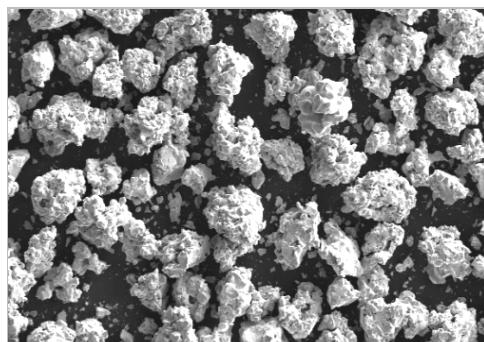
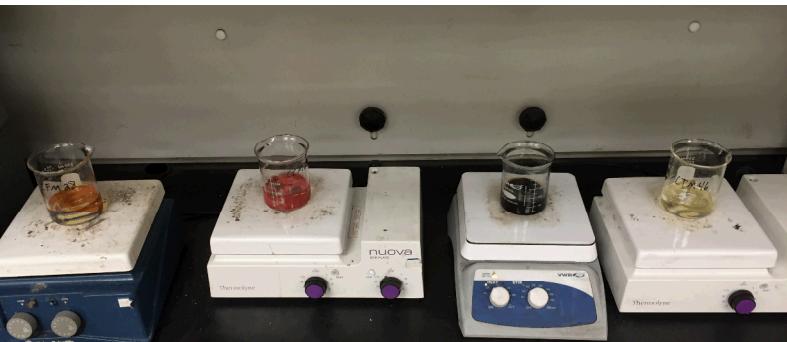


*Exceptional service in the national interest*



# $ABO_3$ (A=La, Ba, Sr, K; B=Co, Mn, Fe) Perovskites for Thermochemical Energy Storage

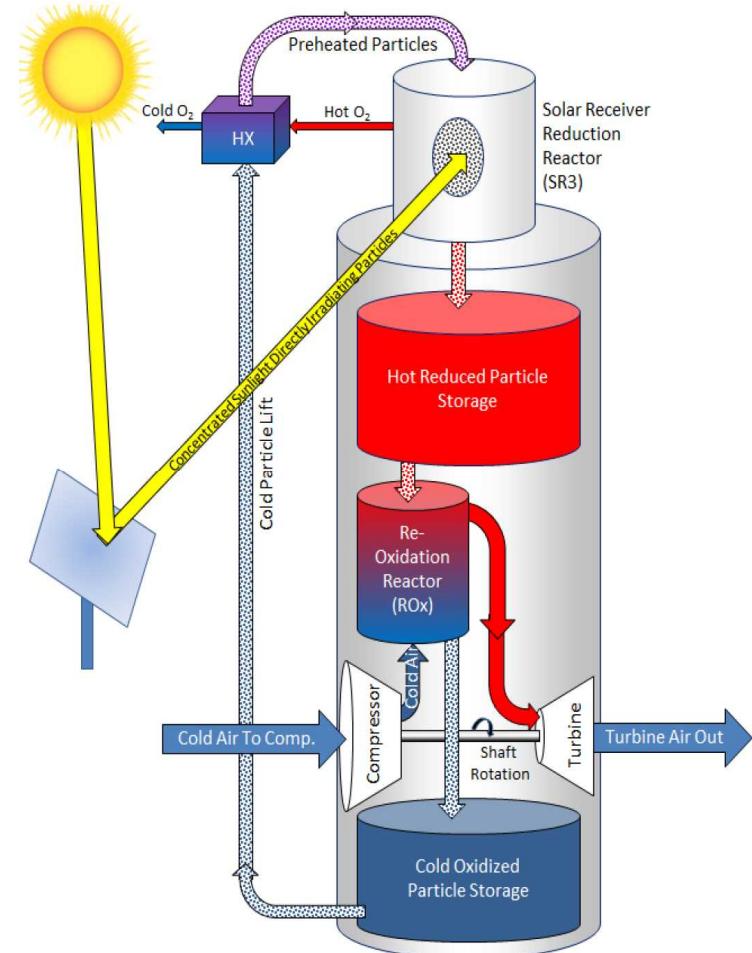
Sean M. Babiniec, Eric N. Coker, Andrea Ambrosini, James E. Miller

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U.S. Department of Energy  
 U.S. DEPARTMENT OF ENERGY  
 National Nuclear Security Administration

Presented by Subhash Shinde

# Thermal storage can be improved by harnessing chemical reactions

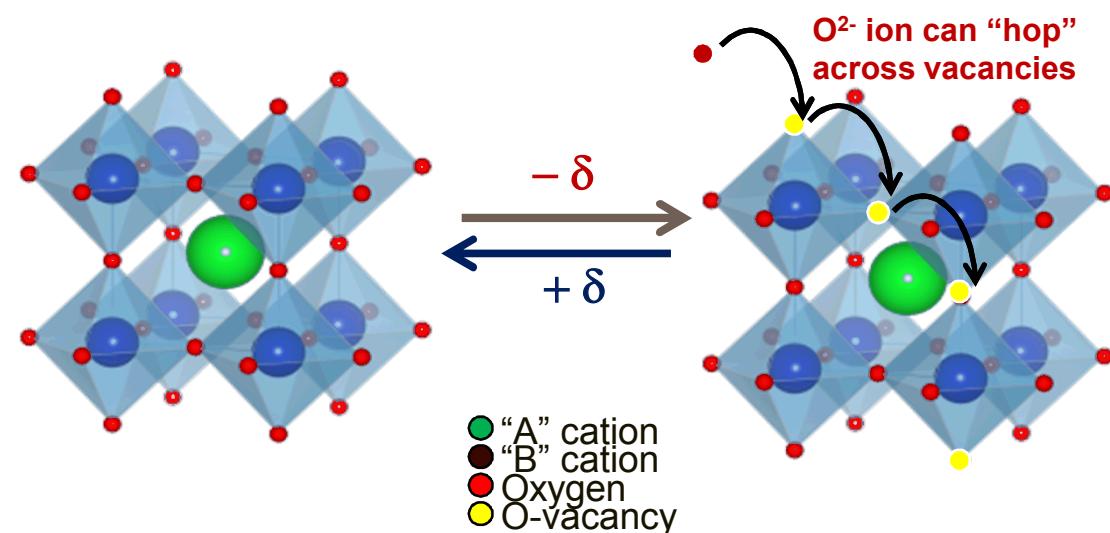
- Current molten-salt storage systems are limited
  - Sensible-only storage, low storage densities
  - Salt decomposition limits turbine operating temperatures
- Solid-particle thermochemical energy storage (TCES) offers many advantages
  - Ability store both sensible and redox reaction enthalpy, resulting in high storage densities
  - Increased storage temperatures potentially supports the use of high-efficiency power cycles
    - Air Brayton inlet  $\geq 1200$  °C
  - Direct irradiation of thermal storage media
  - Re-oxidation reaction can take place directly off compressor outlet



# Materials must be designed to support the operating parameters of new power cycles

- Many Air-Brayton turbines are designed to operate at  $\geq 1200$  °C
- Such temperatures are problematic for existing TCES materials
- Mixed Ionic-Electronic Conducting (MIEC) Perovskites oxides offer a solution for increased storage temperatures
  - $\text{ABO}_3 \leftrightarrow \text{ABO}_{3-\delta} + \delta/2 \text{ O}_2(\text{g})$
  - Continuous reduction reaction allows storage/extraction of heat at high temperatures

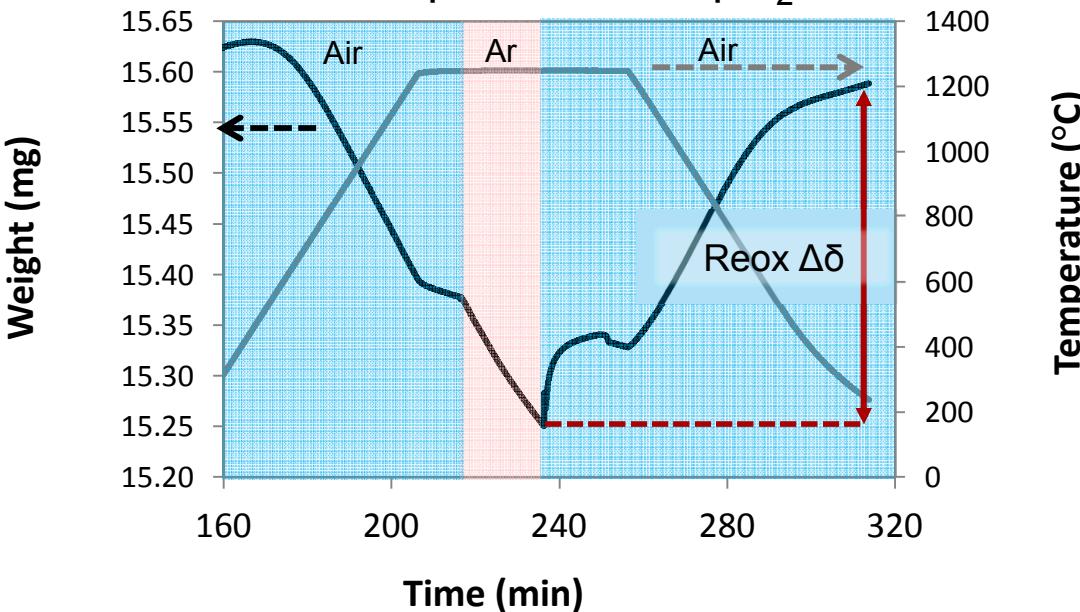
- No crystallographic phase change occurs during redox
- Vacancies facilitate oxide ion transport
- Redox activity continuous over variety of T and  $\text{pO}_2$



# Materials synthesis plan

- Start with known redox active perovskite:  $\text{La}_x\text{Sr}_{1-x}\text{Co}_y\text{Mn}_{1-y}\text{O}_{3-\delta}$  (LSCM)
- Modify promising compositions by A- and B-site cation substitution
  - A = K, Ba, La Sr; B = Fe, Co, Mn
- Initial non-equilibrium thermogravimetric analysis (TGA) used to screen multiple compositions, identify candidates

Mass change measured as a function of temperature and  $\text{pO}_2$



- Reduction occurs during heating to 1250 °C
  - Further reduction observed in argon
- Reoxidation is measured upon switching back to air and cooling to ~200 °C

# LSCF/ LSCM families most promising

Material Composition	Crystallographic Phase	Reduction Onset (°C)	Reoxidation $\Delta\delta$
LSCM1991	Tetragonal	432	0.32
LSCM1982	Tetragonal	438	0.31
LSCM1973	Tetragonal	431	0.28
LSCM2891	Tetragonal	425	0.33
LSCM2882	Tetragonal	256	0.28
LSCM2873	Tetragonal	395	0.31
LSCM3791	Cubic	343	0.39
LSCM3782	Cubic	359	0.36
LSCM3773	Cubic	358	0.31
LSCM4664	Cubic	334	0.24
LSCM7337	Rhombohedral	772	0.01
LSCM8228	Rhombohedral	932	-0.01
LSCM8237	Rhombohedral	972	0.00
LSCM9119	Orthorhombic	825	0.02
LSCM9128	Orthorhombic	834	0.00
LSCM9137	Orthorhombic	901	-0.01

Material Composition	Crystallographic Phase	Reduction Onset (°C)	Reoxidation $\Delta\delta$
LSCF1991	Cubic	406	0.31
LSCF1982	Cubic	394	0.37
LSCF1973	Cubic	372	0.36
LSCF2891	Cubic	369	0.38
LSCF2882	Cubic	357	0.38
LSCF2873	Cubic	366	0.38
LSCF2828	Cubic	340	0.35
LSCF3791	Cubic	352	0.38
LSCF3773	Cubic	348	0.40
LSCF4691	Cubic	342	0.35
LSCF4682	Cubic	332	0.36
LSCF4673	Cubic	336	0.35
LSCF4646	Cubic	349	0.30
LSCF4664	Rhombohedral	342	0.32
LSCF5555	Rhombohedral	500	0.29
LSCF6446	Rhombohedral	609	0.22
LSCF7337	Rhombohedral	736	0.19
LSCF8228	Rhombohedral	926	0.06
LSCF8237	Rhombohedral	886	0.08
LSCF9128	Rhombohedral	1005	0.01
LSCF9137	Rhombohedral	970	0.03

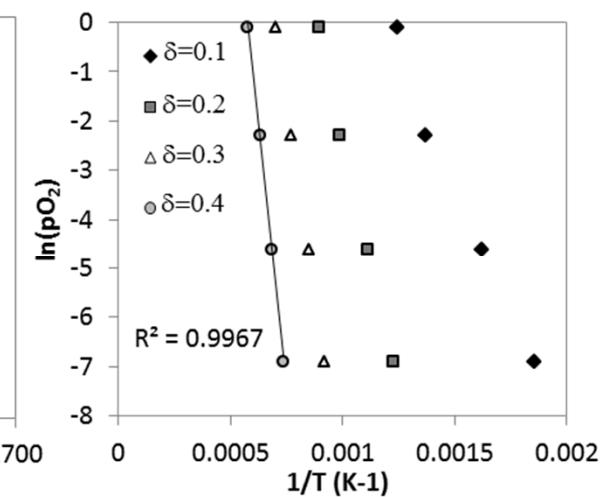
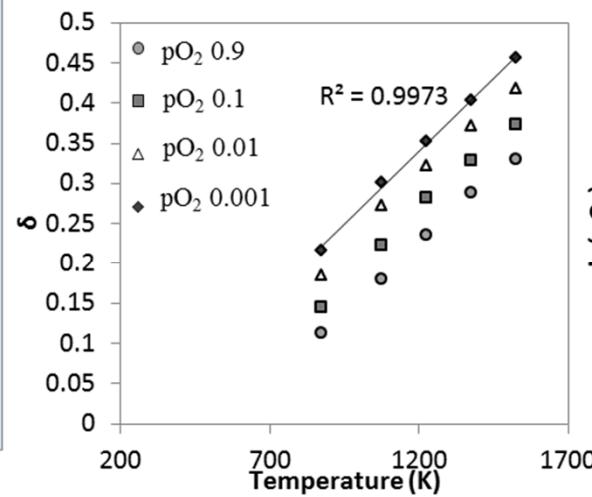
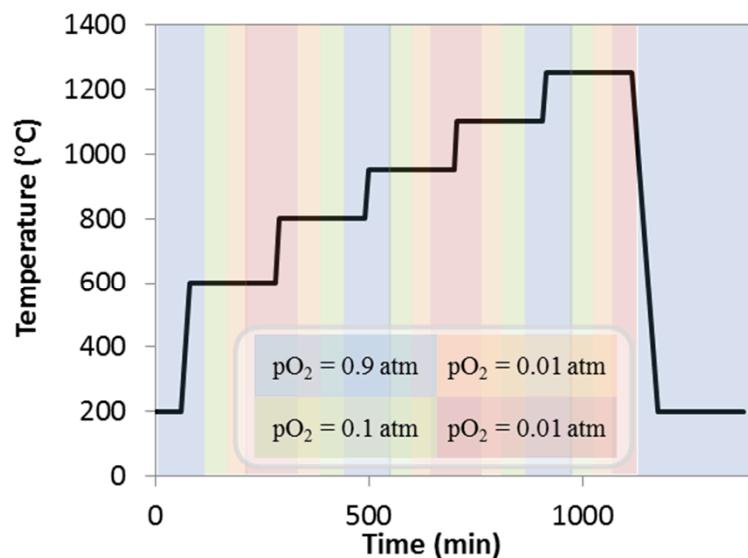
Materials with highest capacity ( $\delta$ ) studied in equilibrium TGA experiment

# High-resolution equilibrium TGA used to estimate thermodynamic parameters

- Thermodynamic parameters extracted by van't Hoff approach:

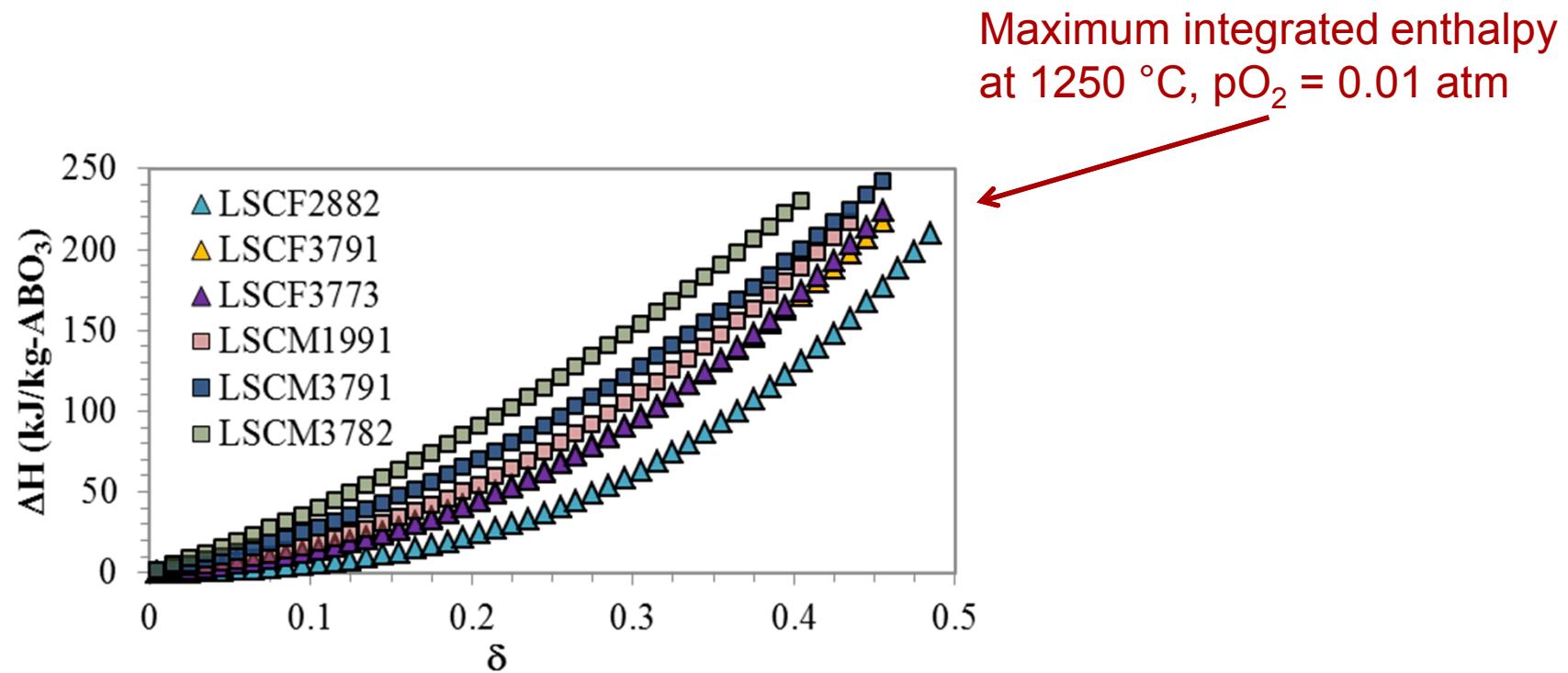
- $$\ln(pO_2) = 2 \frac{-\Delta G_{rxn}}{RT} = 2 \left( \frac{1}{T} \cdot \frac{-\Delta H_{rxn}}{R} + \frac{\Delta S_{rxn}}{R} \right)$$

- Enthalpy determined by slope, entropy by intercept for each value of  $\delta$



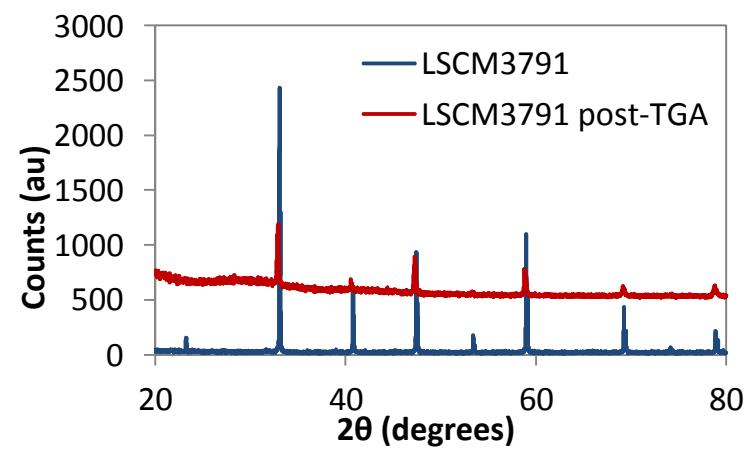
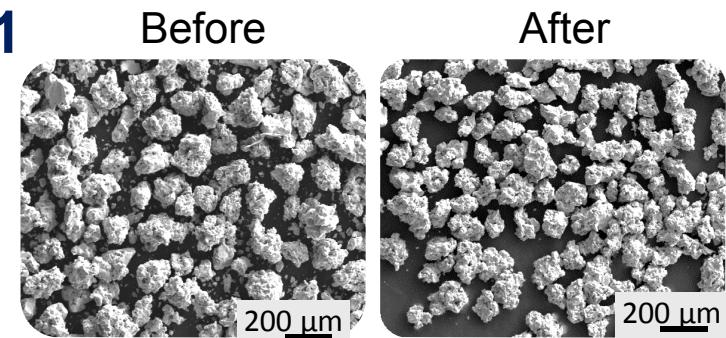
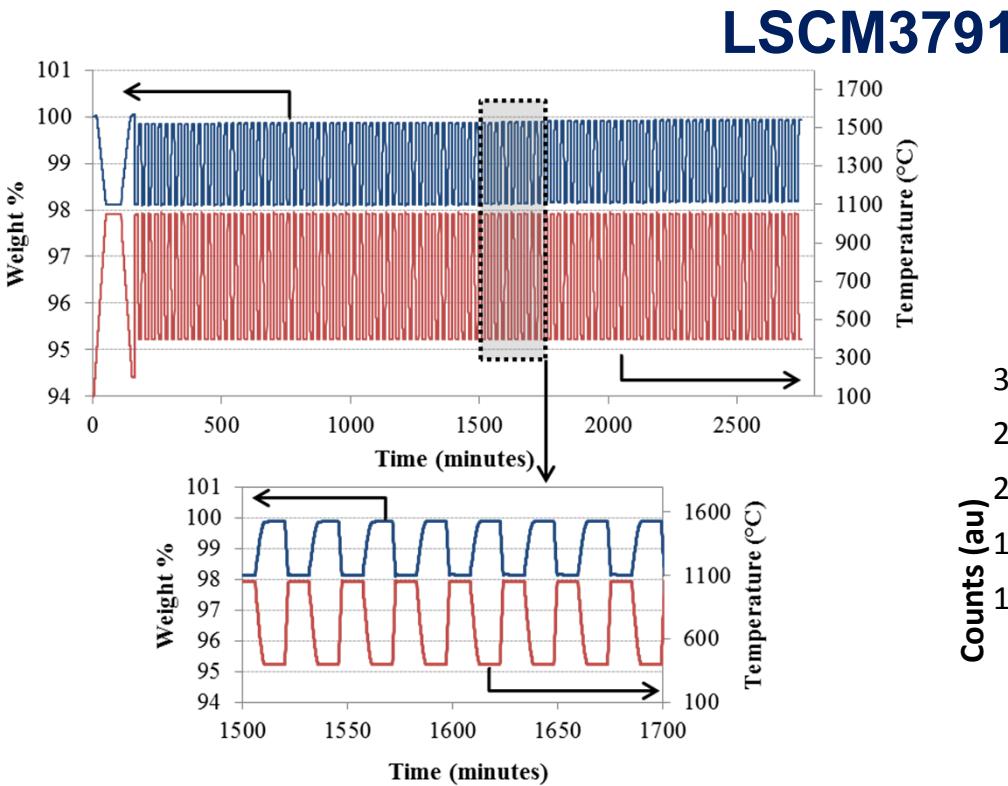
# Reaction energy stored is a function of reaction enthalpy and redox capacity

- Reduction enthalpies indicate a balance between capacity ( $\delta$ ) and enthalpy ( $\Delta H$ ) must be found
- Material with highest measured  $\delta$  has lowest total (integrated) reaction enthalpy, but material with lowest  $\delta$  did not have highest total reaction enthalpy



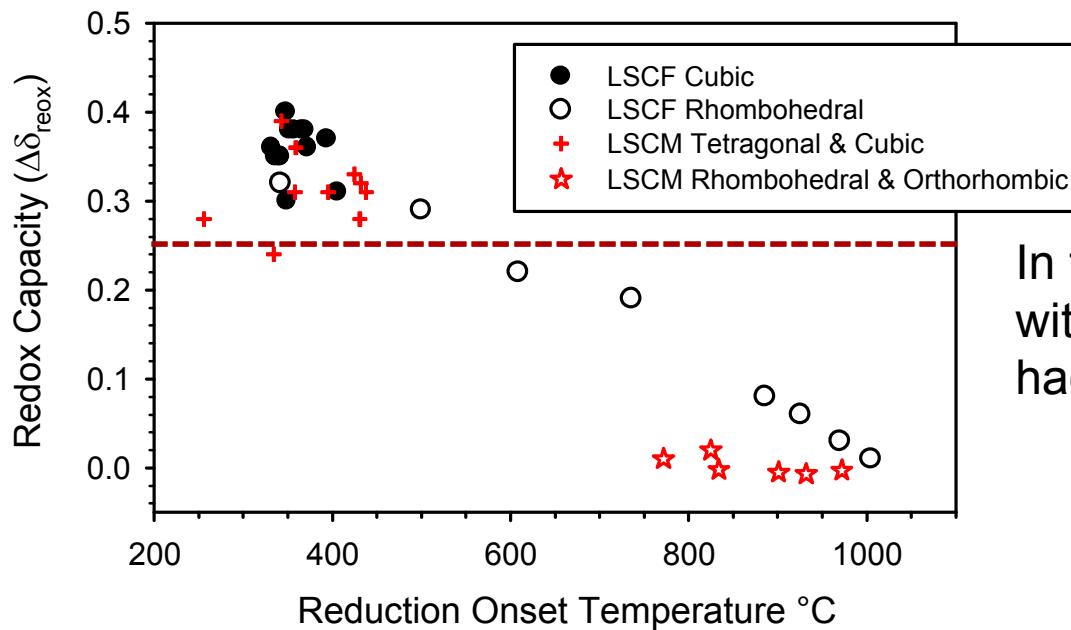
# Characterization of cyclic stability

- Multi-cycle TGA used to measure cyclic repeatability and stability
  - Particles heated to 1050 °C, cooled to 400 °C for 100 cycles
- Scanning electron microscopy shows no change in morphology
- XRD shows no change in crystal phase



# Relationship between enthalpy and reduction temperature

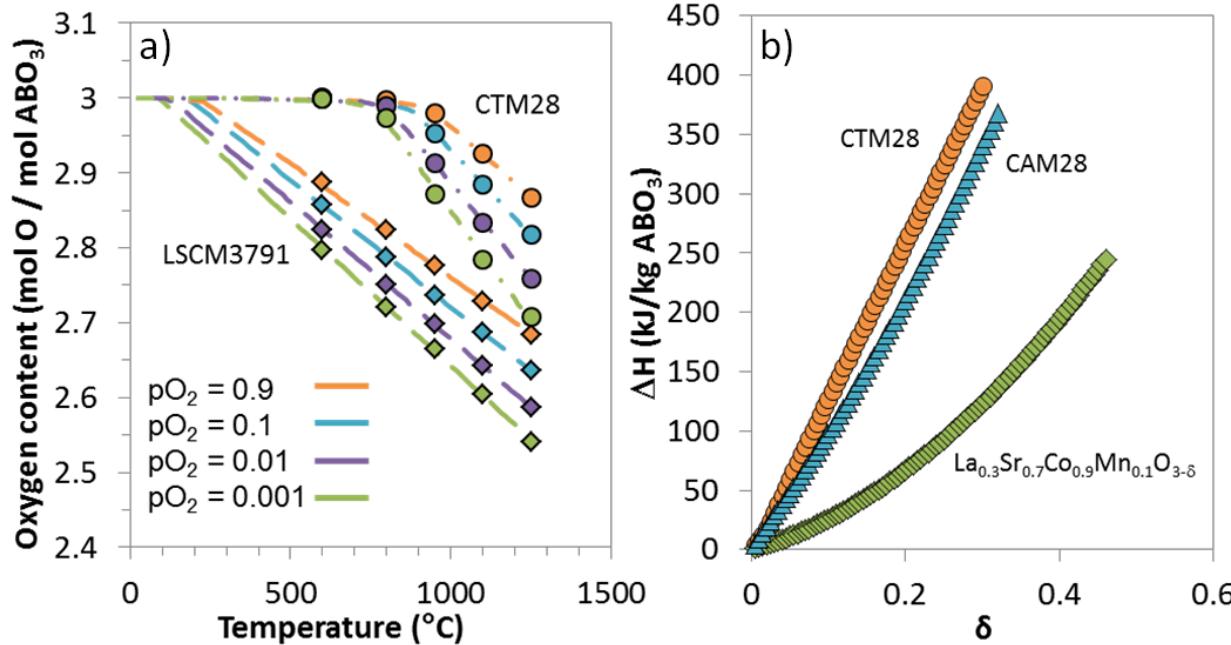
- $\text{ABO}_3 + \Delta H \leftrightarrow \text{ABO}_{3-\delta} + \delta/2 \text{ O}_{2(g)}$ 
  - Gas species dominates entropy term (largest # degrees-of-freedom)
  - $\Delta H$  between two solid compositions likely  $\ll$  entropy in diatomic gas particle
- $\Delta G_{\text{red}} = \Delta H_{\text{red}} - T \Delta s_{\text{red}}$ , where  $\Delta G_{\text{red}} = 0$  is the onset of reduction (equilibrium)
  - For two compositions at equilibrium with nearly equal entropy, a change in reduction enthalpy necessitates a change in reduction temperature



In the LSCX system, materials with high reduction temperatures had low redox capacity ( $\delta < 0.25$ ).

# Next generation:– doped calcium manganese oxides

- Cost
  - Large quantities needed for storage necessitates use of earth-abundant materials e.g., Ca, Ti, Al, Mn
- Performance
  - Higher reduction temperature resulting in higher enthalpy, even with lower capacity



# Conclusions

- The  $\text{La}_x\text{Sr}_{1-x}\text{Co}_y\text{M}_{1-y}\text{O}_{3-\delta}$  ( $\text{M}=\text{Mn,Fe}$ ) perovskites display many of the required characteristics required for high temperature TCES
  - Redox active above 1200 °C
  - Do not degrade when cycled
  - Stable in operating environment
- However, LSCM/LSCF are not optimal
  - Reduction extent is adequate, but reaction enthalpy is low
  - Reduction onset temperature has been identified as a key indicator of reaction enthalpy
- New compositions under development with increased reduction temperature and reaction enthalpy

# Acknowledgements

- We are grateful to Bonnie McKenzie (Sandia National Laboratories) for conducting SEM and providing images, and to Dr. Peter Loutzenhiser (Georgia Institute of Technology) and Dr. Ellen Stechel (Arizona State University) for technical discussions.
- Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.
- This work was supported by the U.S. Department of Energy SunShot initiative under award number DE-FOA-0000805.



# National Solar Thermal Test Facility

## Parabolic Trough R&D



## PV System Reliability



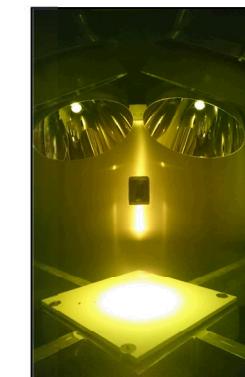
## Dish Stirling R&D



## Thermal Energy Storage R&D



Optics Lab



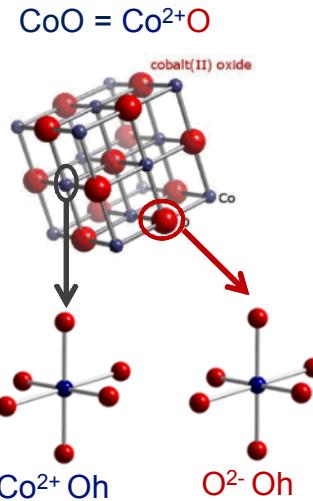
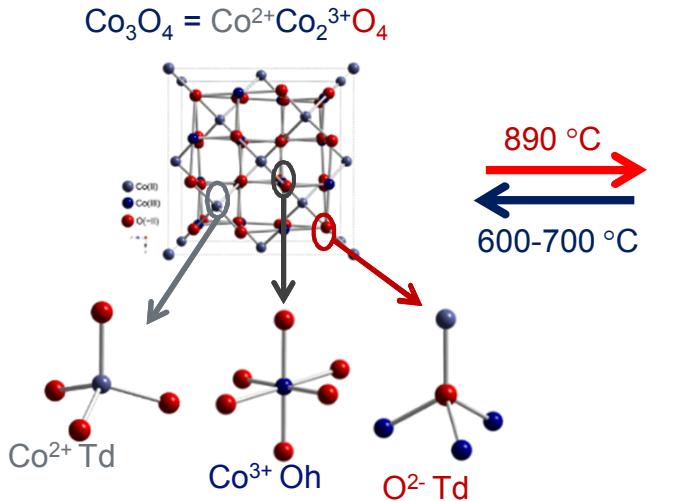
Receivers and Heliostats



Solar Fuels and Selective Absorbers

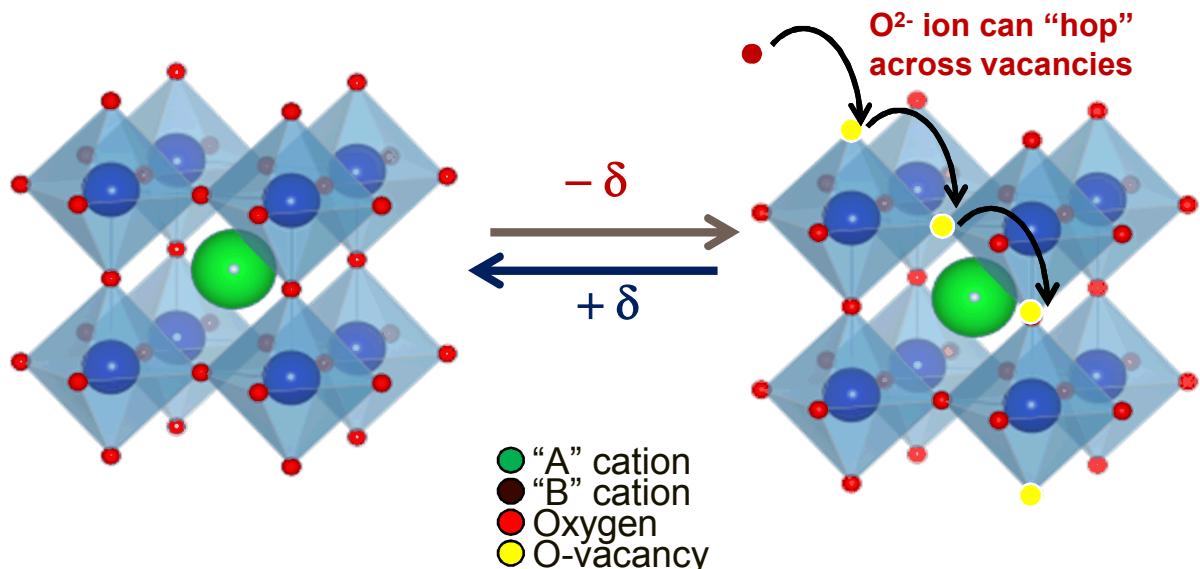
# SUPPLEMENTARY SLIDES

# State of the Art MO vs. Perovskites



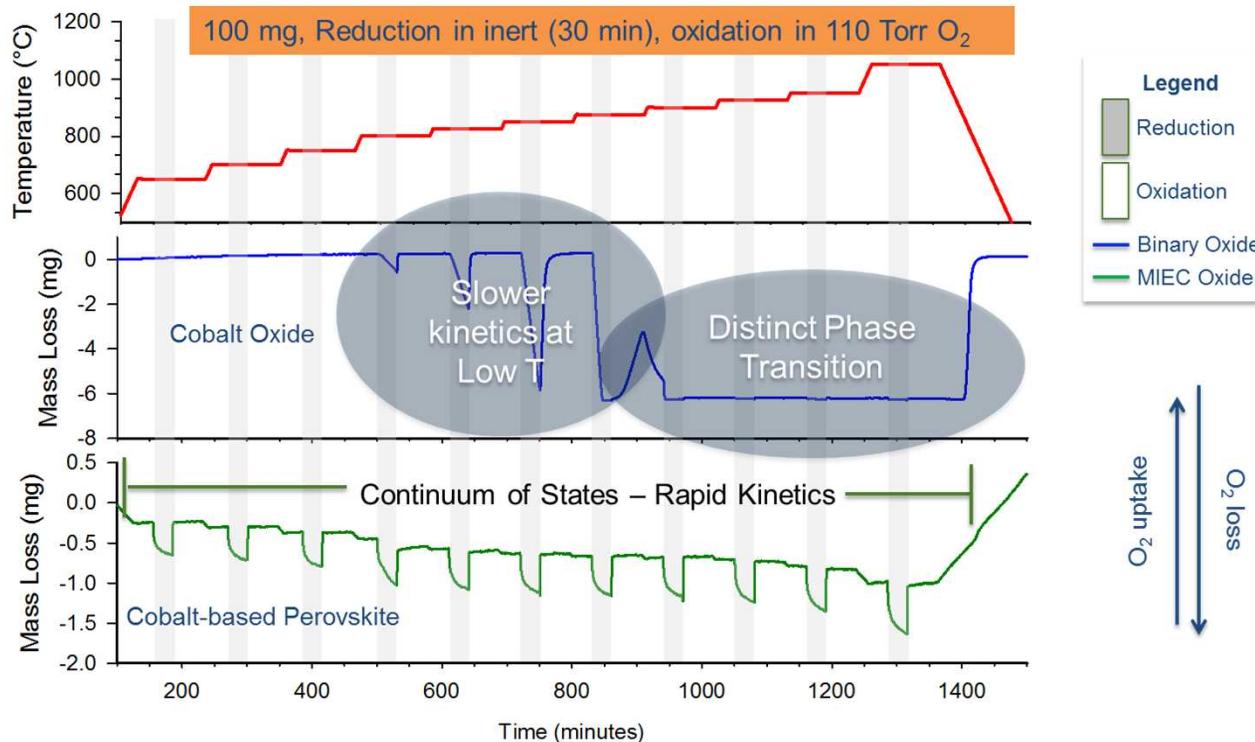
- Energetic crystallographic phase change at redox
- Structure not amenable to oxide ion transport
- Oxidation exotherm typically recovered at lower temperature than reduction

- No crystallographic phase change occurs during redox
- Vacancies facilitate oxide ion transport
- Redox activity continuous over variety of T and  $\text{pO}_2$



# Perovskites offer a solution to increasing turbine inlet temperatures to $\geq 1200$ °C

- Continuous reduction behavior as opposed to discrete reaction
  - Perovskite  $\text{ABO}_3 \leftrightarrow \text{ABO}_{3-\delta} + \delta/2 \text{O}_2(\text{g})$

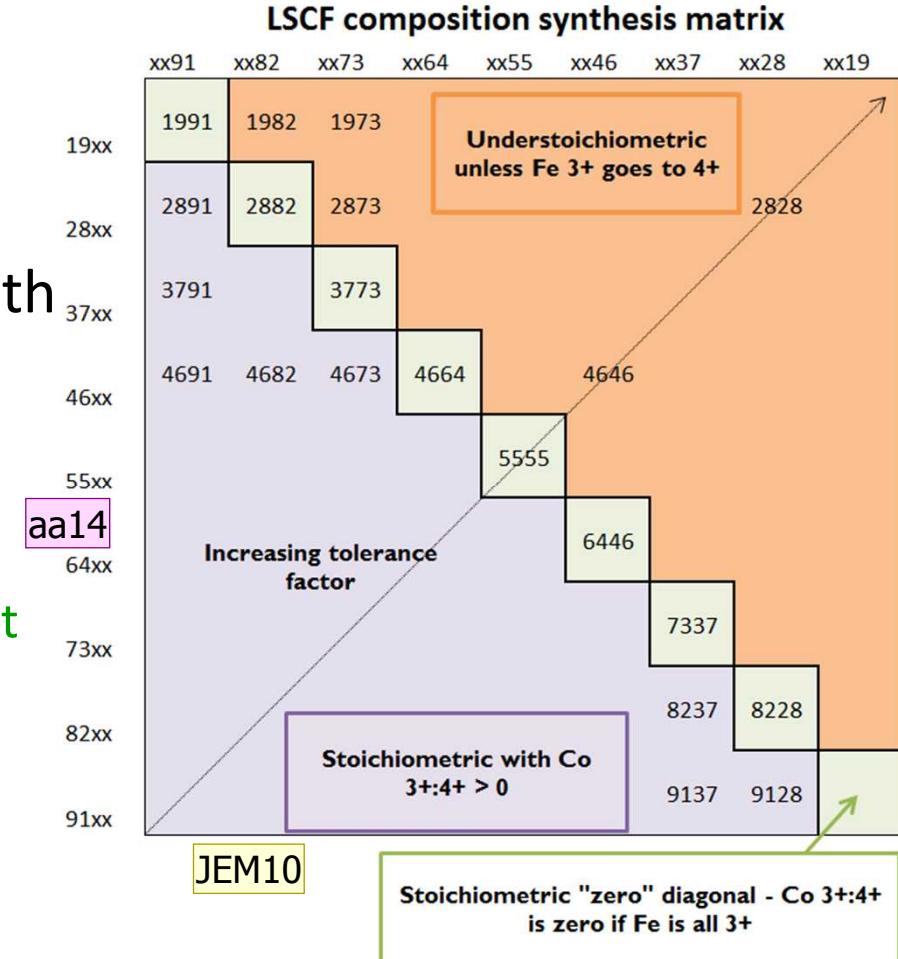


- Perovskites need to be engineered to increase capacity (mass loss) and reaction enthalpy

# Materials synthesis plan



- Start with known redox active perovskite:  $\text{La}_x\text{Sr}_{1-x}\text{Co}_y\text{Mn}_{1-y}\text{O}_{3-\delta}$  (LSCM)
- $\text{La}_{0.a}\text{Sr}_{0.b}\text{Co}_{0.c}\text{Fe}_{0.d}\text{O}_{3-\delta} = \text{LSCFabcd}$ 
  - Example:  $\text{La}_{0.3}\text{Sr}_{0.7}\text{Co}_{0.2}\text{Mn}_{0.8}\text{O}_{3-\delta} = \text{LSCM3728}$
- Modify promising compositions with A- and B-site cations
  - A-site: Ba, K; B-site:  $\text{Fe}, \text{Mn}^{\text{aa}17}$
- Example: LSCF synthesis matrix
  - Focused on compositions with highest reduction capacity
    - Diagonal, B-site fully at 4+
  - ~~Probed other regions of interest~~



## Slide 17

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**JEM10** Maybe make this more compact and bulletized

James E. Miller, 9/23/2015

**SMB4** Should we state here that the LSCM and B-site substituted LSCF were the most promising compositions, and just move on from Ba and K? It is hard to incorporate them without adding unnecessary slides and we can just reference the viewer to the manuscript.

Babiniec, Sean Michael, 9/24/2015

**aa5** We could. Limited time--no need to dwell.

Andrea Ambrosini, 9/24/2015

**aa14** Don't keep this green. (Not sure if it was just for highlighting change purposes.)

Andrea Ambrosini, 10/5/2015

**aa17** Is there a reason Fe is bold?

Andrea Ambrosini, 10/5/2015