

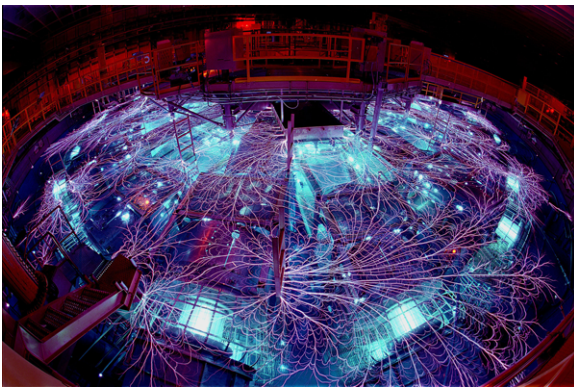
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Exploring magnetized liner inertial fusion with a semi-analytic model*

R. D. McBride, S. A. Slutz, D. B. Sinars, R. A. Vesey, M. R. Gomez, A. B. Sefkow, S. B. Hansen, K. R. Cochrane, P. F. Schmit, P. F. Knapp, M. Geissel, A. J. Harvey-Thompson, C. A. Jennings, M. R. Martin, T. J. Awe, D. C. Rovang, D. C. Lamppa, K. J. Peterson, G. A. Rochau, J. L. Porter, W. A. Stygar, and M. E. Cuneo

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November 17, 2015*

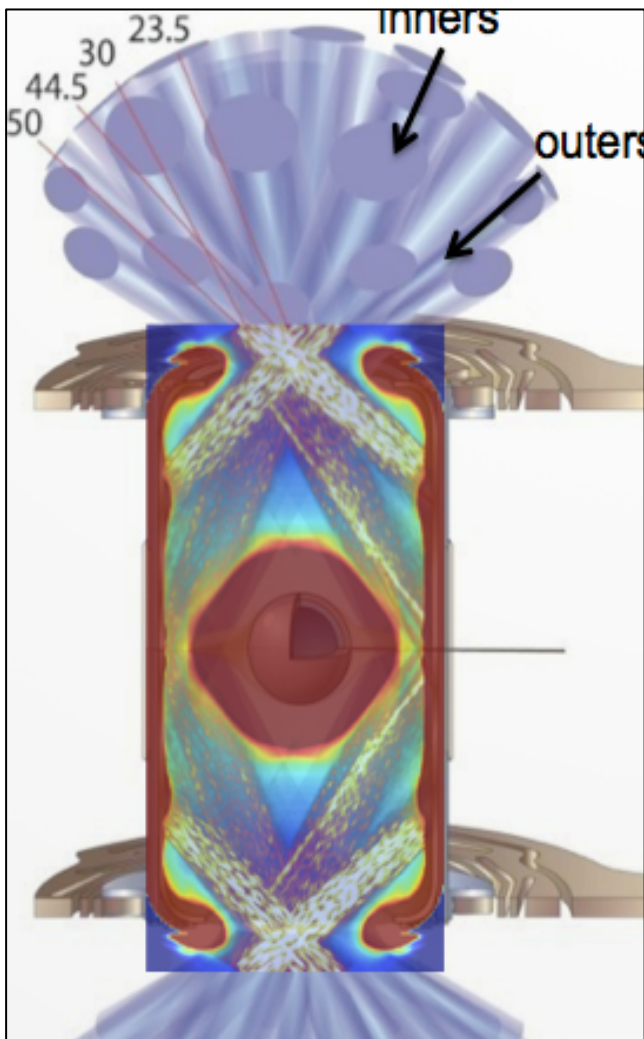


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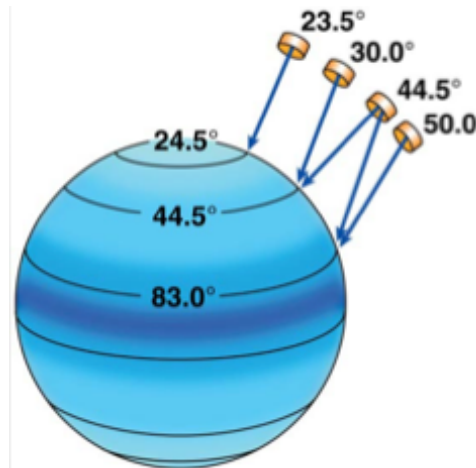
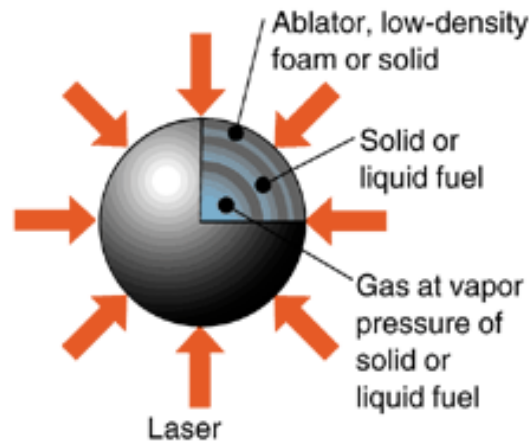
*Corresponding manuscript submitted to Physics of Plasmas (see pinup papers)

The United States ICF program is pursuing three main approaches to ignition

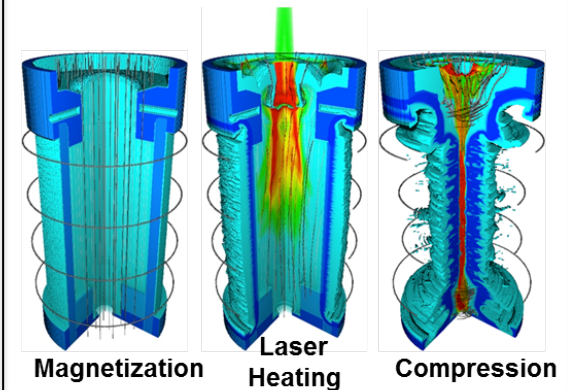
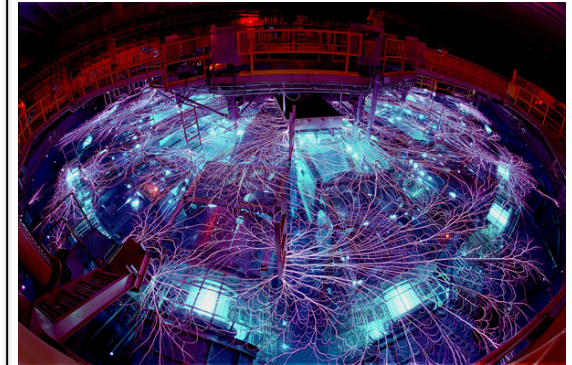
Radiation-driven implosions



Laser-driven implosions

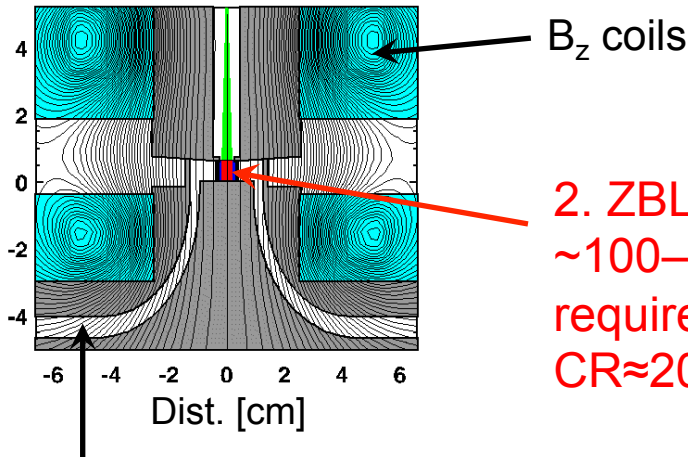


Magnetically-driven implosions

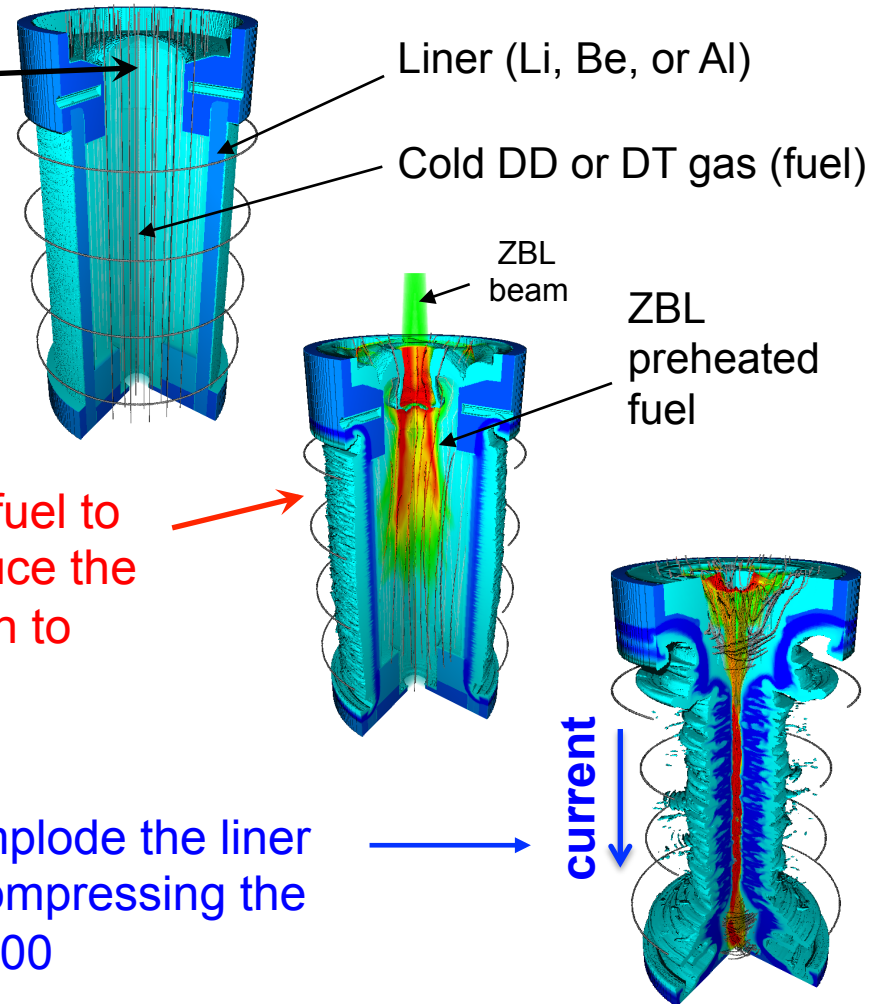


We are presently using the Z facility to study the **Magnetized Liner Inertial Fusion (MagLIF)** concept

1. A 10–50 T axial magnetic field (B_z) is applied (~ 3 -ms rise time) to inhibit thermal conduction losses and to enhance alpha particle deposition



2. ZBL preheats the fuel to ~ 100 –250 eV to reduce the required compression to $CR \approx 20$ –30



3. Z drive current and B_θ field implode the liner (via z-pinch) at 50–100 km/s, compressing the fuel and B_z field by factors of 1000

With DT fuel, simulations indicate scientific breakeven may be possible on Z (fusion energy out = energy deposited in fusion fuel)

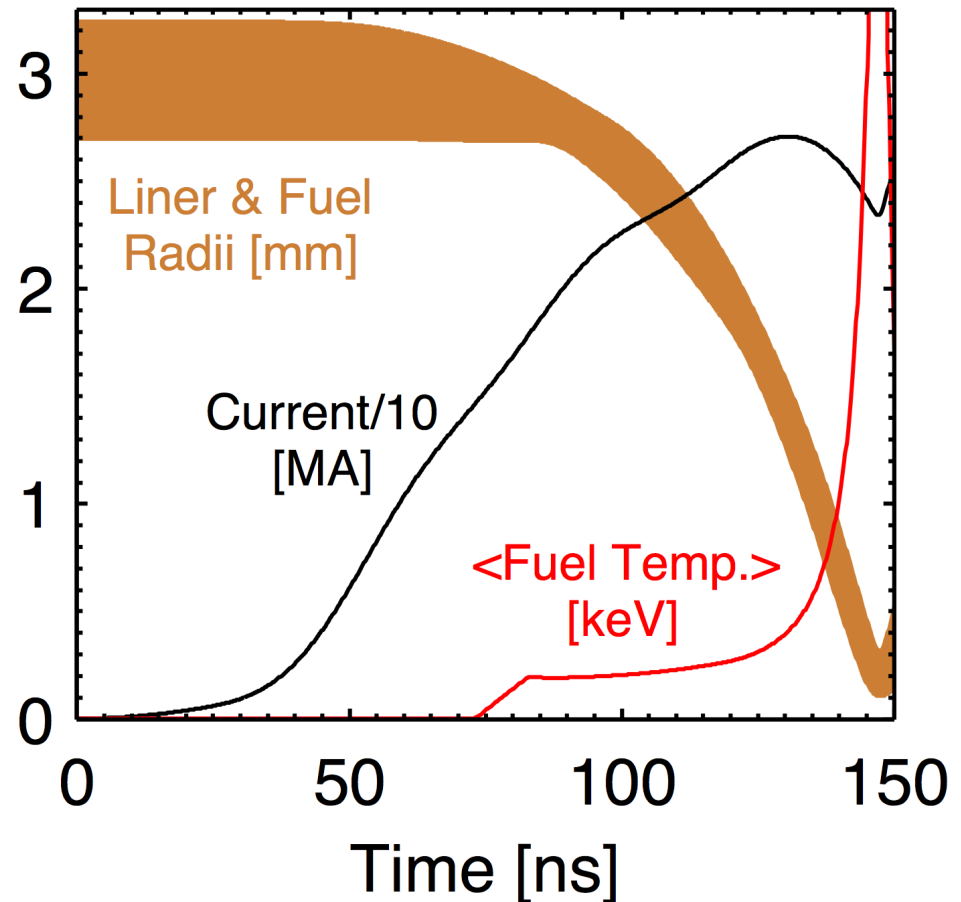
MagLIF Timing Overview

- ~ 60–100-ns implosion times
- ~ adiabatic fuel compression (thus preheating the fuel is necessary)
- ~ 5-keV fuel stagnation temperatures
- ~ 1-g/cc fuel stagnation densities
- ~ 5-Gbar fuel stagnation pressures

$$T \approx T_0 \left(\frac{\rho}{\rho_0} \right) \approx T_0 C_R^{4/3}$$

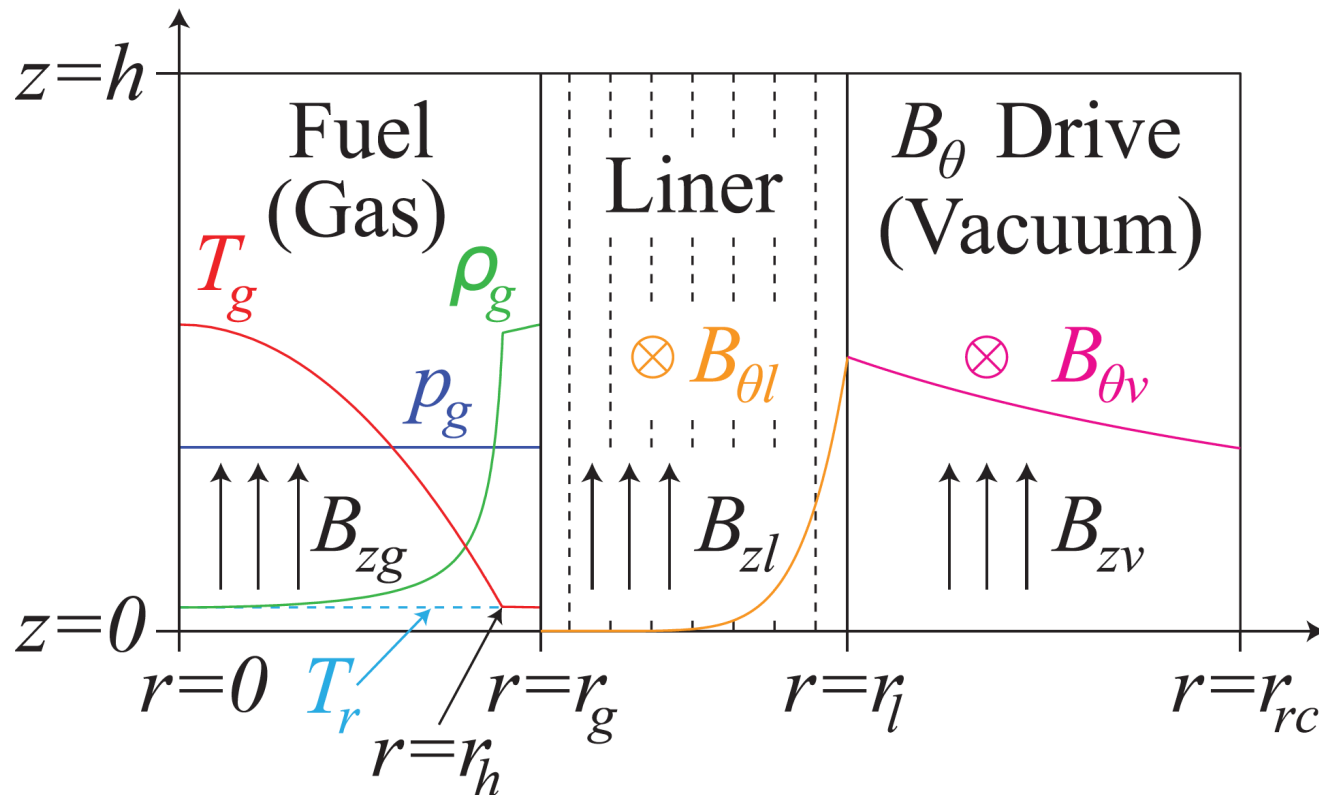
$(C_R = R_0/R_{stagnation})$

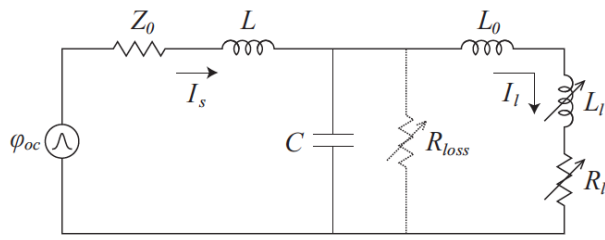
- Typically for ICF (e.g., NIF), faster implosions shock-heat the fuel, not so for MagLIF
- Magnetization is used to keep the preheated fuel from cooling off during the implosion



We have developed a semi-analytic model of MagLIF (SAMM)

- Developed with the “interested student” in mind
- System of $2N_{I_s}+13$ ordinary differential equations that are straight forward to solve with MATLAB, IDL, Mathematica, etc.
- ~30 seconds/simulation on a laptop
- ~3000 simulations in ~10 minutes using Sandia cluster (good for parameter scans)





Drive: circuit model driven by open-circuit voltage φ_{oc}

SAMM ODEs:

Dynamics (fuel and liner)

- p_l = ideal gas + Birch-Murnaghan cold curve (used for analytic fits to SESAME tables)
- $q_l \sim$ simple v^2 dependence

Energetics (fuel and liner)

- P_α = Basko
- P_r = Two-temperature grey model with emissivity & opacity integral over T & ρ profiles
- P_{ce} = Epperlein-Haines
- P_{ci} = Braginskii
- $I_l^2 R_l$ from assumed $B_\theta(r) \sim r^{\beta(\delta skin)}$ and Maxwell's equations

Loss of mix/dopant constituents due to end losses

B_z flux loss due to the Nernst thermoelectric effect (Braginskii)

Ablative transfer rate for cold, dense shelf mass to hotspot mass

DT & DD fusion burn: analytic $\langle \sigma v \rangle$ (Bosch & Hale)

Fuel loss due to fusion burn and end losses

$$\dot{I}_s = \frac{\varphi_{oc} - Z_0 I_s - \varphi_c}{L} \quad (1)$$

$$\dot{\varphi}_c = \frac{I_s - I_l - \varphi_c / R_{loss}}{C} \quad (2)$$

$$\dot{I}_l = \frac{\varphi_c - I_l (\dot{L}_v + \dot{L}_{lc})}{L_0 + L_v + L_{lc}} \quad (3)$$

$$\ddot{r}_{l,i} = \frac{p_{l,s=i-1} - p_{l,s=i}}{m_{ls}} \cdot 2\pi r_{l,i} \cdot h \quad (4)$$

$(i = 2, 3, \dots, N_{li} - 1)$

$$\ddot{r}_g = \frac{p_g + p_{\bar{B}_{zg}} - p_{l,s=1}}{m_{ls}/2} \cdot 2\pi r_g \cdot h \quad (5)$$

$$\ddot{r}_l = \frac{p_{l,s=N_{ls}} - p_{B_{\theta lv}} - p_{\bar{B}_{zv}}}{m_{ls}/2} \cdot 2\pi r_l \cdot h \quad (6)$$

$$\dot{E}_{l,s} = - \left(\frac{2}{3} \frac{E_{l,s}}{V_{l,s}} + q_{l,s} \right) \dot{V}_{l,s} + (P_r + P_c + P_\Omega - P_{BB}) / N_{ls} \quad (7)$$

$(s = 1, 2, \dots, N_{ls})$

$$\dot{E}_g = P_{pdV} + P_{ph} + P_\alpha - P_r - P_c - \dot{E}_{ends} \quad (8)$$

$$\dot{N}_{mix} = - \sum_{s \neq d, t} \dot{N}_{s,ends} \quad (9)$$

$$\dot{\Phi}_{zg} = \left[-2\pi r \cdot \mathcal{F}(x_e) \cdot \frac{k}{q_e} \frac{\partial T_g}{\partial r} \right]_{r=r_g} \quad (10)$$

$$\dot{f}_{mh} = \dot{m}_{s \rightarrow h} / m_g \quad (11)$$

$$\dot{N}_{dt} = h \int_0^{r_g} n_d n_t \langle \sigma v \rangle_{dt} \cdot 2\pi r \cdot dr \quad (12)$$

$$\dot{N}_{dd,^3\text{He}} = \frac{h}{2} \int_0^{r_g} n_d^2 \langle \sigma v \rangle_{dd,^3\text{He}} \cdot 2\pi r \cdot dr \quad (13)$$

$$\dot{N}_{dd,t} = \frac{h}{2} \int_0^{r_g} n_d^2 \langle \sigma v \rangle_{dd,t} \cdot 2\pi r \cdot dr \quad (14)$$

$$\dot{N}_d = -\dot{N}_{dt} - 2\dot{N}_{dd,^3\text{He}} - 2\dot{N}_{dd,t} - \dot{N}_{d,ends} \quad (15)$$

$$\dot{N}_t = -\dot{N}_{dt} - \dot{N}_{t,ends} \quad (16)$$

SAMM

Verification:

Ref. 1 in this figure is:
S. A. Slutz *et al.*, Phys. Plasmas **17**, 056303 (2010);
(see pinup papers).

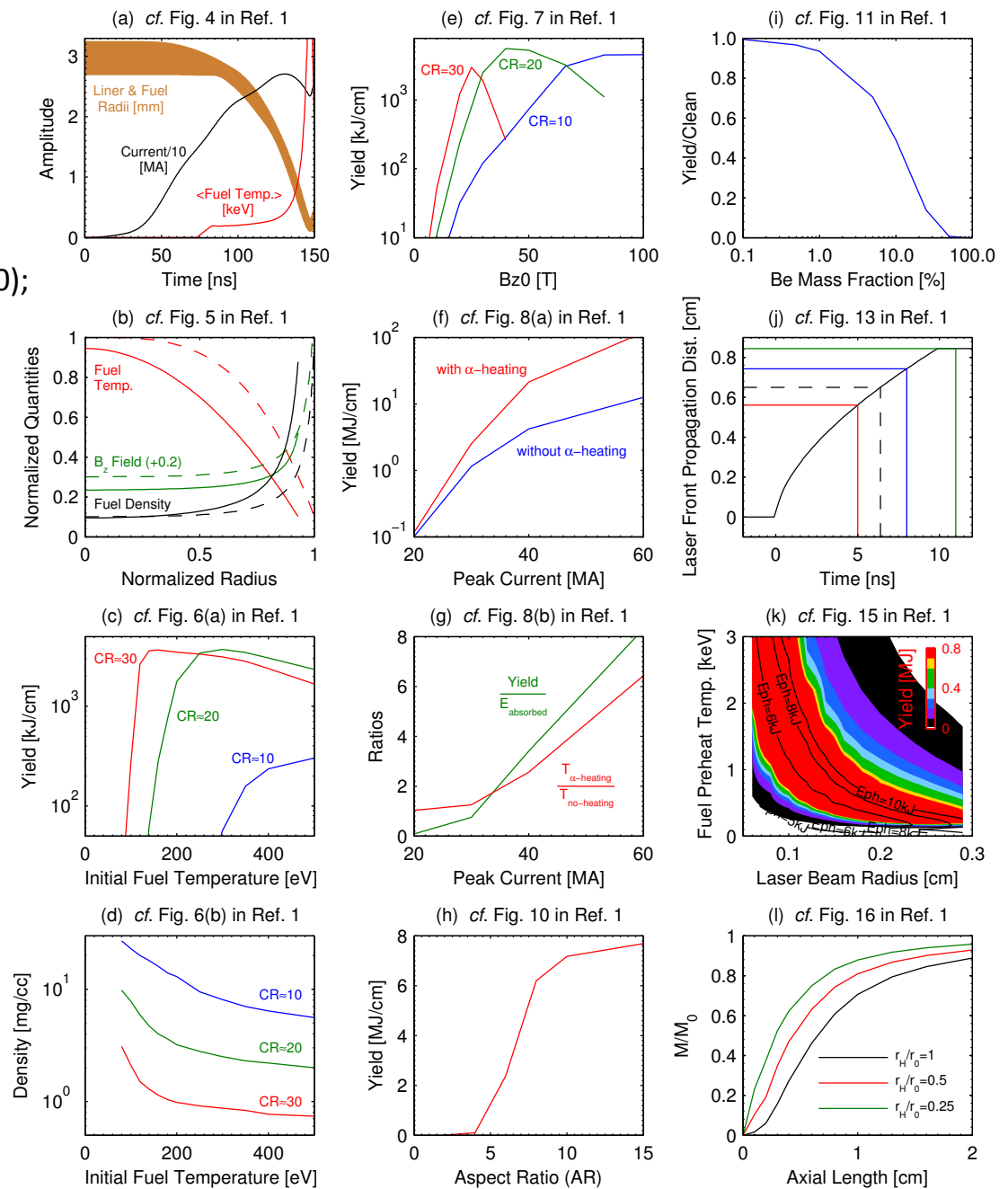


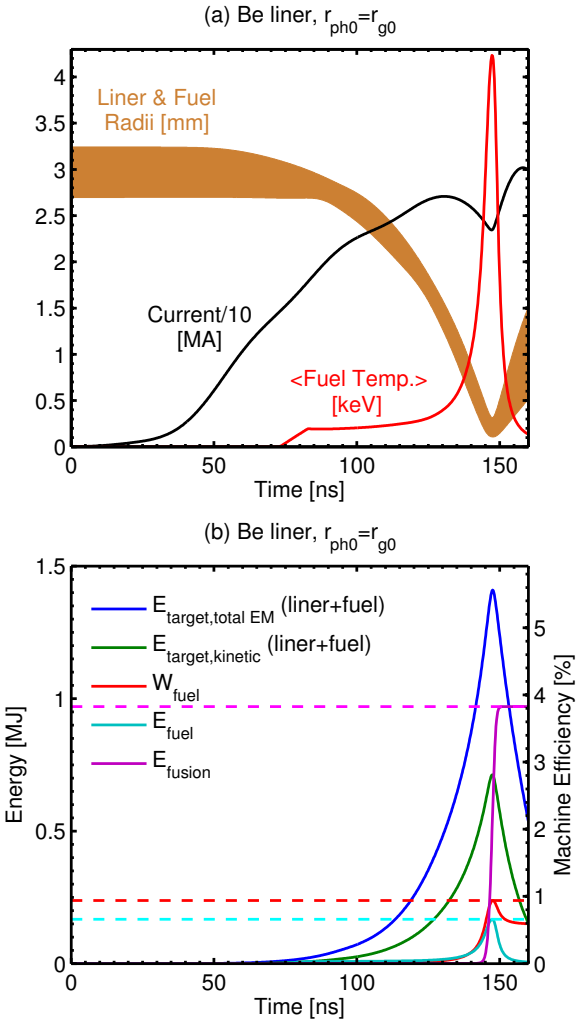
Figure 1 is a contour plot showing the DD Yield [n/cm] as a function of Eheat [kJ/cm] (Y-axis, 0 to 50) and rhofuel [mg/cc] (X-axis, 0 to 10). The plot is titled "Bz = 30 T" and "DD Yield [n/cm]". The color bar on the right indicates the DD Yield scale, ranging from 0 to 8×10^{14} n/cm. The plot shows regions of different DD yield values, with contours labeled from 5e13 to 5e14. The regions are color-coded: blue for low yield, orange for medium yield, and green for high yield. The contours are labeled with values: 5e13, 1e14, 2e14, and 5e14. The plot also shows regions of different DD yield values, with contours labeled from 5e13 to 5e14.

(Rad-MHD contour plots
courtesy of R. A. Vesey)

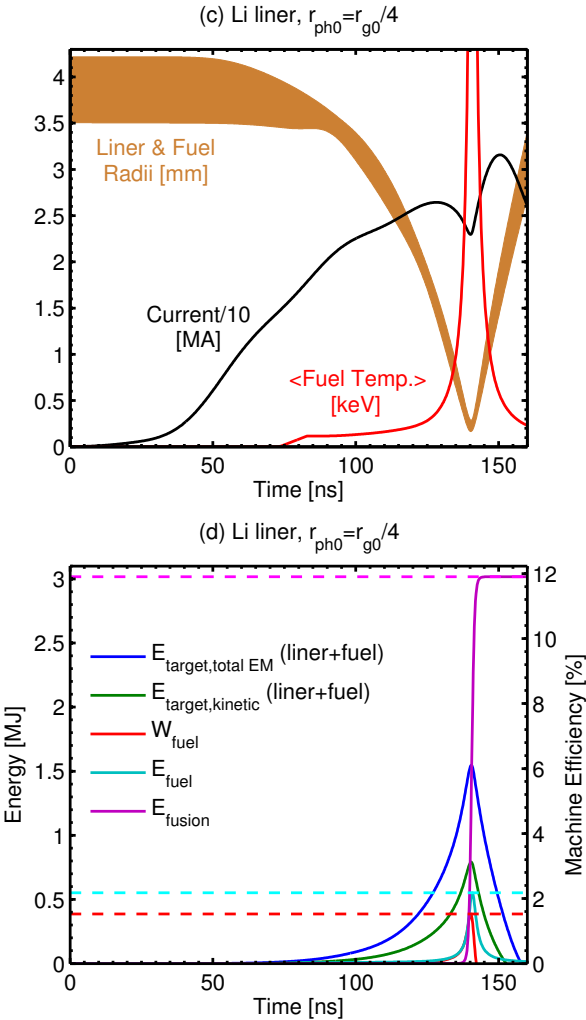
“2010 Point Design” Efficiencies:

“2010 Point Design” is that described in S. A. Slutz *et al.*, Phys. Plasmas **17**, 056303 (2010).

2010 Point Design:
DT fuel, 8 kJ preheat, 30 T, 27 MA, and
95-kV Marx Charge (~25 MJ stored)

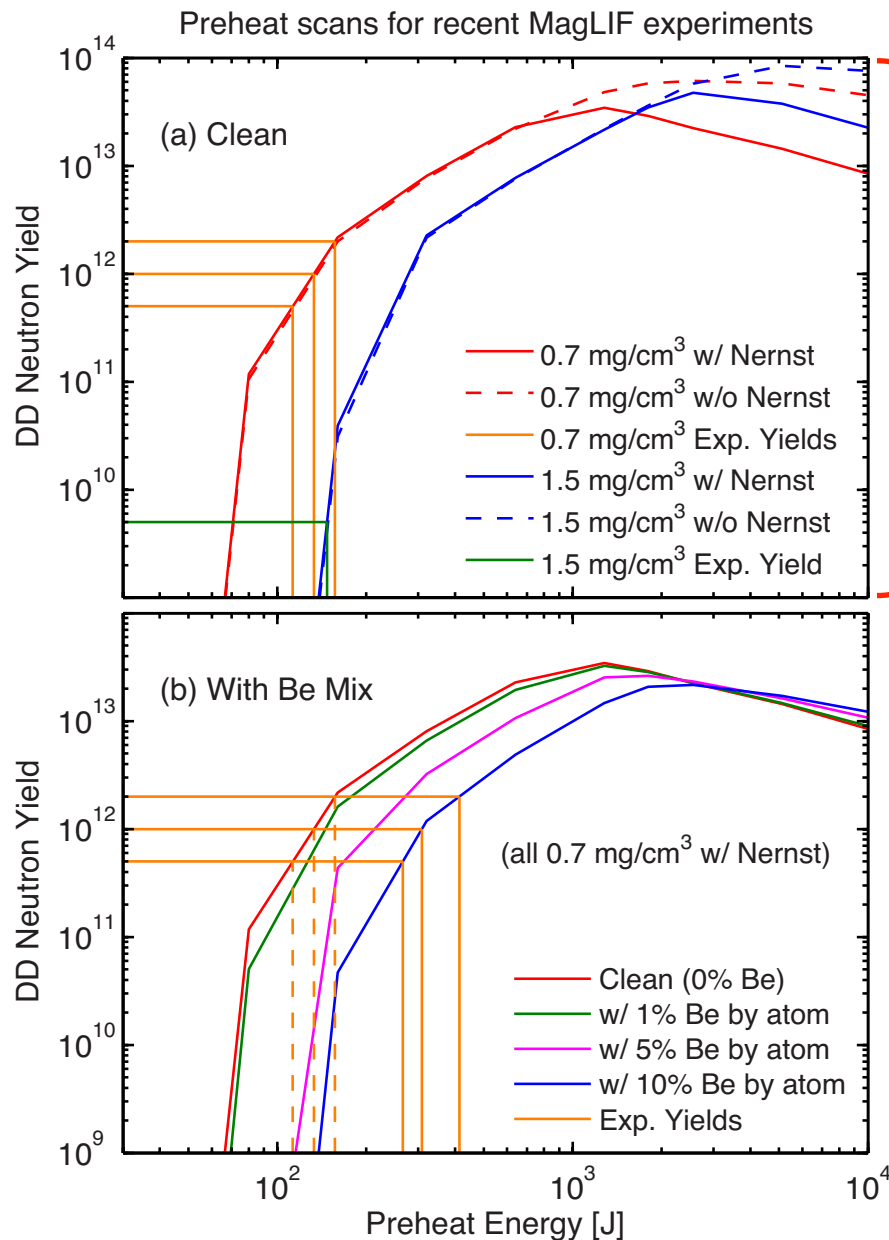


Modified 2010 Point Design:
Li liner and $r_{ph0}=r_{g0}/4$



2014 Experiments:

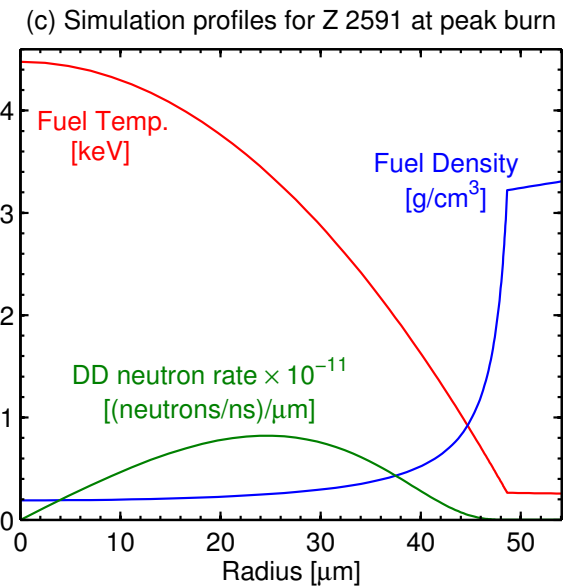
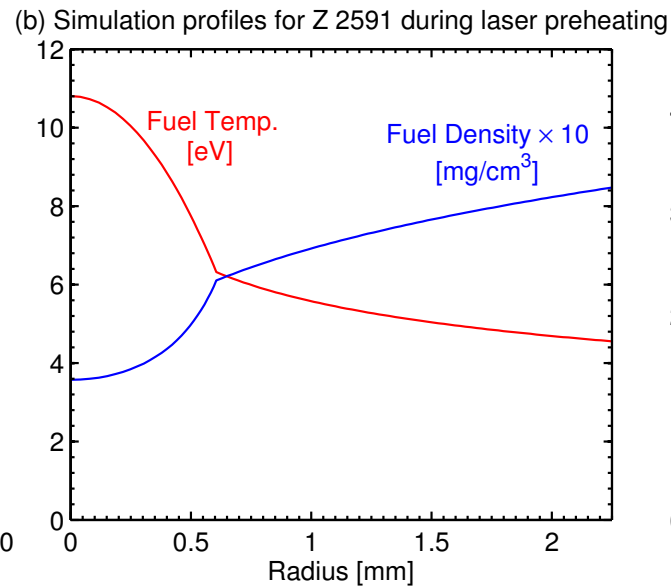
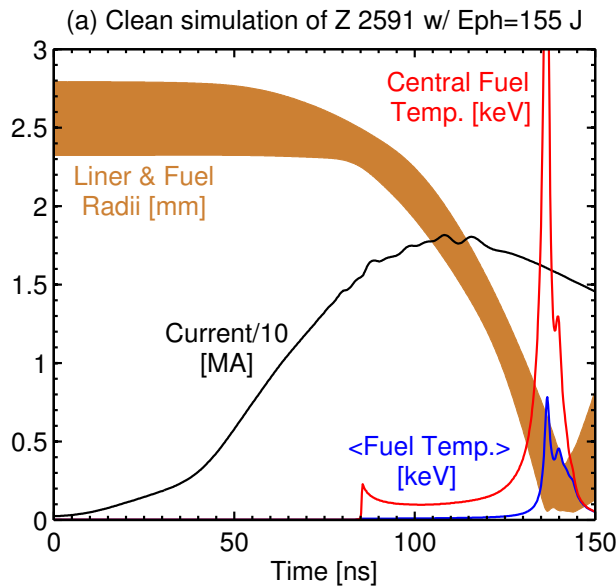
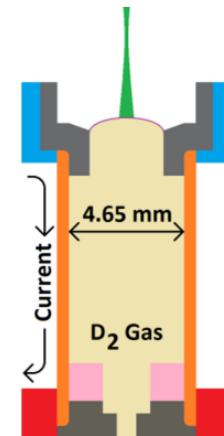
- 2014 Experiments are those described in M. R. Gomez *et al.*, Phys. Rev. Lett., **113**, 155003 (2014).
- DD Fuel, 10 T, 2-kJ laser, 18 MA, and 80-kV Marx charge (~18 MJ stored)
- Inferred laser-coupled preheat energy is low (~150 J), but is dependent on assumed level of uniform contaminant mix
- With 10% Be mix by atom (consistent with that inferred spectroscopically), preheat energy could be ~400 J
 - Thus, with ~100 J absorbed in the laser entrance channel above the imploding region, ~500 J could have been transmitted past the laser entrance window, in agreement with laser-only foil-transmission experiments
- Nernst thermoelectric effect may not be relevant until we can increase the coupled preheat energy



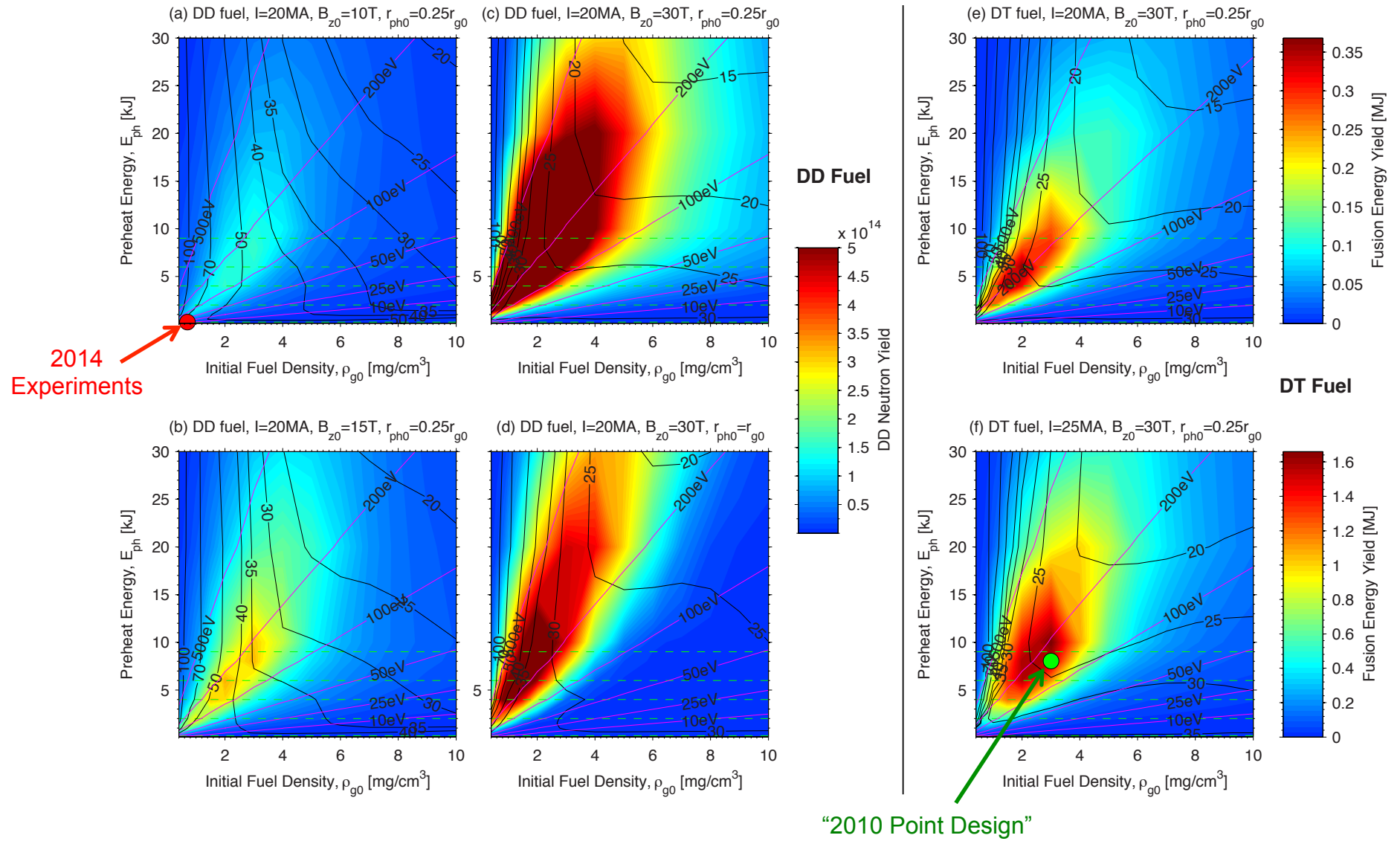
Similar to A. B. Sefkow *et al.*, Phys. Plasmas **21**, 072711 (2014).

2014 Experiments:

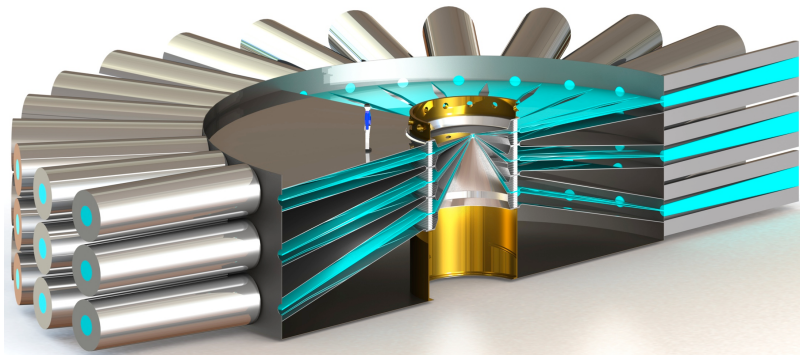
- DD Fuel, 10 T, 2-kJ laser, 18 MA, 2×10^{12} DD neutrons:
 - 155 J of preheat energy, clean
 - 396 J of preheat with 10% Be mix (by atom)
- $r_{ph0} < r_g(t_{ph})$ results in a fuel structure with two regions:
 - A hotspot region with fusion-relevant temperatures at stagnation
 - A cold dense shelf region that surrounds the hotspot and provides a buffer region between the hot fuel and the liner, which reduces radiative, thermal conduction, and magnetic flux losses from the fuel to the liner



Near-term MagLIF parameter space:



MagLIF Scans for Z300 & Z800:



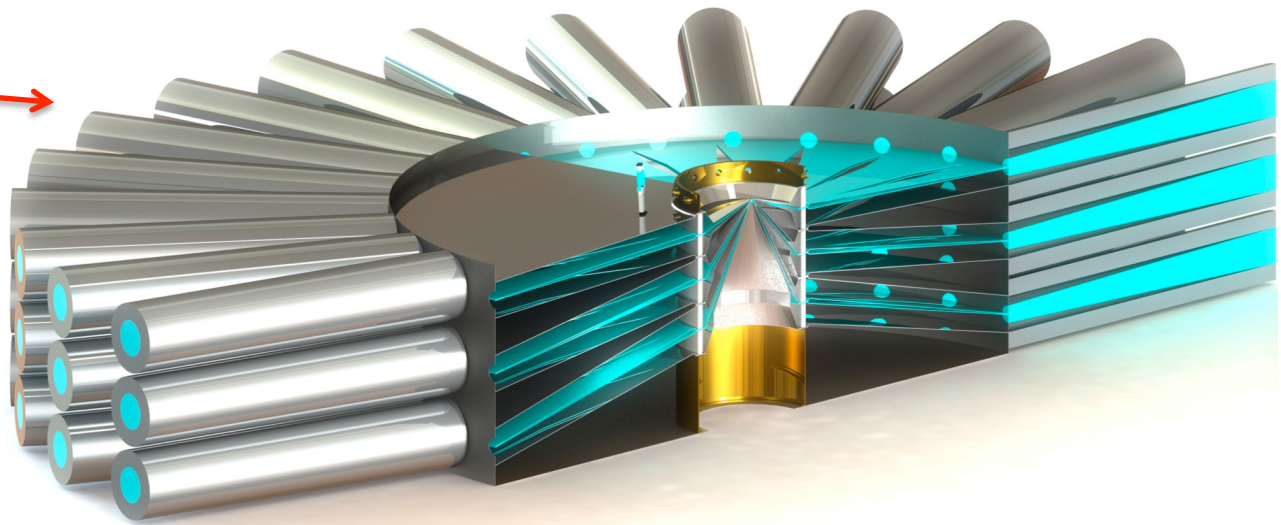
**LTD-based
architectures**

Z300:

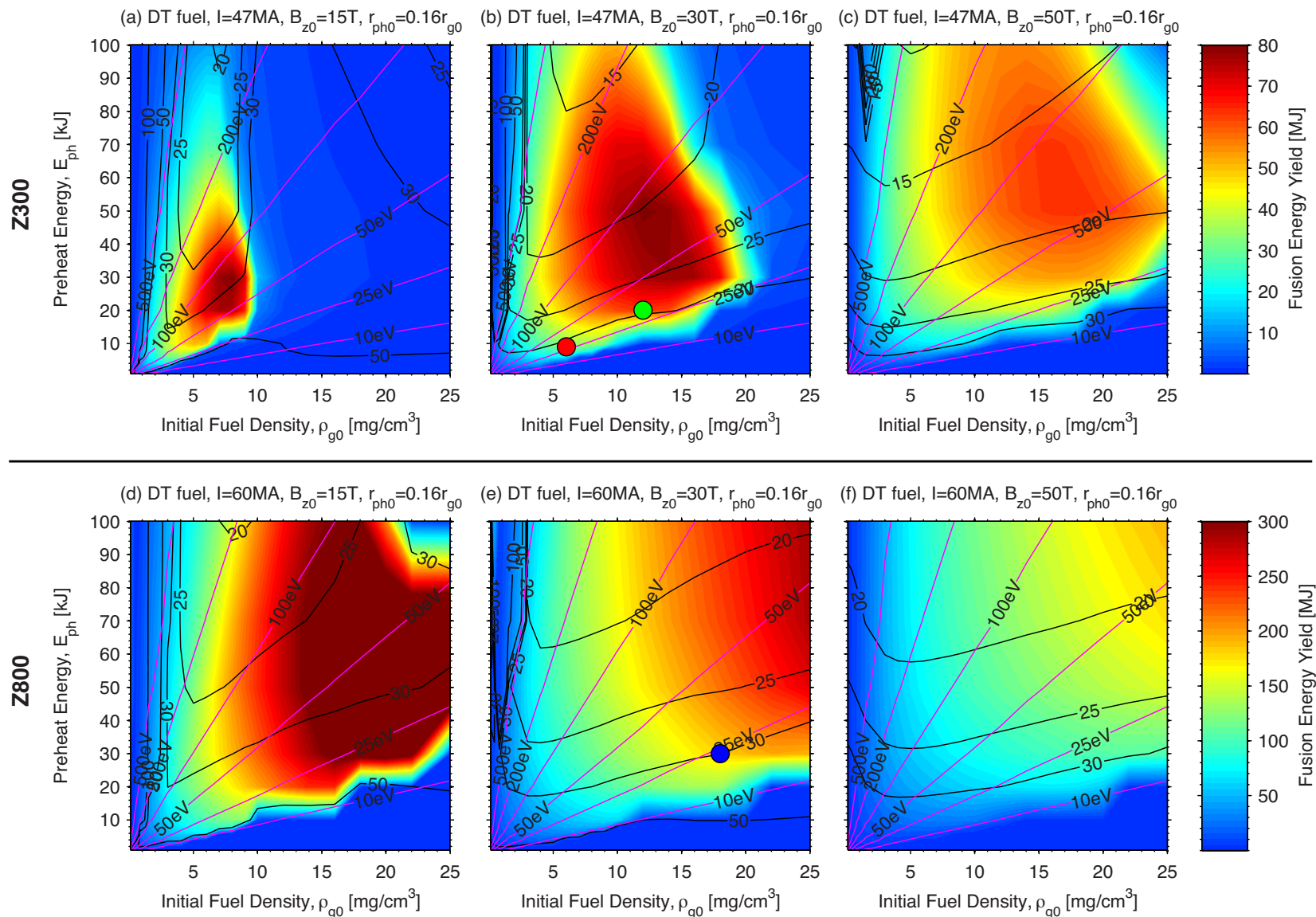
- 320 TW delivered
- 48 MJ stored
- 48 MA
- 120–150 ns rise
- 35 m in diameter (size of Z today)

Z800:

- 890 TW delivered
- 130 MJ stored
- 60–65 MA
- 110–120 ns rise
- 52 m in diameter



MagLIF Scans for Z300 & Z800:

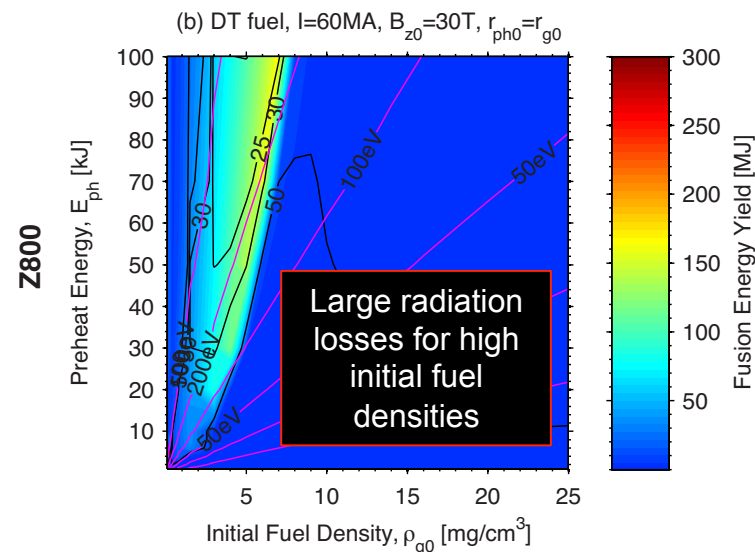
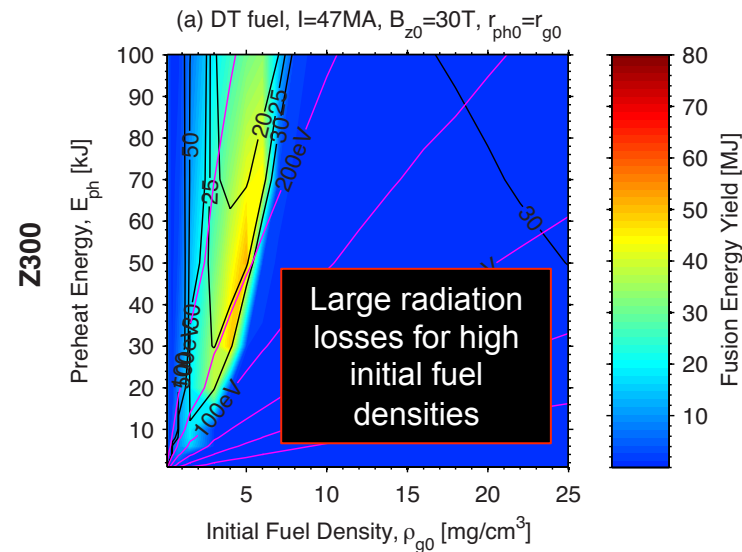
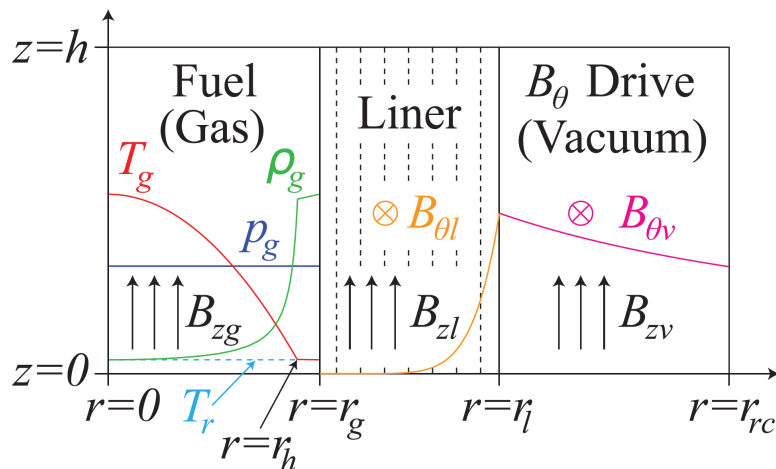


MagLIF Scans for Z300 & Z800:

Particularly for large drive currents, setting $r_{ph0}=r_{g0}$ is not optimal due to increased radiative losses:

$$P_{rv}(r) = A_{br} \cdot 2\pi h \cdot \bar{Z}_g^2 \int_0^r n_i n_e \sqrt{T_g} \left[1 - \left(\frac{T_r}{T_g} \right)^4 \right] r' dr'$$

$$P_{rs}(r) = (1 - \alpha_s) \sigma T_r^4(r) \cdot 2\pi r \cdot h$$



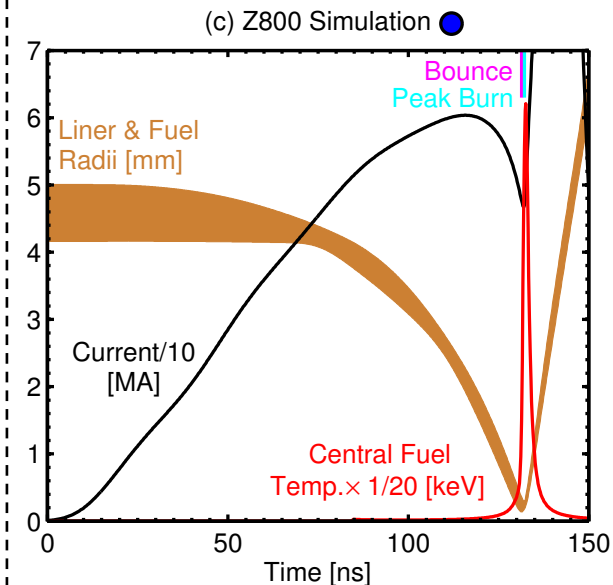
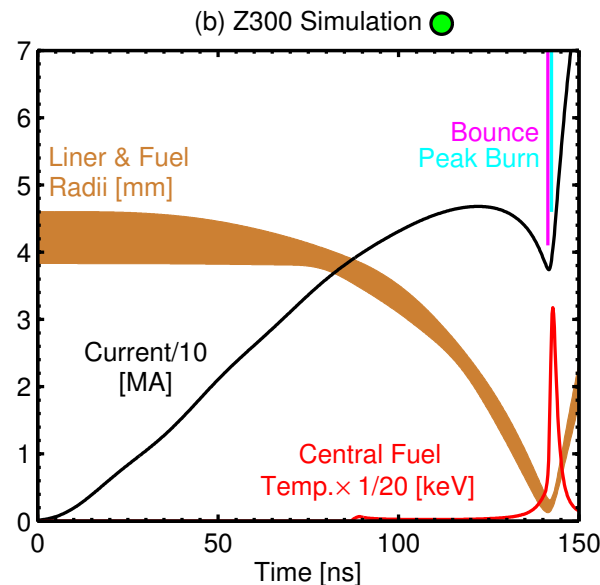
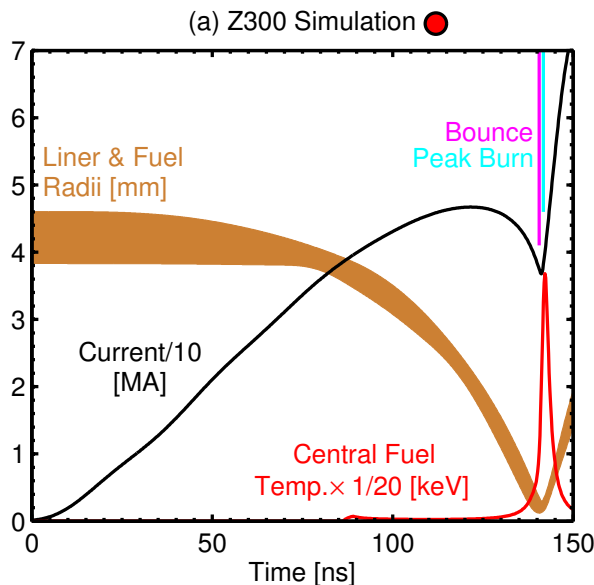
MagLIF Scans for Z300 & Z800:

Z300:

- 48 MJ stored
- 4.3 MJ absorbed by target
- 38 MJ fusion energy (w/ 9 kJ preheat)
- 77 MJ fusion energy (w/ 20 kJ preheat)
- CR~23–32
- $B_{z0} = 30$ T
- LTD-based architecture with footprint the size of Z today

Z800:

- 130 MJ stored
- 8.2 MJ absorbed by target
- 218 MJ fusion energy (w/ 30 kJ preheat)
- CR~23–30
- $B_{z0} = 30$ T



Summary & Conclusions

- The development and use of this semi-analytic model has been a fun, useful, and insightful exercise
 - Led to several physical insights, including the relationship between the preheat radius and bremsstrahlung loss rates
- This model's accessible physics and fast run times (~30 seconds/simulation unoptimized) make it a useful pedagogical tool, especially for students, experimentalists, or any researcher interested in MagLIF
- For more details on this model and its uses, see manuscripts (and pinups):
 - R. D. McBride and S. A. Slutz, "A semi-analytic model of magnetized liner inertial fusion", Phys. Plasmas **22**, 052708 (2015).
 - R. D. McBride *et al.*, "Exploring magnetized liner inertial fusion with a semi-analytic model", submitted to Phys. Plasmas (2015).