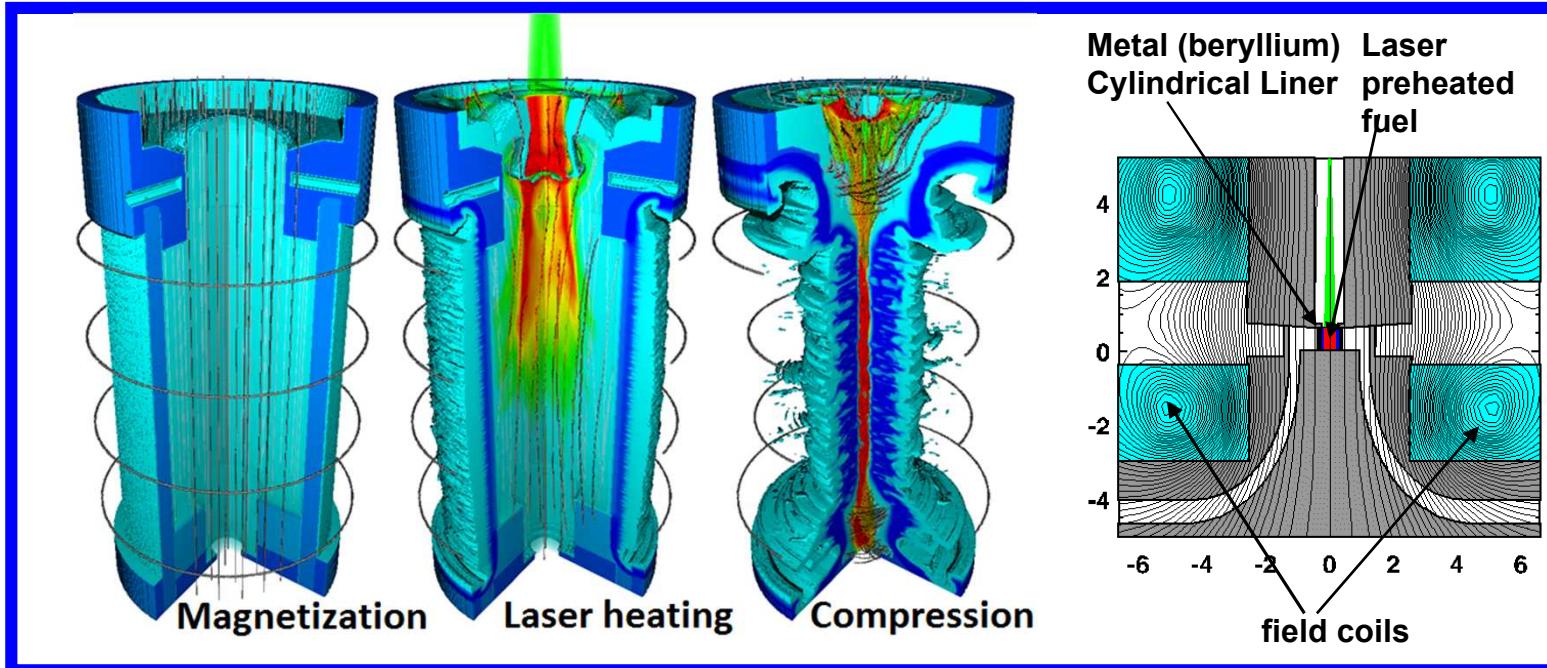


Scaling Magnetized Liner Inertial Fusion (MagLIF) on Z and Future Machines



Inertial Fusion Science & Applications

Seattle, Washington, September 20-25, 2015

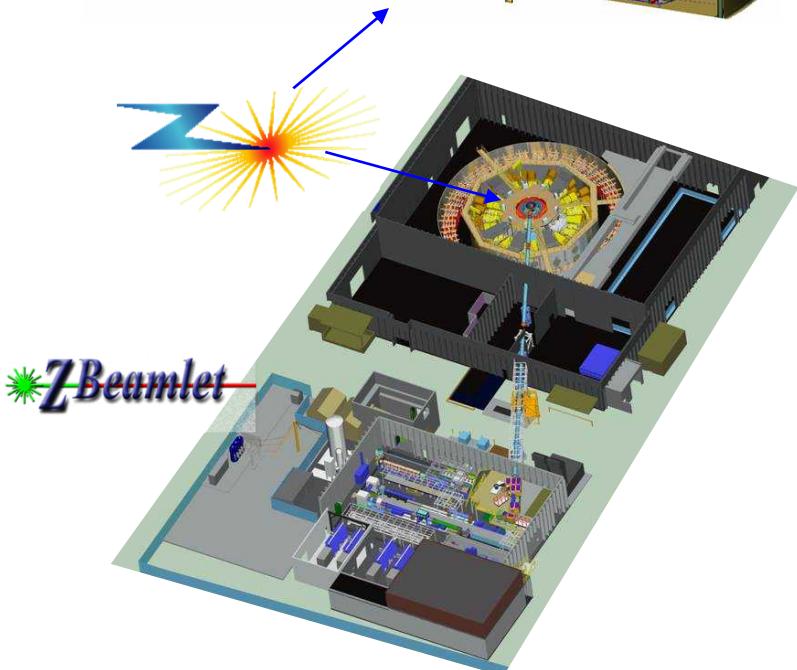
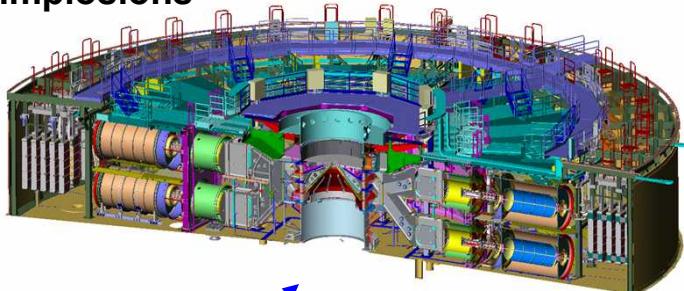
S. A. Slutz, W. Stygar, M.R. Gomez, E.M. Campbell, K.J. Peterson, A. B. Sefkow, D.B. Sinars, R. A. Vesey
Sandia National Laboratories

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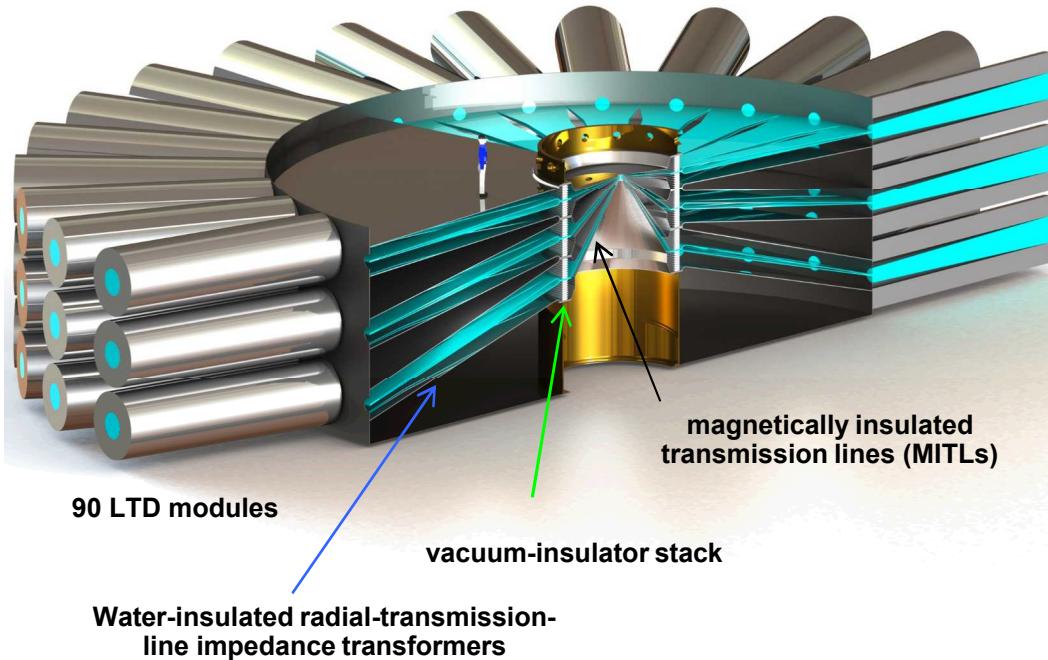
The MagLIF concept¹ is being tested² on the Z facility. Higher drive currents could be provided by future machines³

Z can generate high magnetic pressures to drive cylindrical implosions



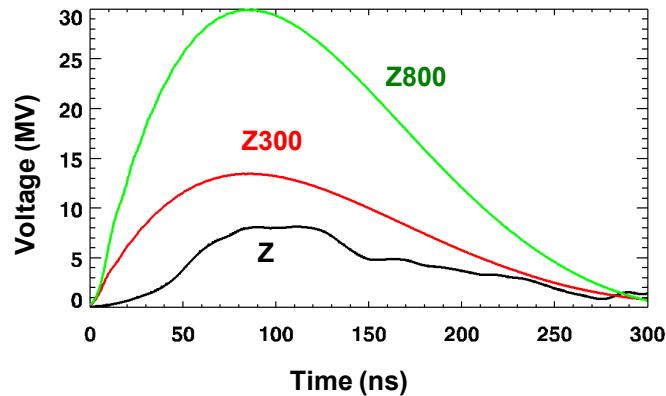
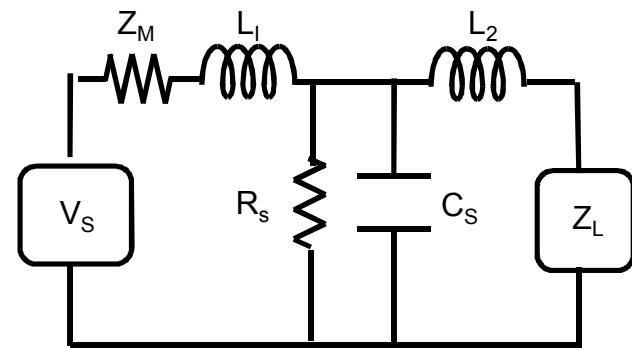
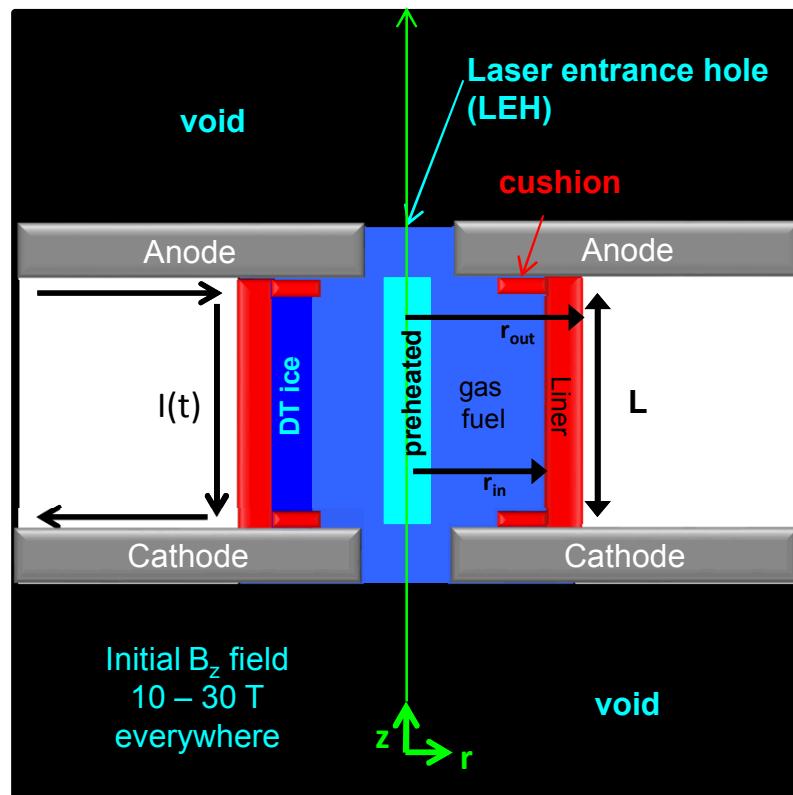
Z-Beamlet provides fuel preheat

Z 300 employs Linear Transformer Driver (LTD) technology to deliver 48 MA to a MagLIF load, and would fit within the existing Z building.



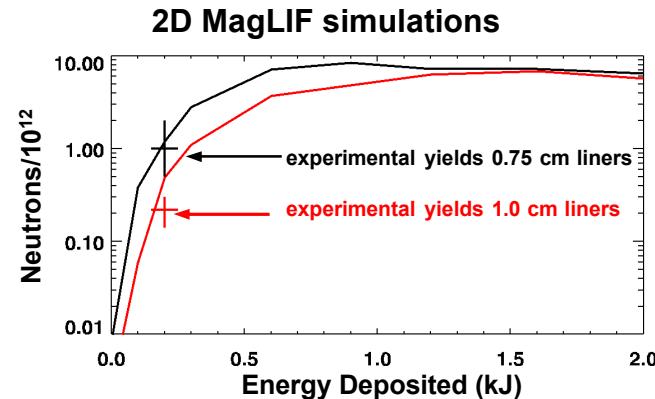
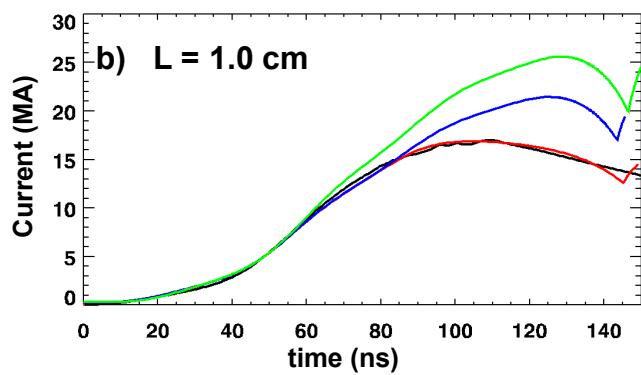
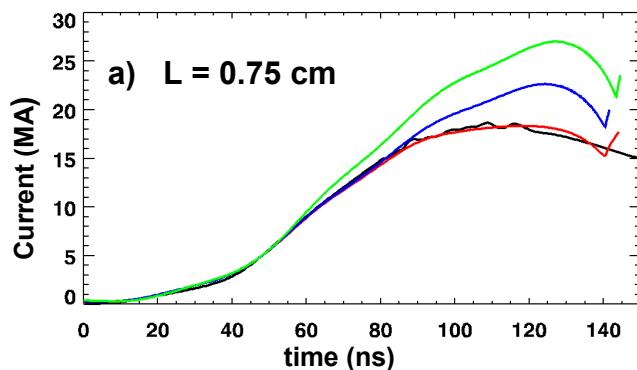
Z800 would deliver 65 MA with the same technology

2D Lasnex simulations based on simplified geometry and circuit model



Simulated yields are comparable to experiments results

Black: 80 kV MagLIF experiments results
Red: 80 kV simulated with feed loss
Blue: 80 kV simulated without feed loss
Green: 95 kV simulated without feed loss

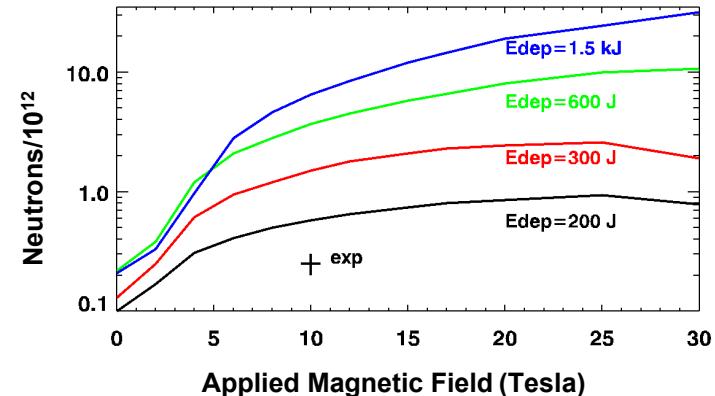
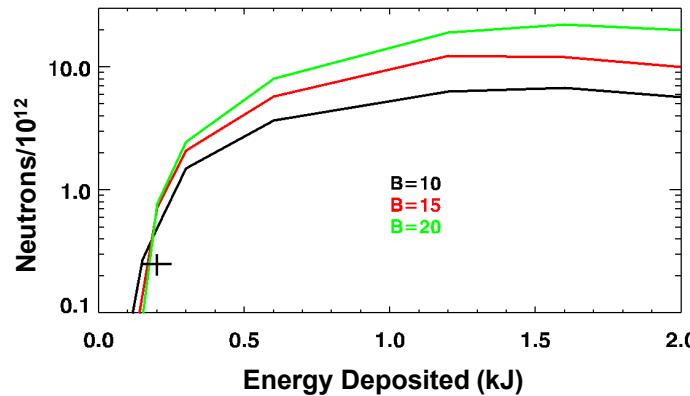


Z Beamlet produces 2 kJ of unsmoothed 0.53 mm light

- Only ~ 200 Joules penetrates foil¹

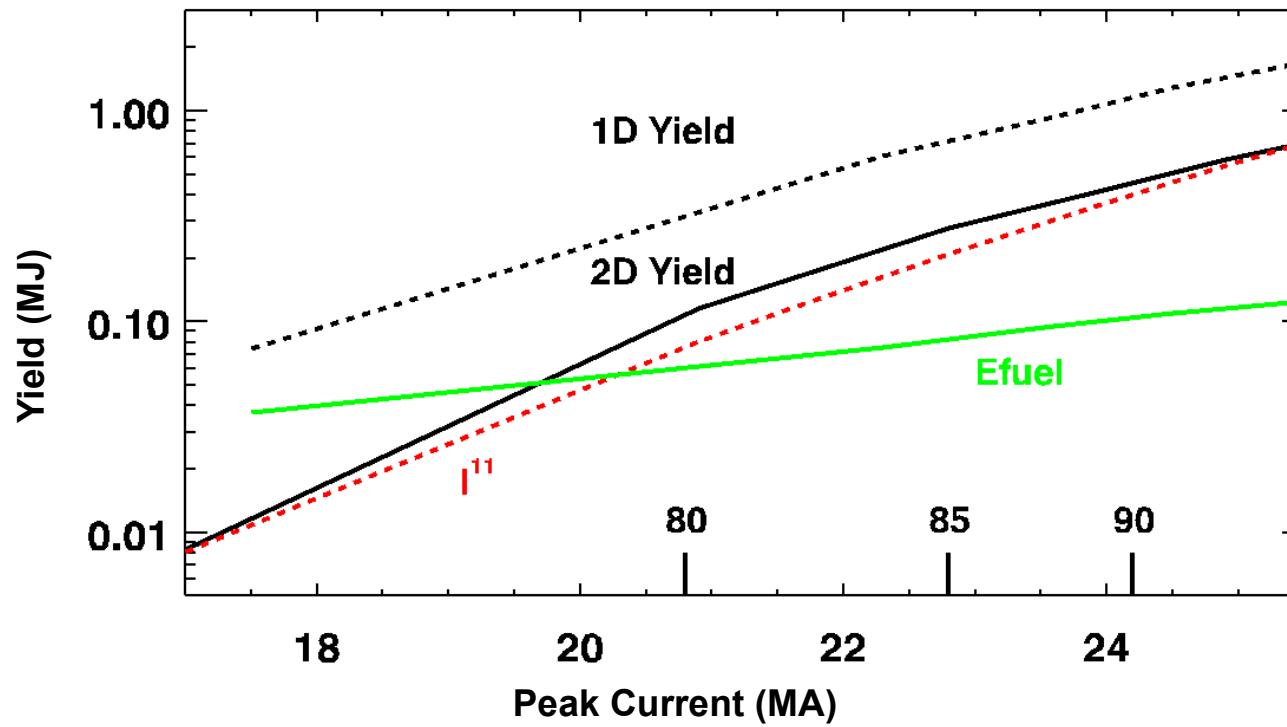
Present experiments on Z at 18 MA do not have optimal values of preheat or applied field according to simulation

2D Lasnex simulations of 1 cm long liners



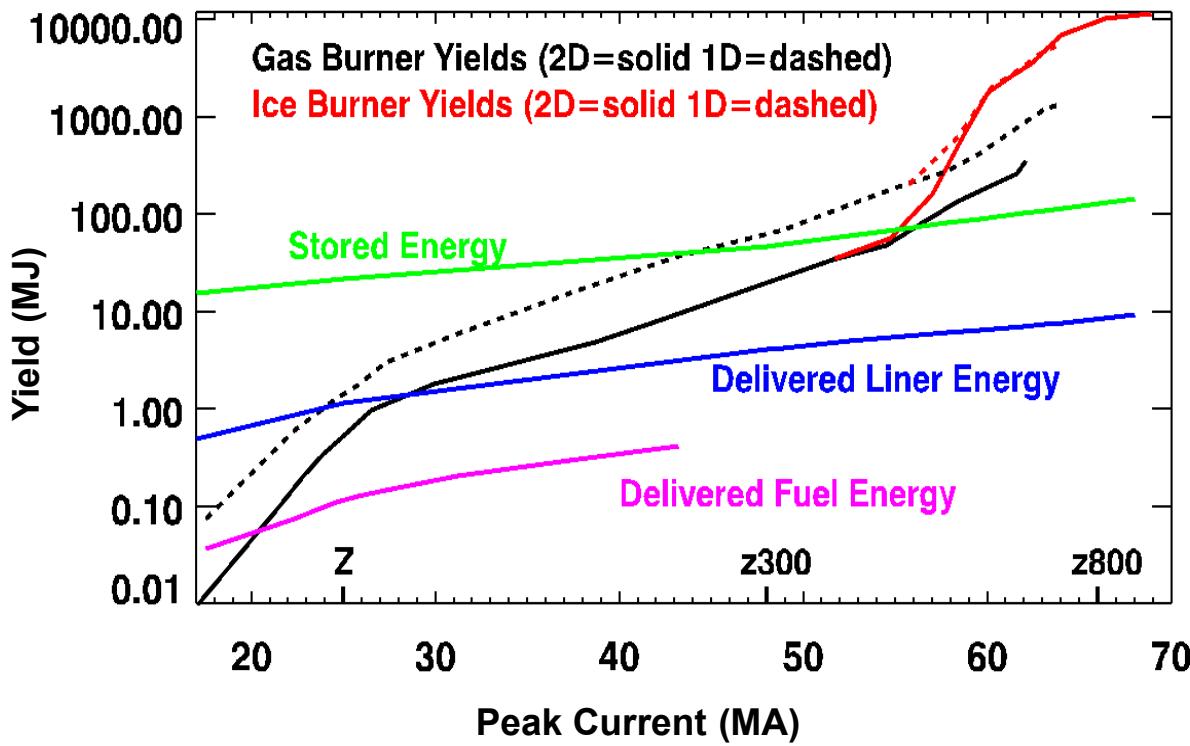
2D simulations predict yield increases with fuel preheat and applied B
Experiments will be performed to test these predictions

Simulations indicate that optimized yields are a strong function of current over the range accessible to Z



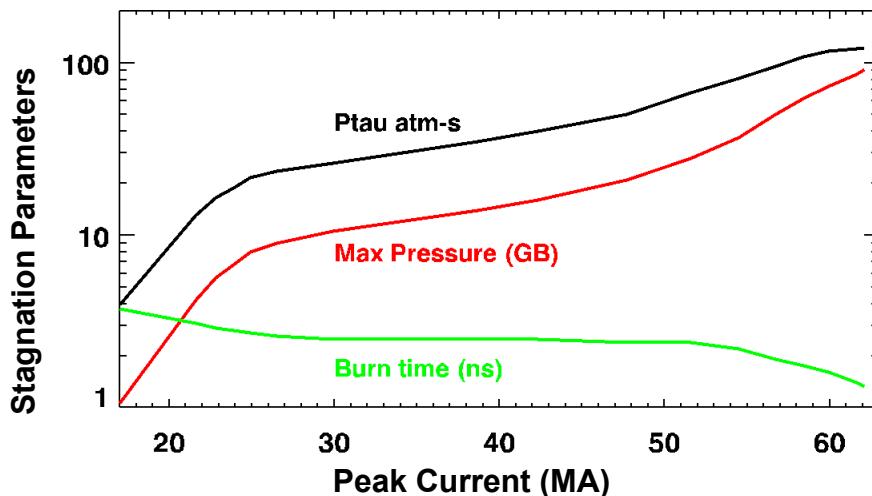
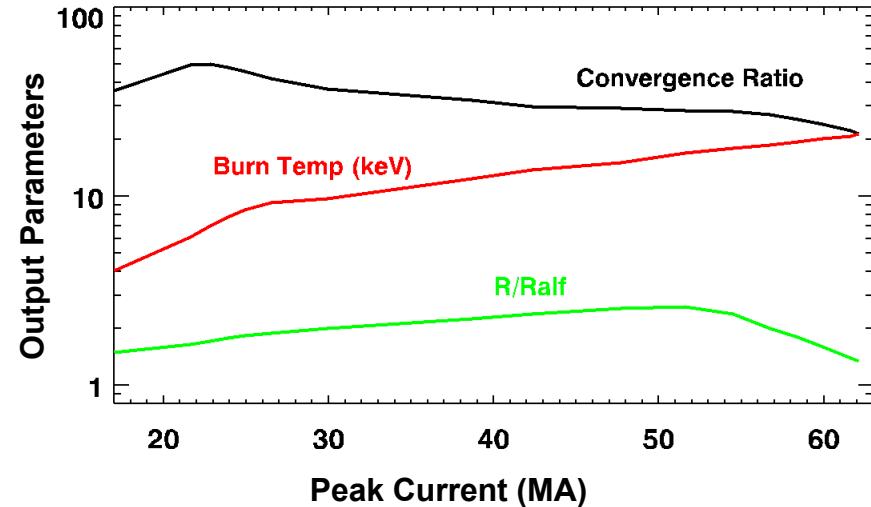
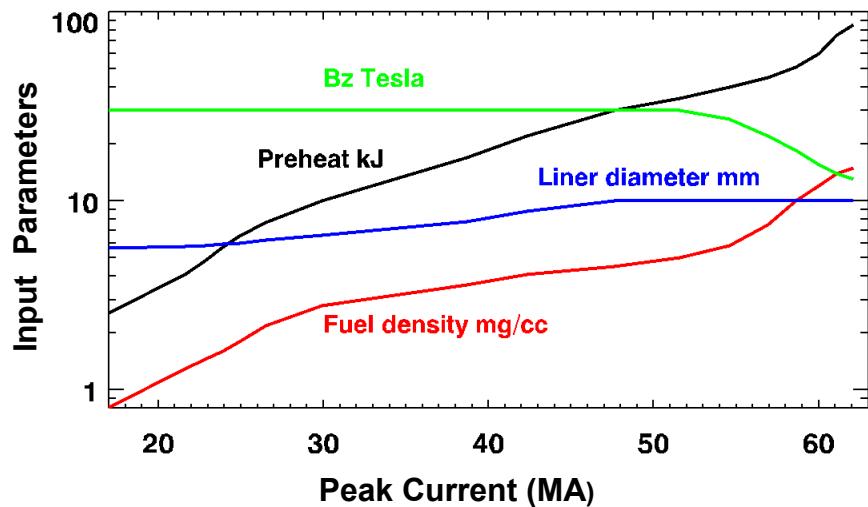
Capsule parameters (radius, fuel density, fuel preheat, and B_z) are optimized at each value of the drive current.

2D simulations indicate that Z300 could drive a MagLIF with gain greater than unity

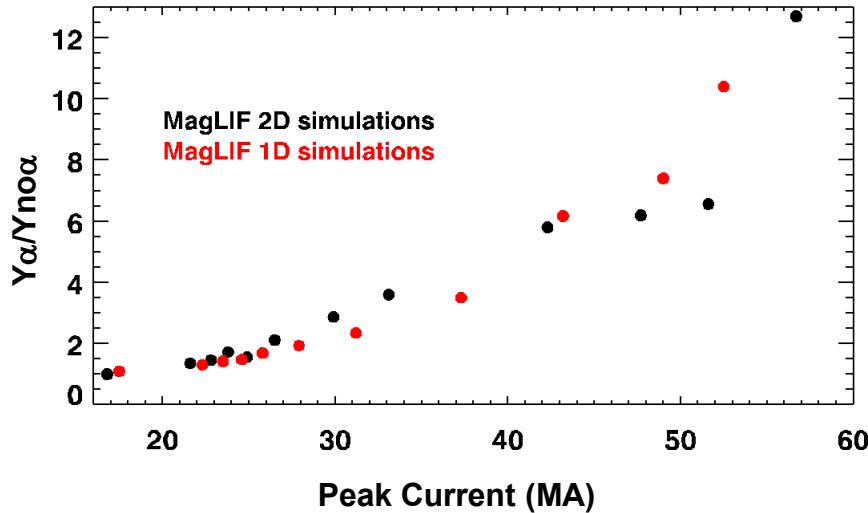


DT ice layers may significantly enhance yields for drive currents > 60 MA

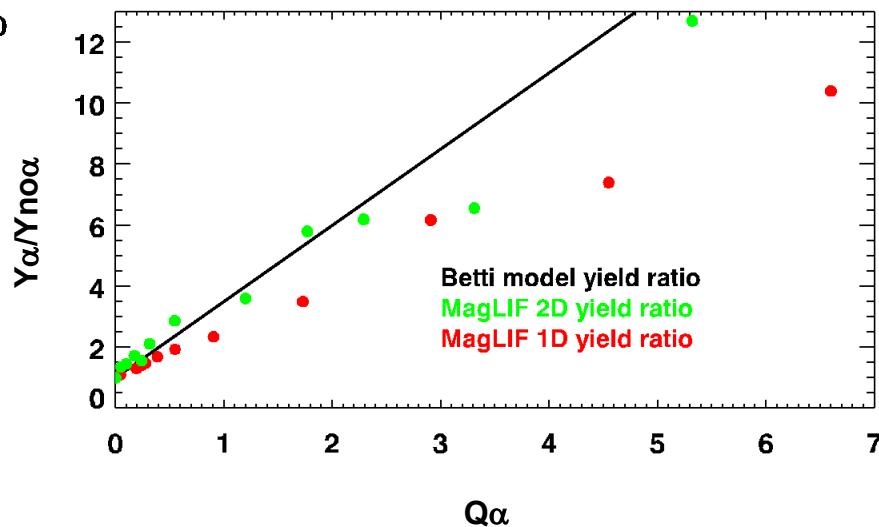
2D simulations indicate optimal design parameters and output quantities



The ratio of the yield with and without alpha particle heating can be used as an ignition metric¹



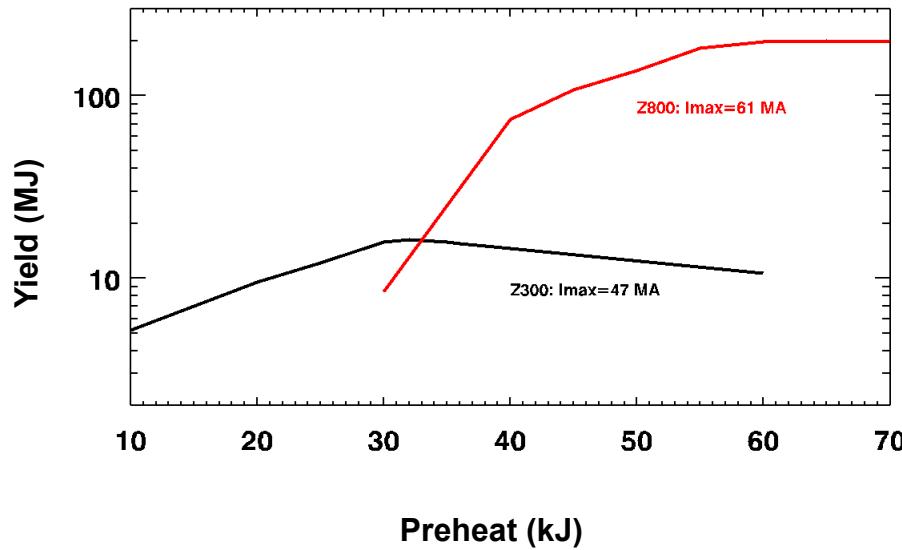
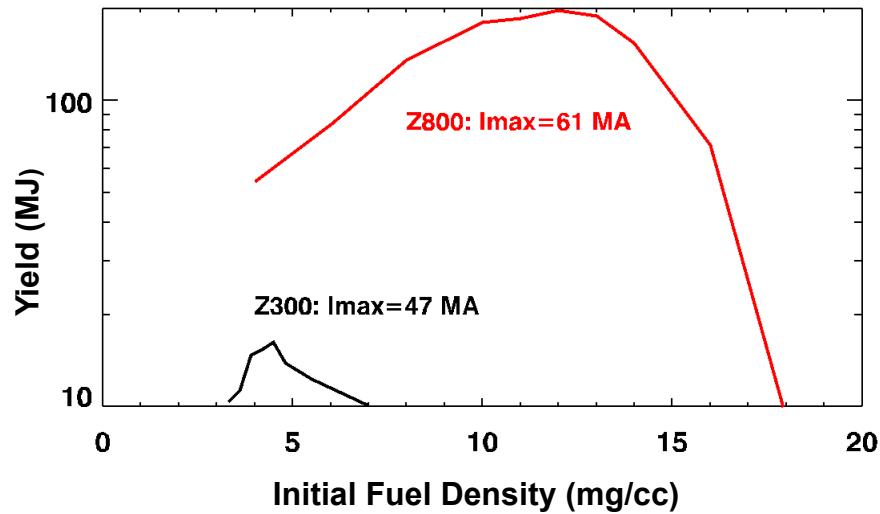
Defined Q_α : as the ratio of the fuel energy at peak burn with and without alpha deposition



¹Betti et al Phys. Rev. Lett. 114, 255003 2015

2D simulations indicate initial fuel density and preheat energies have broad optima

Lasnex simulations of Gas Burners

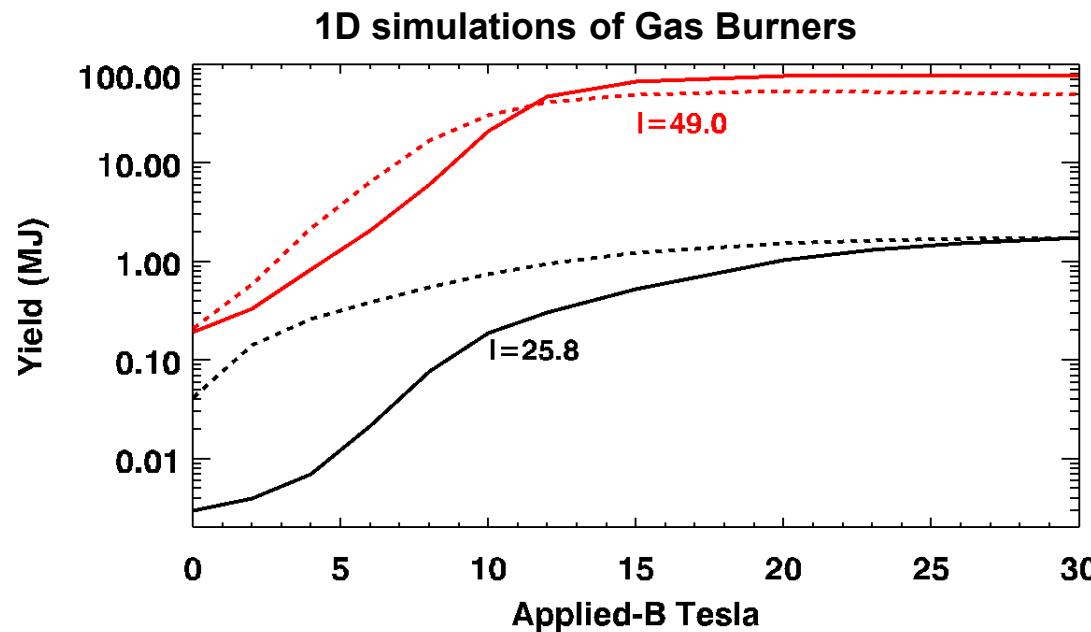


The Nernst effect can be significant

All of the preceding Lasnex simulations have included the Nernst (Ettingshausen) effect

Nernst produces an electric field E_{Nernst} proportional to $B \times \text{grad}(T)$

- The magnetic field is advected with a velocity proportional to E_{Nernst}/B
- The magnetic field is reduced in the hot core and increased near the fuel liner interface
- The effect is decreased when $\omega\tau$ is large and is not large for optimal B
- Experiments determining the yield as a function of B will determine the importance of this effect



Simple analytic theory predicts the laser penetration can be controlled by the beam radius



Laser absorption coefficient dominated by inverse Bremsstrahlung

$$C_V \frac{d\theta}{dt} = \frac{dI}{dz} = -kI \quad k = \frac{v_{ei}\omega_p^2}{c\omega_L^2} \left(1 - \frac{\omega_p^2}{\omega_L^2}\right)^{-1/2} = \frac{k_0}{\theta^{3/2}} \quad k_0 \approx 1.23 \times 10^6 (\rho \lambda_L Z_b)^2 (1 - 227 \rho Z_b \lambda_L^2)^{-1/2}$$

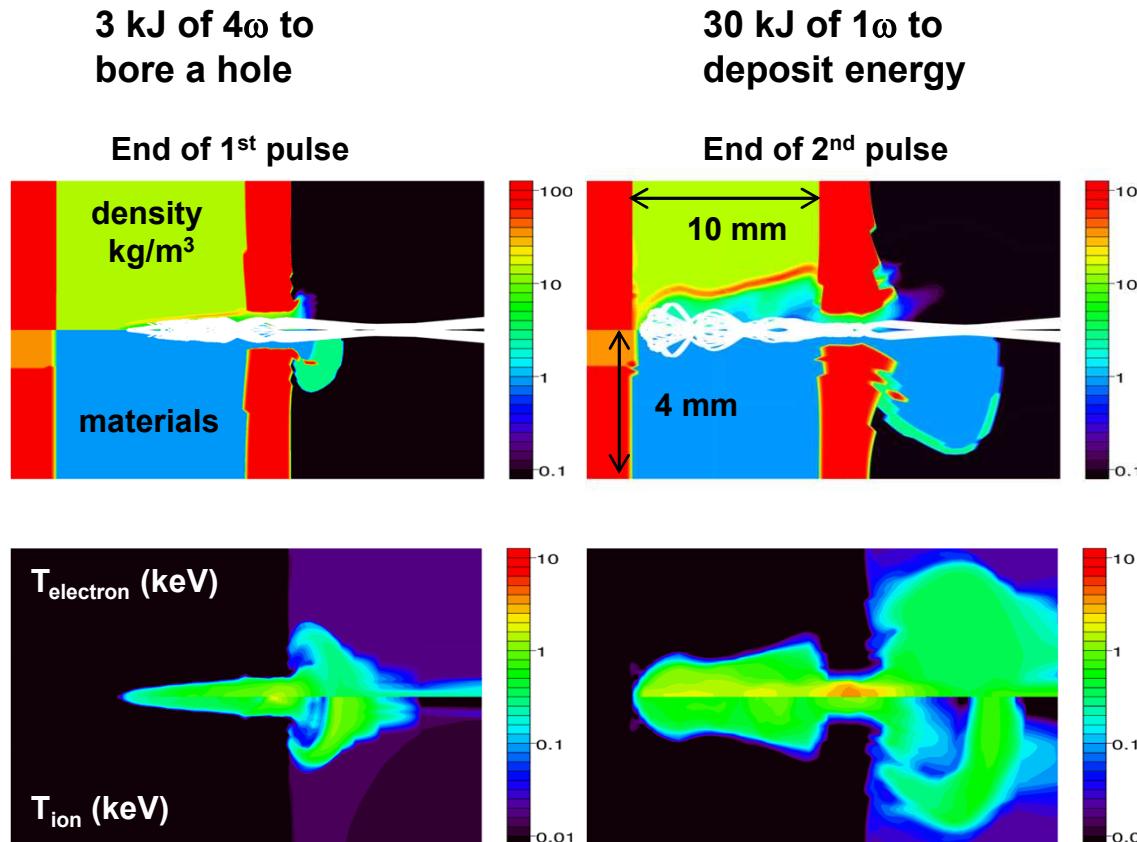
$$I = I_0 \left(1 - \frac{z}{z_f}\right)^{2/3} \quad z_f = \frac{5}{3} \left(\frac{2}{5k_0}\right)^{2/5} \left(\frac{I_0 t}{2C_V \rho}\right)^{3/5} \quad R_{laser} = 5.4 \times 10^{-7} E_{laser}^{1/2} \lambda_L^{-0.67} \rho^{-1.17} z_f^{-0.83} (1 - 227 \rho \lambda_L^2)^{1.17}$$

Hydrodynamics and refraction make this process more complicated

A short wavelength laser ($\lambda \sim 0.25\text{-}0.33 \mu$) could be used to penetrate the initially high density DT forming a low density channel

A second pulse of longer wavelength light ($\lambda = 0.5\text{-}1 \mu$) could then propagate down this channel and efficiently deposit its energy

2D Lasnex simulation of laser deposition indicates that 30 kJ can be absorbed in 1 cm of 12 mg/cc DT fuel



Laser plasma instabilities (LPI) could pose a problem for MagLIF preheat on future accelerators

LPI is unimportant if:

- the plasma density is much lower than the critical density ($n/n_{crit} \ll 1$)
- The laser intensity is low ($I_{Laser} < 10^{14}$ watts/cm 2)

Optimum fuel densities are larger on future accelerators

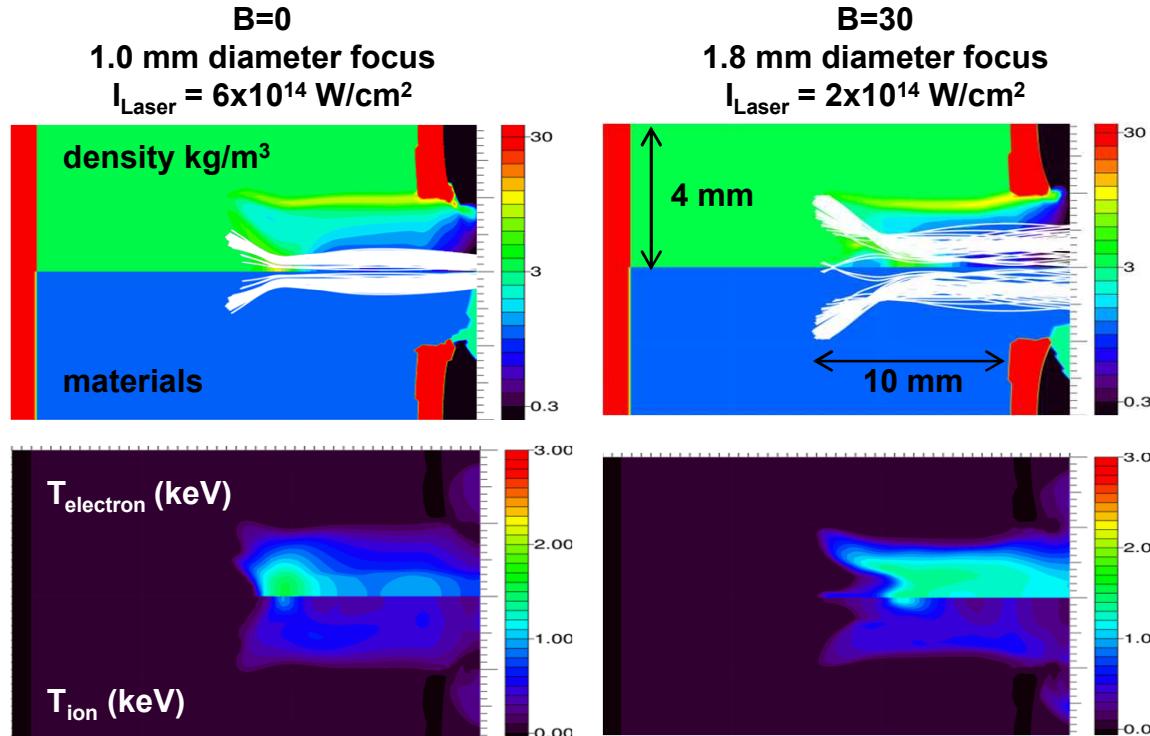
- Optimal fuel density ~ 5 mg/cc on Z300 ($n/n_{crit} \sim 0.13$) for 3ω

Optimum preheat energies are larger on future accelerators

- Optimum preheat ~ 30 kJ on Z300
- Laser pulse can not be too long or gas moves out of the way. Beam intensity may need to be $> 10^{14}$ watt/cm 2

Laser preheating at Z300 levels could be tested using a quad of NIF

30 kJ 3ω at 5 TW stopped in 1 cm of DT at 4.5 mg/cc



We have presented 1D and 2D simulations of MagLIF on upgraded Z and future machines



Simulations indicate that large yields and gains may be possible on a future machine such as Z300

Simulation predictive capability is greatest when the extrapolation is not large

Present experiments have been performed at 18 MA with B=10 Tesla and low preheat \sim 200 joules

- Phase plates have been designed of Z Beamlet to enable larger preheat energies
- 30 Tesla fields are possible with the existing field coil system
- An improved convolute design will be tested with MagLIF to obtain higher drive currents on Z

Full scale laser deposition experiments could be performed using one quad of the NIF to remove uncertainties about laser preheating

Agreement between the simulation scaling presented here and the results of experimental scaling will greatly increase our confidence to predict MagLIF performance on future machines