

Survivability of first-wall fusion materials: relevance to IFE and MFE

In an IFE Reactor, the First-wall is subjected to a Programmed High Fluence of Energetic Ion pulses ($3 \times 10^8/\text{year}$)

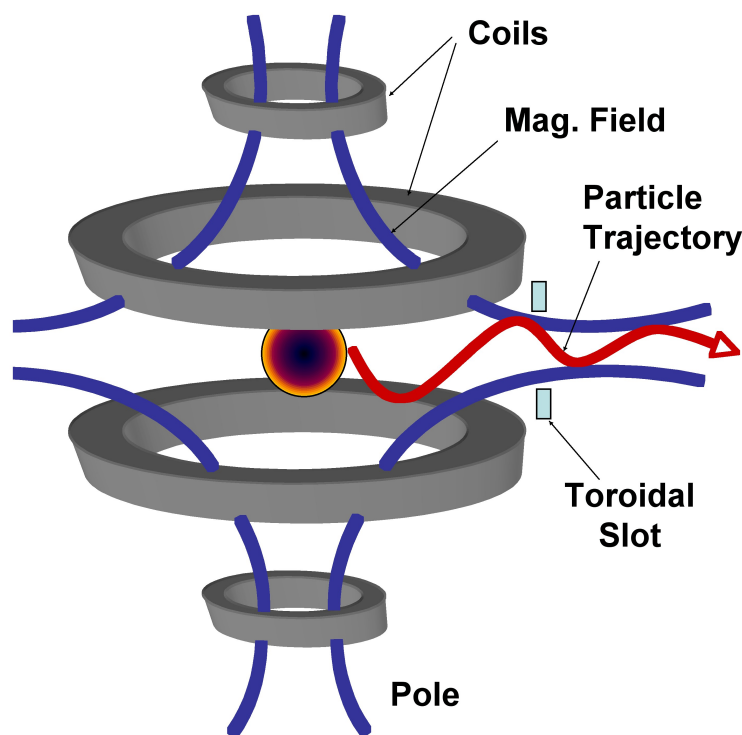


Image provided by R. Raffray,
UC San Diego

Unlike MFE, no Steady State phase, only 'transient' events.

Level per pulse is known, ~ few MeV ions normal to surface. At 10 Hz operation, 3×10^8 pulses per year

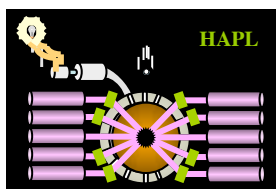
At 10 nm erosion/pulse, 3 METER thickness lost per year. So NOTHING can be lost per pulse. Melting should be avoided as well.

Biggest threat below Melting is Thermomechanical stress

Leading Geometry: Spherical w/ or w/o gas fill

Backup Geometry (LEFT): Cusp with 'beam dump' on axis

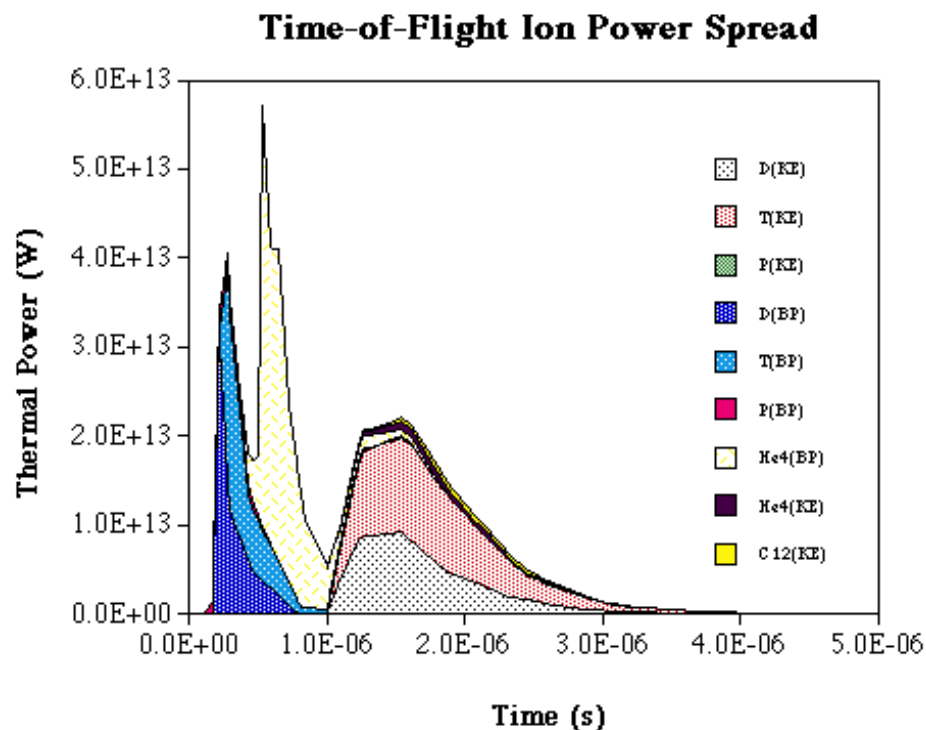
- Leading materials: tungsten and W alloys, SiC



Sandia
National
Laboratories



Laser IFE Direct Drive Threat Spectra (note: NIF is indirect drive)



**Simulation: Thermal Power to Wall in Ions
from 154 MJ Yield. Wall Radius: 6.5 m**

- For Direct-drive Laser IFE:
~70% neutrons, 1-2% x-rays
30% ions (50-50 fusion and 'debris')
- Ions: several MeV, ~ few μsec each,
8-20 J/cm² fluence, judged
Significant Threat
- X-rays: ~ 1 J/cm², up to 10 keV energies,
judged less significant threat
- RHEPP-1: 700 keV N, higher for N⁺²,
100-150 ns pulsewidth, 75-95 GW/m²
- RHEPP-1 energy delivery too short, but
otherwise good fidelity with reactor ion
threat

$F = P \cdot \sqrt{t}$: High Heat Flux conditions with Heat Diffusion
effect included. *Comparison:*

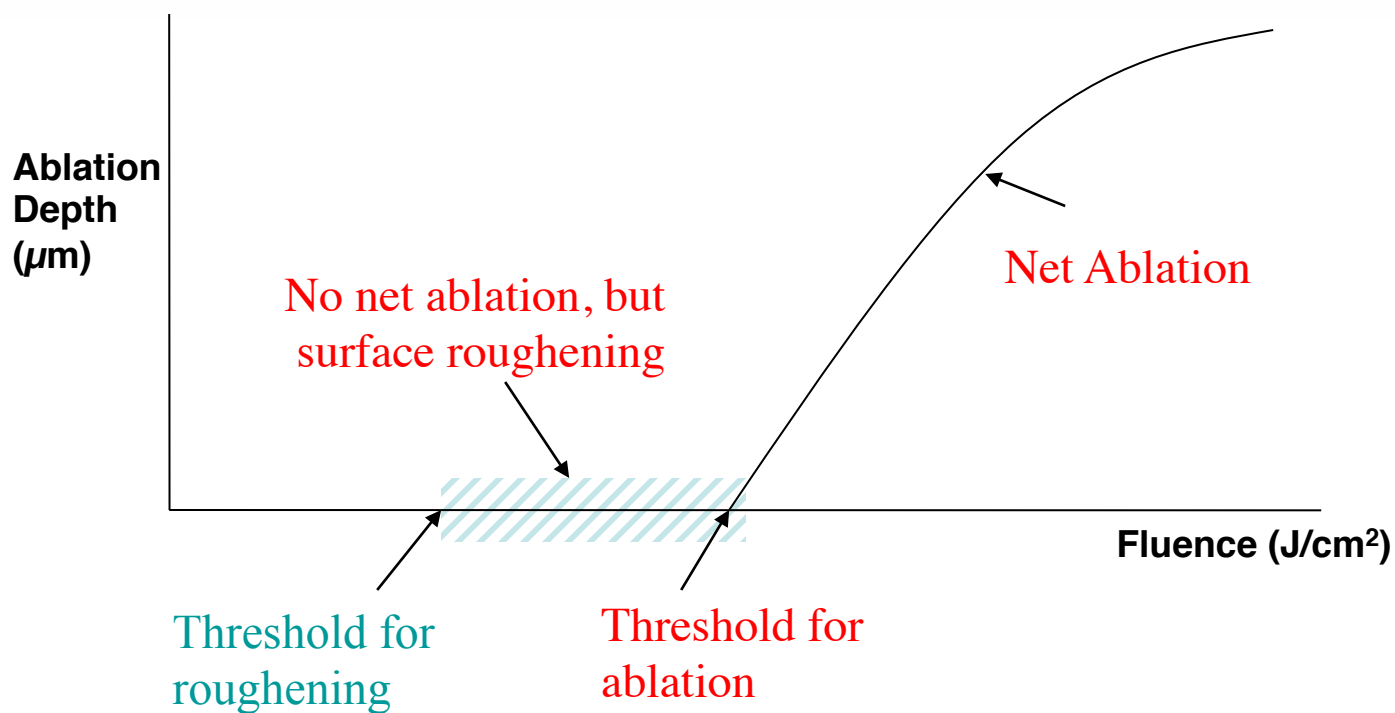
ITER ELMs (est):

22.4 - 67.1 MW m⁻² s^{1/2}

RHEPP-1:

33 - 112 MW m⁻² s^{1/2}

Regimes of IFE Materials Response to Ions



Goals (for each material): examine net ablation to validate codes **DONE**
find threshold for ablation

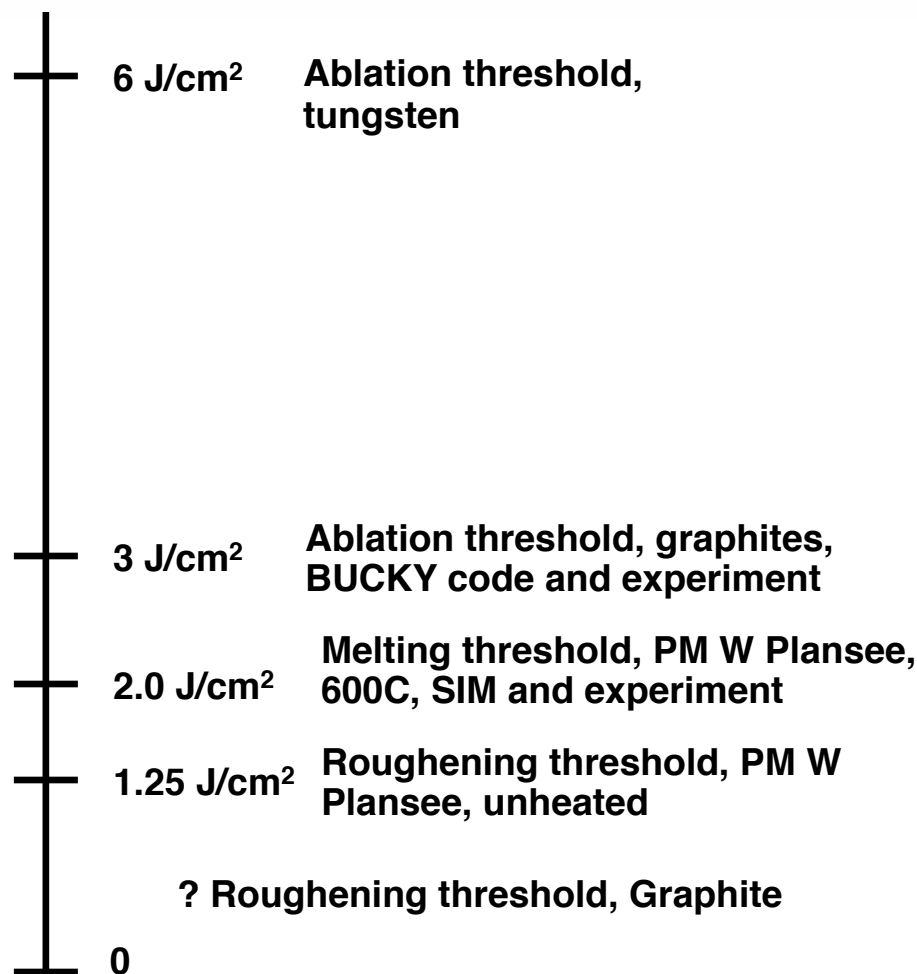
Area of Interest

Understand roughening. Is there mass loss?

Find threshold for roughening

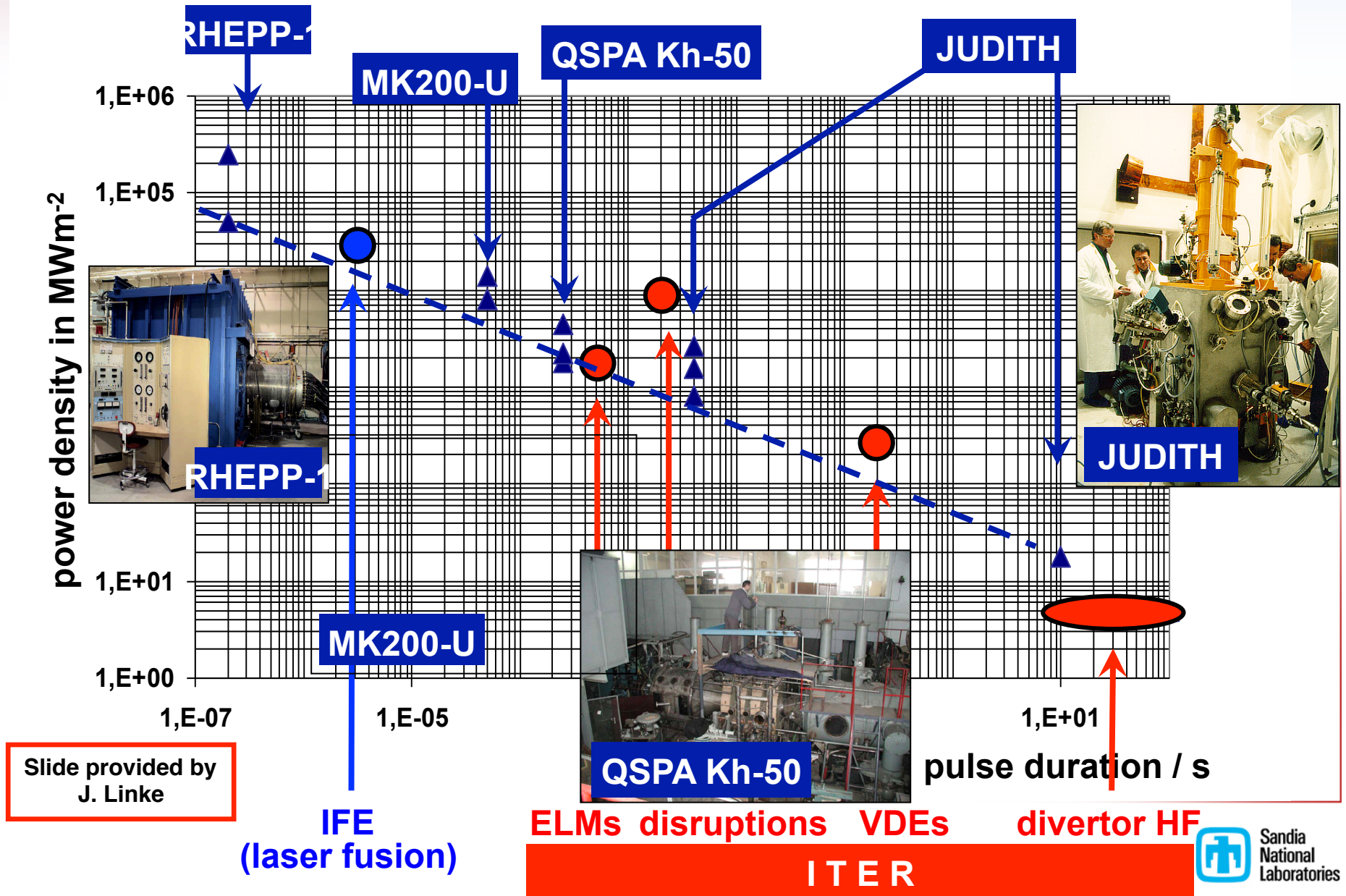
(Fluence/pulse, No. of pulses)

Thresholds for Materials exposure to ions on RHEPP

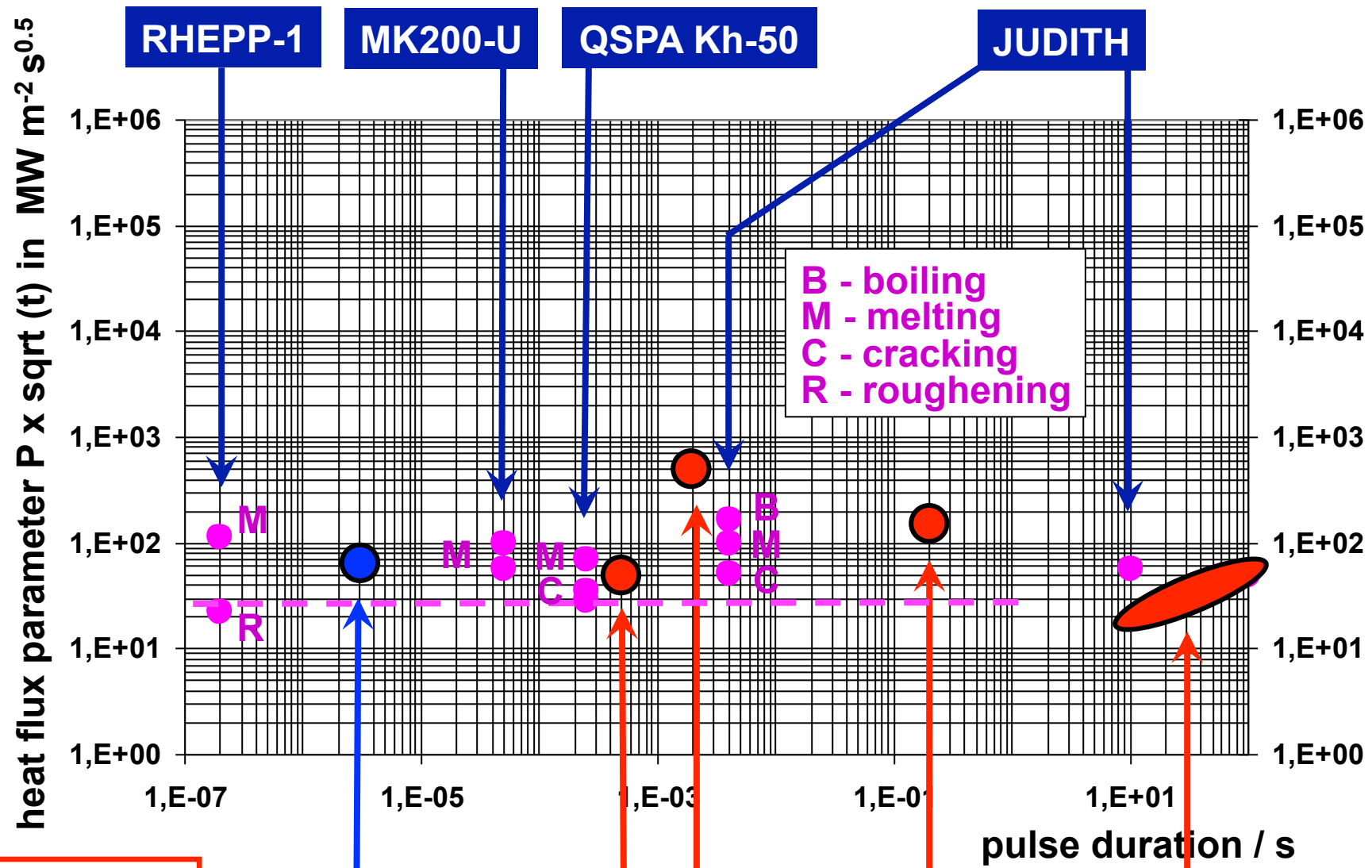


- General exposure conditions: MAP nitrogen beam, 150 ns pulsewidth, single shot.
- Roughening threshold for graphite (matrix) is unknown, but probably below 0.5 J/cm²
- Roughening threshold for tungsten for He beam is below that for MAP Nitrogen
- Chart to left: '**PM W Plansee**' refers to random-grain Powder Met Tungsten provided by Plansee

Adding $P^*\sqrt{t}$ connects IFE with MFE simulation of short transient thermal loads



Performance of tungsten under short transient thermal loads. Confirms heat conduction dominates over direct energy deposition



Slide provided by
J. Linke

IFE
(laser fusion)

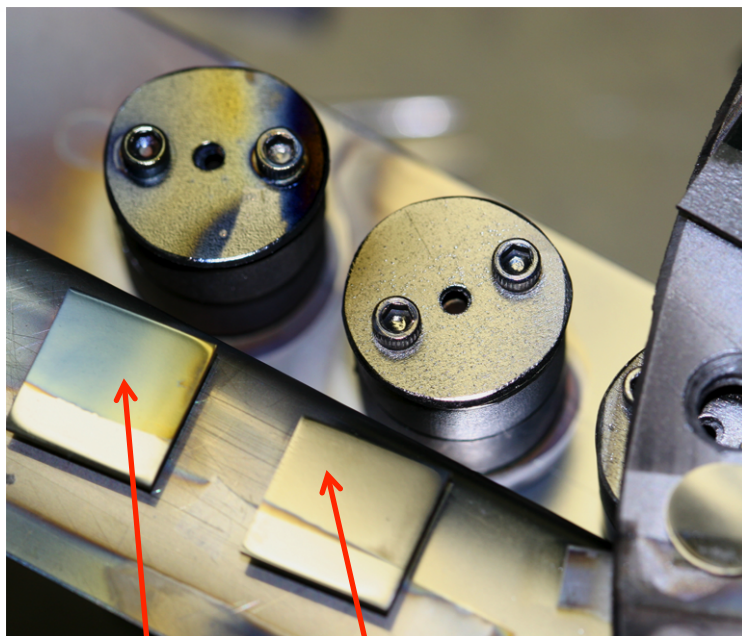
ELMs disruptions VDEs

divertor HF

ITER

RHEPP-1 Roughening Threshold, PM W, Multi-pulse, nitrogen beam exposure

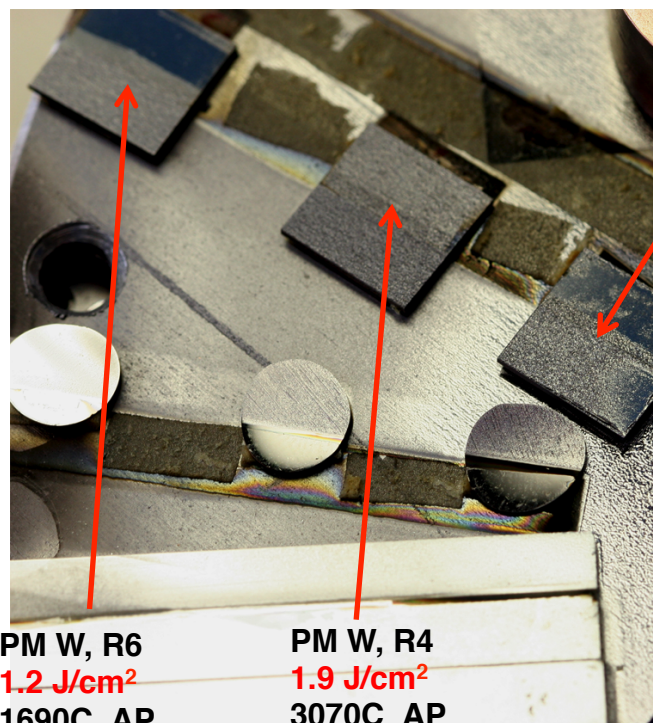
2000 shot series: PM W samples laid out radially from center. 10 and 8cm out are sub-threshold for roughening, 6cm is above. Note temperature excursions from modeling, based on fluence scatter from FCup data.



PM W, R10
0.2 J/cm²
270C_AP
Hi 415C
Lo 145C

PM W, R8
0.6-0.9 J/cm²
1290C_AP
Hi 1960C
Lo 535C

These PM W appear unaffected



PM W, R6
1.2 J/cm²
1690C_AP
Hi 2278C (5%)
Lo 1175C (5%)
 $R_a \sim 2.5 \mu\text{m}$

PM W, R4
1.9 J/cm²
3070C_AP
Hi 3650C
Lo 2100C
 $R_a \sim 4 \mu\text{m}$

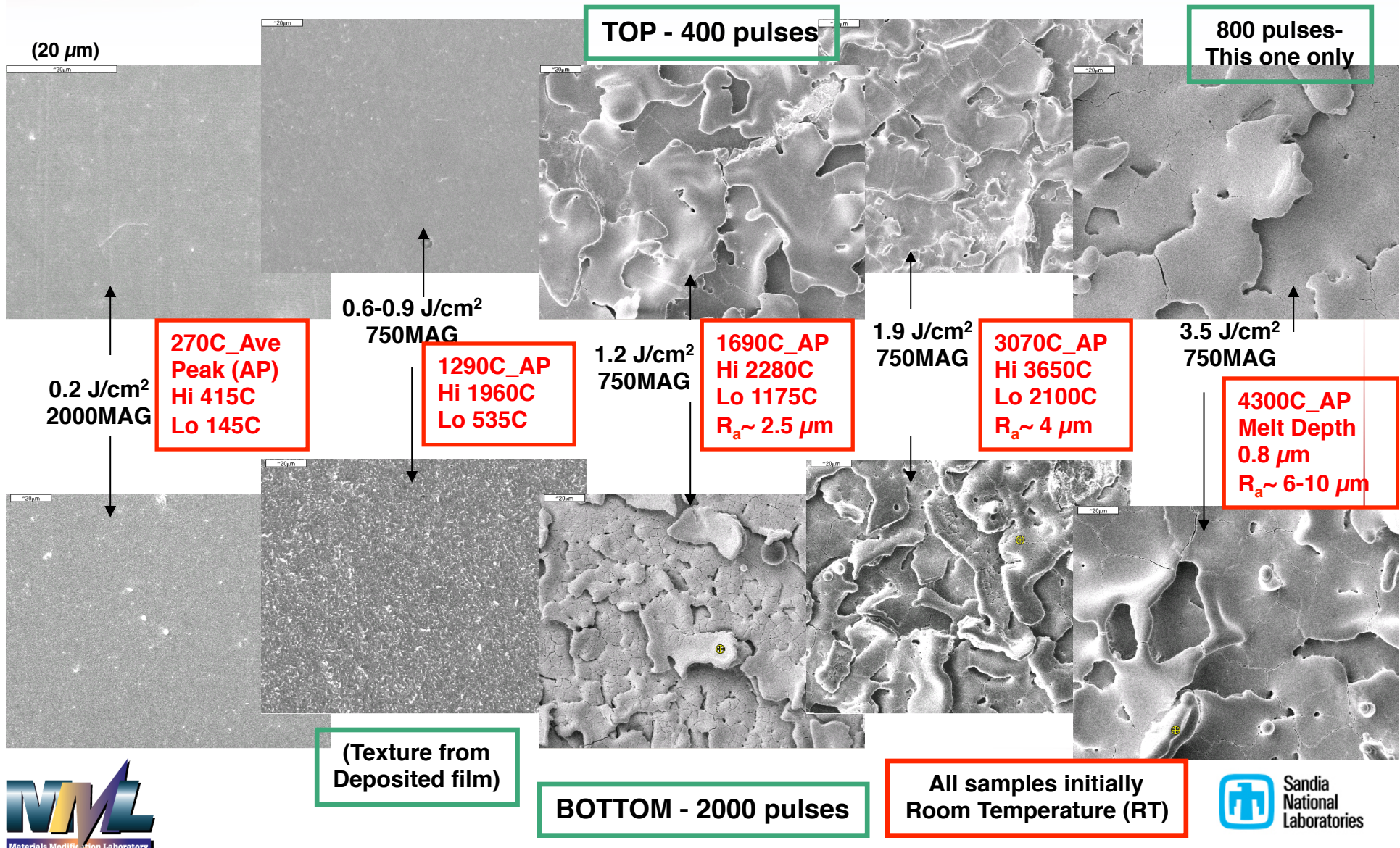
These PM W are very rough

PM W, R2
3.5 J/cm²
4300C_AP
Melt Duration 159 ns
Melt Depth $0.8 \mu\text{m}$
 $R_a \sim 6-10 \mu\text{m}$

BEAM CENTER

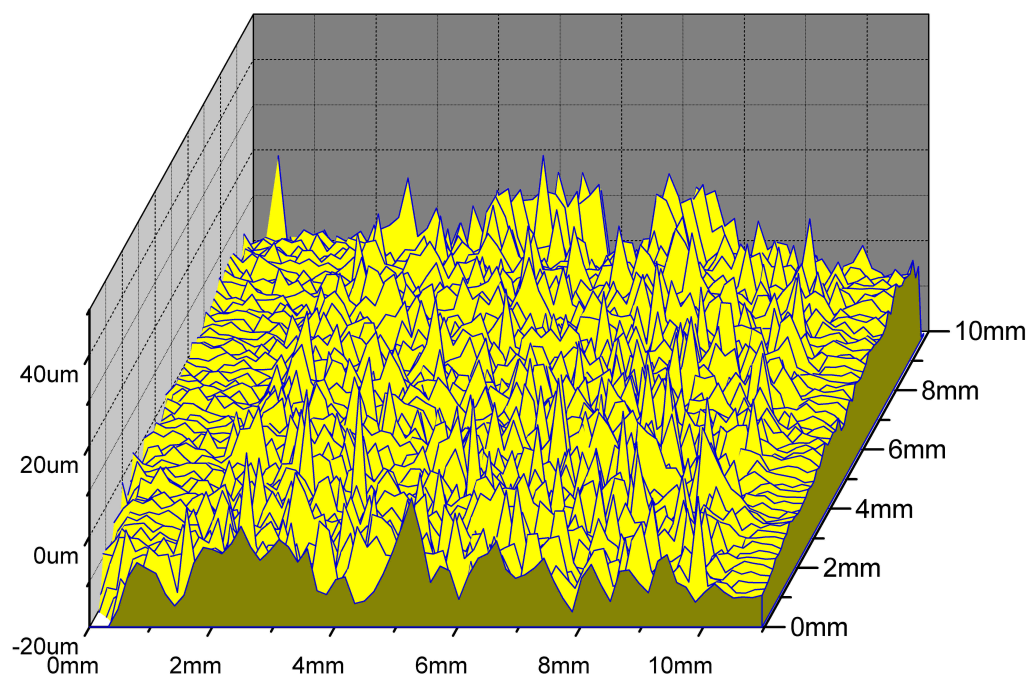
R6 = 6 cm from
Beam center

SEMs of Polycrystalline (PM) Tungsten Roughening from previous slide: Threshold at $\sim 1 \text{ J/cm}^2$, roughening saturates after ~ 400 pulses



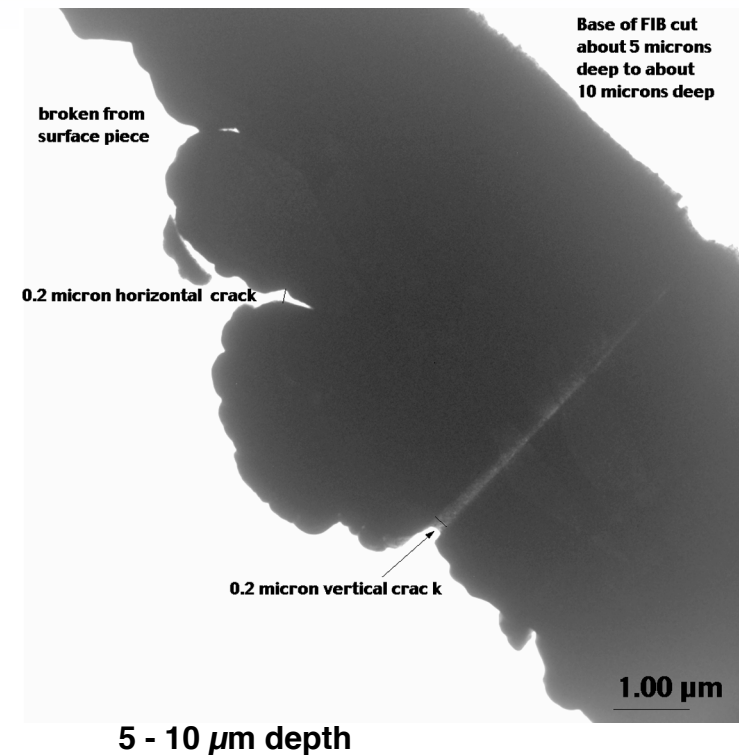
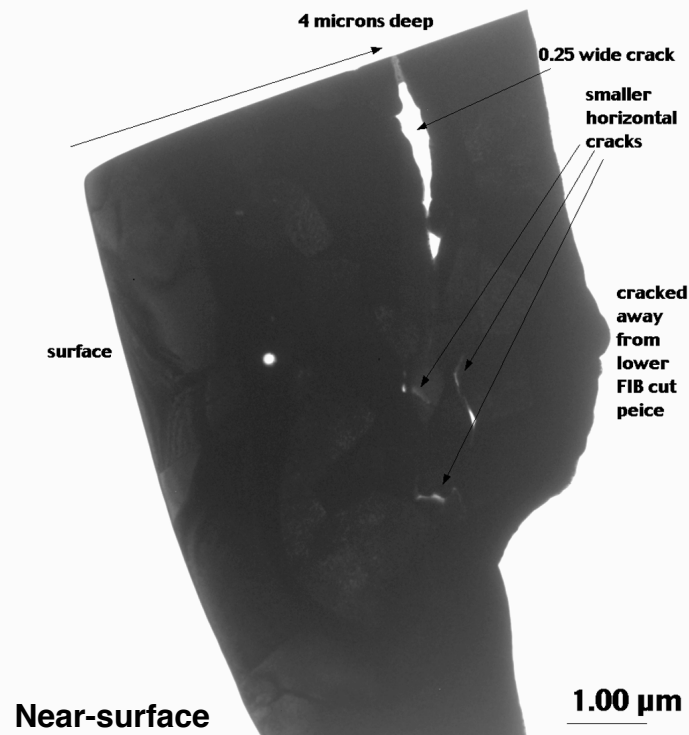
Is this erosion from melting? No. PM Tungsten after 1600 pulses (non-melting): Mostly mountains

Tungsten 1600 Pulses



- Heated/treated PM W examined with NEXIV laser interferometry
- Comprehensive line-out scan: max height 30 μm , min height < 10 μm compared to untreated
- Very deep micro-cracking not visible here
- Hypothesis: Thermal expansion from heating, plastic deformation

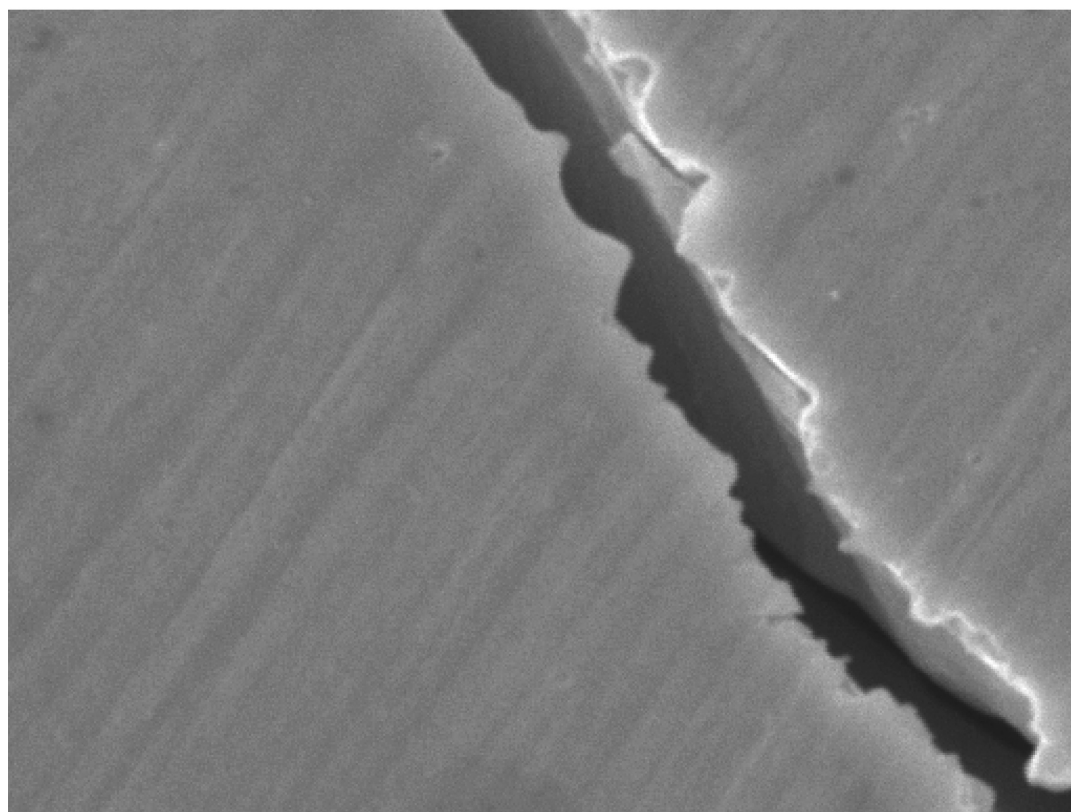
FIB-XTEM of 1000-pulse W at 2.25 J/cm² (ave): Deep horizontal/vertical cracking without melt



- Polished Powder Met W exposed to 100 shots N beam @ 2.25 J/cm² ave / pulse, ~ melting temperature at surface. No melt layer observed.
- 600°C exposure
- Sample cracking horizontally/vertically down to 10 μm depth

Suspect fatigue-cracking. If deep enough to reach steel substrate, wall will fail

Evidence of lack of melt on Single Crystal Surface: 15,000X SEM



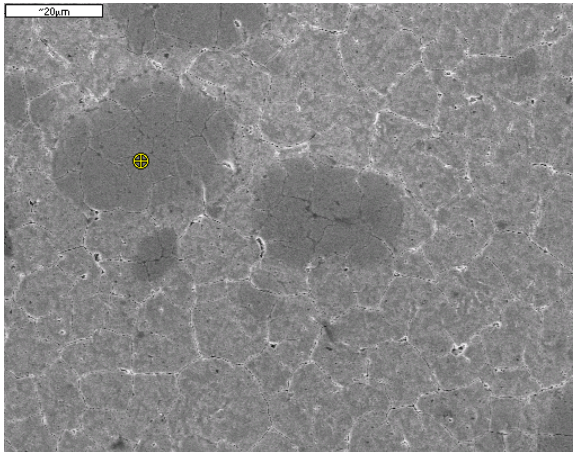
3 μ m

Electron Image 1

- Surface of Single-Crystal Tungsten, heated 510°C, after ~ 800 exposures at various fluences
- SEM at 15,000 magnification shows Clean Break along crack - stress cracking only
- Away from crack, surface is unaffected by Helium beam exposure

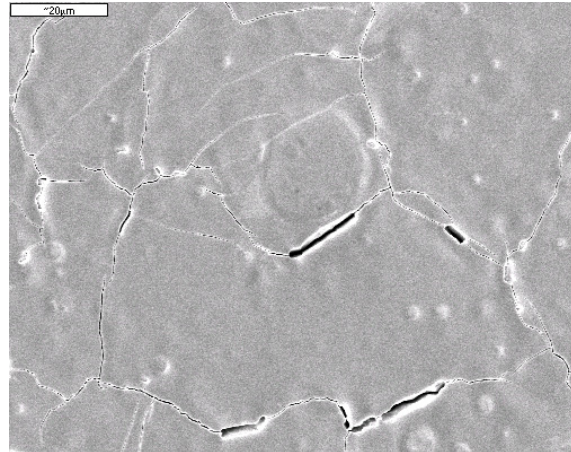
Three Forms of tungsten, treated at about same fluence: Its all about the grains.

1,000X MAG



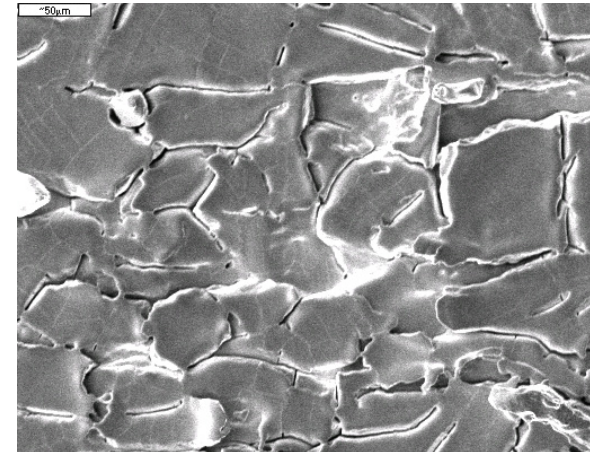
W-0.5%TiC 1.5 J/cm².
Ra = 0.04 μm

1,000X MAG



M182Perp ~ 1.25 - 1.5 J/cm²
Ra ~ 0.15 μm

300X MAG



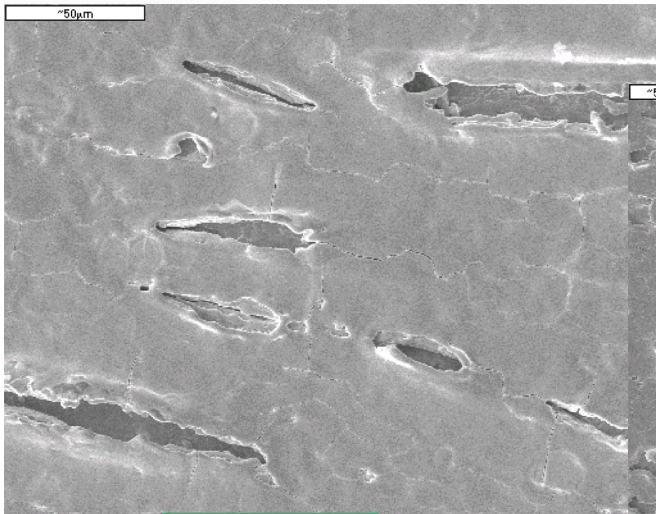
M182Parallel ~ 1.3 J/cm²
Ra ~ 4.5 μm

Two on right are SAME material

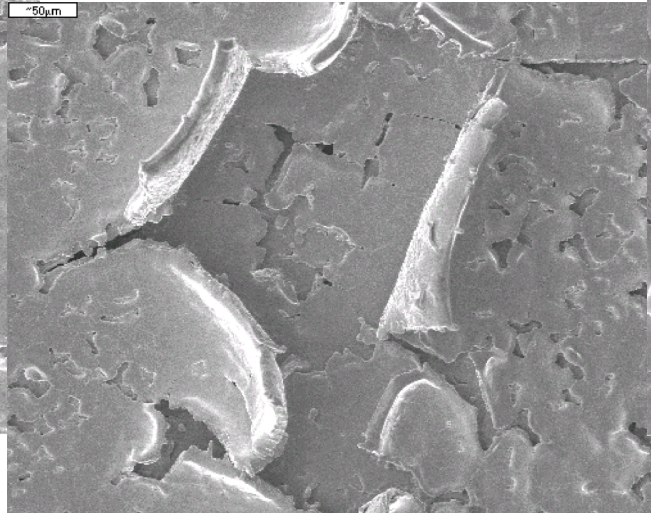
- (LEFT) W-0.5%TiC (Kurishita) formed by Hot Isostatic Press (HIP) – strengthens grain boundaries
- (CENTER) M182Perp tungsten: grains vertical to surface. Bottom of grains protected. (RIGHT) M182Parallel – grain corners get lifted.

PM Tungsten exposed to Nitrogen (top) and Neon (bottom):
Mass loss with N, not with Neon

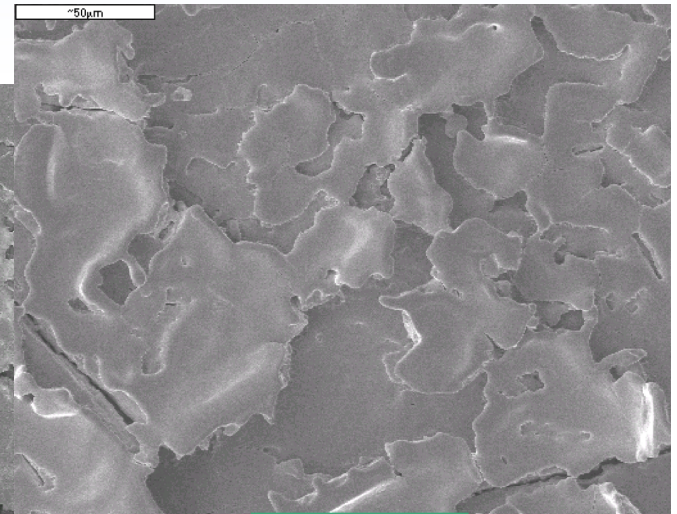
Top: Nitrogen



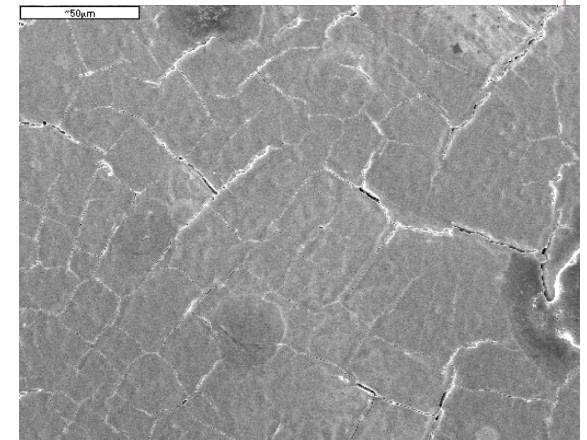
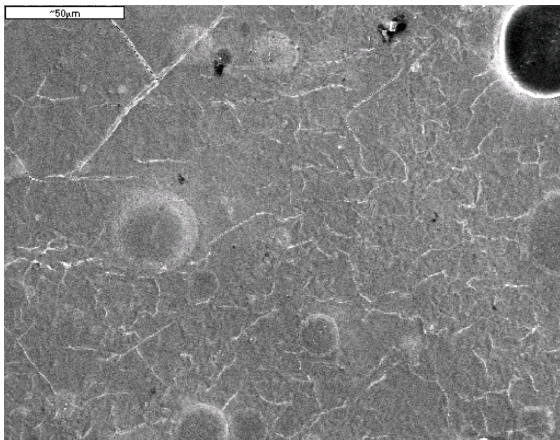
< 1.2 J/cm²



~ 1.2 J/cm²



> 1.2 J/cm²



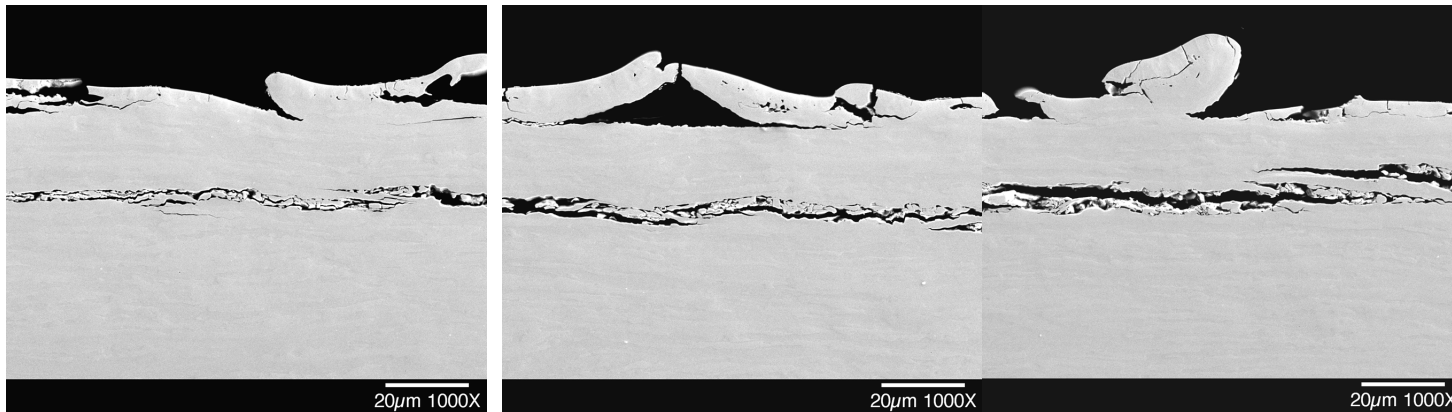
All images 500X Mag except above (250X)

Bottom: Neon

Mass loss: N -306.1 µg, Ne +167.4 µg
(gain due to entrained Cu)

500X Mag

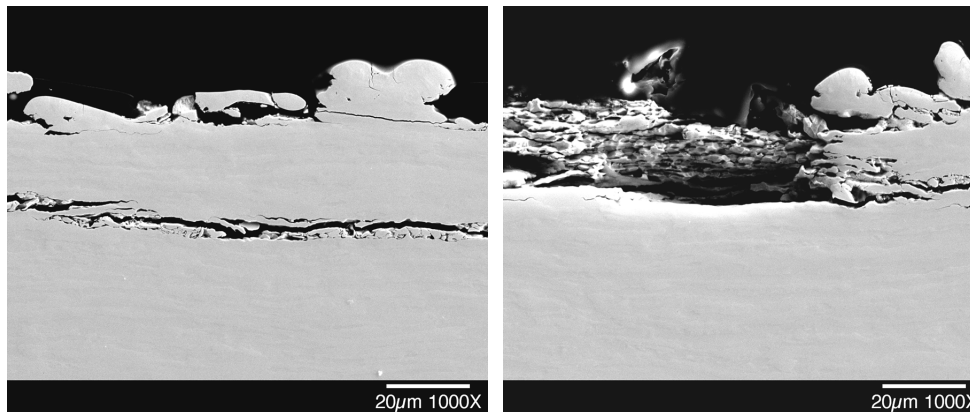
PM Tungsten, 1.9 J/cm² RT, sectioned SEMs (near Melt): Large distortions in near-surface zone



400 pulses

Increasing pulse number →

- Wholesale failure down to 20 μm level in last image

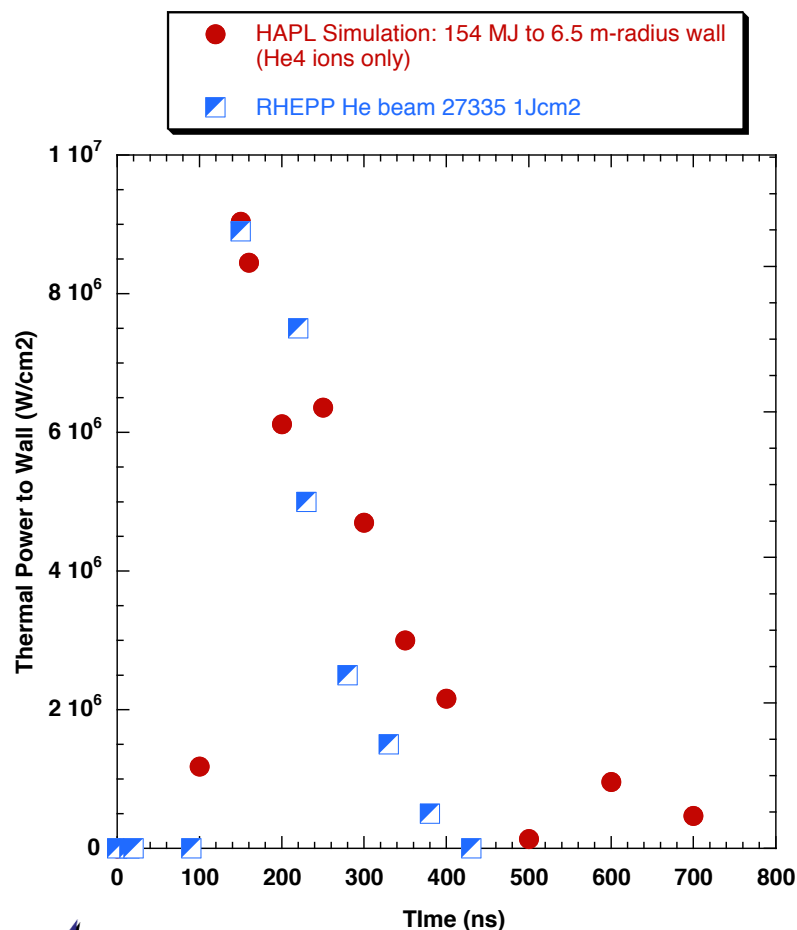


All images BEI 1000X MAG

1600 pulses

Helium beam exposure

The RHEPP helium beam well simulates IFE threat from both He ion and total ion current



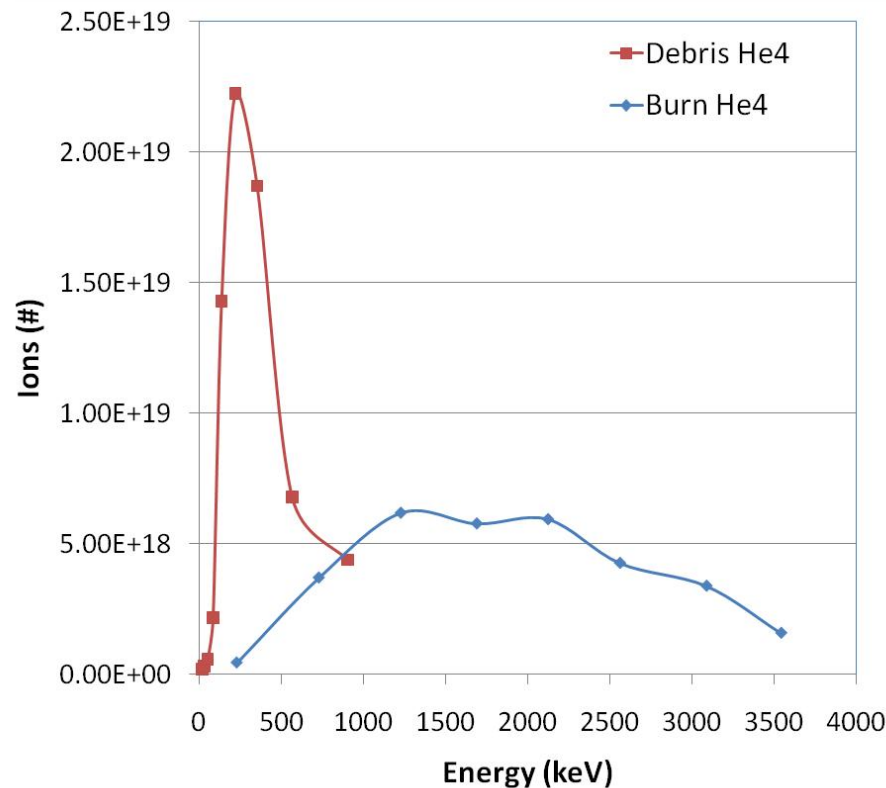
- **RED:** Simulation, 154 MJ IFE yield, at 6.5 meter wall radius, He₄ ions only
- **BLUE:** RHEPP pulse 27335, He beam, 1 J/cm² fluence, 9e6 W/cm² power density
- He component is ~ 1/3 of total ion pulse (fusion plus debris ions)
- Total pulsewidth ~ 1.5 μsec FWHM, vs ~ 80 ns Thermal Power FWHM for RHEPP
- RHEPP 1 J/cm² needs to be 3 J/cm² to include all ion effects. But shorter delivery increases *effective* RHEPP dose by 4x
- RHEPP He beam matches pulse heating time for reactor pulse, and 1-2 J/cm² matches overall power delivery to first wall expected for 154 MJ pulse

Energy Distribution of He⁴ for 401 MJ Target

Raw data: <http://aries.ucsd.edu/ARIES/WDOCS/ARIES-IFE/SPECTRA/>

Range of RHEPP He ions

Thanks to
Shahram Sharafat



COMPARISON:
Each RHEPP pulse delivers
~3e13 He⁴/cm² to treatment
surface at 2.25 J/cm² fluence.
Max surface temp at 2.25J/cm²
~ 2350C

Total: Burn = 3.13e19 He⁴/shot
Debris = 7.31e19 He⁴/shot

He⁴ Fluence (10 m radius chamber):
Burn = 2.49e12 He⁴/cm²
Debris = 5.82e12 He⁴/cm²
Total = 0.83e13 He⁴/cm²

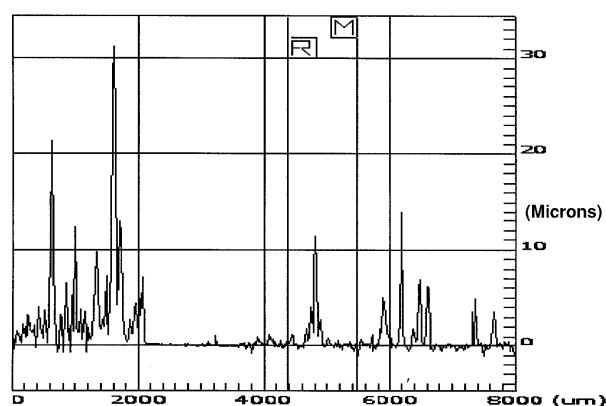
Presented at HAPL Meeting, Madison, September 2003

R_a as function of Number of Nitrogen pulses @ 4.0 J/cm² Helium actually roughens less than nitrogen

I-D 8 mm Profilometer Scans, 450 shots He (Left) and Nitrogen (Right)

He Beam 1.3 J/cm²

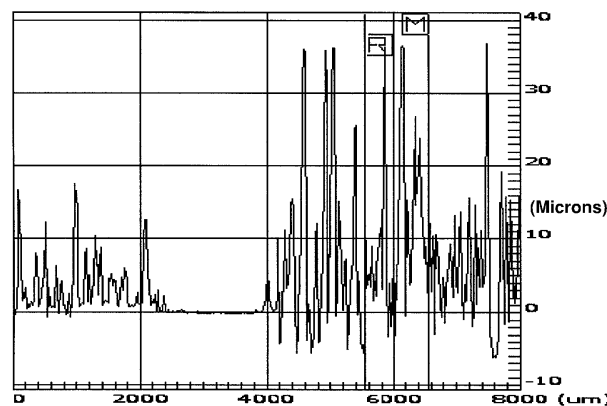
N Beam 4J/cm²



(He-450) (None) (N-200)

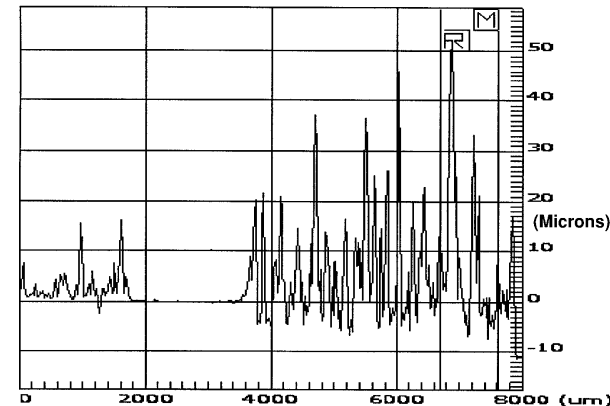
$R_a \sim 1-3 \mu\text{m}$
 $P-V \sim 10-30 \mu\text{m}$

$R_a \sim 1-3 \mu\text{m}$
 $P-V \sim 5-15 \mu\text{m}$



(He-450) (None) (N-400)

$R_a \sim 4-9 \mu\text{m}$
 $P-V \sim 20-35 \mu\text{m}$



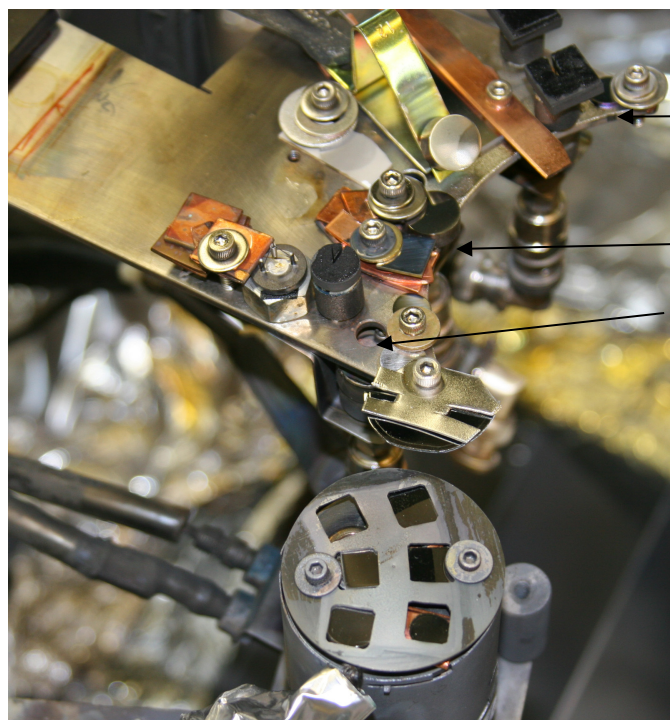
(He-450) (None) (N-600)

$R_a \sim 7-10 \mu\text{m}$
 $P-V \sim 50-70 \mu\text{m}$

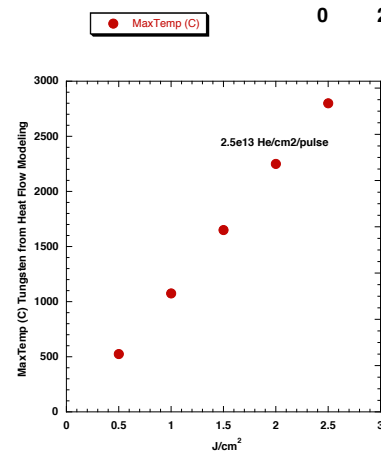
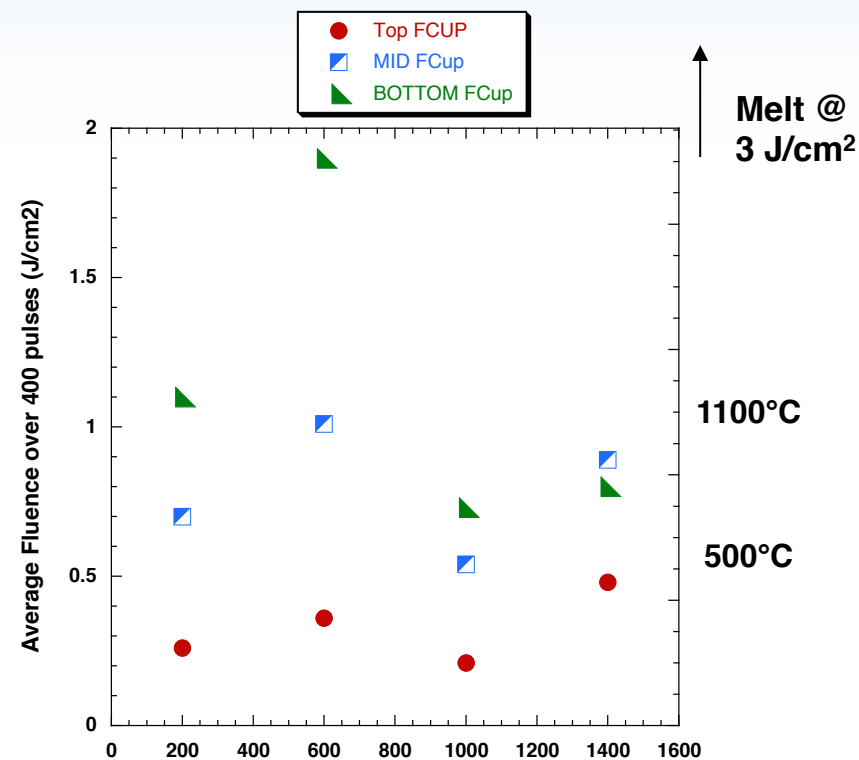
- Roughening of PM Tungsten: 450 pulses He @ 1.3 J/cm² roughens more than 200 pulses N @ 4 J/cm² (Melt)
- N-beam roughening catches up and passes at 400 pulses

Sample Setup for He1*_1600: four 400 shot series

Samples mounted before Start
Beam Center off to center Right



500°C Heater at bottom



- Shot Number
- 1 J/cm² ~ 1.25e13 He/cm²/pulse
- Fluences and MaxTemps are Averages. ±30% variation in fluence, with outliers to ±50%
- Vacuum ~ Mid e-5 Torr (no Cryos)
- Heated samples not discussed – heating to 520°C doesn't affect results
- 520°C may be below DBTT

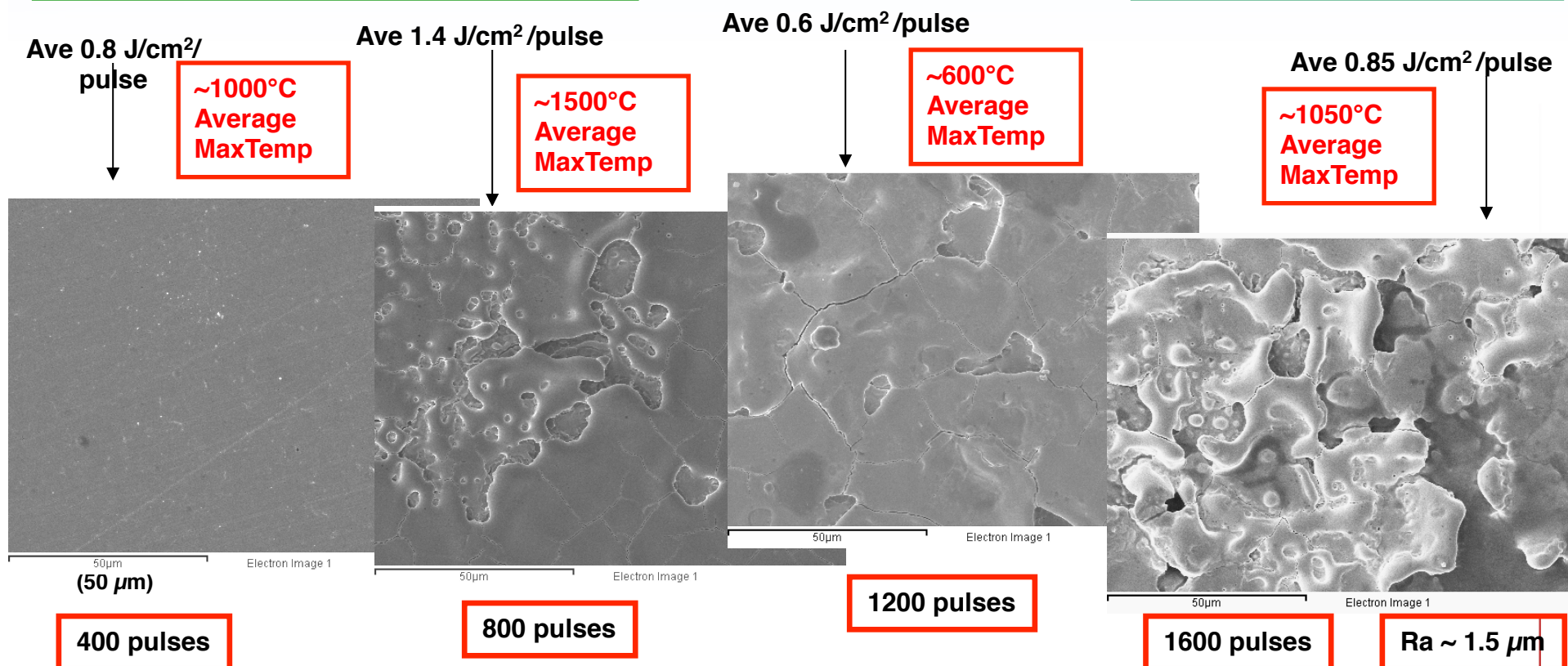
MaxTemp Vs Fluence (from Heat-Flow modeling)

'Porosity' evidence in images different from nitrogen

Polycrystalline Tungsten He exposure behavior - 1600 pulses

All samples initially Room Temperature (RT)

All images 1000X magnification



- Average maximum surface temperature < 1500°C
- No effect 1st 400 pulses: below threshold
- Using \sqrt{t} scaling: 0.8 J/cm² equivalent of 0.4 MJ/m². Consistent with QSPA plasma exposure of tungsten PFCs (ref: A. Zhitukhin et al, JNM 363-365 (2007) 301-307)
- Final 400 pulses @ 0.85 J/cm²: probable cumulative mass loss

(Est) total He implantation
~ 1.8e16 /cm²

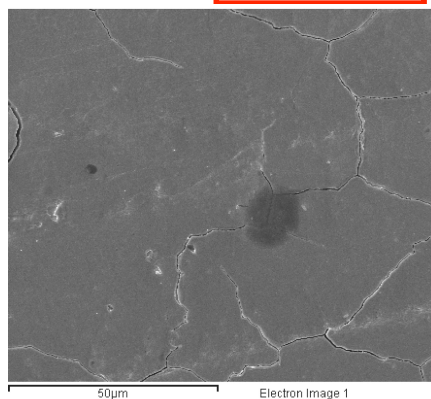
M184(P) oriented grain tungsten - 1600 pulses

All samples initially Room Temperature (RT)

All images 1000X magnification

Ave 0.8 J/cm²/pulse

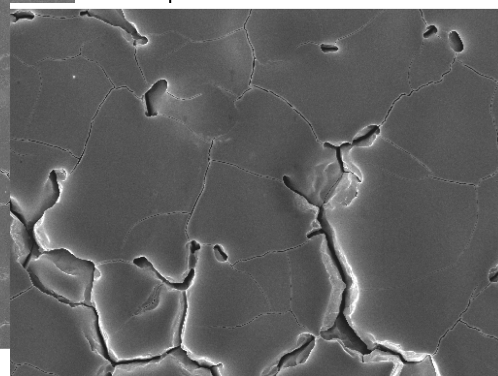
~1000°C



400 pulses

Ave 1.2 J/cm²/pulse

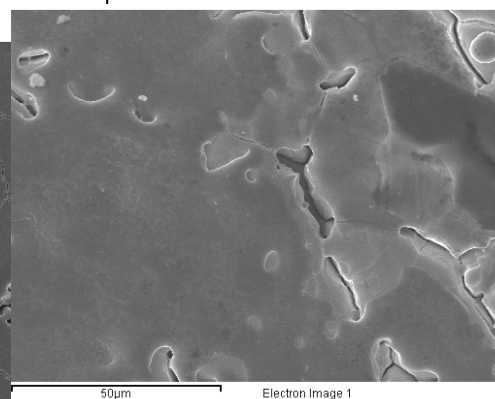
~1300°C



800 pulses

Ave 0.6 J/cm²/pulse

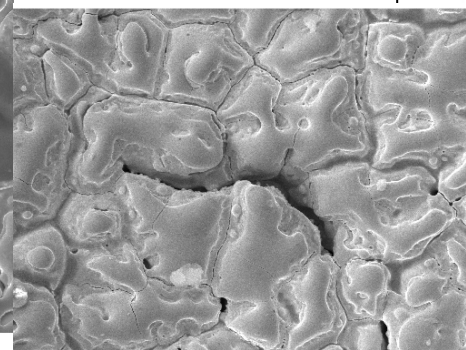
~600°C



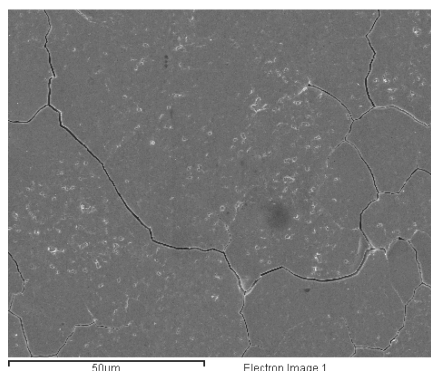
1200 pulses

Ave 0.85 J/cm²/pulse

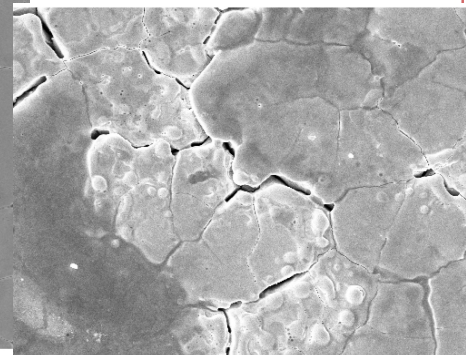
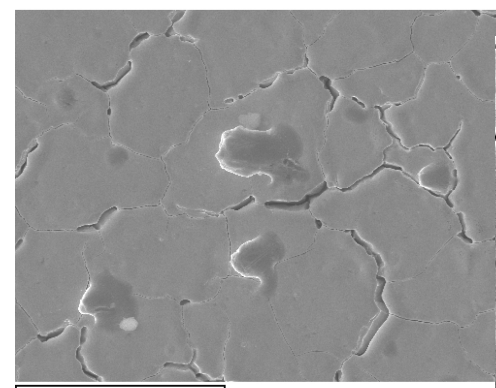
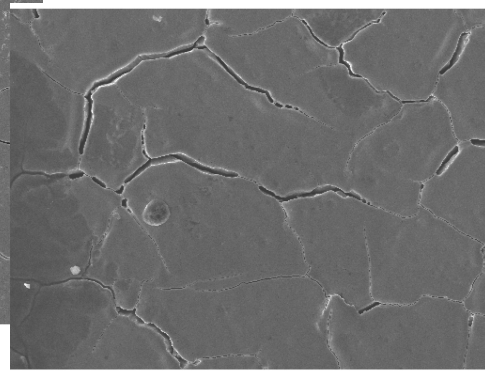
~1050°C



1600 pulses

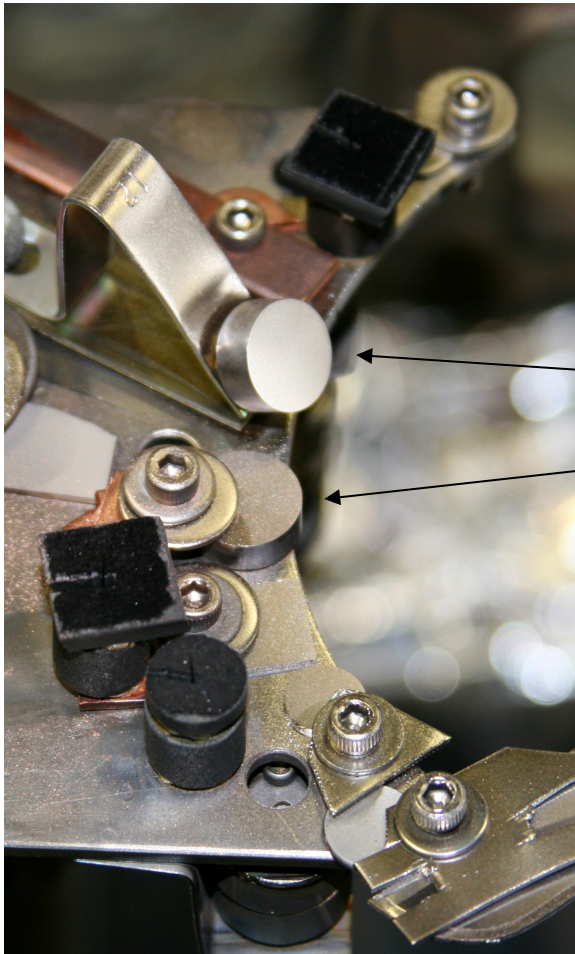


(50 µm)



- Bottom Row: improved performance.
- R_a (TOP) ~ 1.5 µm, (BOT) ~ 0.26 µm – SMOOTHER SURFACE

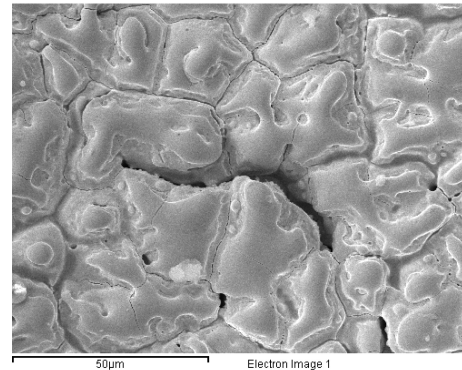
Bottom Row from last slide: Same M184p material tilted at 55° to beam



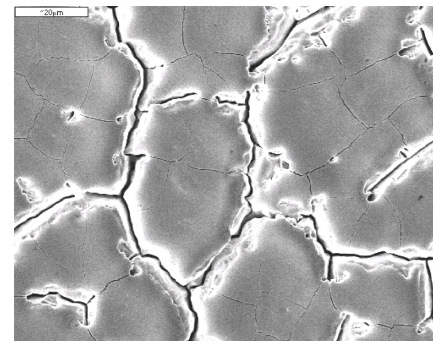
M184p
'Tilt'

M184p

- 55° tilt reduces effective fluence in half
- Does this lead to longer-term survivability?
- Helium looks to cause more roughening than nitrogen beam



M184p – 1600 He pulses



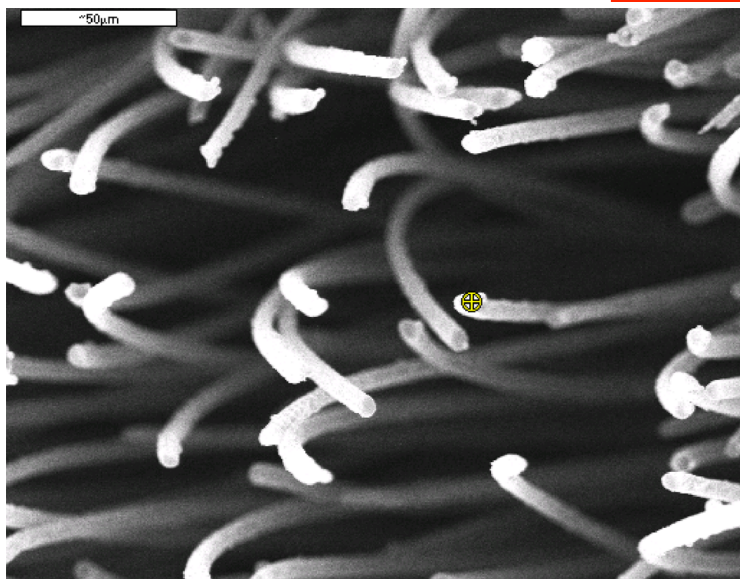
M182p – 1600 N pulses

Alternate material: W-coated Carbon 'Velvet' survives 1600 pulses amazingly well

Carbon fibers w/ 1.6 μm W coating,
2% areal coverage

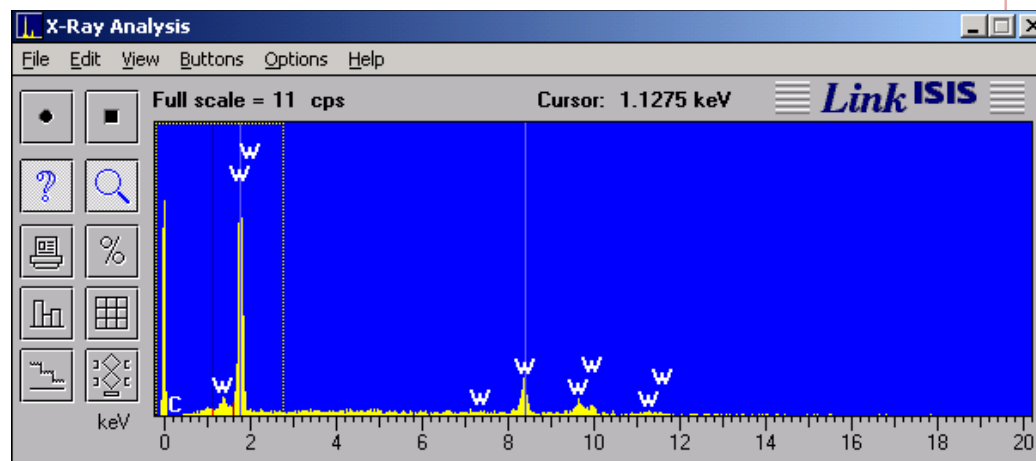
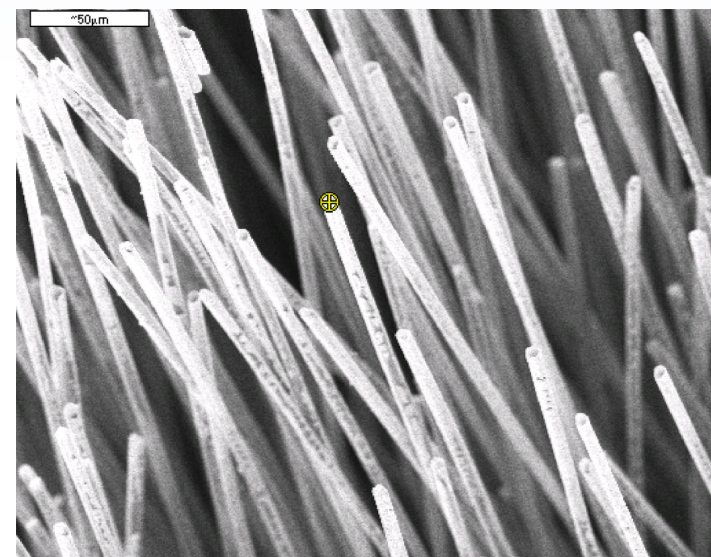
(RIGHT)
520C (nominal), 1600
pulses, 1.5 J/cm²/pulse

NOTE: W remaining on
tips (see below) and
sides



(ABOVE)
RT @ ~ 2.8 J/cm², 1600 pulses

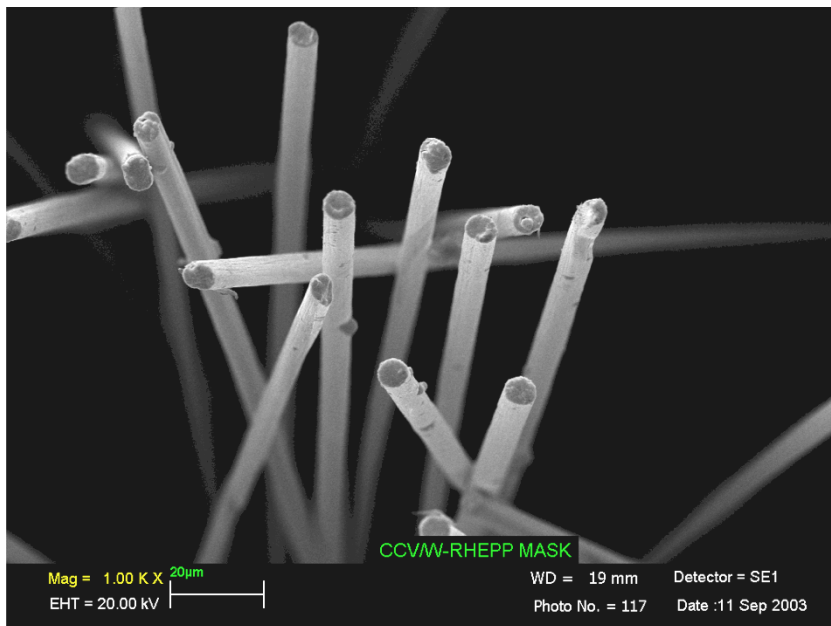
NOTE: bent tips, flat ends have W
removed, rounded ends still have W



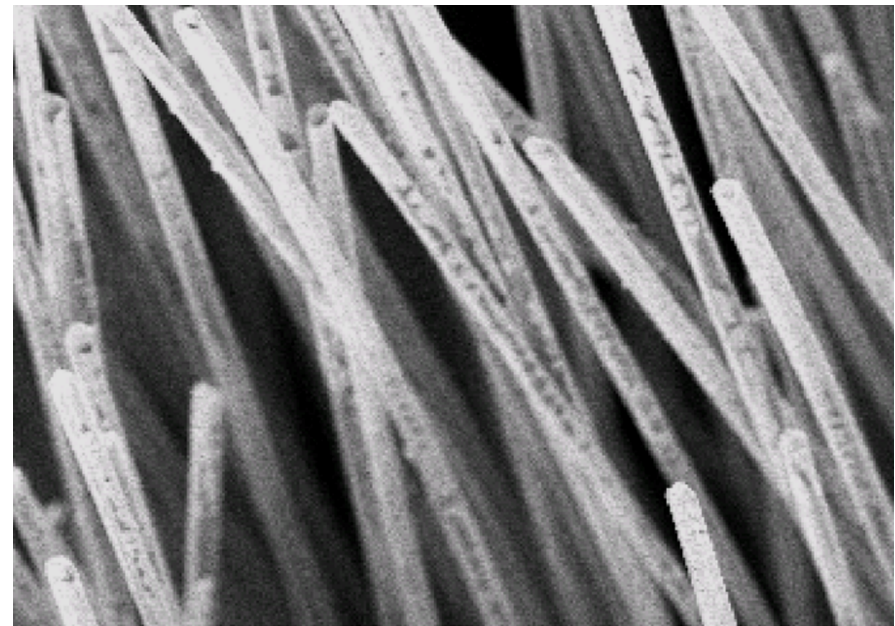
EDS scan of tip (cross): W rich

Comparison of SEMs, exposed/unexposed velvet

Carbon fibers w/ 1.6 μm W coating,
2% areal coverage



Untreated Velvet Fibers



After 1600 pulses at 520C
(nominal), 1.5 J/cm²/pulse

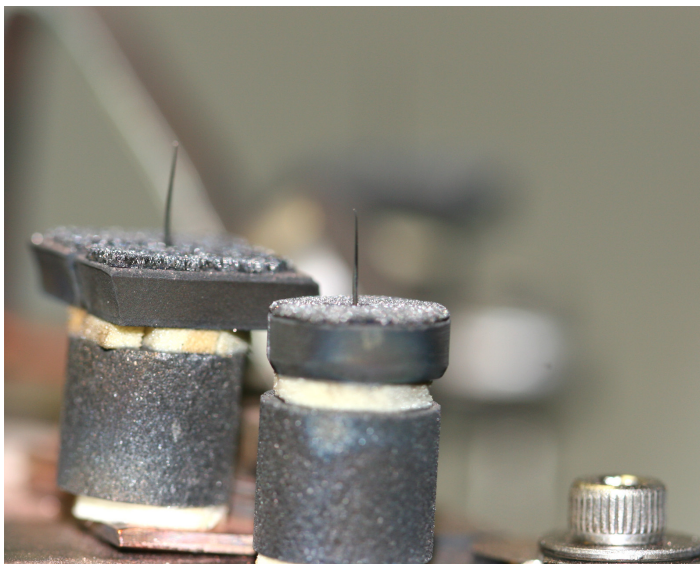
Needles and needle groups as a first wall

T.J. Renk, P. P. Provencio, T. J. Tanaka, J. P. Blanchard, C. J. Martin, and T. R. Knowles,
*Survivability of First-Wall Materials in Fusion Devices: an Experimental Study of Material
Exposure to Pulsed Energetic Ions*, Fusion Science and Technology **61** (2012), 57-80.

'Needle' geometry minimizes full-exposure area, maximizes 'glancing blow' area, minimizes He penetration depth

Incoming Beam

Dimensions (Knowles W):
Tip Length 3000 μm
Radius 125 μm
Rtip 0.25 μm
Shaft 1.5 cm X 250 μm diam

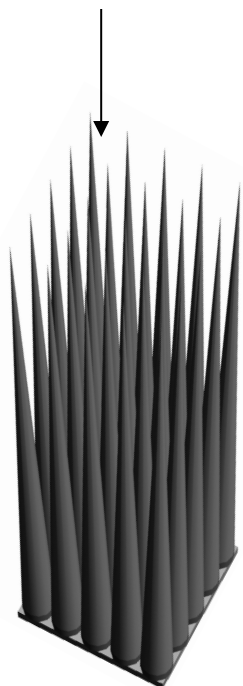


- Design issues: overall length, tip geometry (sharpness, etc), assembly into groups
- Several designs investigated here:
 - Single Tungsten needle (Knowles-left)
 - Mo-coated W needle: $\sim 0.25 \mu\text{m}$ Mo deposited by RHEPP
 - 'Array' -more later
 - 'Bundle' -more later
- Single W needles mounted in holder with carbon velvet at base to minimize blowoff

Arrays of Needles could be used in both IFE and MFE walls

Incoming Ions

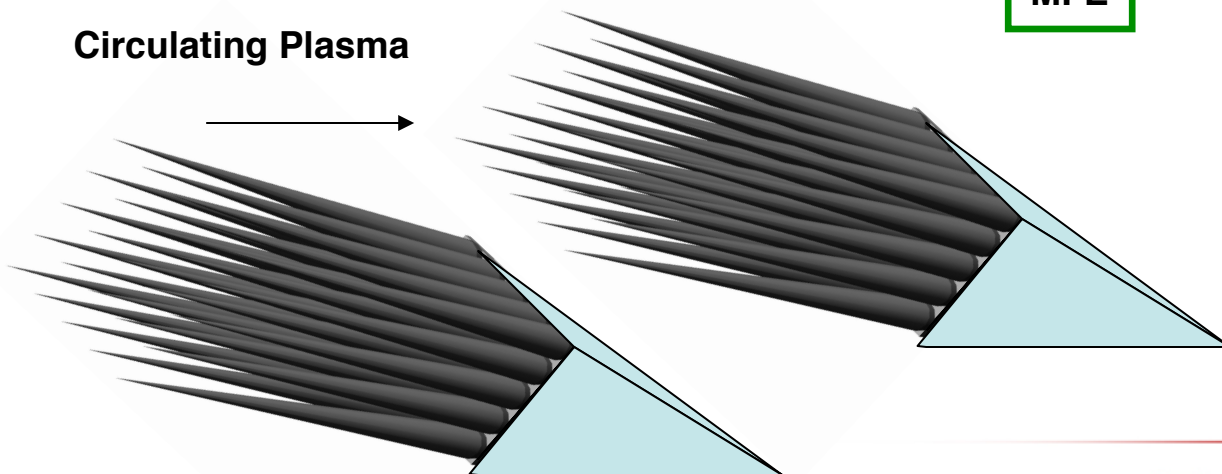
IFE



- Spacing, orientation aspect ratio to be determined
- MFE: arrays of needles on 'pedestals' facing circulating plasma direction

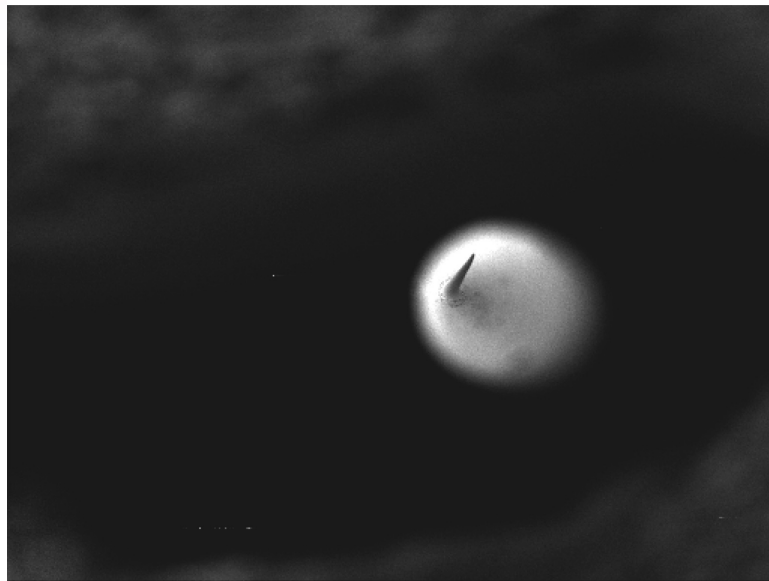
Circulating Plasma

MFE



Dimensions (Knowles W):
Tip Length 3000 μm

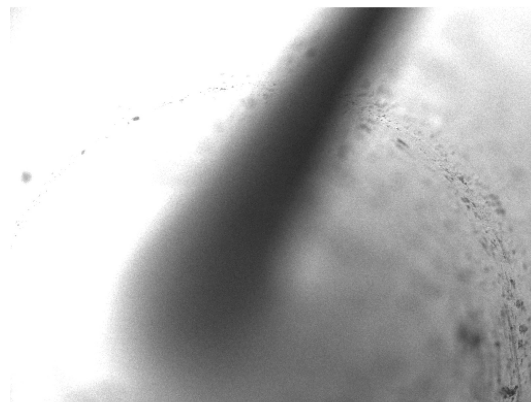
Top SEM view: 400-pulse coated needle compared to virgin (right)



500µm

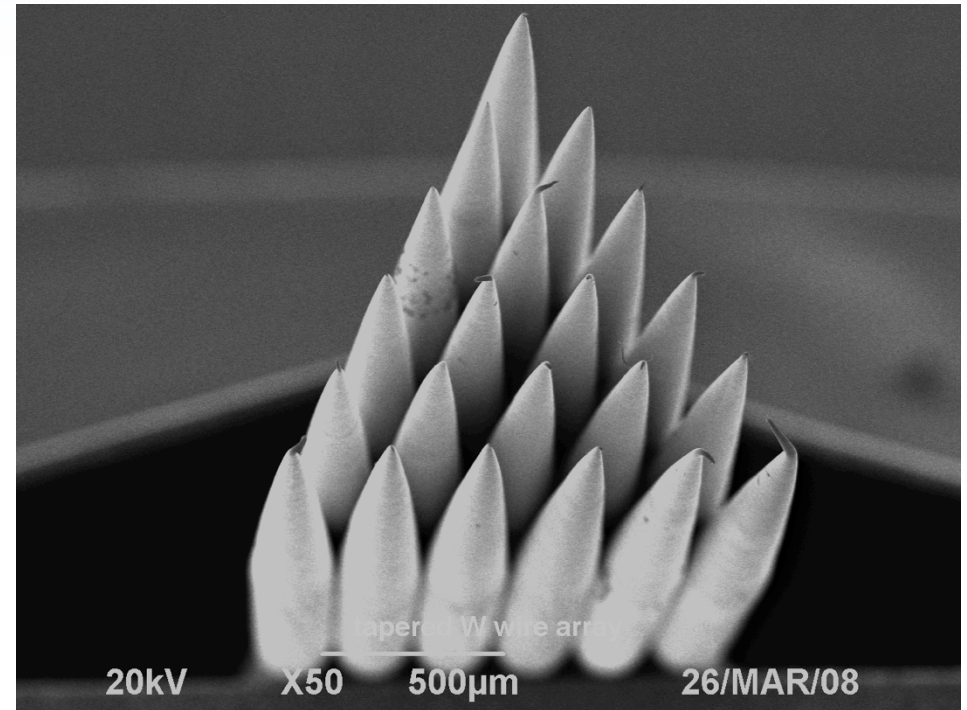
Electron Image 1

Treated 400 pulses.
Diameter at
'bend' ~ 25 µm



30µm

Electron Image 1



20kV

X50

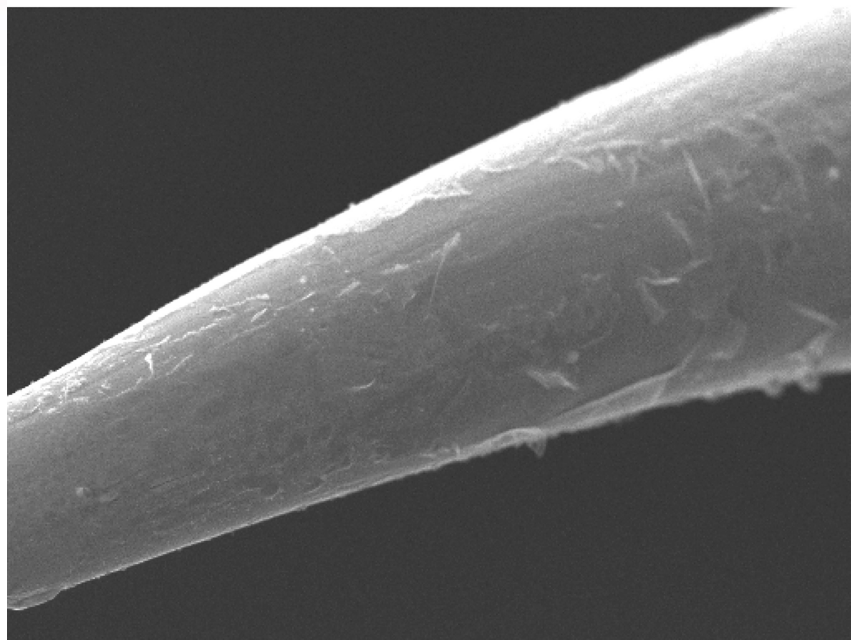
500µm

26/MAR/08

(right) diameter at bend ~ 30 µm

Tip geometry identical to virgin needle at 400 pulses

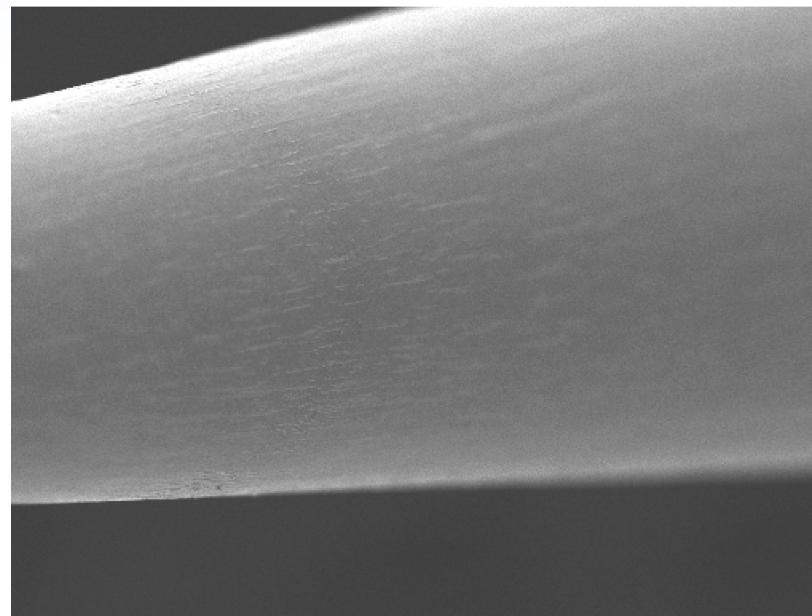
Mo-coated tungsten needle shows no sign of He bubble formation at 800 shots



20µm

Electron Image 1

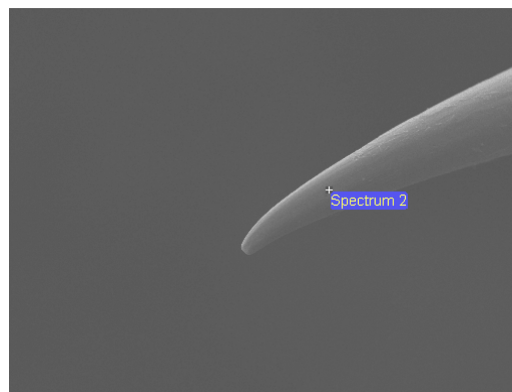
Near tip



100µm

Electron Image 1

Where EDS shows Mo

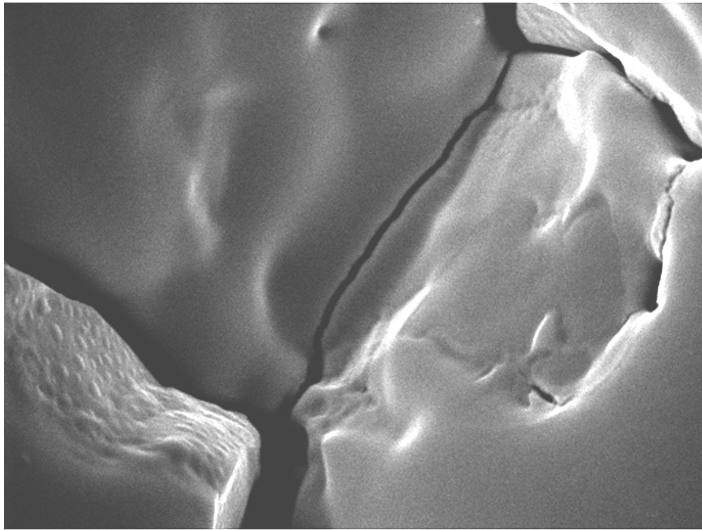


50µm

Electron Image 1

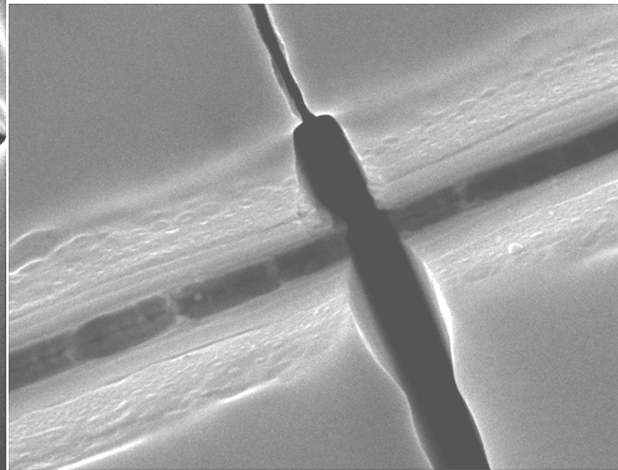
Tip may be blunted

There IS evidence of He bubbles in both flat M184p and single crystal W, at $\sim 1.2 \text{ J/cm}^2$

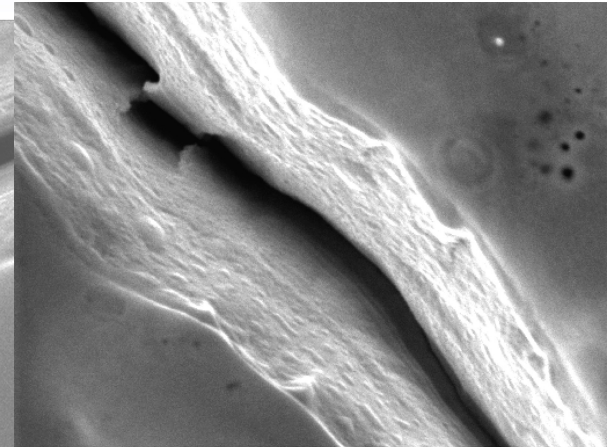


7µm Electron Image 1

M184perp Room Temp

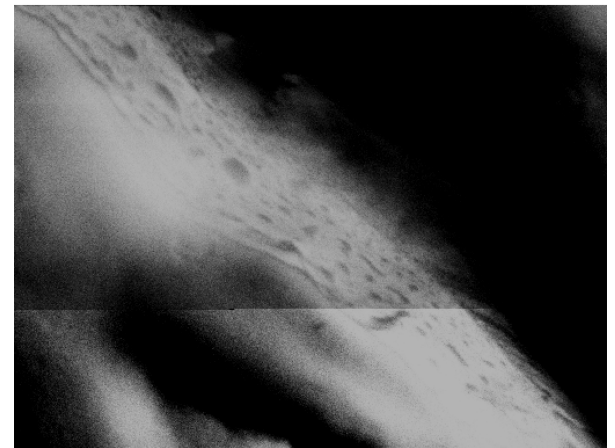


Single Crystal W RT



7µm Electron Image 1

**Single Crystal 520°C 1200x
Below: BSE image**

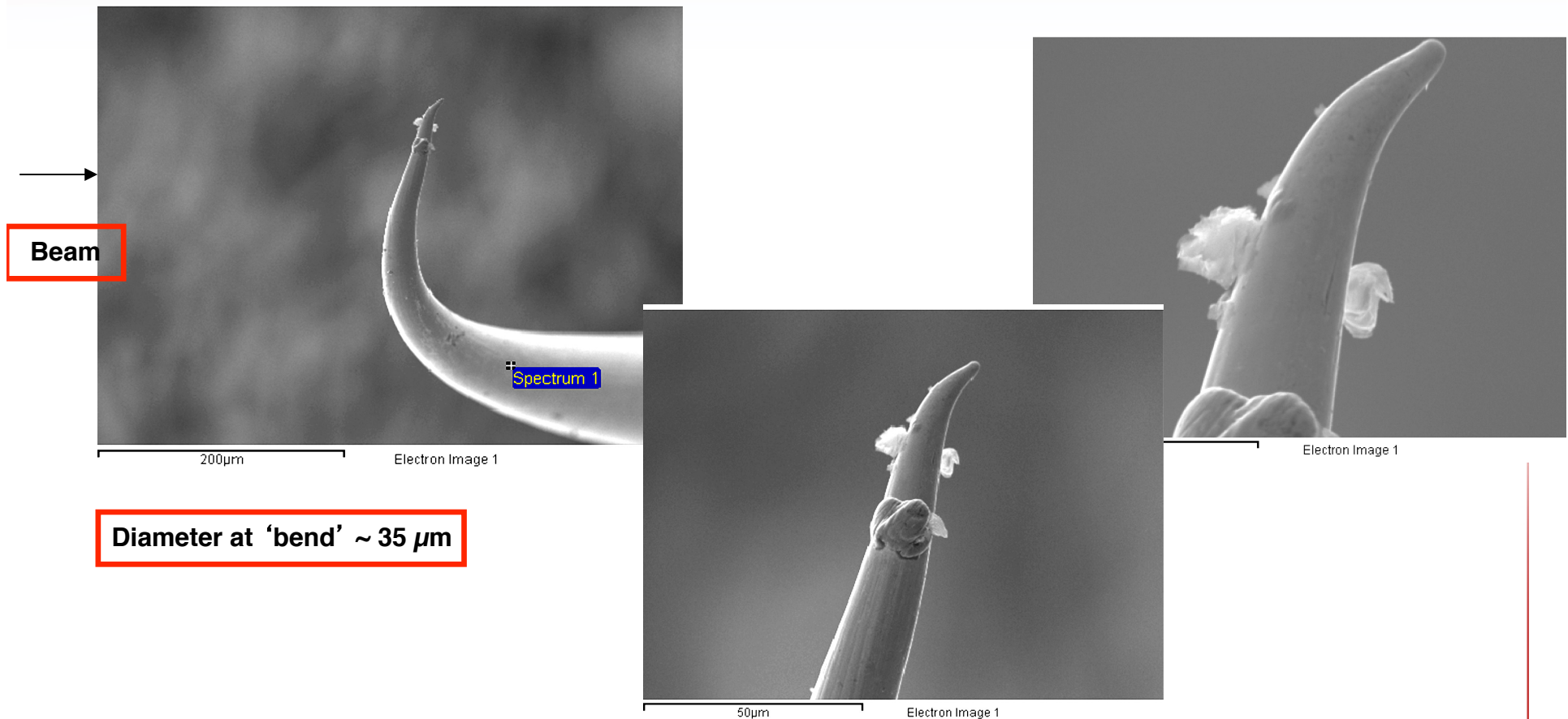


7µm Electron Image 1

- Structures occur at 400 pulses and up
- Mostly observed in cracks - consistent with $\sim 1 \mu\text{m}$ He range in RHEPP
- More work is needed to assess exact nature of He retention
- **NO EVIDENCE** of He bubble/blister formation on needles - up to 1600 pulses

**All Images
7500MAG**

Mo-coated W needle at 1200 pulses:
markers are Mo coating, 90° bend

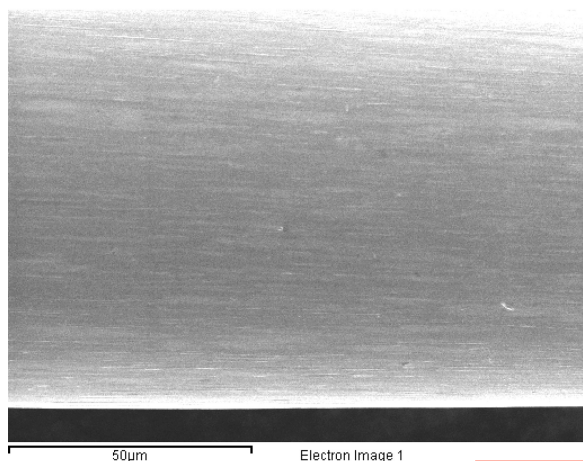


Diameter at 'bend' ~ 35 µm

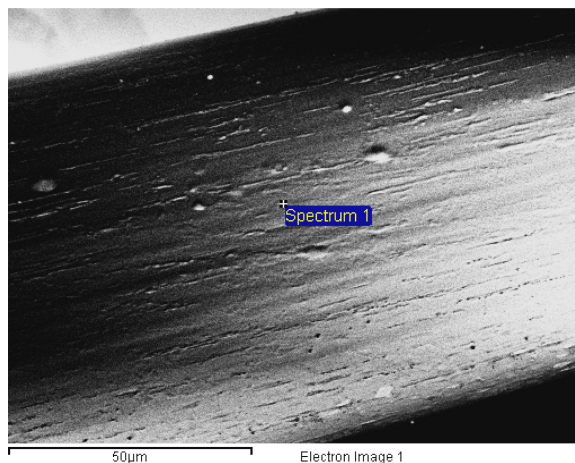
Mo coating is peeling back from tip, but intact down shaft

Bent at tip: means full force hits bend. Also means tip cannot erode back
In step-back fashion. This tip almost unaffected by beam

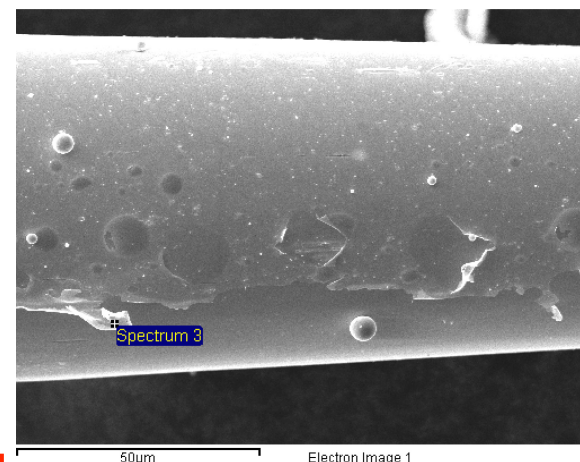
Tungsten needles compared - down shaft away from tip



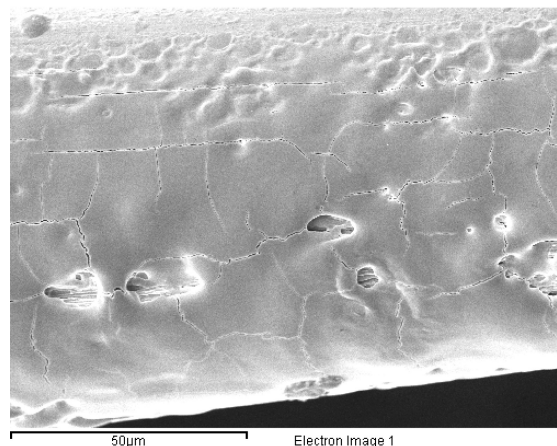
Virgin: 1mm from tip



Mo coated (BSE image): ripples are coating still intact after 1600 pulses. Confirmed by EDS



W needle-uncoated: 1600 pulses



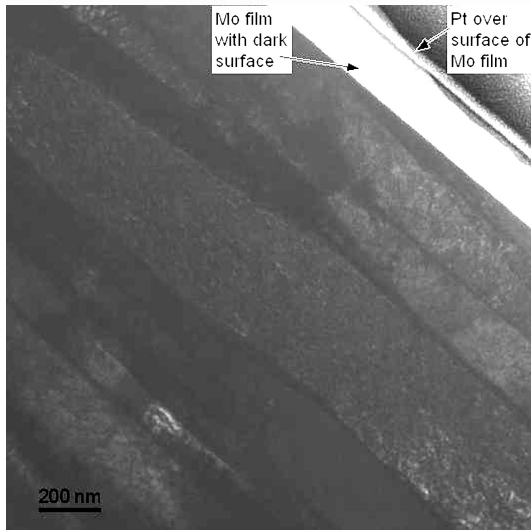
W needle-flat - 400 pulses

A FIB cut is made into the Mo-coated tungsten needle for XTEM

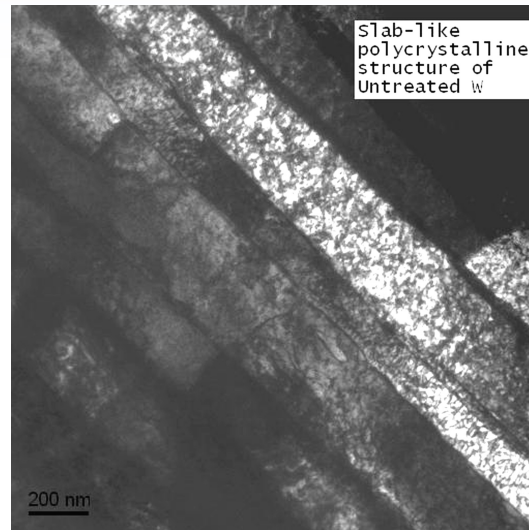
Cut Location

300 μm

FIB-XTEM: Mo-coated W needle survives 1600 pulses with no apparent effect vs uncoated untreated W needle



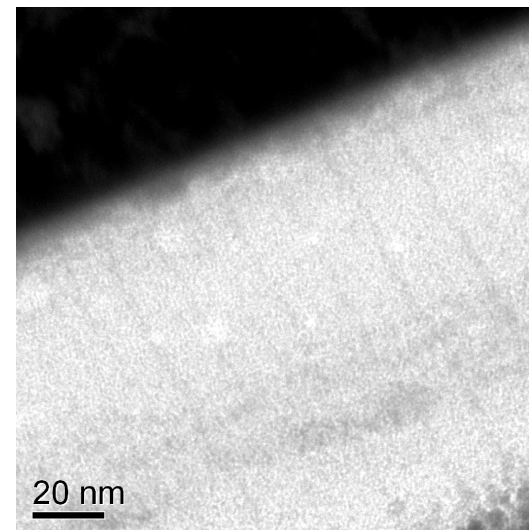
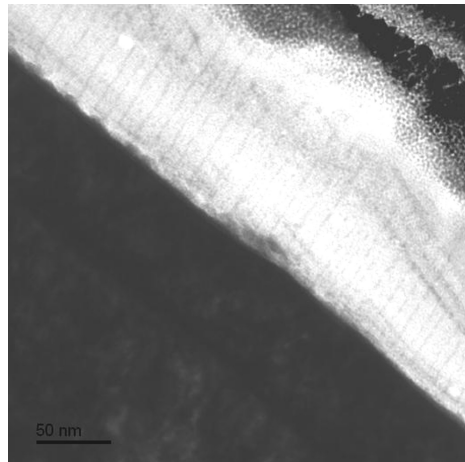
Mo coated - 1600 pulses



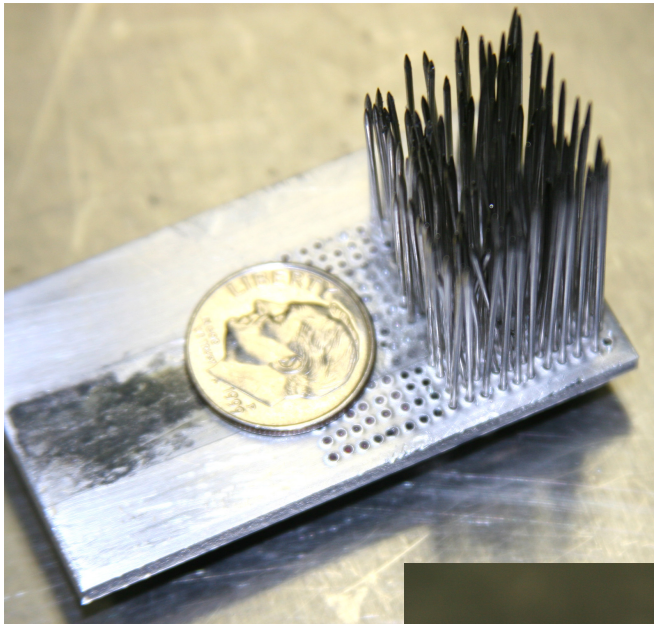
W needle uncoated virgin

- FIB cuts made in both needle surfaces 300 μm from tip
- Both XTEMs show fully dense tungsten with long oriented grains, no voids, no bubbles/blisters
- Close-up (bottom) shows columnar structure of as-deposited Mo - 200 nm thick - original thickness unknown
- No apparent effect from exposure

Magnified
Coated
Treated

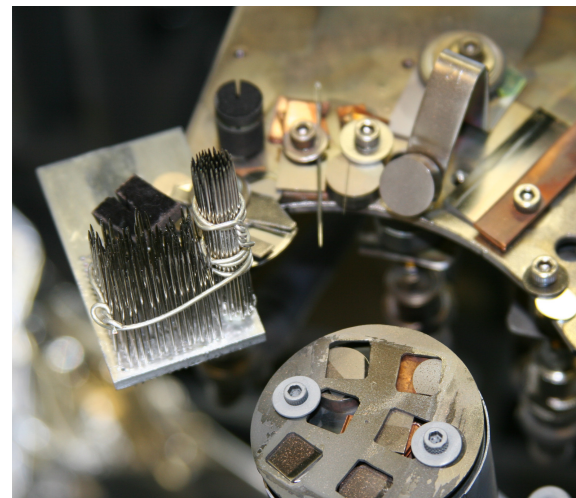
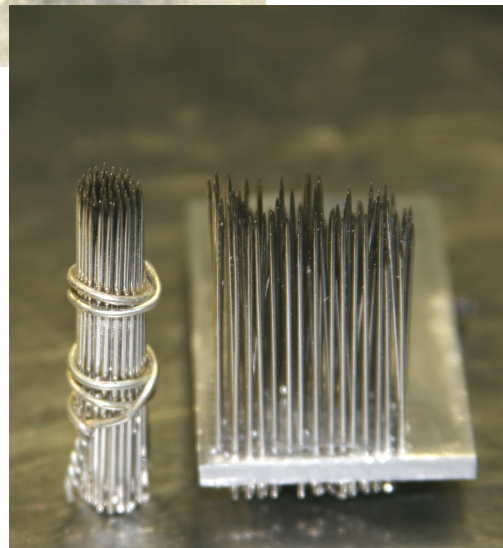


Two arrayed needle geometries investigated



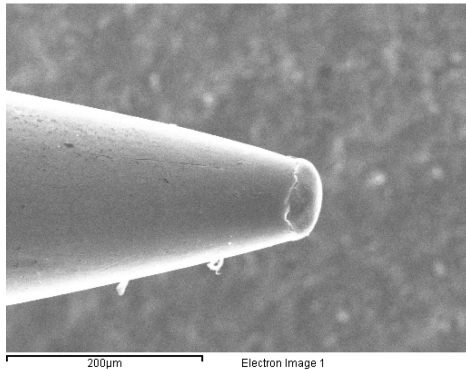
Cost ~ \$5

- Left: 'Array' - Sewing needles and dressmaker pins on Al-6061 substrate, **mylar strip in center**. Hole diameter 0.029in, 175 drilled into 1/8 in substrate 0.060in apart.
- Needle Composition; high carbon steel with Nickel plating
- Bottom Left: 'Bundle' - sewing needles tied together by wires
- Below: Arrays mounted before Shots 1201-1600

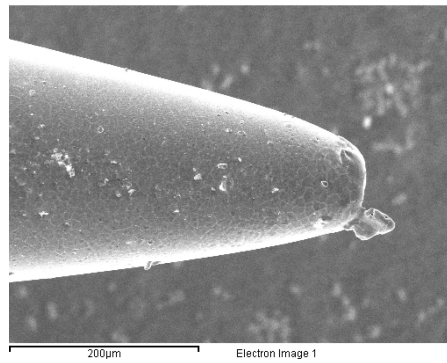


Comparison of Steel needles 400 pulses: virgin, in array, bundled, flat

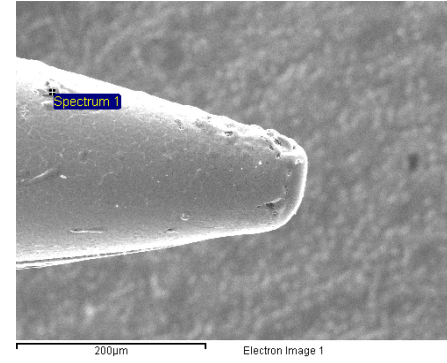
Virgin-Tip



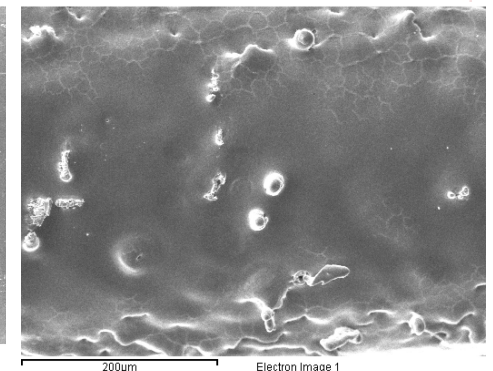
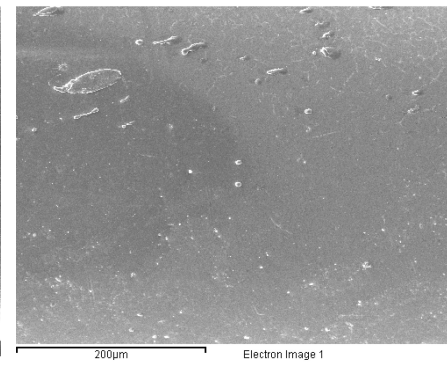
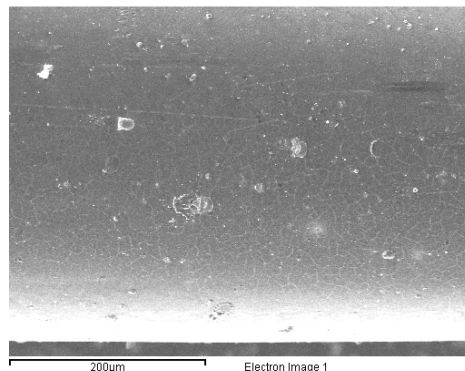
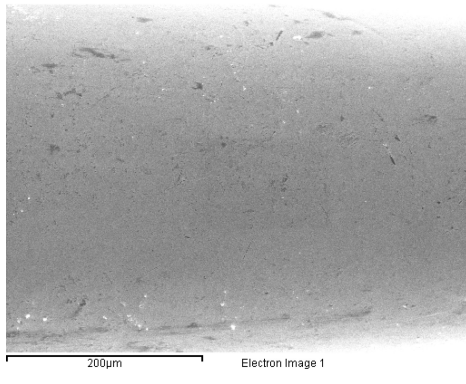
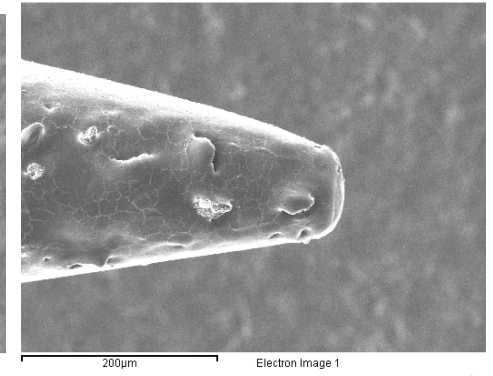
Tip in array



Tip in 'bundle'



Tip. flat



Virgin – 1mm from tip

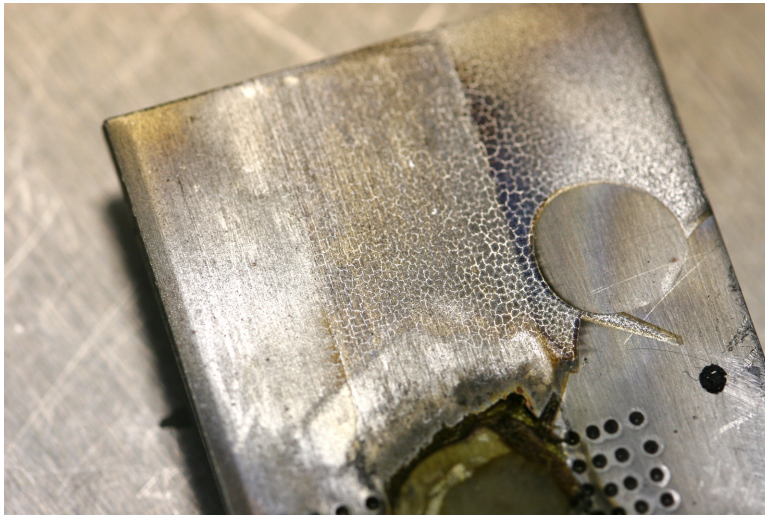
In array – 1mm from tip

In bundle – 2mm from tip

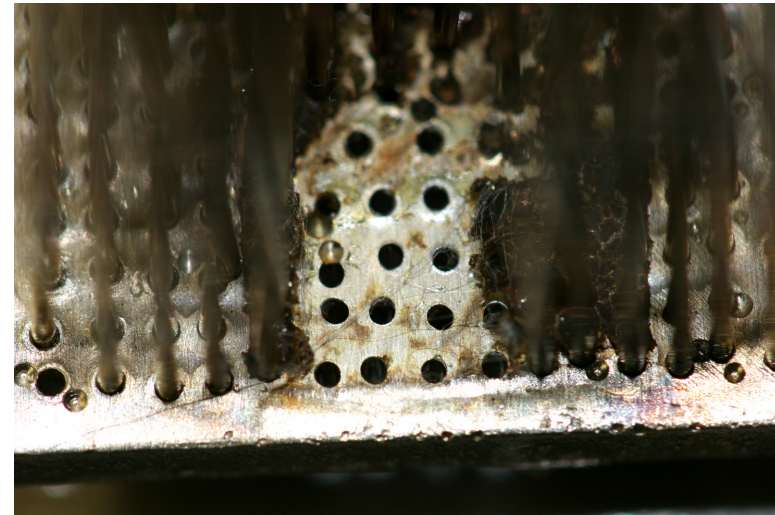
FLAT – 1mm from tip

Away from tip, both bundled and array needle shows almost no effect from 400 pulses

The needles protect the Al-6061 base very effectively:
Mylar strip used as a marker



**BACK of Al (no needles):
Mylar removed, Al melted**



**LEADING edge: Al heavily melted.
In needle 'forest', no Al damage**

- Exposed mylar eroded away
- Inside the 'forest', complete protection of Al substrate, mylar partially intact

Attempt to measure Mass Loss: 4 samples tested post-1600 show mass GAIN

| Sample | Mass Gain (μg) | % Gain | $\mu\text{g}/\text{cm}^2$ |
|-------------|-----------------------------|--------|---------------------------|
| PM Tungsten | 6.358 | 0.35 | 6.358 |
| M184p FLAT | 5.378 | 0.0532 | 5.378 |
| M184p TILT | 115.9 | 1.07 | 115.9 |
| W/M Needle | 2.768 | 1.72 | (35.2) |

- Gain occurs due to Cu adsorption from incoming beam
- M184p TILT gained by far the most mass
- PM tungsten AND M184P FLAT gained similar mass/cm²
- On Areal basis, W/M Needle gained similarly with M184p FLAT
- Assume 116 μg on M184P tilt is entrained Cu. Then Pm tungsten LOST $\sim 95 \mu\text{g}$.
- Then needle area is consistent with $< 1 \mu\text{g}$ gain. Actually gained 2.7 μg .
- Total data on W needles consistent with little or no mass loss due to 1600 exposures.

Summary – fusion materials exposure

- RHEPP pulsewidth similar to He₄ component in reactor, 1-2 J/cm² produces comparable power loading as 154 MJ pulse to 6.5 m-radius wall, comparable He implantation as 415 MJ pulse to 10m-radius wall.
- ‘Needles’ show promise as robust alternative to flat geometry. Little or no affect from 1600 He beam pulses.
 - CAVEAT: THE RHEPP IONS ARE NOT PARALLEL. Must investigate affective fluence compared to parallel ion path expected in reactor.
- Helium exposure of tungsten flats at up to 1600 pulses shows in all cases more surface roughening/signs of exfoliation than with comparable nitrogen pulses. **Not Clear That Any of FLAT Materials RHEPP-tested will survive.**
 - ROCK: effects here **are NOT** due to He entrainment, i.e. **1e18 cm-2** reported He blister formation threshold holds here, and results seen here are due to thermomechanical stress only. Then samples do not appear to be able to reach 1e18 cm-2 without unacceptable morphology change/weight loss.
 - HARD PLACE: effects seen **ARE** due to He entrainment, then threshold for pulsed He exposure is more like upper 1e15 cm-2.



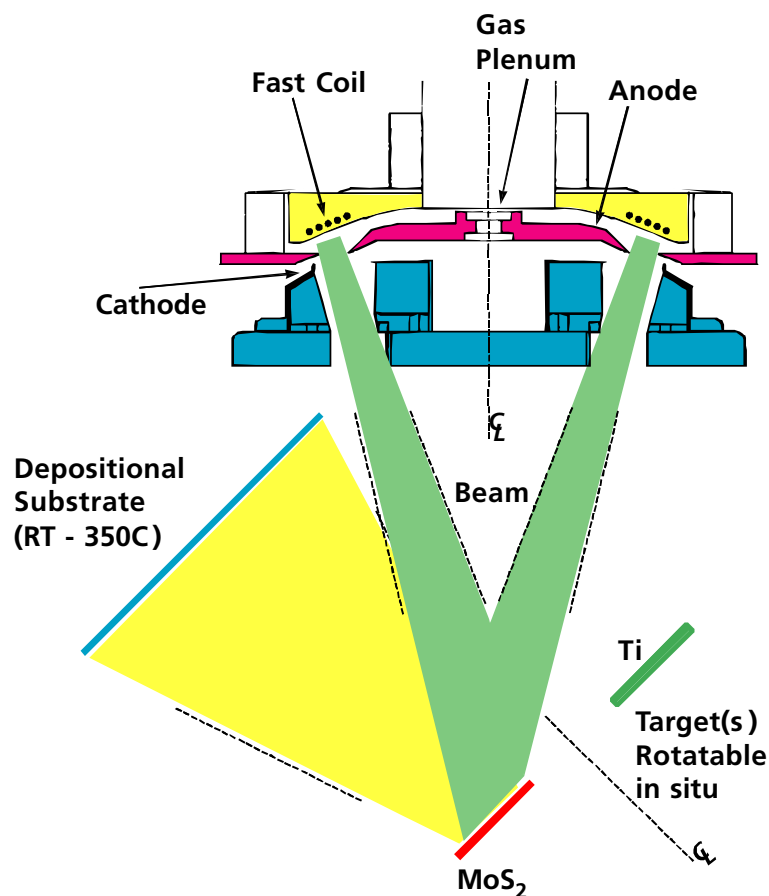
Questions?



Backup Slides

Ablation study of sub-range foils

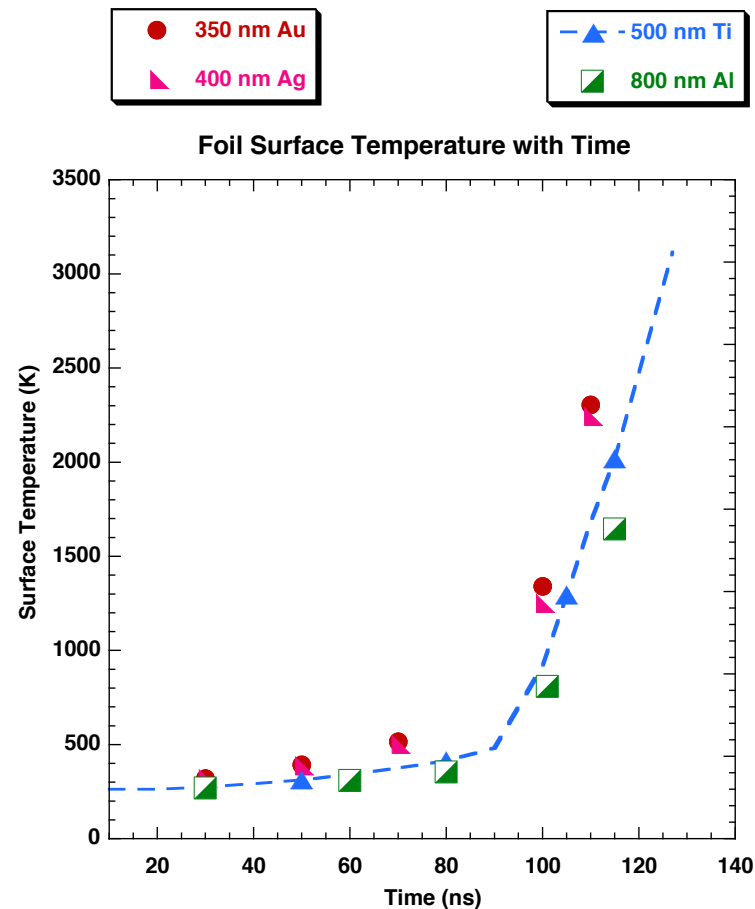
The RHEPP-1 nitrogen beam was used in sub-range foil ablation experiments



- High-energy pulsed ions (700 kV, 200 A/cm²) vaporize and redeposit material. Geometry as shown.
- Foils mounted on same ablation setup for mechanical rigidity. Normal 6-8 J/cm² at beam center reduced by factor 0.707.
- Foils exposed:
 - 650 nm, 800 nm Al 2 - 6.4 to 11.5 cm (Lebow)
 - 400 nm Ag 4 cm
- Conditions DURING ablation not known: analysis of framing images MAY yield clues about ablation dynamics

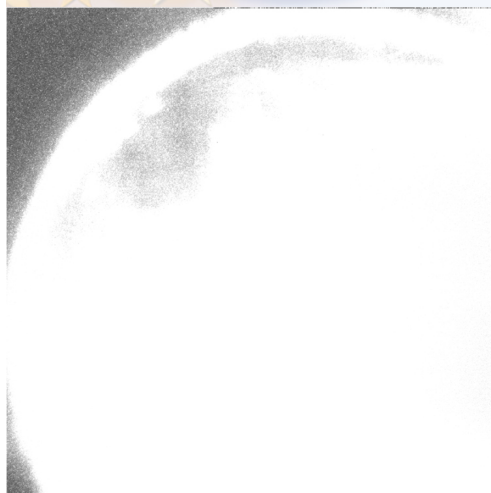
1-D Heat flow modeling: RHEPP nitrogen beam on sub-range foils

- Purpose – predict thermal response of sub-range (for RHEPP) Au, Ag, Ti, Al. Look for fastest heating rate.
- Proton precursor to 90 ns, then Ni (++) heating starts
- Au heats from surface melting to ablation in ~ 15 ns
 - Ag not far behind
 - 800 nm Al too slow



1st Experiment: plume evolution, solid titanium target

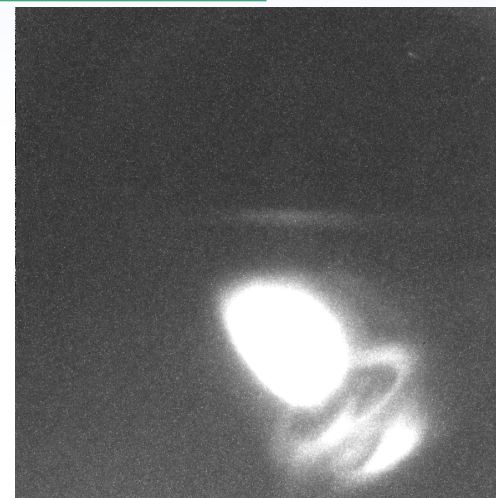
Exposure = 100 ns



T = 0 sec (arbitrary)



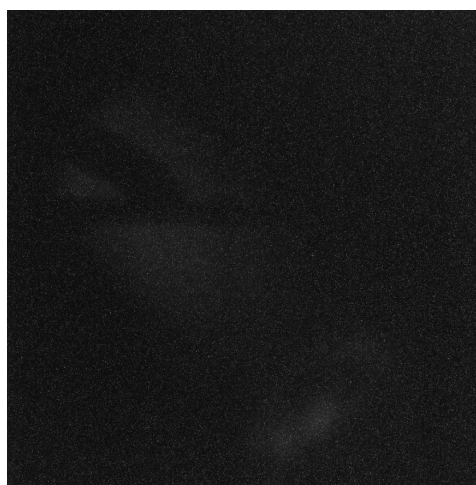
T = 2.35 μ sec



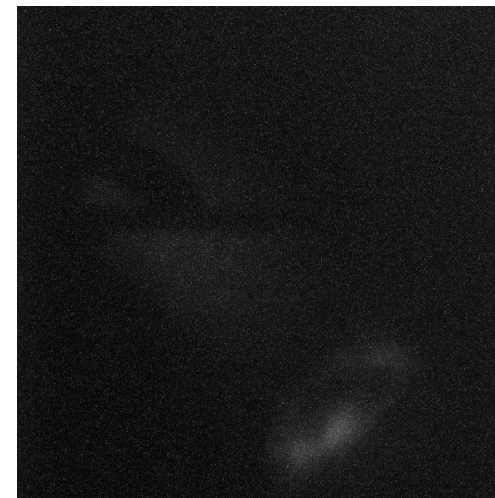
T = 7.35 μ sec



T = 12.35 μ sec



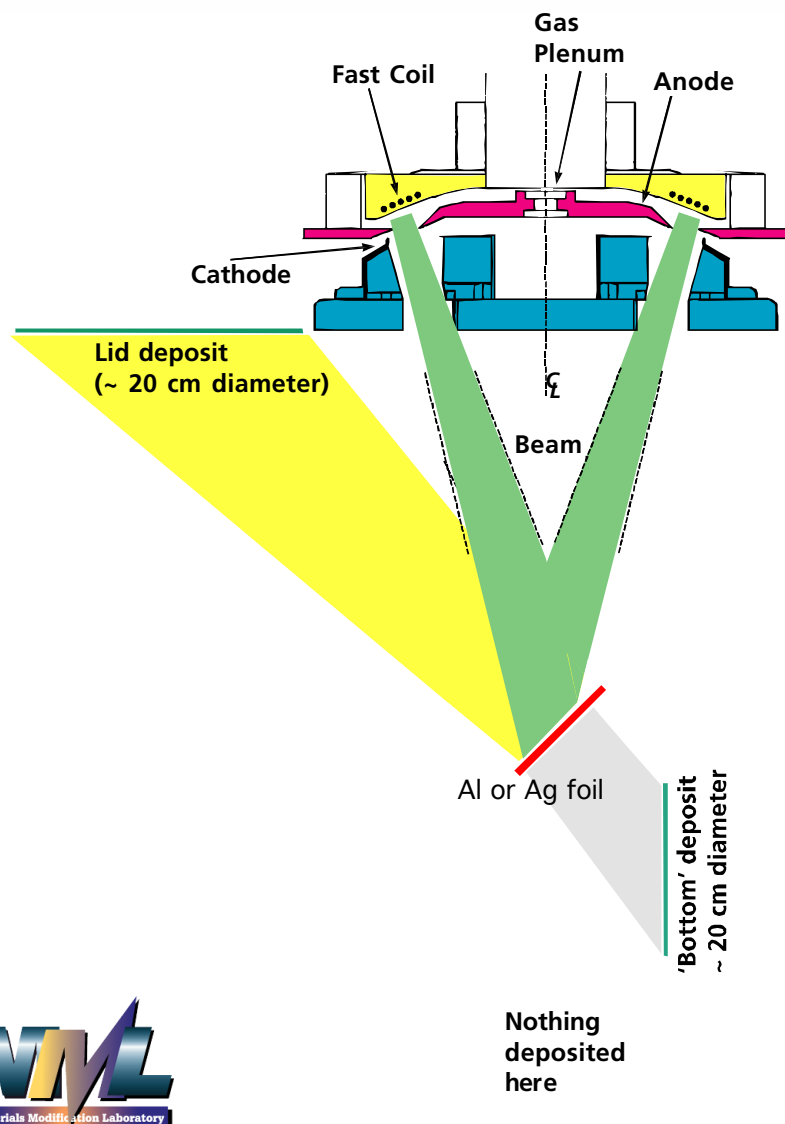
T = 17.35 μ sec



T = 22.35 μ sec

Note: 1) slowness of plume evolution, 2) 100 nsec exposure time

The RHEPP-1 nitrogen beam strikes foil at 45°, and film is deposited in both directions normal to foil plane



- High-energy pulsed ions (700 kV, 200 A/cm²) vaporize and redeposit material. Geometry as shown.
- 'Lid' deposit at ~ 50-60 cm distance, 'bottom' deposit at ~ 20 cm distance. Si wafer mounted for 1-D dek-tak thickness profile measurements
- No deposition observed at tank bottom
- Foils exposed:
 - 650 nm Al 11.5 cm diam (Lebow)
 - 400 nm Ag 4 cm diam (Lebow)

40 mm diameter Ag target, Shot 2039

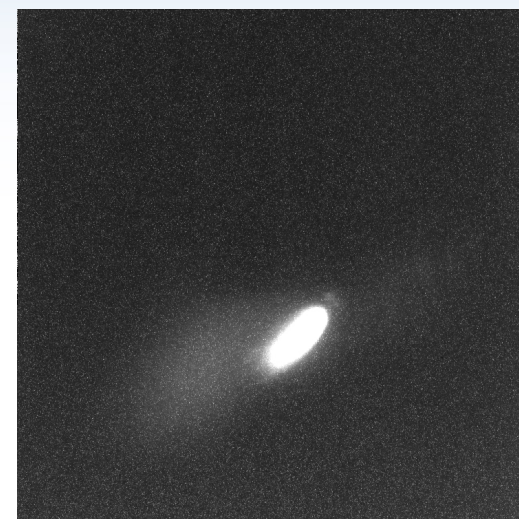
Exposure = 5 ns



T = 4100 ns (arbitrary)



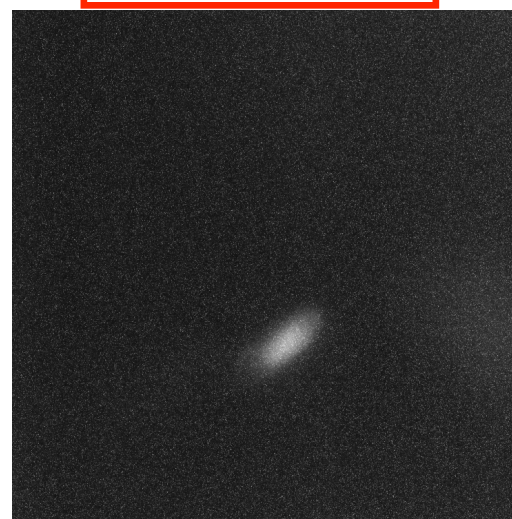
T = 4250 ns



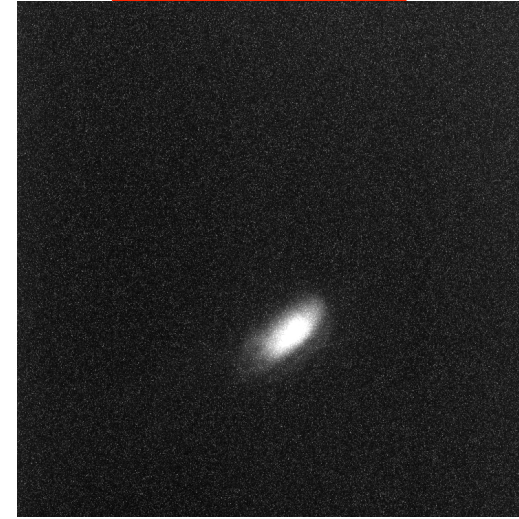
T = 4400 ns



T = 4700 ns



T = 4850 ns

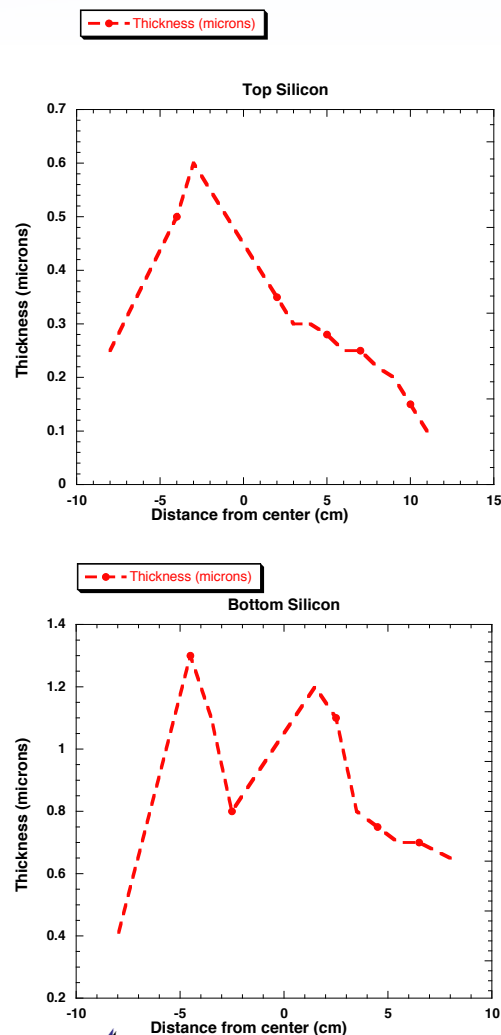


T = 5000 ns

Note: 1) diameter shrinks with time, 2) 900 ns total time duration

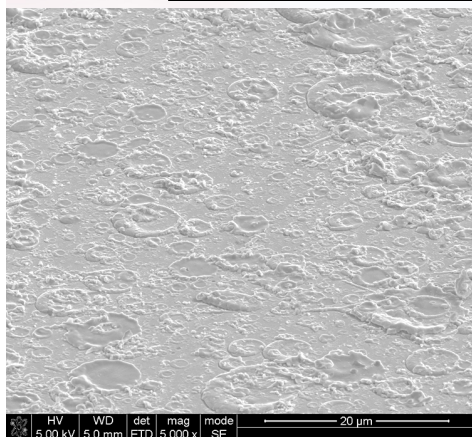


The RHEPP-1 nitrogen beam strikes foil at 45°, and film is deposited in both directions normal to foil plane

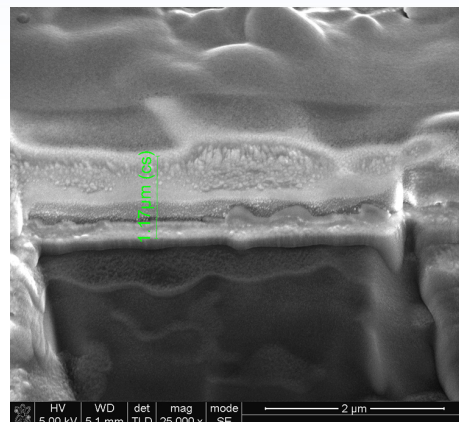


- 1-D dek-tak thickness measurements made of both top and bottom depositions. Two chords measured from (approx) deposition center (left).
- 'Smoothed profile overlaid, material inventoried using average thicknesses and $2\pi r \Delta r$ additions.
- Totals: 81 $\mu\text{m-cm}^2$ top, 181 $\mu\text{m-cm}^2$ bottom, 265 $\mu\text{m-cm}^2$ total. FIB-SEM of samples shows ~ 25-50% increase in thickness compared to dek-tak
- Total volume of 7 foils shot (not including He shot): 479 $\mu\text{m-cm}^2$. So between 70 and 85% of initial mass accounted for.
- Foil surface rough - typical $R_A \sim 0.3 \mu\text{m}$

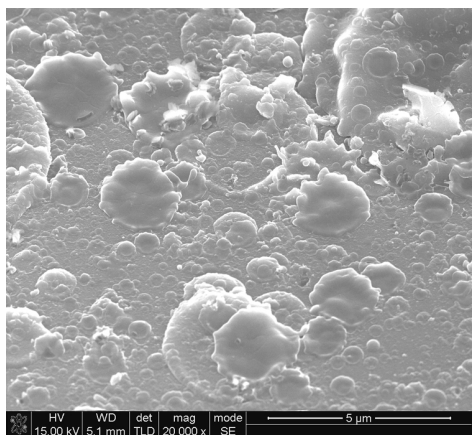
The RHEPP-1 deposited film appears to be formed of droplets, but film appears slightly porous to fully dense



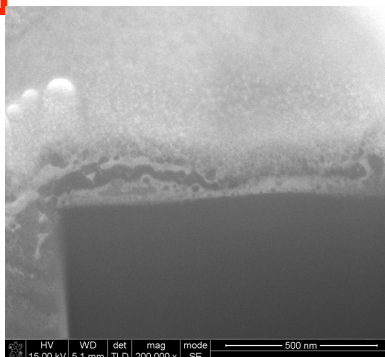
SEM, deposited material, 'top' 3 cm radius



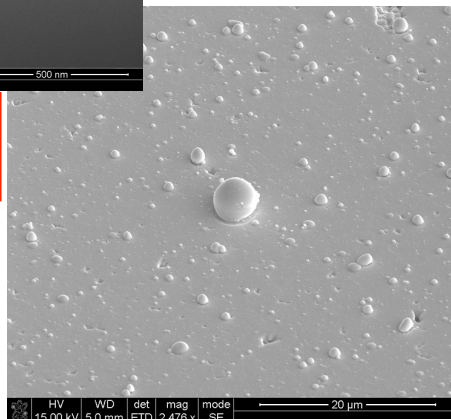
FIB/XTEM, top 3 cm film



SEM, deposited material, 'top' 5 cm radius



FIB/XTEM, top 5 cm film



SEM, Ni film from solid target

- 'Smoothed profile overlaid, material inventoried using average thicknesses and $2\pi r \Delta r$ additions.
- FIB-SEM of Top 3 cm radius point (right) shows twice the thickness as Dek-tak indicates. So 265 becomes 530.
- Total volume of 7 foils shot (not including He shot): $479 \mu\text{m-cm}^2$. So about equal to deposited material.
- Surface of Ni film deposited from **thick target** is much smoother (below)
- SEM shows 'droplets' - indication from FIB is 'overlapped pancakes'
- EDX shows Al, O in film. Since we break vacuum every shot (unlike with films from solid targets), much more oxidation occurs.

Summary of sub-range foil shots

- Extended timescale imaging: 40 mm Ag shows lighted image for 900 ns.
- Al (much larger diameter target) light shows much shorter duration.
- Deposited film measurements show twice as much film deposited from foils in 'transmission' direction, compared to 'reflected' direction. No material is deposited in direction of beam propagation.
- FIB cut and SEM images of film surface show 'droplet' appearance. Viewing of the cut indicates fully dense to slightly porous layer. This may be expected since the most of material is probably deposited in molten state. Measured thickness shows that dek-tak is off by factor ~ 2 . Therefore, the two spots together account for roughly all the material in the foils.