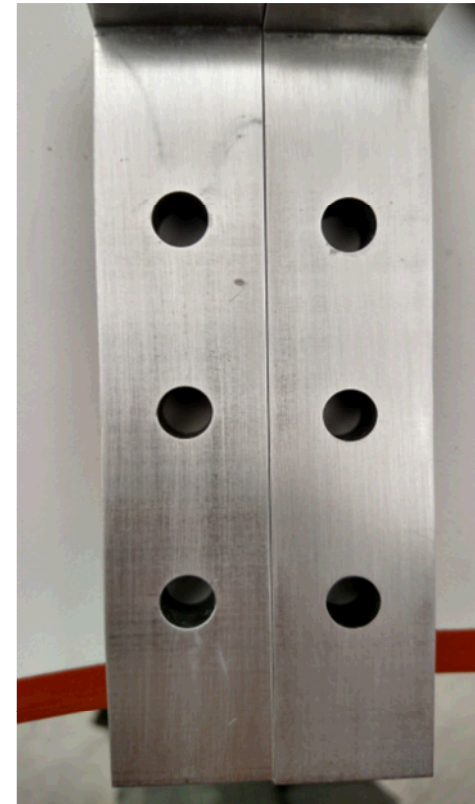
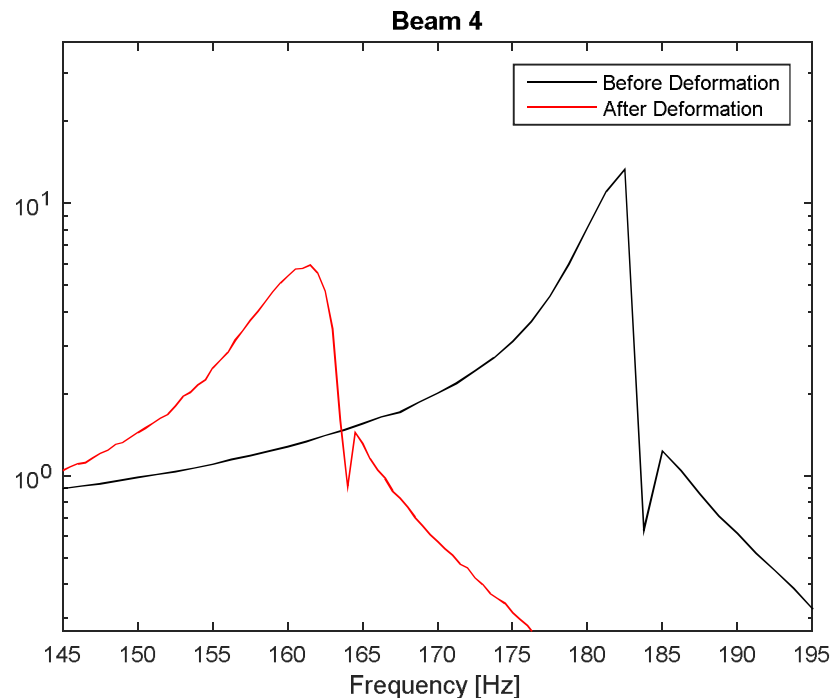
$$\phi_{\max} \sim \Gamma(\alpha_{\phi}, \beta_{\phi})$$



$$B \sim \Gamma(100, .01) \dots (Assumption)$$

# Plasticity Effect #1

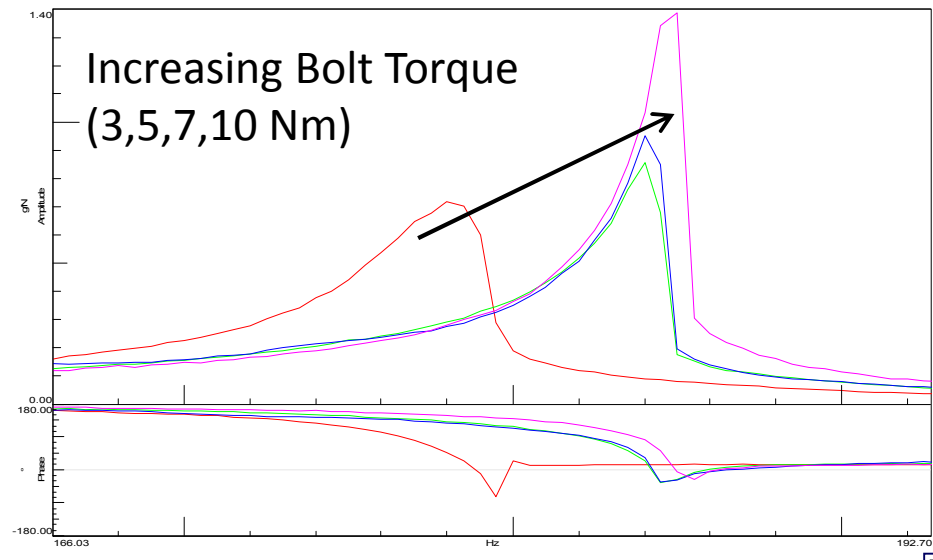
- **Problem:** Permanent change in fundamental frequency of beam 4
- **Tests:** New bolts; took out middle bolt; Mixed beams 3 and 4
- **Results:** All attempts showed same results, can conclude that beam 4 has permanent deformation at the interface and is no longer valid for comparison



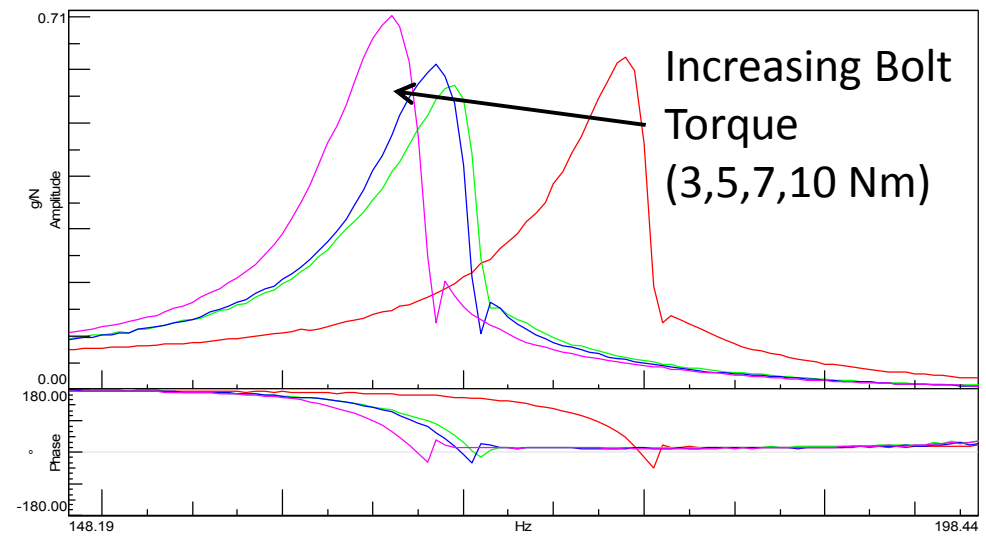
Beam 4 (left)  
Beam 3 (right)

# Plasticity Effect #2

- **Problem:** As bolt tightness was increased, the fundamental frequency was decreasing (counterintuitive as tighter bolts create stiffer interface)
- **Test:** Tested beams 1:5 (we only used 3 and 4 previously)
- **Results:** Only 3 and 4 decrease. 1, 2, and 5 increase as expected



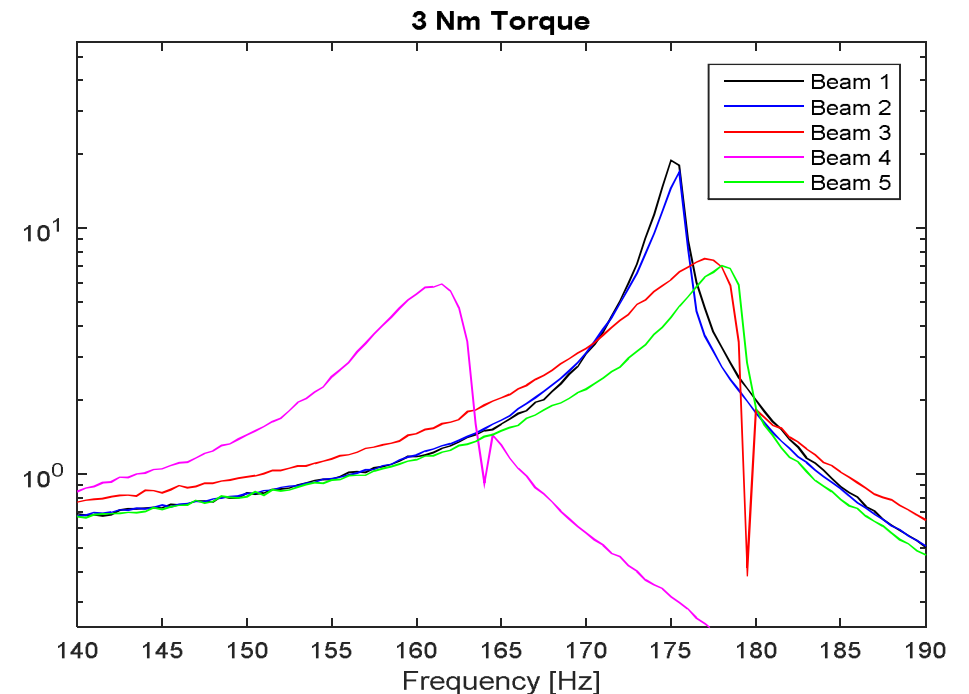
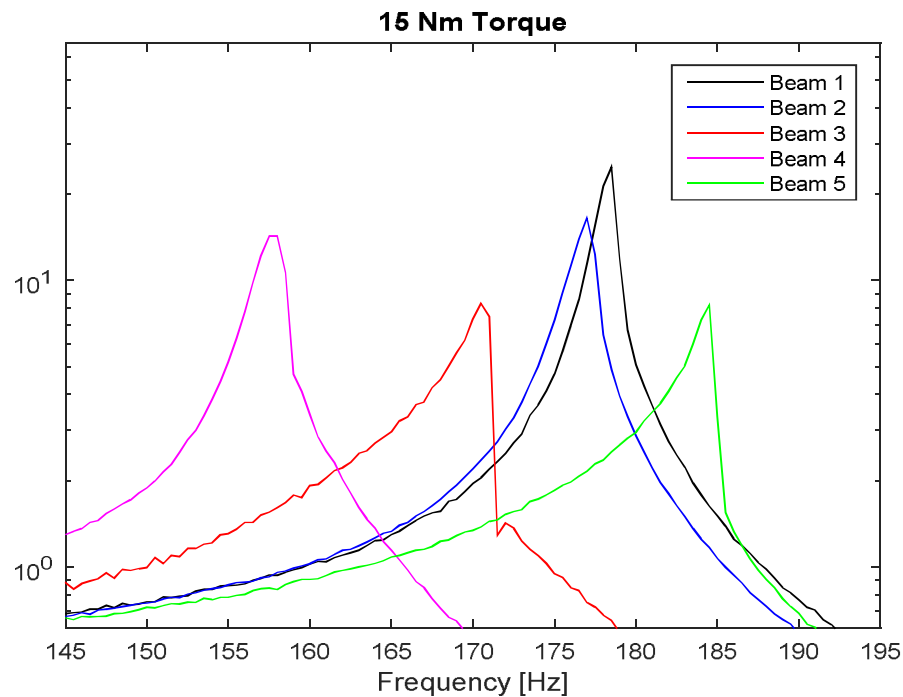
Beam 5



Beam 3

# Plasticity Effect #3

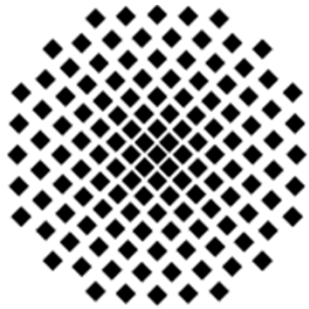
- **Problem:** As beams go from rough to smooth, the fundamental frequency was decreasing
- **Test:** Tested beams 1:5 (we were comparing 1 with 4 previously)
- **Results:** Rough beams have fundamental frequency  $\sim 178$  Hz and smooth beams have fundamental frequency  $\sim 184$  Hz (Disregarding beams 3 and 4)





# References

- B. Robertson and M. Bonney, et al. "Quantifying Epistemic and Aleatoric Uncertainty in the Ampair 600 Wind Turbine", Proceedings of IMAC 2015, February 2015.
- C. Soize, "Generalized probabilistic approach of uncertainties in computational dynamics using random matrices and polynomial chaos decompositions." *International Journal for Numerical Methods in Engineering* 81.8 (2010): 939-970.
- L. Gaul and R. Nitsche, "The Role of Friction in Mechanical Joints", Applied Mechanics Review, vol. 54, no. 2, pp. 93-105, 2001.
- D. J. Segalman, "A Four-Parameter Iwan Model for Lap-Type Joints", ASME Journal of Applied Mechanics, vol. 72, pp.752-760, September 2005.
- M. Mignolet, P. Song, X.Q. Wang, "A stochastic Iwan-type model for joint behavior variability modeling", Journal of Sound and Vibration, Volume 349, 4 August 2015, Pages 289-298, ISSN 0022-460X,
- M. Mayer, "Zum Einfluss von Fügstellen auf das dynamische Verhalten zusammengesetzter Strukturen", Bericht aus dem Institut für Angewandte und Experimentelle Mechanik 2007/1, Der Andere Verlag
- M. Allen, "Introduction to Iwan Models and Modal Testing for Structures with Joints", Presentation at the Nonlinear Mechanics and Dynamics Summer Research Institute



**University of Stuttgart**  
Germany

| Slide 1<br>Title                         |   |                          |
|--|---|--------------------------|
|  | Slide 2<br>Motivation                       |                          |
| Slide 9<br>Deducing Iwan<br>Parameters   | Slide 3 4 5<br>Friction Models              | Slide 14<br>Plasticity 1 |
| Slide 10<br>Deducing Iwan<br>Parameters  | Slide 6 7 8<br>Setup/FRF's                  | Slide 15<br>Plasticity 2 |
| Slide 11<br>Hilbert<br>Transform<br>Data | Slide 12 13<br>Iwan Parameter Distributions | Slide 16<br>Plasticity 3 |
| Slide 18<br>Logos                        | Slide 17<br>References                      |                          |

Recommended Layout