

# **The Derivation of Appropriate Laboratory Vibration Test Durations and Number of Shocks Hits from Non-Stationary Field Test Data\***

**86<sup>th</sup> Shock and Vibration Symposium.  
October 5-8, 2015  
Orlando Florida**

**Jerome S. Cap, Sandia National Laboratories**

**Melissa C' de Baca, Sandia National Laboratories**

\* Sandia is a multiprogram laboratory operated by Sandia Corporation, a Lockheed Martin Company, for the United States Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.



# Outline

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- **Vibration Damage Model**
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- **Shock Test Results**
- **Using Test Specification as Reference**



## Purpose of Study

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- **A series of field tests were recently conducted with the goal of establishing the Maximum Predicted Environment (MPE)**
  - **Using the total measured durations and/or number hits with the MPE spectra to define a test is overly conservative**
- **The purpose of this study was to derive the optimal durations / # of hits for use when testing with the MPE spectra**



# Description of Field Test

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- **The field test consisted of two phases**
  - **A long distance road test (60+ hours of data)**
  - **A series of short distance in-house handling operations using forklifts and motorized carts (minutes of data)**
- **Ensembles of vibration and shock acceleration histories were collected and grouped by test configuration**
  - **Skyline plots were used to separate shocks from vibration**
  - **Vibration data are presented as Acceleration Spectral Densities (ASDs)**
  - **Shock data are presented as Shock Response Spectra (SRS)**



# Description of Field Test

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- **The number of measured vibration events were defined based on the analysis segment duration (30 seconds)**
  - **A 720 minute test have 1440 events**
- **The number of measured shock events were taken directly from the skyline analysis**



# Maximum Predicted Environment (MPE)

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- The P99/90 MPE responses were generated from the measured field data
- For large sample sets a Distribution Free Tolerance Limit (DFTL) model was used
  - Simple rank ordering of the ensemble
  - Bootstrap realizations were used to increase confidence
- For small sample sets a Lognormal Tolerance Limit model (NASA 7005) was used

$$Y = \log(X)$$

$$Y_{MPE} = \mu + k\sigma$$

$$X_{MPE} = 10^{Y_{MPE}}$$



# Power Law Fatigue Damage Model

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- Many references document the use of a power law fatigue damage model (Minor's Rule) to shorten the duration associated with a vibration environment

$$(G2/G1) = (T1/T2)^b$$



# Vibration Damage Model

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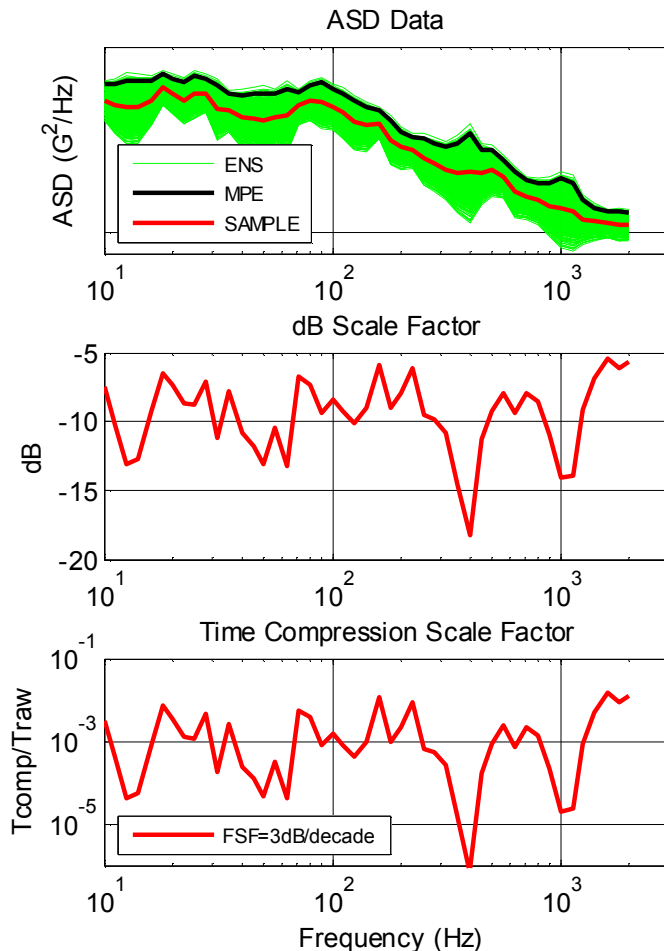
- For each random vibration event use the MPE ASD,  $S_{mpe}$ , and the individual ASD,  $S_i$ , to compute the compressed time,  $T_c$ , from the baseline time,  $T_i$

$$\log\left(\frac{S_{mpe}}{S_i}\right) = 2b * \log\left(\frac{T_i}{T_c}\right)$$

- The definition of dB is simply left hand side of this equation multiplied by 10
- The scaling is applied frequency by frequency



# Frequency Dependent Compression Example



- Compute dB ratio for MPE and sample ASDs
- Compute compressed time using fatigue scale factor
  - 3dB/decade
- Sum by frequency for each curve in the ensemble
  - The final duration is the maximum of the frequency specific sums



# Vibration Damage Model Ensembles

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- **Even for cases where there were hundreds of data points there is no guarantee that the ensemble is statistically significant**
- **The solution was to generate ensembles based on the sample statistics**
  - **The mean,  $\mu$ , was computed from the “as measured” data**
  - **The standard deviation,  $\sigma$ , was computed based on the fact that the P99/90 spectra is  $\approx$  equal to  $\mu + 2.33\sigma$**
  - **The desired # of events was defined by multiplying the measured # of events by the ratio of the desired duration divided by the measured duration**
- **This approach was used for both dense and sparse data sets**

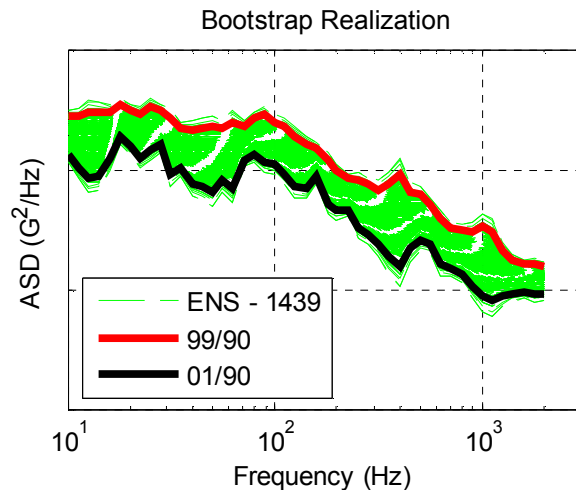
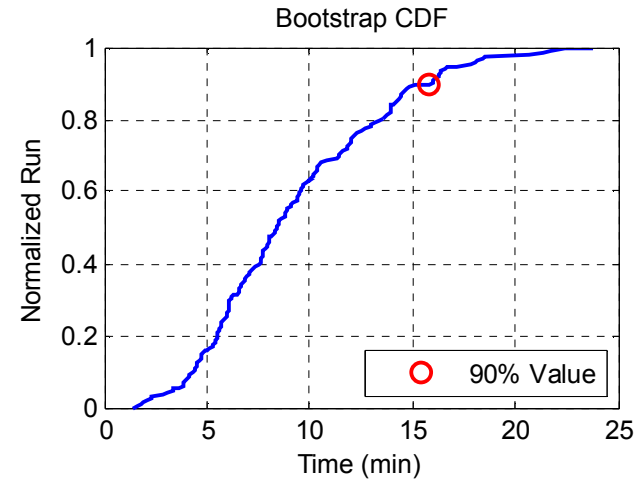
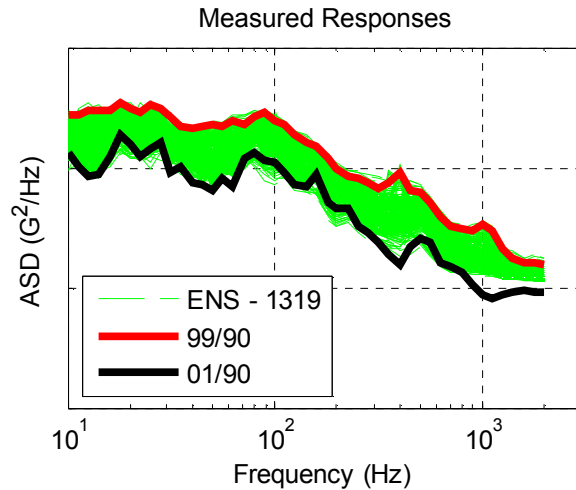


# Vibration Damage Model Confidence

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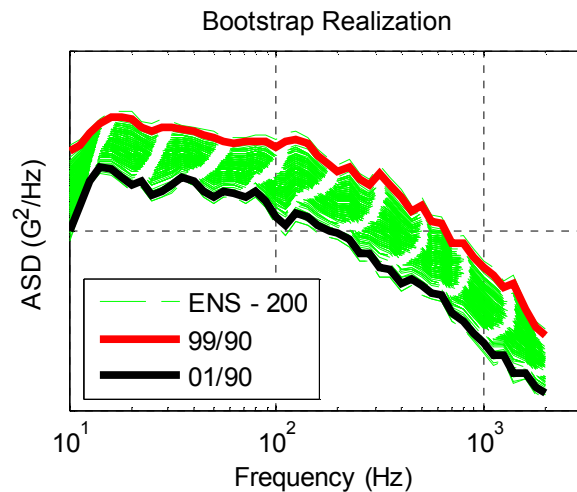
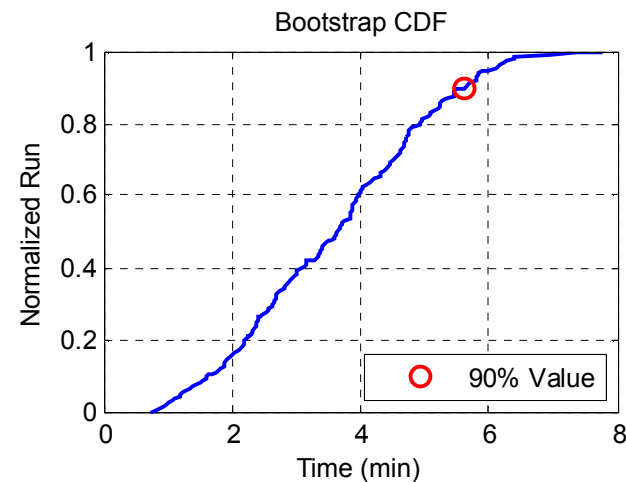
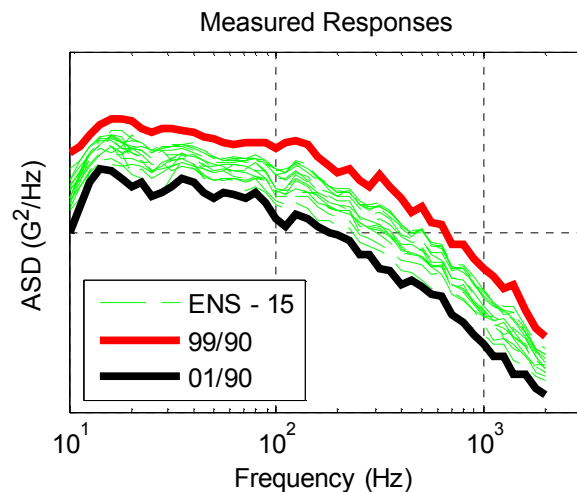
- **The compressed duration for a single ensemble does not provide sufficient confidence in the results**
- **Bootstrap sampling was used to generate multiple realizations of the desired ensemble**
  - **The resulting collection of compressed durations are then ranked in ascending order**
  - **The 90% highest value is used to define the worst case duration**

# Example for Large Vibration Sample Set



Field Duration: 720 min  
Compressed Duration: 15.5 min

# Example for Small Vibration Sample Set



Field Duration: 100 min  
Compressed Duration: 5.7 min



# Shock Damage Model

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- **Transportation and handling shocks tend to be oscillatory in nature and comparable in magnitude to the background vibration**
- **This allows us to treat the shocks as just another portion of a large cycle fatigue environment**



# Shock Damage Model

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- Use the MPE SRS,  $G_{mpe}$ , and the individual SRS,  $G_i$ , to compute the compressed time,  $T_c$ , from the baseline time,  $T_i$

$$\log\left(\frac{G_{mpe}}{G_i}\right) = b * \log\left(\frac{T_i}{T_c}\right)$$

- The scaling is applied frequency by frequency



# Shock Damage Model

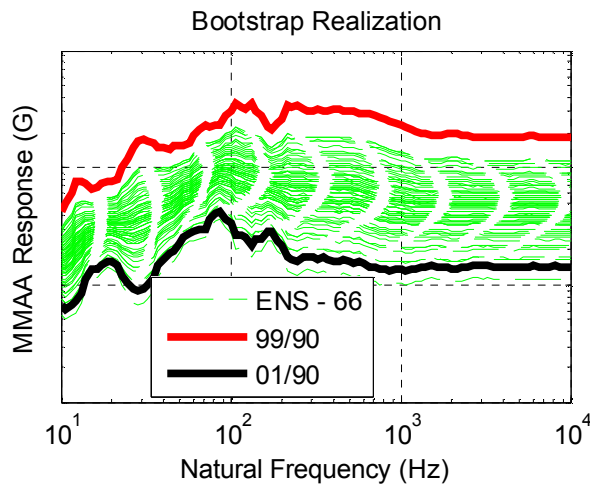
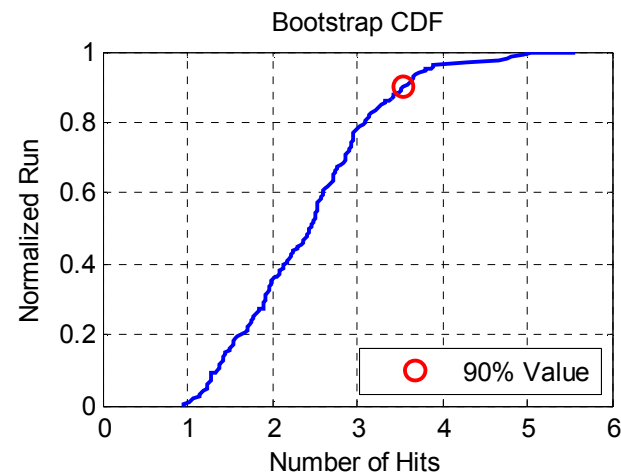
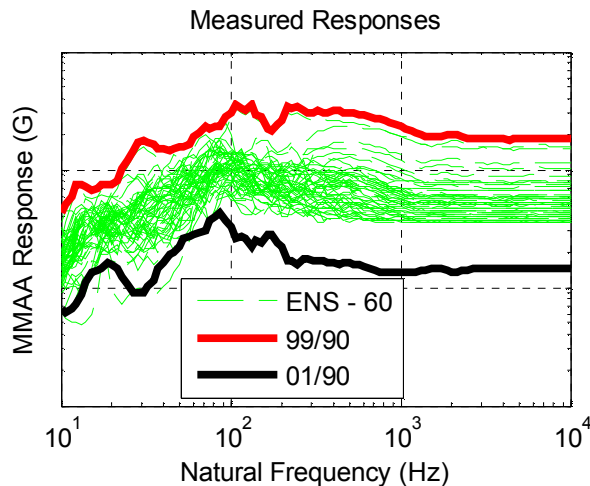
## Ensembles and Confidence

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- **Just as was done for the vibration ensembles, SRS ensembles were generated using the sample statistics**
  - The desired # of field hits,  $N$ , were defined as the measured number of hits multiplied by the ratio of the desired field duration divided by the measured field duration
  - The compressed number of hits were computed as the maximum of the frequency specific hit totals for the ensemble
- **Bootstrap realizations were used to generate the 90% confidence number of compressed hits**



# Example for Shock Sample Set



Field Hits: 66 hits  
Compressed Hits: 3.5 hits  
(round up to 4)

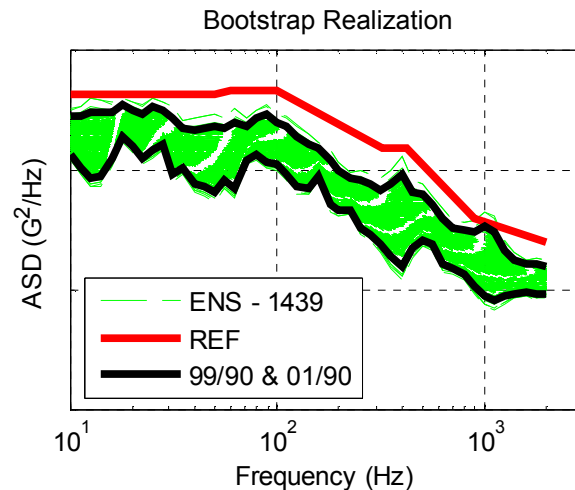
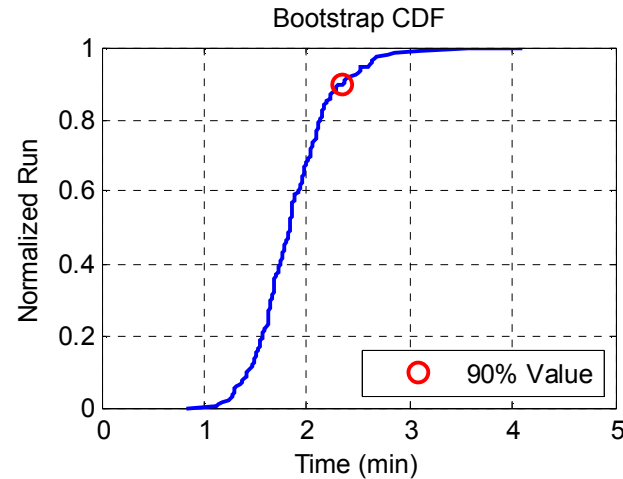
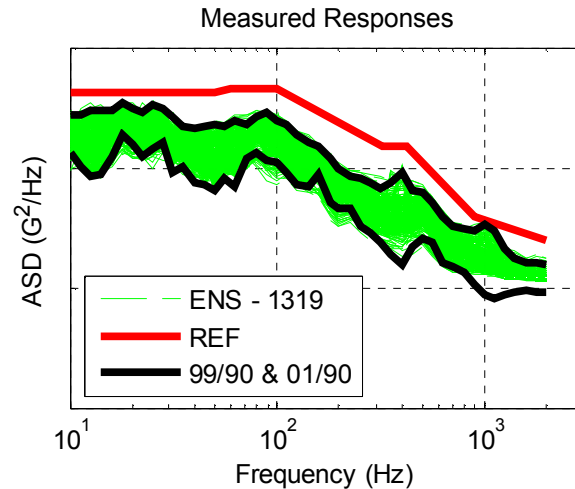


# Using Test Specifications as the Reference

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- **Until now all of the examples have used the P99/90 MPE spectra as the basis for computing the compressed durations and number of hits**
- **Often the actual test specification is higher (enveloping other environments, etc.)**
  - **Allows for greater time compression**

# Example of Test Specification Reference



Duration (Re: MPE): 15.5 min  
Duration (Re: Spec): 2.5 min



# Observations

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- **The compression rates for the same road type varied based on tie down scheme**
  - **More loosely tied down packages exhibited more variation and hence higher MPE responses**
  - **This actually resulted in higher compression rates**
- **The long haul road compression rates are higher than defined in Mil-Std 810**
  - **40:1 for this test**
  - **16:1 for Mil-Std 810**
  - **We believe that this is at least partly due to the fact that we were shipping light weight, loosely constrained packages**



# Summary

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- **The methodology described in this presentation can be used to identify the appropriate vibration duration and/or number of shock hits associated with using the MPE spectra to define a test**