

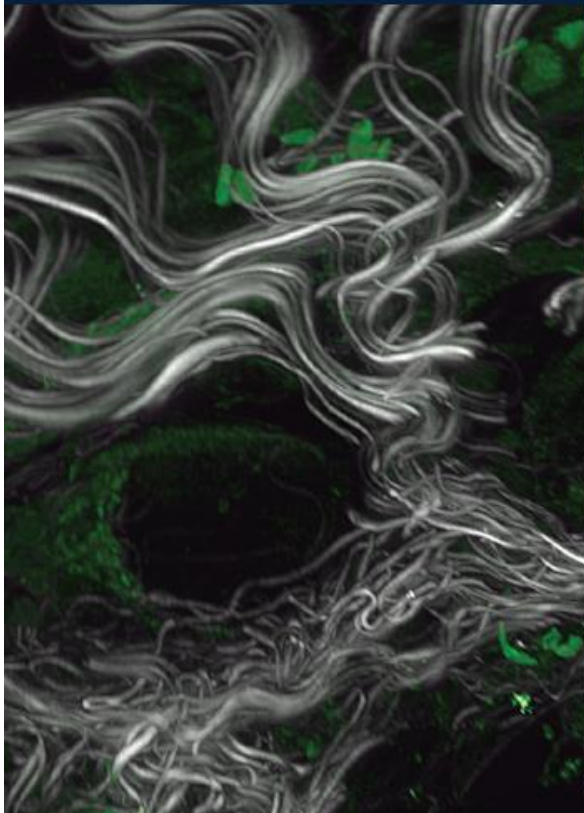
ancillary meeting times,
and much more.



M&M 2015
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MICROANALYSIS**
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www.microscopy.org/MandM/2015 for up-to-date meeting information

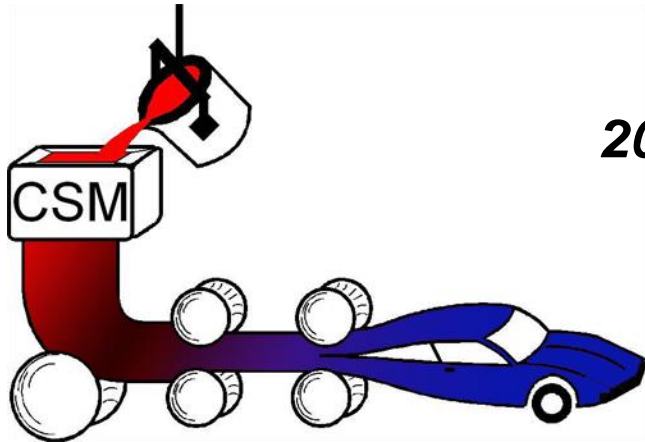


Microstructural Developments Leading to New Advanced High Strength Sheet Steels: *A Historical Assessment of Critical Metallographic Observations*

**David K. Matlock, Larrin S. Thomas, Mark D. Taylor,
Emmanuel De Moor, and John G. Speer**

Advanced Steel Processing and Products Research Center*
Colorado School of Mines
Golden, Colorado

***2015 IMS Henry Clifton
Sorby Award
August 3, 2015***



****An NSF Industry/University Cooperative
Research Center - Est. 1984***

...Perspective...



“...More than half of the steels present in today’s vehicles didn’t exist 10 years ago and with breakthrough technologies and industry innovations, just imagine what steel will be able to accomplish tomorrow...” <http://driveusingsteel.com/> (accessed July 2015)

...development of new steels facilitated by advanced microstructural analyses...!!

Henry Clifton Sorby (1826 – 1908)



Portrait in Mappin Hall
University of Sheffield

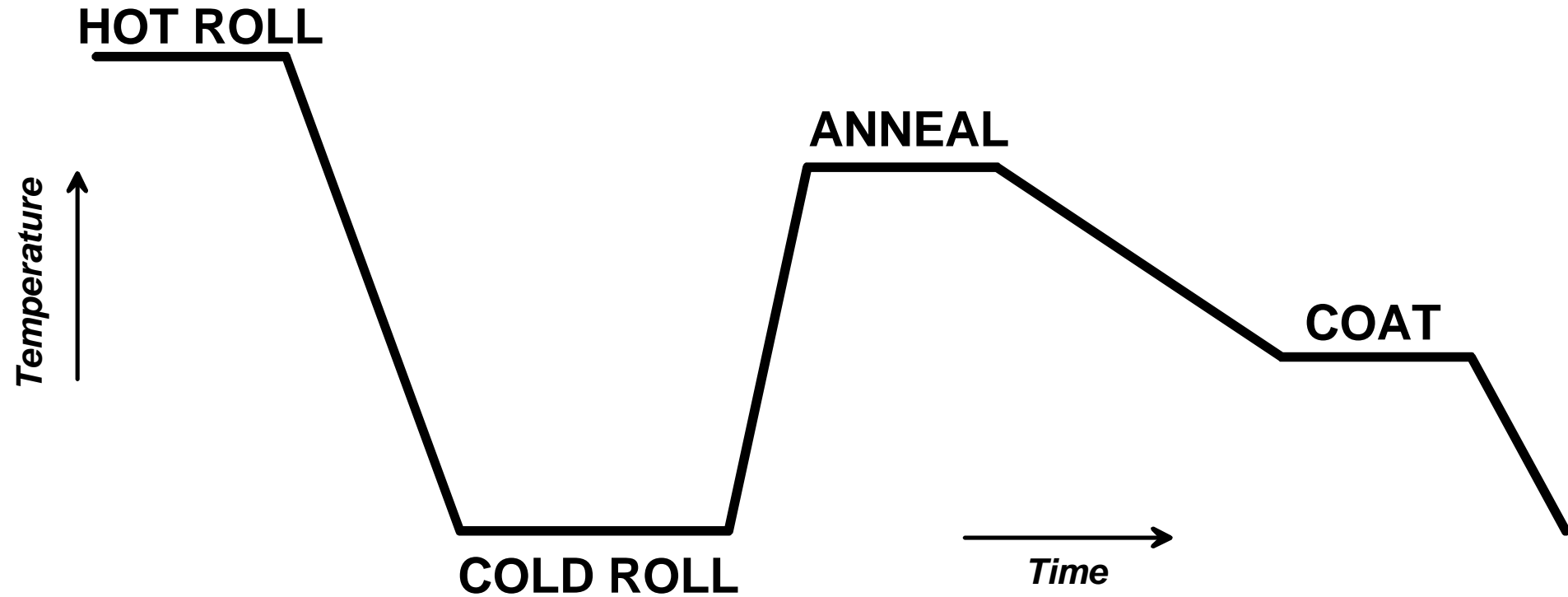
Pioneer of Ferrous Metallurgy Metallography

"In those early days, if railway accident had occurred and I had suggested that the company should take up a rail and have it examined with the microscope, I should have been looked upon as a fit man to send to an asylum. But that is what is now being done..."

Theme: Process Control



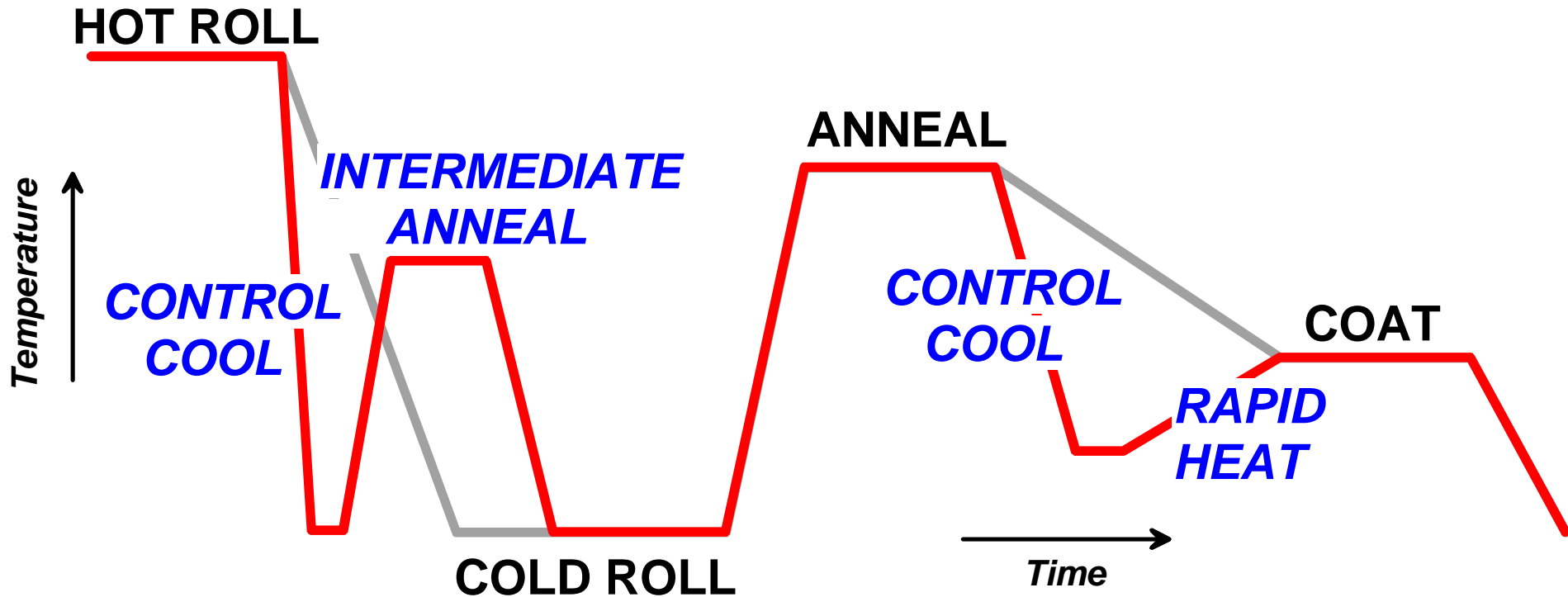
Historical



Theme: Process Control

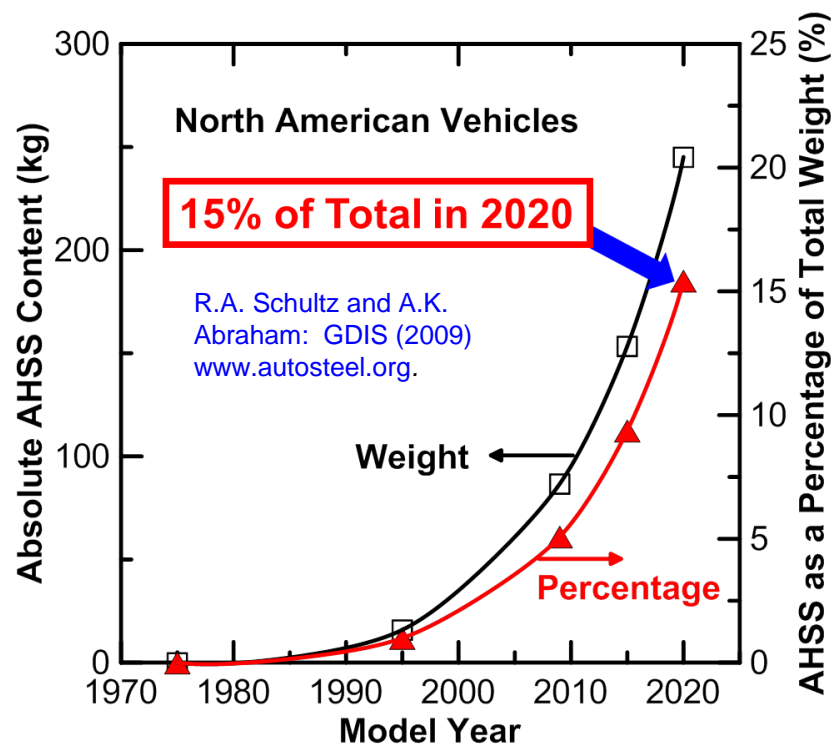


Process Control and Alloying = Advanced High Strength Sheet Steels (AHSS)



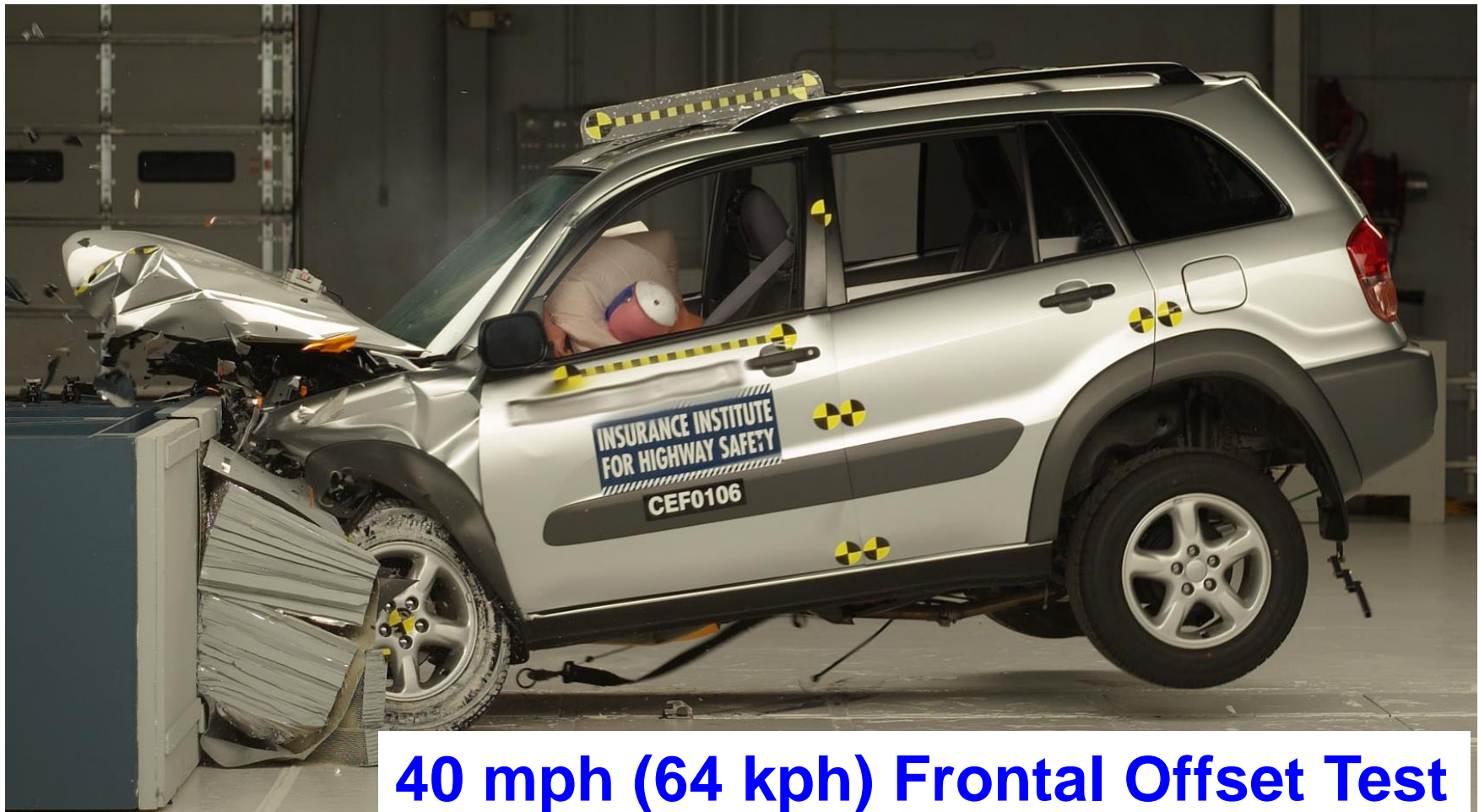
Why do we need AHSS?

High strength steels to enable safe, fuel-efficient lightweight designs



US Requirements for Automotive Steels

- Design vehicle to produce “5-star” crash worthiness rating
 - High toughness steels to absorb energy



40 mph (64 kph) Frontal Offset Test

US Requirements for Automotive Steels

- **Roof crush resistance: increase to 4.0 times vehicle weight - (by 2017)**



- **High strength steels to maintain safety cage**



US Requirements for Automotive Steels

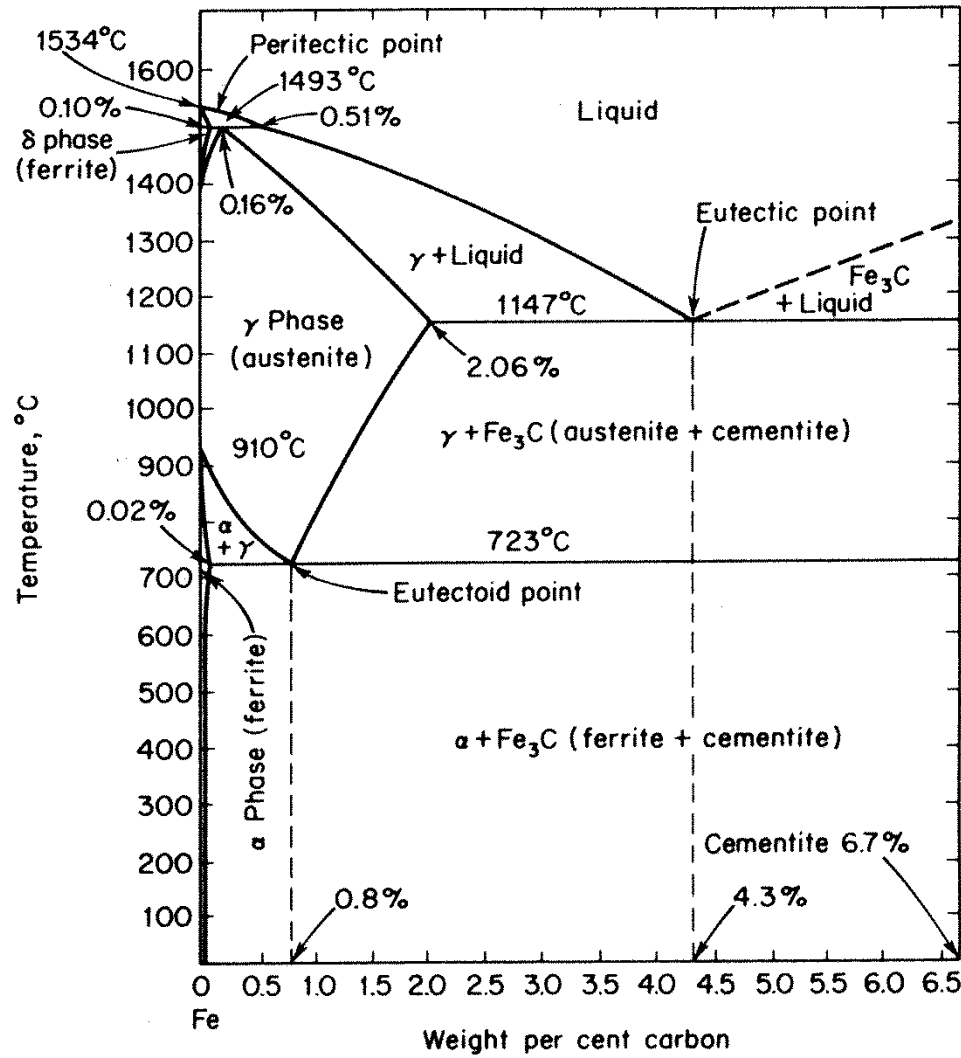
- **CAFE (Corporate Average Fuel Economy)**
 - Increase to 54.5 mpg (23.2 km/liter) by 2025
- **Enhance competition to meet CAFE**
 - Alternate vehicle technologies
 - Alternate materials
 - *High-strength steels for light-weight designs*



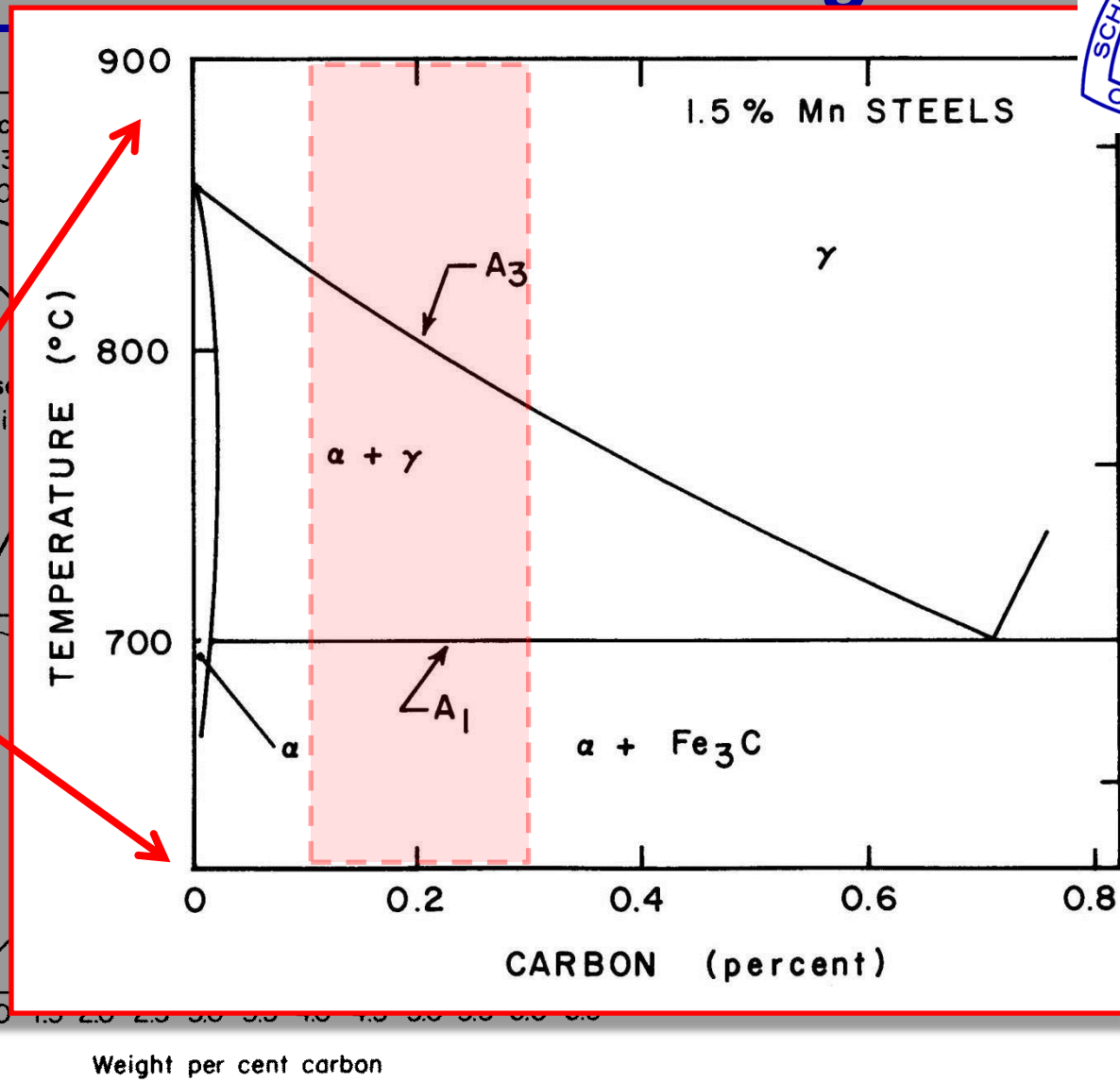
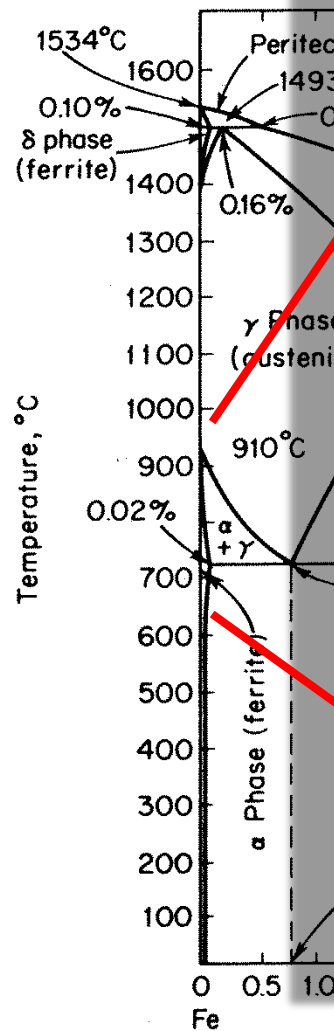


What are Advanced High Strength Sheet Steels (AHSS)?

Background: Fe-C Phase Diagram



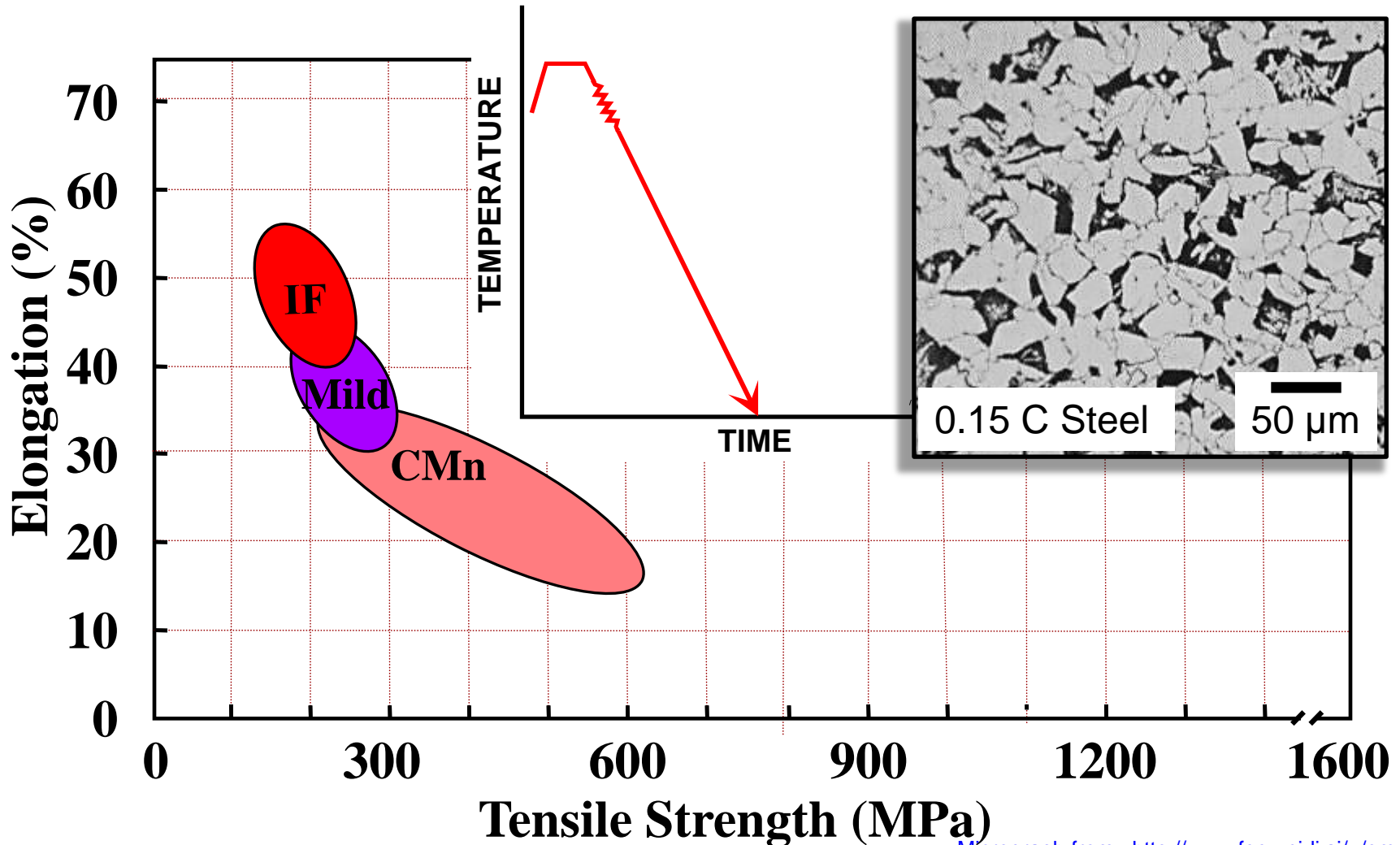
Background: Fe-C Phase Diagram



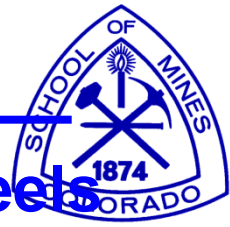
Background: AHSS Developments



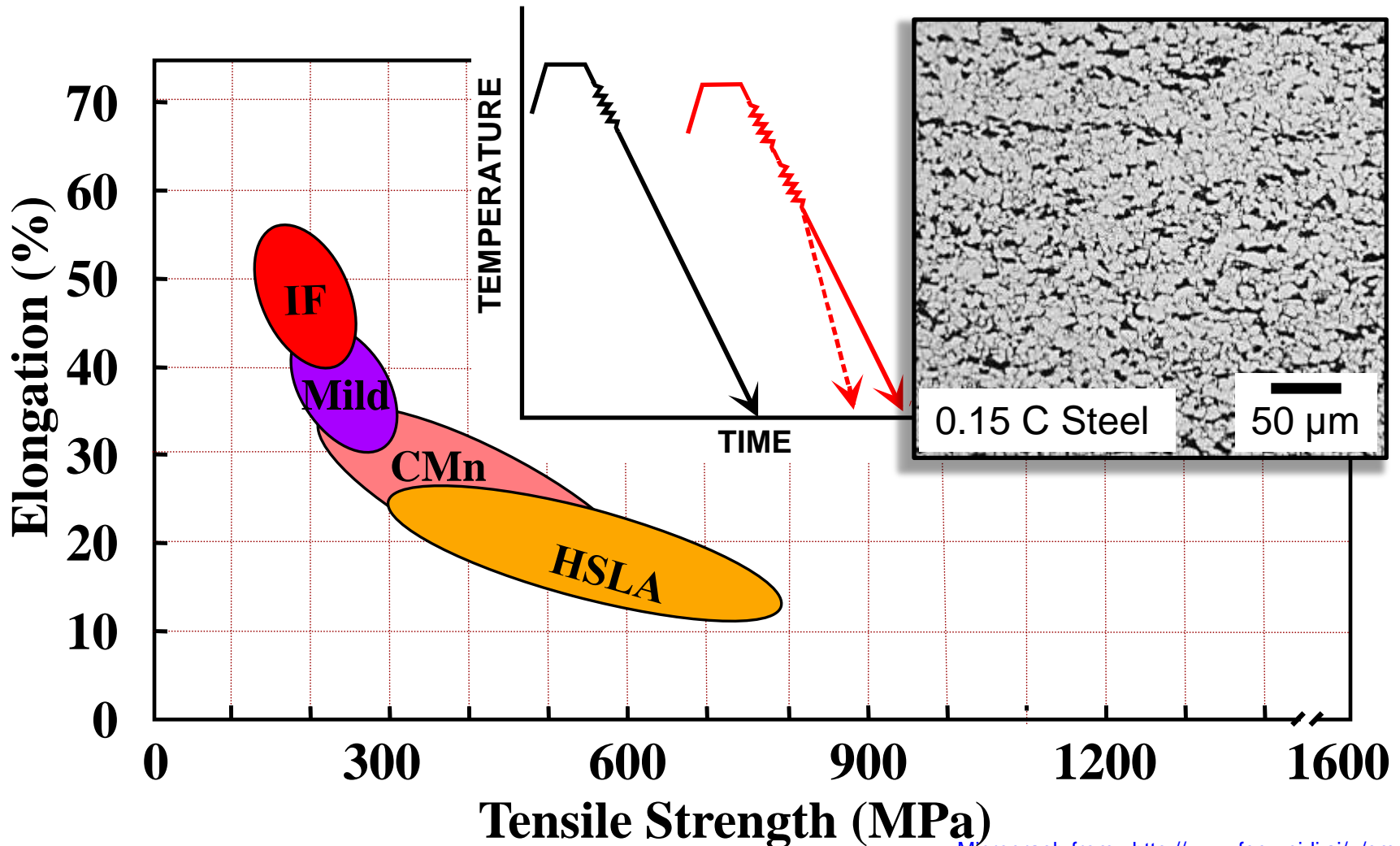
- **Earlier times:** Hot rolled low carbon steels
 - Ferrite – Pearlite



Background: AHSS Developments



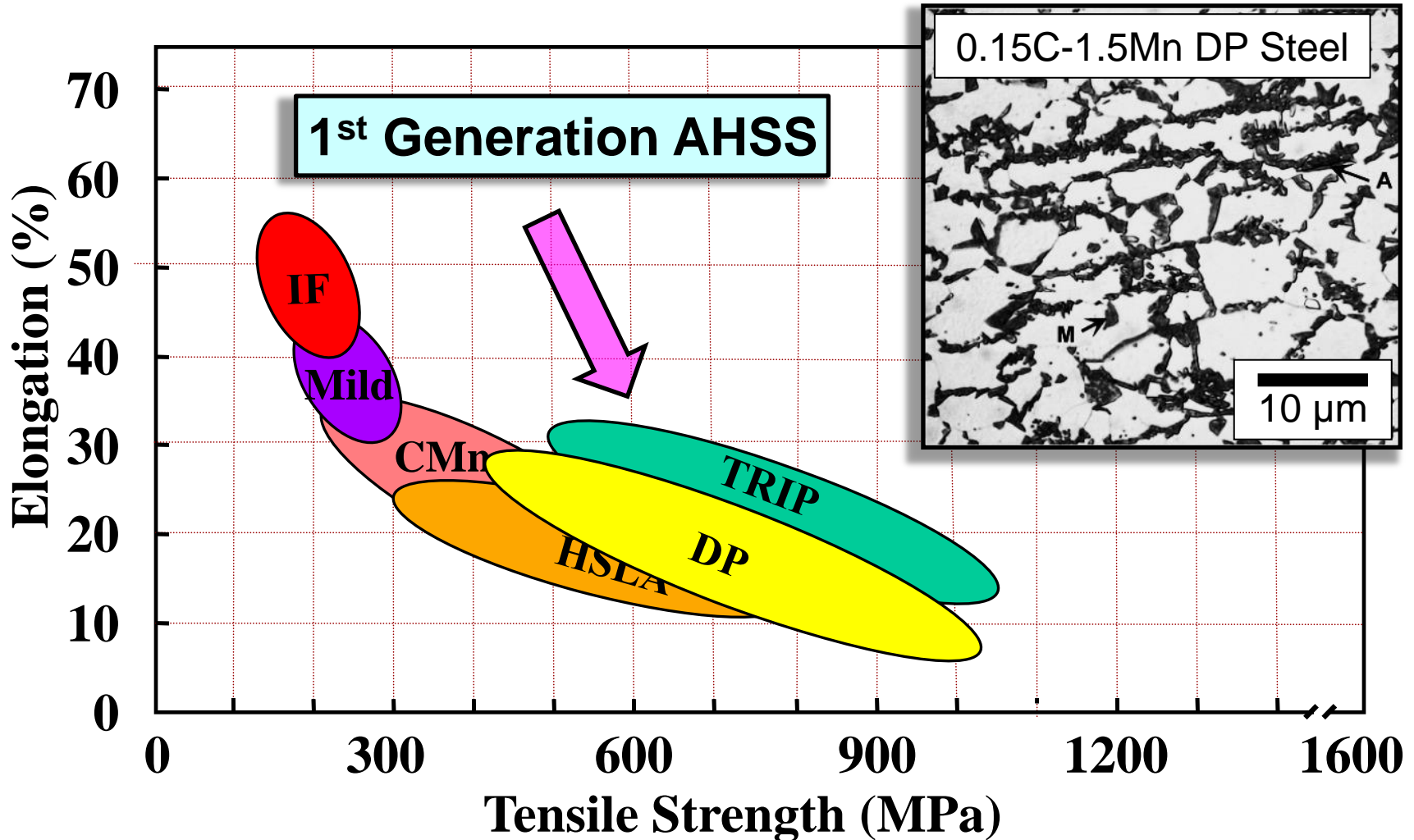
- 1960's – 1970's: High Strength Low Alloy (HSLA) steels
- Thermomechanical processing + microalloy additions



Background: AHSS Developments



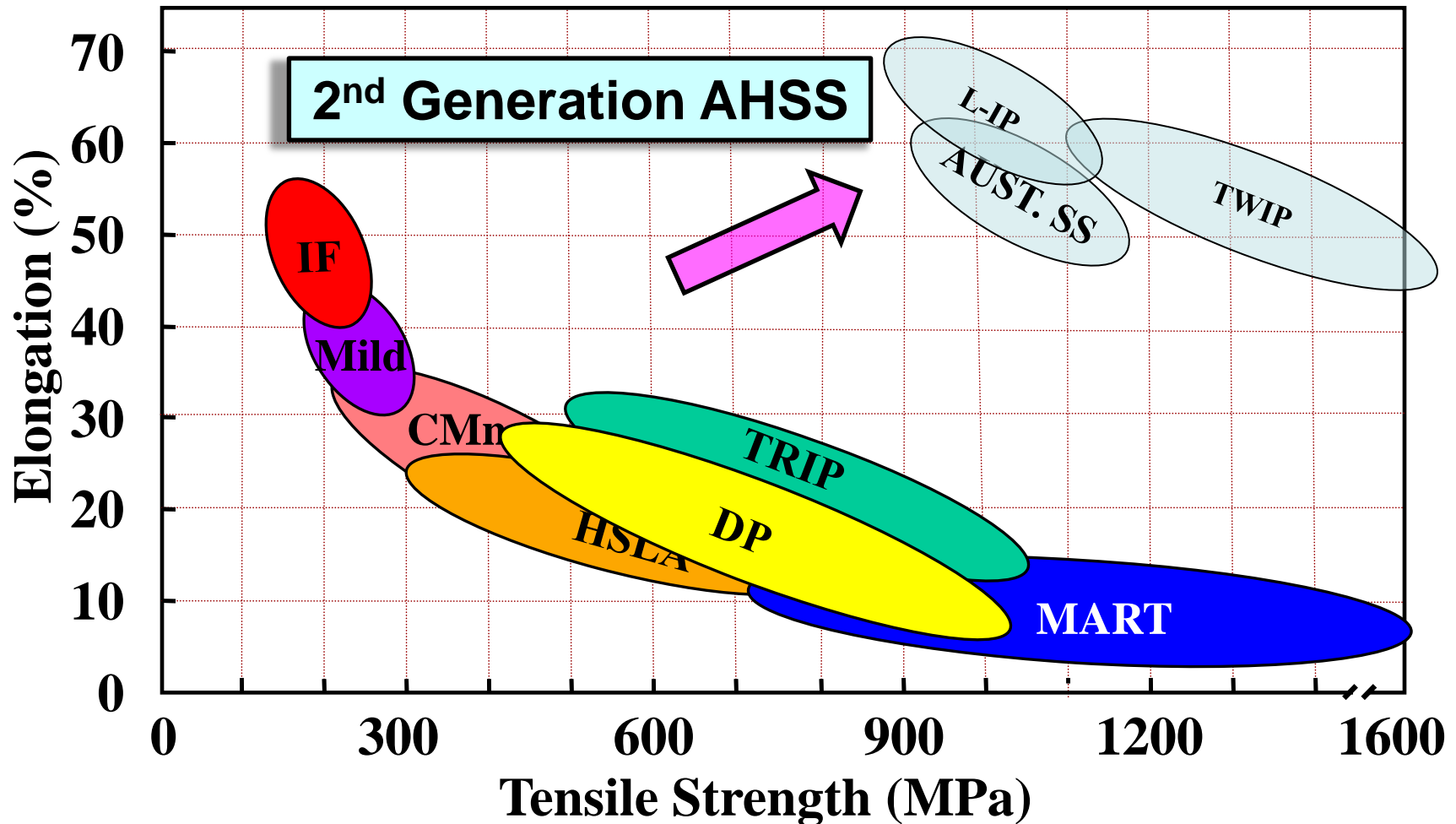
- 1970's – 1990's: Dual-phase (DP) and Transformation Induced Plasticity (TRIP) steels



Background: AHSS Developments



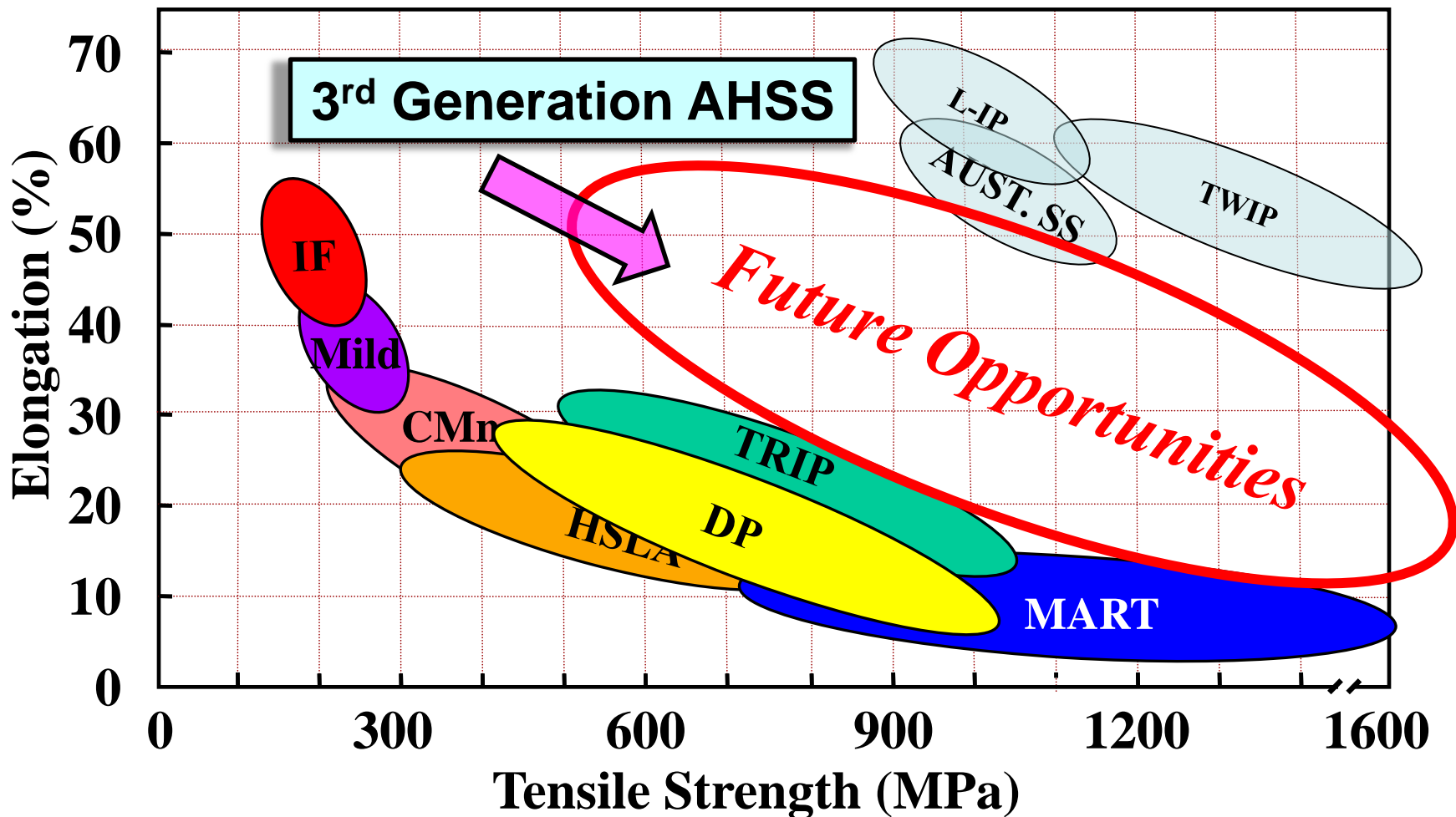
- **Historical:** Austenitic steels = expensive
- Stainless and Twinning Induced Plasticity Steels (TWIP)



Background: AHSS Developments



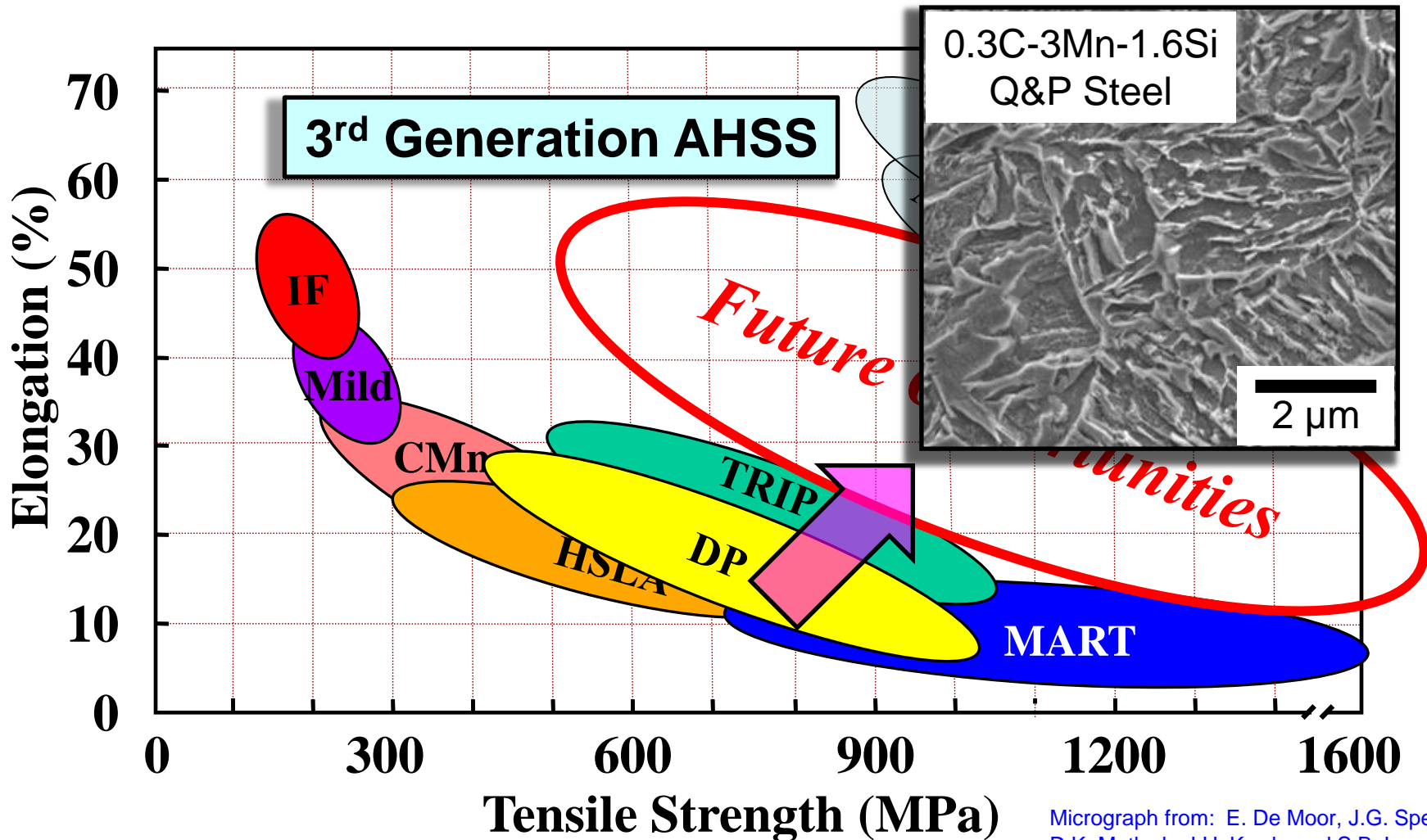
- **2000's and Beyond:** Multiple new grades
- Cost effective alternatives



Background: AHSS Developments



- **2000's and Beyond: 3rd Generation AHSS**
- **Example: Quenched and Partitioned Steel (Q&P)**



Micrograph from: E. De Moor, J.G. Speer, D.K. Matlock, J.H. Kwak, and S.B. Lee, *ISIJ Intl.* Vol. 51, no. 1, 2011, pp.137-144.

Plot adapted from - AISI: www.steel.org (2006)

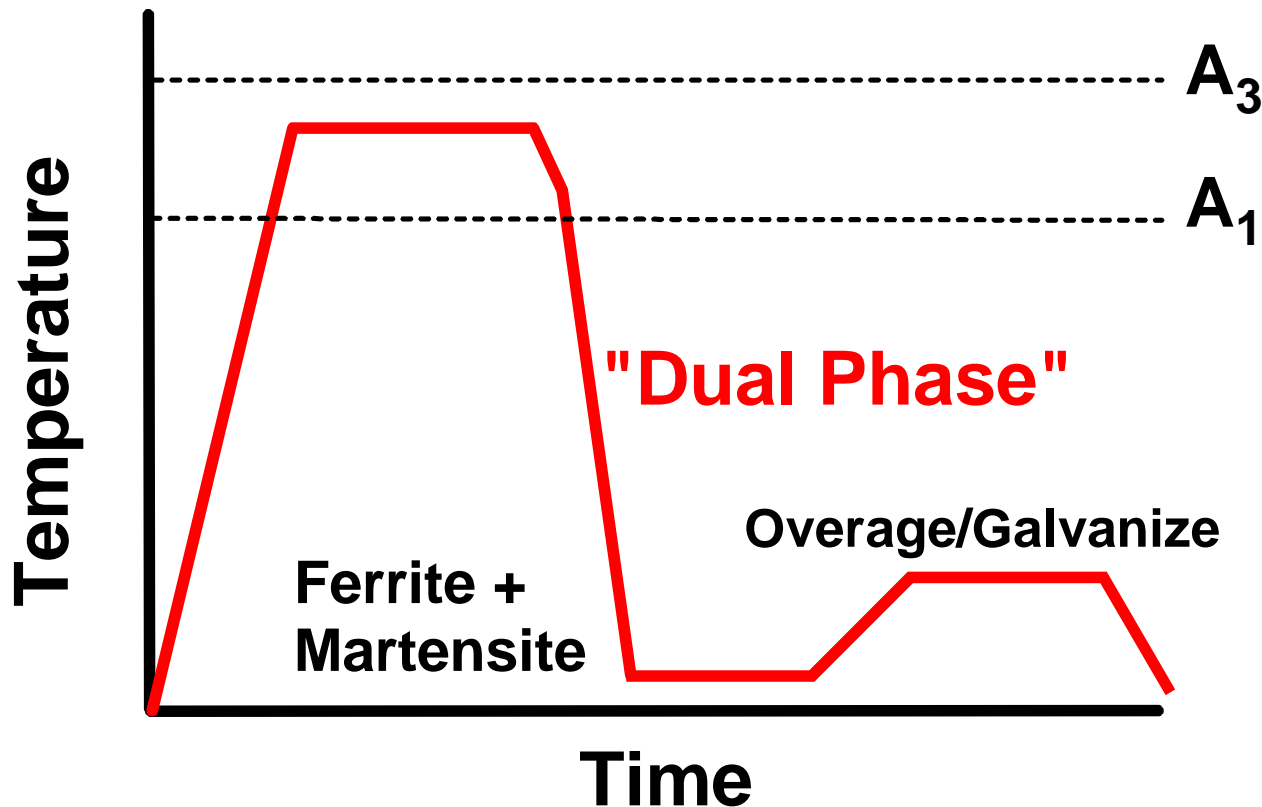


Dual-Phase Steel “Fundamentals”

**Hot Rolled DP Steels
Cold Rolled DP Steels**

DP Steel Processing

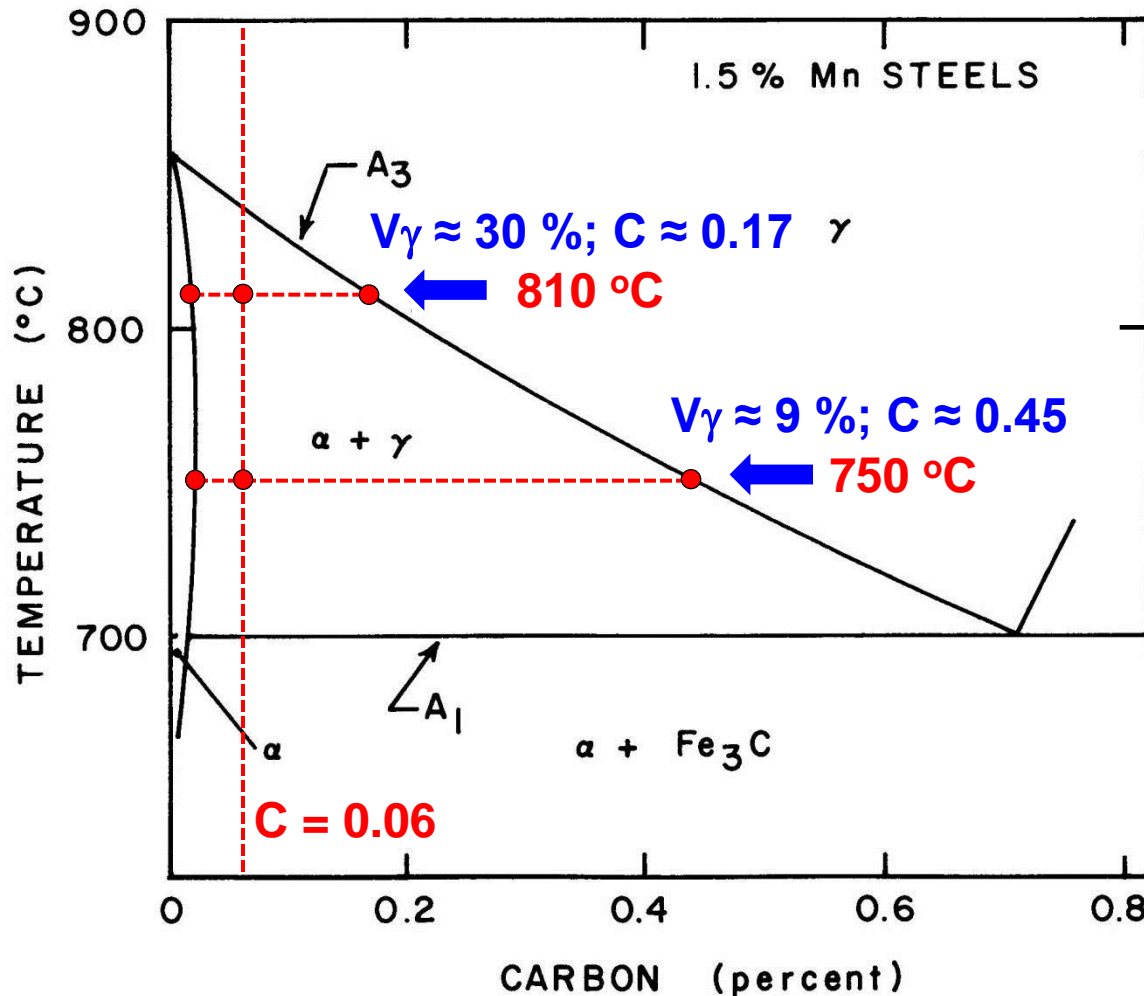
- Initially conceived based on “simple” routes for hot and cold rolled steels
 - Now, process controls offer significant opportunities to produce enhanced properties



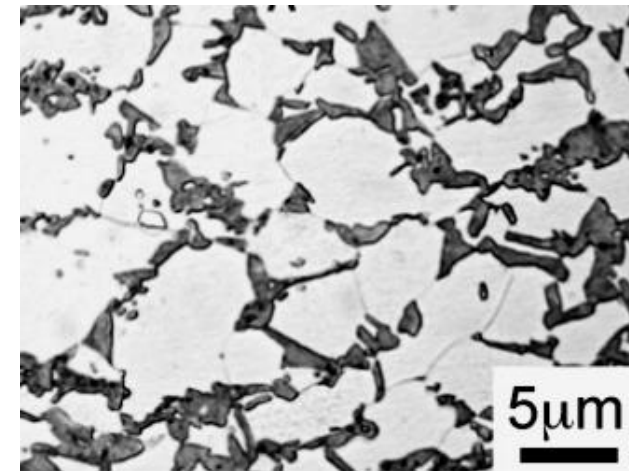
DP Steel Processing



“Typical:” **C: 0.05 - 0.15** **Mn: 1.0 – 2.0**
Others: Si, Cr, Ni, Mo, Nb, V



0.15C, 1.5 Mn, 1.5 Si
WQ from 775°C



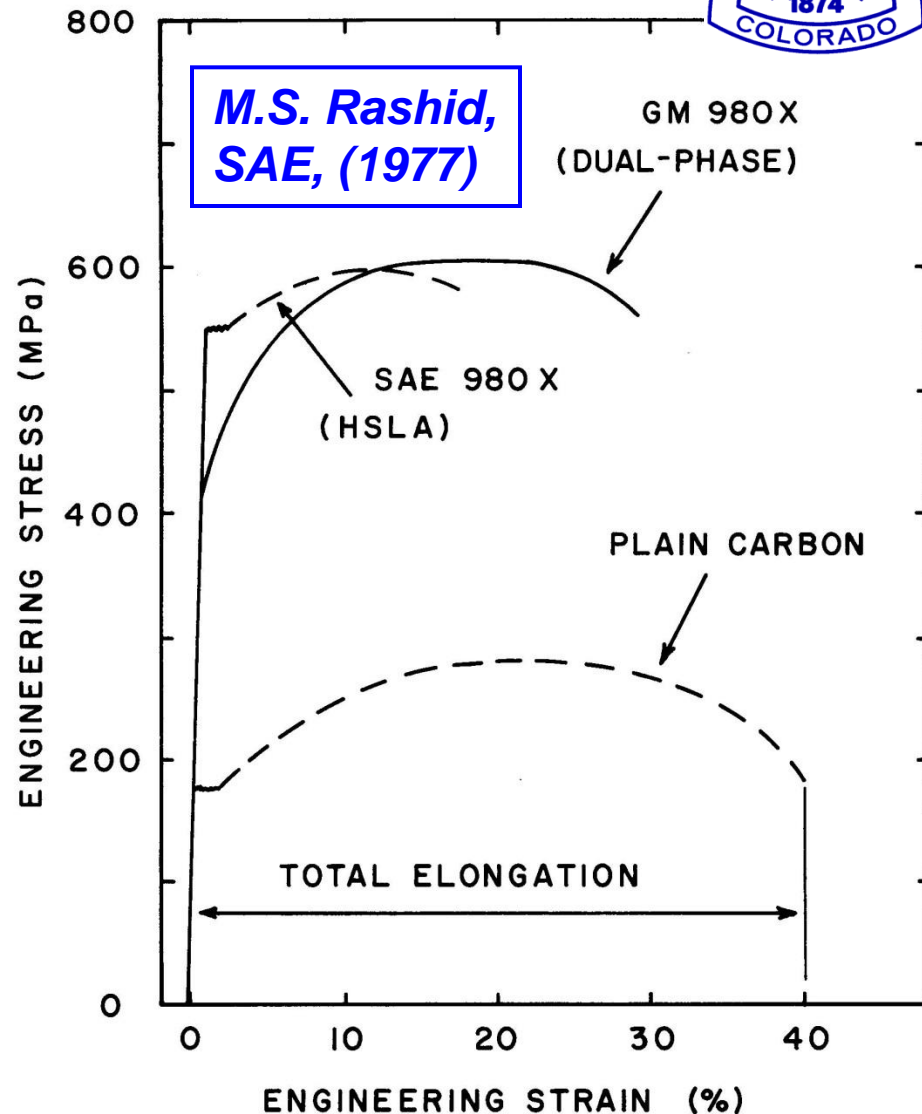
A.K. De, J.G. Speer, and D.K. Matlock, *Applied Materials and Processes*, vol. 161, Feb. 2003.

Dual-Phase Steels: “The Early Days”



Significant Parallel Research Activities

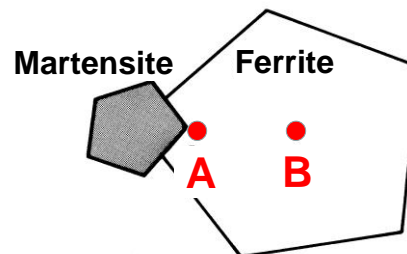
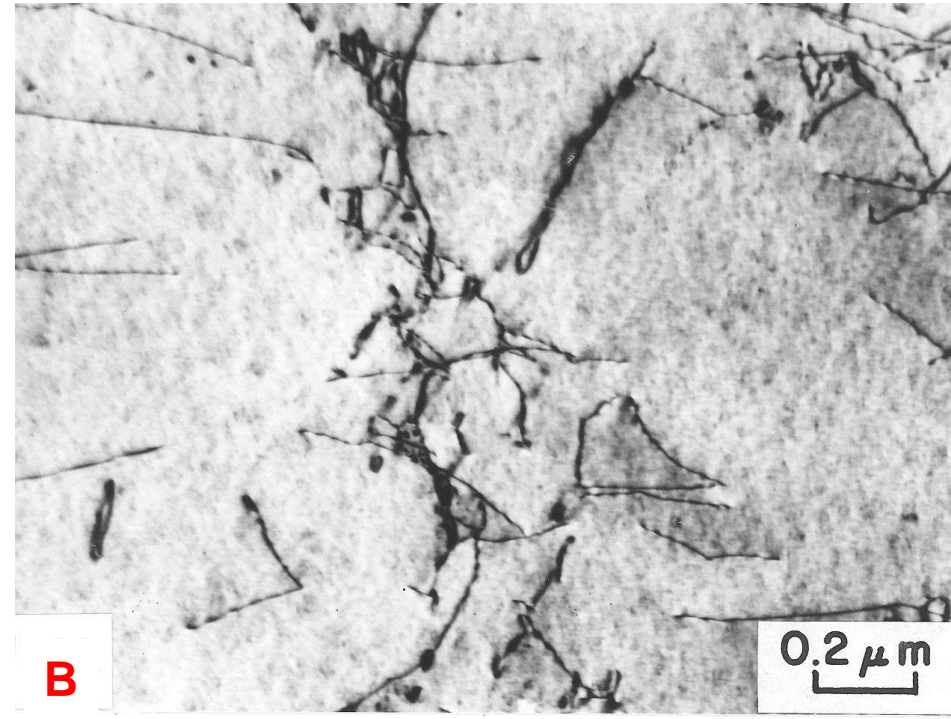
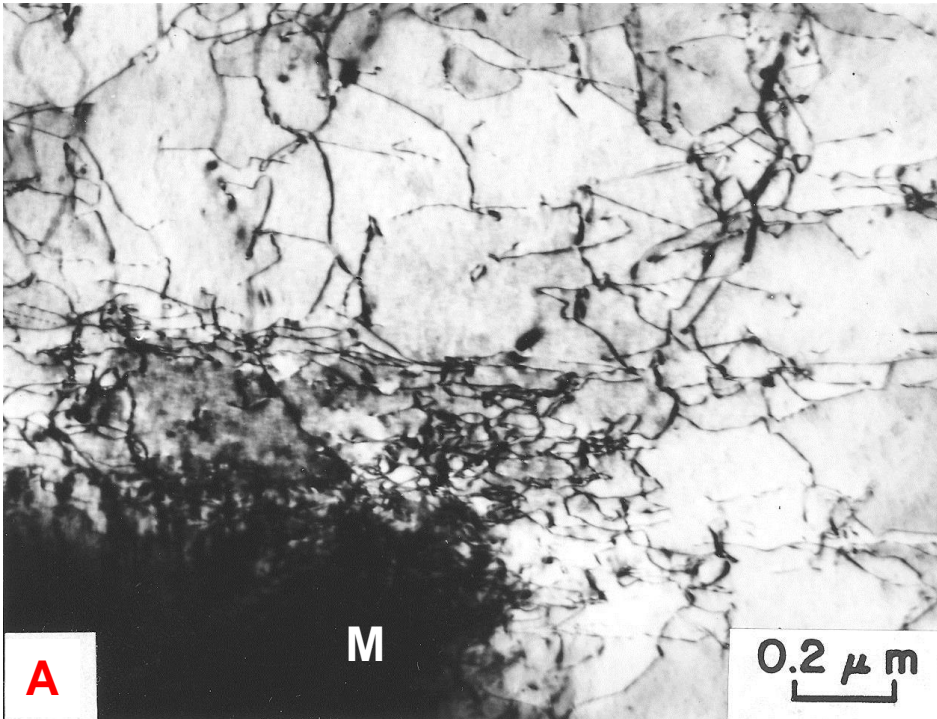
- **Nippon Steel**
 - **1975:** S. Hayami and T. Furukawa, Microalloying '75
- **GM**
 - **1976:** M.S. Rashid, SAE + others
- **Ford**
 - **1978:** R.G. Davies, Met. Trans. + others



Strain Accumulation in Ferrite



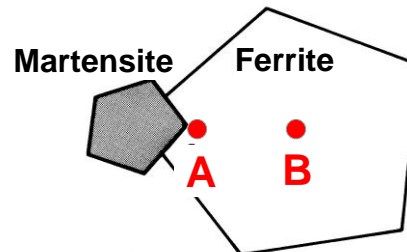
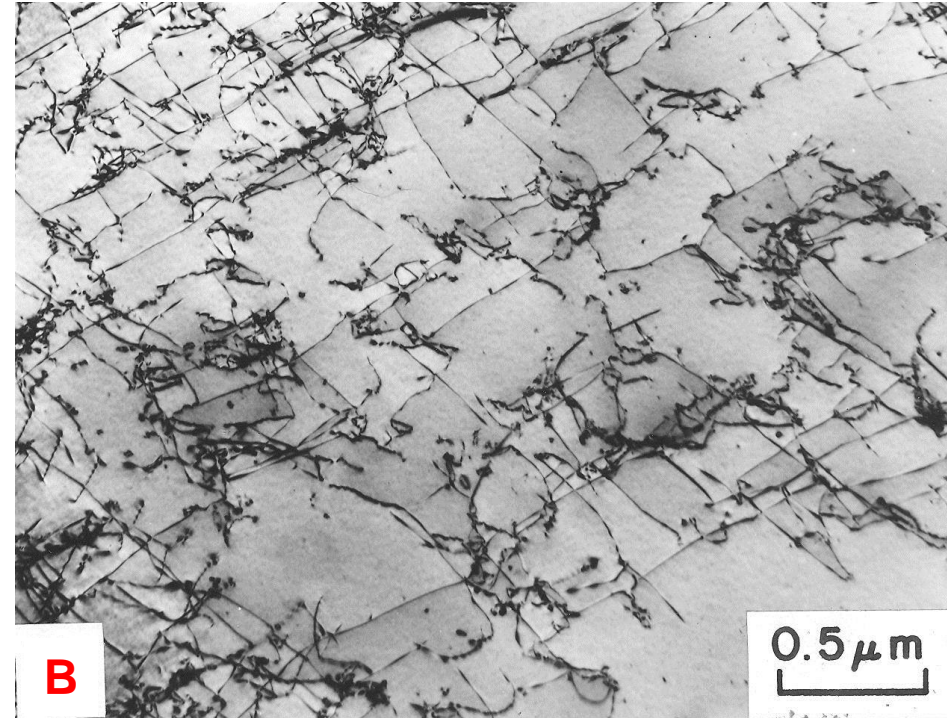
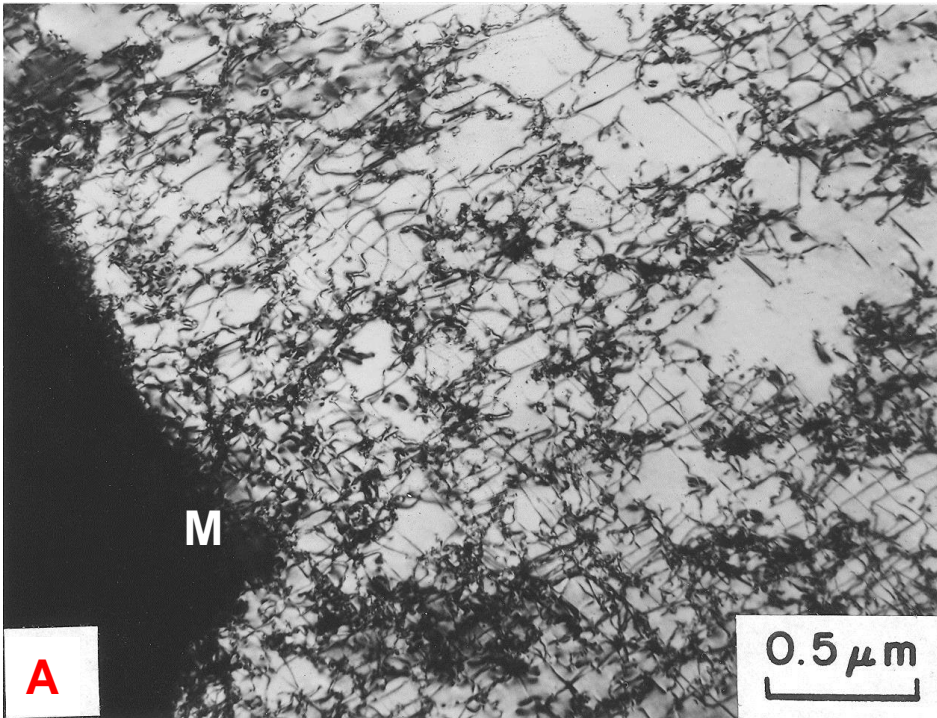
- C-Mn-Si DP Steel
- As heat treated



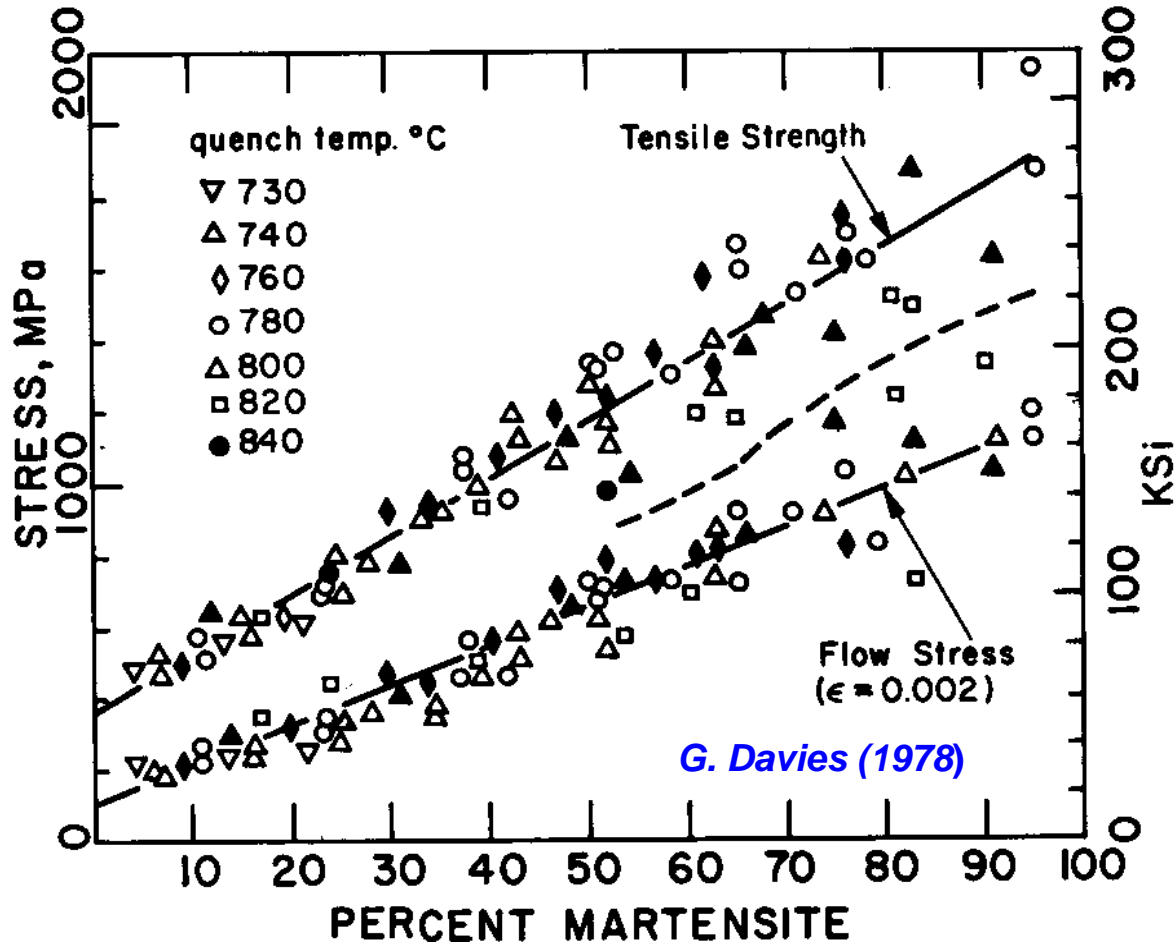
Strain Accumulation in Ferrite



- C-Mn-Si DP Steel
- 2 % Tensile Strain

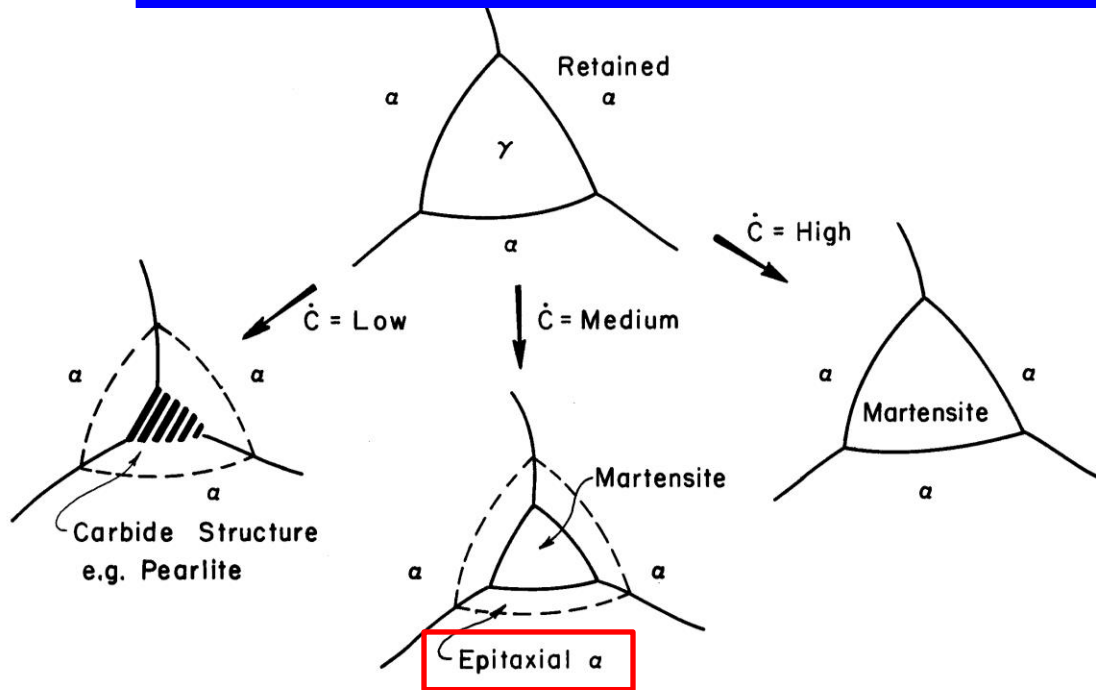


Strengthening in DP Steels

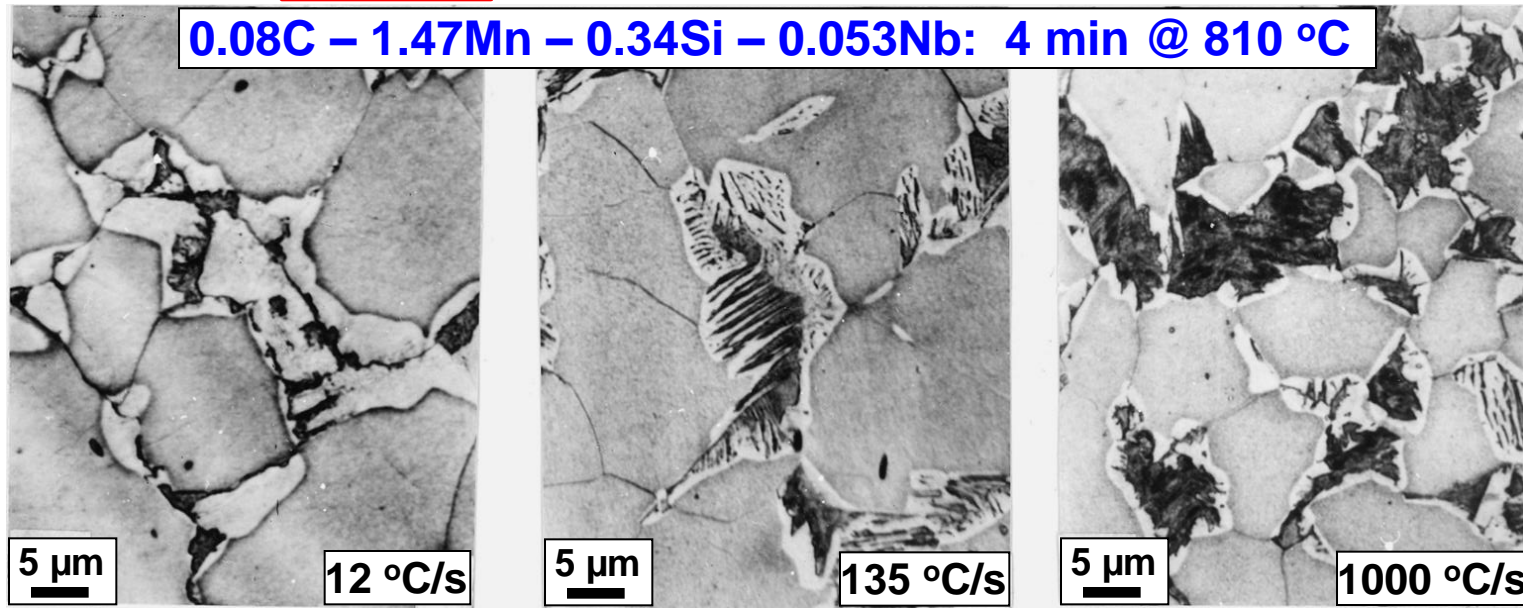


Strength increase follows rule of mixtures for composites: $\sigma_T = V_f \sigma_f + V_M \sigma_M$

Austenite Transformation in DP Steels

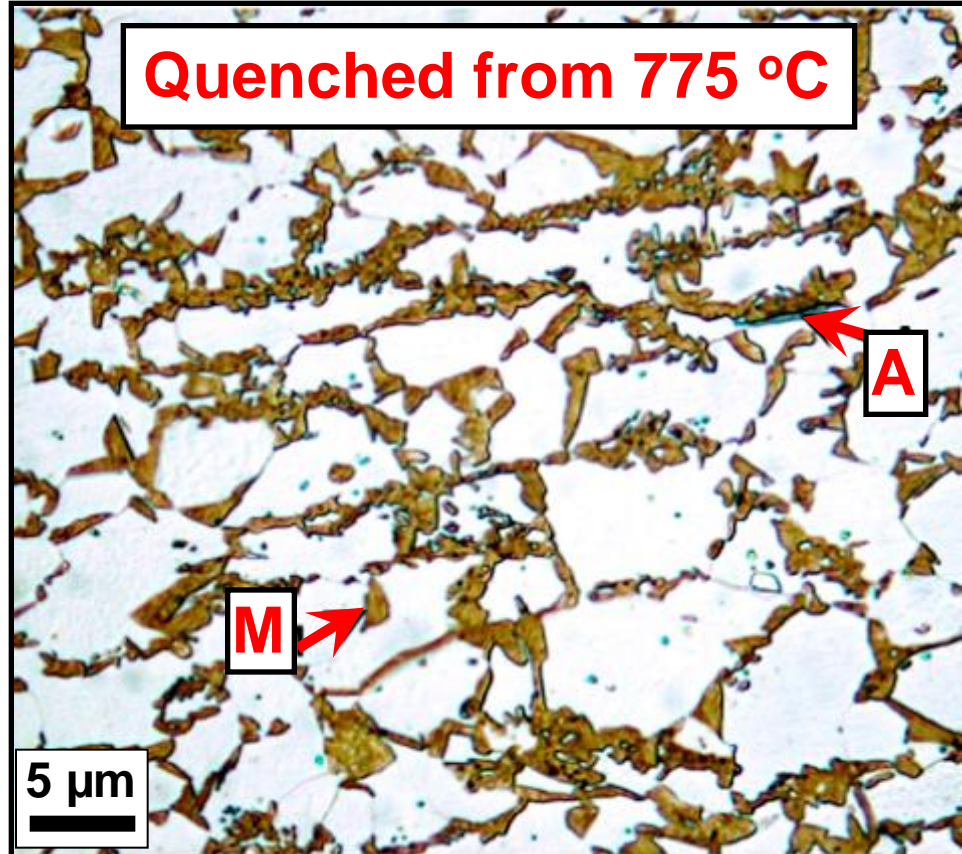
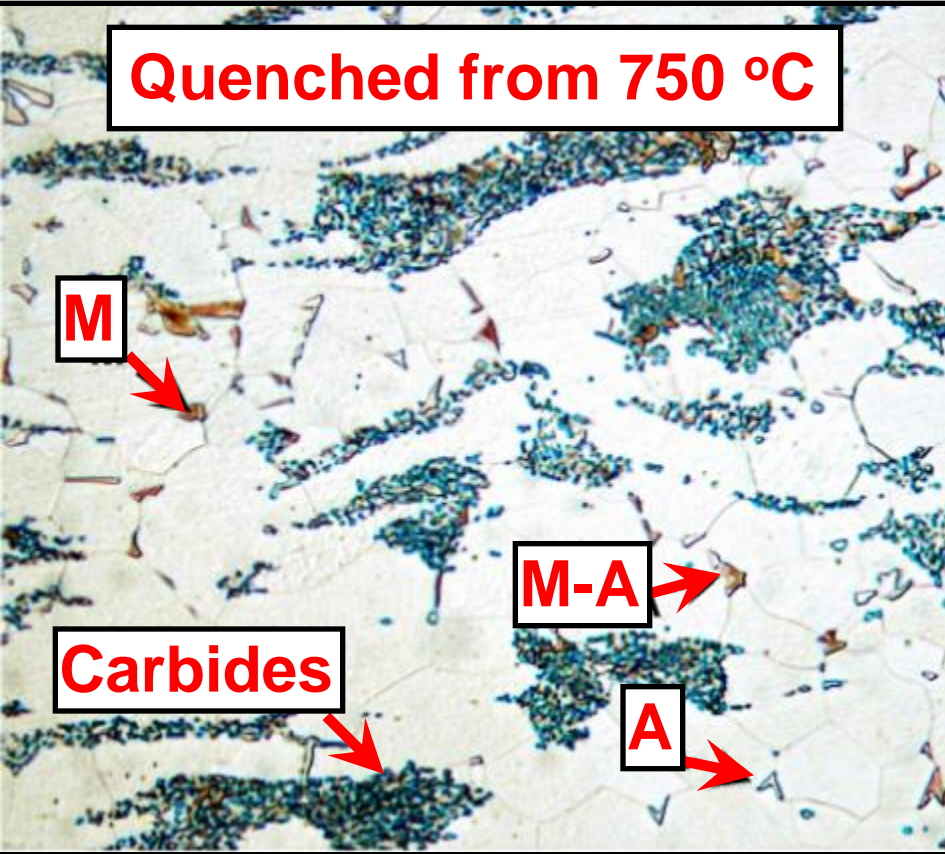


*R.D. Lawson, D.K. Matlock,
and G. Krauss, "An Etching
Technique for Microalloyed
Dual Phase Steels,"
Metallography, Vol. 13, 1980,
pp. 71-87.*



DP Microstructures.....

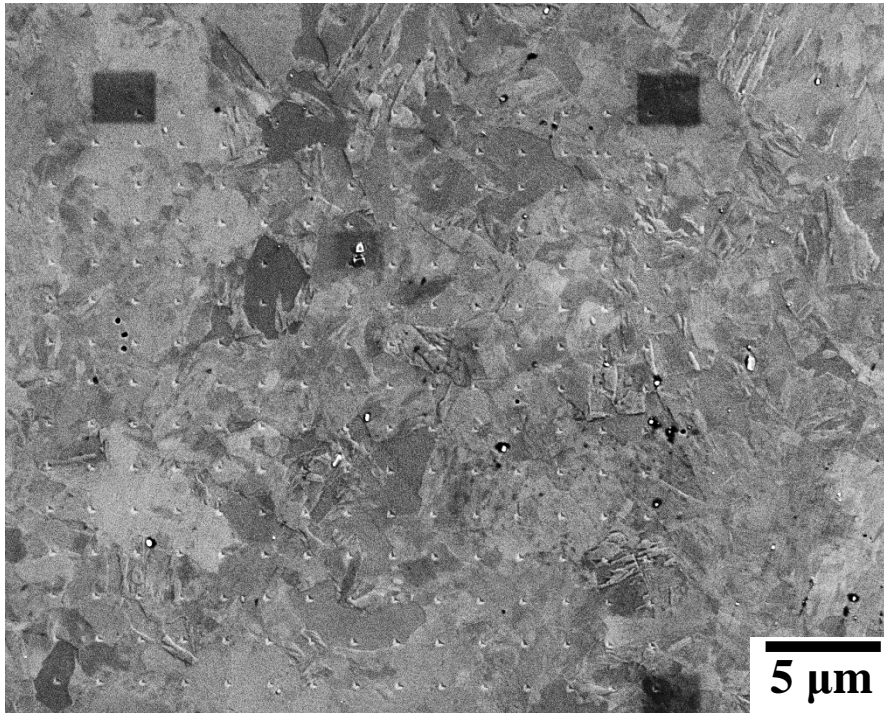
Special color tint etching: 0.15C – 1.5Mn – 1.5Si



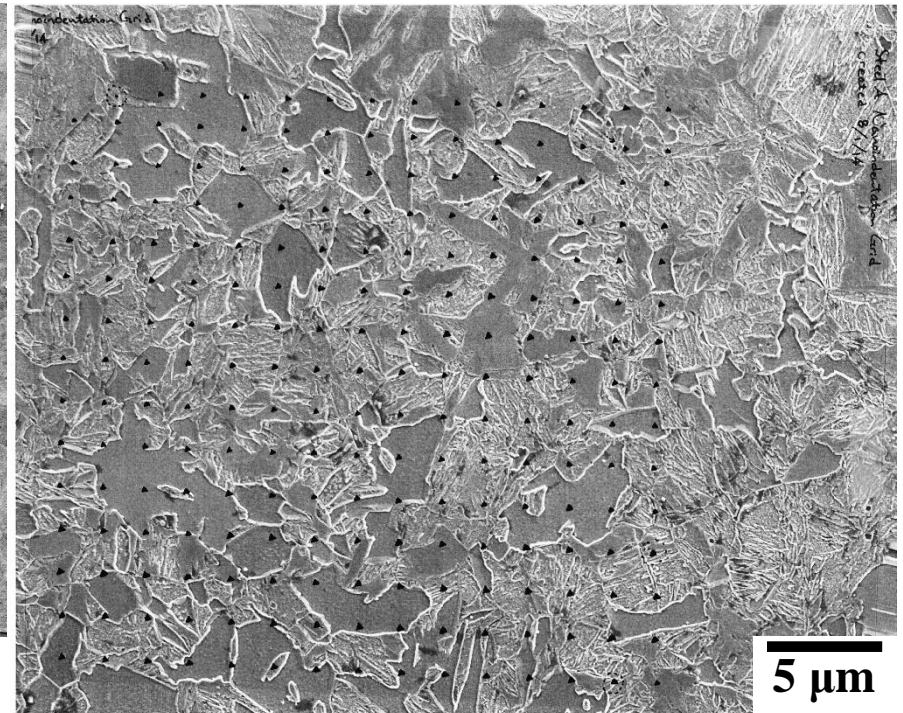
DP Steels = “More” than martensite and ferrite

Martensite and Ferrite Properties

- **Nanoindentation**
- **DP Steel: 0.14 C, 2.04 Mn – cold rolled and heat treated**
- **YS = 920 MPa; UTS = 1220 MPa**



SEM Micrograph: Unetched



SEM Micrograph: 2 pct nital etch

**Black reference boxes = 4 minutes of SEM beam raster
View = normal to rolling plane**

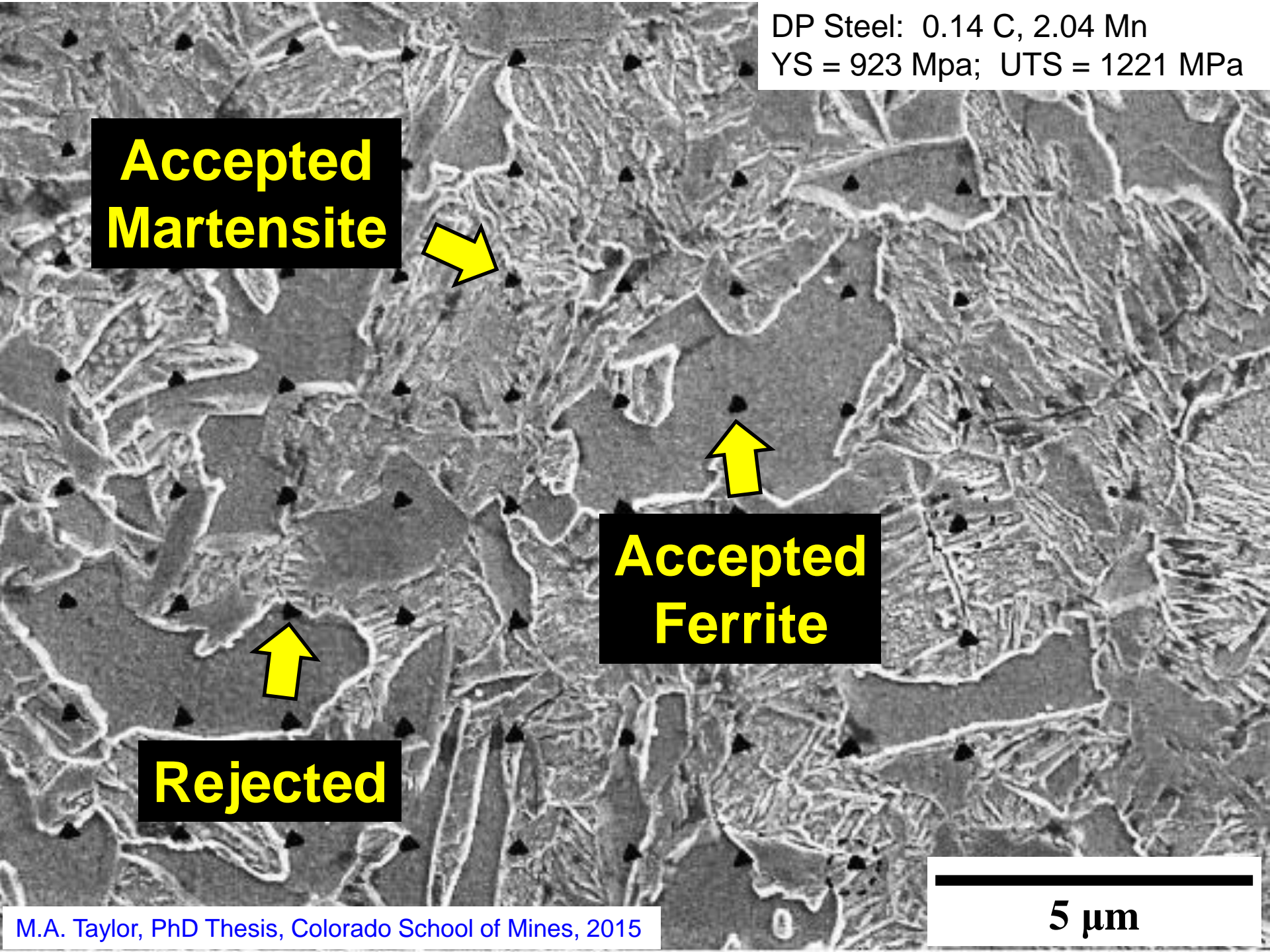
DP Steel: 0.14 C, 2.04 Mn
YS = 923 Mpa; UTS = 1221 MPa

**Accepted
Martensite**

**Accepted
Ferrite**

Rejected

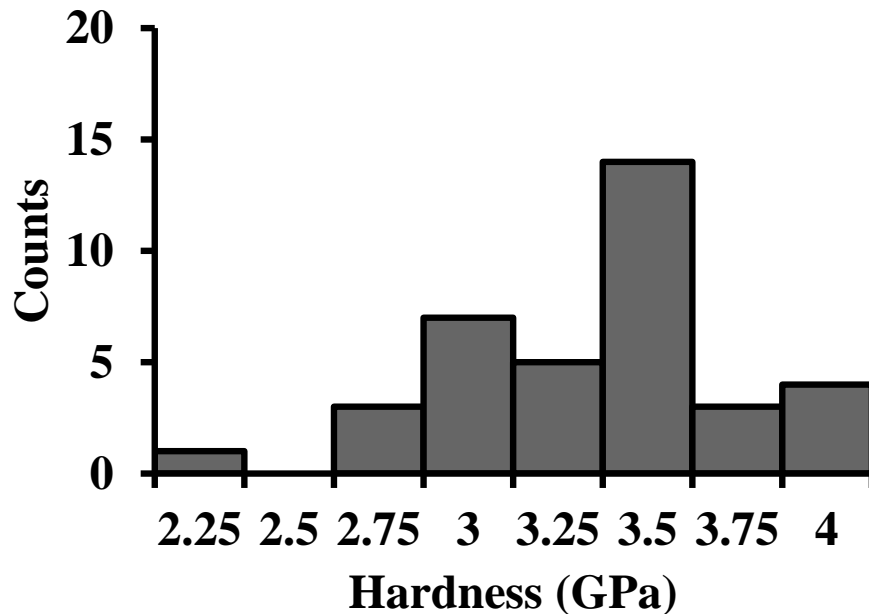
5 μm



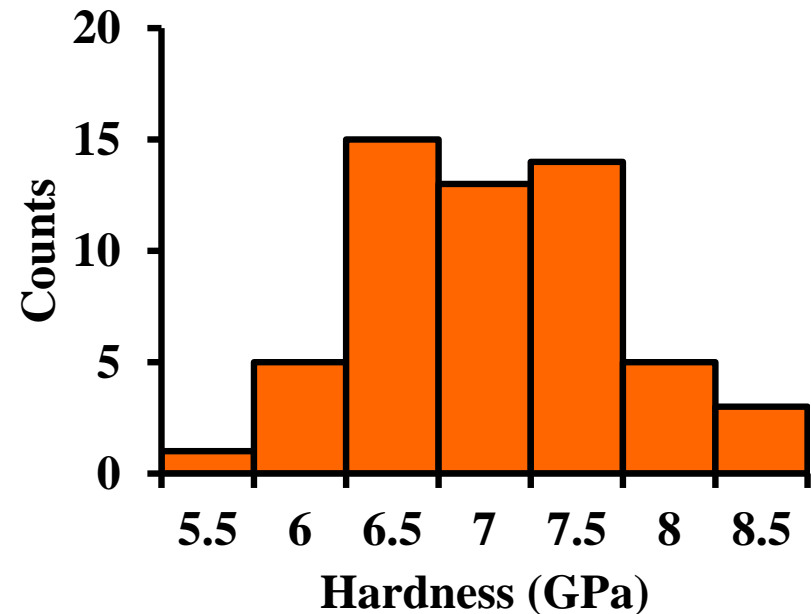
Martensite and Ferrite Properties

- **Nanoindentation**
- **DP Steel: 0.14 C, 2.04 Mn – cold rolled and heat treated**
- **YS = 920 MPa; UTS = 1220 MPa**

Ferrite: Avg = 3.2 GPa



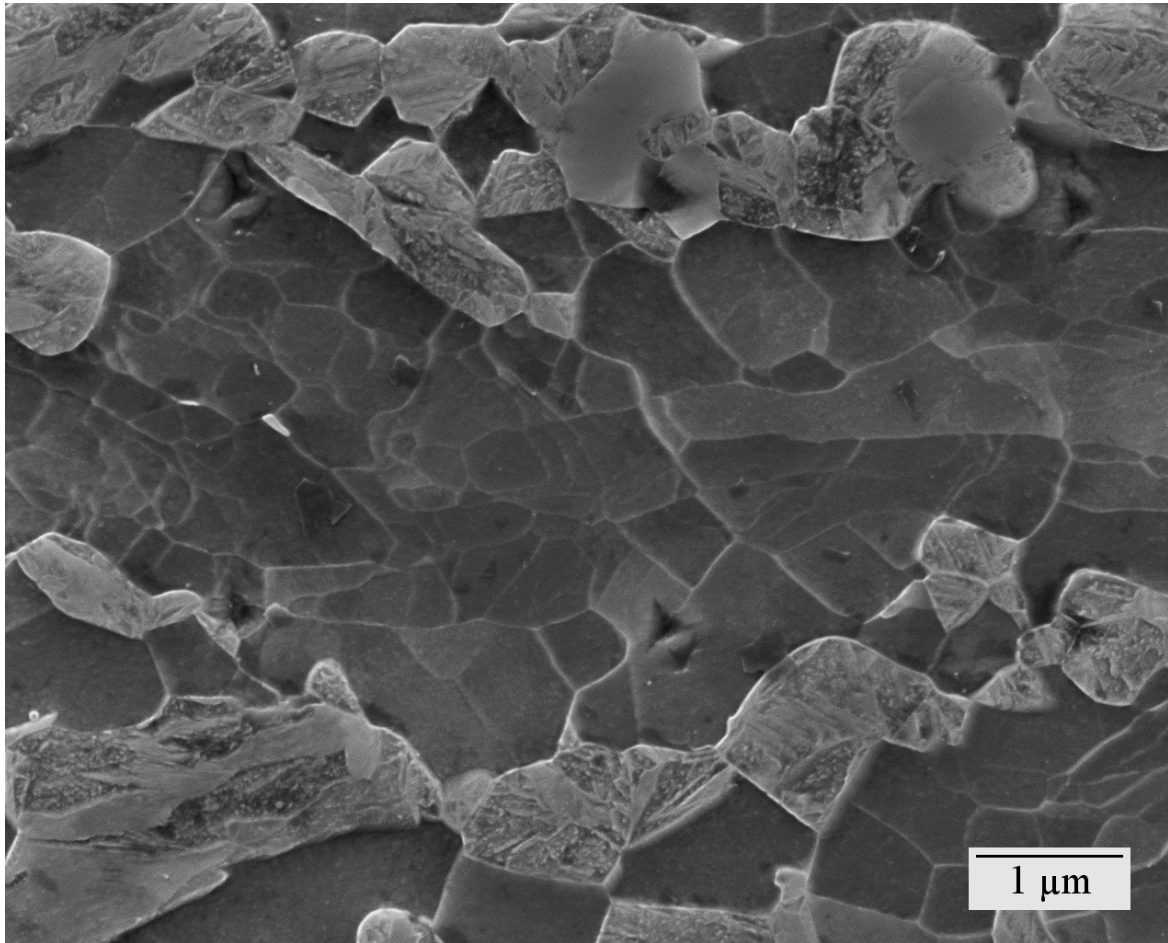
Martensite: Avg = 7.3 GPa



Data approximate a normal distribution

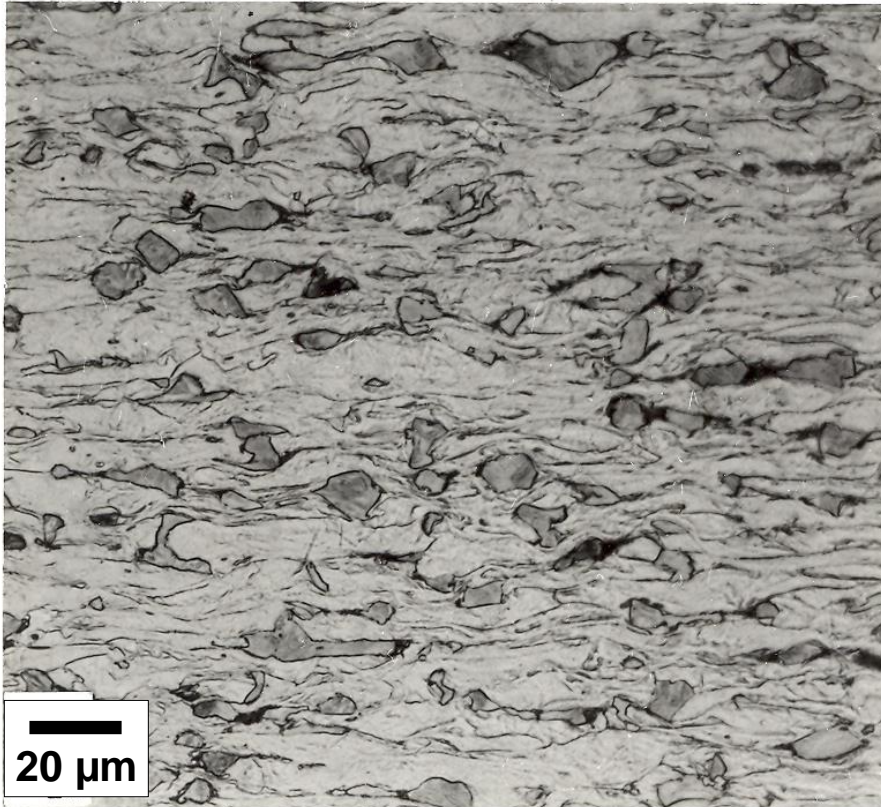
Why Hardness Variability?

Influenced by the mixture of recovered (in example) and recrystallized ferrite in the samples

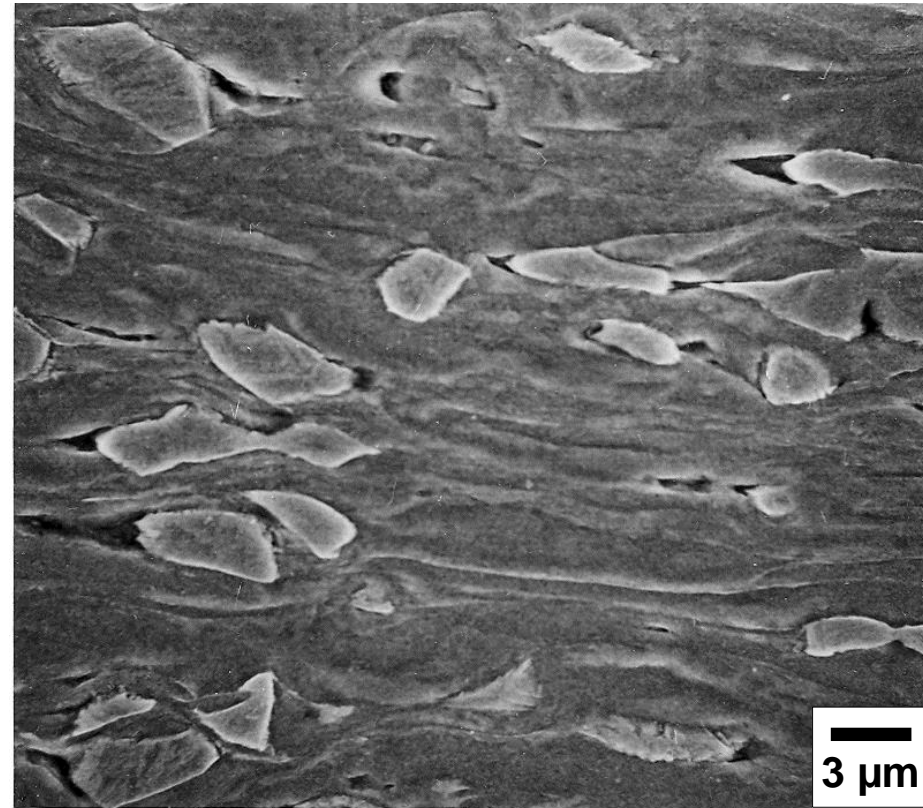


Consequence of Hardness Differences

- 1008 steel heat treated to DP microstructure
- Cold drawn to wire – true strain = 1.3



Light Optical Micrograph



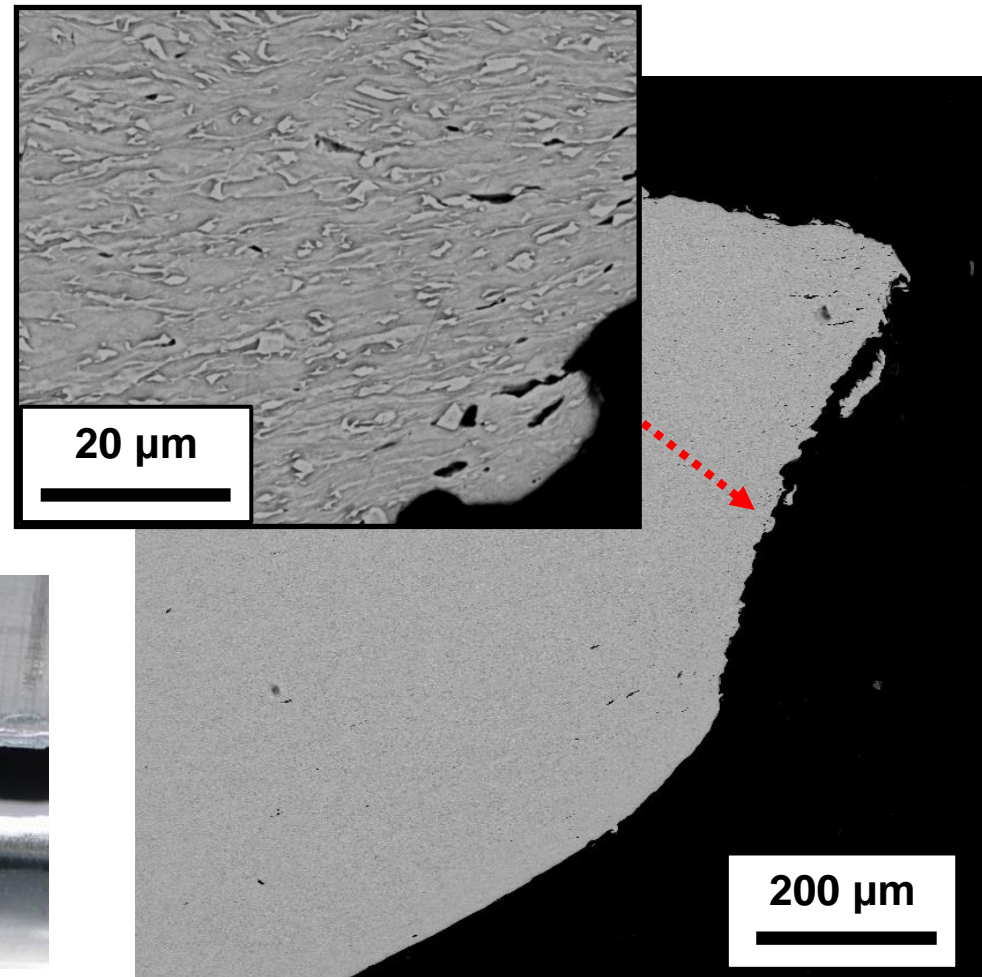
SEM Micrograph

Dual-Phase Processing:
30 min @ 760 °C + WQ
25 vol % Martensite

2 pct nital etch

Example Failures: Formability Limited by Fracture

DP Steels

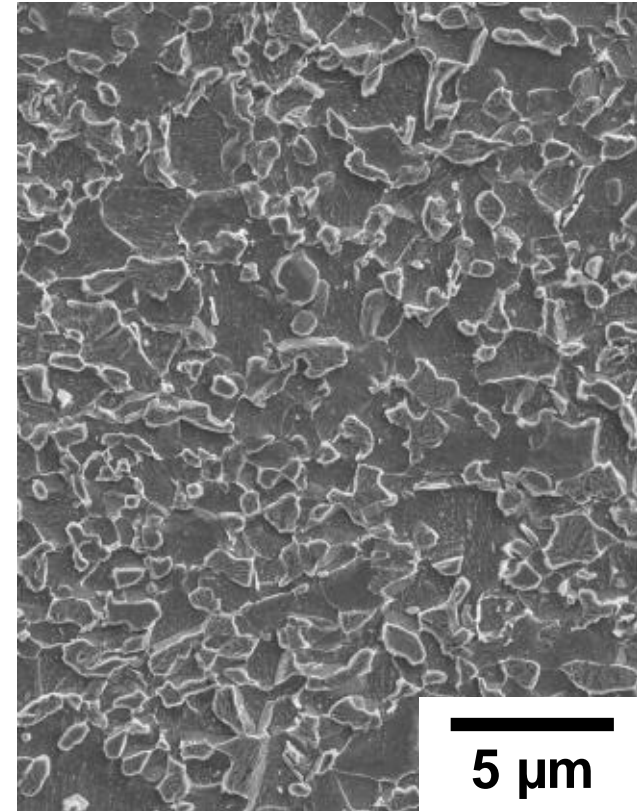
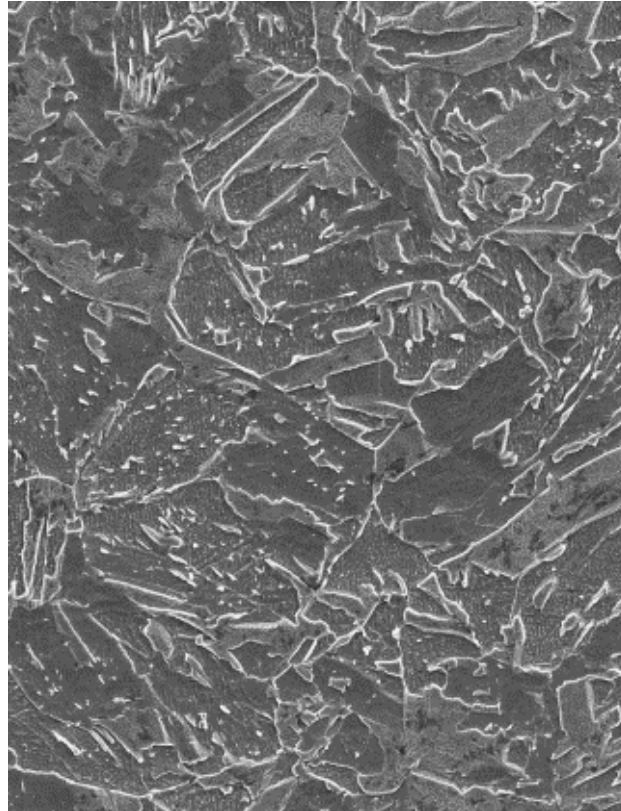
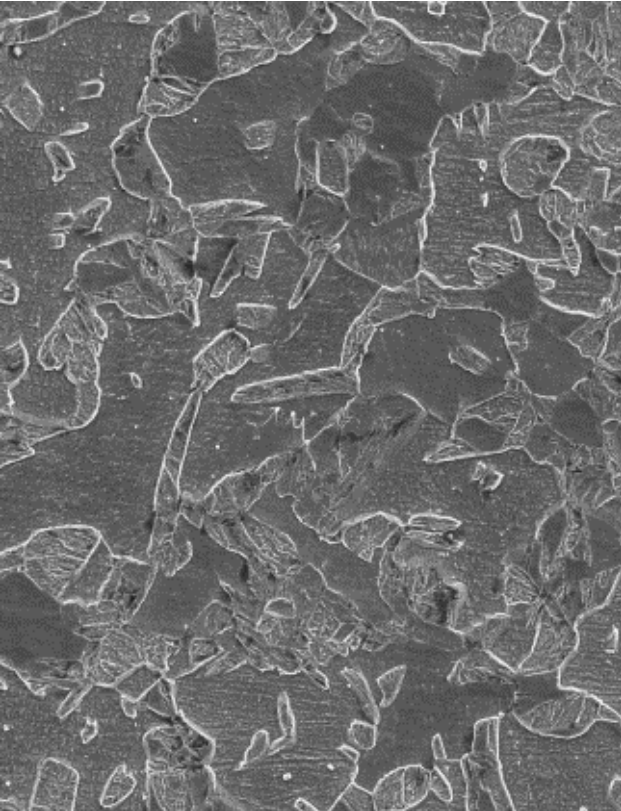


Fractures often referred to as “Shear Fractures”

Commercially-Produced DP980 Steels

SEM Micrographs; Secondary Electron Images

2 pct nital etch



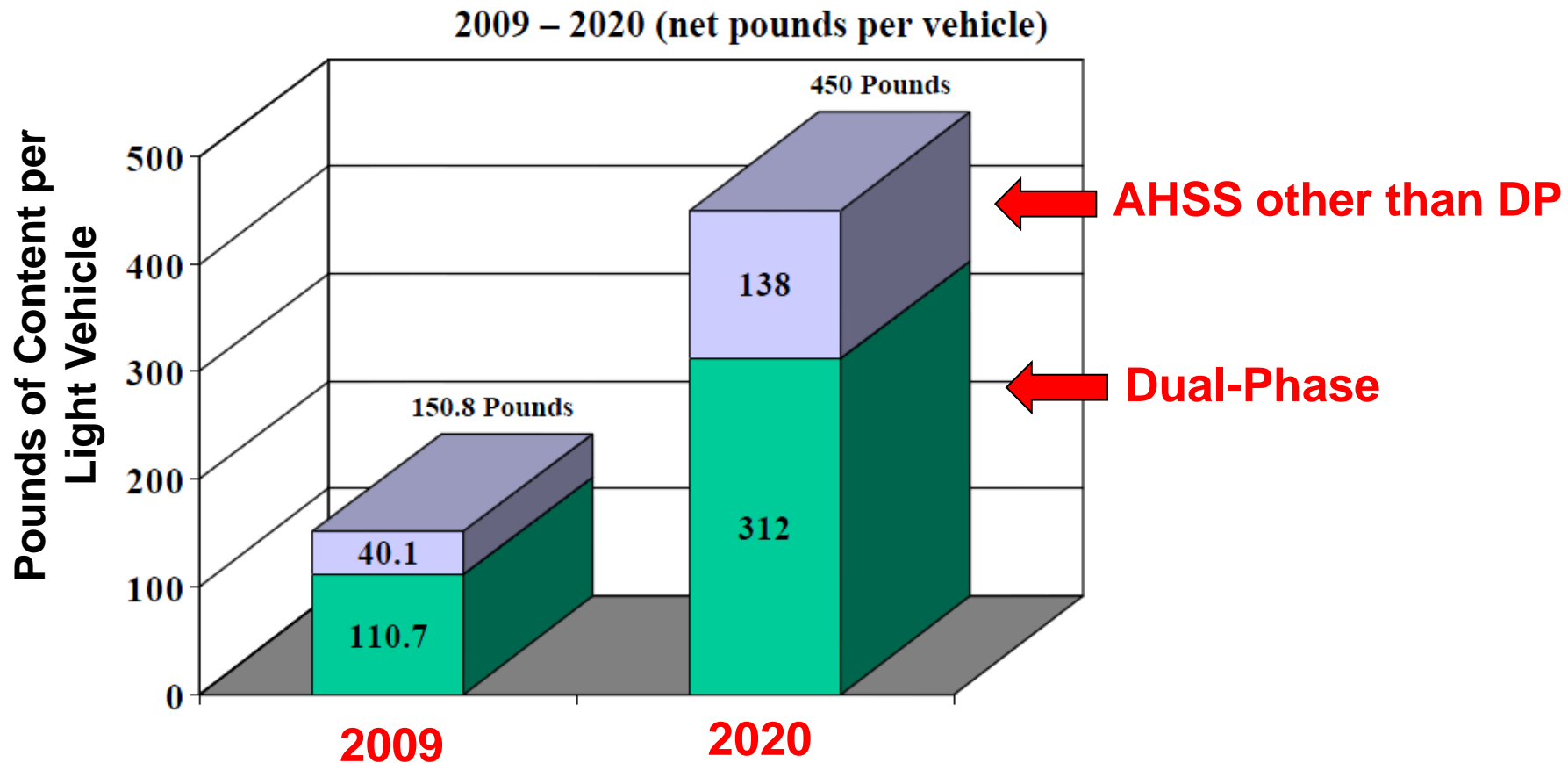
Steel A:
0.09 C, 2.13 Mn, 0.57 Si
0.02 Cr, 0.07 Mo

Steel D:
0.12 C, 2.47 Mn, 0.03 Si
0.25 Cr, 0.36 Mo

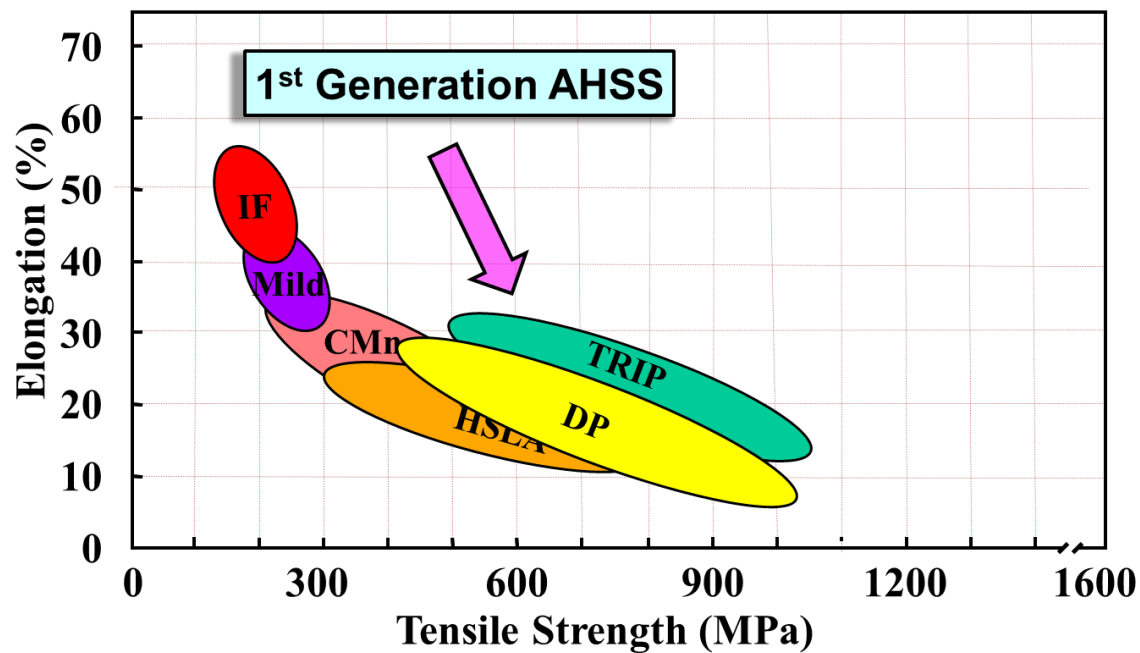
Steel H:
0.15 C, 1.93 Mn, 0.64 Si
0.32 Cr, 0.01 Mo

Trends: AHSS use in North America

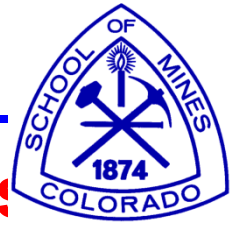
- **Dual-phase steels, AHSS of choice**



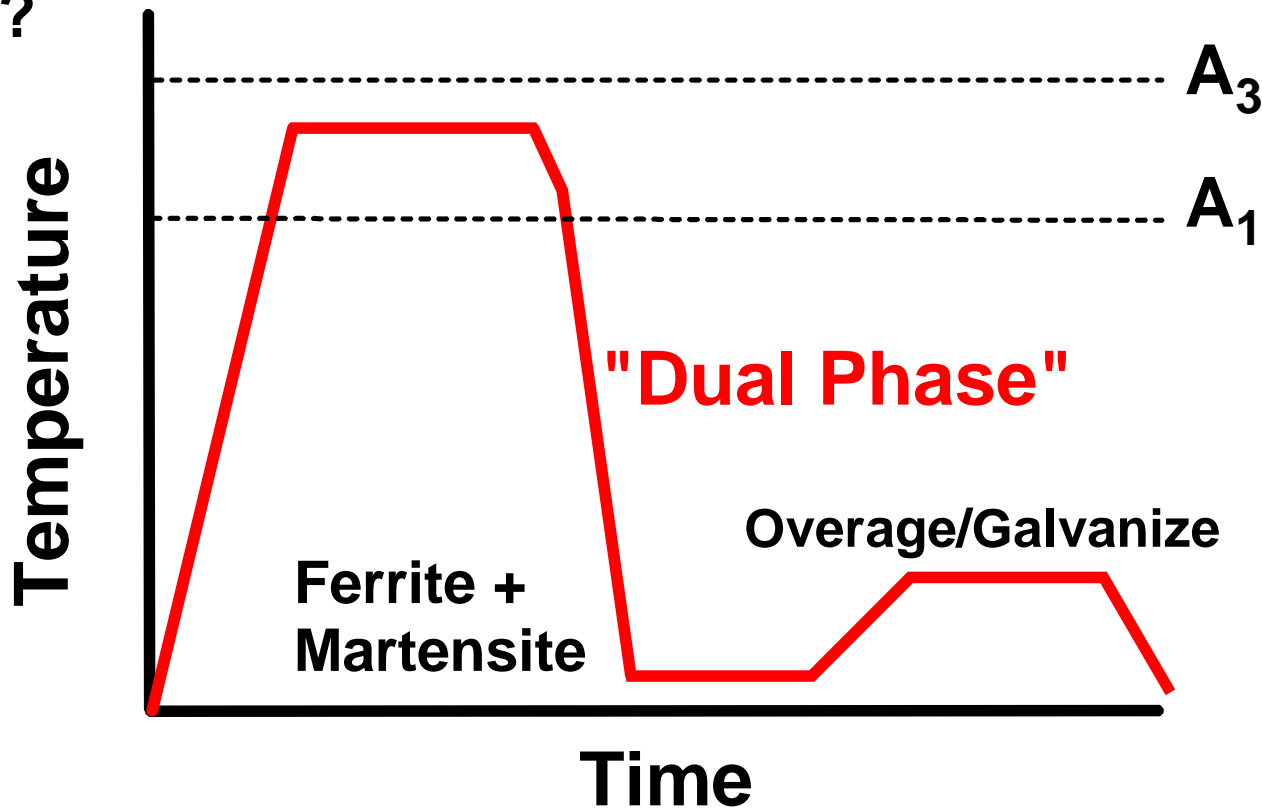
Fundamentals of TRIP (TRansformation Induced Plasticity Steels)



DP Steel Processing



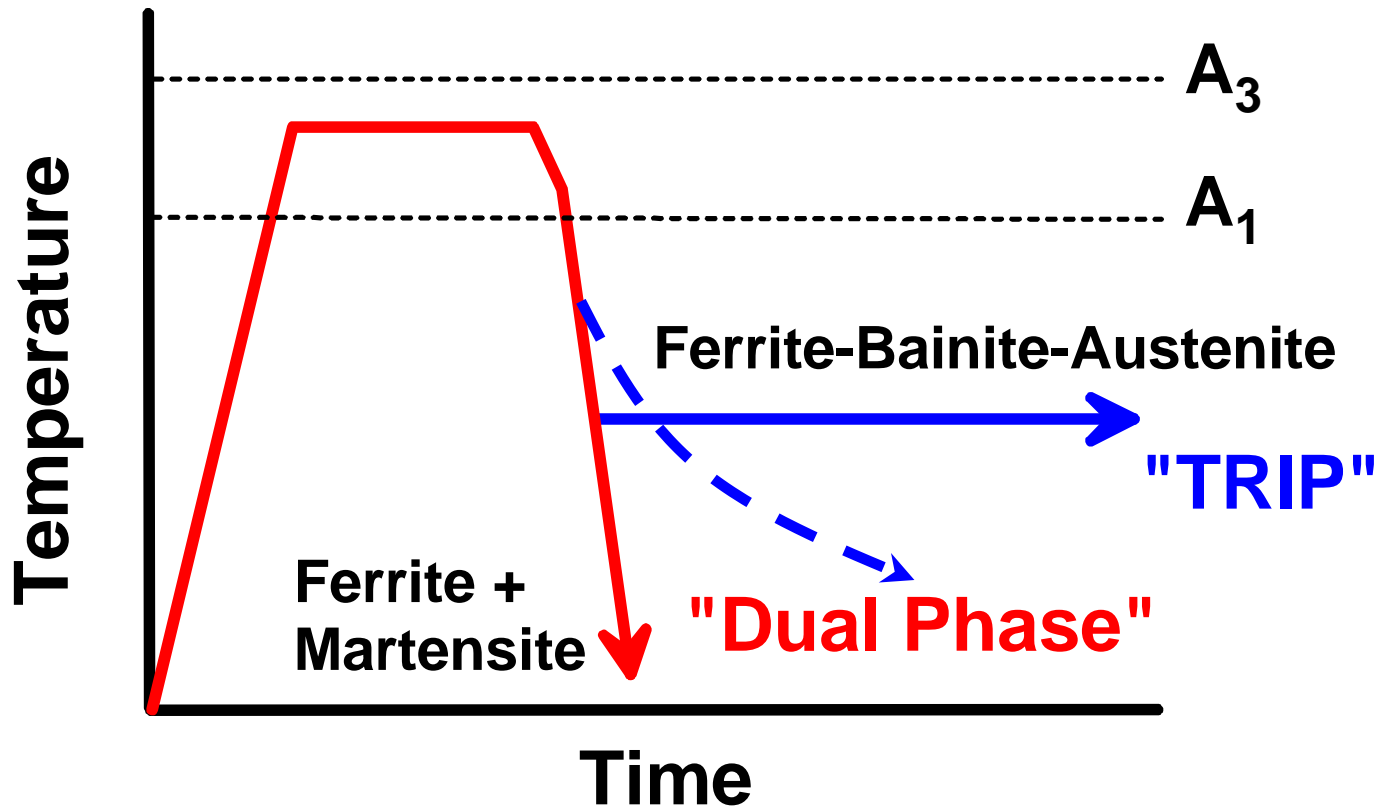
- Initially conceived based on “simple” routes for hot and cold rolled steels
 - Microstructures more complex than simply ferrite + martensite and contained retained austenite + ??



TRIP Steel Processing



- Isothermally transform or control cool
- Austenite in high strength matrix (e.g. fine grain ferrite, martensite, bainite, ...)

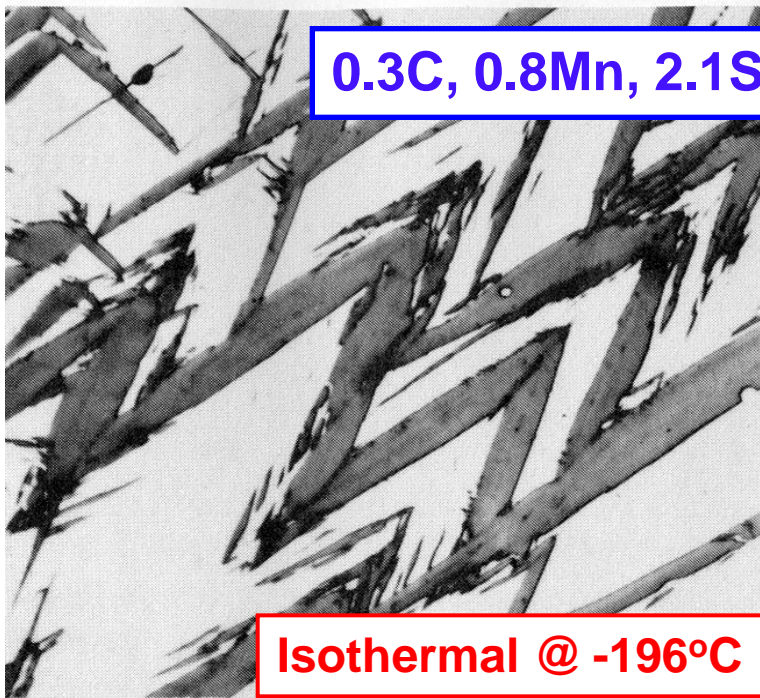
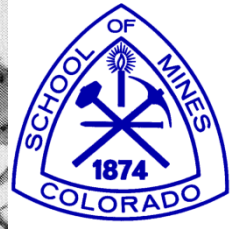


The “TRIP EFFECT”

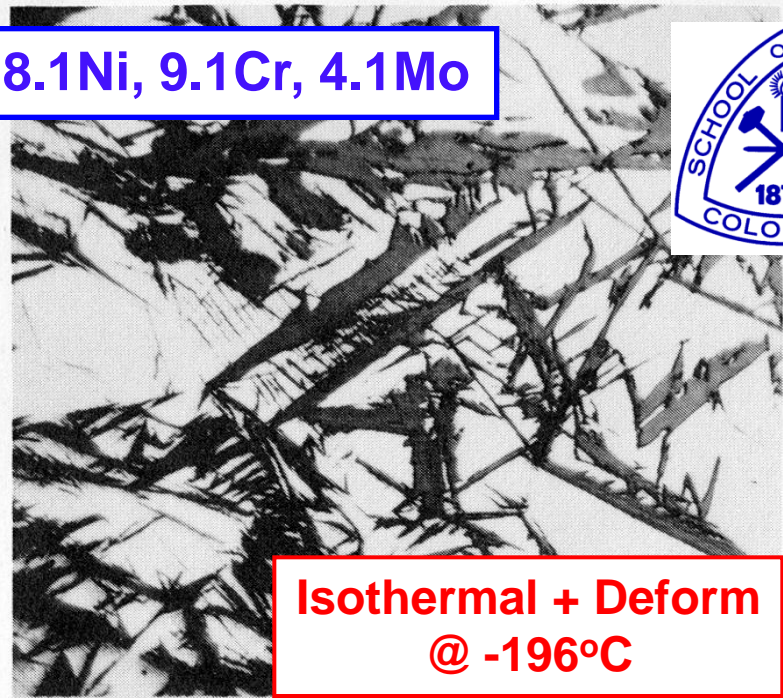


- **“Stress-Assisted”**
 - Heterogeneous martensite nucleation on the same sites responsible for transformation on cooling but assisted by stress – (*e.g. at prior austenite grain boundaries; lattice defects...*)
- **“Strain-Assisted” or “Strain-Induced”**
 - Martensite nucleates on new sites created by plastic deformation -- (*e.g. at slip band intersections*)
- **Important consequences of the “TRIP Effect:”**
 - Volume expansion: austenite to martensite
 - Strength of martensite > austenite

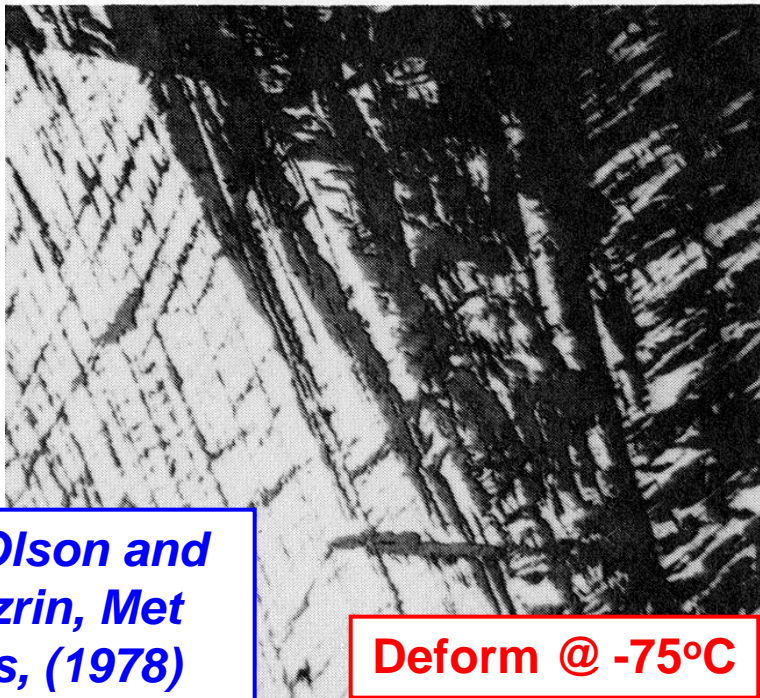
0.3C, 0.8Mn, 2.1Si, 8.1Ni, 9.1Cr, 4.1Mo



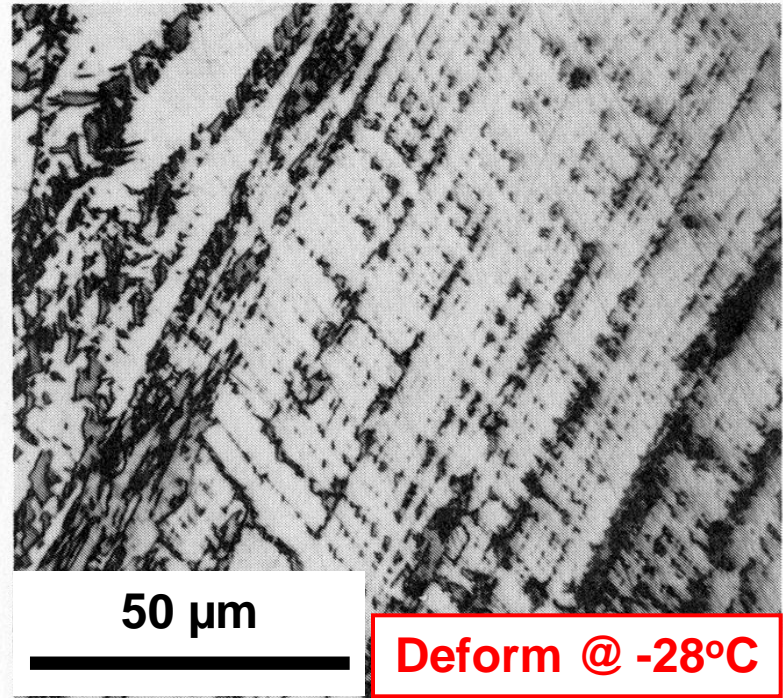
Isothermal @ -196°C



Isothermal + Deform @ -196°C



Deform @ -75°C



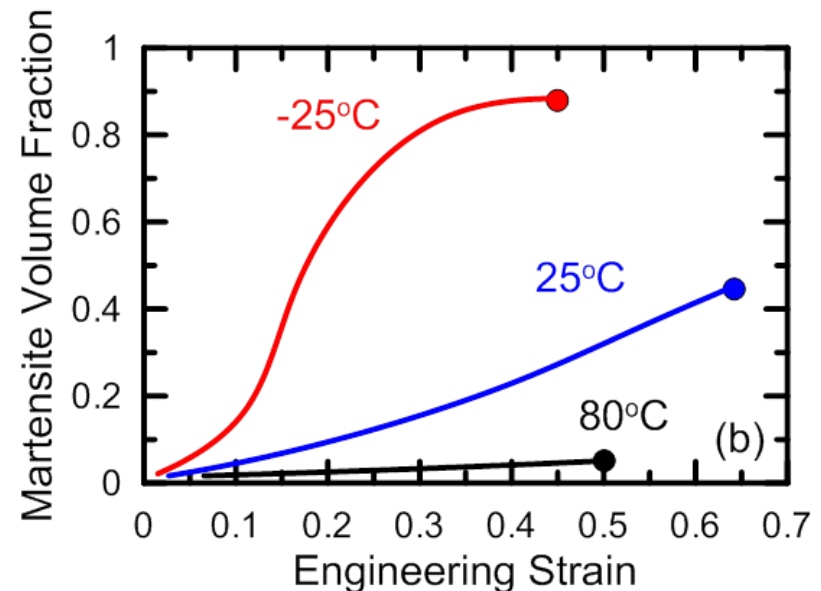
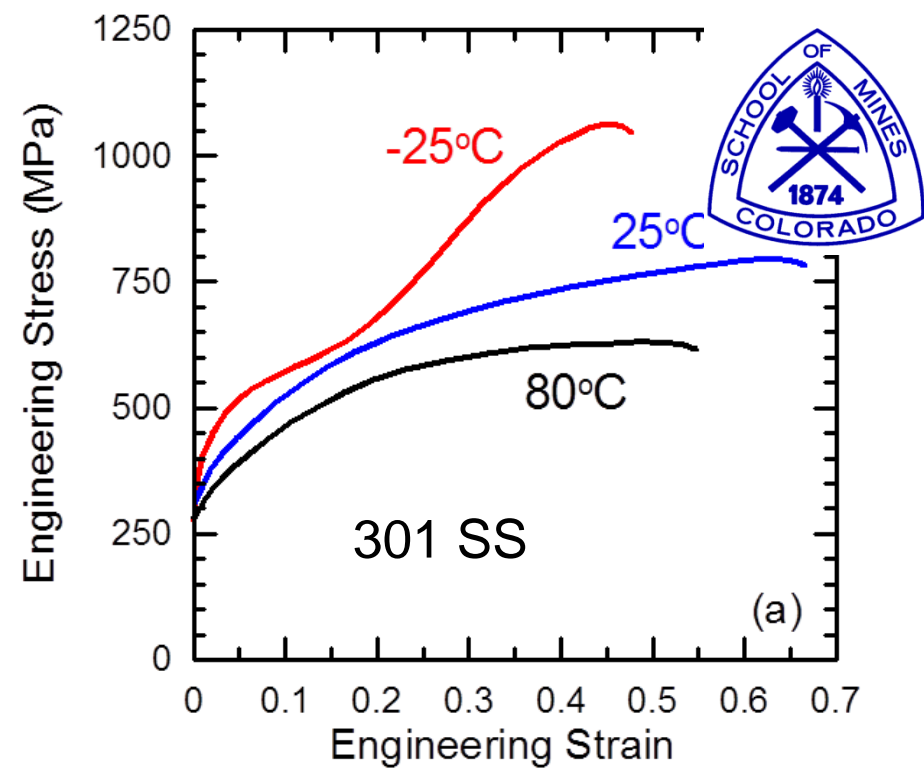
50 μm

Deform @ -28°C

G.B. Olson and M. Azrin, *Met Trans*, (1978)

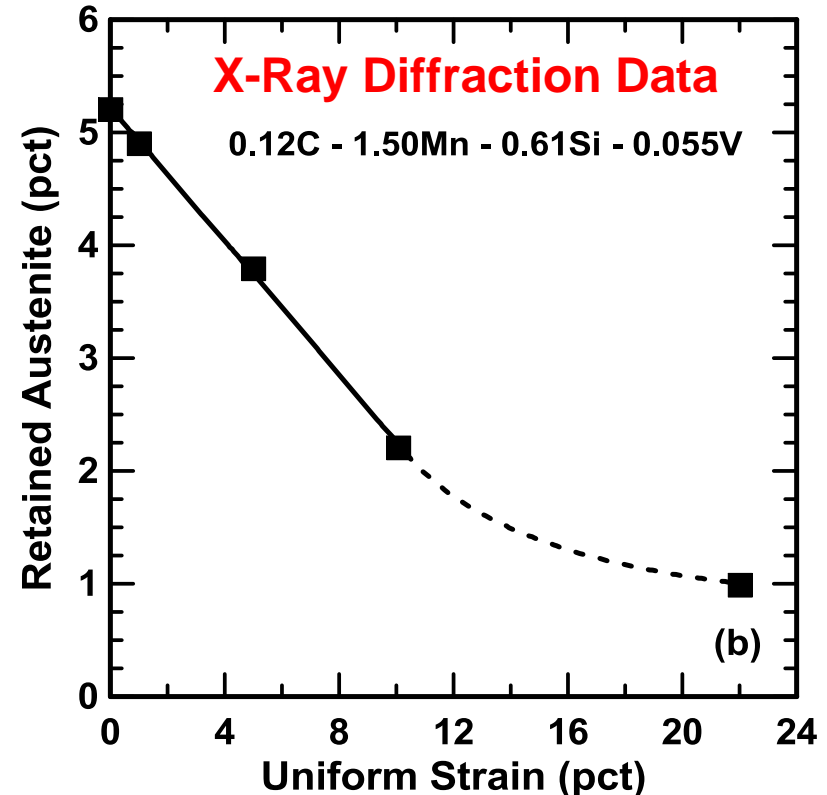
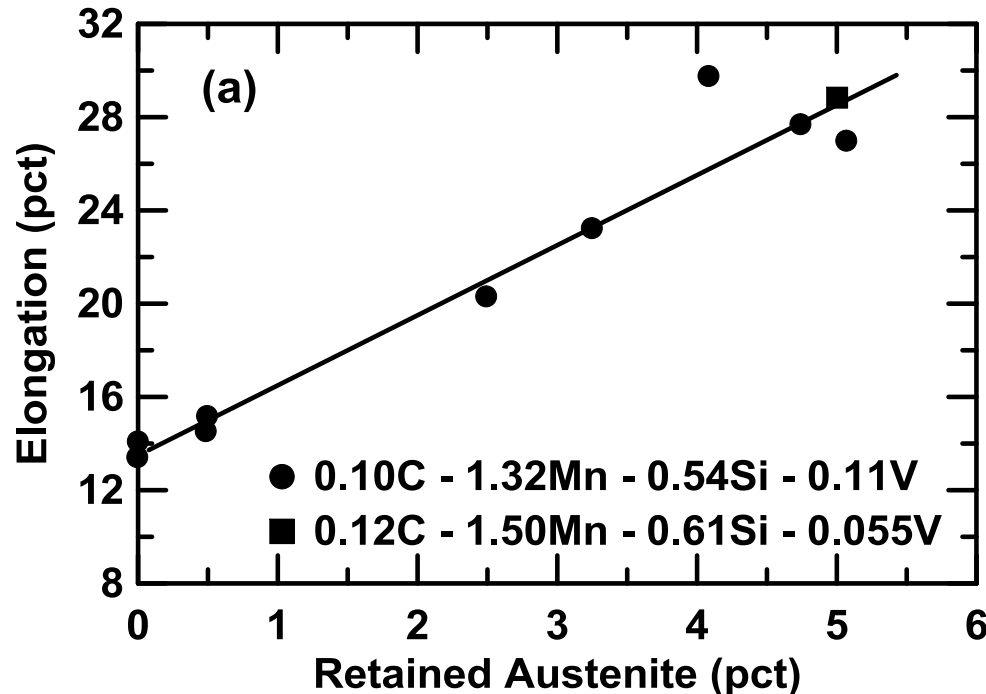
Strain-Assisted TRIP: Metastable Austenitic Stainless Steel

- **301 Stainless Steel**
- **0.096C-1.85Mn-17.33Cr-6.66Ni**
- **Isothermal tensile tests**
- **MVF measurements based on x-ray diffraction and magnetic inductance**
- **Peak ductility at intermediate temperature**



...Lessons Learned from “Early” DP Steels

- Processed as dual-phase steel
- Observed microstructures more complex than ferrite + martensite



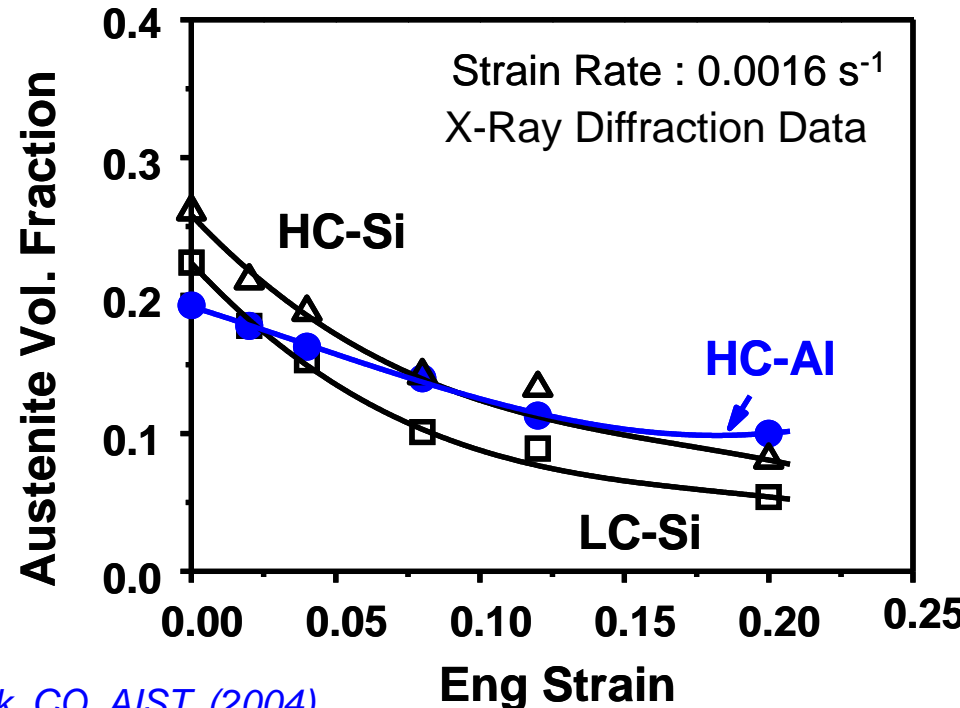
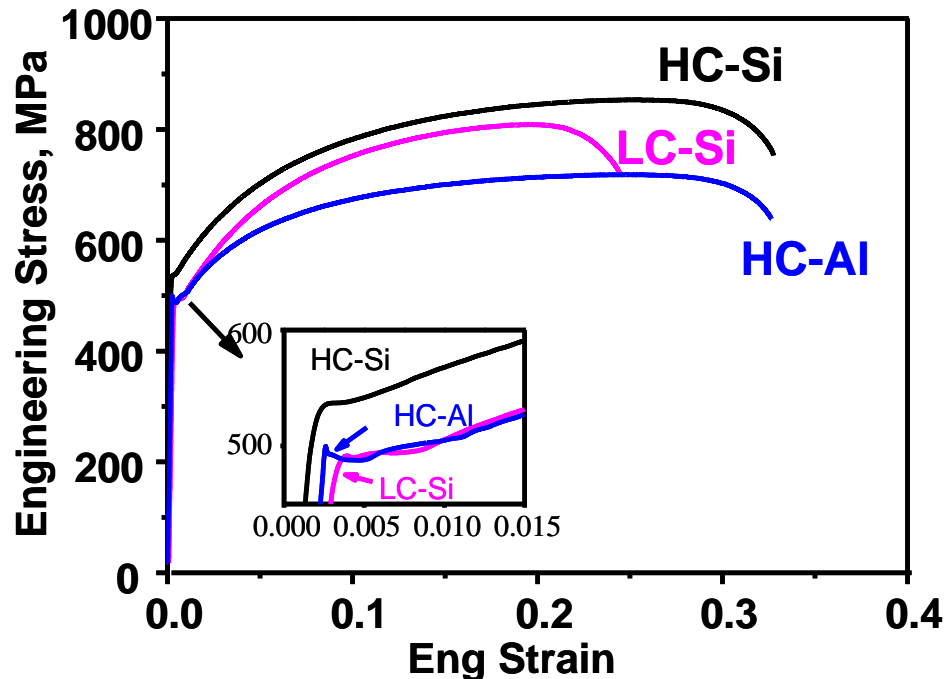
“...the ductility could be further improved by increasing the amount of retained austenite...” A. Marder (1977)

Austenite Stability: Alloying Effects

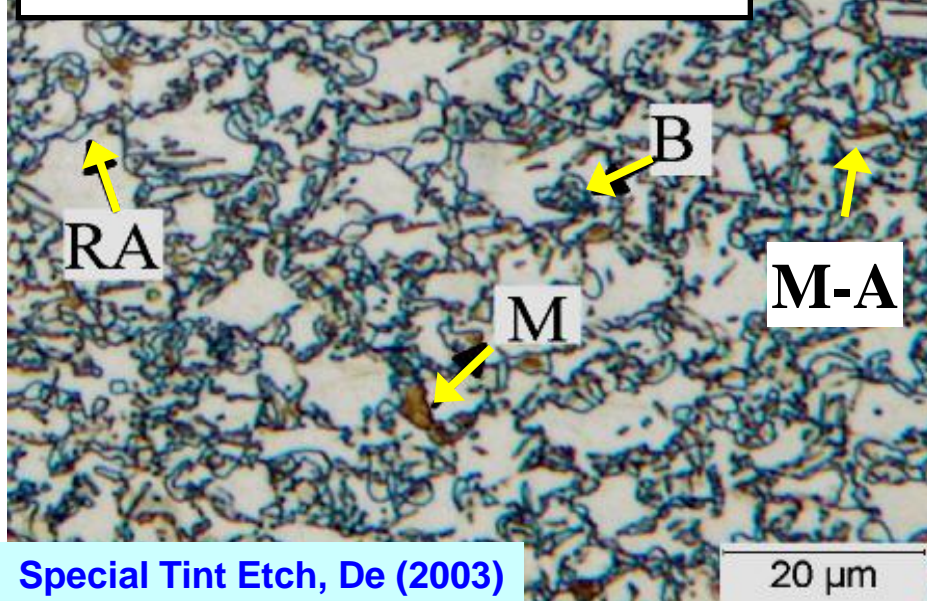
Steel	C	Mn	Si	Al
LC-Si	0.14	1.5	1.46	0.03
HC-Si	0.21	1.5	1.47	0.03
HC-Al	0.21	1.5	0.37	1.00

De, Kircher, Speer, and Matlock, AHSS Conf, Winter Park, CO, AIST, (2004)

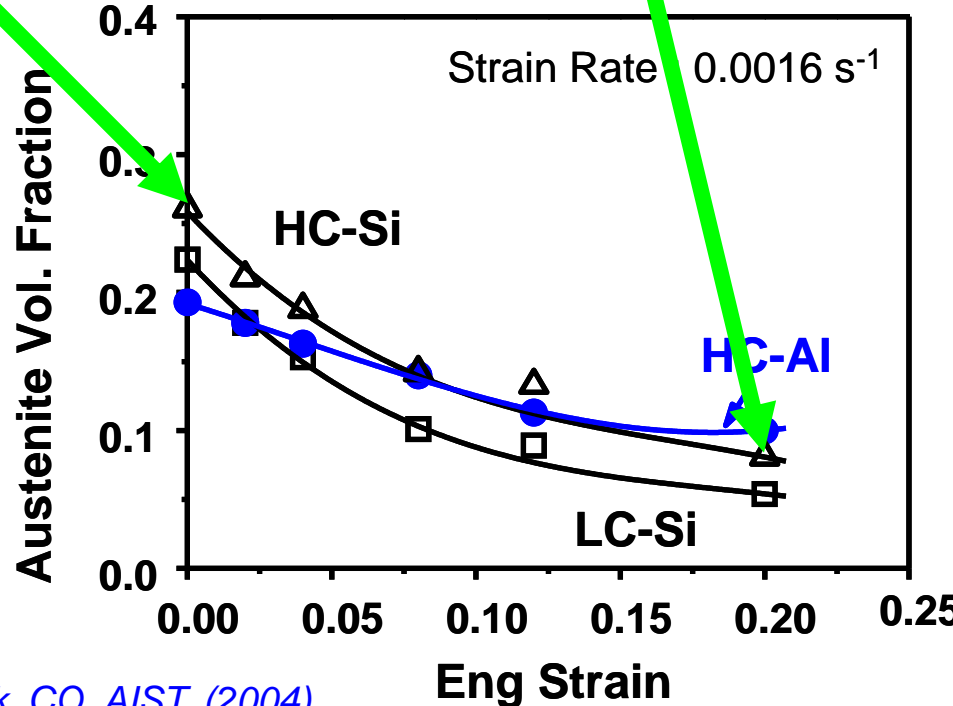
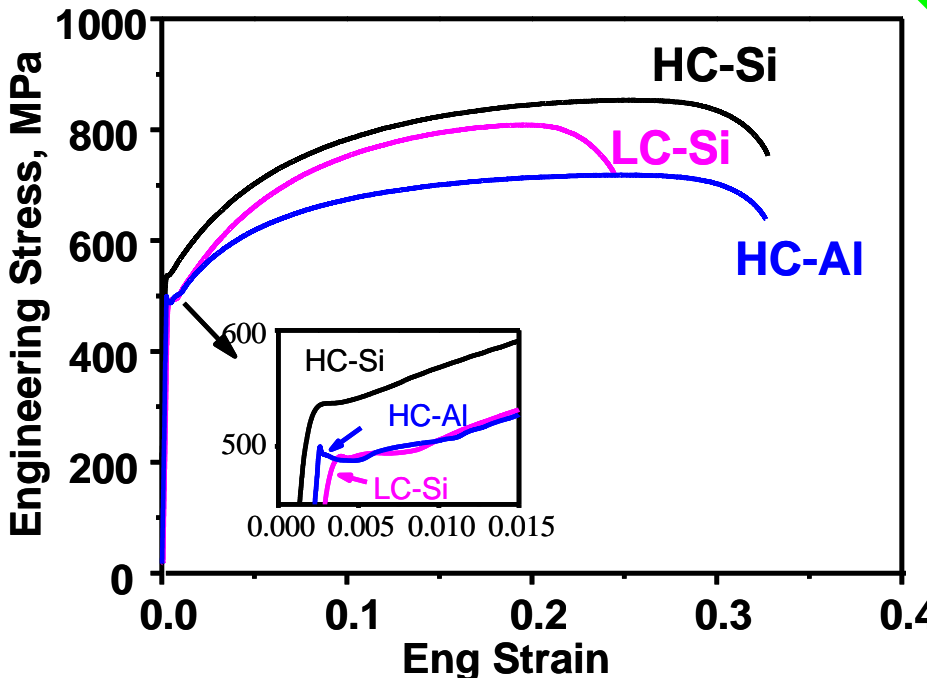
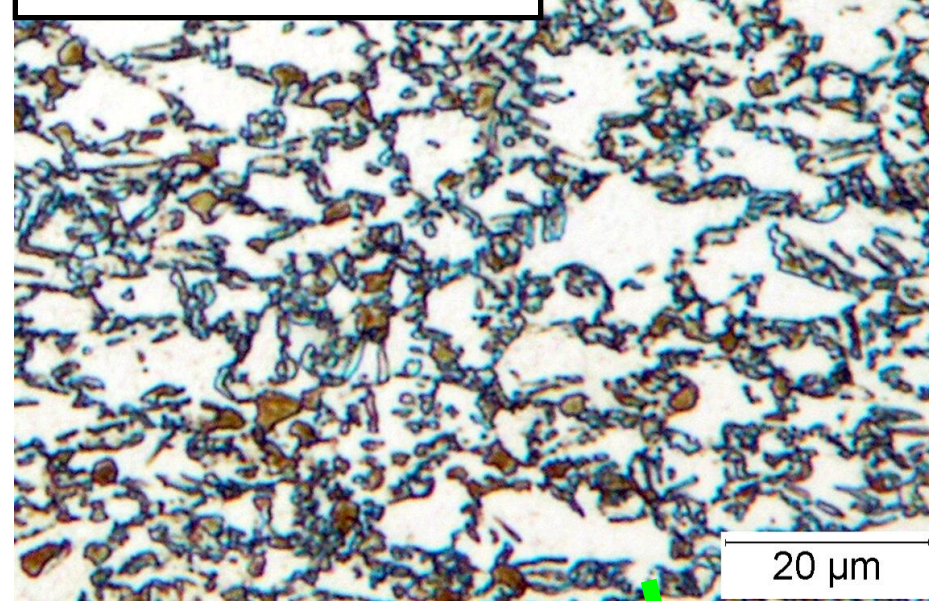
(760 °C - 6 min) + (420 °C - 5 min) + WQ



HC-Si: As Heat Treated



HC-Si: 0.2 strain



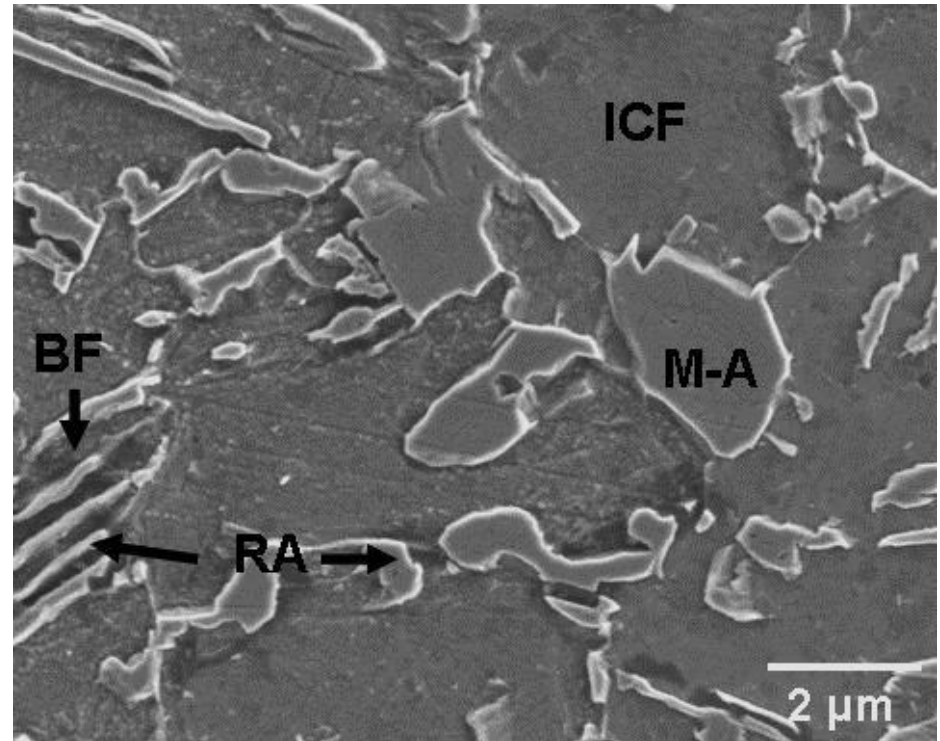
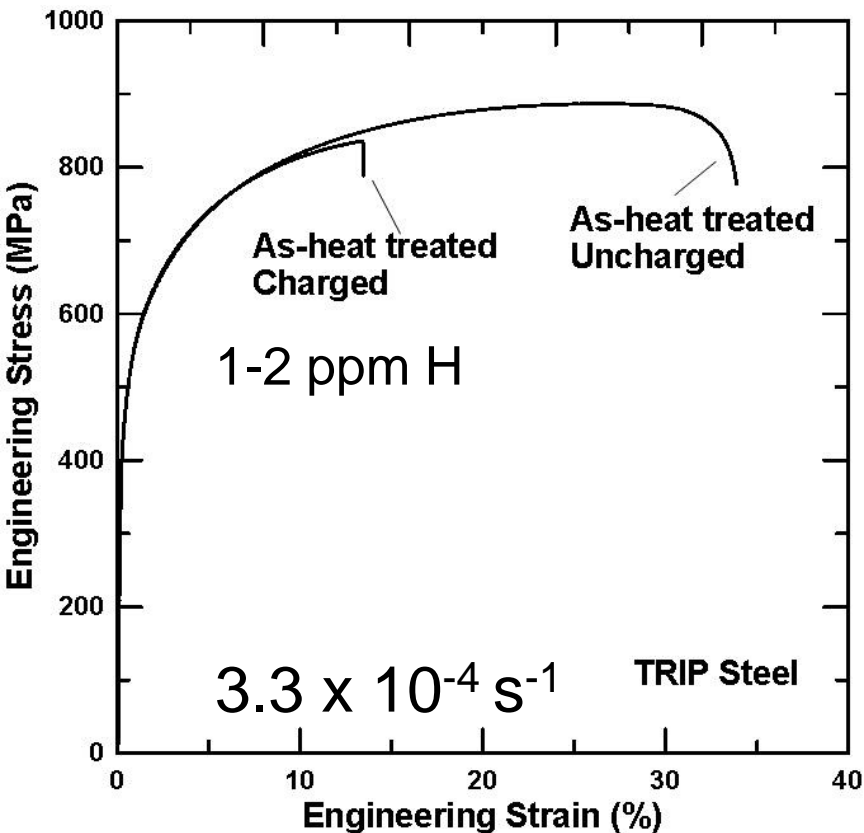
De, Kircher, Speer, and Matlock, AHSS Conf, Winter Park, CO, AIST, (2004)

***The Hydrogen Microprint Technique to
Reveal Hydrogen Distributions in TRIP
Steels***

Hydrogen in TRIP Steels



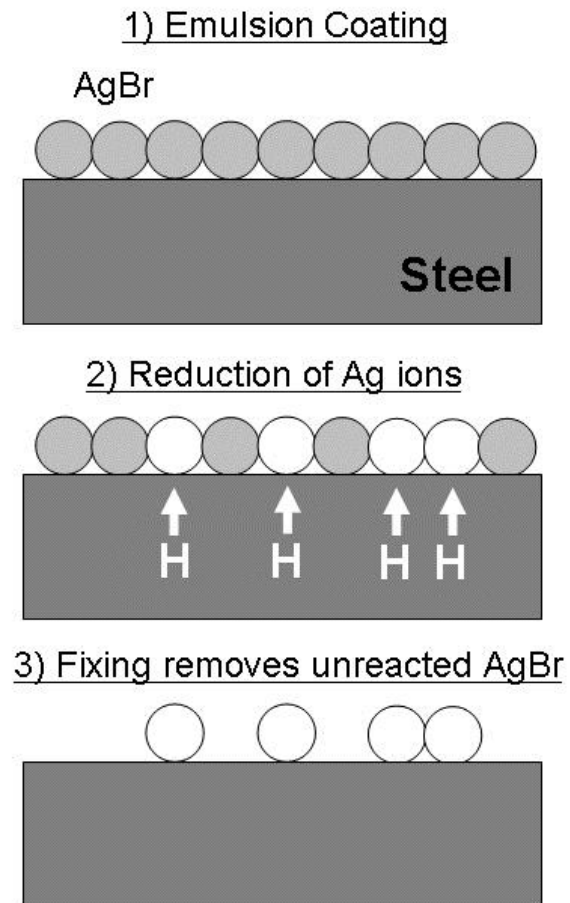
0.19C, 1.59Mn, 1.63Si (wt-%)



Hydrogen Microprint Technique

Image-before-etch method ... for fine microstructures

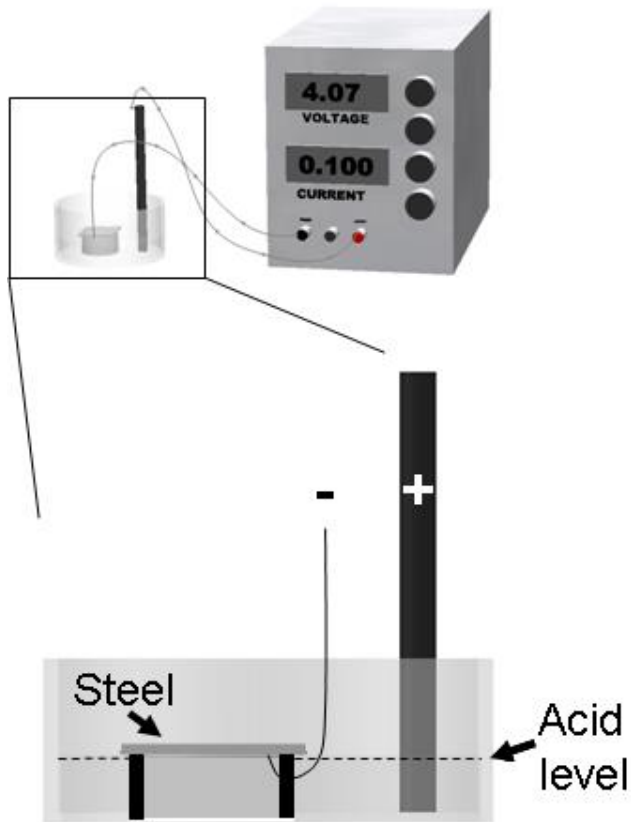
- Utilizes $\text{AgBr} \rightarrow \text{Ag}$ reduction with H
 - AgBr emulsion gel
- Hydrogen diffuses through steel (one way)
 - Reduces $\text{Ag}^+ \rightarrow \text{Ag}$
 - Fixing removes excess AgBr
 - SEM analysis reveals Ag grains where H has exited steel
 - Observe microstructural features where H is located



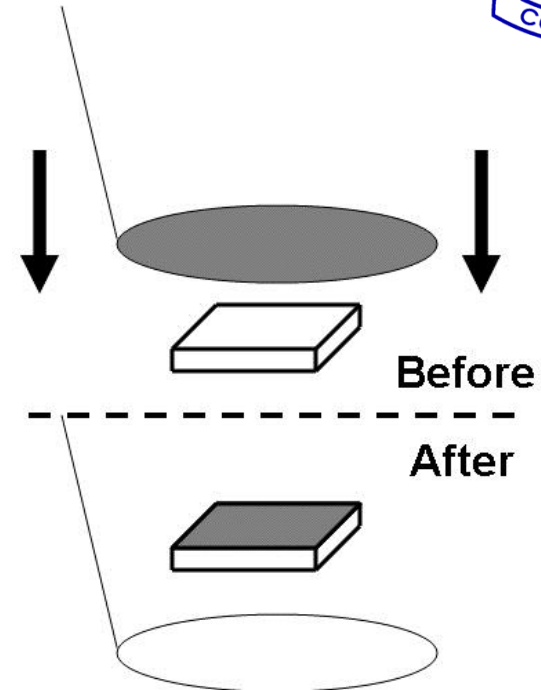
Hydrogen Microprint Technique



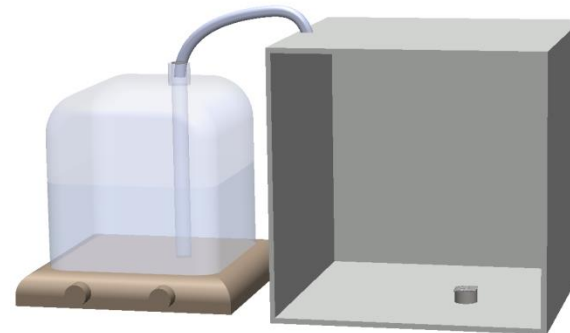
1)



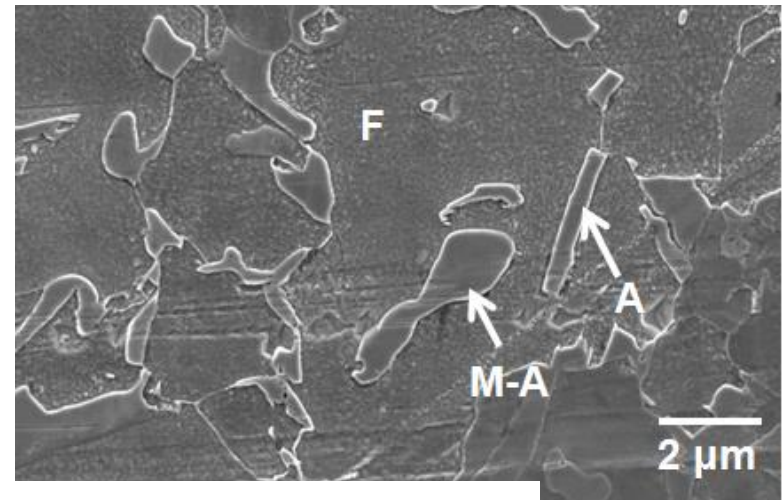
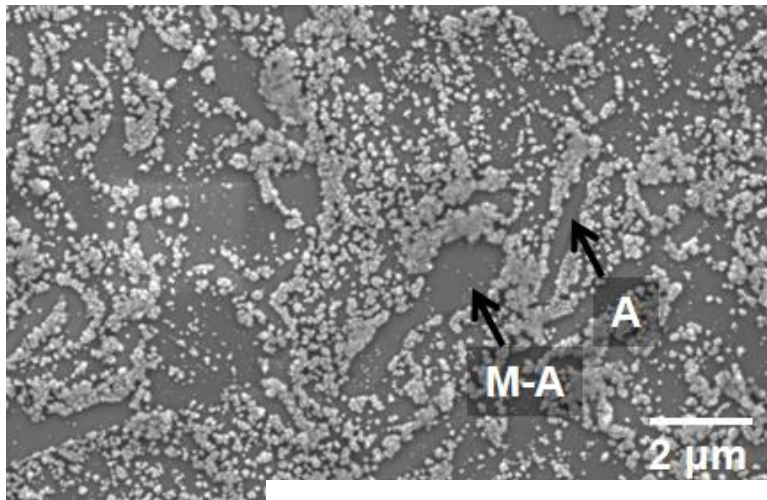
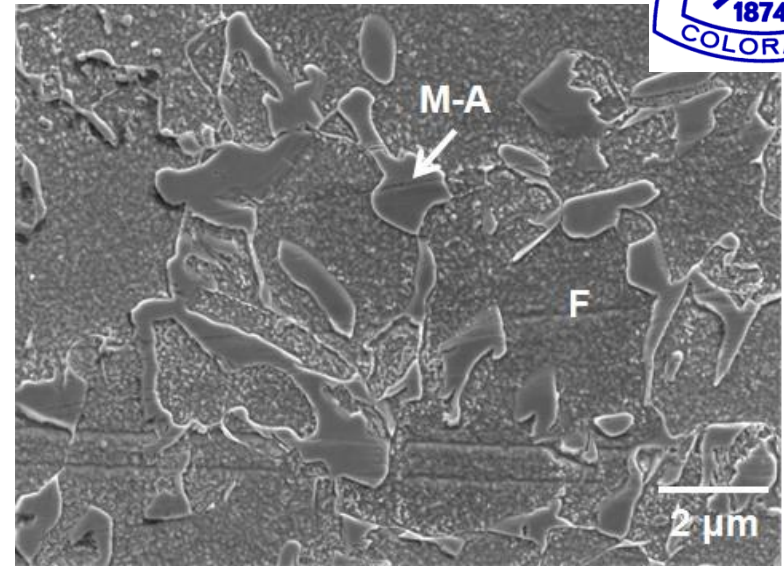
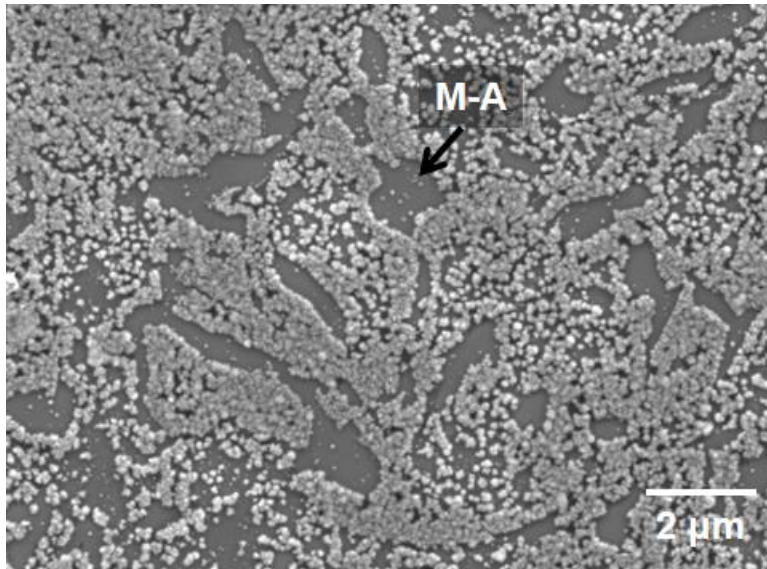
2)



3)



Hydrogen Microprint Technique



$D_{\alpha}^H \sim 10^{-5} \text{ cm}^2/\text{s}$

$D_{\gamma}^H \sim 10^{-12} \text{ cm}^2/\text{s}$

TRIP Steel Summary



- **TRIP effect enhances strength and ductility**
 -requirements - austenite with controlled stability
- **Assessment of stability**
 - Color tint etching
 - Diffraction: x-ray and neutron
 - EBSD
 - Mechanical properties (stress-strain curve shape)
 -



Alloying and Processing Strategies to Produce 3rd Generation AHSS

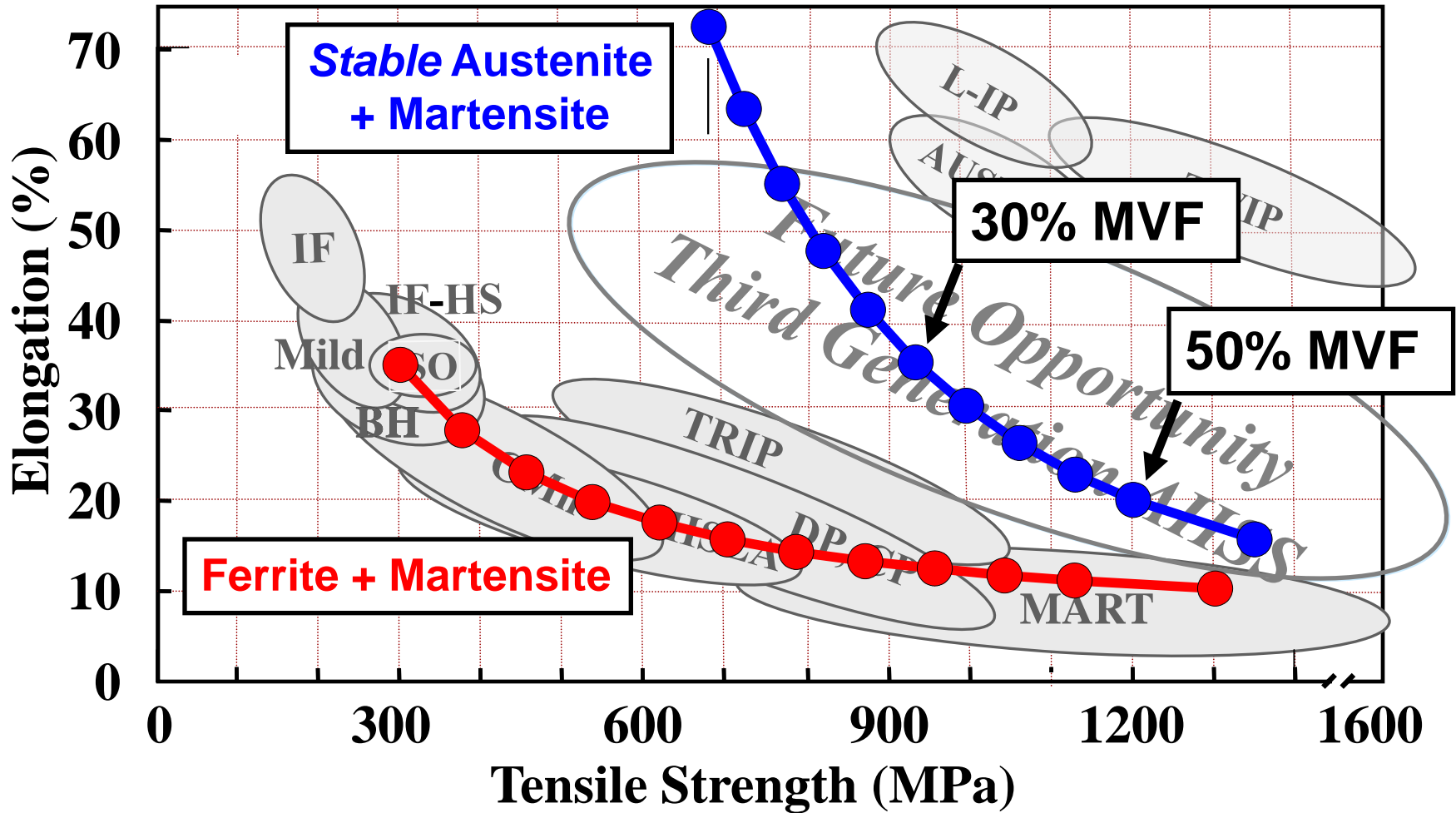
Example:

Quenched and Partitioned (Q&P) Steels

....a fundamentally new processing approach to produce high strength sheet steels with significant amounts of austenite....

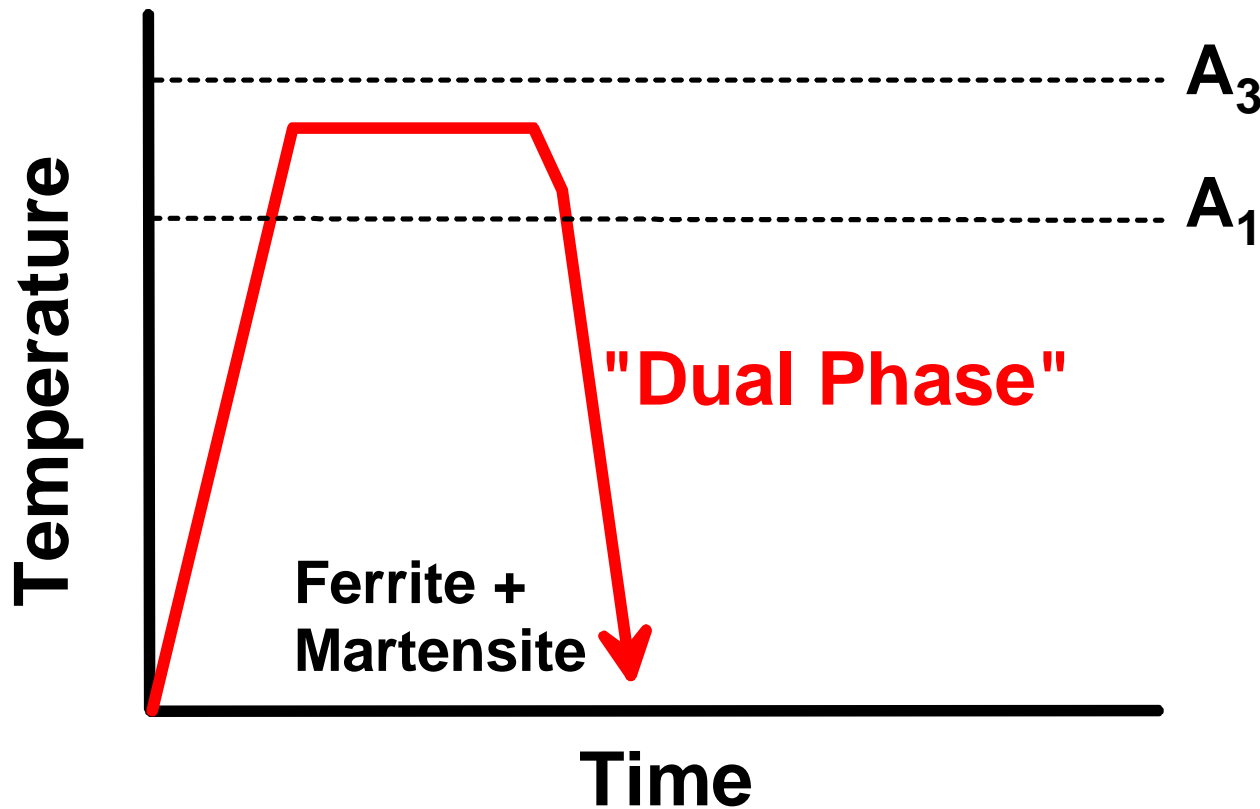
Predictions Based on Composite Modeling

Austenite is a key enabler for new AHSS



DP Steel Processing

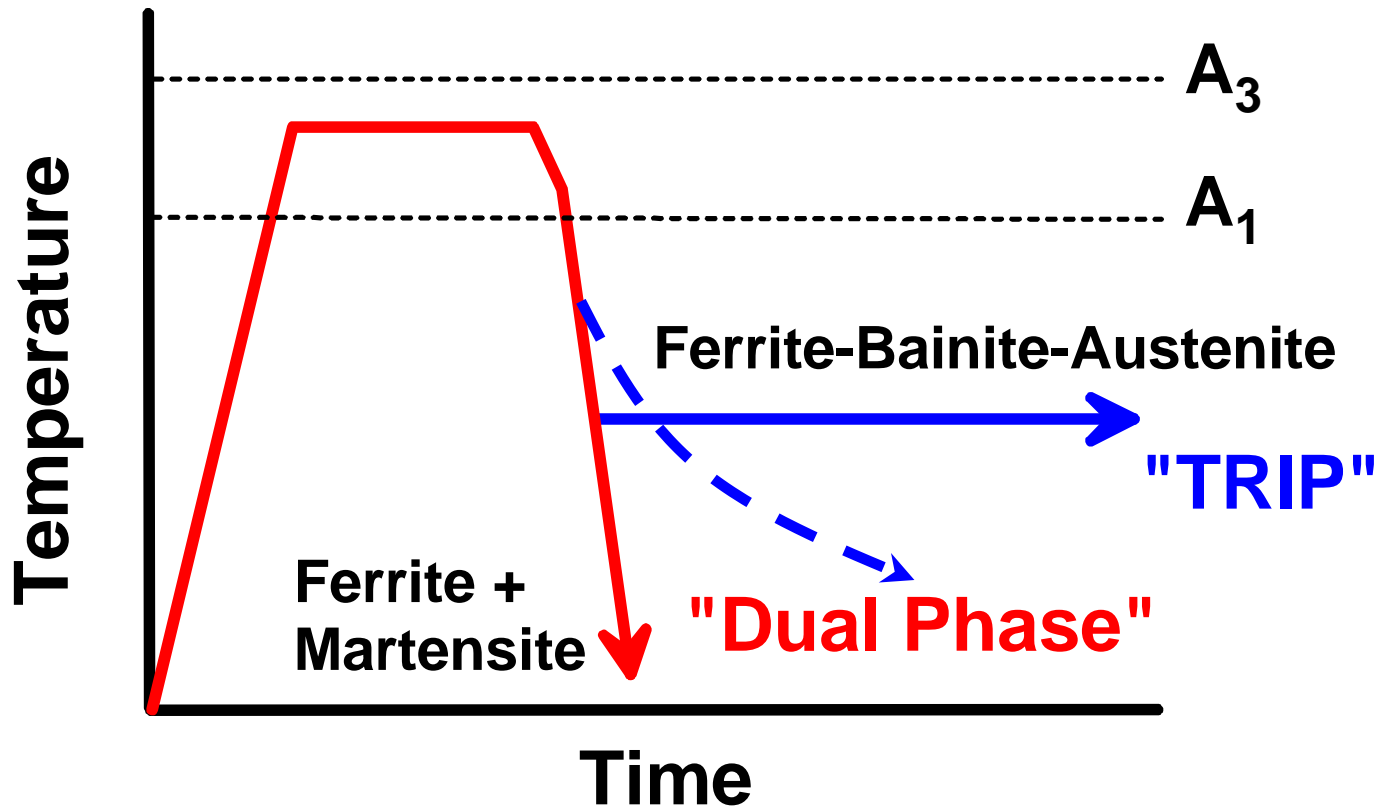
- **Initially conceived based on “simple” routes for hot and cold rolled steels**
 - Microstructures may be more complex than simply ferrite + martensite



TRIP Steel Processing

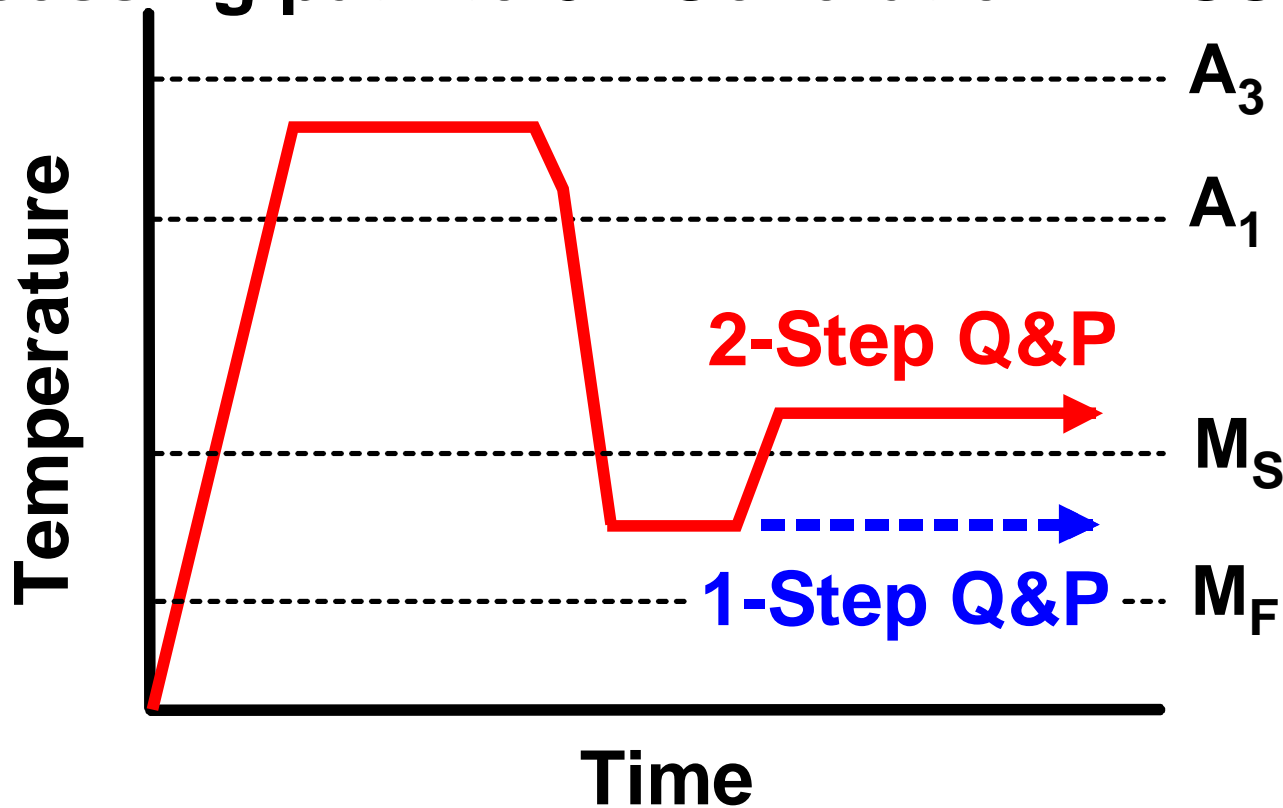


- Isothermally transform or control cool
- Austenite in high strength matrix (e.g. fine grain ferrite, martensite, bainite, ...)

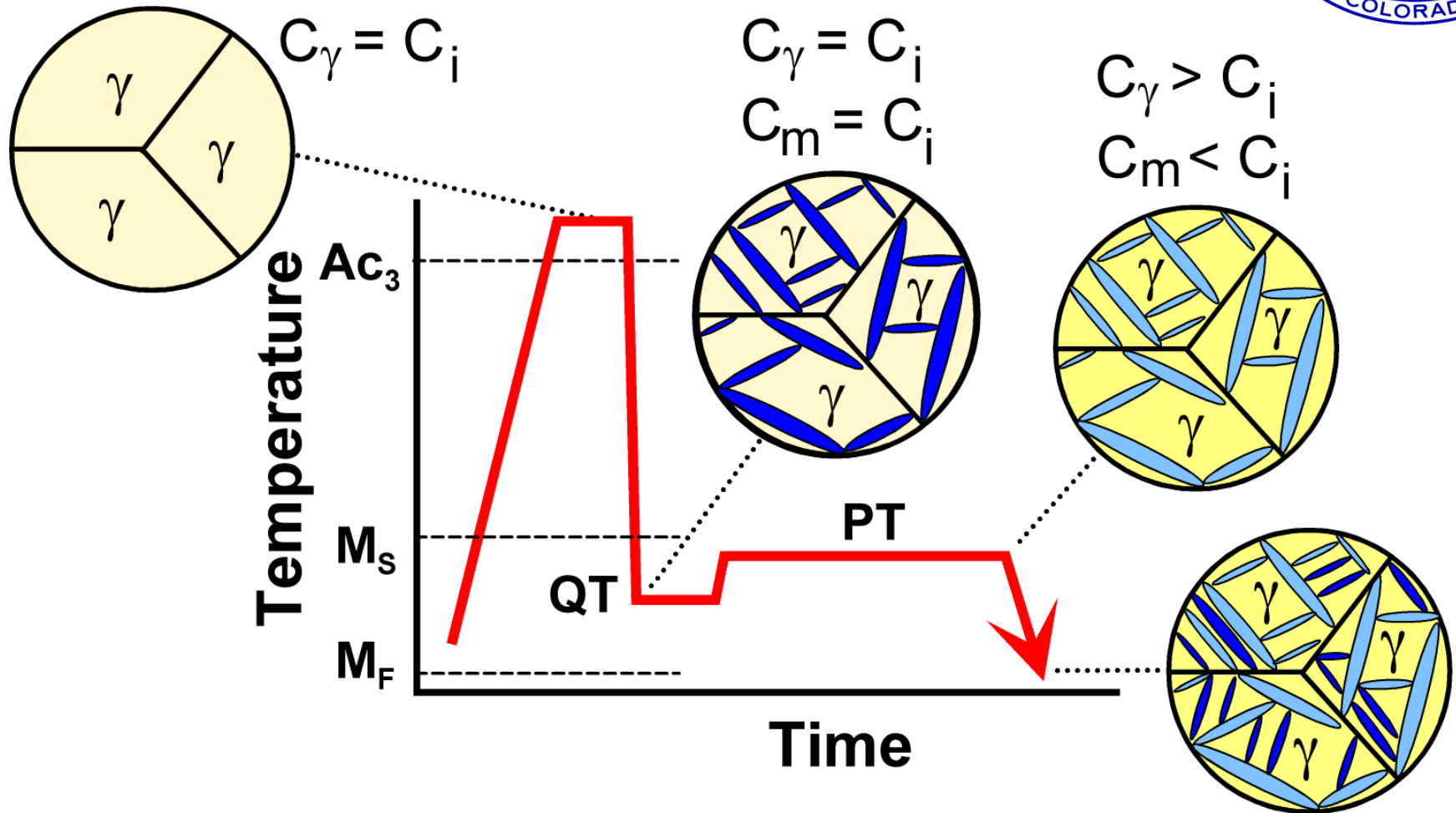


Interrupted Cooling: The “Q&P” Process

- Novel method to produce high strength material with significant amounts of retained austenite
- Processing path to 3rd Generation AHSS



Q & P Processing - Overview



Final Austenite Amount Modified by Additional Martensite Formation on Cooling to Room Temperature

Q&P Selection Methodology



- Evaluate austenite stability

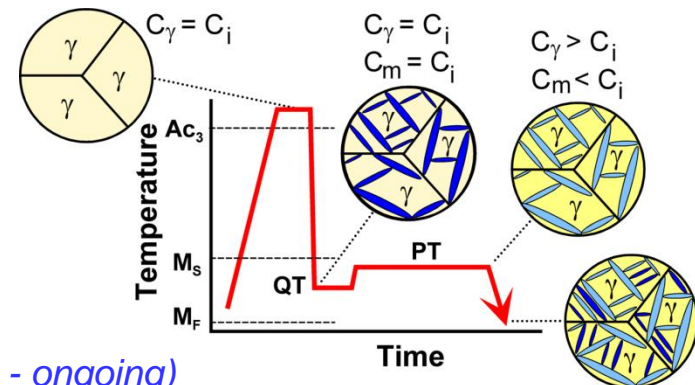
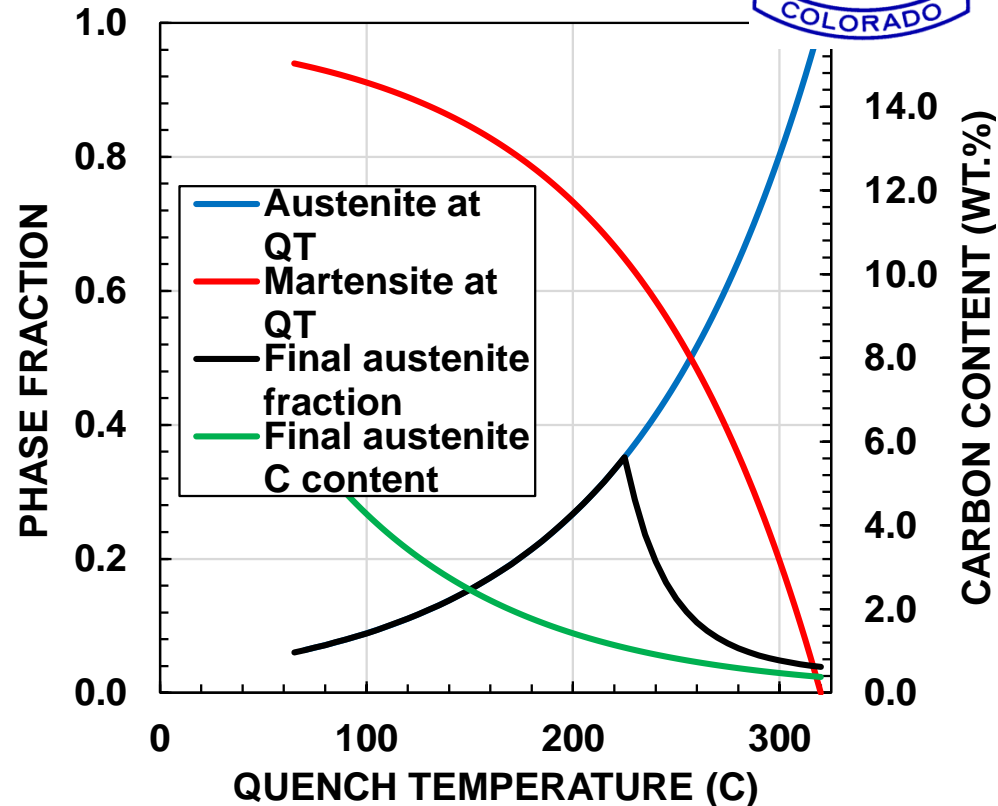
$$M_s = 539 - 423C - 30.4Mn - 7.5Si + 30Al$$

- Predict fraction transformed on cooling (Koistinen-Marburger equation)

$$f_M = 1 - e^{-0.011(M_s - T)}$$

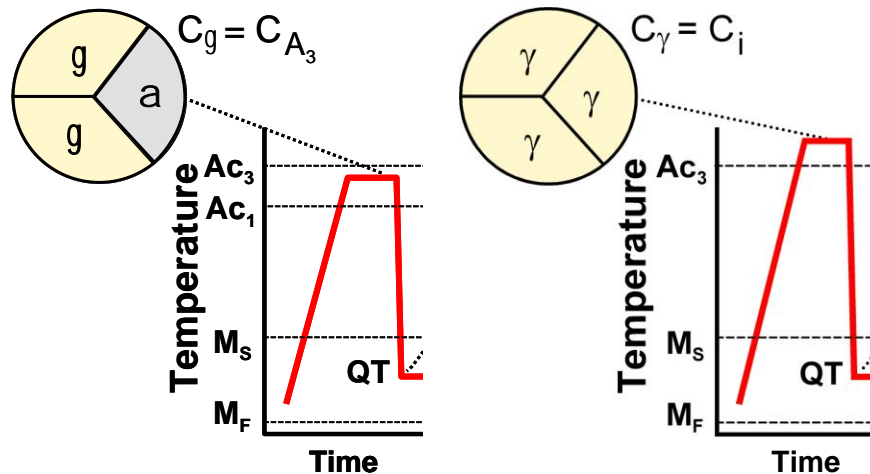
Assumptions:

- No austenite decomposition
- Assumes **all** C partitions from martensite to austenite
- No carbide formation



Q&P: Unique Designed Microstructures

(1) Annealing temperature controls amount of initial ferrite

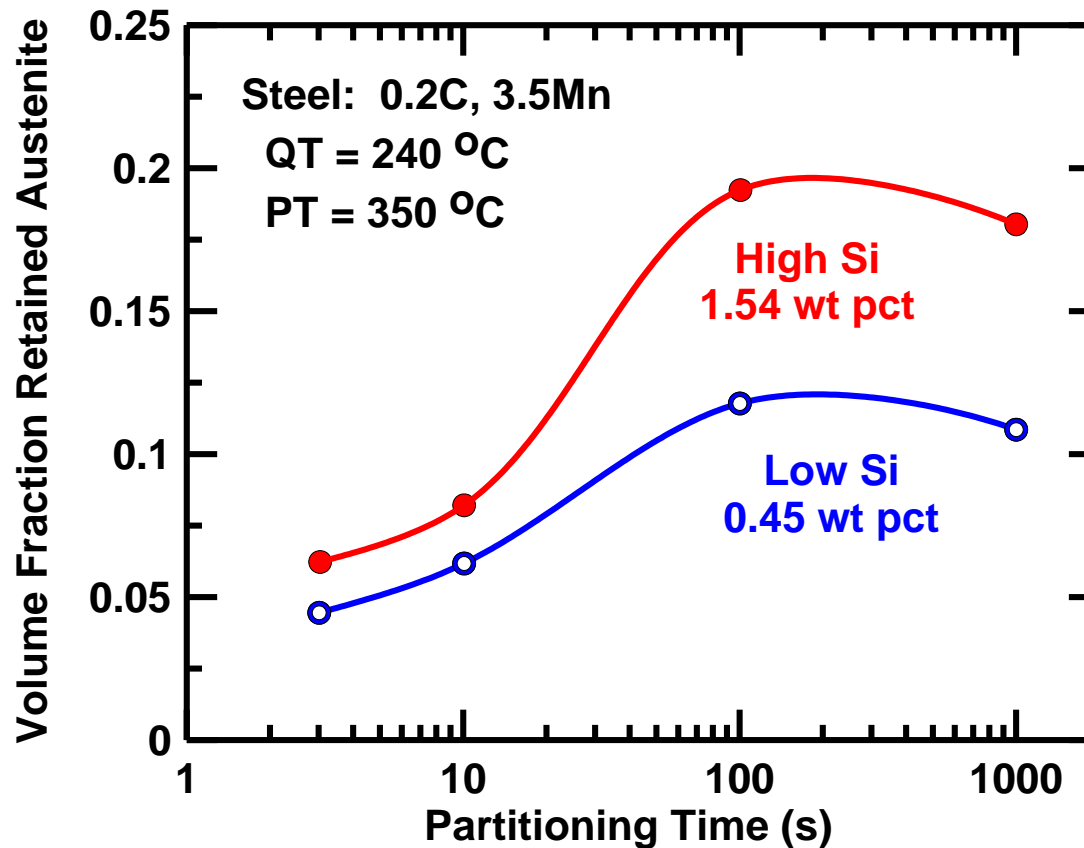


- (2) Quench temperature (QT): controls amount of initial martensite
- (3) Alloying controls carbide stability – e.g. add Si
- (4) Partitioning temperature and time: control austenite stability
- (5) Result: unique combinations of martensite + austenite + ferrite + ..other..

“Q&P” Alloying and Processing



- Alloying: e.g. Mn Si Al C Mo
- ... to control critical temperatures: M_s M_f
- ... to suppress cementite formation

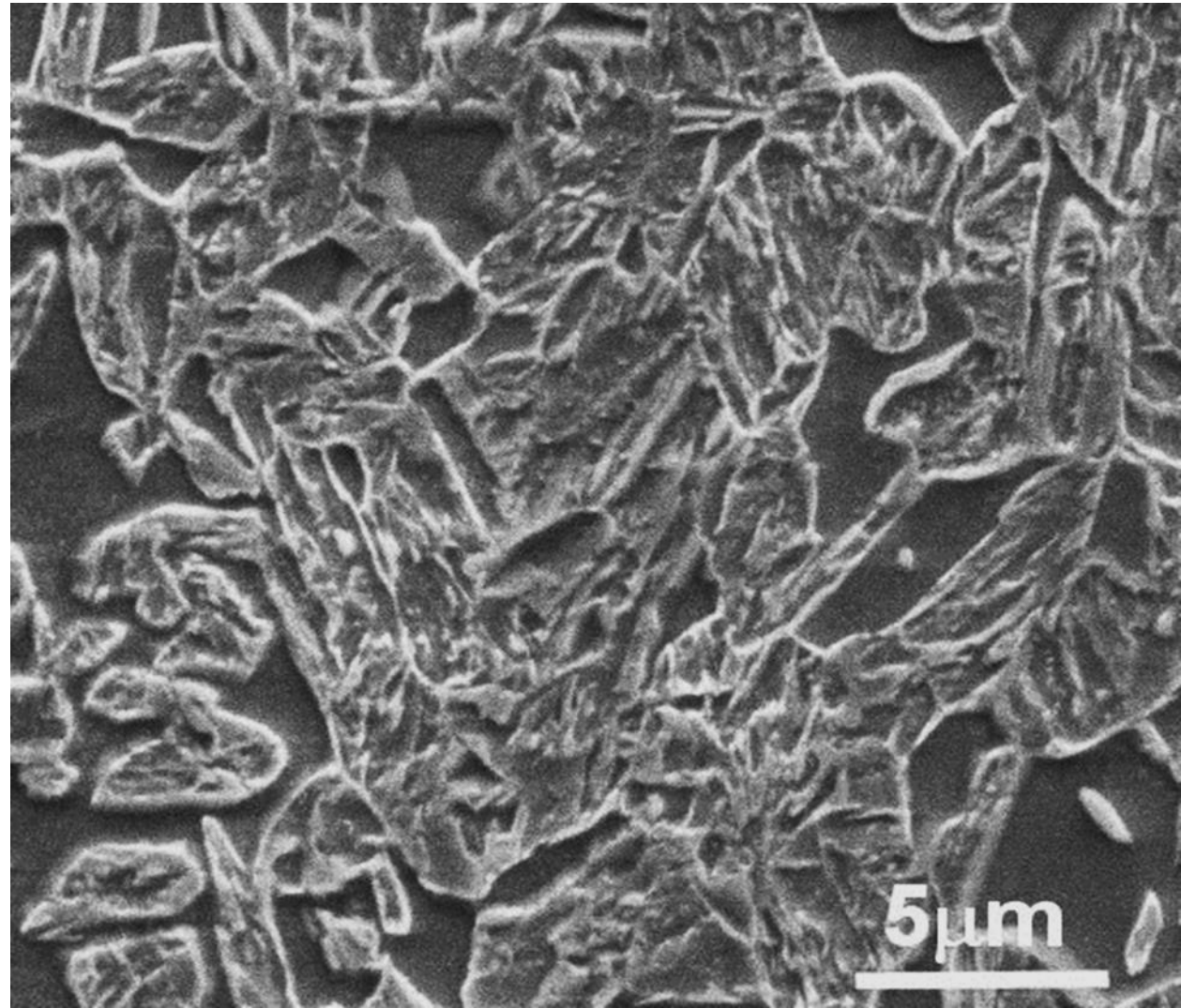
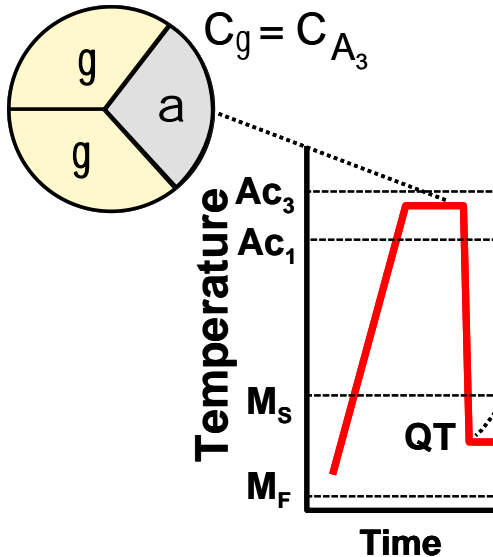


Example Q&P Microstructure:



- Intercritically annealed: $\alpha_{IC}=25\%$
- 0.19C, 1.59Mn, 1.63Si (wt-%)
- QT = 200 °C, 10 s
- PT = 400 °C, 10s
- Austenite = 11.4%

SEM Micrograph: 2% nital etch

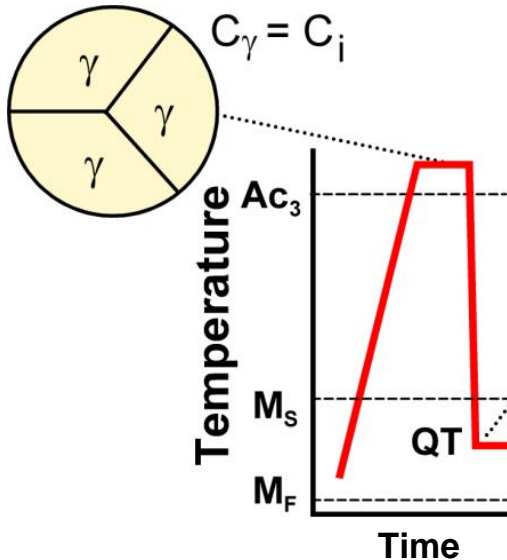
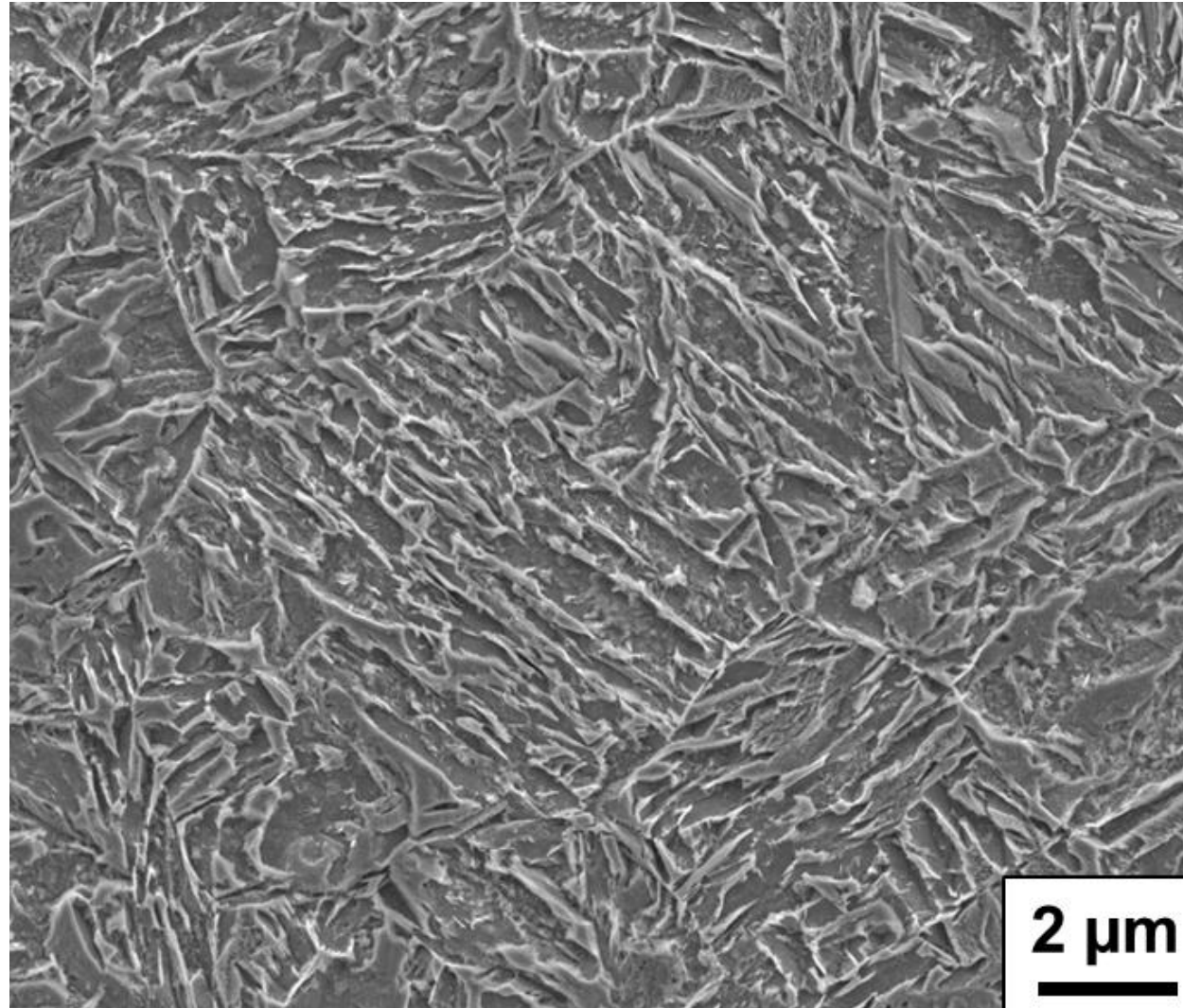


Example Q&P Microstructure:



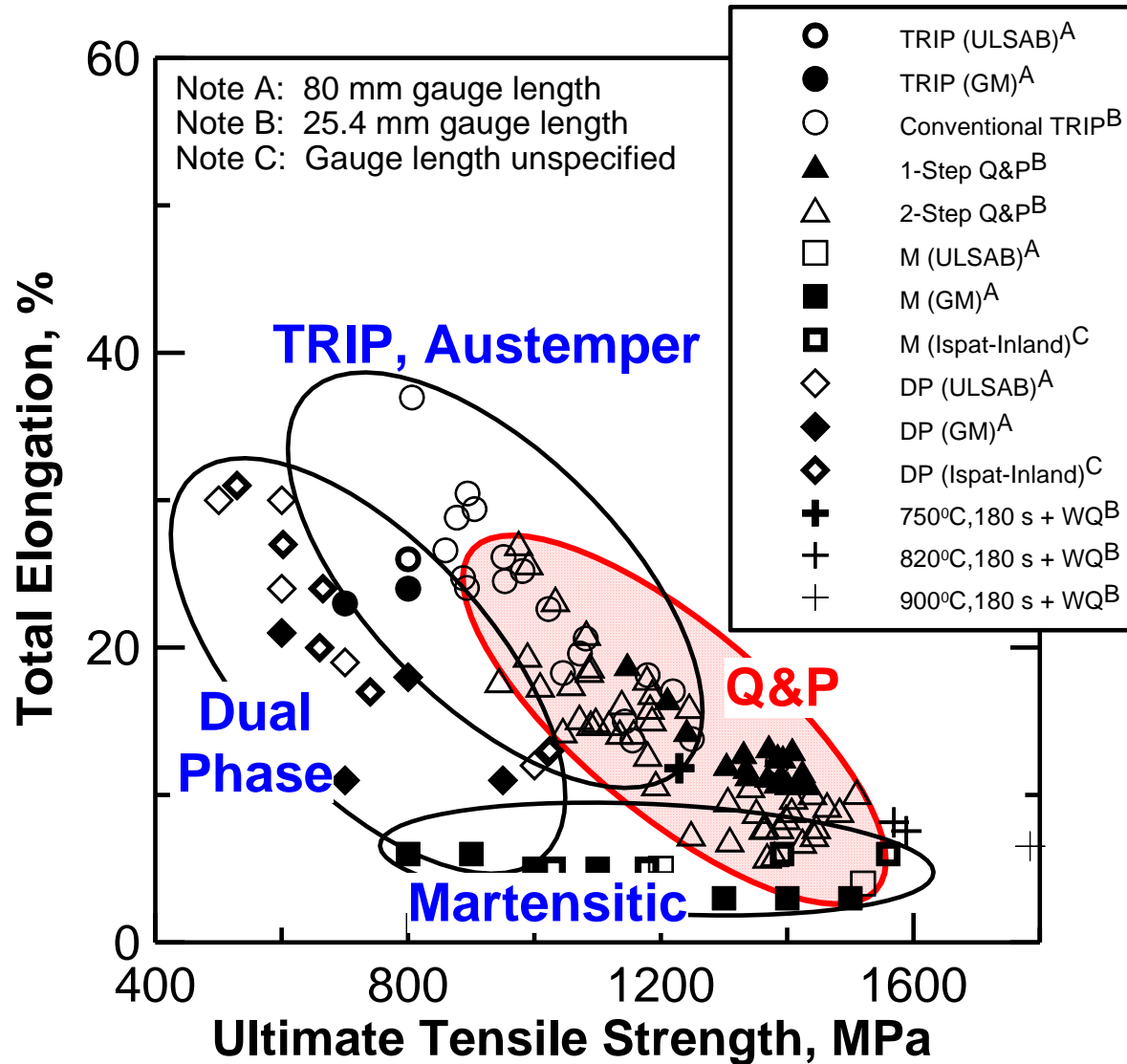
- **Annealed as austenite: $\alpha_{IC} = 0\%$**
- **0.3C, 3Mn, 1.6Si (wt-%)**
- **QT = 200 °C**
- **PT = 400 °C, 30 s**
- **Austenite = 10.9%**

SEM Micrograph: 2% nital etch



Properties of Q&P

Summary and Comparison with AHSS



Clarke, Speer, et al. ASPPRC, Colorado School of Mines (2006)

Assessment of Q&P Microstructures

Competing Reactions:

Carbon Partitioning

Compositions change:

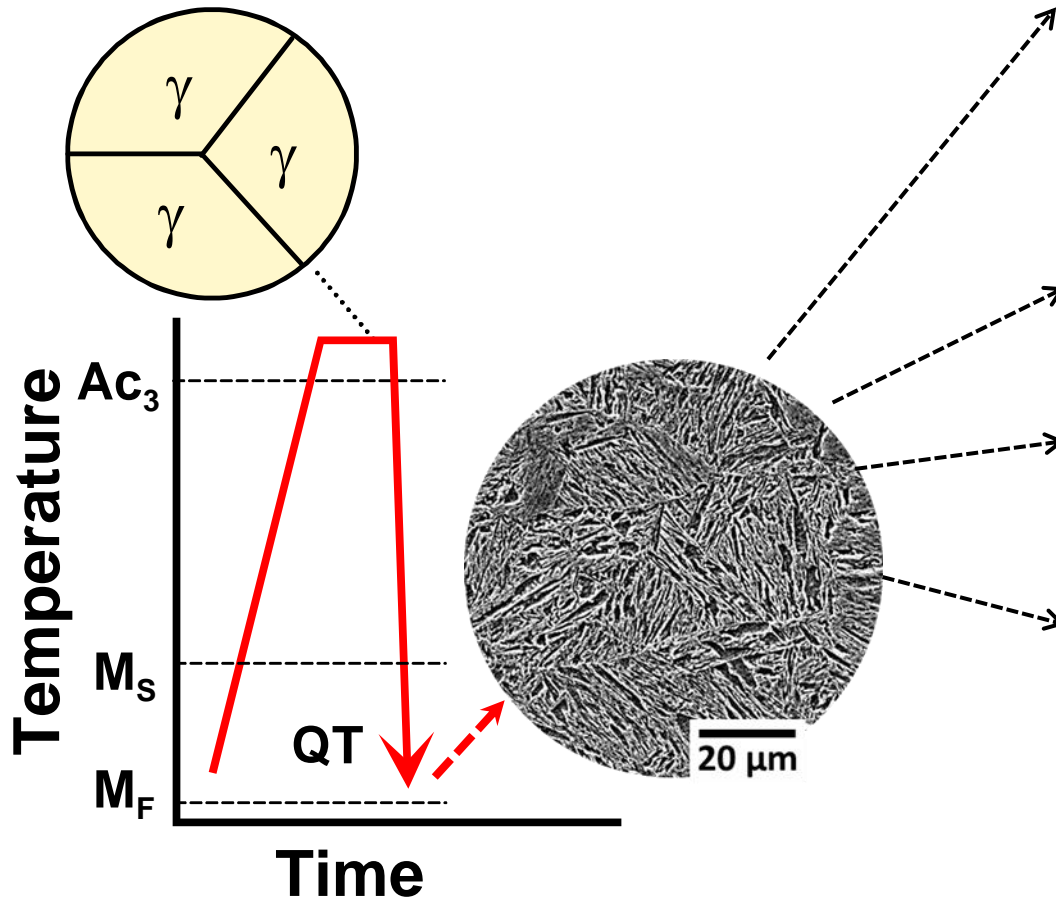
Austenite and martensite

Martensite Tempering

Stage 1: Formation of transition carbides, epsilon carbide

Stage 2: Transformation of retained austenite to ferrite and cementite

Stage 3: Replacement of transition carbides and martensite by cementite and ferrite



Micrograph: 0.2 C, 1.2 Mn, Direct Quenched:
N. Muckelroy, MS Thesis, ASPPRC/CSM, 2010.





***Application of Advanced Analytical
Techniques to Assess Q&P and
AHSS Microstructures***



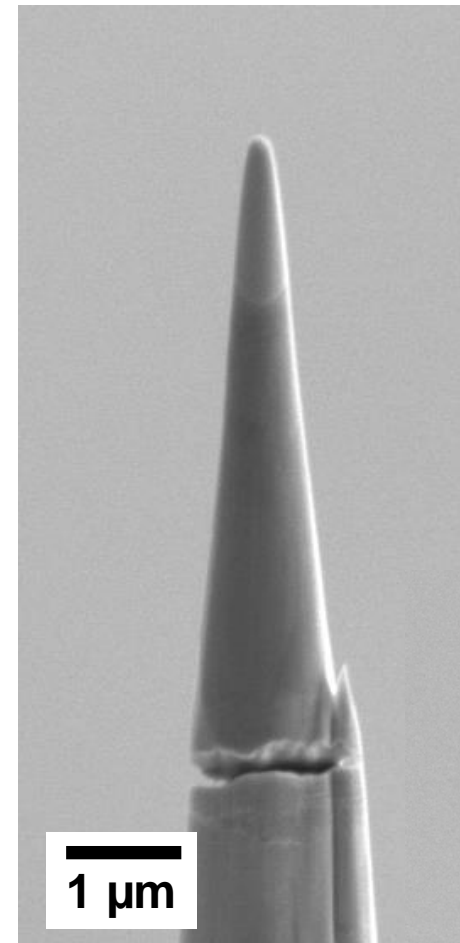
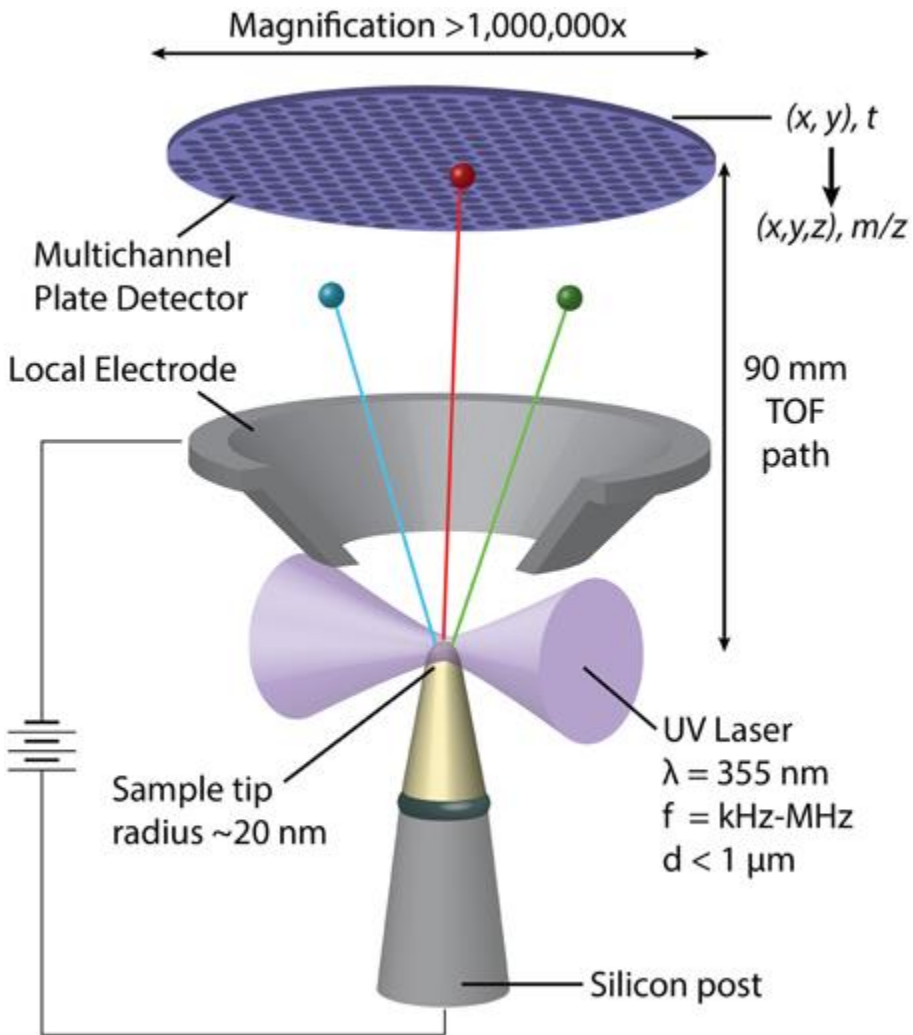
Atom Probe

Atom Probe Tomography

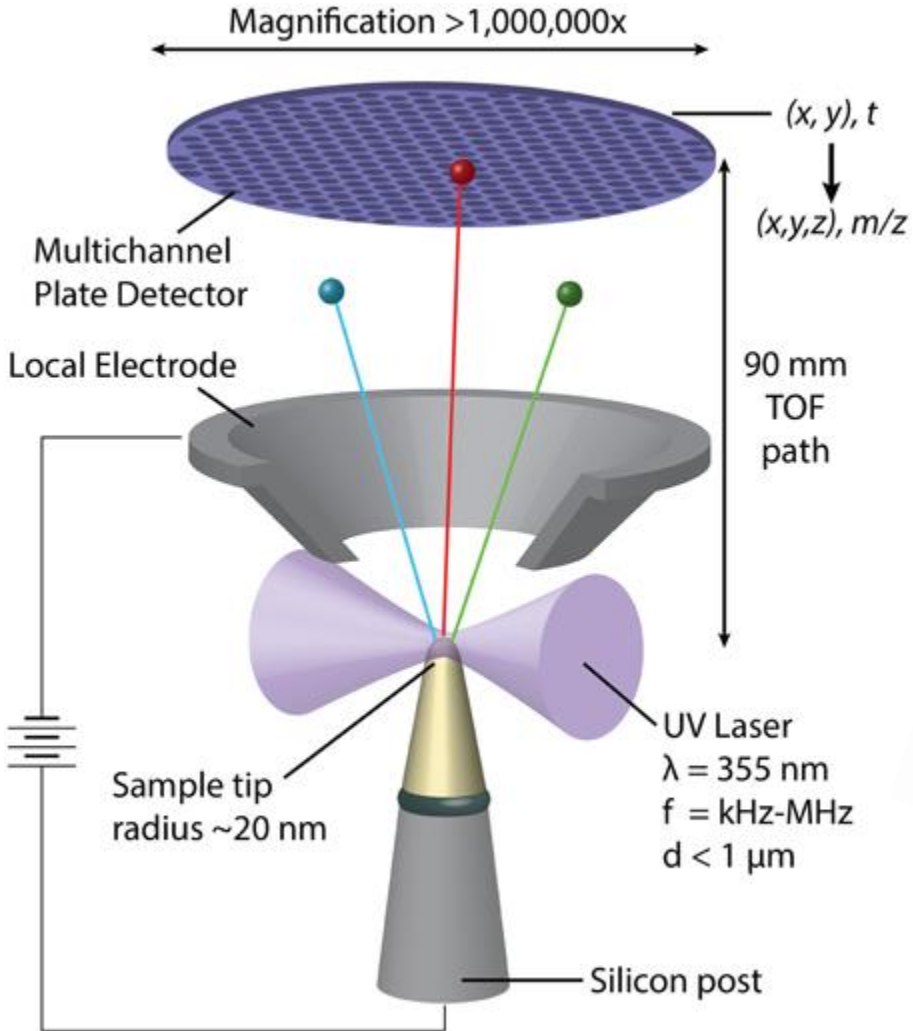
- 3D imaging and chemical composition measurements at the atomic scale
- Assess carbon (and nitrogen) partitioning and local compositions
 - **DP Steel - 0.10 C, 2.0 Mn, 0.3 Cr, 0.3 Mo (wt-%)**
 - **Q&P Steels**
 - **0.19 C, 1.59 Mn, 1.63 Si (wt-%) -- $M_s = 399\text{ }^\circ\text{C}$**
 - **Special alloys designed for QT = RT**
 - **0.32 C, 1.91 Si, 13.95 Ni, 0.25 Mo (wt-%)**
 - $M_s = 258\text{ }^\circ\text{C}$
 - **0.27 C, 8.31 Mn, 1.94 Si, 0.24 Mo (wt-%)**
 - $M_s = 142\text{ }^\circ\text{C}$



Atom Probe Tomography

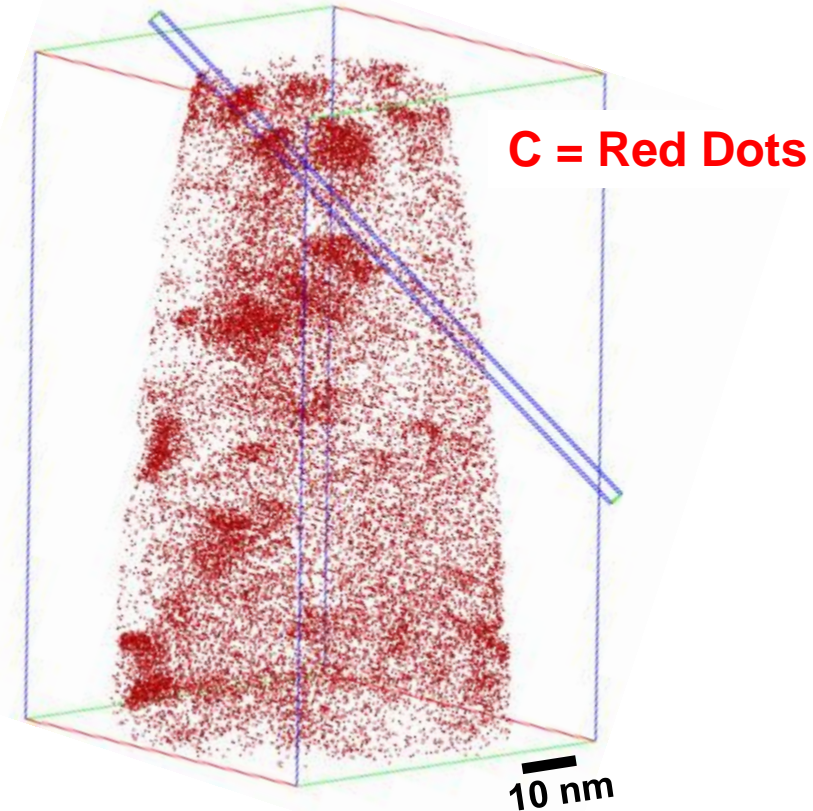


Atom Probe Tomography



Evidence of Carbide Formation

0.19C, 1.59Mn, 1.63Si (wt-%)



Anneal = 900 °C, 180 s

QT = 240 °C, 10 s

PT = 400 °C, 30 s

APT DP Steel Specimen – TEM



**Ferrite-Martensite
Interface**

**Nitrogen partitioning
Dual-Phase Steel
0.10 C, 2.0 Mn, 0.3 Cr, 0.3 Mo**

**Depth
evaporated by
atom probe**

100 nm

APT DP Steel Specimen – Dark Field TEM

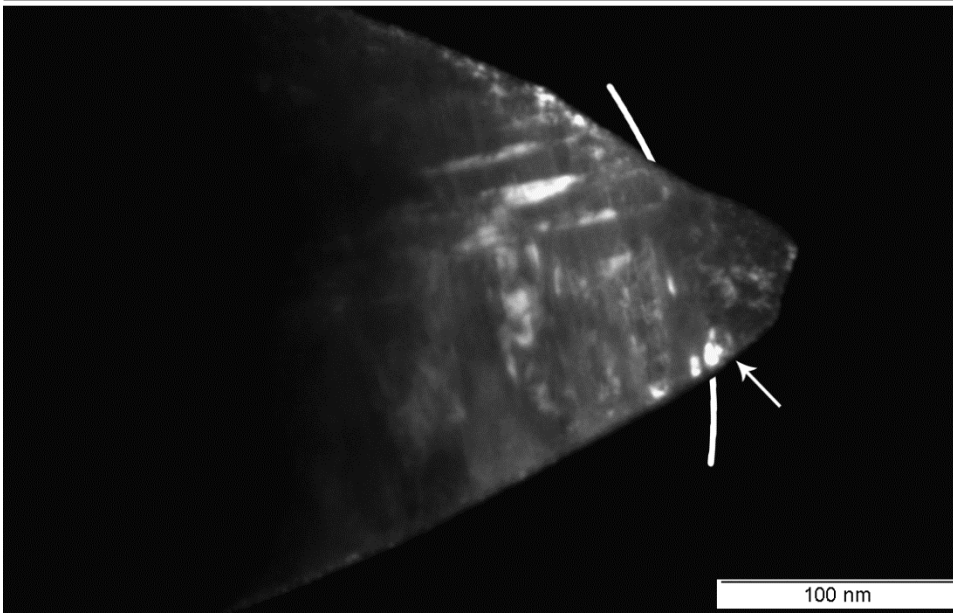
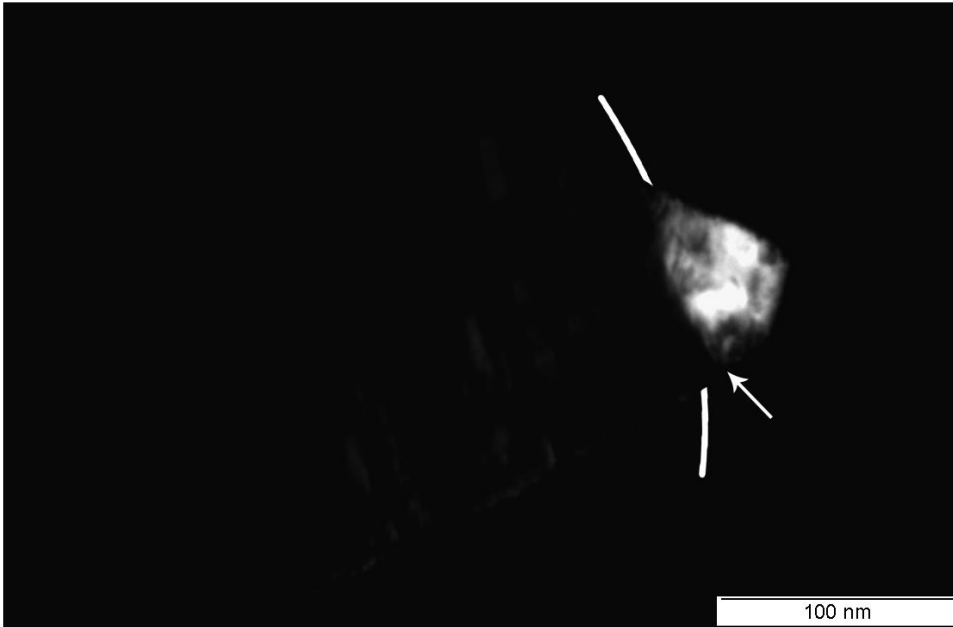
**Nitrogen partitioning
Dual-Phase Steel
0.10 C, 2.0 Mn, 0.3 Cr, 0.3 Mo**

Ferrite illuminated at tip

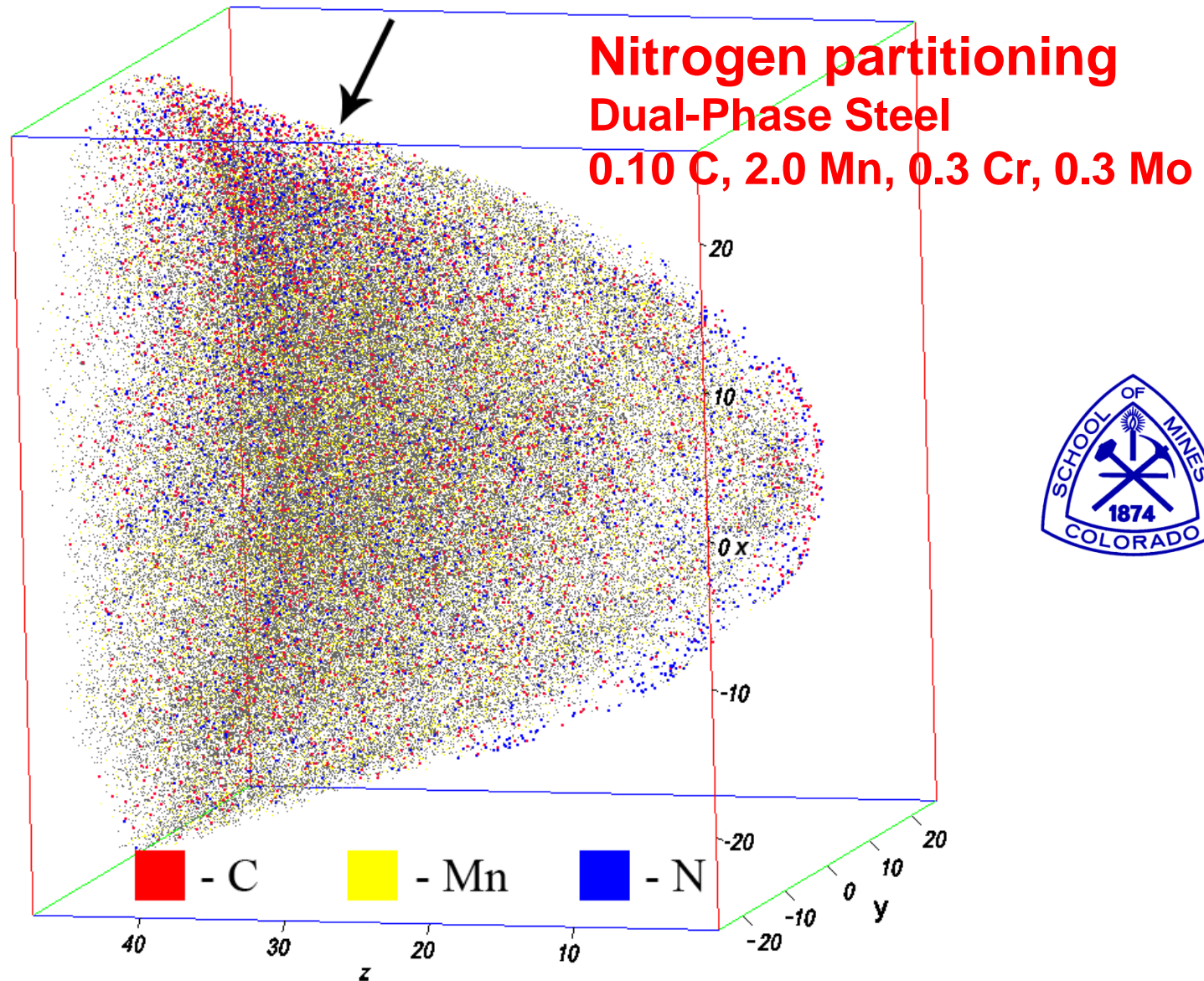


**Martensite identified by
lath structure**

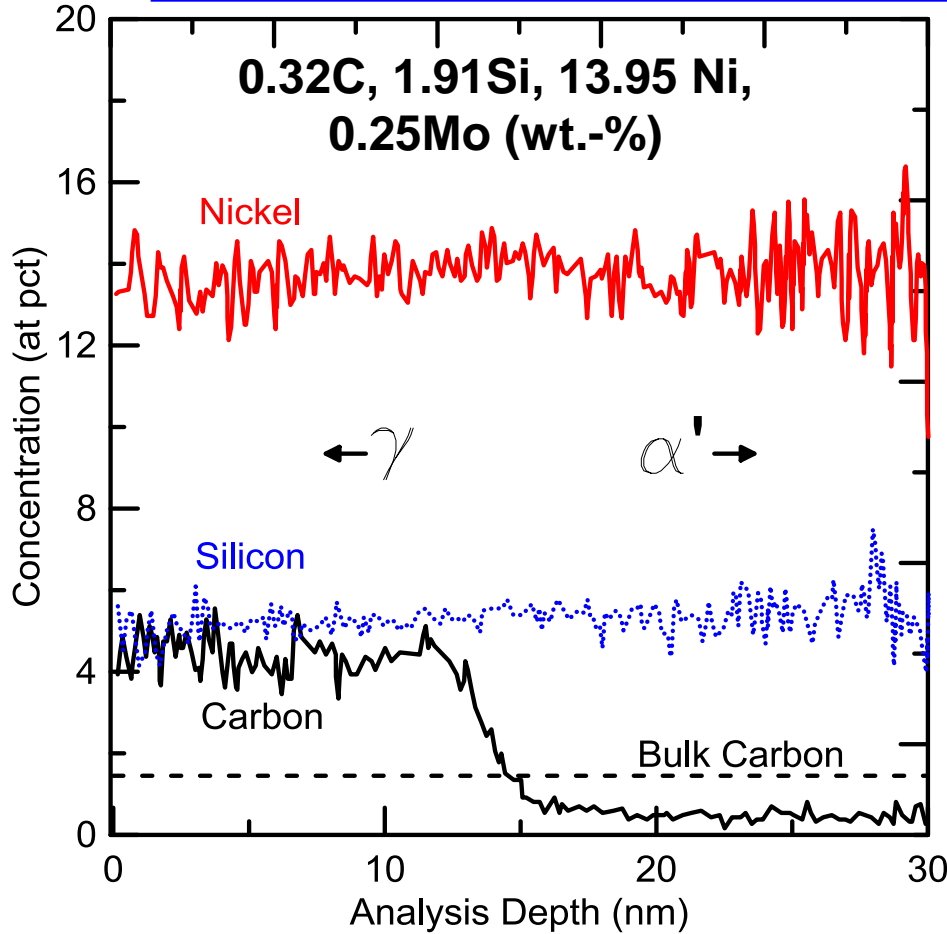
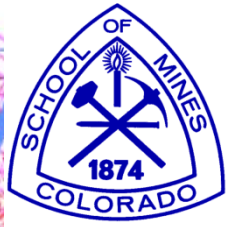
**One of two variants
illuminated**



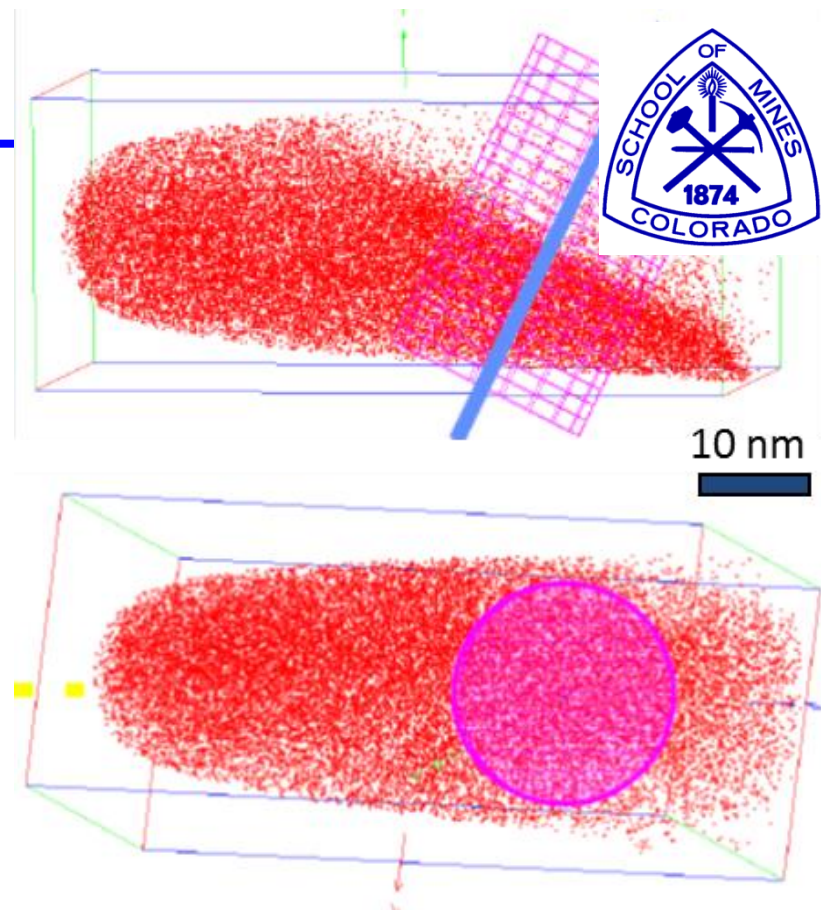
APT DP Steel: Atom Probe Reconstruction



APT: High Ni Alloy



- **Austenitize = 875 °C**
- **QT = Room T (23 °C)**
- **PT = 400 °C, 100 s**

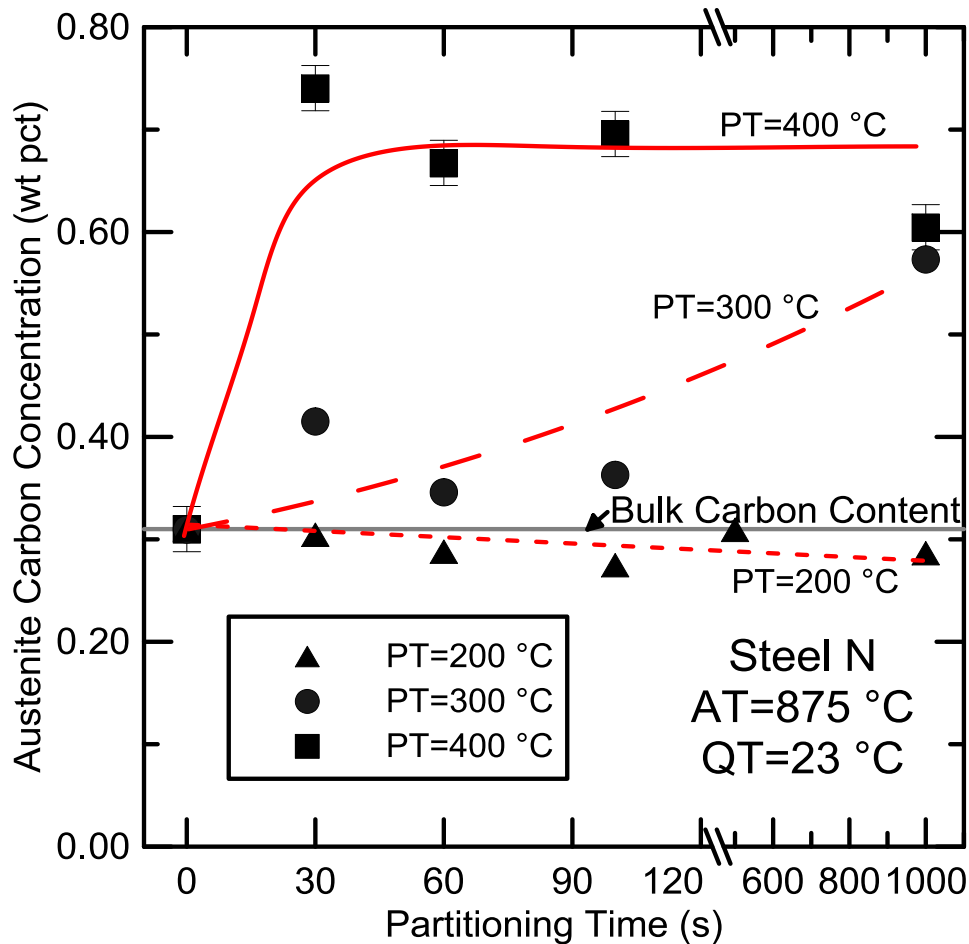


Austenite (at.-%)			
C	Si	Ni	Fe
4.51	5.1	14.2	76.3
Martensite (at.-%)			
0.18	5.3	13.7	80.9
Bulk Steel (at.-%)			
1.45	3.7	13.0	81.9

High Ni Alloy: X-Ray Diffraction + APT



0.32C, 1.91Si, 13.95 Ni, 0.25Mo



Austenite				
	C	Si	Ni	Fe
at pct	4.51	5.06	14.2	76.3
wt pct	1.05	2.69	15.8	80.5
Martensite				
	C	Si	Ni	Fe
at pct	0.18	5.27	13.7	80.9
wt pct	0.04	2.71	14.7	82.6
Bulk Steel				
	C	Si	Ni	Fe
at pct	1.45	3.71	13	81.9
wt pct	0.32	1.91	14	83.8

- Austenitize = 875 °C
- QT = Room T (23 °C)
- PT = 400 °C, 100 s

Atom Probe Tomography: Summary

- **APT technique applicable to Q&P steels**
- **APT confirmed C partitioning based on XRD analyses**
- **APT provided evidence of carbon atom “clustering” in martensite during partitioning**
 - **Clustering related to carbide formation**
 - **Carbon partitioning and martensite partitioning occur simultaneously**





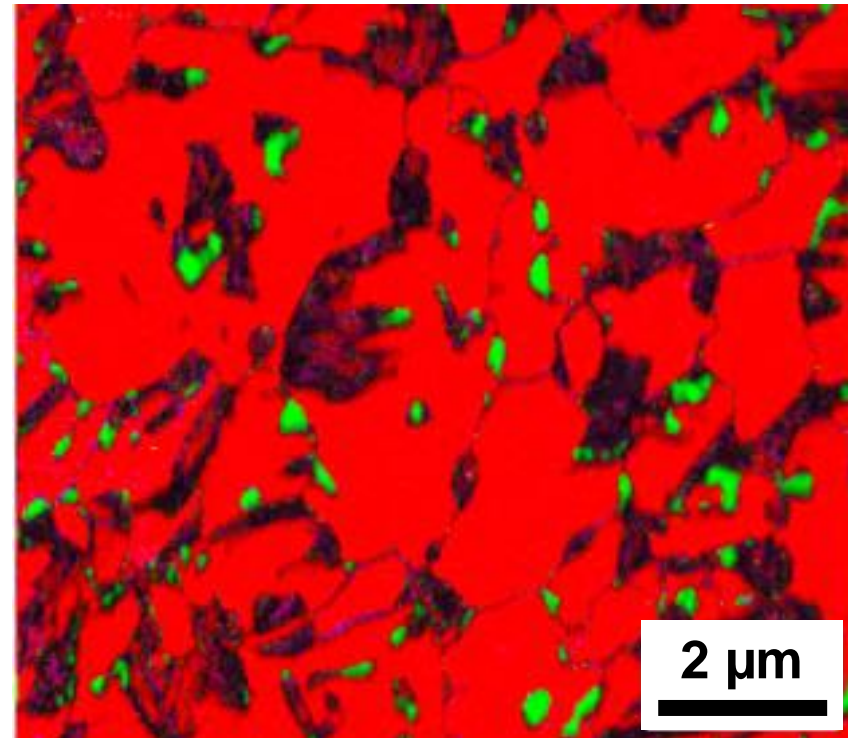
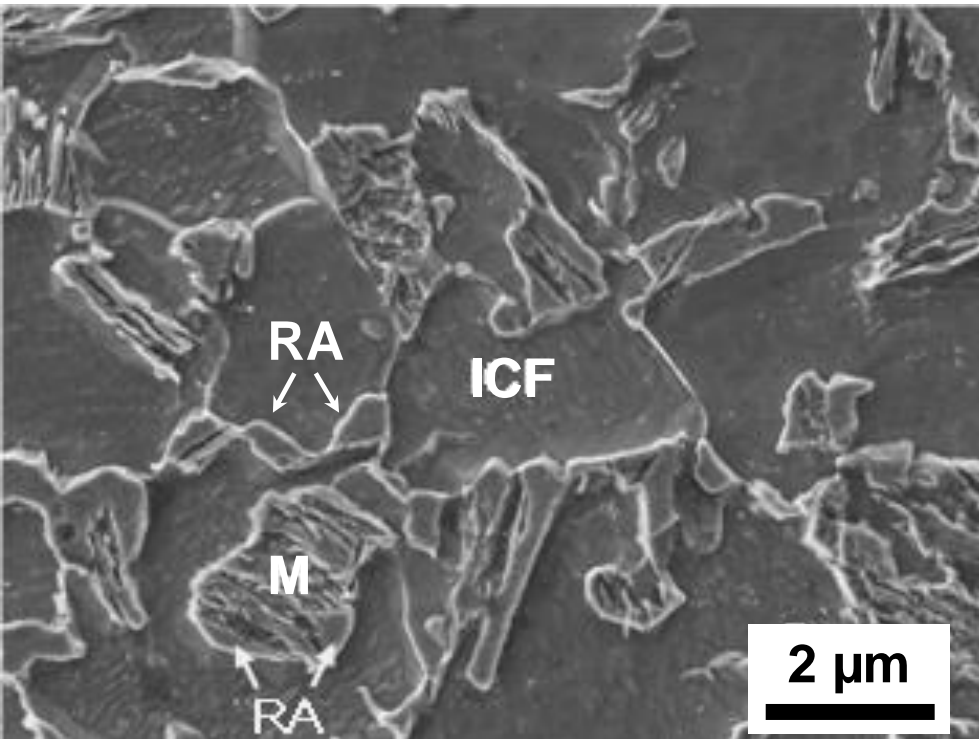
EBSD

Grant Thomas, John Speer, David Matlock and Joseph Michael, “Application of Electron Backscatter Diffraction Techniques to Quenched and Partitioned Steels,” *Microscopy and Microanalysis*, vol. 17, pp 368-373.

Example: EBSD of Q&P Microstructure

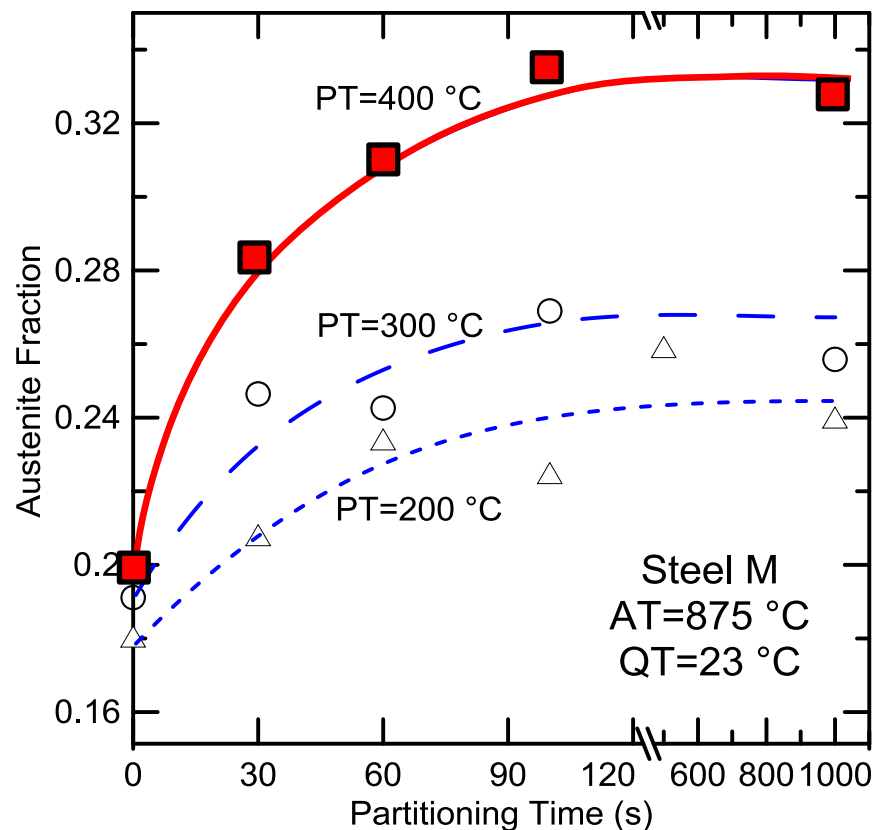


- 0.19C, 1.59Mn, 1.63Si (wt-%) steel
- Intercritically annealed at 820 °C
- QT = 250 °C
- Partitioned on cooling to simulate processing during hot rolling

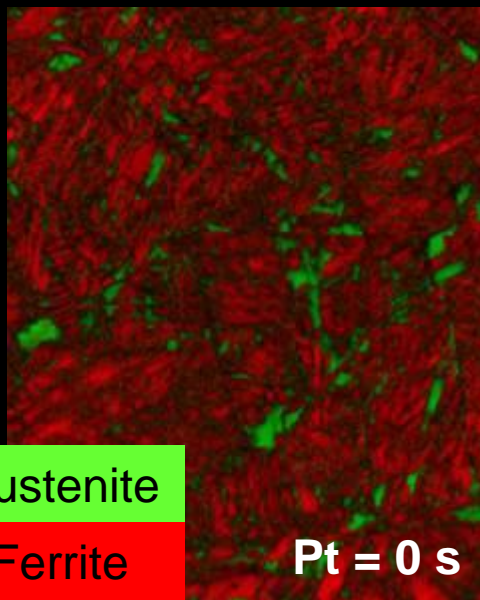


With partitioning time.....Growth of Existing Austenite or Nucleation of New?

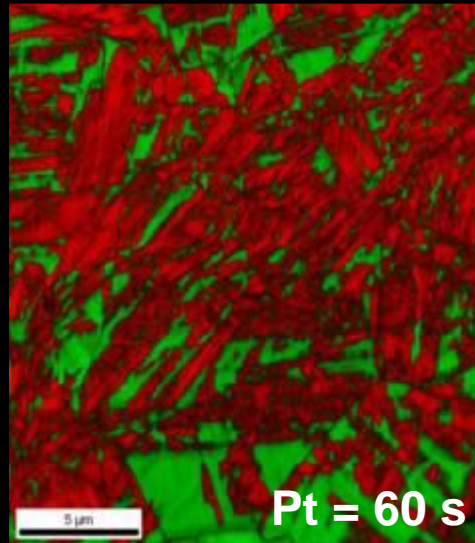
- Application of EBSD to assess austenite contents and density = $f(t)$.
- Evaluate special steel with QT = Room T
- 0.27 C, 8.31 Mn, 1.94 Si, 0.24 Mo (wt-%)
 - $M_s = 142\text{ }^\circ\text{C}$



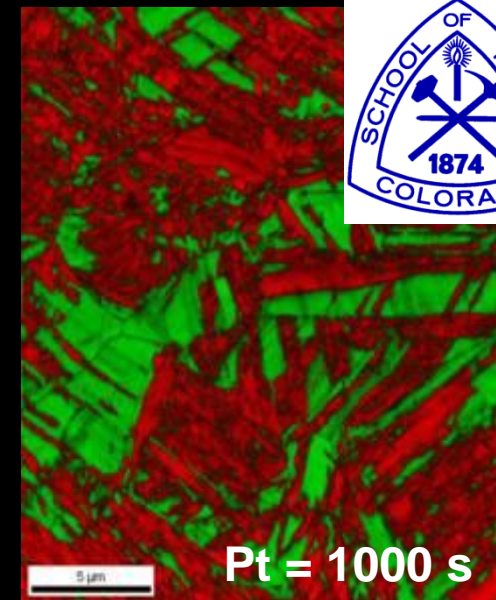
EBSD: IQ + Phase Maps



Pt = 0 s



Pt = 60 s



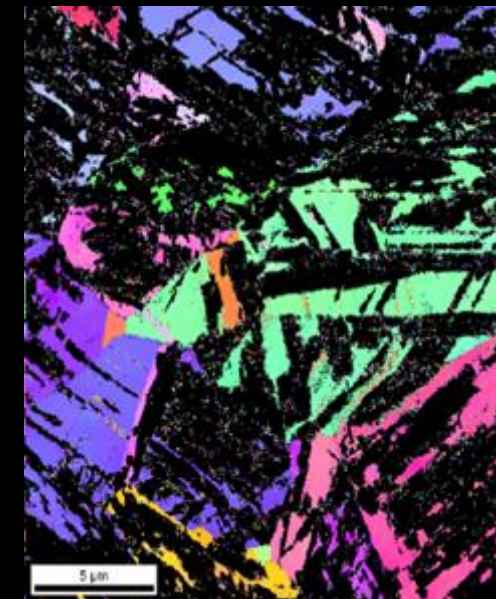
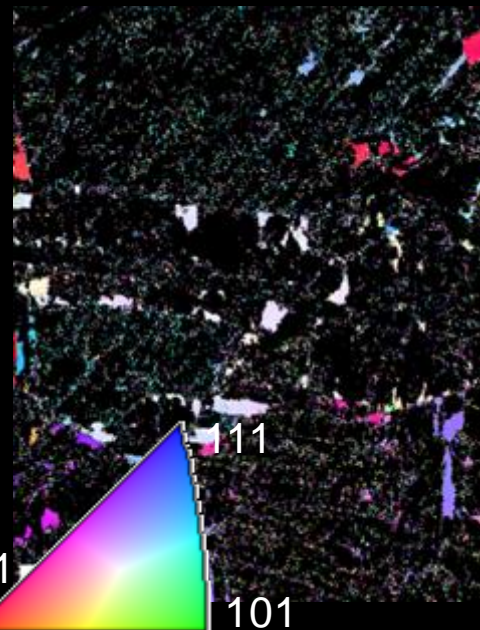
Pt = 1000 s

10 μm

0.27 C - 8.31 Mn -
1.94 Si - 0.24 Mo

AT=875, QT=23 °C, PT=400°C

EBSD: Austenite IPF Maps





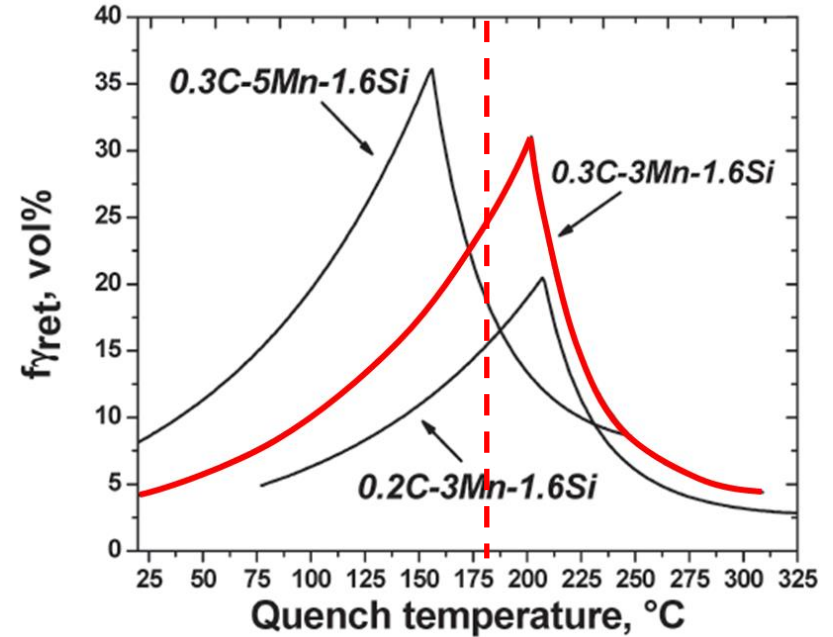
Nanoscale Secondary Ion Mass Spectroscopy (NanoSIMS)

Kyoo Sil Choi, Zihau Zhu, Xin Sun, Emmanuel De Moor, Mark D. Taylor, John G. Speer, and David K. Matlock, "Determination of Carbon Distributions in Quenched and Partitioned Microstructures using Nanoscale Secondary Ion Mass Spectroscopy," Scripta Mater., Vol. 104, 2015, pp.79-82.

NanoSIMS - Experiment



- Steel 0.3C-3Mn-1.6Si
- Q&P
 - Anneal at 830 °C
 - QT = 180 °C (10 s)
 - PT = 400 °C (100 s)
- Assess C distribution in microstructure
- Evaluate with SEM, EBSD, NanoSIMS**

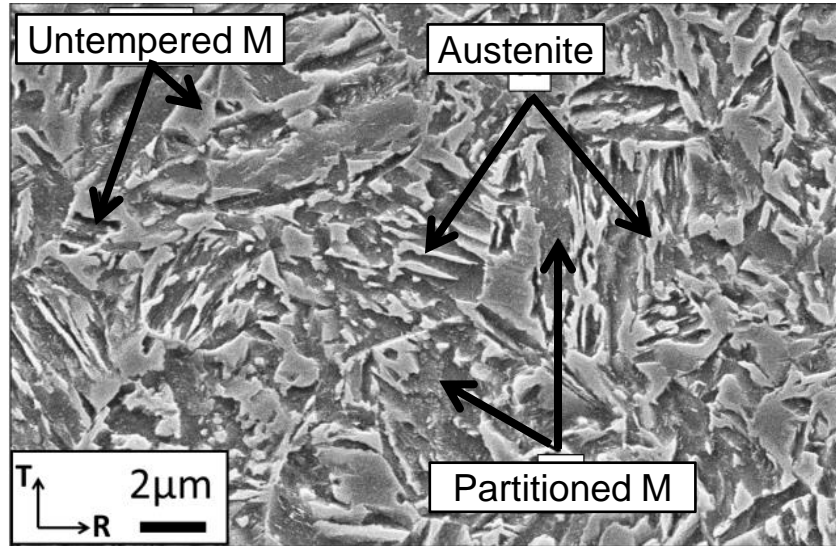


E. De Moor, J.G. Speer, D.K. Matlock, J.H. Kwak, and S.B. Lee, "Effect of Carbon and Manganese on the Quenching and Partitioning Response of CMnSi Steels," *ISIJ Intl.* Vol. 51, no. 1, 2011, pp.137-144.

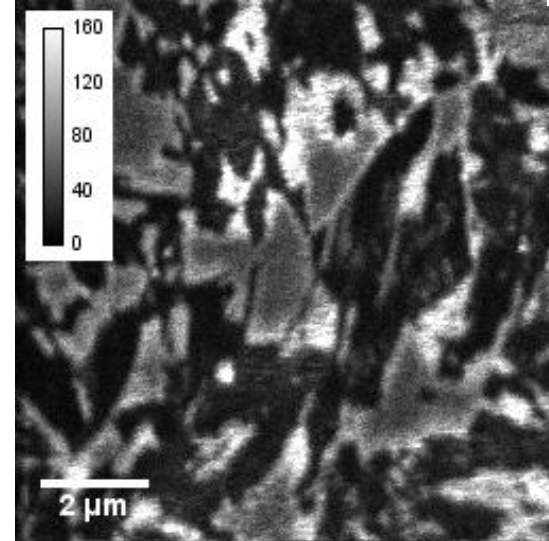
NanoSIMS - Experiment



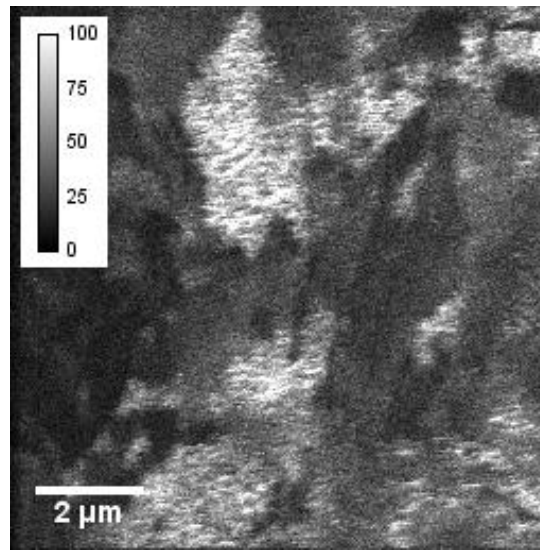
SEM Image (2 pct nital)



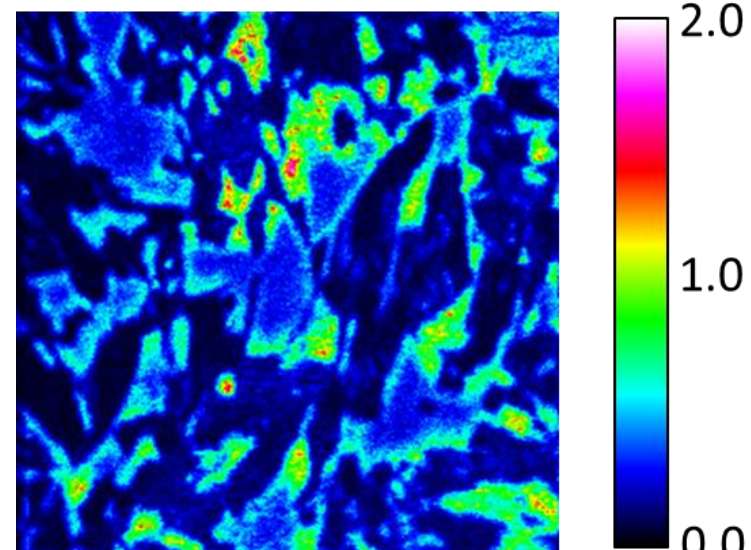
Carbon ($^{12}\text{C}^-$) counts



Silicon ($^{28}\text{Si}^-$) counts



Carbon distribution in wt-%



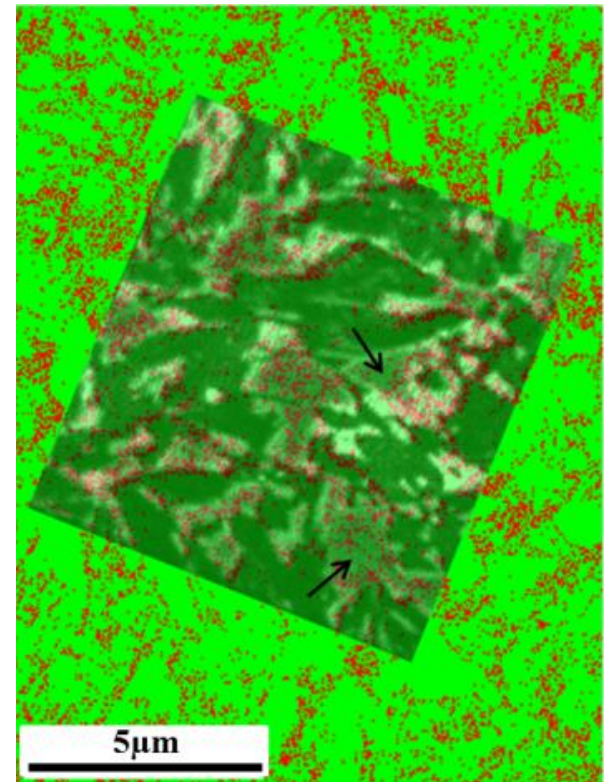
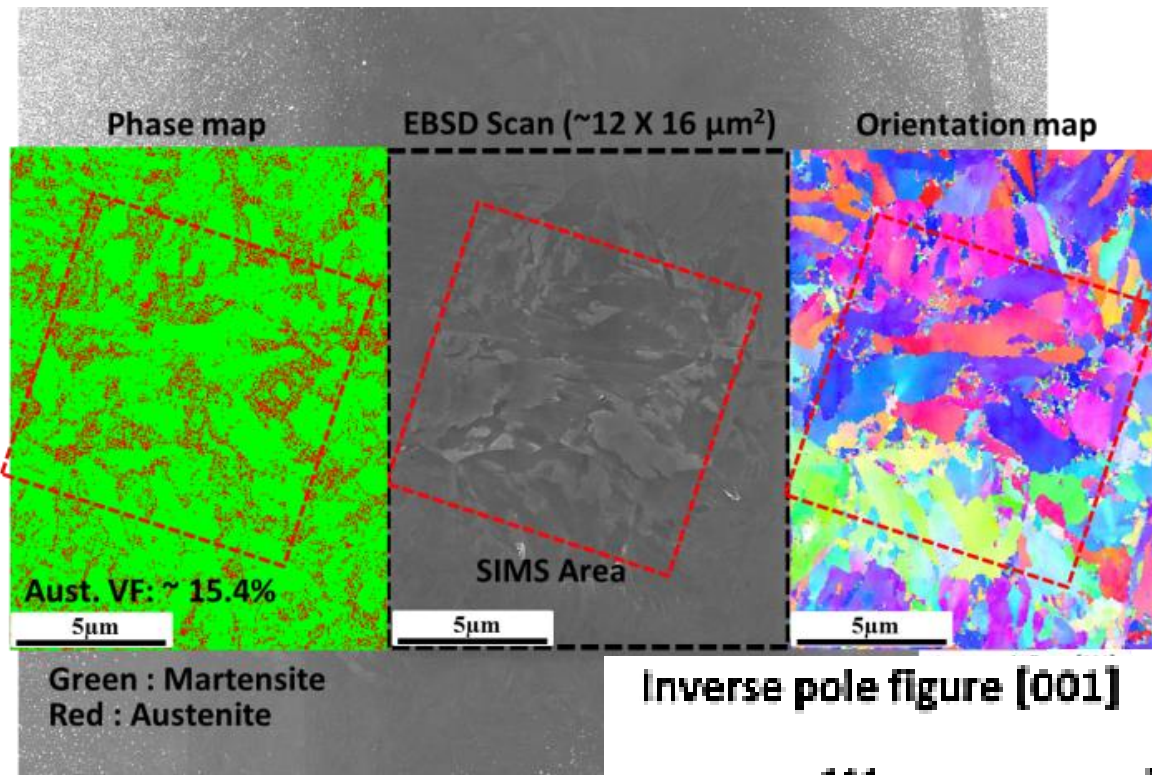
Kyoo Sil Choi, Zihau Zhu, Xin Sun, Emmanuel De Moor, Mark D. Taylor, John G. Speer, and David K. Matlock, "Determination of Carbon Distributions in Quenched and Partitioned Microstructures using Nanoscale Secondary Ion Mass Spectroscopy," *Scripta Mater.*, Vol. 104, 2015, pp.79-82.

NanoSIMS - Experiment

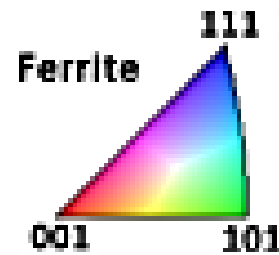
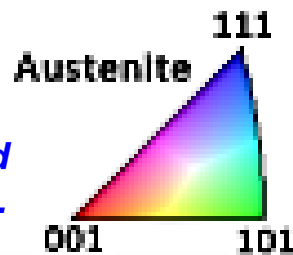


EBSD results for location investigated using Nano-SIMS

Overlay of carbon count image on EBSD phase map



Inverse pole figure [001]



K.S. Choi, Z. Zhu, X. Sun, E. De Moor, M.D. Taylor, J.G. Speer, and D.K. Matlock, "Scripta Mater.", Vol. 104, 2015, pp.79-82.

NanoSIMS Summary



- **Significant carbon enrichment of austenite confirmed**
- **Carbon content of martensite less than bulk**
- **NanoSIMS capable of evaluating C and Si distributions in very fine AHSS microstructures**

Kyoo Sil Choi, Zihau Zhu, Xin Sun, Emmanuel De Moor, Mark D. Taylor, John G. Speer, and David K. Matlock, "Determination of Carbon Distributions in Quenched and Partitioned Microstructures using Nanoscale Secondary Ion Mass Spectroscopy," Scripta Mater., Vol. 104, 2015, pp.79-82.



Mössbauer Spectroscopy: Characterization of Transition Carbides in Q&P Steel

DT Pierce, DR Coughlin, DL Williamson, KD Clarke, AJ Clarke, JG Speer, DK Matlock, E De Moor, "Mössbauer Spectroscopy and Transmission Electron Microscopy Analysis of Transition Carbides in Quenched and Partitioned Steel," Session P07.06, - Metallography and Microstructural Characterization of Metals, Location C123, Thursday, Aug 6 @ 2:15 PM

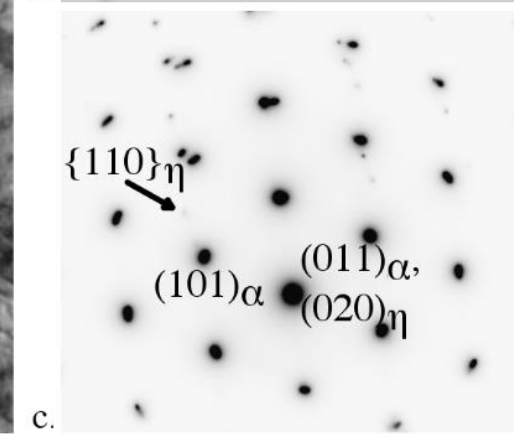
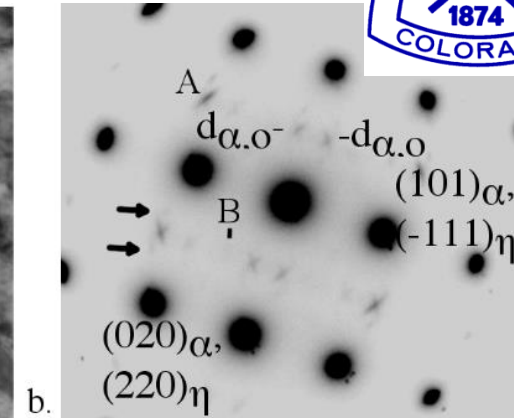
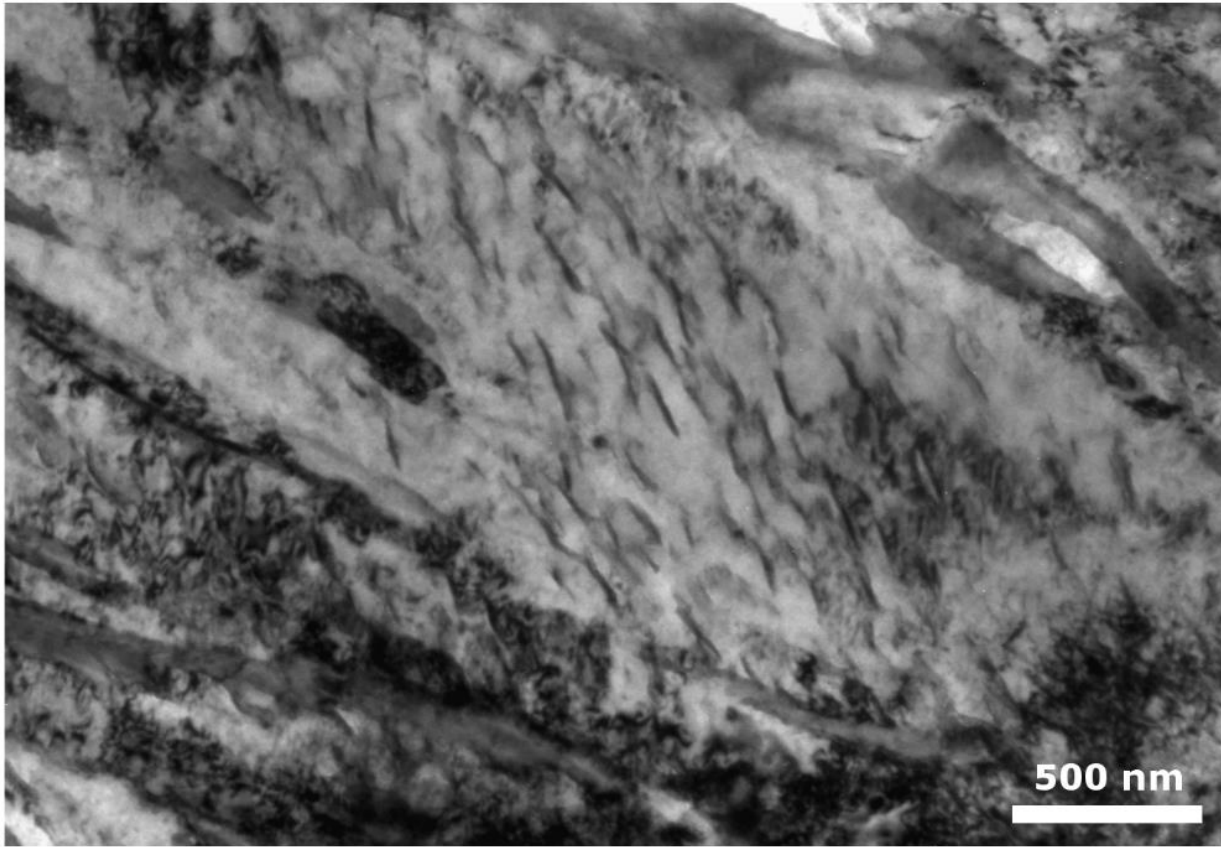
Mössbauer Spectroscopy



- Develop Mössbauer methodology for Q&P
- Characterize evolution of carbide formation during Q&P.
- Mössbauer spectra sensitive to atom nearest neighbors and can be used to assess structure and composition
- Previously applied to binary high-C steels
- Experiment:
 - Evaluate effects of Q&P processing parameters and alloy content

C	Mn	Si	Al	N
0.38	1.54	1.48	0.070	0.0022

TEM Evidence for η -carbide Formation



C	Mn	Si	Al	N
0.38	1.54	1.48	0.070	0.0022

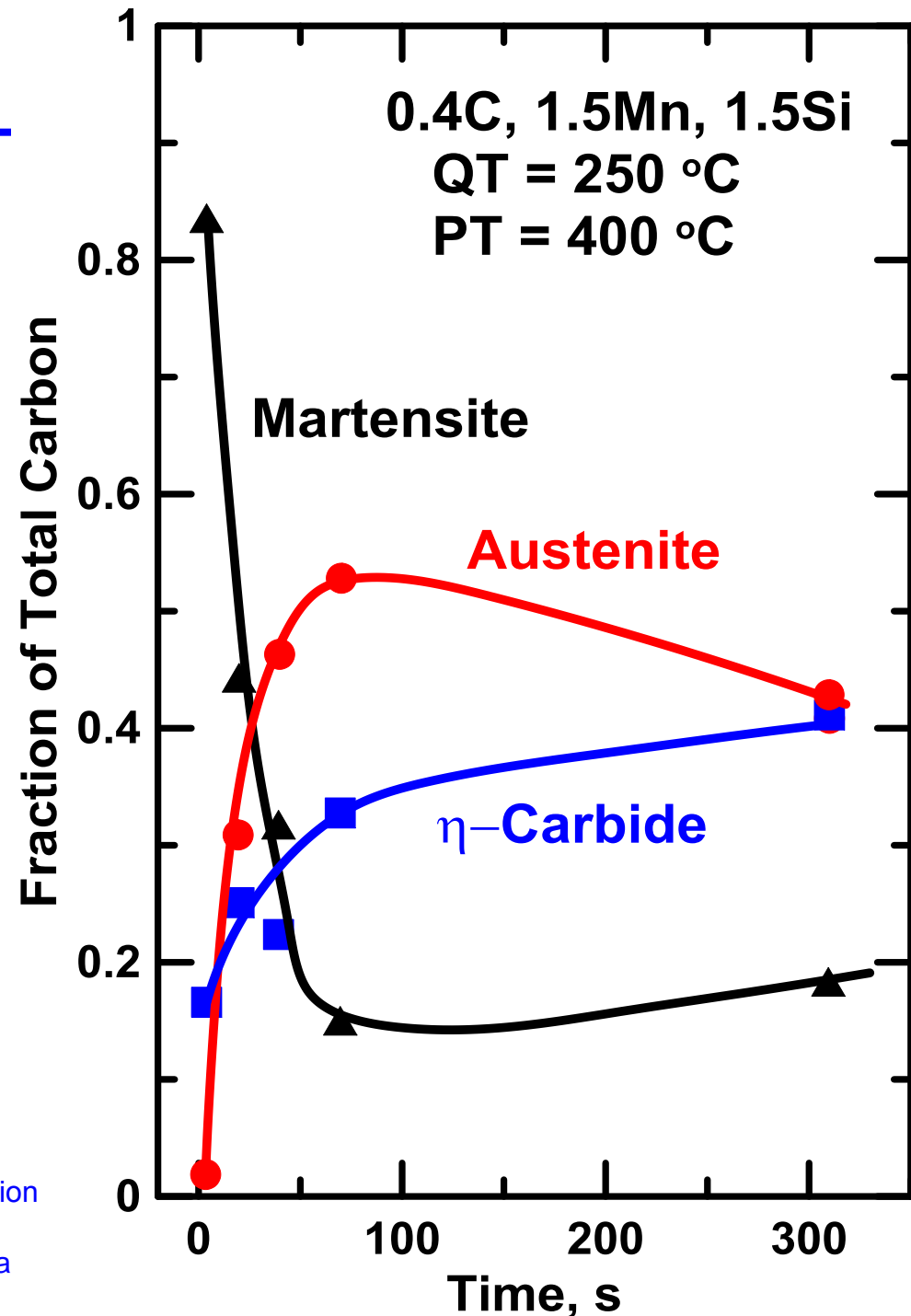
Q&P Processed: QT = 225°C PT = 400°C for 300 s

DT Pierce, DR Coughlin, DL Williamson, KD Clarke, AJ Clarke, JG Speer, DK Matlock, E De Moor, "Mössbauer Spectroscopy and Transmission Electron Microscopy Analysis of Transition Carbides in Quenched and Partitioned Steel," Session P07.06

Mössbauer

- **With partitioning time:**
 - Carbon in martensite decreases
 - Carbon partitioned to austenite
 - Up to 40% of available carbon tied up as η -carbide

C	Mn	Si	Al	N
0.38	1.54	1.48	0.07	0.0022



Mössbauer Summary

- **Significant carbon enrichment of austenite confirmed**
- **η -carbide formation consumes a portion of available carbon**
- **Carbon content of martensite is depleted**

D.T. Pierce, D.R. Coughlin, D.L. Williamson, K.D. Clarke, A.J. Clarke, J.G. Speer and E. De Moor, "Characterization of Transition Carbides in Quench and Partitioned Steel Microstructures by Mössbauer Spectroscopy and Complementary Techniques" *Acta Mater.*, Vol. 90, 2015, pp. 417-430.

DT Pierce, DR Coughlin, DL Williamson, KD Clarke, AJ Clarke, JG Speer, DK Matlock, E De Moor, "Mössbauer Spectroscopy and Transmission Electron Microscopy Analysis of Transition Carbides in Quenched and Partitioned Steel," Session P07.06, - Metallography and Microstructural Characterization of Metals, Location C123, Thursday, Aug 6 @ 2:15 PM



Status Update: AHSS Developments

Government Initiatives and Industrial Commercialization

Integrated Computational Materials Engineering (ICME) Development of Advanced Steel for Lightweight Vehicles

- “...develop 3rd Generation Advanced High Strength Steel (3GAHSS) technology .. Advance ICME techniques to support a reduced development-to-deployment lead time in all lightweight materials systems.”
- \$8.5 million US for 4 years - steel and automobile companies, national laboratories, and universities.

Advanced Manufacturing Office - Innovative Manufacturing Initiative

- CSM received \$1.2 million USD for 3-year program on new Q&P steels

National Network for Manufacturing Innovation

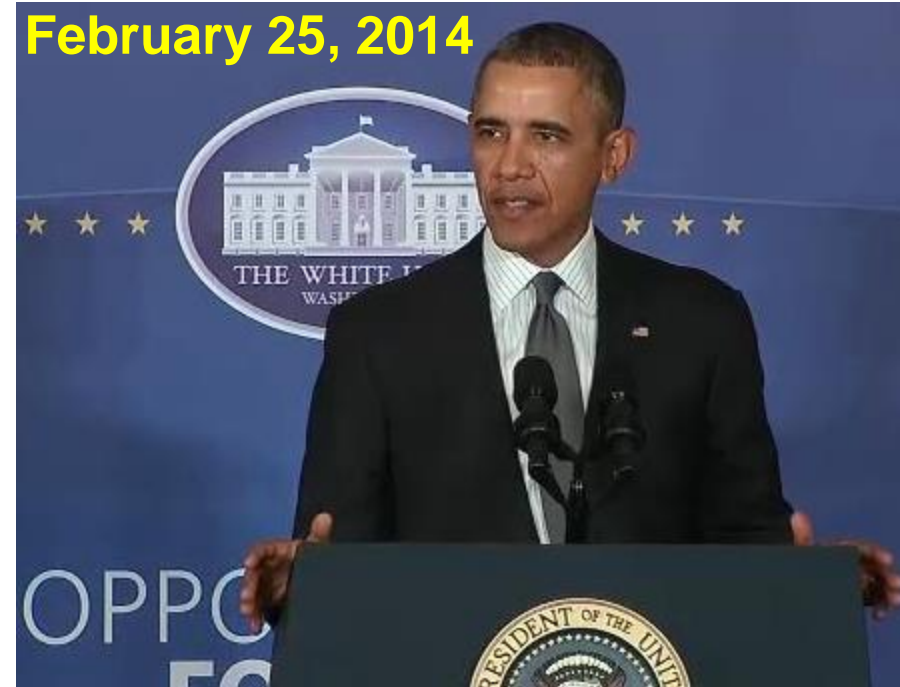
- **Lightweight Modern Metals Manufacturing Innovation (LM3I) Institute**

- **Focus:**
 - **High Strength Steel**
 - **Mg, Ti, Al**
- **\$140M+ for 5 years**



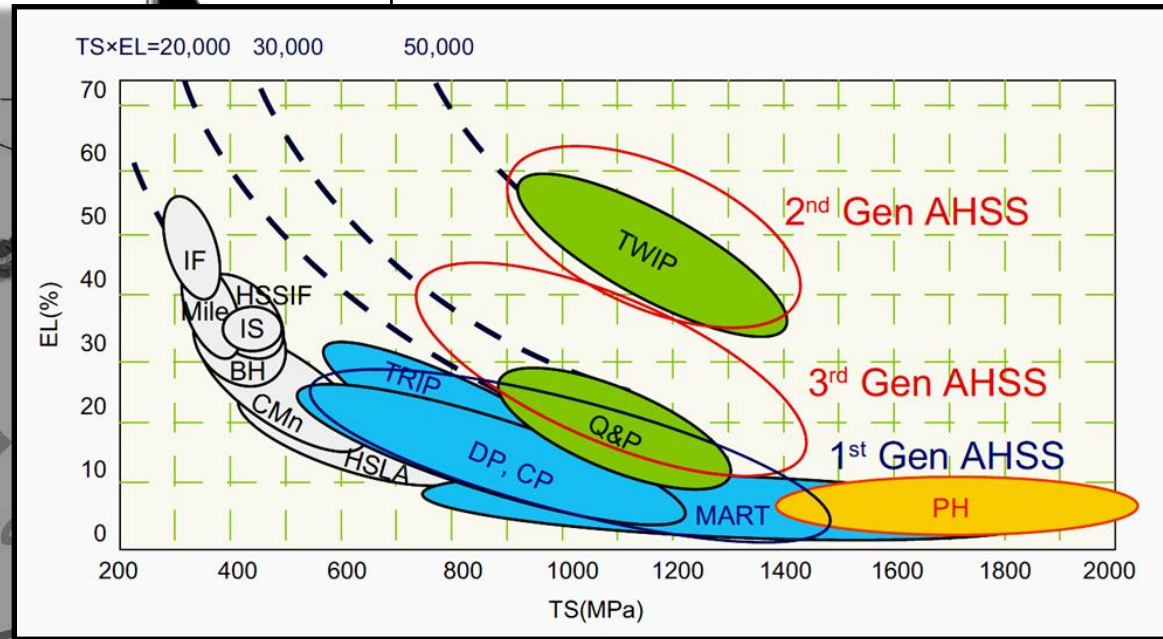
<http://lift.technology/>

A program operated by the American Lightweight Materials and Manufacturing Innovation Institute (ALMMII)



Initial Commercialization

BaoSteel Automotive Advanced High Strength Steels



New Pro-Tec CAL in Leipsic, Ohio



Joint Venture USS/Kobe Opened May 2013

- ***“..state-of-the-art line”***
- ***“...equipped with both advanced water quench ...and rapid gas jet cooling...”***
- ***“...to make next-generation high-strength steel products...”***



ArcelorMittal – July 2015



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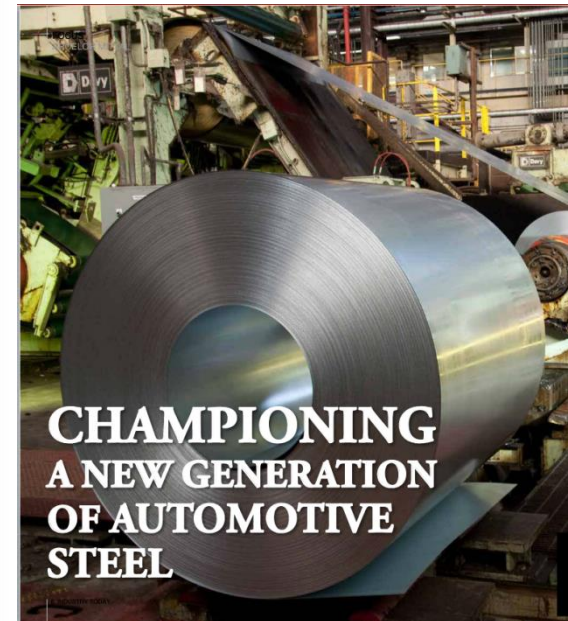
Volume 18, Issue 4

ARCELORMITTAL

Championing a New Generation of Automotive Steel



Preparing for future regulations
Automotive manufacturers face an immense
challenge in the coming years.



“ArcelorMittal ...has been developing new, lightweight solutions using a range of advanced high strength steels (AHSS)”

<http://industrytoday.com/currentissue.asp> (accessed July 2015)

AK Steel – June 2015

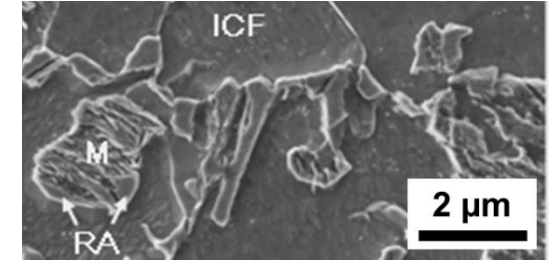
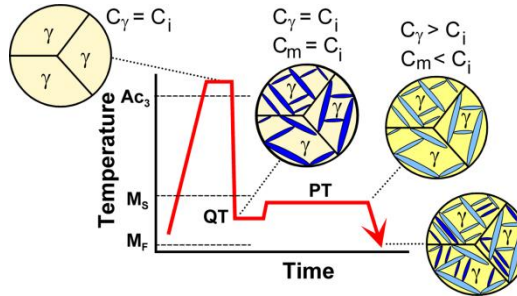
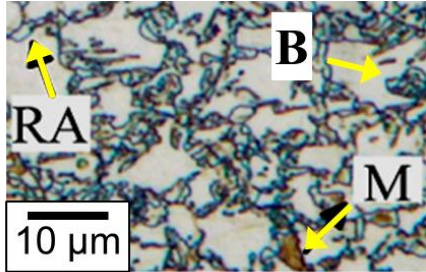


AK Steel to Produce Next-Generation Advanced High Strength Steels: West Chester, OH, June 01, 2015—AK Steel today announced plans to introduce one of the first commercially available Next-Generation Advanced High Strength Steels in the world -- \$29 million project ...at AK Steel's Dearborn Works, using new process technology..

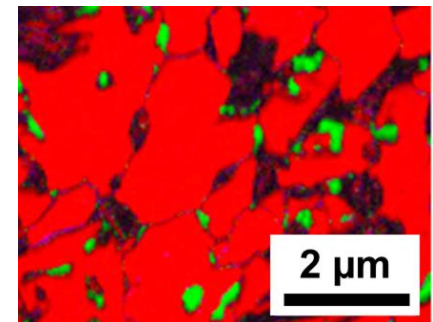
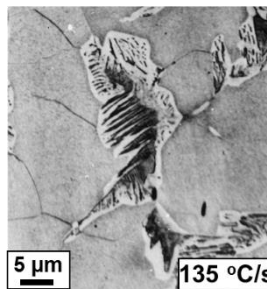
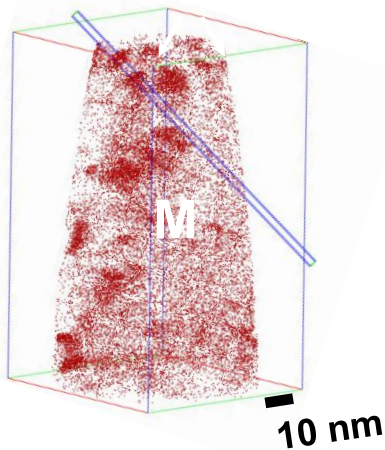
AK Steel Breaks Ground for New World-Class Research and Innovation Center: West Chester, OH, June 19, 2015



Closing Comments



Results based on advanced metallographic techniques provide critical insight to facilitate developments of new AHSS products



Acknowledgements



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- The support of the sponsors of the **Advanced Steel Processing and Products Research Center**, an industry-university cooperative research center at the Colorado School of Mines is gratefully acknowledged