



Survivability of first-wall fusion materials: relevance to IFE and MFE

In an IFE Reactor, the First-wall is subjected to a Programmed High Fluence of Energetic Ion pulses (3×10^8 /year)

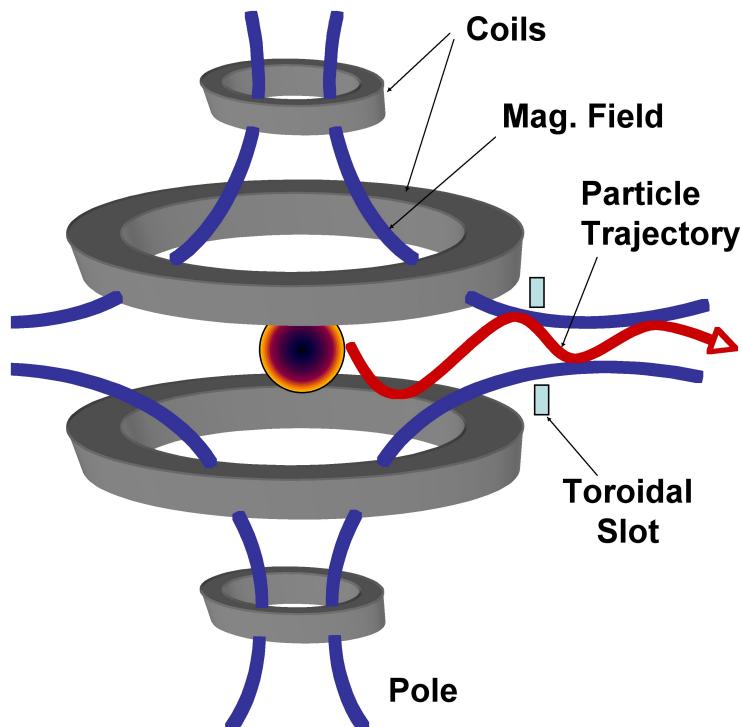
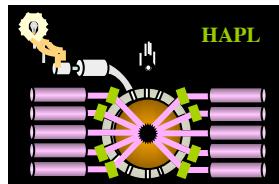


Image provided by R. Raffray,
UC San Diego



Unlike MFE, no Steady State phase, only 'transient' events.

Level per pulse is known, ~ few MeV ions normal to surface. At 10 Hz operation, 3×10^8 pulses per year

At 10 nm erosion/pulse, 3 METER thickness lost per year. So NOTHING can be lost per pulse. Melting should be avoided as well.

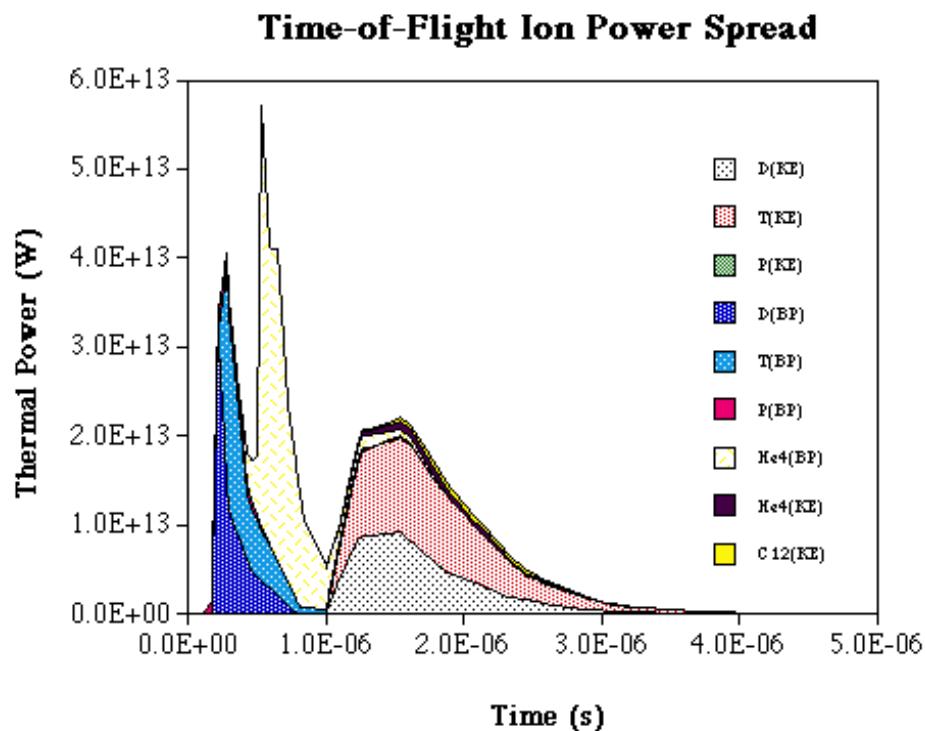
Biggest threat below Melting is Thermomechanical stress

Leading Geometry: Spherical w/ or w/o gas fill

Backup Geometry (LEFT): Cusp with 'beam dump' on axis

- Leading materials: tungsten and W alloys, SiC

Laser IFE Direct Drive Threat Spectra (note: NIF is indirect drive)



Simulation: Thermal Power to Wall in Ions
from 154 MJ Yield. Wall Radius: 6.5 m

- For Direct-drive Laser IFE:
~70% neutrons, 1-2% x-rays
30% ions (50-50 fusion and 'debris')
- Ions: several MeV, ~ few μ sec each,
8-20 J/cm^2 fluence, judged
Significant Threat
- X-rays: ~ 1 J/cm^2 , up to 10 keV energies,
judged less significant threat
- RHEPP-1: 700 keV N, higher for N⁺²,
100-150 ns pulsewidth, 75-95 GW/m^2
- RHEPP-1 energy delivery too short, but
otherwise good fidelity with reactor ion
threat

$F=P^* \sqrt{t}$: High Heat Flux conditions with Heat Diffusion effect included. Comparison:

ITER ELMs (est):

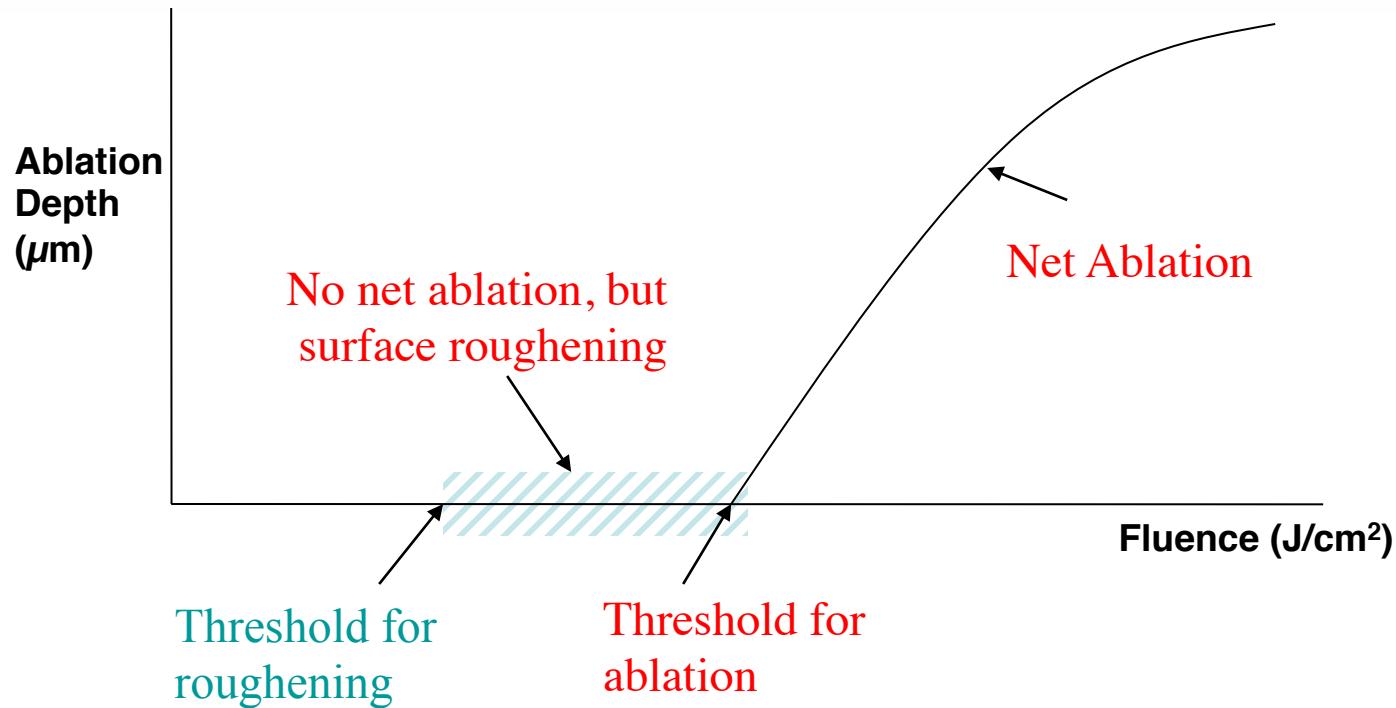
22.4 - 67.1 $\text{MW m}^{-2} \text{s}^{1/2}$

RHEPP-1:

33 - 112 $\text{MW m}^{-2} \text{s}^{1/2}$



Regimes of IFE Materials Response to Ions

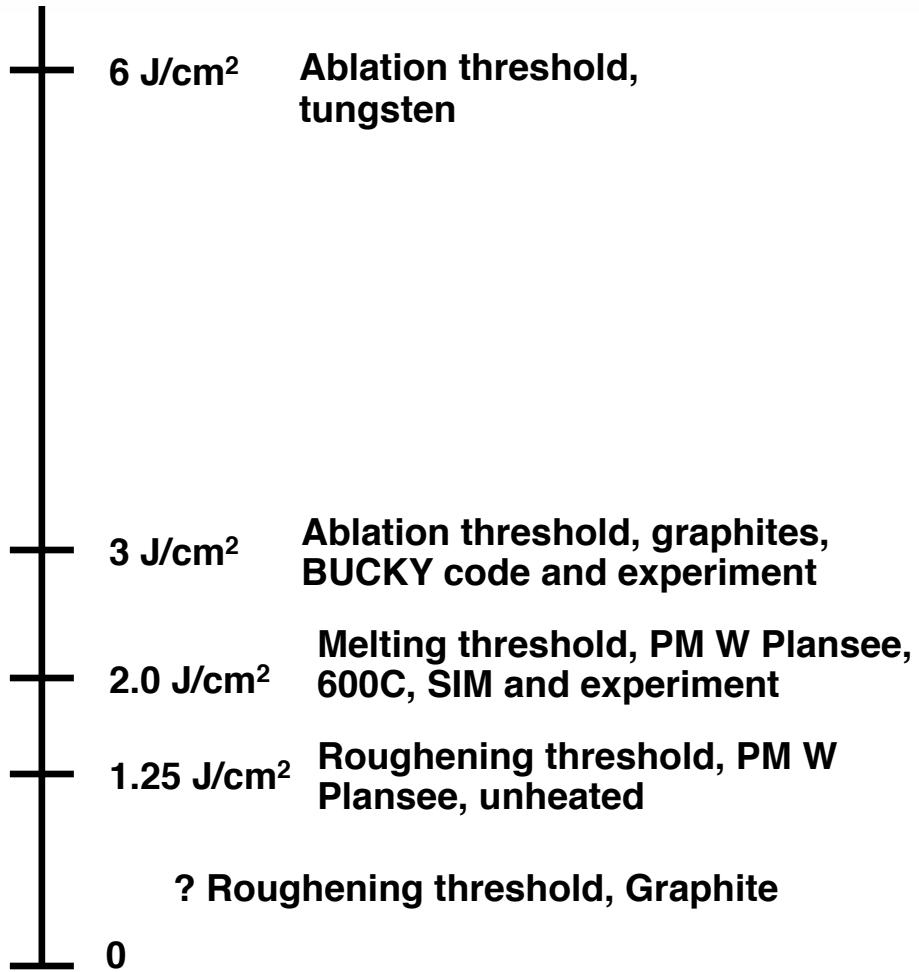


Goals (for each material): examine net ablation to validate codes DONE
find threshold for ablation

Area of Interest

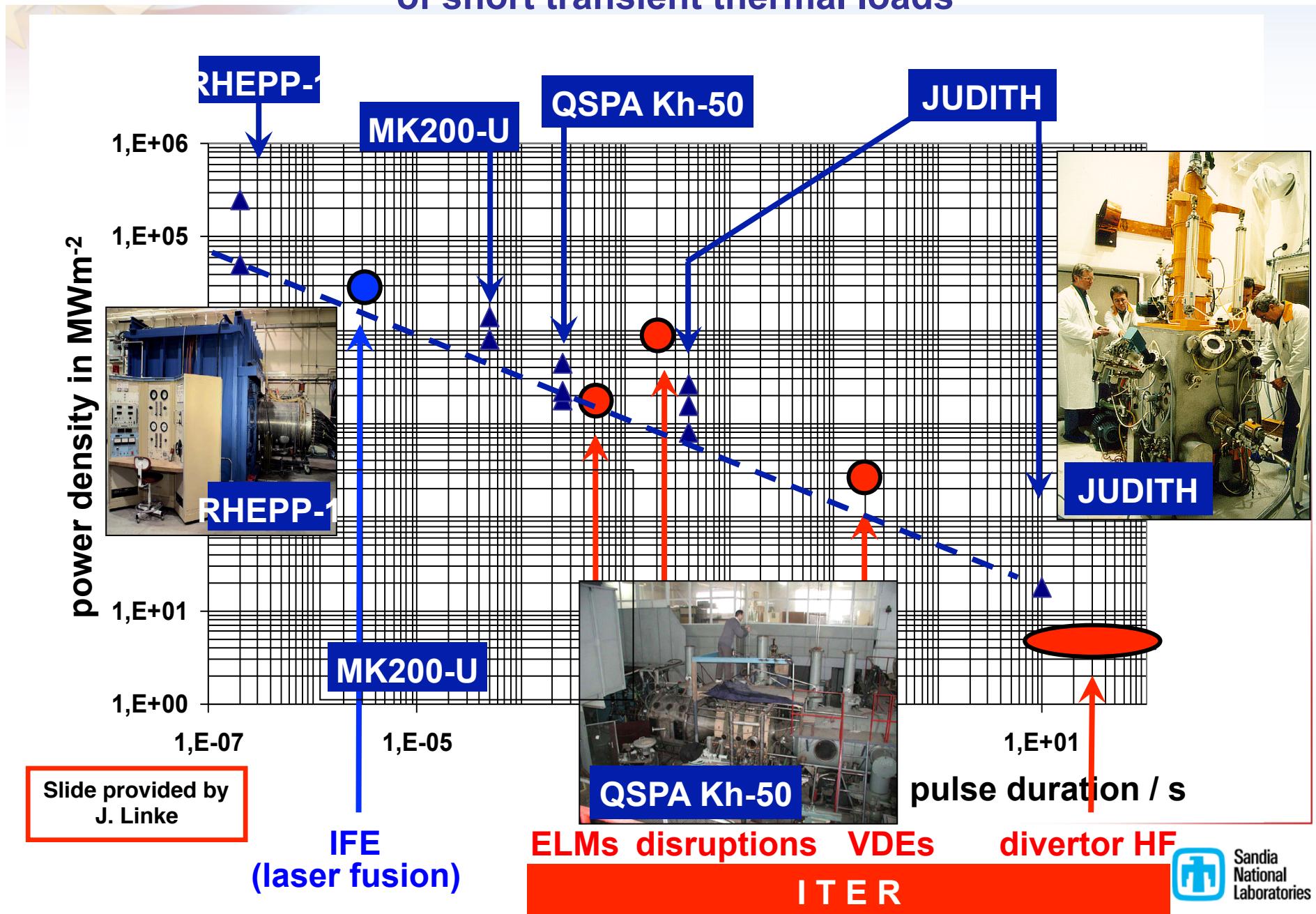
Understand roughening. Is there mass loss?
Find threshold for roughening
(Fluence/pulse, No. of pulses)

Thresholds for Materials exposure to ions on RHEPP

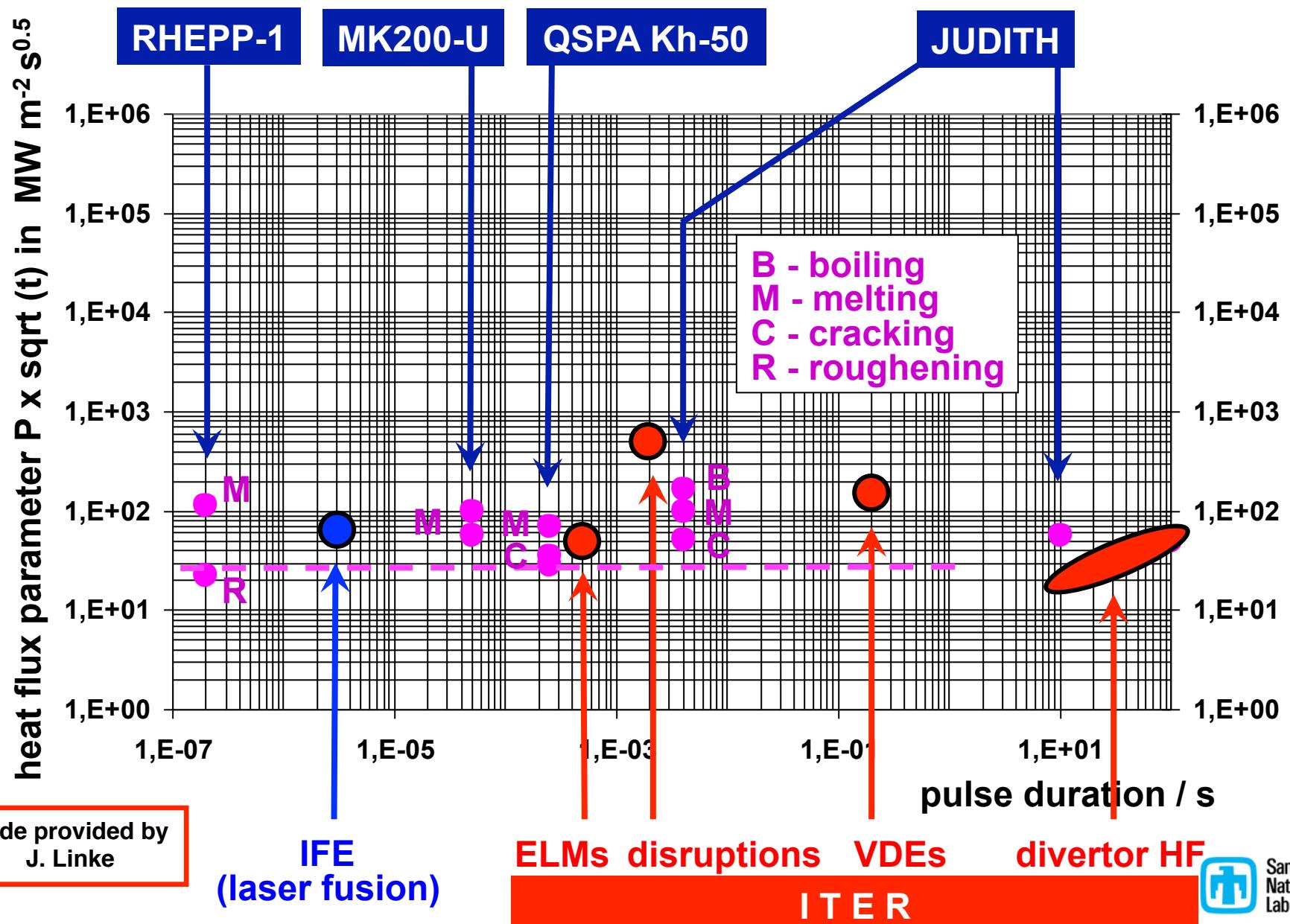


- General exposure conditions: MAP nitrogen beam, 150 ns pulselength, single shot.
- Roughening threshold for graphite (matrix) is unknown, but probably below 0.5 J/cm²
- Roughening threshold for tungsten for He beam is below that for MAP Nitrogen
- Chart to left: 'PM W Plansee' refers to random-grain Powder Met Tungsten provided by Plansee

Adding $P^* \sqrt{t}$ connects IFE with MFE simulation of short transient thermal loads



Performance of tungsten under short transient thermal loads. Confirms heat conduction dominates over direct energy deposition



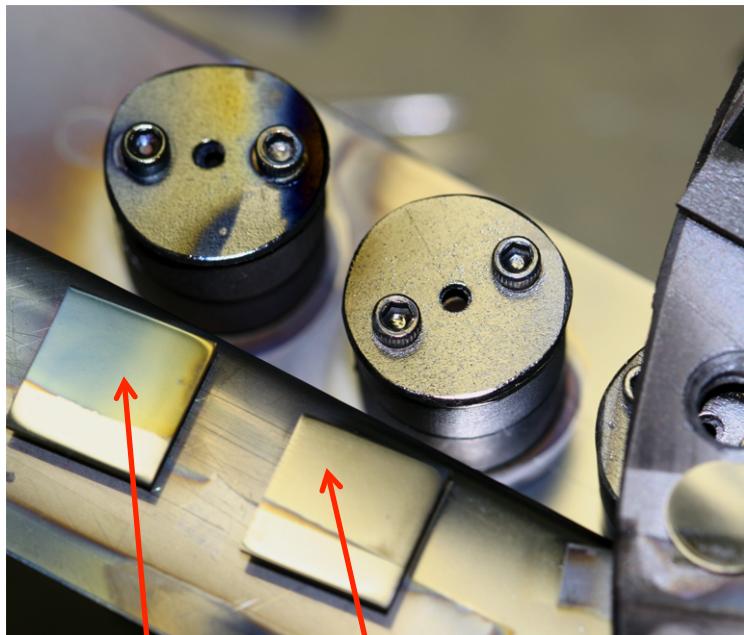
Slide provided by
J. Linke

IFE
(laser fusion)

ELMs disruptions VDEs divertor HF
ITER

RHEPP-1 Roughening Threshold, PM W, Multi-pulse, nitrogen beam exposure

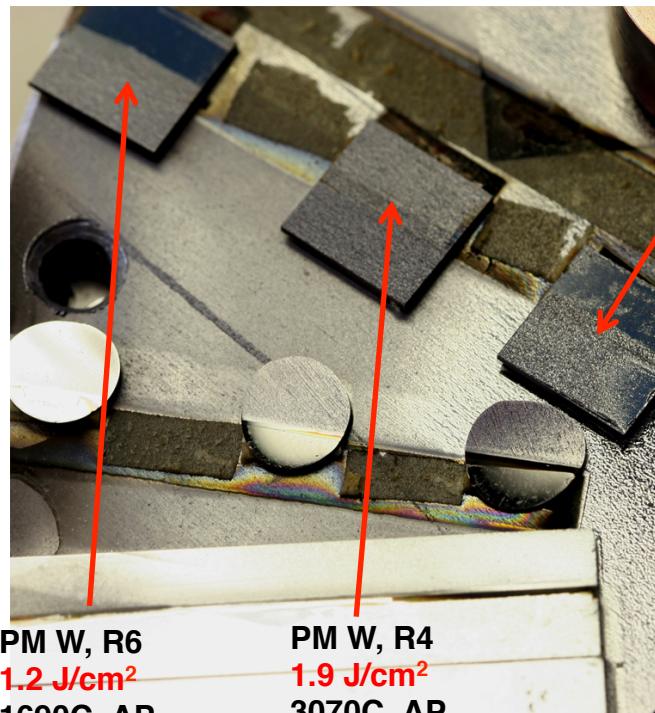
2000 shot series: PM W samples laid out radially from center. 10 and 8cm out are sub-threshold for roughening, 6cm is above. Note temperature excursions from modeling, based on fluence scatter from FCup data.



PM W, R10
0.2 J/cm²
270C_AP
Hi 415C
Lo 145C

PM W, R8
0.6-0.9 J/cm²
1290C_AP
Hi 1960C
Lo 535C

These PM W appear unaffected



PM W, R6
1.2 J/cm²
1690C_AP
Hi 2278C (5%)
Lo 1175C (5%)
R_a ~ 2.5 μm

PM W, R4
1.9 J/cm²
3070C_AP
Hi 3650C
Lo 2100C
R_a ~ 4 μm

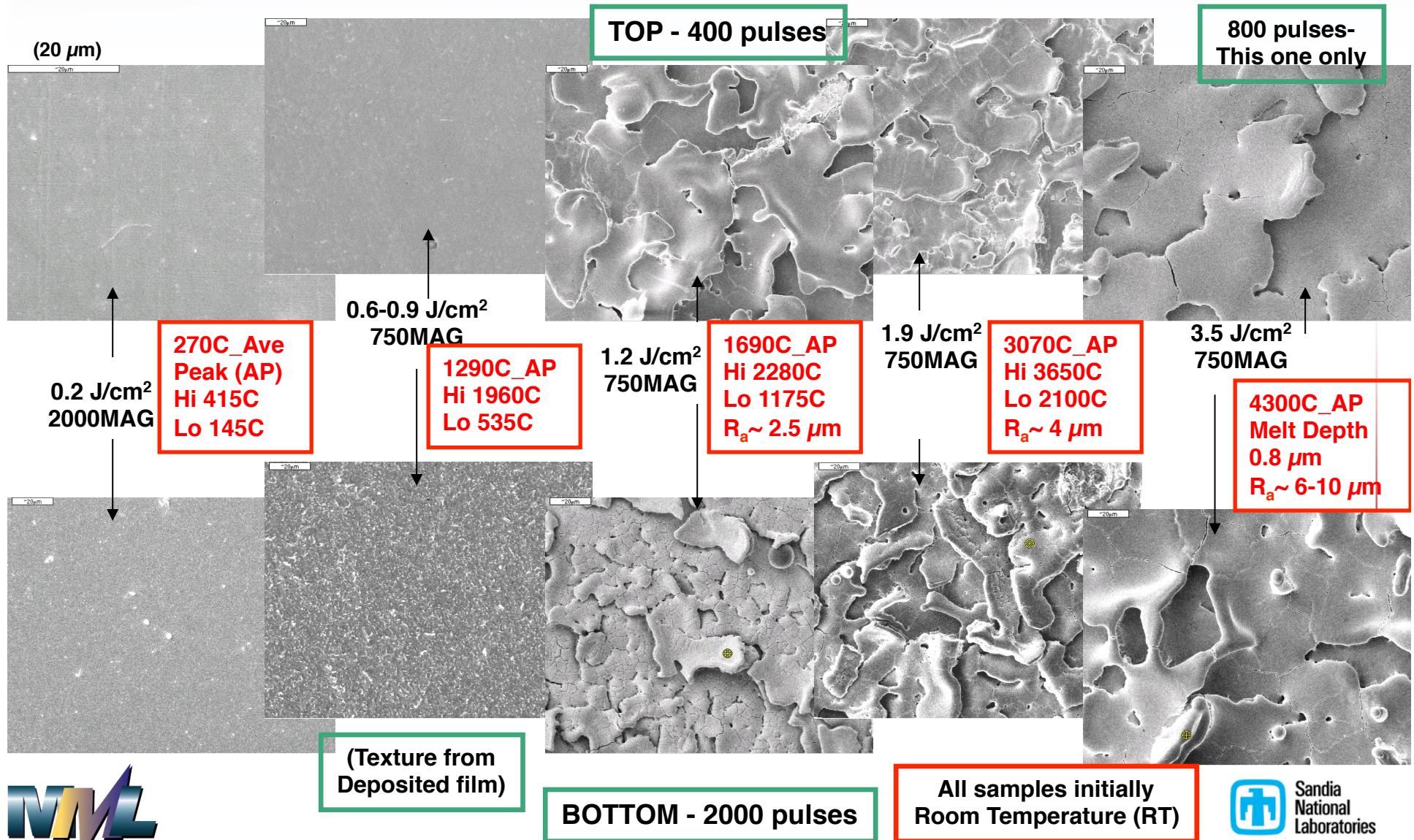
These PM W are very rough

PM W, R2
3.5 J/cm²
4300C_AP
Melt Duration 159 ns
Melt Depth 0.8 μm
R_a ~ 6-10 μm

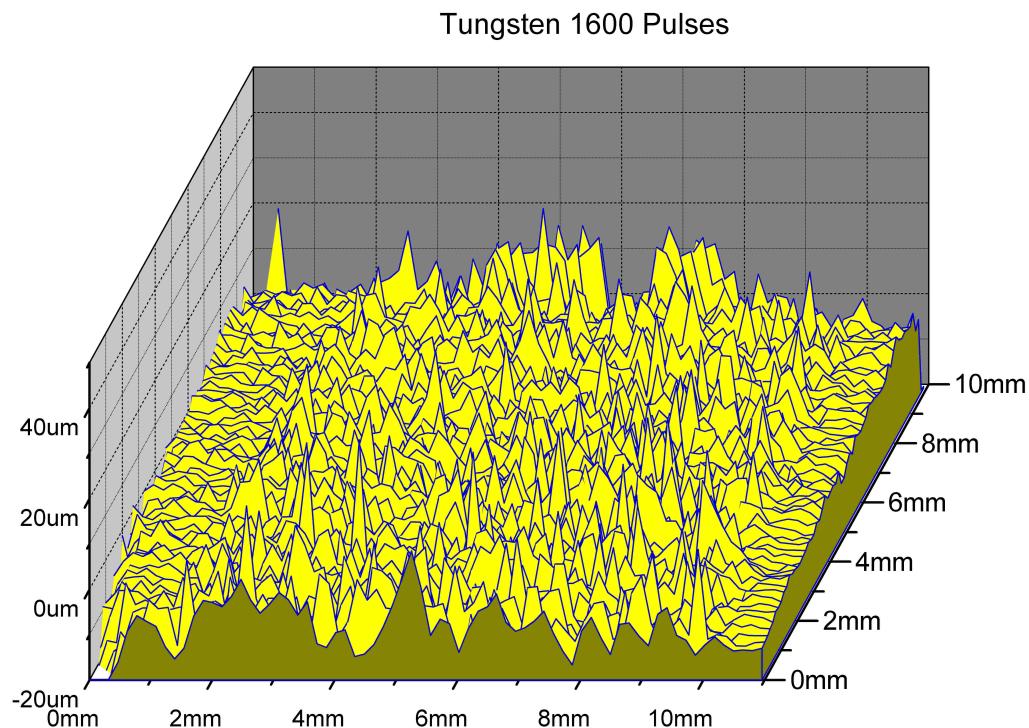
BEAM CENTER

R6 = 6 cm from
Beam center

SEMs of Polycrystalline (PM) Tungsten Roughening from previous slide:
Threshold at $\sim 1 \text{ J/cm}^2$, roughening saturates after ~ 400 pulses

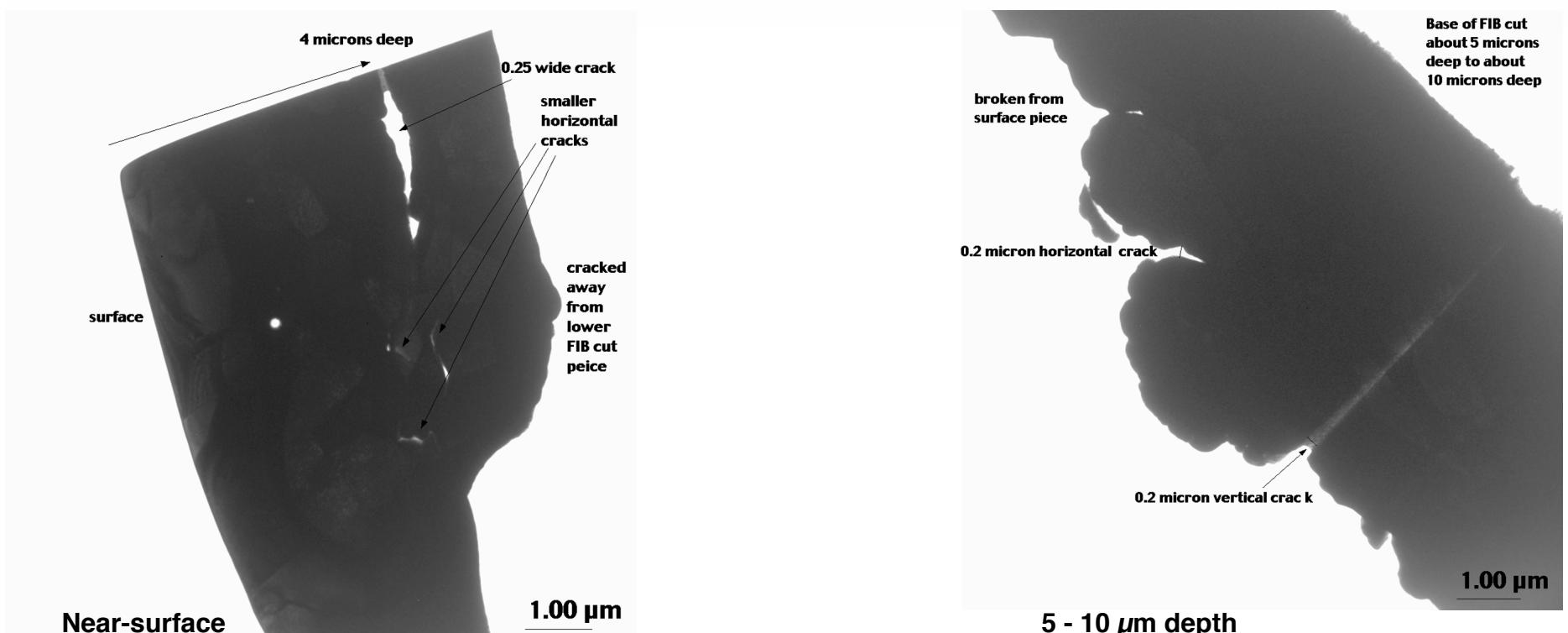


Is this erosion from melting? No. PM Tungsten after 1600 pulses (non-melting): Mostly mountains



- **Heated/treated PM W examined with NEXIV laser interferometry**
- **Comprehensive line-out scan: max height $30 \mu\text{m}$, min height $< 10 \mu\text{m}$ compared to untreated**
- **Very deep micro-cracking not visible here**
- **Hypothesis: Thermal expansion from heating, plastic deformation**

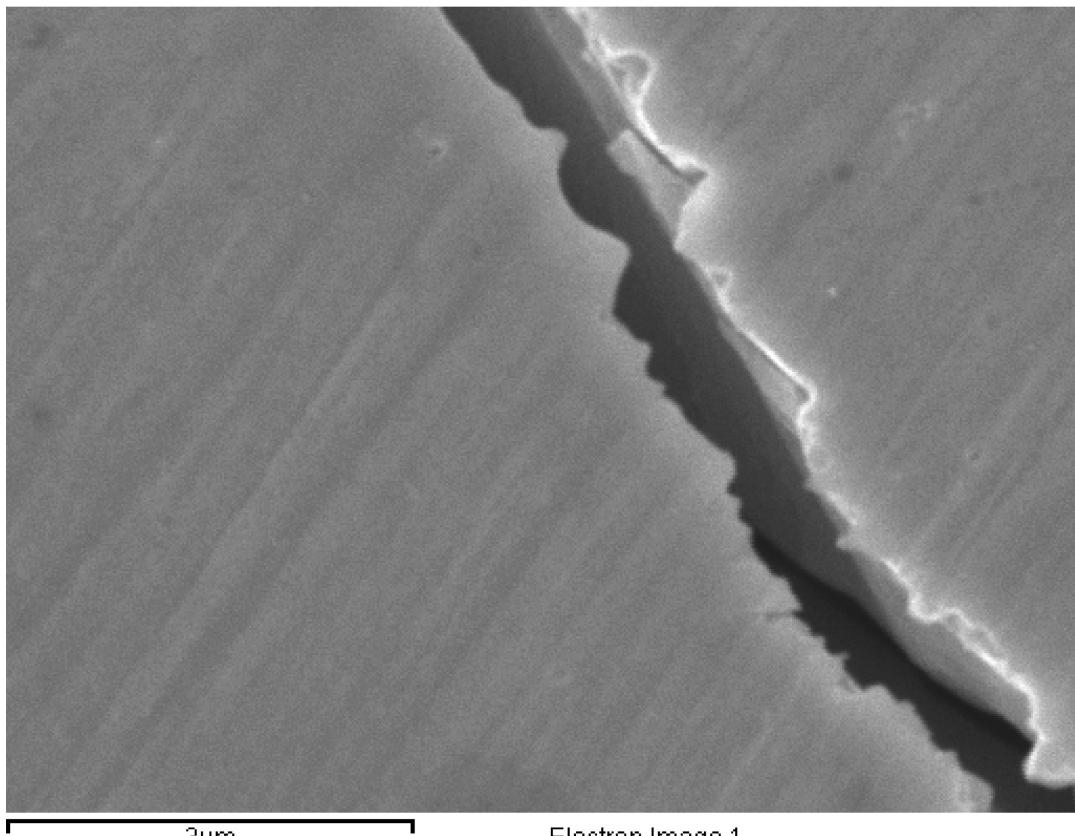
FIB-XTEM of 1000-pulse W at 2.25 J/cm² (ave): Deep horizontal/vertical cracking without melt



- Polished Powder Met W exposed to 100 shots N beam @ 2.25 J/cm² ave / pulse, ~ melting temperature at surface. No melt layer observed.
- 600°C exposure
- Sample cracking horizontally/vertically down to 10 μ m depth

Suspect fatigue-cracking. If deep enough to reach steel substrate, wall will fail

Evidence of lack of melt on Single Crystal Surface: 15,000X SEM



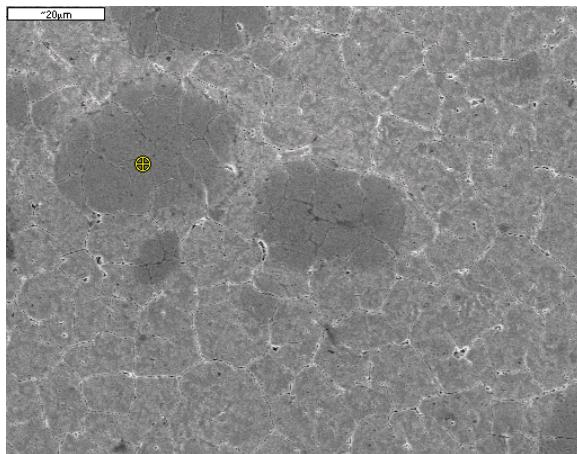
- Surface of Single-Crystal Tungsten, heated 510°C, after ~ 800 exposures at various fluences
- SEM at 15,000 magnification shows Clean Break along crack - stress cracking only
- Away from crack, surface is unaffected by Helium beam exposure

Three Forms of tungsten, treated at about same fluence: Its all about the grains.

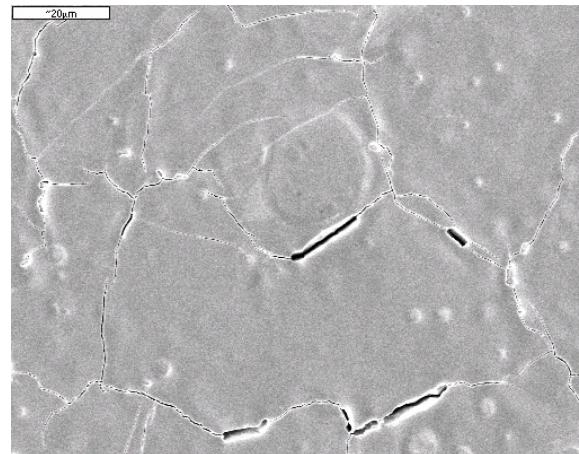
1,000X MAG

1,000X MAG

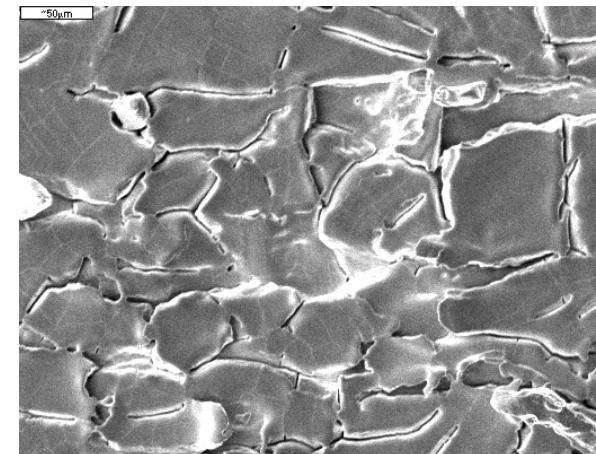
300X MAG



W-0.5%TiC 1.5 J/cm^2 .
 $\text{Ra} = 0.04 \mu\text{m}$



M182Perp $\sim 1.25 - 1.5 \text{ J/cm}^2$
 $\text{Ra} \sim 0.15 \mu\text{m}$

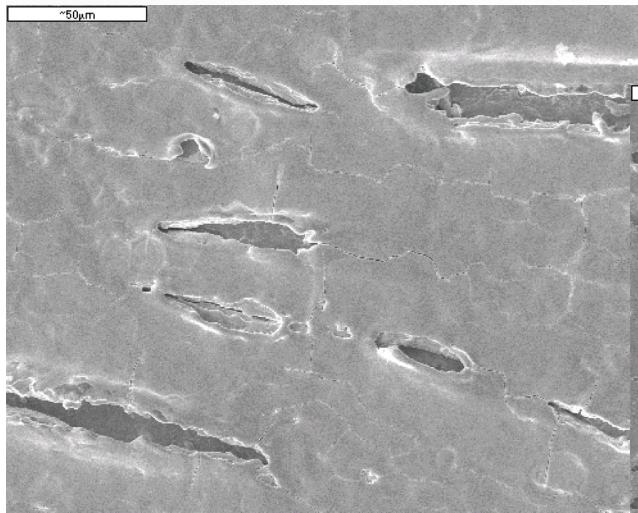


M182Parallel $\sim 1.3 \text{ J/cm}^2$
 $\text{Ra} \sim 4.5 \mu\text{m}$

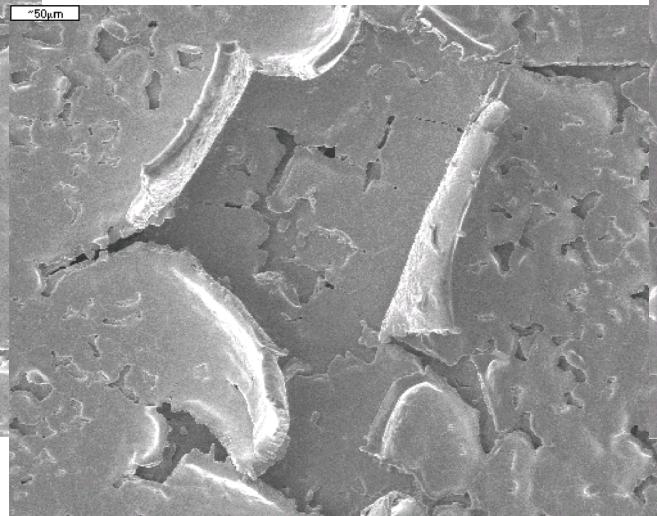
Two on right are SAME material

- (LEFT) W-0.5%TiC (Kurishita) formed by Hot Isostatic Press (HIP) – strengthens grain boundaries
- (CENTER) M182Perp tungsten: grains vertical to surface. Bottom of grains protected. (RIGHT) M182Parallel – grain corners get lifted.

PM Tungsten exposed to Nitrogen (top) and Neon (bottom):
Mass loss with N, not with Neon

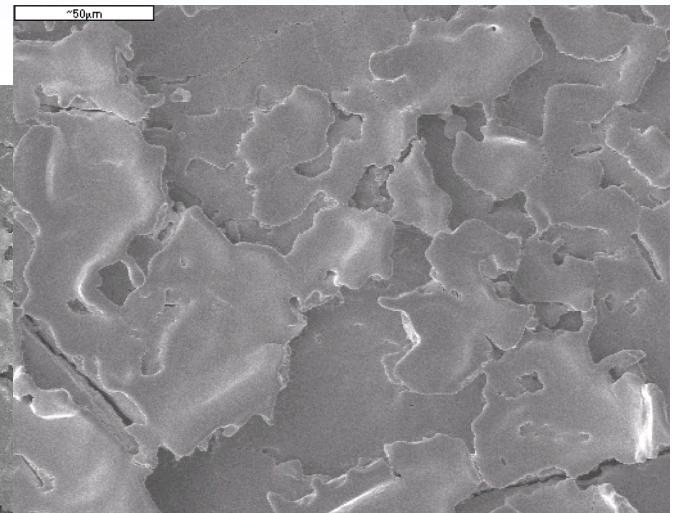


< 1.2 J/cm²

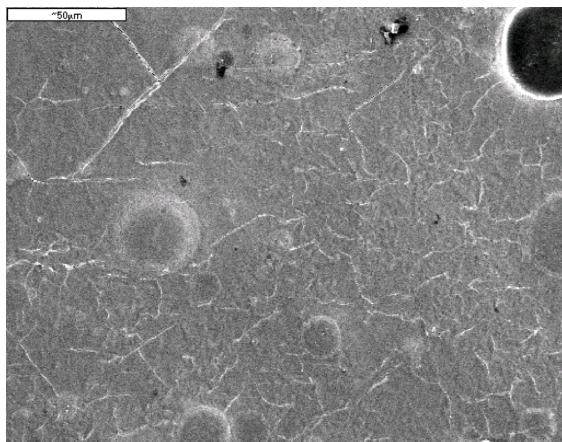


~ 1.2 J/cm²

Top: Nitrogen

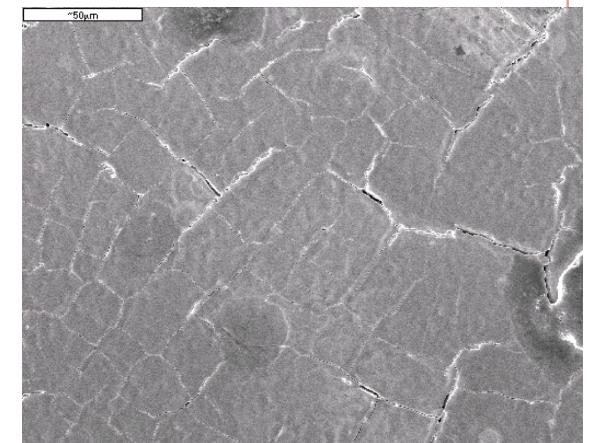


> 1.2 J/cm²



All images 500X Mag except above (250X)

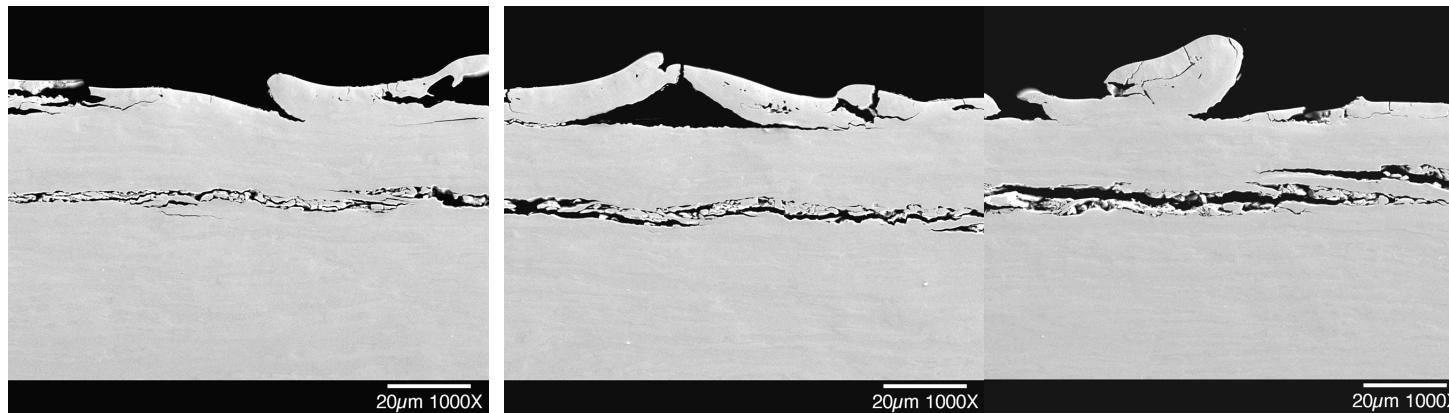
Bottom: Neon



500X Mag

Mass loss: N -306.1 µg, Ne +167.4 µg
(gain due to entrained Cu)

PM Tungsten, 1.9 J/cm² RT, sectioned SEMs (near Melt): Large distortions in near-surface zone

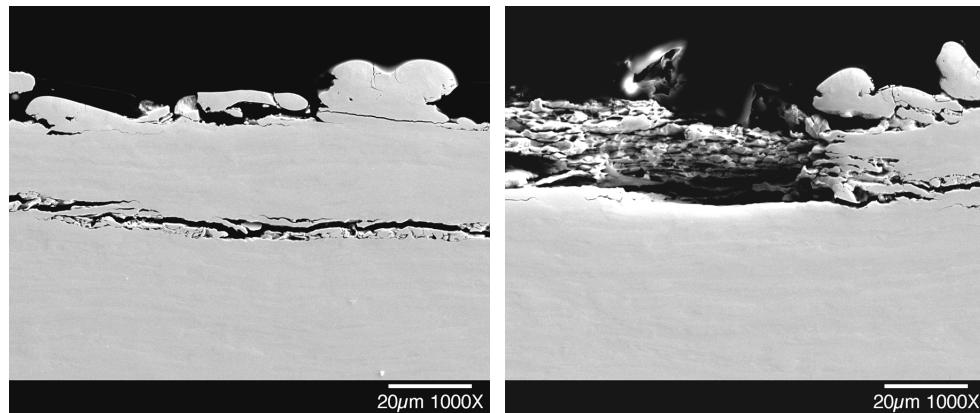


400 pulses

Increasing pulse number



- Wholesale failure down to 20 µm level in last image



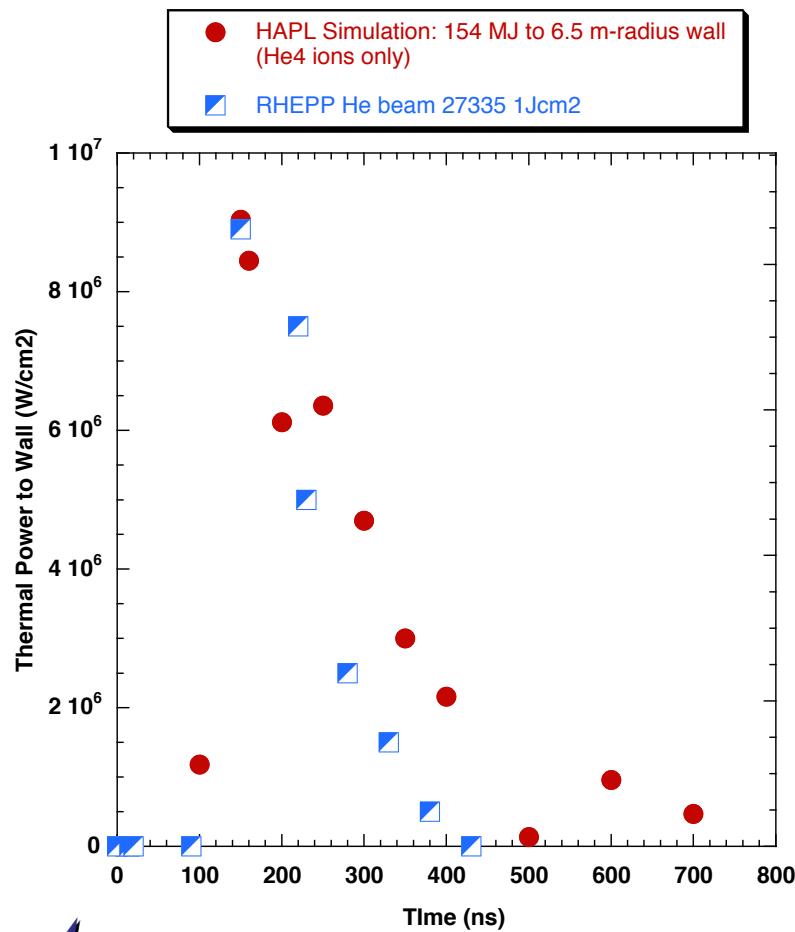
All images BEI 1000X MAG

1600 pulses



Helium beam exposure

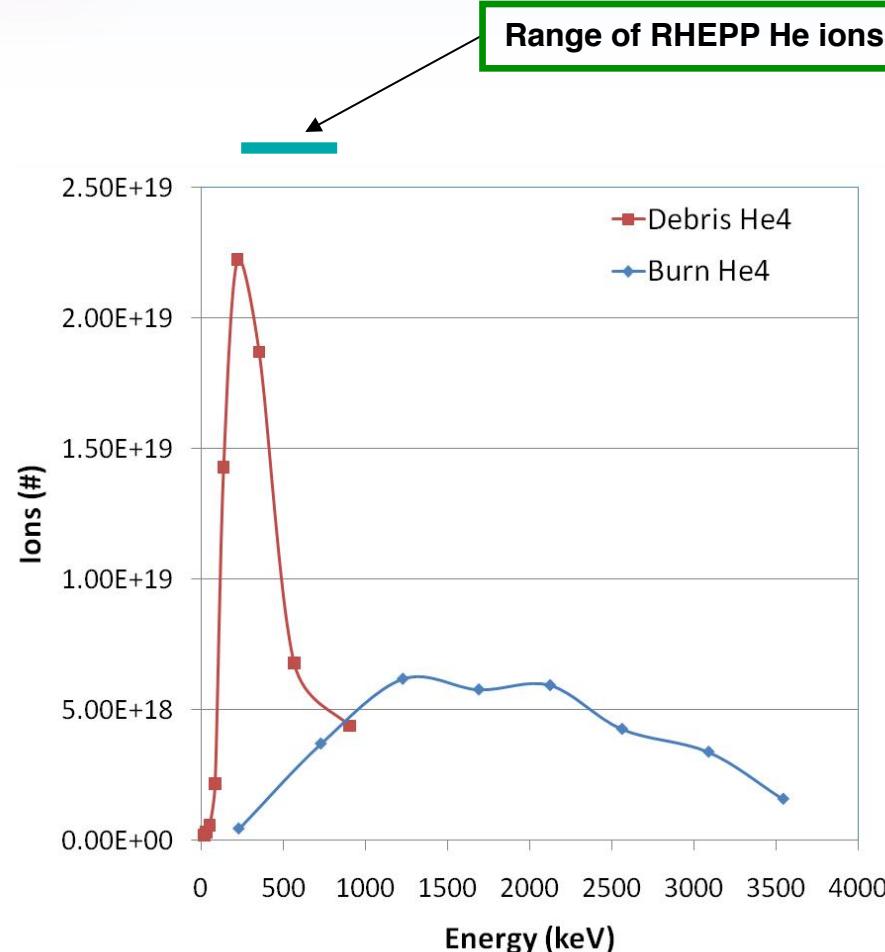
The RHEPP helium beam well simulates IFE threat from both He ion and total Ion current



- **RED:** Simulation, 154 MJ IFE yield, at 6.5 meter wall radius, He₄ ions only
- **BLUE:** RHEPP pulse 27335, He beam, 1 J/cm² fluence, 9e6 W/cm² power density
- He component is ~ 1/3 of total ion pulse (fusion plus debris ions)
- Total pulselength ~ 1.5 μ sec FWHM, vs ~ 80 ns Thermal Power FWHM for RHEPP
- RHEPP 1 J/cm² needs to be 3 J/cm² to include all ion effects. But shorter delivery increases **effective** RHEPP dose by 4x
- RHEPP He beam matches pulse heating time for reactor pulse, and 1-2 J/cm² matches overall power delivery to first wall expected for 154 MJ pulse

Energy Distribution of He⁴ for 401 MJ Target

Raw data: <http://aries.ucsd.edu/ARIES/WDOCS/ARIES-IFE/SPECTRA/>



Thanks to
Shahram Sharafat

COMPARISON:
Each RHEPP pulse delivers
~3e13 He⁴/cm² to treatment
surface at 2.25 J/cm² fluence.
Max surface temp at 2.25J/cm²
~ 2350C

Total: Burn = 3.13e19 He⁴/shot
Debris = 7.31e19 He⁴/shot

He⁴ Fluence (10 m radius chamber):

Burn = 2.49e12 He⁴/cm²
Debris = 5.82e12 He⁴/cm²
Total = 0.83e13 He⁴/cm²

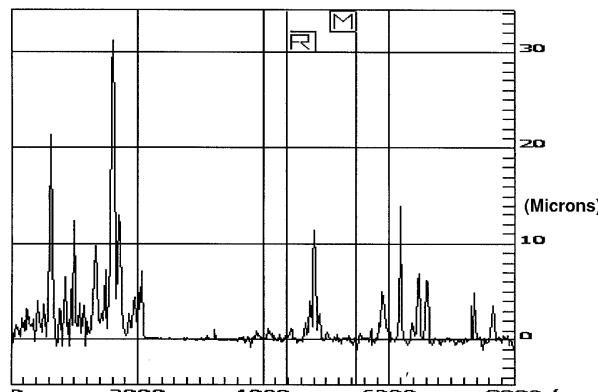
Presented at HAPL Meeting, Madison, September 2003

R_a as function of Number of Nitrogen pulses @ 4.0 J/cm² Helium actually roughens less than nitrogen

I-D 8 mm Profilometer Scans, 450 shots He (Left) and Nitrogen (Right)

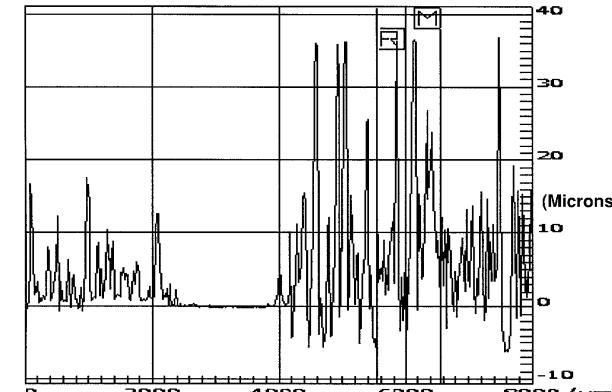
He Beam 1.3 J/cm²

N Beam 4J/cm²



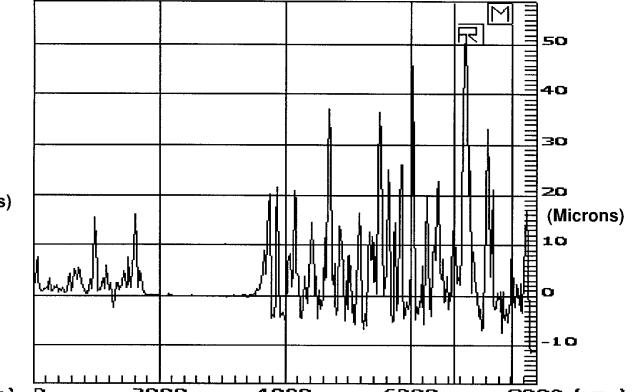
(He-450) (None)

$R_a \sim 1-3 \mu\text{m}$
 $P-V \sim 10-30 \mu\text{m}$



(He-450) (None)

$R_a \sim 1-3 \mu\text{m}$
 $P-V \sim 5-15 \mu\text{m}$



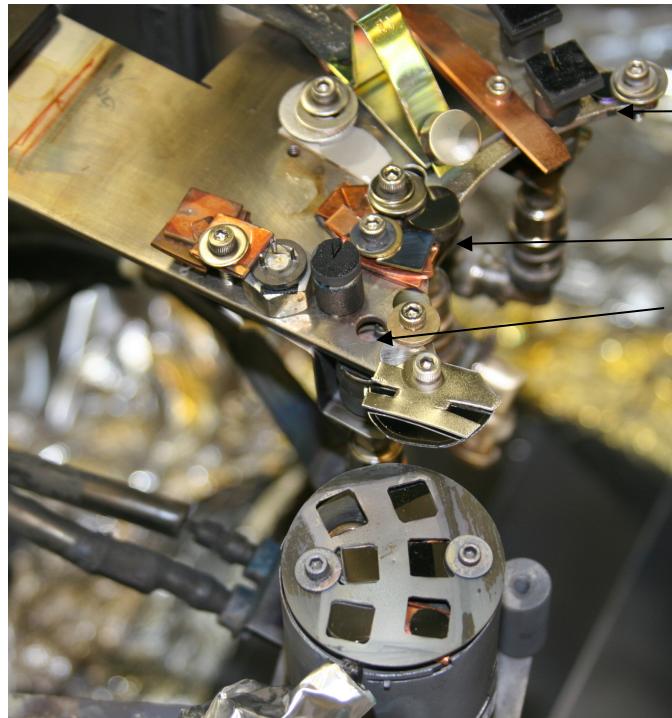
(He-450) (None)

$R_a \sim 7-10 \mu\text{m}$
 $P-V \sim 50-70 \mu\text{m}$

- Roughening of PM Tungsten: 450 pulses He @ 1.3 J/cm² roughens more than 200 pulses N @ 4 J/cm² (Melt)
- N-beam roughening catches up and passes at 400 pulses

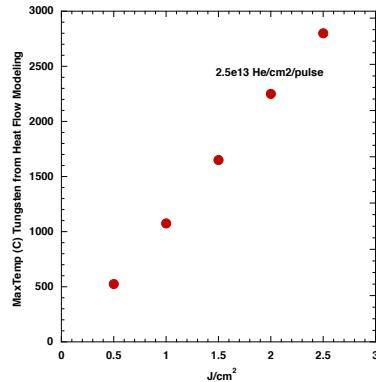
Sample Setup for He1*_1600: four 400 shot series

Samples mounted before Start
Beam Center off to center Right

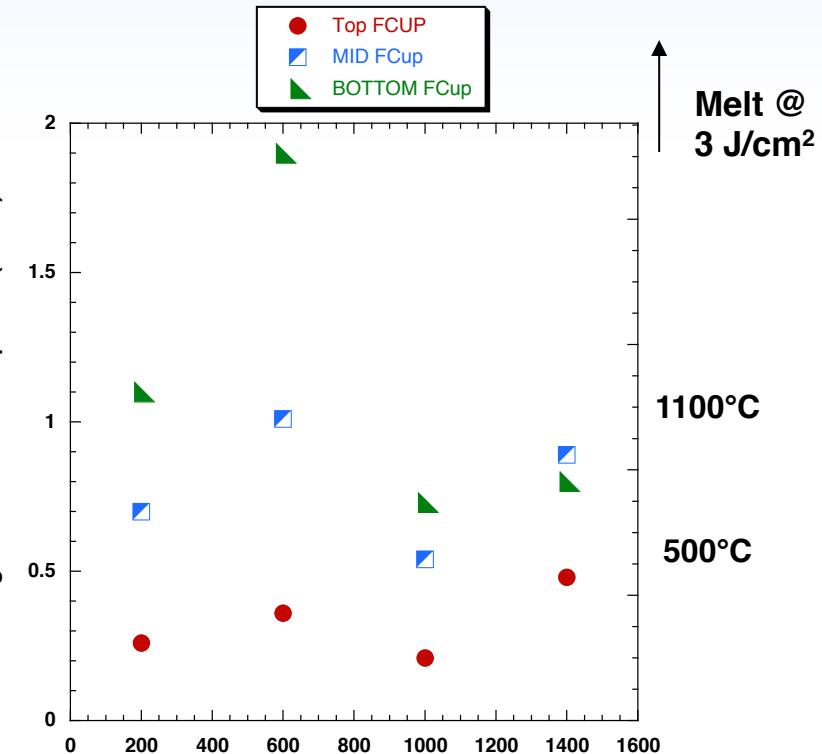


500°C Heater at bottom

'TOP' FCup
'MID' FCup
'BOT' FCup



MaxTemp Vs Fluence (from Heat-Flow modeling)



Shot Number

- 1 J/cm² ~ 1.25e13 He/cm²/pulse
- Fluences and MaxTemps are Averages. ±30% variation in fluence, with outliers to ±50%
- Vacuum ~ Mid e-5 Torr (no Cryos)
- Heated samples not discussed – heating to 520°C doesn't affect results
- 520°C may be below DBTT

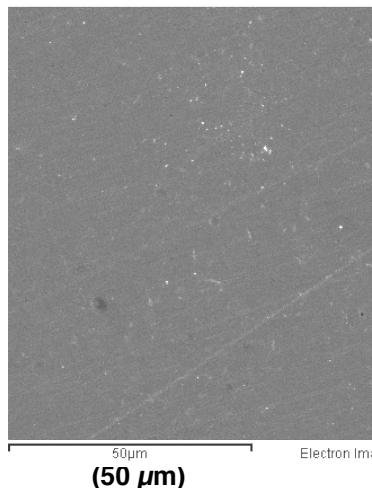
‘Porosity’ evidence in images different from nitrogen

Polycrystalline Tungsten He exposure behavior - 1600 pulses

All samples initially Room Temperature (RT)

Ave 0.8 J/cm²/pulse

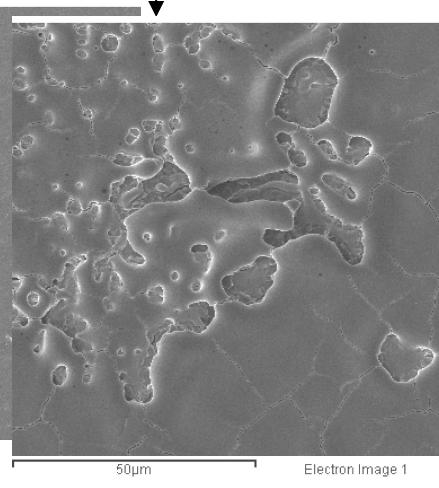
~1000°C
Average
MaxTemp



400 pulses

Ave 1.4 J/cm²/pulse

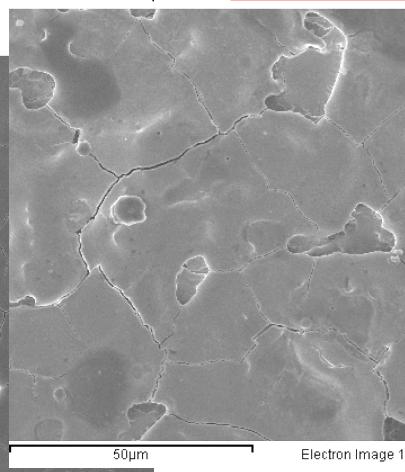
~1500°C
Average
MaxTemp



800 pulses

Ave 0.6 J/cm²/pulse

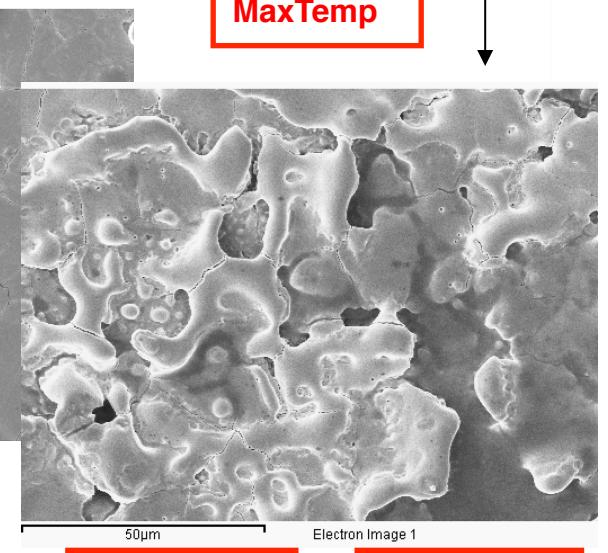
~600°C
Average
MaxTemp



1200 pulses

Ave 0.85 J/cm²/pulse

~1050°C
Average
MaxTemp



1600 pulses

$R_a \sim 1.5 \mu$ m

(Est) total He implantation
 $\sim 1.8 \times 10^{16} / \text{cm}^2$

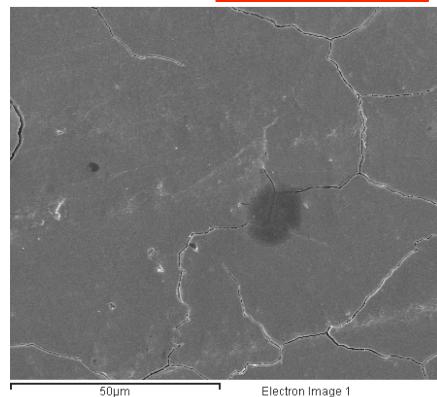
- Average maximum surface temperature < 1500°C
- No effect 1st 400 pulses: below threshold
- Using \sqrt{t} scaling: 0.8 J/cm² equivalent of 0.4 MJ/m². Consistent with QSPA plasma exposure of tungsten PFCs (ref: A. Zhitukhin et al, JNM 363-365 (2007) 301-307)
- Final 400 pulses @ 0.85 J/cm²: probable cumulative mass loss

M184(P) oriented grain tungsten - 1600 pulses

All samples initially Room Temperature (RT)

Ave 0.8 J/cm²/pulse

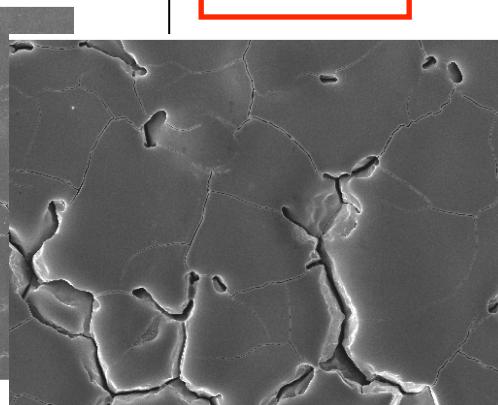
~1000°C



400 pulses

Ave 1.2 J/cm²/pulse

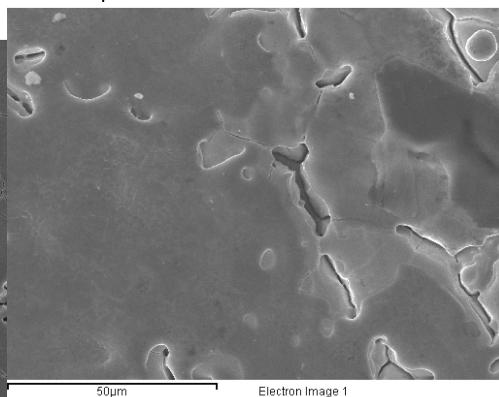
~1300°C



800 pulses

Ave 0.6 J/cm²/pulse

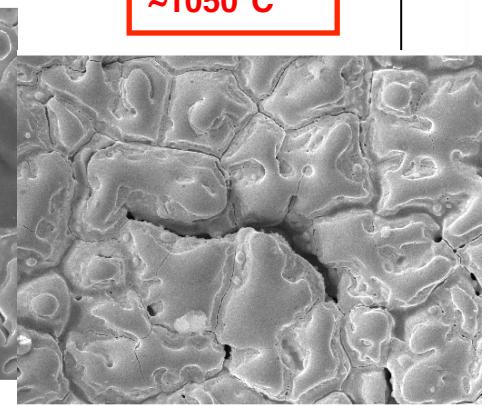
~600°C



1200 pulses

Ave 0.85 J/cm²/pulse

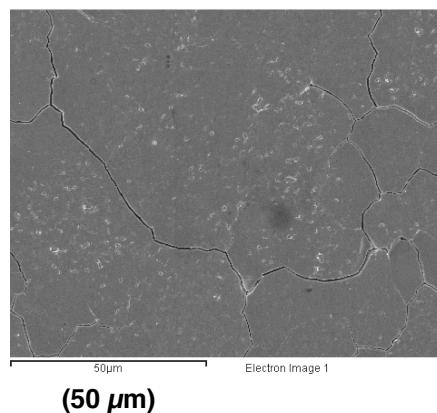
~1050°C



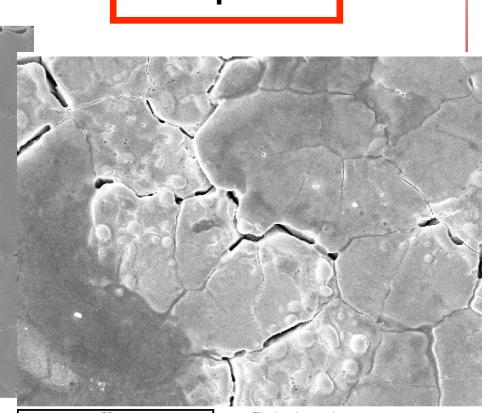
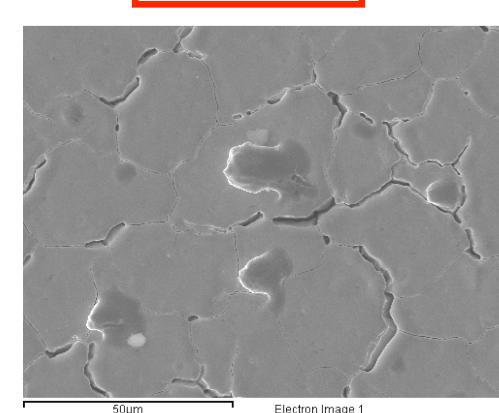
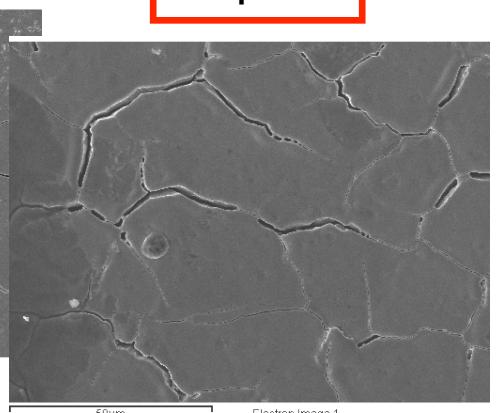
1600 pulses



All images 1000X magnification



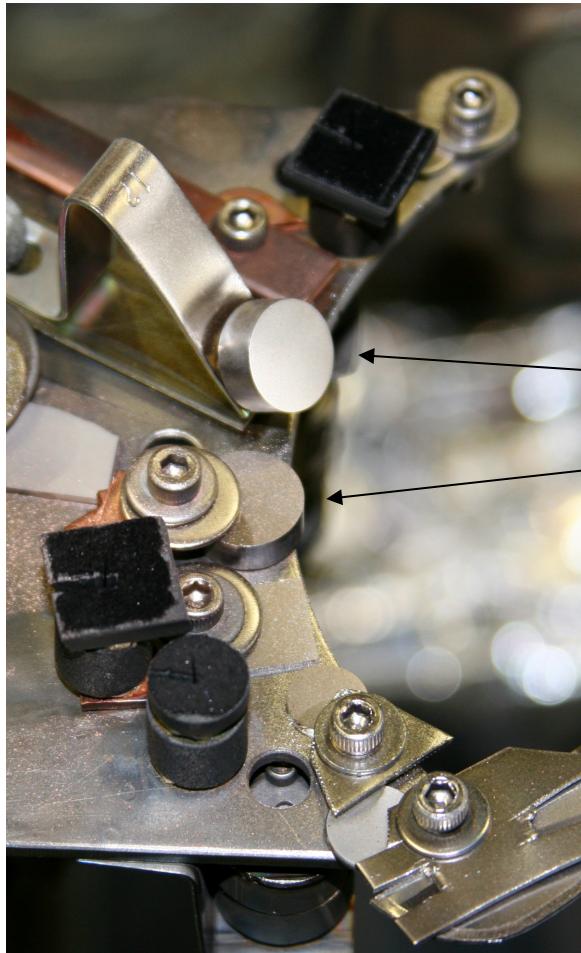
(50 µm)



- Bottom Row: improved performance.
- R_a (TOP) $\sim 1.5 \mu\text{m}$, (BOT) $\sim 0.26 \mu\text{m}$ – SMOOTHER SURFACE



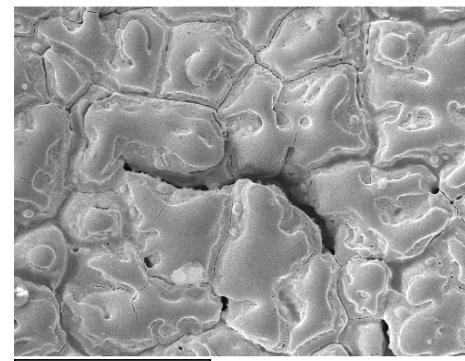
Bottom Row from last slide: Same M184p material tilted at 55° to beam



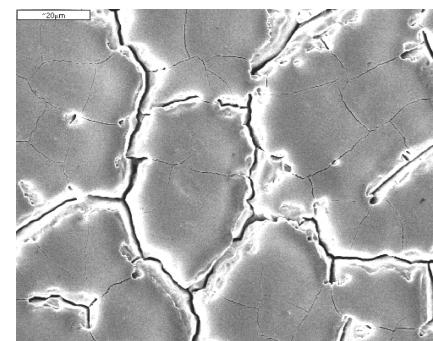
M184p
'Tilt'

M184p

- 55° tilt reduces effective fluence in half
- Does this lead to longer-term survivability?
- Helium looks to cause more roughening than nitrogen beam



M184p – 1600 He pulses

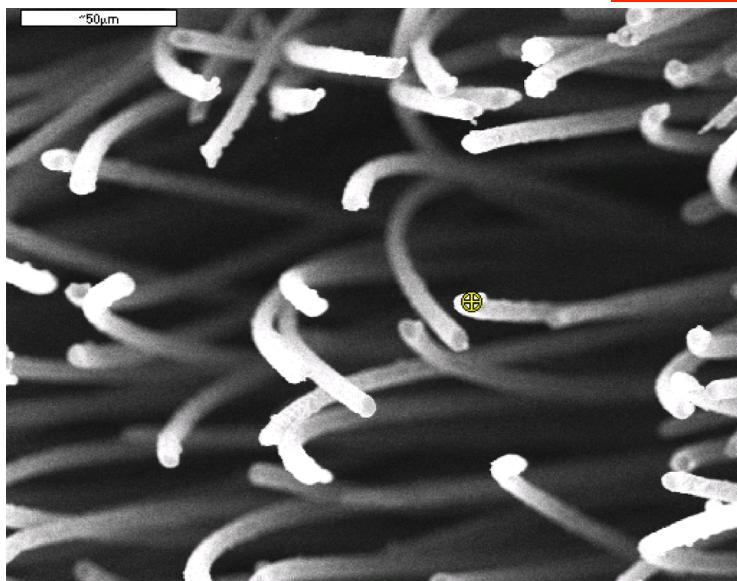


M182p – 1600 N pulses



RHEPP-1 nitrogen beam exposure

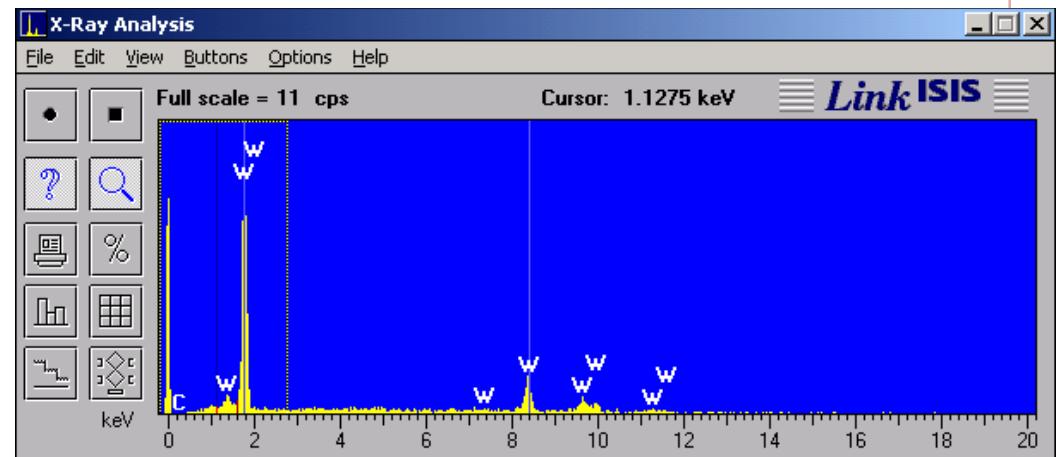
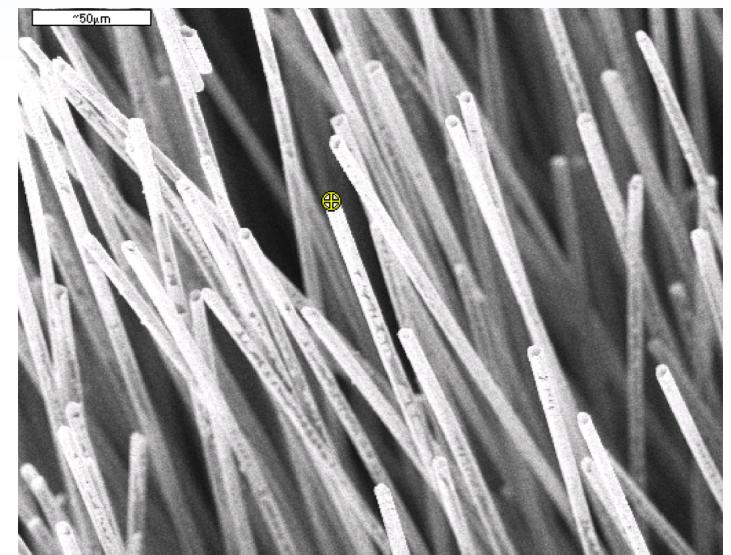
Alternate material: W-coated Carbon 'Velvet' survives 1600 pulses amazingly well



Carbon fibers w/ $1.6 \mu\text{m}$ W coating,
2% areal coverage

(RIGHT)
520C (nominal), 1600
pulses, $1.5 \text{ J/cm}^2/\text{pulse}$

NOTE: W remaining on
tips (see below) and
sides



EDS scan of tip (cross): W rich

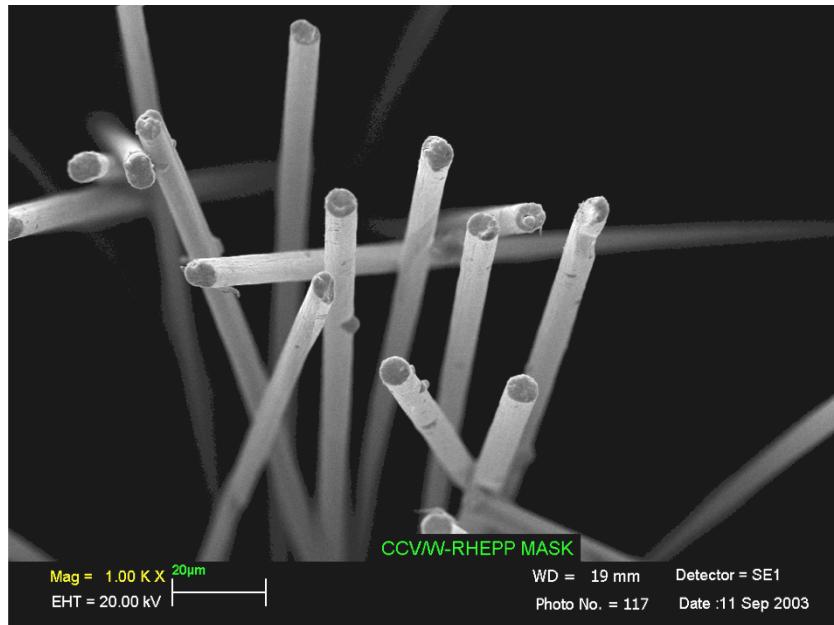


RHEPP-1 nitrogen beam exposure

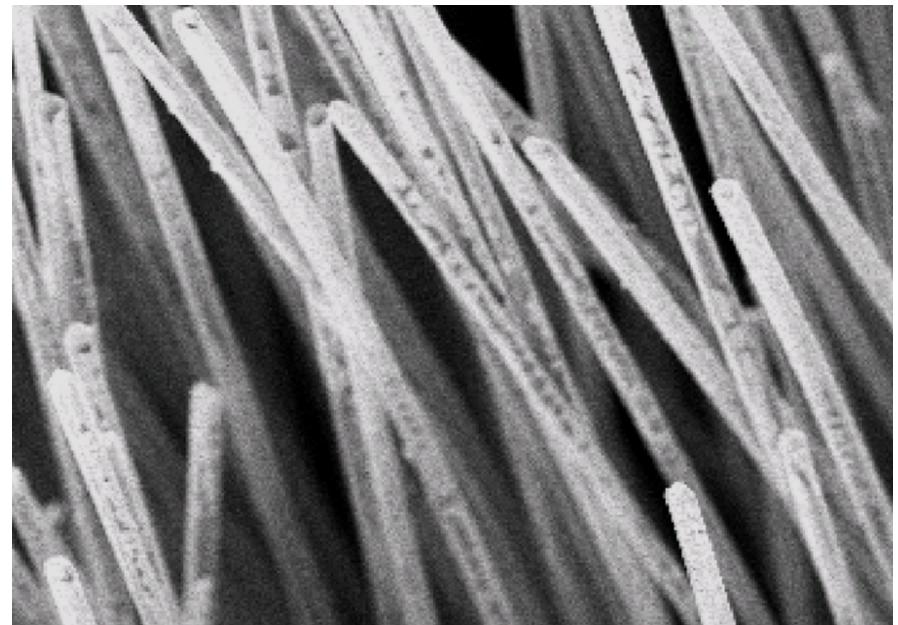
Pulsed Power Sciences, Sandia National Laboratories
TJR 11/25/03

Comparison of SEMs, exposed/unexposed velvet

Carbon fibers w/ 1.6 μm W coating,
2% areal coverage



Untreated Velvet Fibers

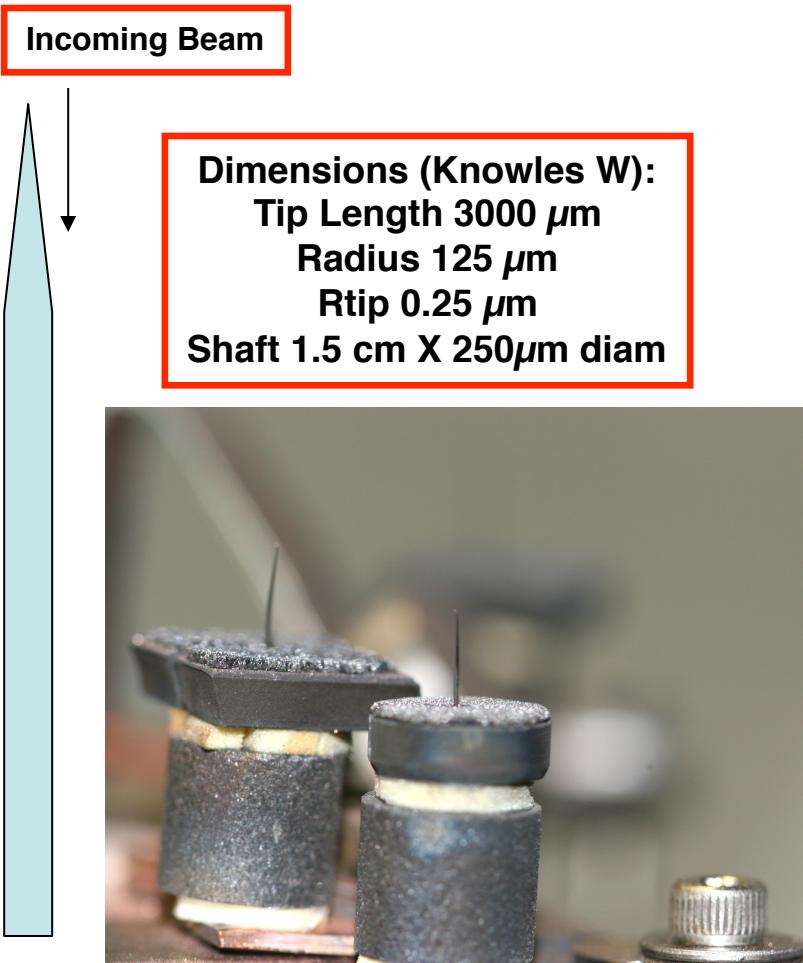




Needles and needle groups as a first wall

T.J. Renk, P. P. Provencio, T. J. Tanaka, J. P. Blanchard, C. J. Martin, and T. R. Knowles,
Survivability of First-Wall Materials in Fusion Devices: an Experimental Study of Material Exposure to Pulsed Energetic Ions, Fusion Science and Technology **61** (2012), 57-80.

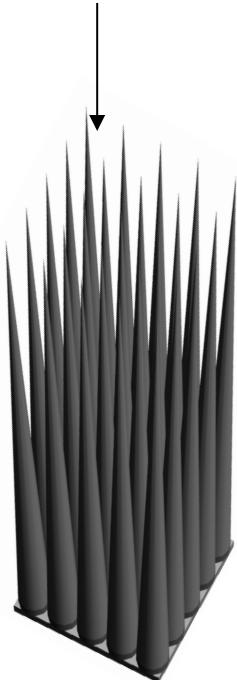
‘Needle’ geometry minimizes full-exposure area, maximizes ‘glancing blow’ area, minimizes He penetration depth



- **Design issues:** overall length, tip geometry (sharpness, etc), assembly into groups
- **Several designs investigated here:**
 - Single Tungsten needle (Knowles-left)
 - Mo-coated W needle: $\sim 0.25 \mu\text{m}$ Mo deposited by RHEPP
 - ‘Array’ -more later
 - ‘Bundle’ -more later
- **Single W needles mounted in holder with carbon velvet at base to minimize blowoff**

Arrays of Needles could be used in both IFE and MFE walls

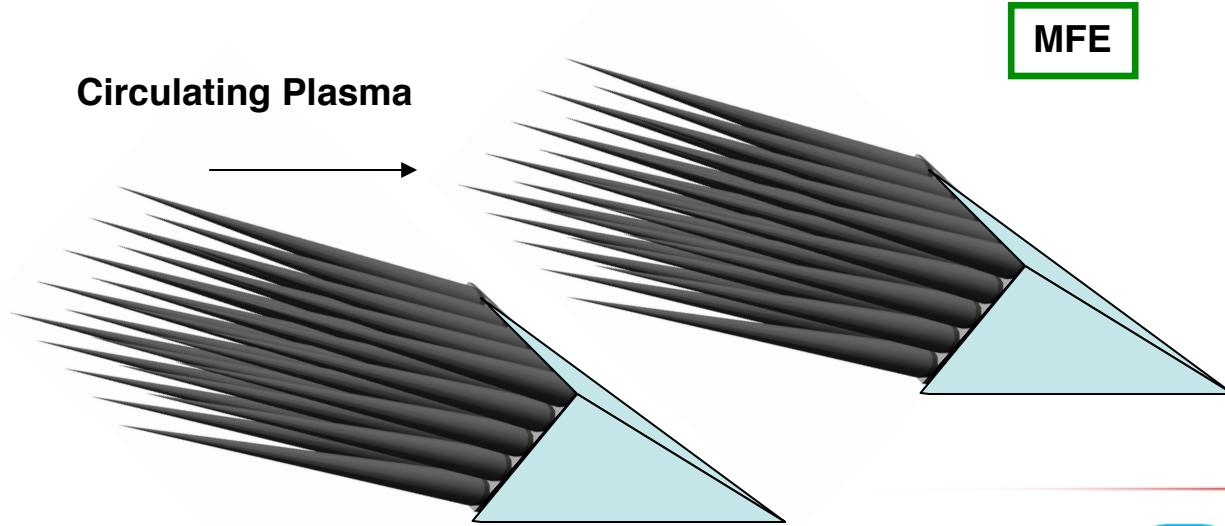
Incoming Ions



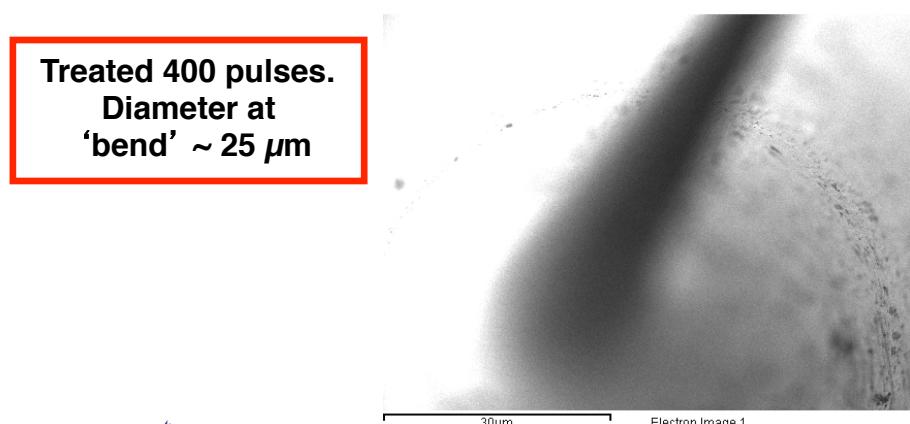
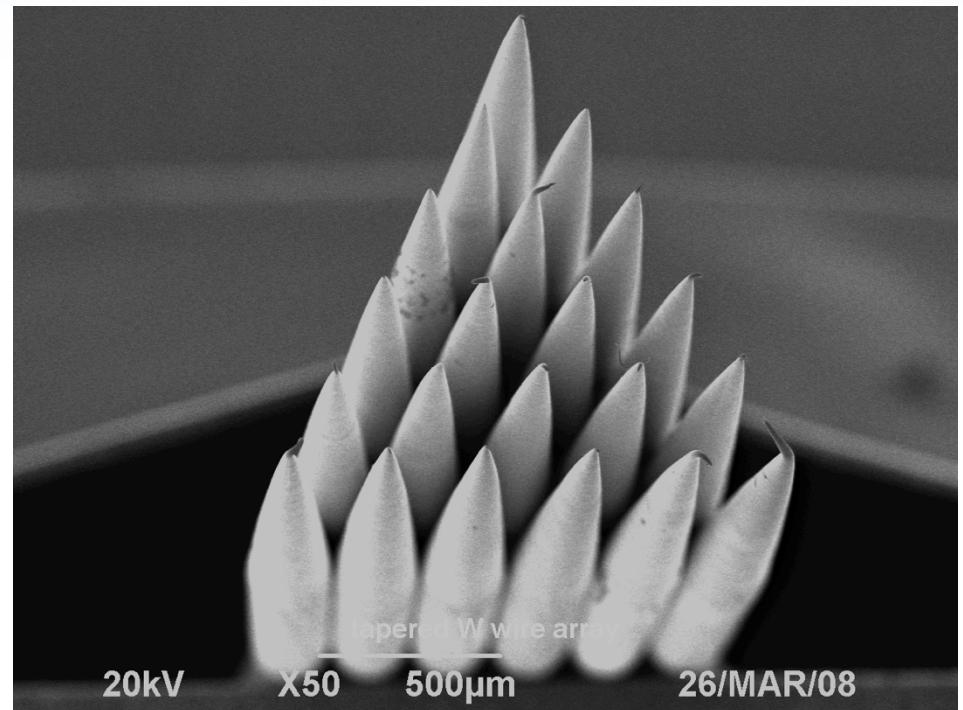
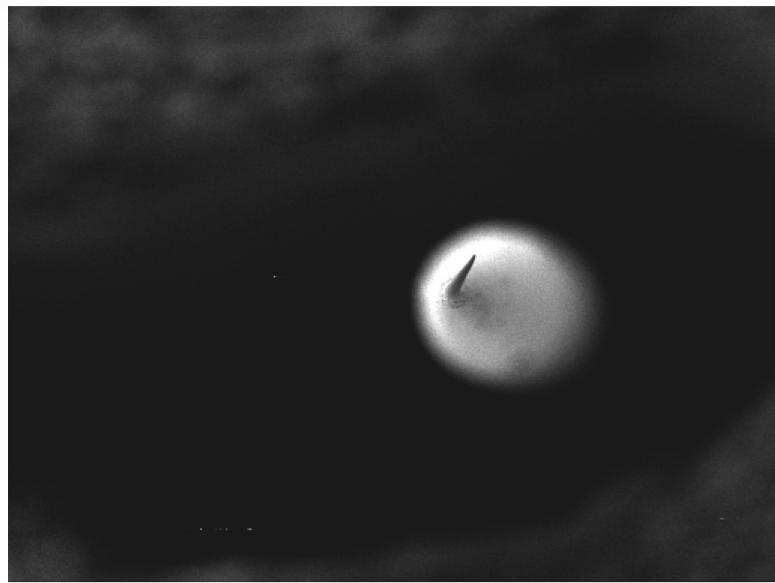
Dimensions (Knowles W):
Tip Length 3000 μm

- Spacing, orientation aspect ratio to be determined
- MFE: arrays of needles on 'pedestals' facing circulating plasma direction

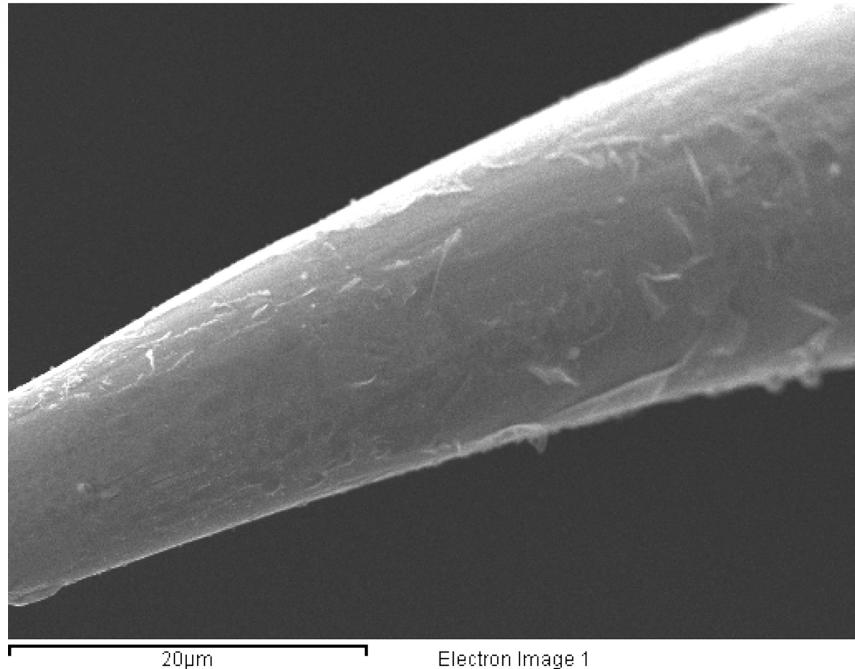
Circulating Plasma



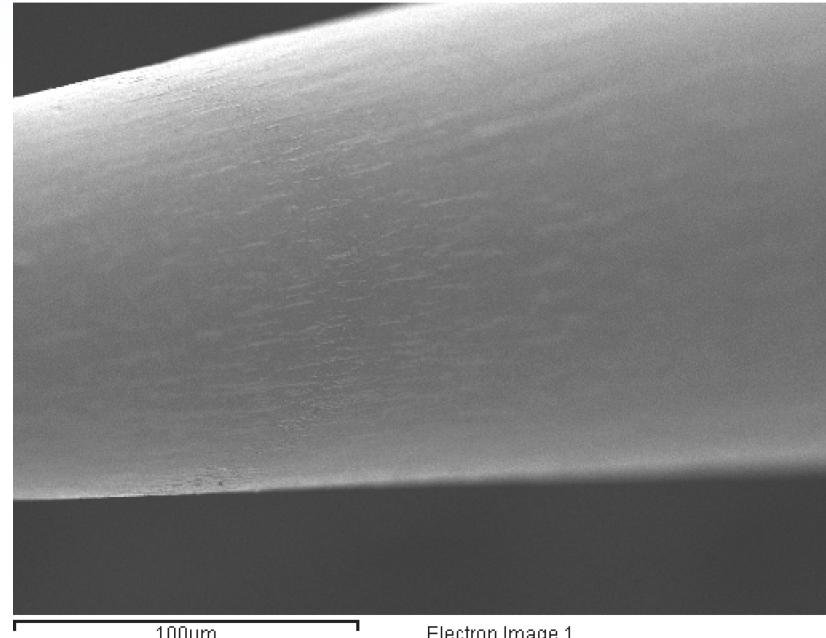
Top SEM view: 400-pulse coated needle compared to virgin (right)



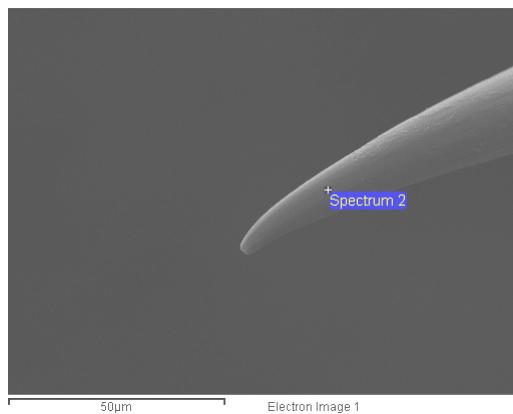
Mo-coated tungsten needle shows no sign of He bubble formation at 800 shots



Near tip

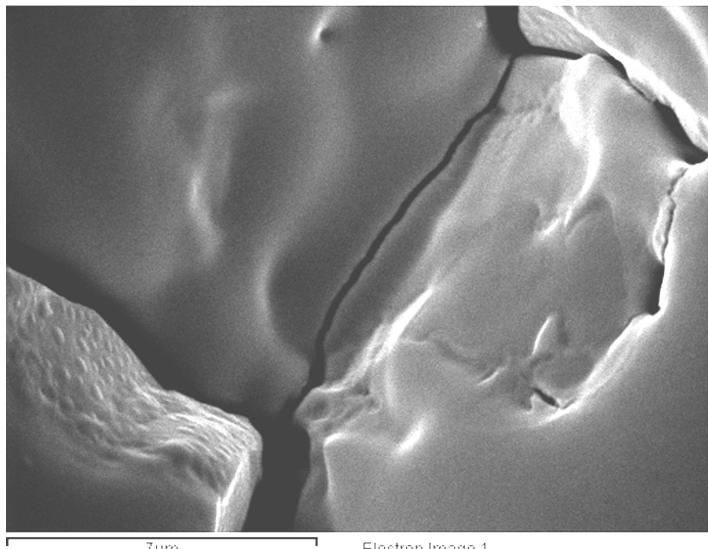


Where EDS shows Mo

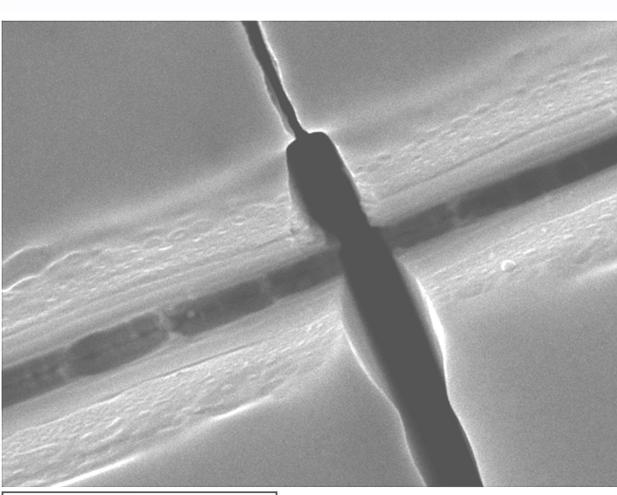


Tip may be blunted

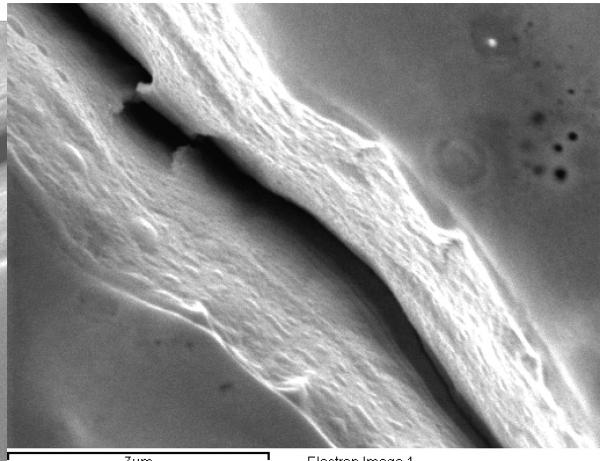
There IS evidence of He bubbles in both flat M184p and single crystal W, at $\sim 1.2 \text{ J/cm}^2$



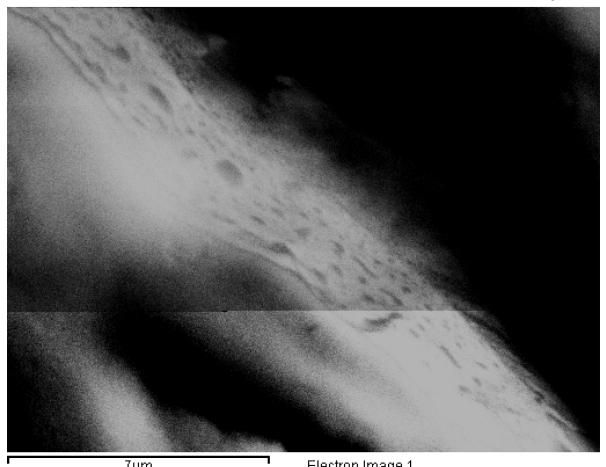
M184perp Room Temp



Single Crystal W RT



Single Crystal 520°C 1200x
Below: BSE image



- Structures occur at 400 pulses and up
- Mostly observed in cracks - consistent with $\sim 1 \mu\text{m}$ He range in RHEPP
- More work is needed to assess exact nature of He retention
- NO EVIDENCE of He bubble/blister formation on needles - up to 1600 pulses

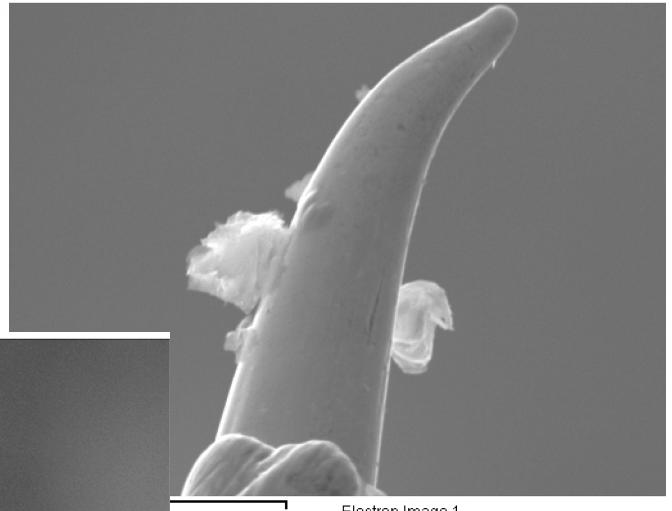
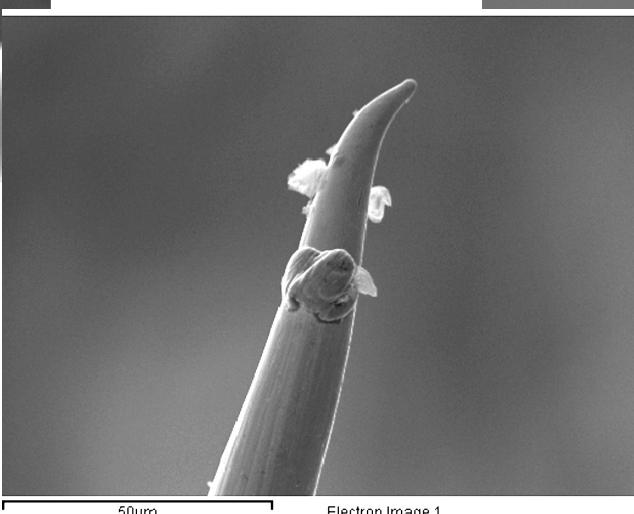
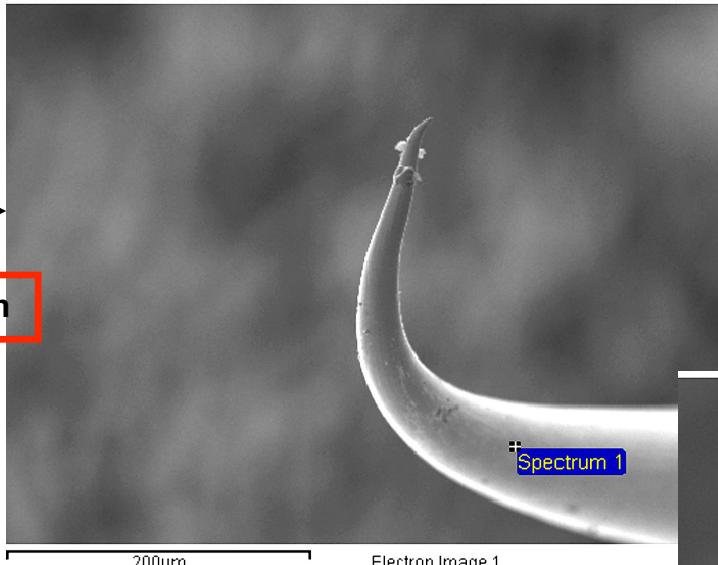
All Images
7500MAG



RHEPP-1 He Ion Exposure

Pulsed Power Sciences, Sandia National Laboratories
TJR 04/16/2004

Mo-coated W needle at 1200 pulses:
markers are Mo coating, 90° bend



Diameter at 'bend' ~ 35 μ m

Mo coating is peeling back from tip, but intact down shaft

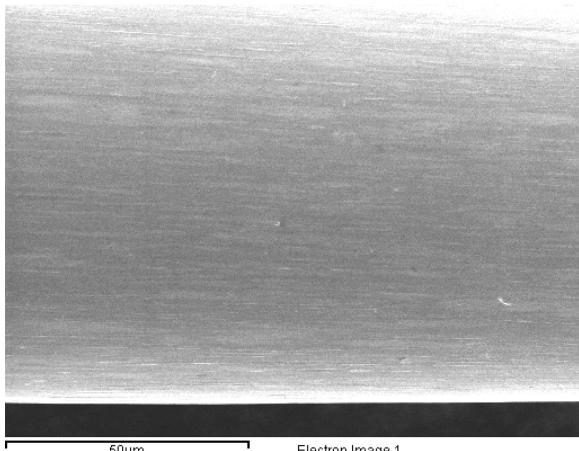
Bent at tip: means full force hits bend. Also means tip cannot erode back
In step-back fashion. This tip almost unaffected by beam



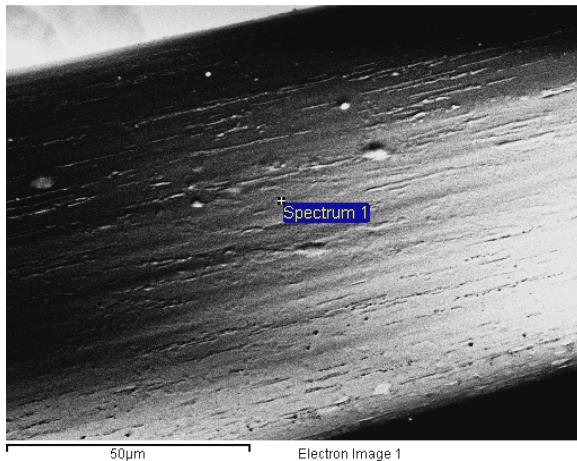
RHEPP-1 He Ion Exposure

Pulsed Power Sciences, Sandia National Laboratories
TJR 04/16/2004

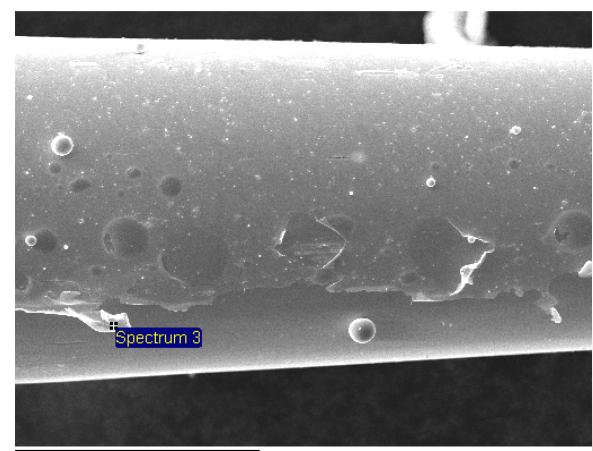
Tungsten needles compared - down shaft away from tip



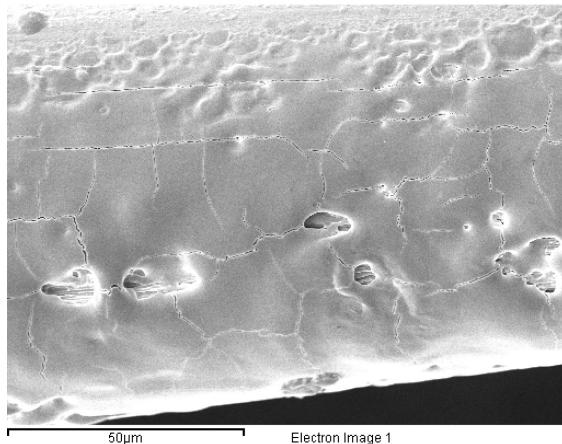
Virgin: 1mm from tip



Mo coated (BSE image): ripples are coating still intact after 1600 pulses. Confirmed by EDS



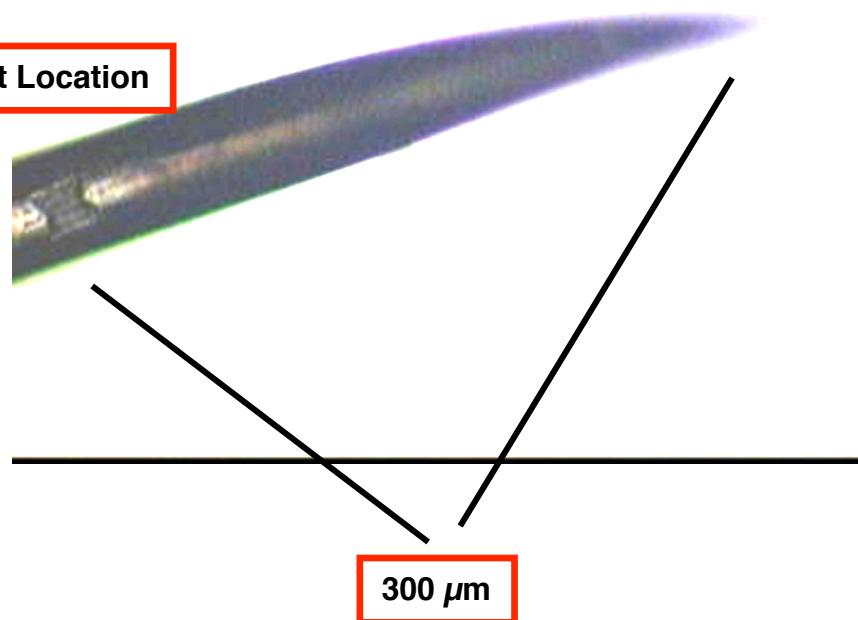
W needle-uncoated: 1600 pulses



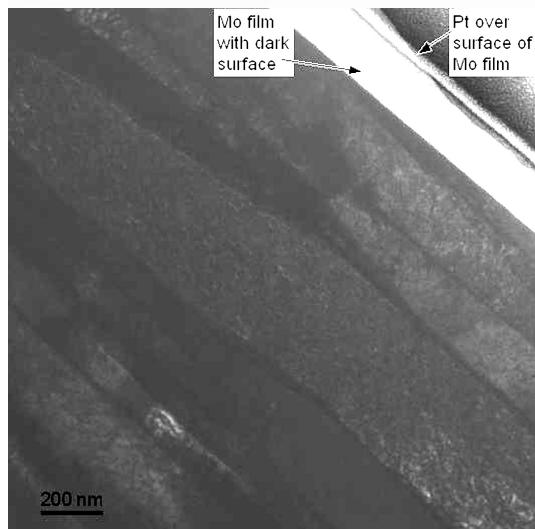
W needle-flat - 400 pulses



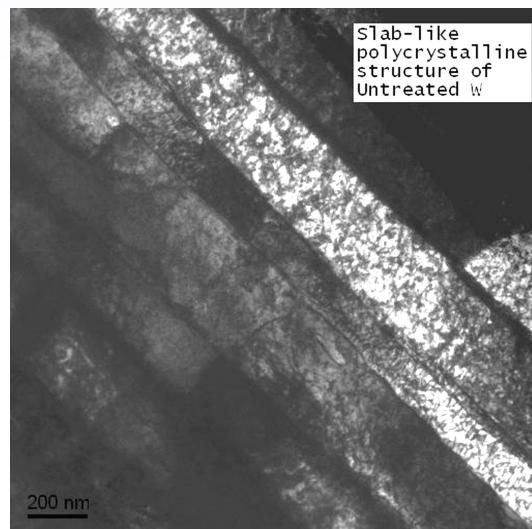
A FIB cut is made into the Mo-coated tungsten needle for XTEM



FIB-XTEM: Mo-coated W needle survives 1600 pulses with no apparent effect vs uncoated untreated W needle

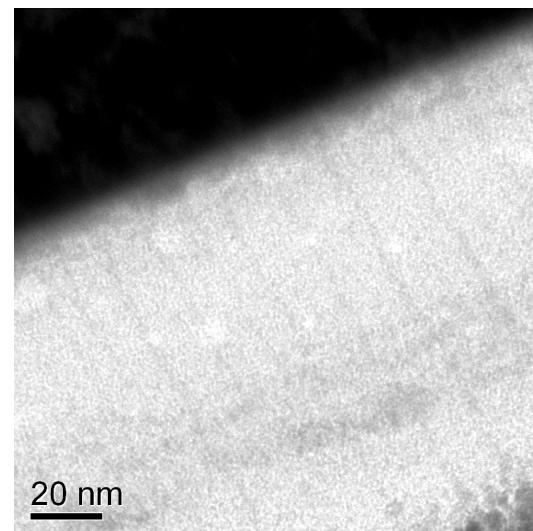


Mo coated - 1600 pulses

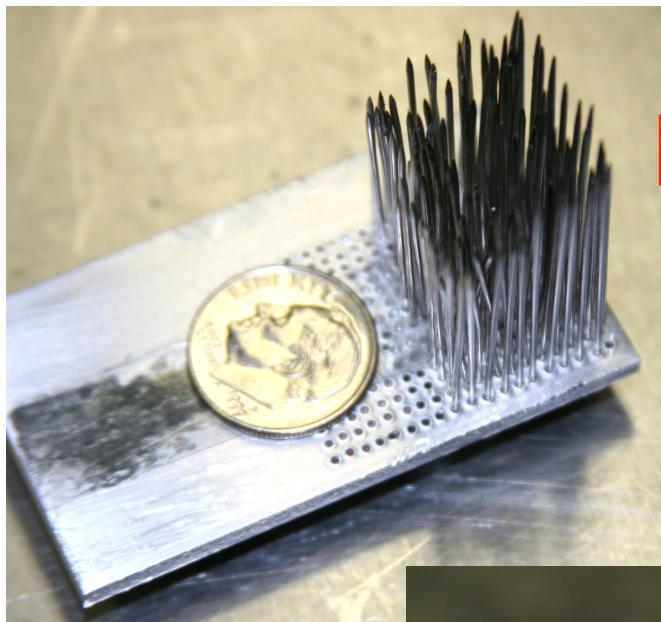


W needle uncoated virgin

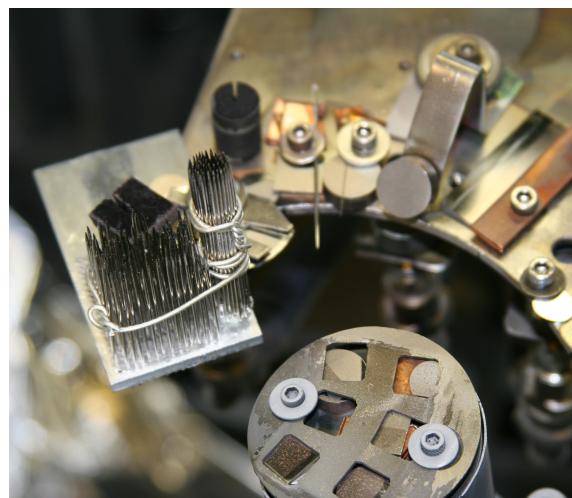
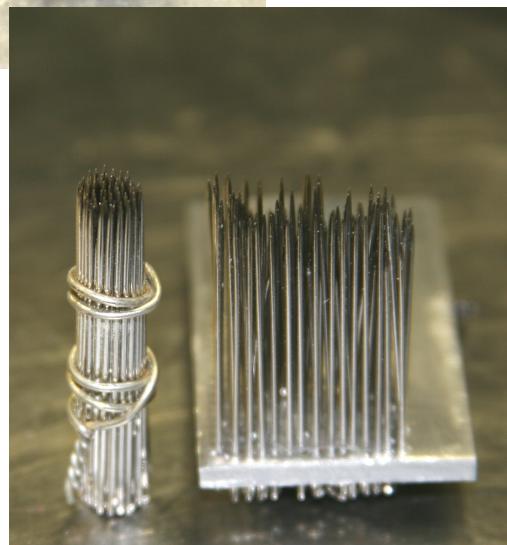
- FIB cuts made in both needle surfaces 300 μm from tip
- Both XTEMs show fully dense tungsten with long oriented grains, no voids, no bubbles/blisters
- Close-up (bottom) shows columnar structure of as-deposited Mo - 200 nm thick - original thickness unknown
- No apparent effect from exposure



Two arrayed needle geometries investigated



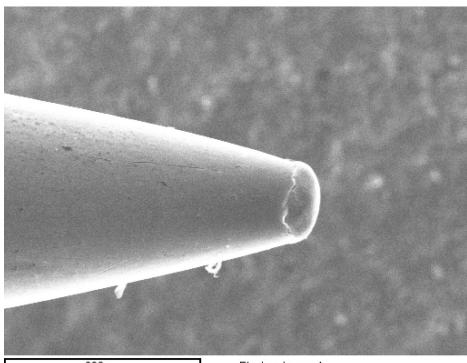
- Left: 'Array' - Sewing needles and dressmaker pins on Al-6061 substrate, **mylar strip in center**. Hole diameter 0.029in, 175 drilled into 1/8 in substrate 0.060in apart.
- Needle Composition; high carbon steel with Nickel plating
- Bottom Left: 'Bundle' - sewing needles tied together by wires
- Below: Arrays mounted before Shots 1201-1600



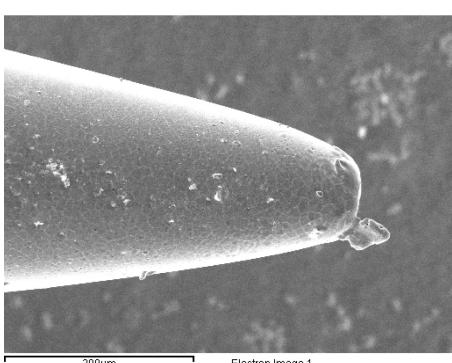


Comparison of Steel needles 400 pulses: virgin, in array, bundled, flat

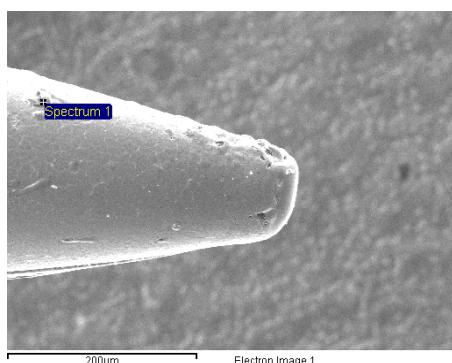
Virgin-Tip



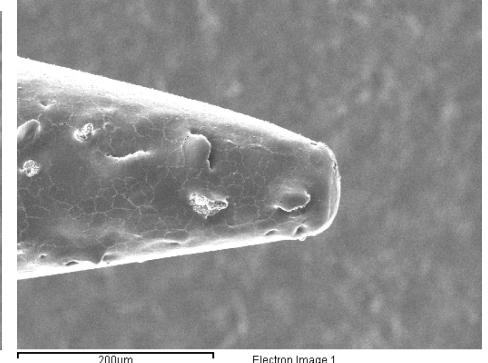
Tip in array



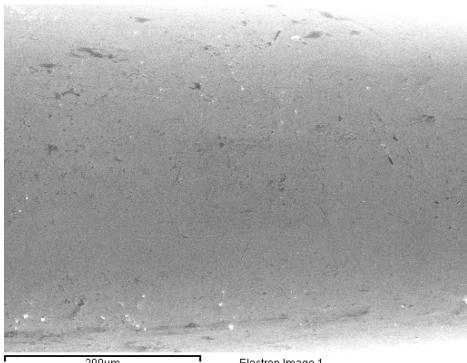
Tip in 'bundle'



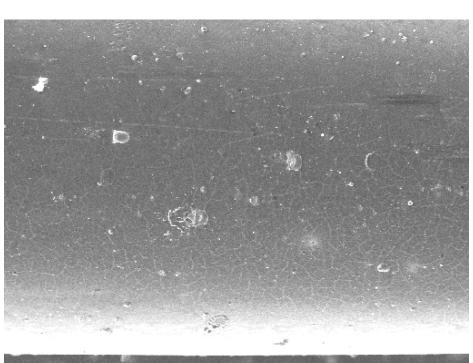
Tip. flat



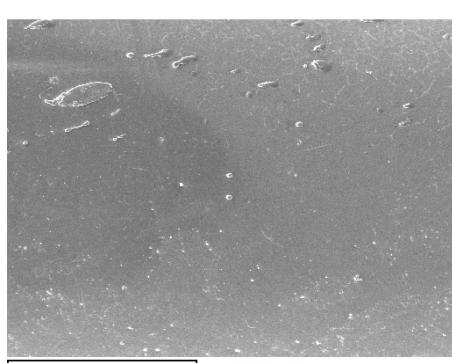
Virgin – 1mm from tip



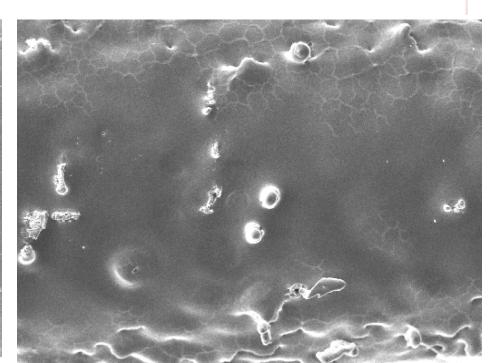
In array – 1mm from tip



In bundle – 2mm from tip

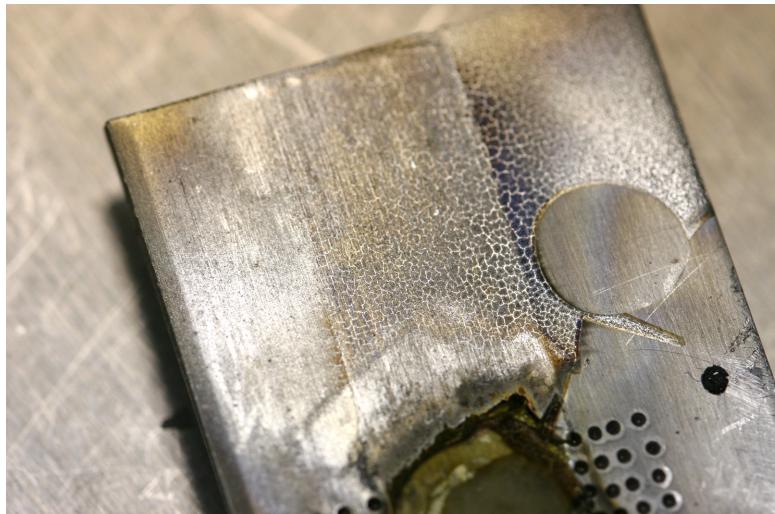


FLAT – 1mm from tip



Away from tip, both bundled and array needle shows almost no effect from 400 pulses

The needles protect the Al-6061 base very effectively:
Mylar strip used as a marker



BACK of Al (no needles):
Mylar removed, Al melted



LEADING edge: Al heavily melted.
In needle 'forest', no Al damage

- Exposed mylar eroded away
- Inside the 'forest', complete protection of Al substrate, mylar partially intact

Attempt to measure Mass Loss: 4 samples tested post-1600 show mass GAIN

Sample	Mass Gain (μg)	% Gain	$\mu\text{g}/\text{cm}^2$
PM Tungsten	6.358	0.35	6.358
M184p FLAT	5.378	0.0532	5.378
M184p TILT	115.9	1.07	115.9
W/M Needle	2.768	1.72	(35.2)

- Gain occurs due to Cu adsorption from incoming beam
- M184p TILT gained by far the most mass
- PM tungsten AND M184P FLAT gained similar mass/ cm^2
- On Areal basis, W/M Needle gained similarly with M184p FLAT
- Assume 116 μg on M184P tilt is entrained Cu. Then Pm tungsten LOST $\sim 95 \mu\text{g}$.
- Then needle area is consistent with $< 1 \mu\text{g}$ gain. Actually gained 2.7 μg .
- Total data on W needles consistent with little or no mass loss due to 1600 exposures.

Summary – fusion materials exposure

- RHEPP pulsed width similar to He_4 component in reactor, 1-2 J/cm^2 produces comparable power loading as 154 MJ pulse to 6.5 m-radius wall, comparable He implantation as 415 MJ pulse to 10m-radius wall.
- ‘Needles’ show promise as robust alternative to flat geometry. Little or no affect from 1600 He beam pulses.
 - CAVEAT: THE RHEPP IONS ARE NOT PARALLEL. Must investigate affective fluence compared to parallel ion path expected in reactor.
- Helium exposure of tungsten flats at up to 1600 pulses shows in all cases more surface roughening/signs of exfoliation than with comparable nitrogen pulses. **Not Clear That Any of FLAT Materials RHEPP-tested will survive.**
 - ROCK: effects here **are NOT** due to He entrainment, i.e. **1e18 cm-2** reported He blister formation threshold holds here, and results seen here are due to thermomechanical stress only. Then samples do not appear to be able to reach **1e18 cm-2** without unacceptable morphology change/weight loss.
 - HARD PLACE: effects seen **ARE** due to He entrainment, then threshold for pulsed He exposure is more like upper **1e15 cm-2**.



Questions?

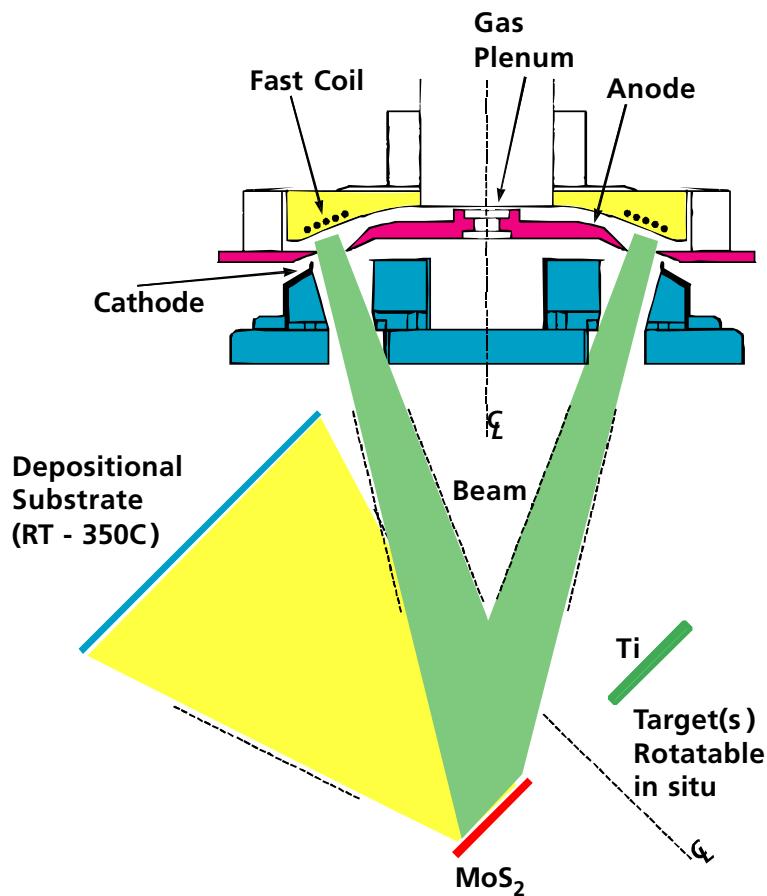


Backup Slides



Ablation study of sub-range foils

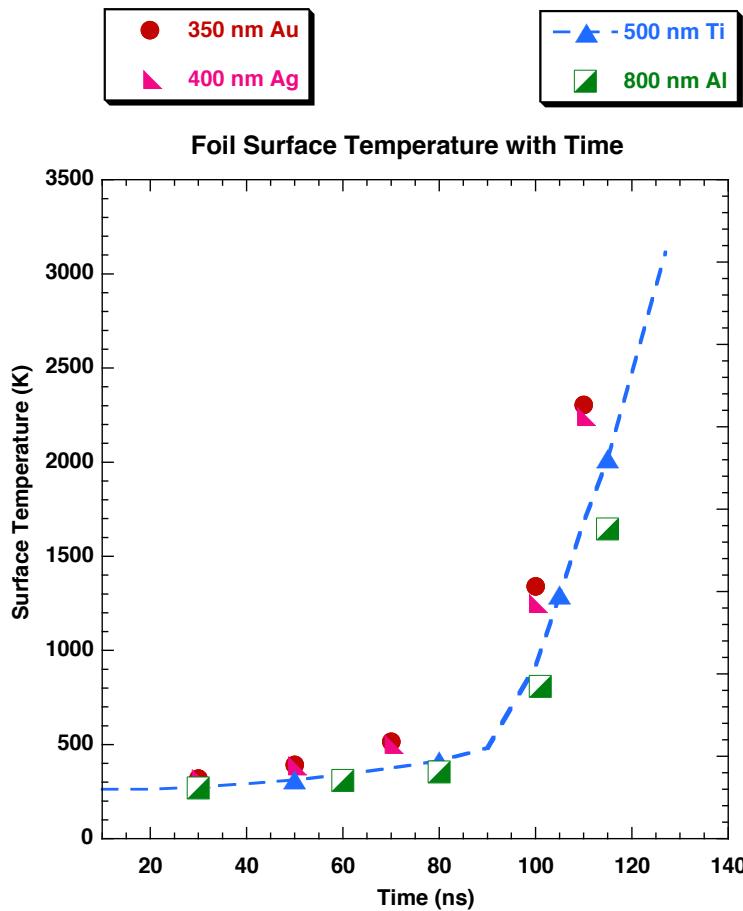
The RHEPP-1 nitrogen beam was used in sub-range foil ablation experiments



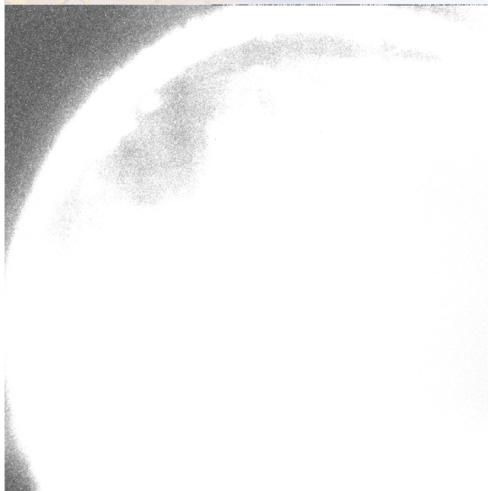
- High-energy pulsed ions (700 kV, 200 A/cm²) vaporize and redeposit material. Geometry as shown.
- Foils mounted on same ablation setup for mechanical rigidity. Normal 6-8 J/cm² at beam center reduced by factor 0.707.
- Foils exposed:
 - 650 nm, 800 nm Al 2 - 6.4 to 11.5 cm (Lebow)
 - 400 nm Ag 4 cm
- **Conditions DURING ablation not known: analysis of framing images MAY yield clues about ablation dynamics**

1-D Heat flow modeling: RHEPP nitrogen beam on sub-range foils

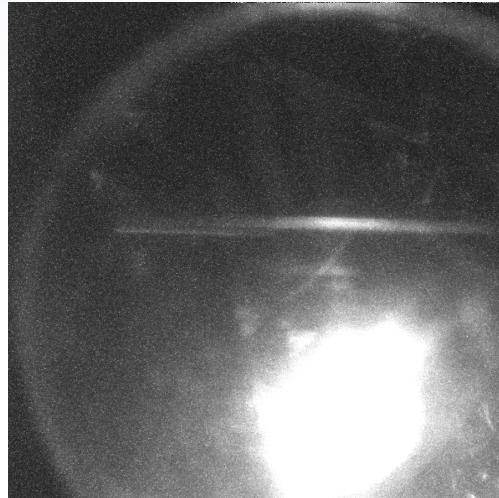
- Purpose – predict thermal response of sub-range (for RHEPP) Au, Ag, Ti, Al. Look for fastest heating rate.
- Proton precursor to 90 ns, then Ni (++) heating starts
- Au heats from surface melting to ablation in ~ 15 ns
 - Ag not far behind
 - 800 nm Al too slow



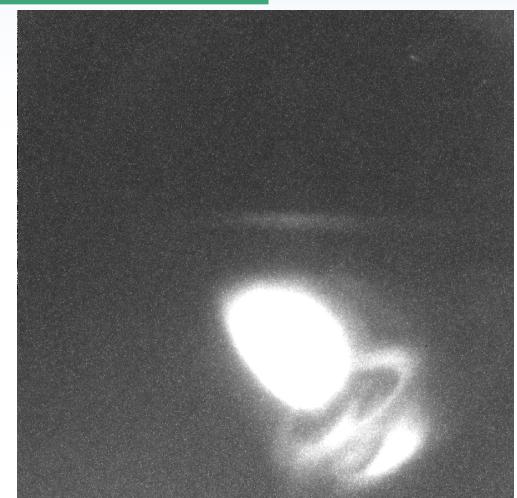
1st Experiment: plume evolution, solid titanium target



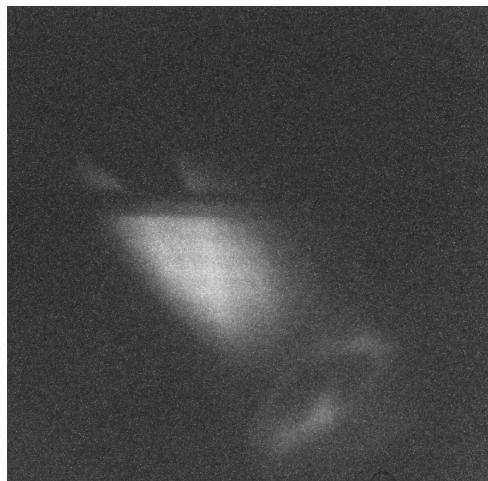
$T = 0 \text{ sec (arbitrary)}$



$T = 2.35 \mu\text{sec}$



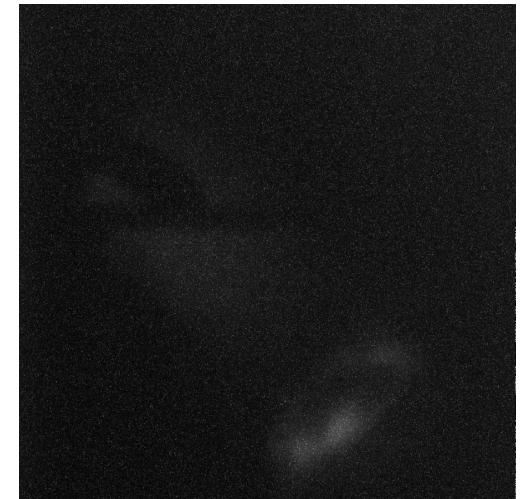
$T = 7.35 \mu\text{sec}$



$T = 12.35 \mu\text{sec}$



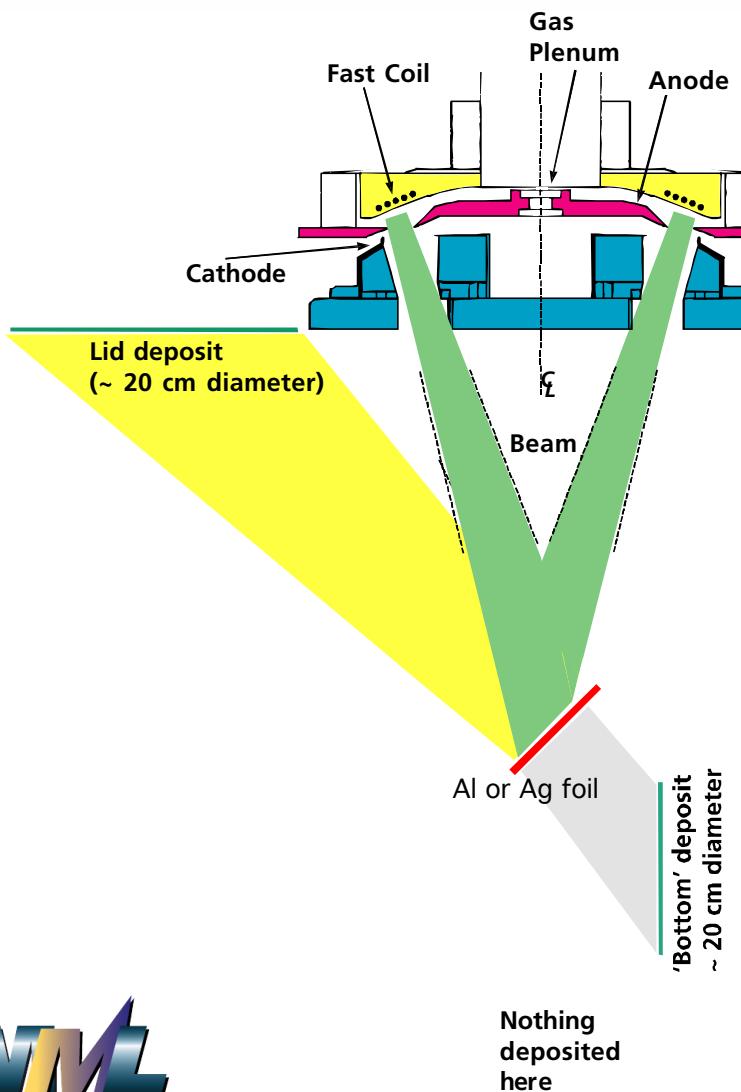
$T = 17.35 \mu\text{sec}$



$T = 22.35 \mu\text{sec}$

Note: 1) slowness of plume evolution, 2) 100 nsec exposure time

The RHEPP-1 nitrogen beam strikes foil at 45°, and film is deposited in both directions normal to foil plane



- High-energy pulsed ions (700 kV, 200 A/cm²) vaporize and redeposit material. Geometry as shown.
- 'Lid' deposit at ~ 50-60 cm distance, 'bottom' deposit at ~ 20 cm distance. Si wafer mounted for 1-D dek-tak thickness profile measurements
- No deposition observed at tank bottom
- Foils exposed:
 - 650 nm Al 11.5 cm diam (Lebow)
 - 400 nm Ag 4 cm diam (Lebow)

40 mm diameter Ag target, Shot 2039

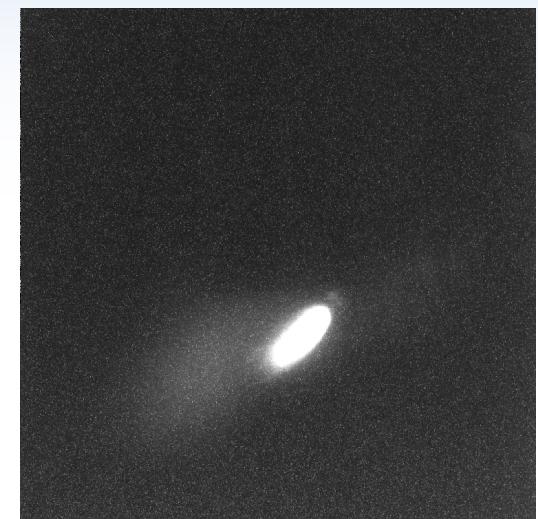
Exposure = 5 ns



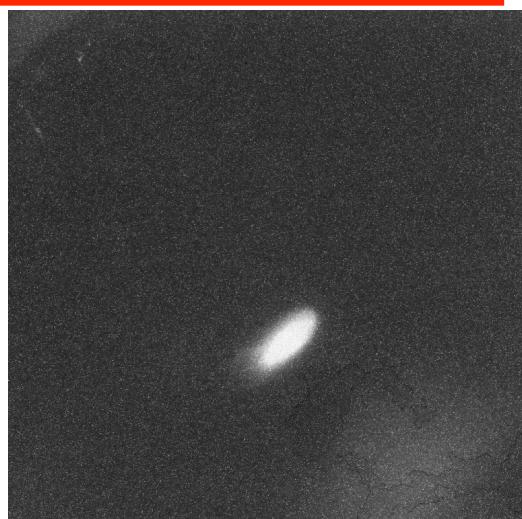
T = 4100 ns (arbitrary)



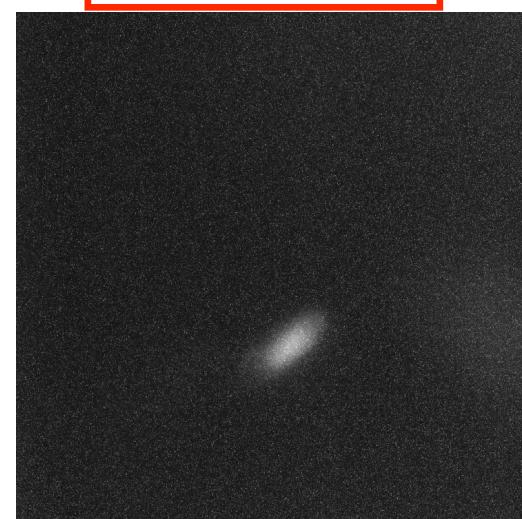
T = 4250 ns



T = 4400 ns



T = 4700 ns



T = 4850 ns



T = 5000 ns

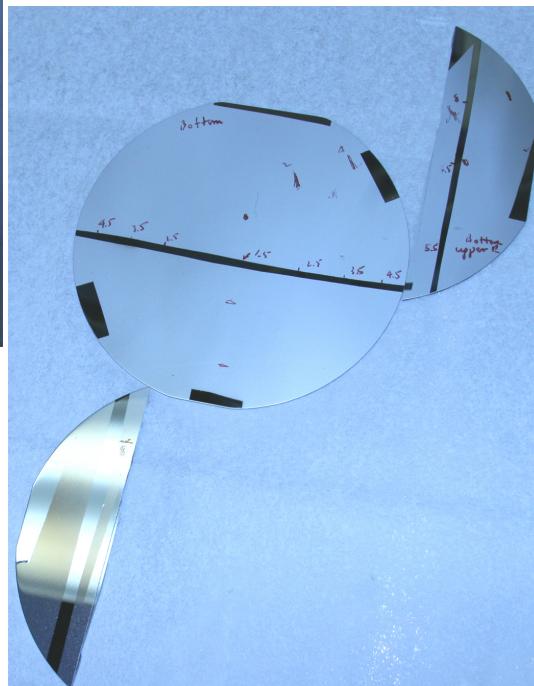
Note: 1) diameter shrinks with time, 2) 900 ns total time duration

Photos of Si wafers after 7 shots



Si wafers on top lid after shots

- (Left) Deposit on top lid
- (Bottom) bottom Si wafers demounted on bench
- (lower right) note cm-markers on close-up of film, heterogeneous appearance.

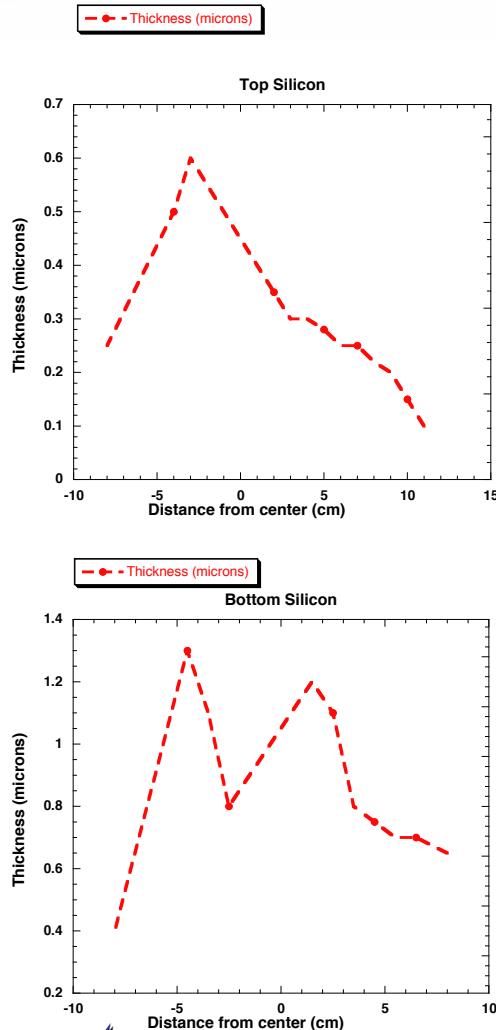


Bottom Si wafers on bench



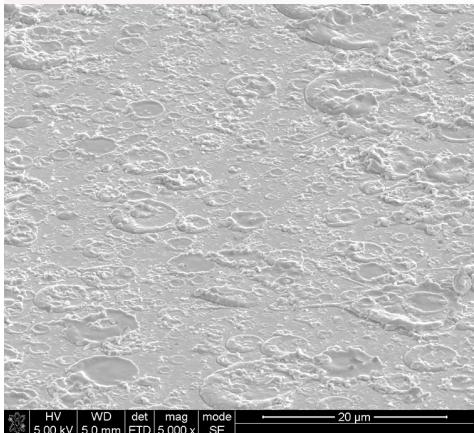
Closeup, deposited material

The RHEPP-1 nitrogen beam strikes foil at 45°, and film is deposited in both directions normal to foil plane

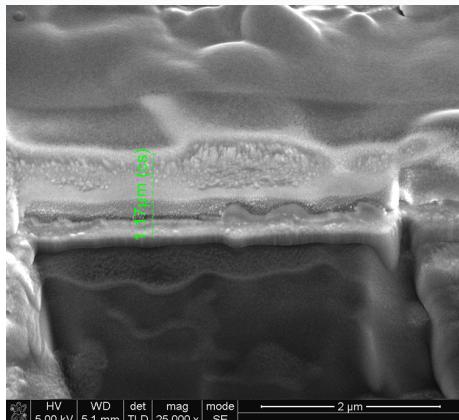


- 1-D dek-tak thickness measurements made of both top and bottom depositions. Two chords measured from (approx) deposition center (left).
- 'Smoothed profile overlaid, material inventoried using average thicknesses and $2\pi r \Delta r$ additions.
- Totals: $81 \mu\text{m}\cdot\text{cm}^2$ top, $181 \mu\text{m}\cdot\text{cm}^2$ bottom, $265 \mu\text{m}\cdot\text{cm}^2$ total. FIB-SEM of samples shows $\sim 25\text{-}50\%$ increase in thickness compared to dek-tak
- Total volume of 7 foils shot (not including He shot): $479 \mu\text{m}\cdot\text{cm}^2$. So between 70 and 85% of initial mass accounted for.
- Foil surface rough - typical $R_A \sim 0.3 \mu\text{m}$

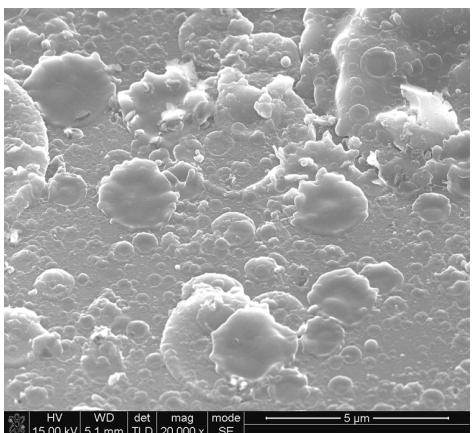
The RHEPP-1 deposited film appears to be formed of droplets, but film appears slightly porous to fully dense



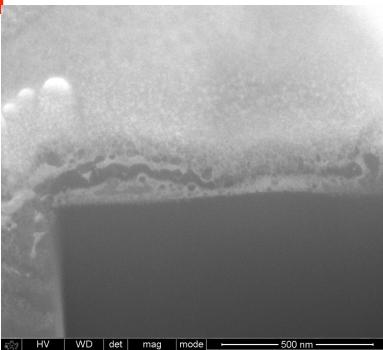
SEM, deposited material, 'top' 3 cm radius



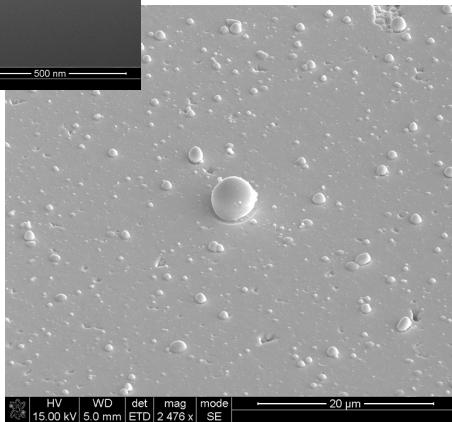
FIB/XTEM, top 3 cm film



SEM, deposited material, 'top' 5 cm radius



FIB/XTEM, top 5 cm film



SEM, Ni film from solid target

- 'Smoothed profile overlaid, material inventoried using average thicknesses and $2\pi r\Delta r$ additions.
- FIB-SEM of Top 3 cm radius point (right) shows twice the thickness as Dek-tak indicates. So 265 becomes 530.
- Total volume of 7 foils shot (not including He shot): $479 \mu\text{m}\cdot\text{cm}^2$. So about equal to deposited material.
- Surface of Ni film deposited from **thick target** is much smoother (below)
- SEM shows 'droplets' - indication from FIB is 'overlapped pancakes'
- EDX shows Al, O in film. Since we break vacuum every shot (unlike with films from solid targets), much more oxidation occurs.

Summary of sub-range foil shots

- Extended timescale imaging: 40 mm Ag shows lighted image for 900 ns.
- Al (much larger diameter target) light shows much shorter duration.
- Deposited film measurements show twice as much film deposited from foils in ‘transmission’ direction, compared to ‘reflected’ direction. No material is deposited in direction of beam propagation.
- FIB cut and SEM images of film surface show ‘droplet’ appearance. Viewing of the cut indicates fully dense to slightly porous layer. This may be expected since the most of material is probably deposited in molten state. Measured thickness shows that dek-tak is off by factor ~ 2. Therefore, the two spots together account for roughly all the material in the foils.