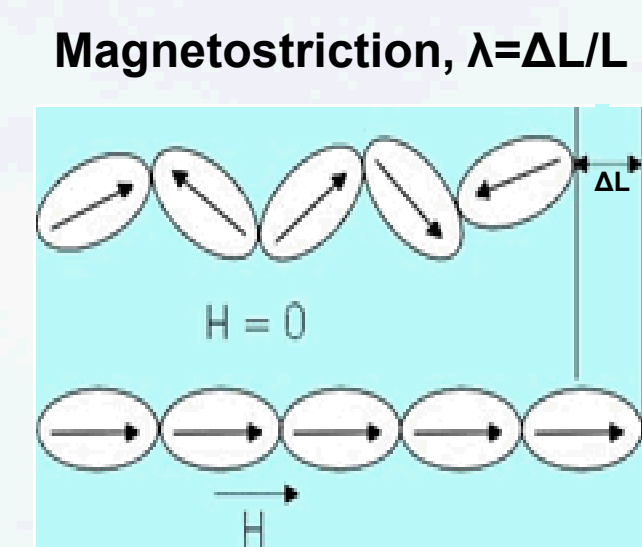


Todd C. Monson<sup>1\*</sup>, Eric Langlois<sup>1</sup>, Jamin R. Pillars<sup>1</sup>, Christian L. Arrington<sup>1</sup>, Andrew E. Hollowell<sup>1</sup>, Patrick S. Finnegan<sup>1</sup>, Christopher B. DiAntonio<sup>1</sup>, Tom P. Chavez<sup>1</sup>, Baolong Zheng<sup>2</sup>, Yizhang Zhou<sup>2</sup>, Enrique Lavernia<sup>2</sup>  
<sup>1</sup>Sandia National Laboratories, Albuquerque, NM, USA, <sup>\*</sup>Email: tmonson@sandia.gov, <sup>2</sup>University of California, Irvine, CA, USA

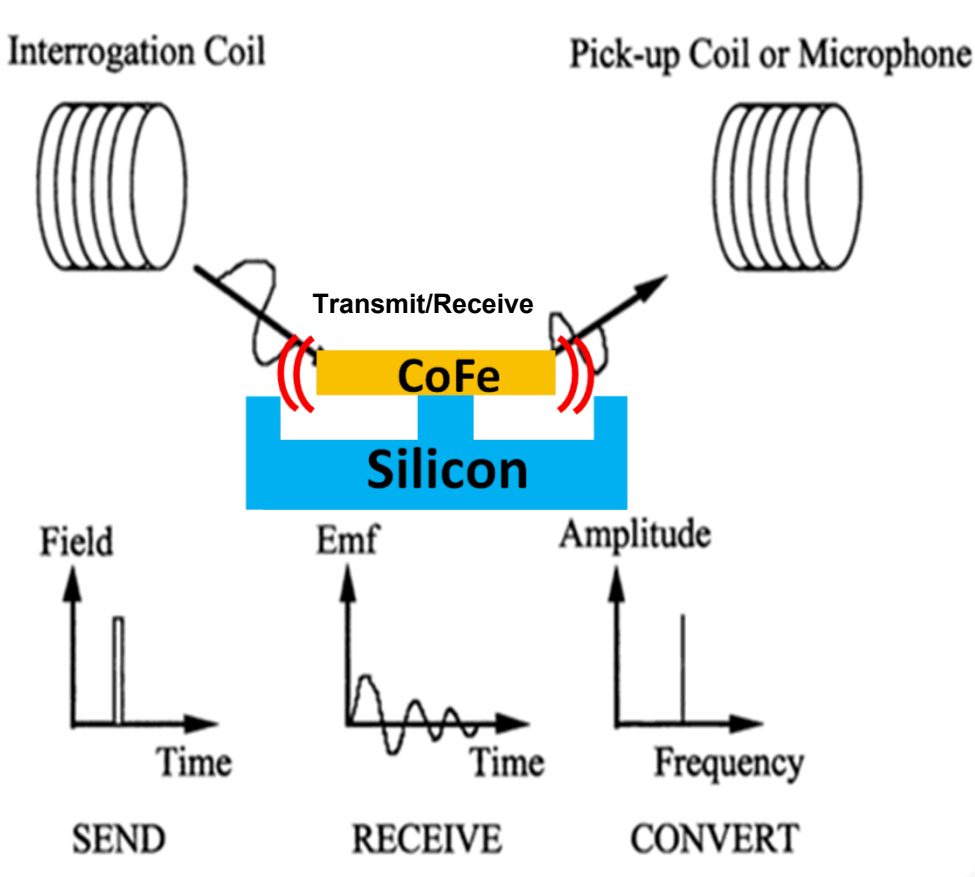
## CoFe Micro Magnetoelastic Resonators for Smart Sensors and Tags

Electrodeposited, highly magnetostrictive, CMOS compatible, rare earth, and oxide free CoFe alloys

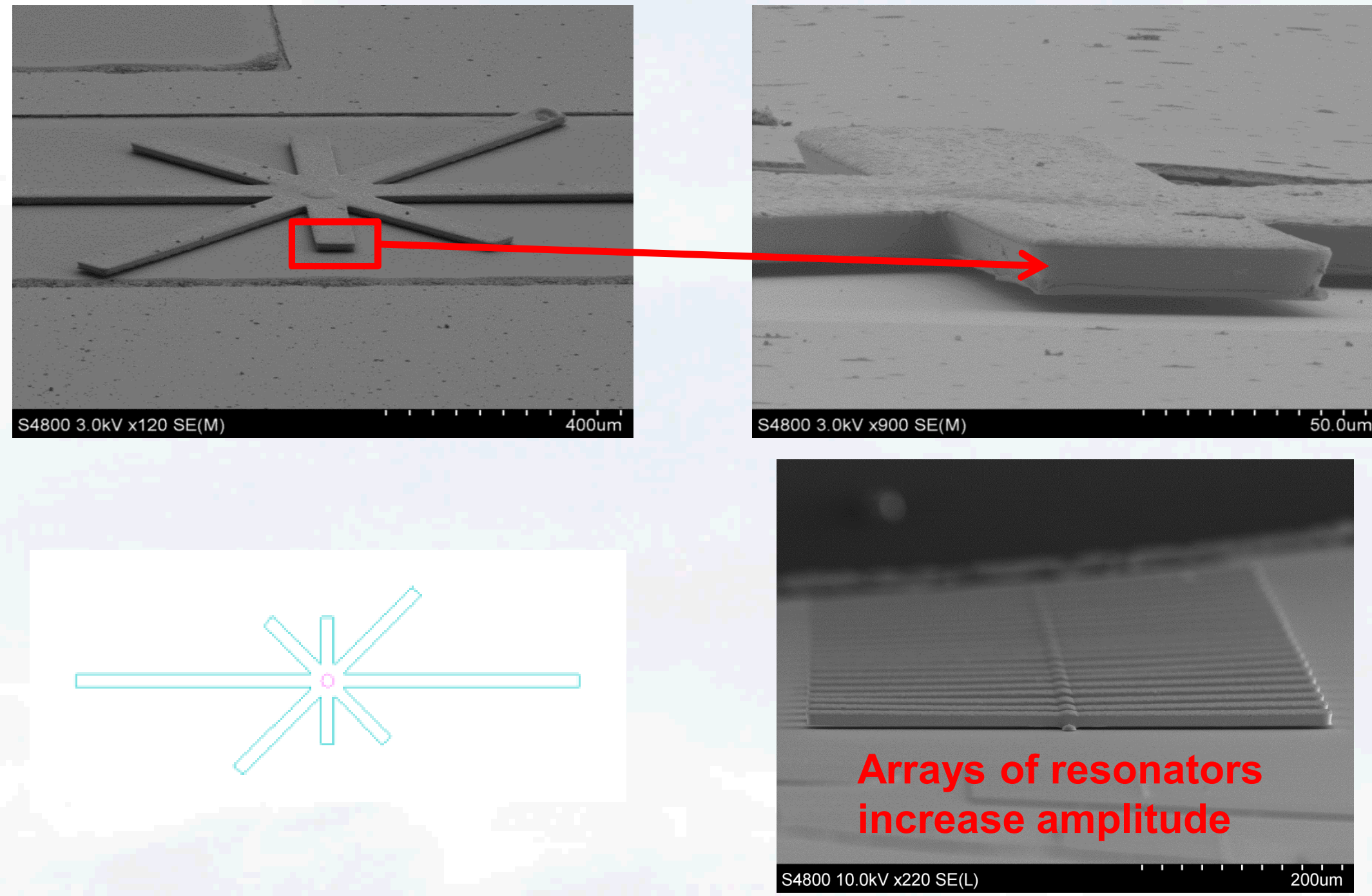


Magnetoelastic Material	$\lambda_s$ (ppm)
Metglas 2605SA1	$26 \pm 4$
CoFe plated on Cu	$172 \pm 25$
CoFe plated on Au	$229 \pm 32$

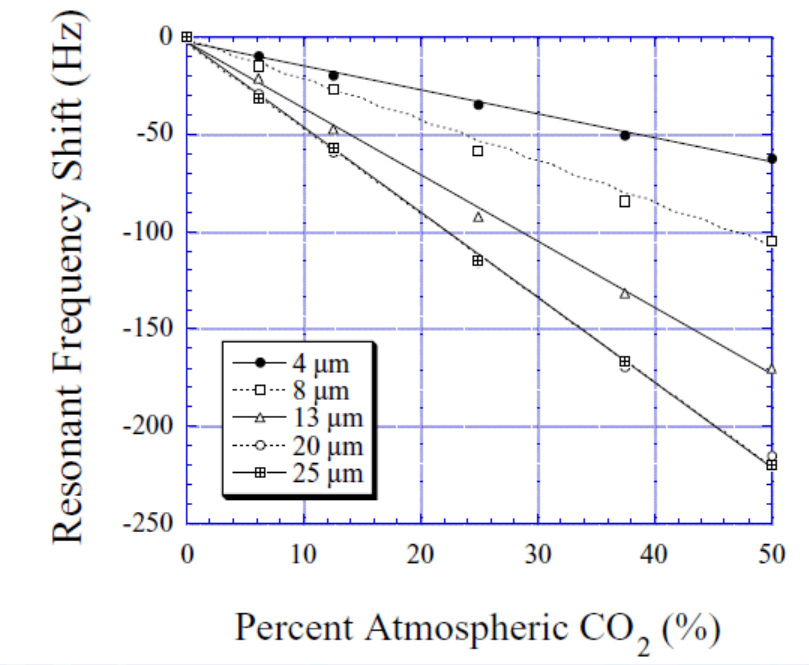
### Tag/Sensor method of operation



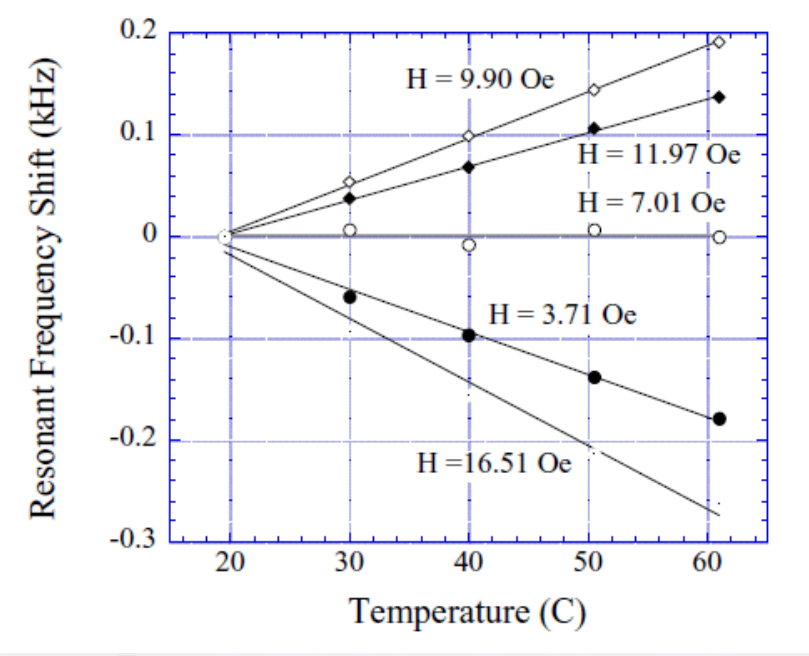
### First demonstration of electroplated CoFe released micro resonators



### Gas sensing



### Temperature sensing



**“Dumb Tag”**

**“Smart Tag”**

a) Single frequency resonator  
b) Multi-Frequency resonator (3)

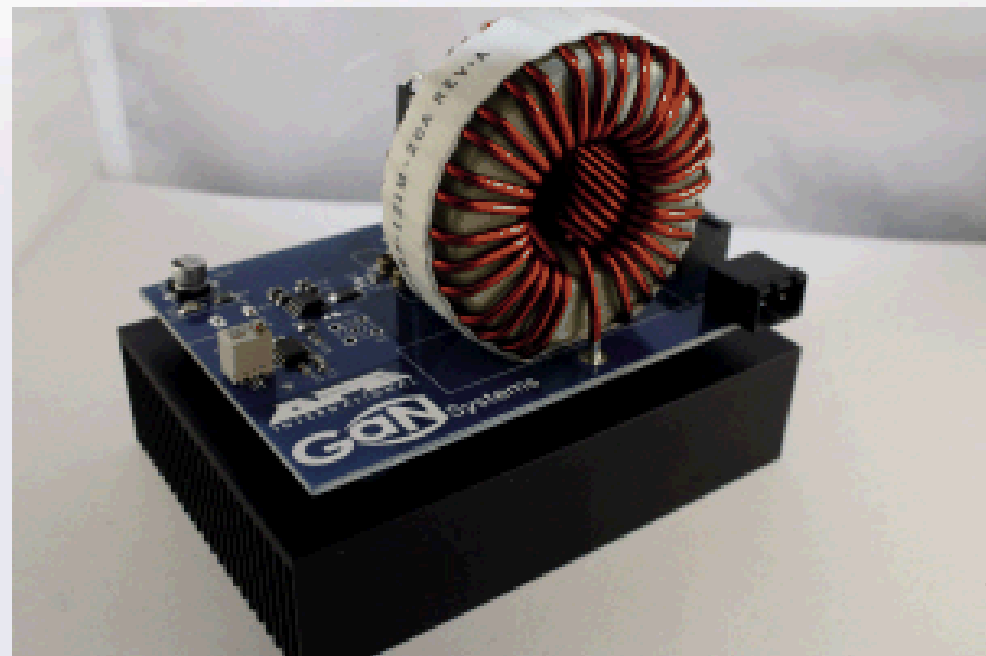
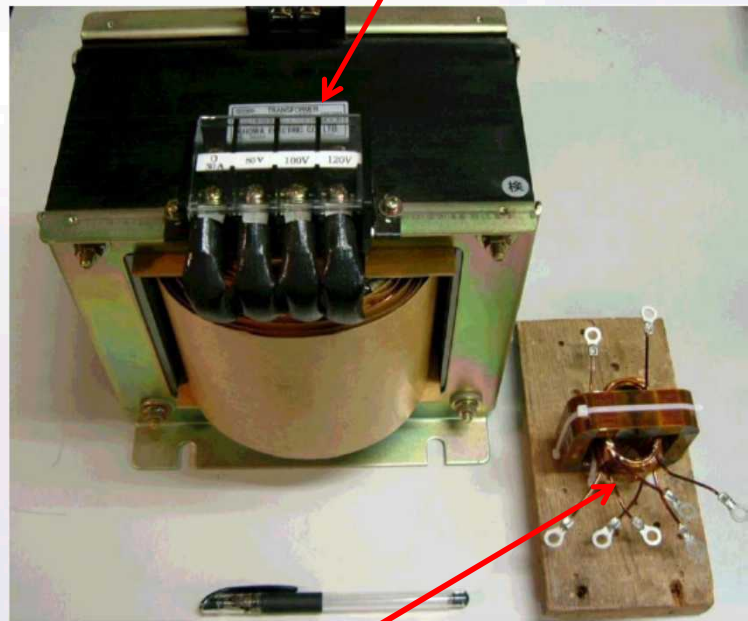
$$f_r = \frac{1}{2L} \left[ \frac{\rho}{E_0} + \frac{9\lambda_s^2 \rho (|H_B| \cos(\beta))^2}{J_s H_A^3} \right]^{-1}$$

$N_K$  = # labels  
 $N_T$  = # resonator types  
 $N_R$  = # resonators  
 $N_W$  = # possible angles

✓ millions of different coded sensors  
 ✓ Centimeter scale tags

## $\gamma'$ -Fe<sub>4</sub>N Soft Magnetic Materials for High Power and High Frequency Transformers and Inductors – First ever bulk $\gamma'$ -Fe<sub>4</sub>N materials and devices!

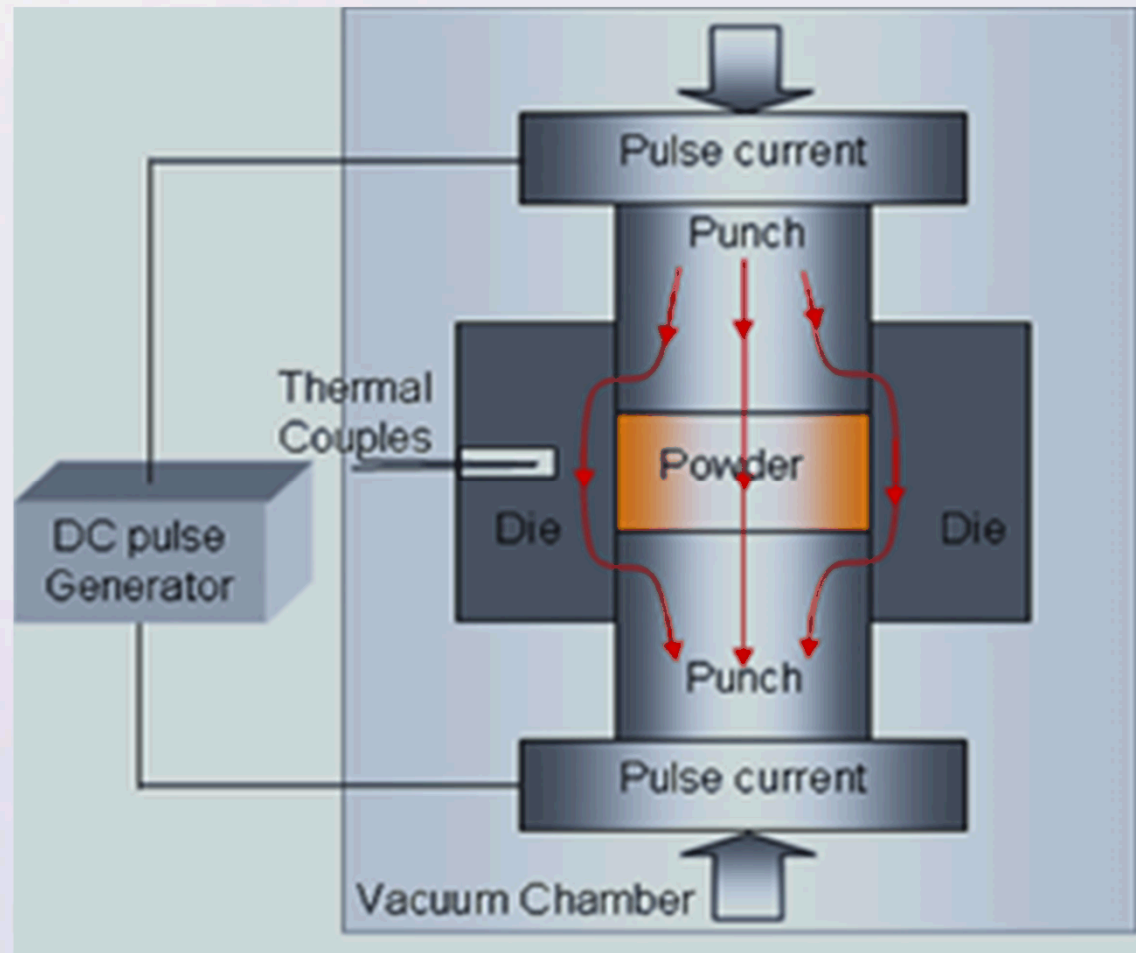
Line frequency (50 Hz) transformer



High frequency (20 kHz) transformer

S. Krishnamurthy, Half Bridge AC-AC Electronic Transformer, IEEE, 1414 (2012).

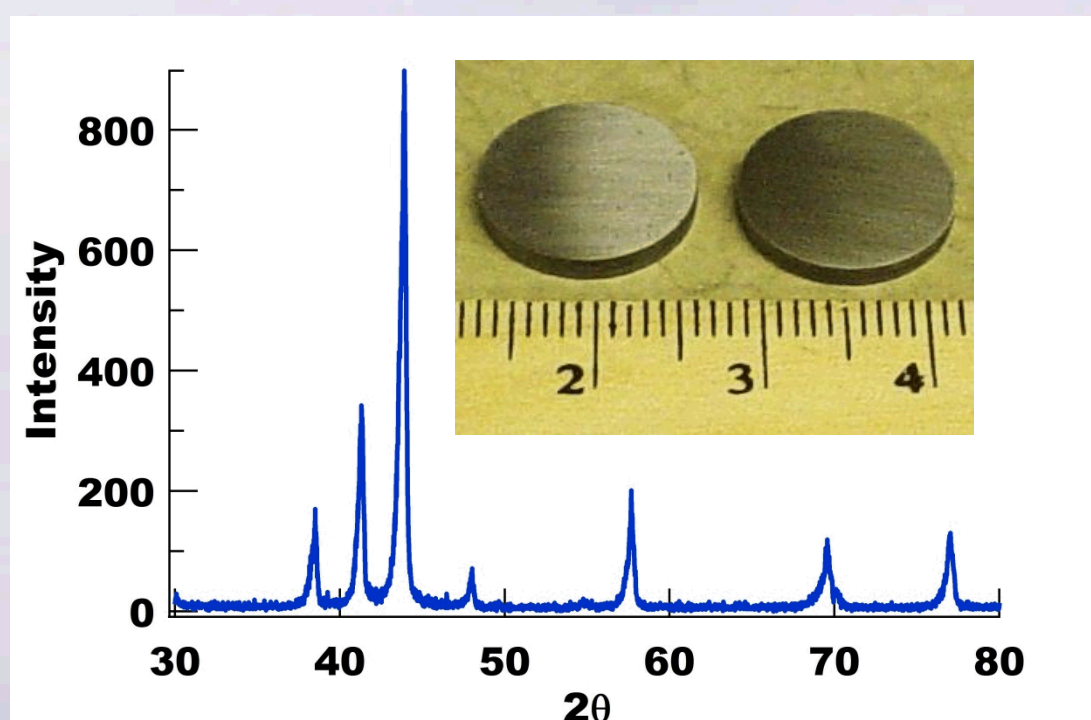
High frequency magnetic materials complement wide bandgap (WBG) semiconductors



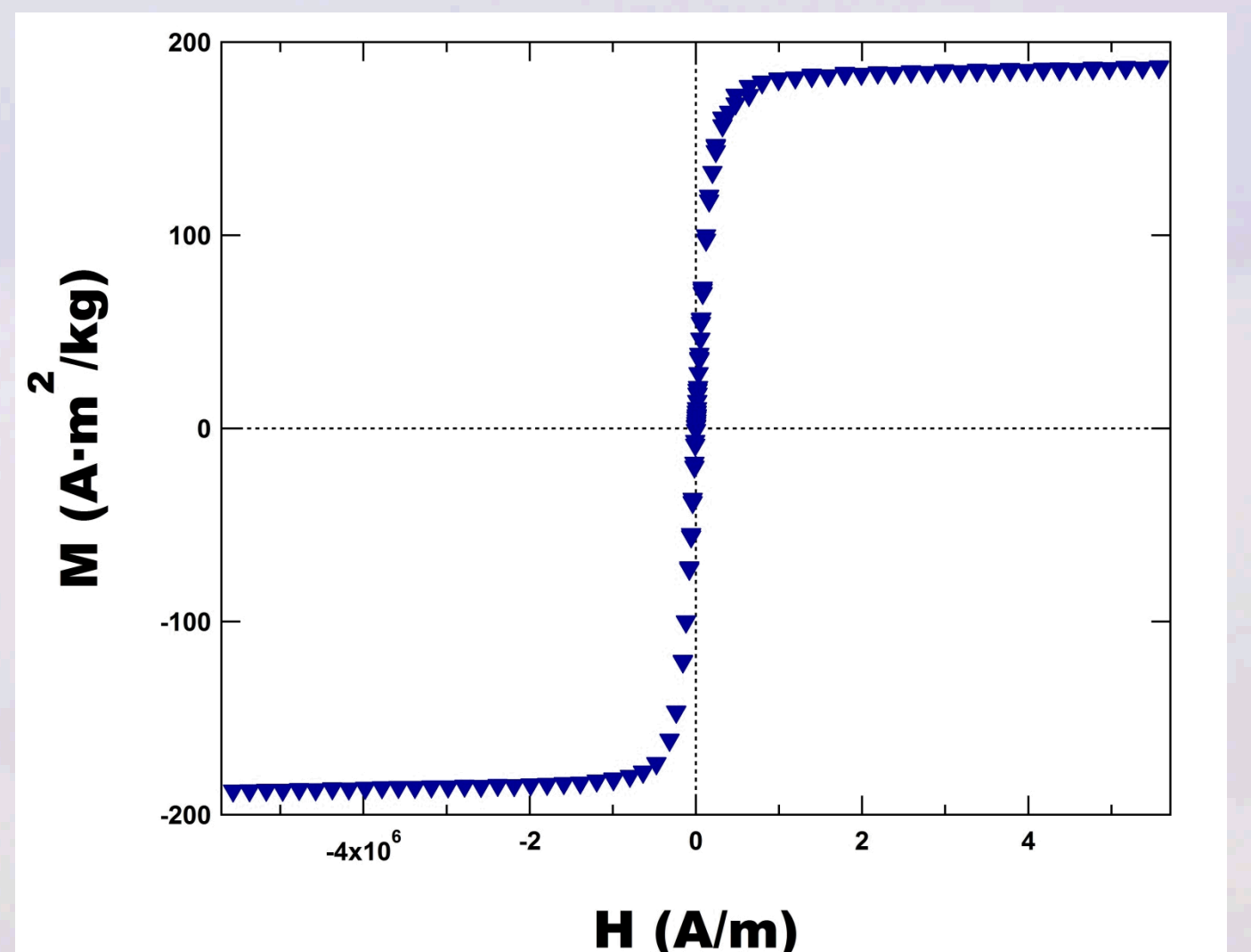
- SPS allows for net-shaping by using shaped dies
- Toroids, E-cores, and other shapes can be fabricated directly without the need for any machining



Raw powders are rapidly consolidated using spark plasma sintering (SPS)

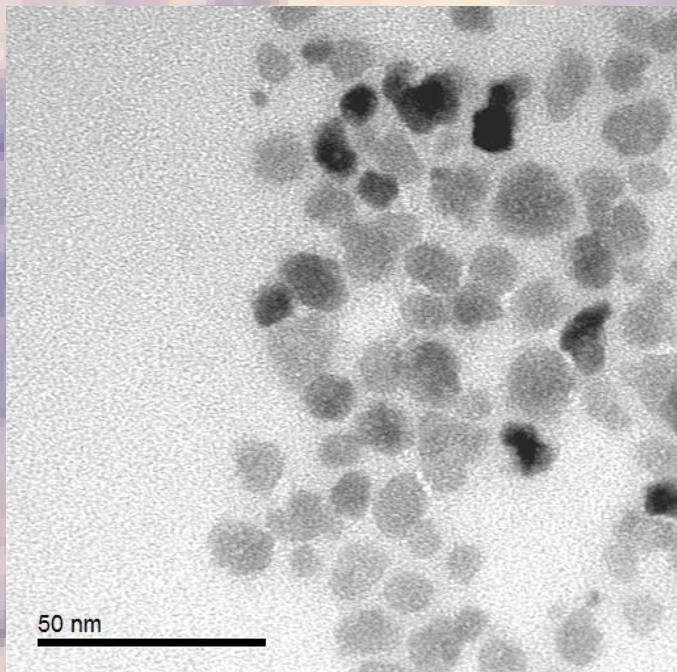


- Fe nitride powders well consolidated with little porosity
- Grain sizes 200 nm – 1 μm → fine grain size = low loss
- $\gamma'$ -Fe<sub>4</sub>N primary phase
- Fe<sub>3</sub>N secondary phase from mixed phase starting material

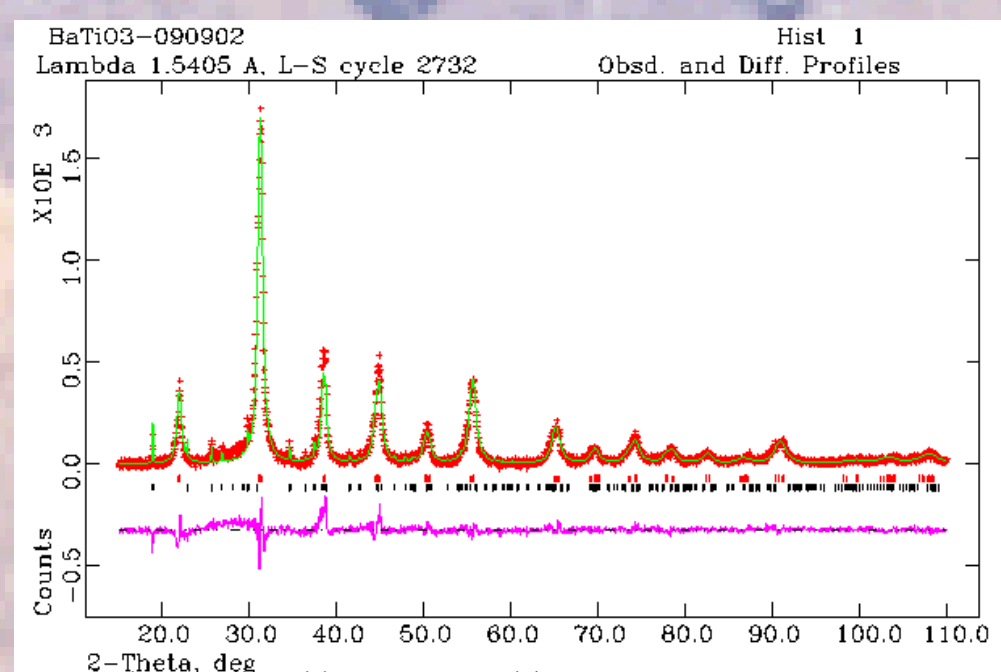


- Fe<sub>4</sub>N SPSed at 550°C and 100 MPa achieved an  $M_{sat}$  of 188 A·m²/kg.
- Predicted  $M_{sat}$  of bulk  $\gamma'$ -Fe<sub>4</sub>N is 209 A·m²/kg (Fe is 217 A·m²/kg)
- Negligible coercivity

## Ferroelectric (BaTiO<sub>3</sub> and PZT) Nanoparticles for Electrostatic Capacitors



Sandia solution synthesized BaTiO<sub>3</sub>



XRD pattern fits tetragonal phase

### Spark Plasma Sintering (SPS) of BaTiO<sub>3</sub> nanoparticles:

- Dramatically shorter overall sintering times
- Lower sintering temperatures, shorter hold times
- Ability to limit/control grain sizes
  - Porosity and oxygen defects minimized at same time
- Effective in removing resistive grain boundary component commonly observed in conventionally sintered BTO
- Improved frequency response

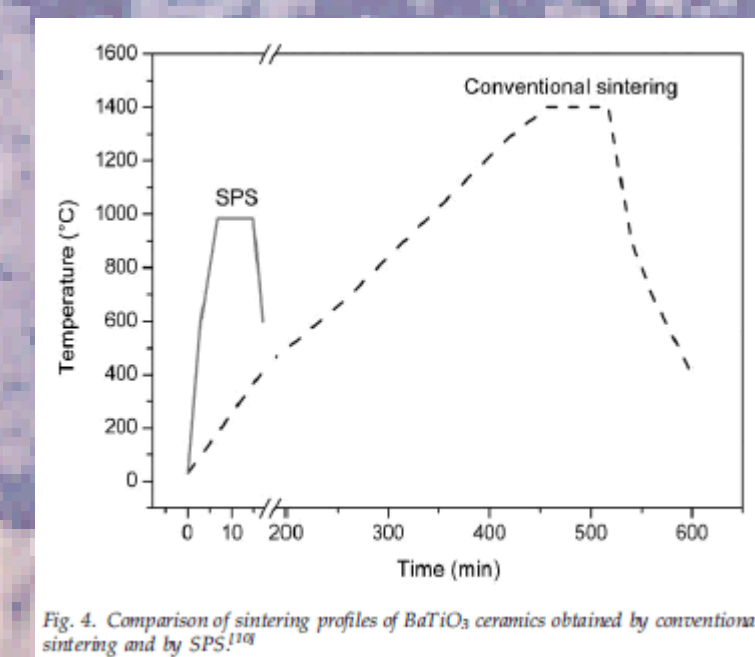
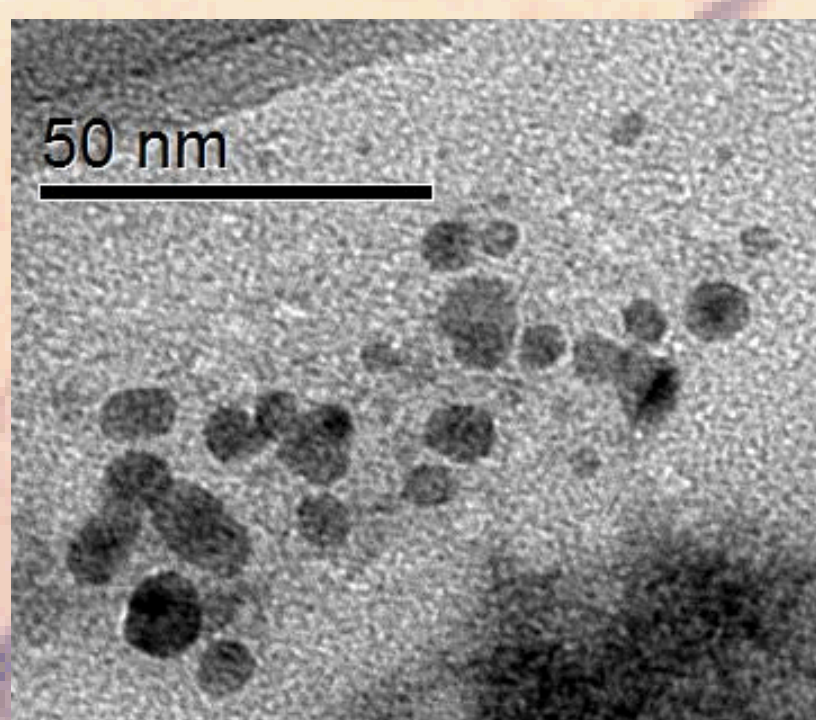


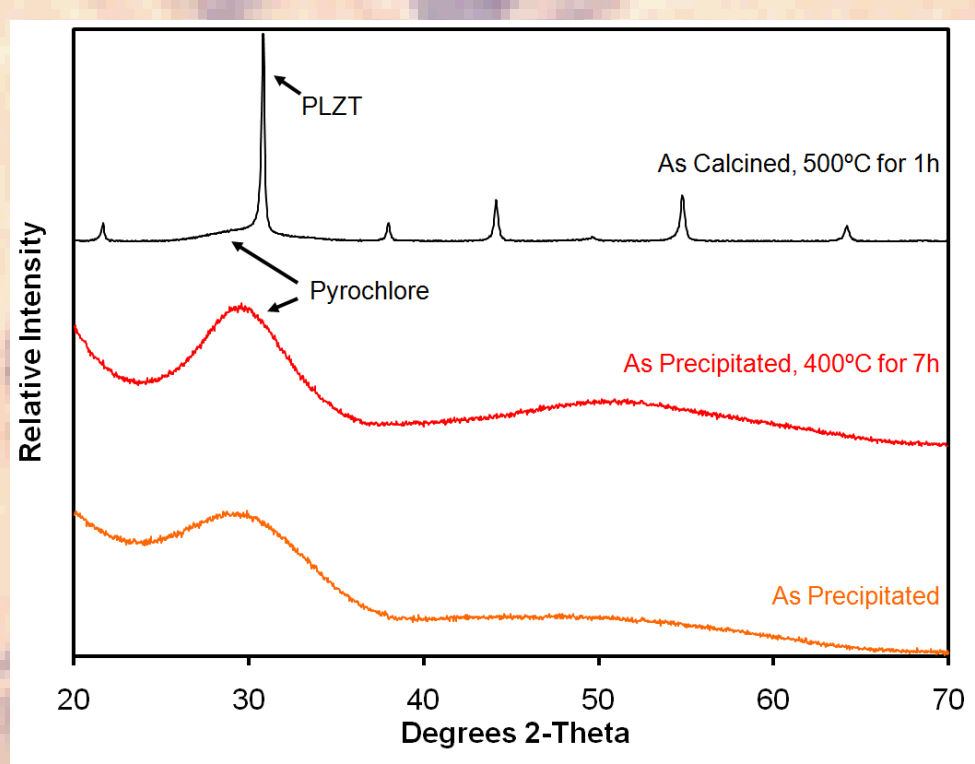
Fig. 4. Comparison of sintering profiles of BaTiO<sub>3</sub> ceramics obtained by conventional sintering and by SPS<sup>108</sup>



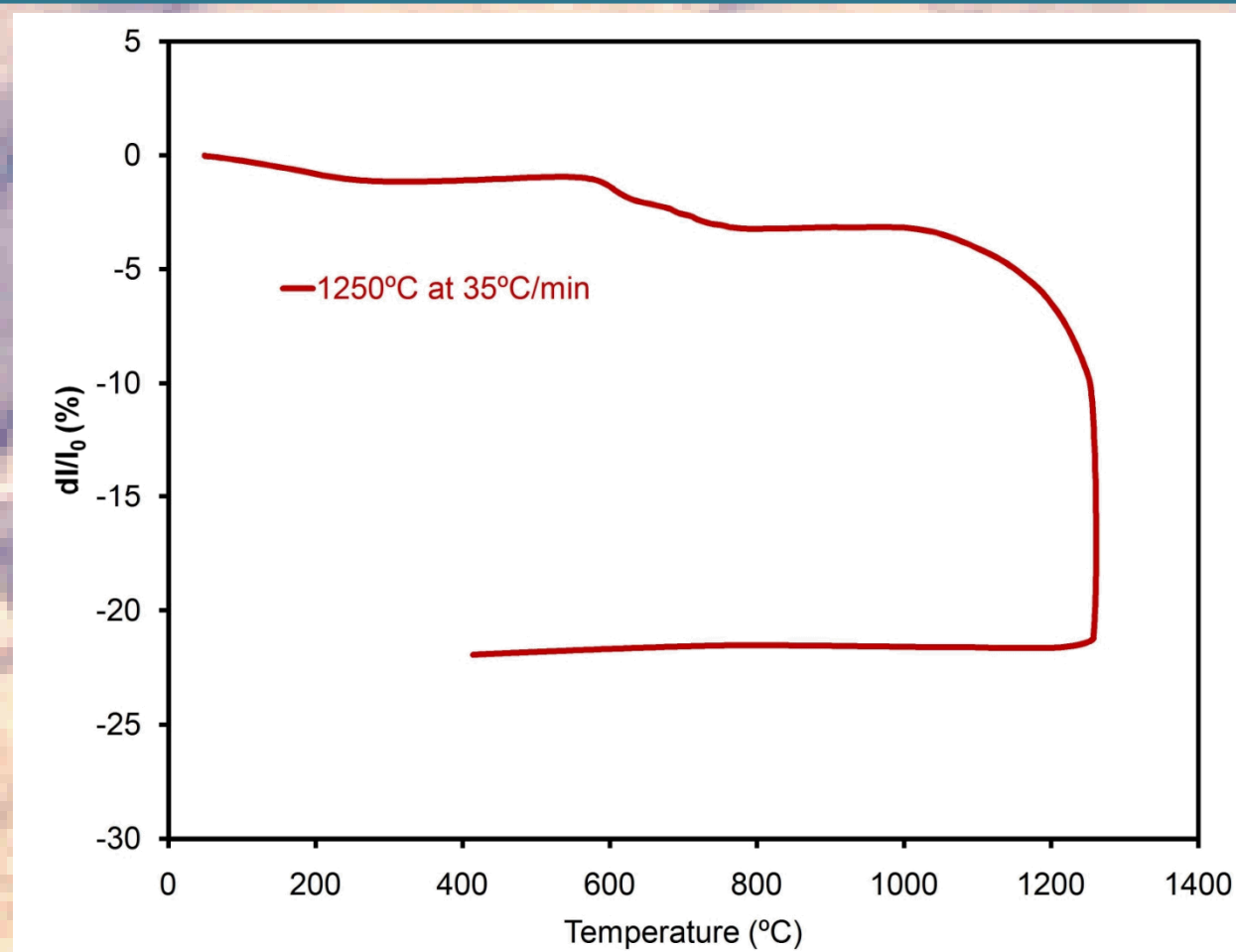
SPS graphite die during sintering



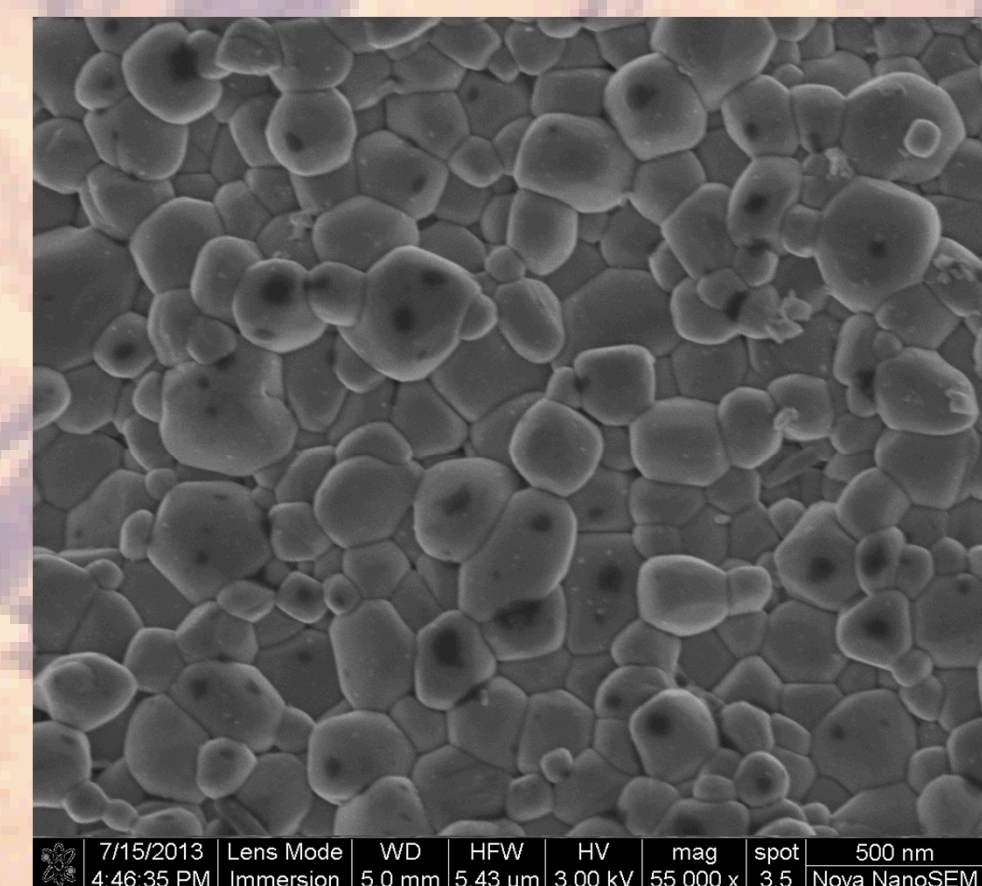
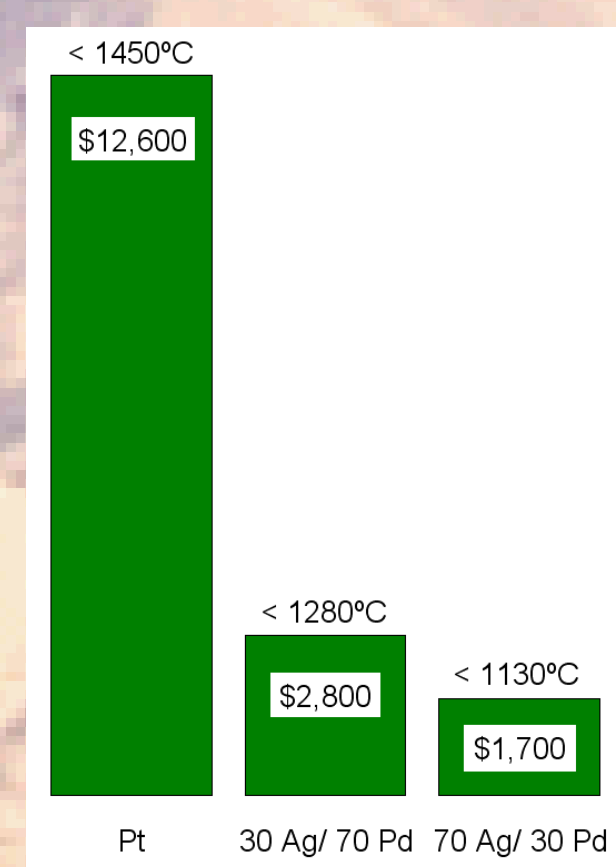
Sandia solution synthesized PZT



Significant lowering of calcining temperature (300 – 500 °C)



- Reduced PLZT sintering temperature with nanoparticle precursors
- > 4 fold reduction in electrode (and device) cost



SPSed BaTiO<sub>3</sub>



BaTiO<sub>3</sub>/epoxy composite with “graceful” failure mode

\* Currently supporting TPL, Inc. in Army Phase I SBIR: “Nanoparticle Capacitors for Multi-Point Initiation”