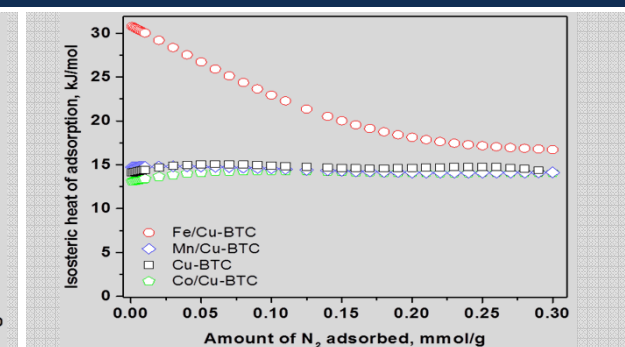
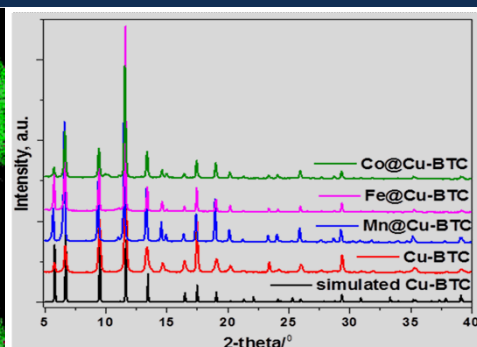
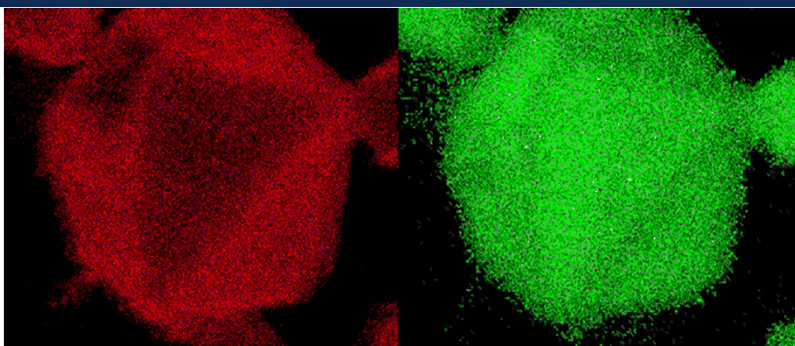


Exceptional service in the national interest



Light Gas Separations with MOFs via Predictive Modeling and Tuned Synthesis

Tina M. Nenoff, Dorina F. Sava Gallis, Marie V. Parkes, Jeffery A. Greathouse, Mark A. Rodriguez, Scott M. Paap, and Christopher R. Shaddix

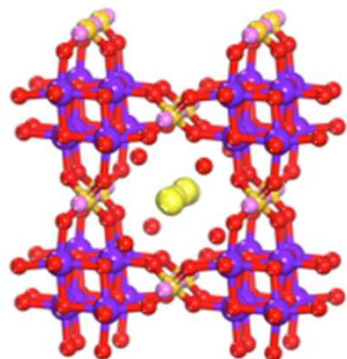
Sandia National Laboratories, Albuquerque NM & Livermore CA, USA

6th Microporous and Mesoporous Materials Symposium
Sunset-Black Sea, Bulgaria
September 8, 2015



This work is supported by the Laboratory Directed Research and Development Program at Sandia National Laboratories. Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.

Novel SNL Separations and Waste Forms: Technologies for Environment and Energy Applications



R&D100 1996

JACerS, 2009, 92(9), 2144

JACerS, 2011, 94(9), 3053

Solvent Extr. & Ion Exch, 2012, 30, 33

**CST, Cs⁺ removal from
water to Pollucite Waste Form**

US Patents 6,479,427; 6,110,378

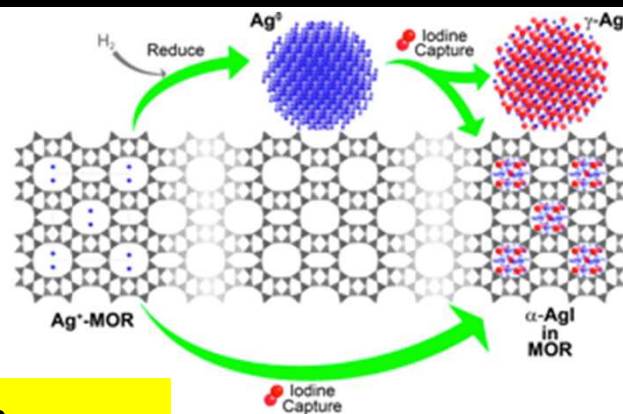
**I₂/ZIF-8, Isolation
to Waste Form**

JACS, 2011, 133(32), 12398

US Patent filed 2012

JACS 2013, 135, 16256

**Fundamental Research to
Applied to Commercial Products
Design the Separation Material
To Develop the Waste Form**



Ag-MOR

**I₂(g) capture &
mechanisms**

JACS, 2010, 132(26), 8897

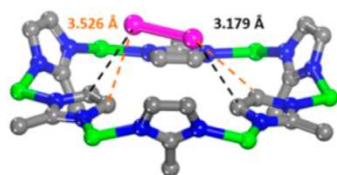
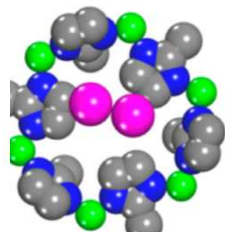
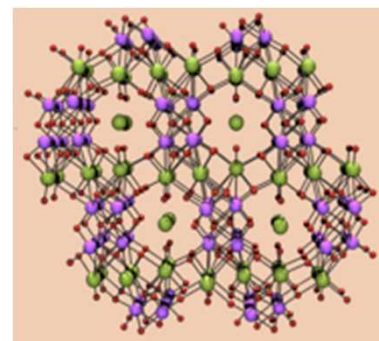
J Phys Chem Letters, 2011,
2, 2742

SOMS, Sr²⁺ getter,

1-step to Perovskite WF

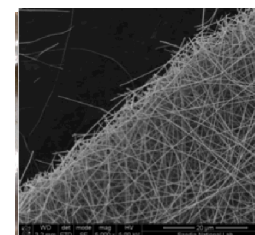
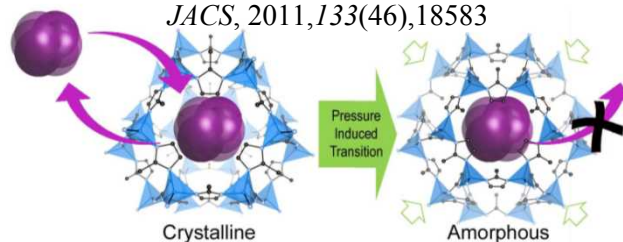
JACS, 2002, 124(3), 1704

US Patent 7,122,164



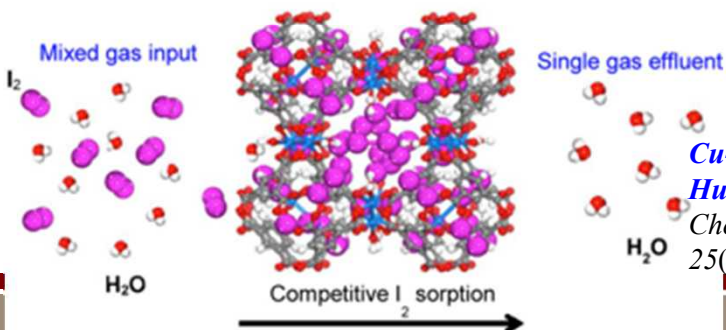
MOF Amorphization for Gas Storage

JACS, 2011, 133(46), 18583



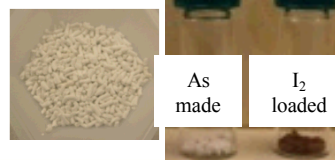
**Nanoporous Nanofibers
Volatile Gas Removal**

US Patent Application, 2011



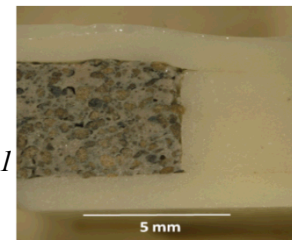
**Cu-BTC: I₂ from
Humid Gas Stream**

Chem. Mater. 2013,
25(13), 2591



**Binder Free MOF
Pelletization**

US Patent
Pending 2014

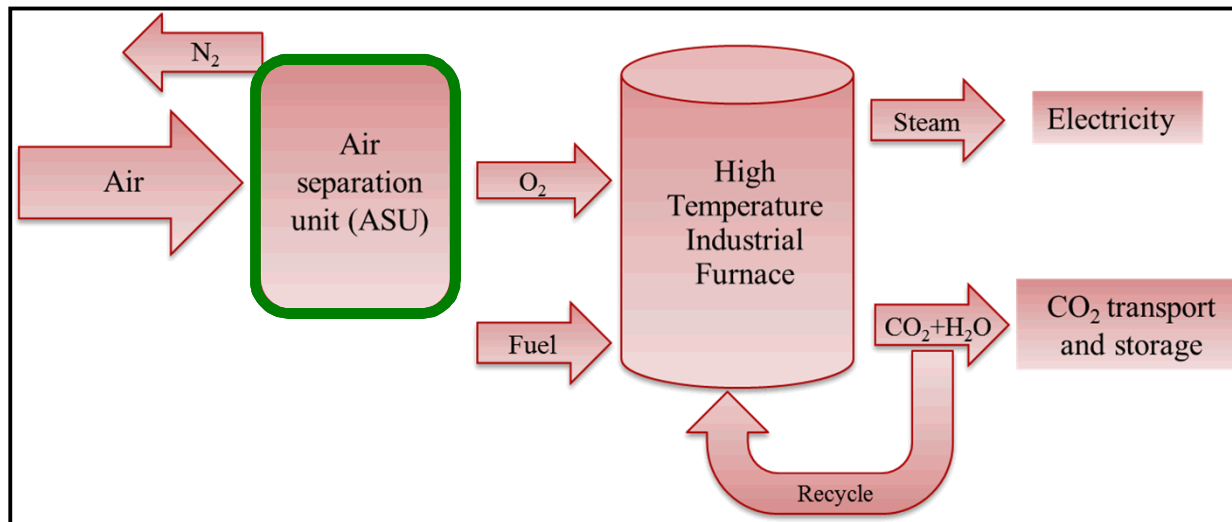


**Universal Core-Shell Iodine
Glass Waste Form & Getter**

JACerS, 2011, 94(8), 2412

US Patent 8,262,950: 2012

O_2/N_2 air separations with MOFs to Increase the Efficiency of the *ASU*



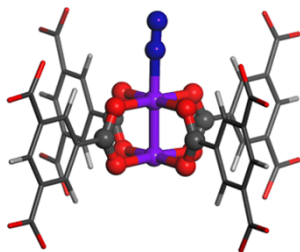
- Oxygen-enriched (oxy-fuel) combustion: burning the fossil fuel in an O_2 rich atmosphere results in a flue gas composed mainly of CO_2 and water (little or no SO_x and NO_x emissions)
- The limiting factor of this technology is the efficiency of the cryogenic ASU, a costly and energy intensive process (primarily compression)
- Our study is focused on new highly selective materials to increase the efficiency of this separation process

Goal: determine the O_2 and N_2 uptake dependency with temperature in MOFs with coordinatively unsaturated metal sites

Integrated Research Plan: Modeling, Materials Development, Combustion Testing, & Systems Analysis

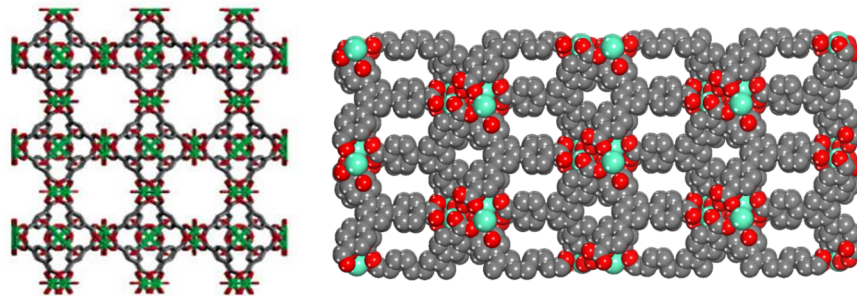
Predictive molecular modeling

Predictive molecular modeling designed to *measure the binding energy for O_2 and N_2* on coordinatively unsaturated metal sites in MOFs



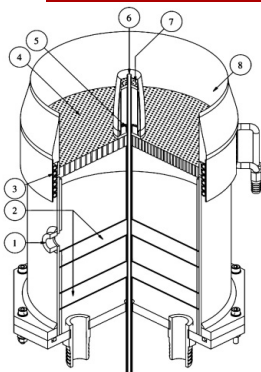
Materials development

Guided by the modeling results, experiments are directed at both the *synthesis of analogs of known/modified materials and of novel frameworks.*



New burner design

New lab burner constructed to mimic practical oxy-fuel combustion in industrial applications: coupling burner design and oxy-fuel combustion to radiant heat transfer



Balloon number	Description
1	Flushback over-pressure sensing port
2	Glass bead filled cavity
3	Cooling water coil
4	Collow perforated baseplate
5	Pilot mixture feed exit
6	Central jet exit
7	Pilot perforated baseplate
8	Collow collar

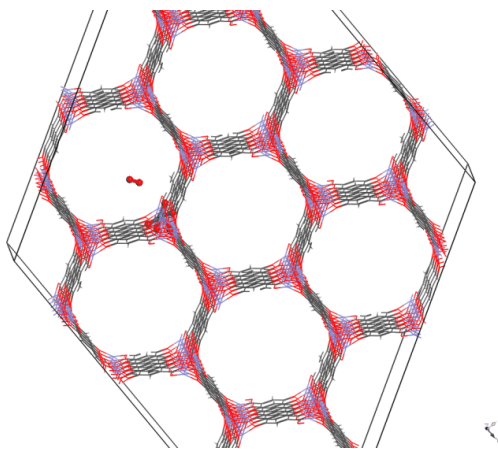
Schematic diagram of the modified version of the Cabra Burner developed by Dunn et al. (Combust. Flame, 2007, 151, 46)- studying flame attachment in hot combustion products

Systems Analysis

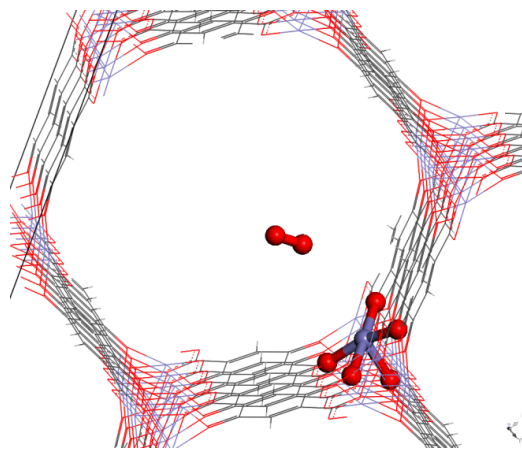
Data input to Systems Analysis for calculations of efficiency improvements of combined developed MOFs into Oxy-fuel Process Stream

Input information/data from combustion to systems analysis for calculation of percent efficiency improvements

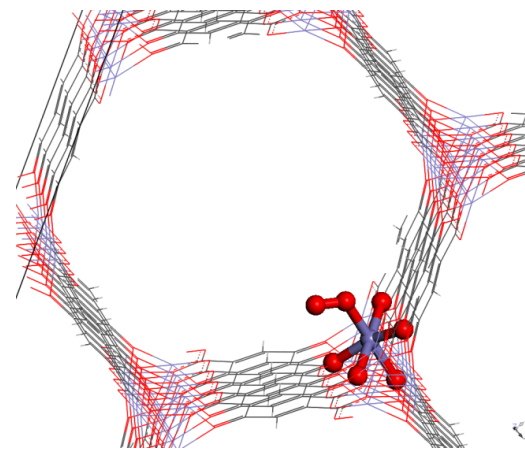
- MOFs with coordinatively unsaturated metal centers are promising materials for O₂/N₂ separations
- Two prototypical MOFs from this category, **Cr₂(BTC)₃** (*J. Am. Chem. Soc.* **2010**, *132*, 7856–7857) and **Fe₂(DOBDC)** (*J. Am. Chem. Soc.* **2011**, *133*, 14814–14822) both show preferential adsorption of O₂ over N₂
- Plane wave DFT calculations were performed on periodic structures in the [Vienna Ab initio Simulation Package \(VASP\)](#)
- Binding geometries for side-on and bent O₂ and bent and linear geometries for N₂ were evaluated
- Static binding energies for O₂ and N₂ at 0 K



MOF with O₂ in pore

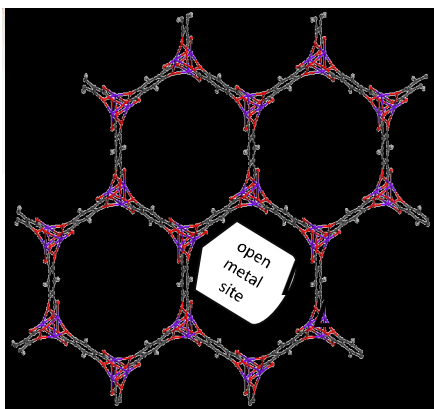


O₂ ready to bind to metal

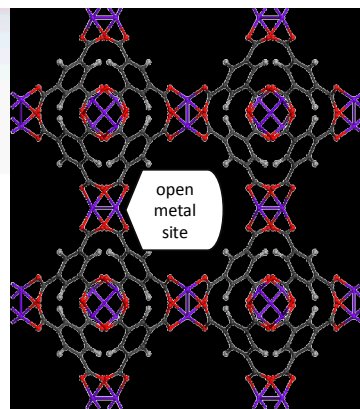


O₂ bound to metal

DFT modeling of of Oxygen Adsorption in Varied Metal-Centered MOFs



$M_2(\text{dobdc})$



$M_3(\text{btc})_2$

Plan wave density functional theory (DFT) calculations were performed on periodic structures of each MOF in the Vienna ab initio simulation package (**VASP**) with the Perdew-Burke-Ernzerhof (**PBE**) functional including dispersion corrections (**DFT-D2**). Geometries were optimized and **static binding energies** (ΔE_{O_2} , ΔE_{N_2}) were calculated by

$$\Delta E_{O_2} = E_{MOF+O_2} - E_{MOF} - E_{O_2}$$

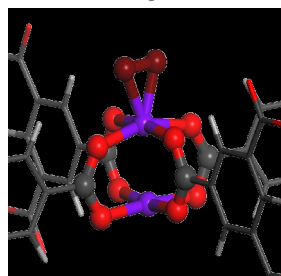
The **differences in binding energies** ($\Delta \Delta E$) for oxygen and nitrogen were calculated by

$$\Delta \Delta E = -(\Delta E_{O_2} - \Delta E_{N_2})$$

MOF metal sites = separate O_2/N_2 by differences in bonding & electronic properties

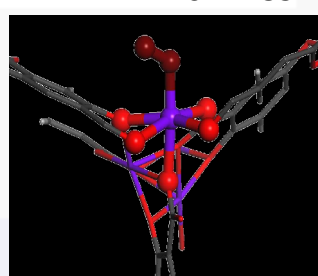
Attention Paid to Bonding Geometries

Side-on bonding
 $\angle M-X-X$ $67^\circ - 71^\circ$



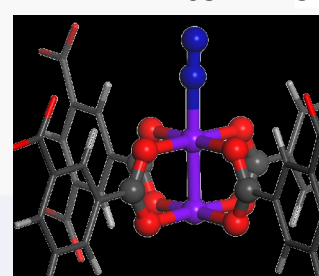
$\text{Cr}_3(\text{btc})_2(\text{O}_2)$

Bent bonding
 $\angle M-X-X$ $116^\circ - 159^\circ$



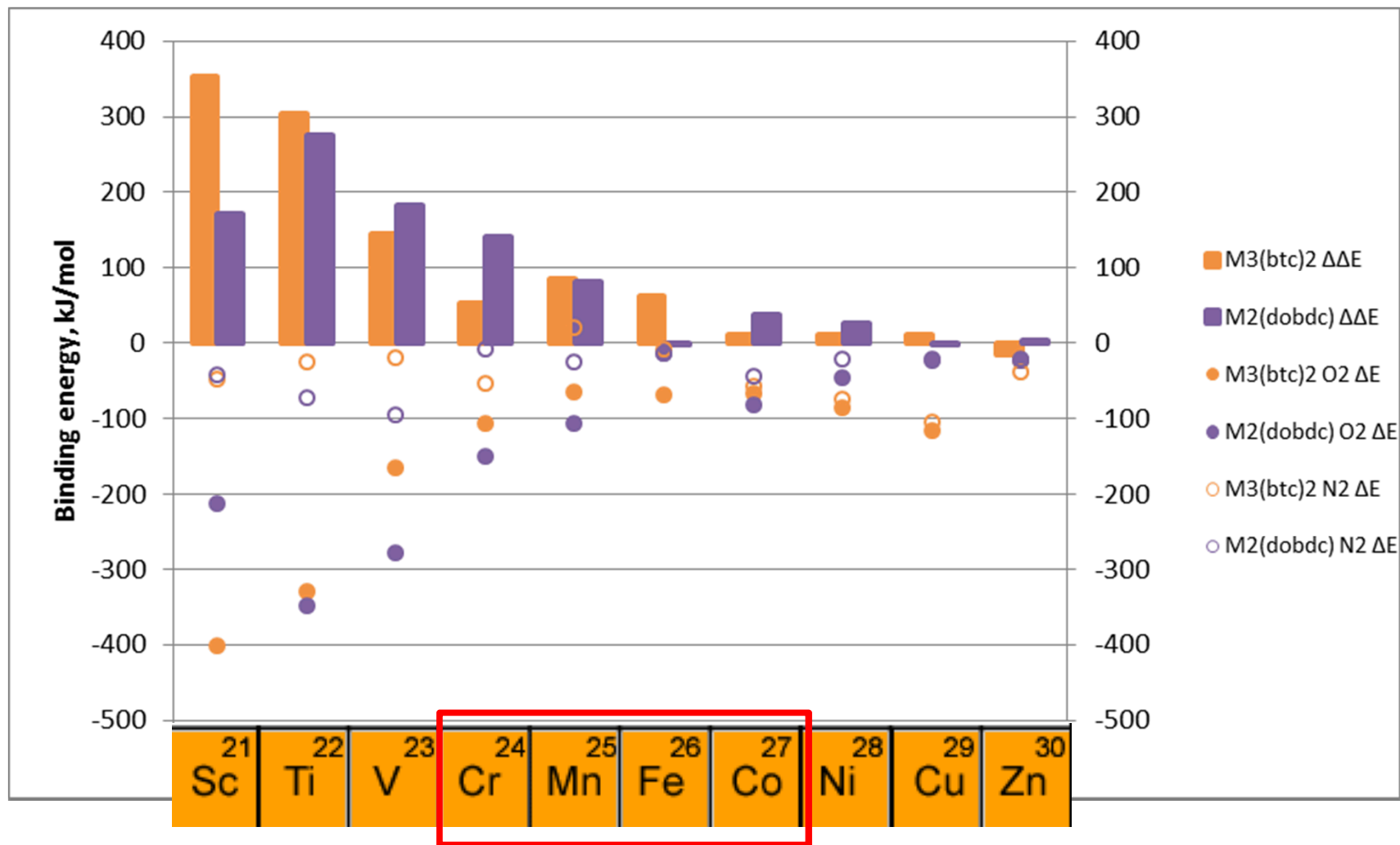
$\text{Mn}_2(\text{dobdc})(\text{O}_2)$

Linear bonding
 $\angle M-X-X$ $165^\circ - 179^\circ$



$\text{Fe}_3(\text{btc})_2(\text{N}_2)$

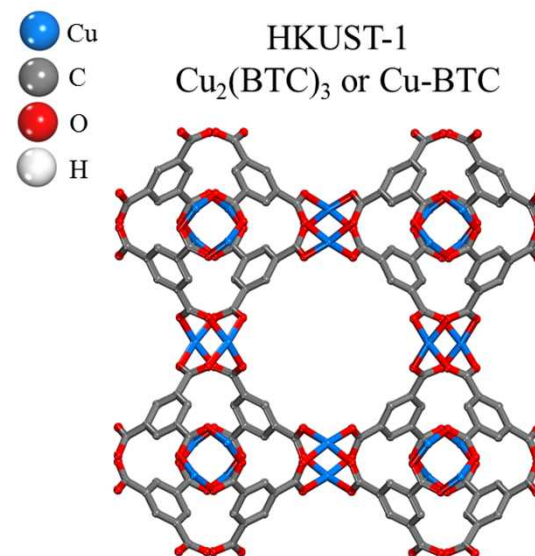
O₂ and N₂ binding energies trends across the first row transition metal series



Targeted Synthesis of Porous Mn-, Fe- and Co- Analogues of Cu-BTC

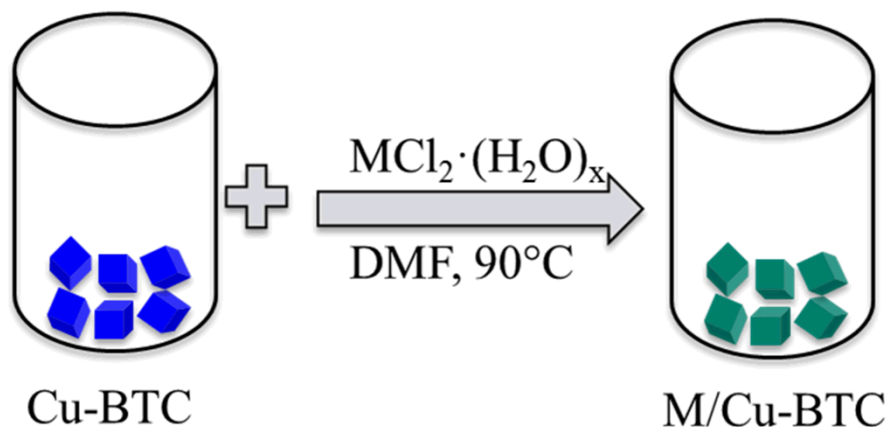
Need/Desire To Retain Porosity of MOF For Studies of Metal-O₂ Bonding Effects

- The effect of Porous analogues of Cu-BTC include: Cr, Mo, Ru, Ni (the Ru and Ni have much lower than expected surface areas, 1000-1100 m²/g)
- Porphyrin-templated Mn-, Fe- and Co- Cu-BTC analogues known, however no measurable accessible porosity (*J. Am. Chem. Soc.* **2012**, 134, 928–933)



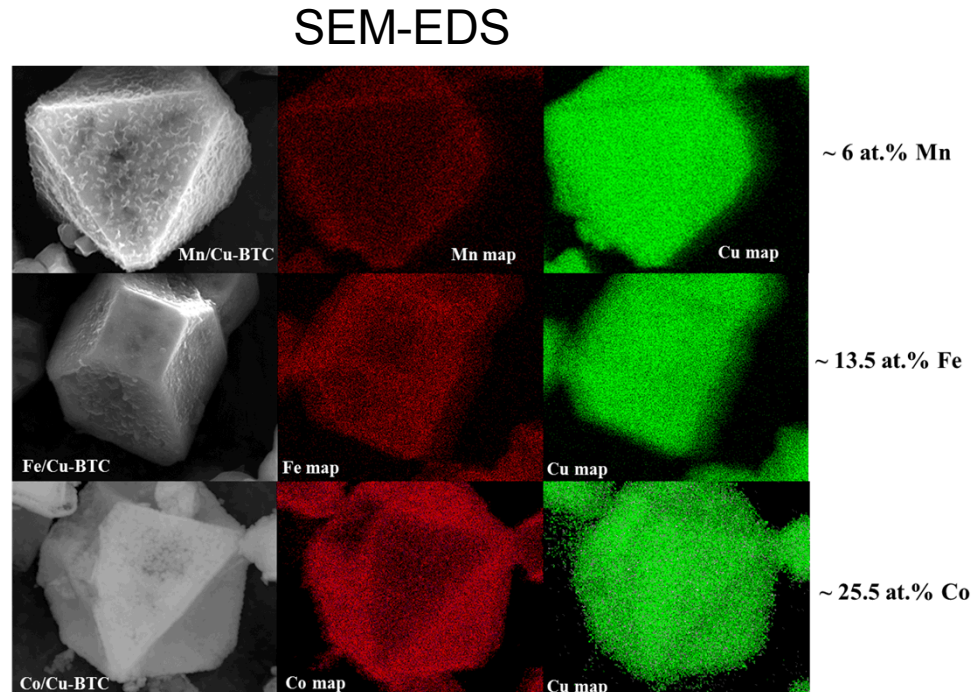
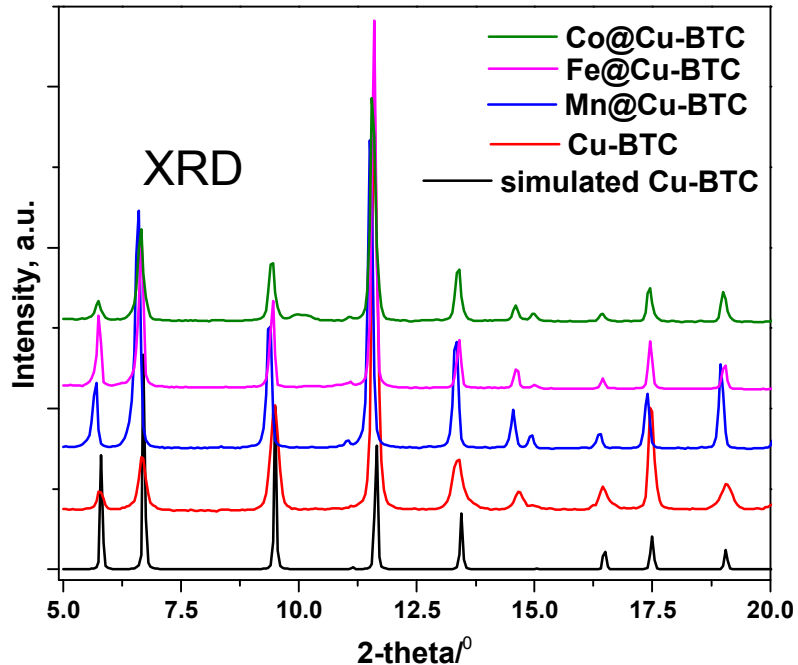
Chui, S. S. Y et.al Science **1999**, 283, 1148.

Postsynthetic metal ion exchange

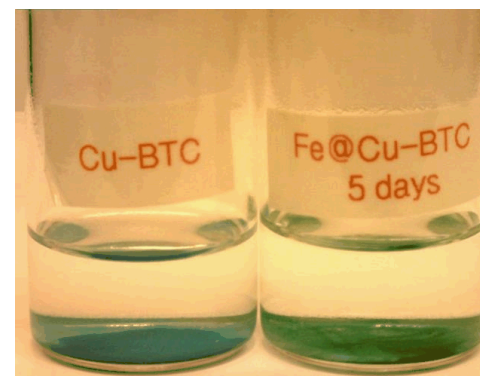


M = Mn, Fe, Co

Confirmation of In-Framework Metal Substitution – Unit Cell Expansion & Elemental Mapping



	Expansion (Å)	M-O average bond length (Å)
Cu-BTC	—	1.7
Co/Cu-BTC	0.043	2.08
Fe/Cu-BTC	0.019	2.0
Mn/Cu-BTC	0.030	2.17

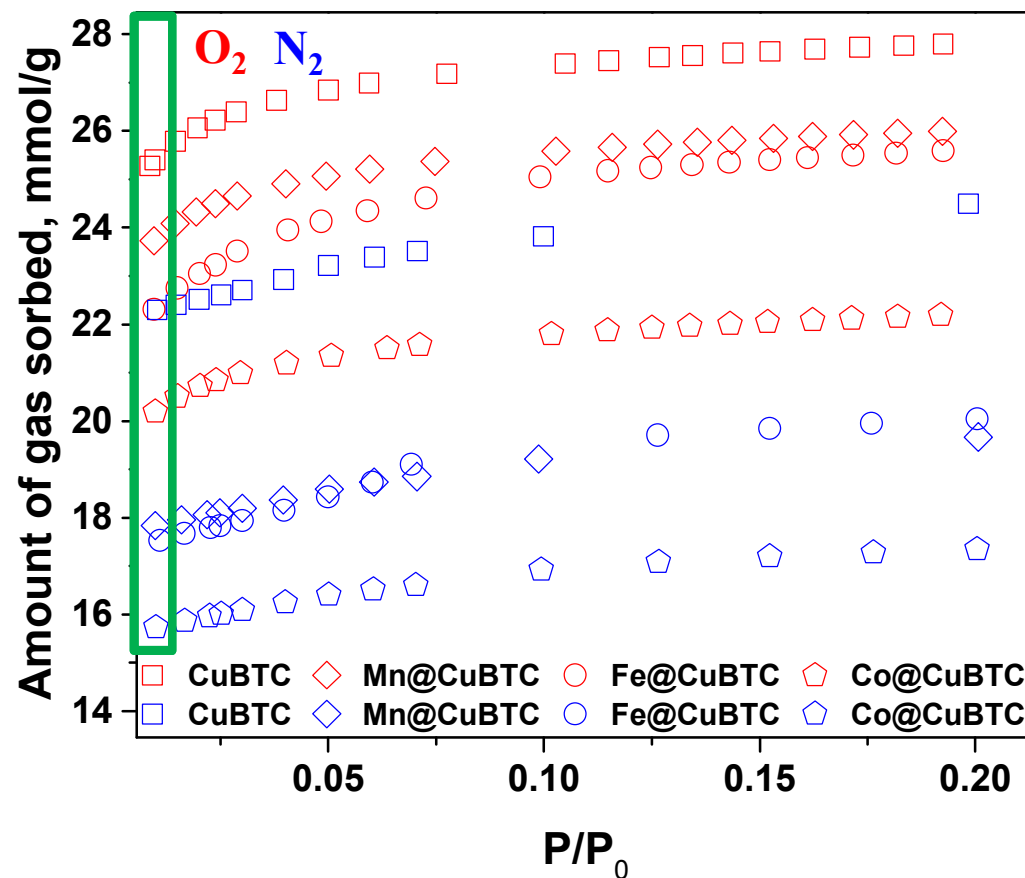


Excellent DFT and Experiment Correlation at Low Temperature and Low Pressure

Cu>Mn>Fe>Co (DFT)
Cu>Mn>Fe>Co (exp)

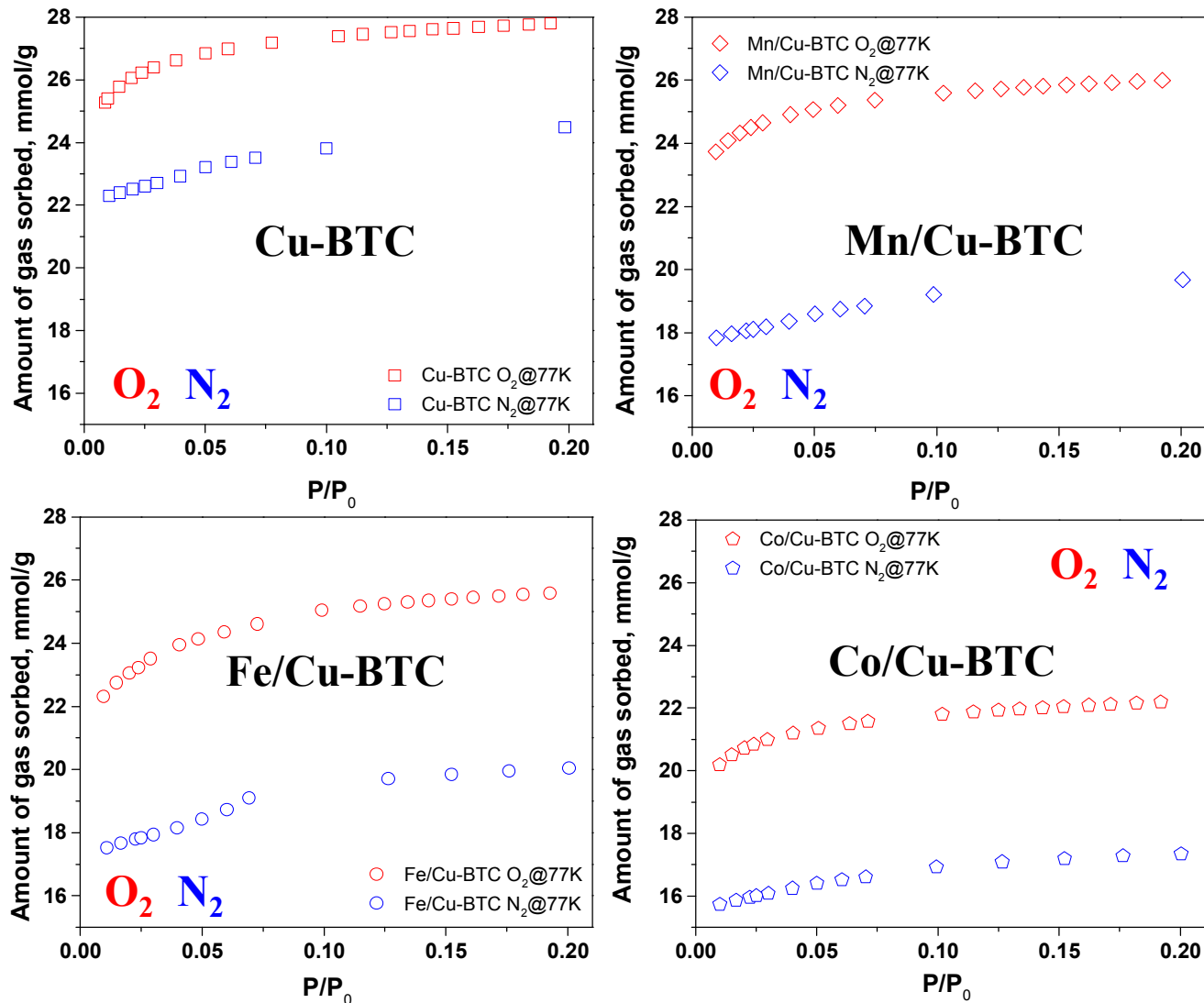
	DFT O ₂ binding energy, kJ/mol	DFT N ₂ binding energy, kJ/mol
Cu-BTC	-116	-105
Mn/Cu-BTC	-113	-97
Fe/Cu-BTC	-110	-92
Co/Cu-BTC	-104	-93

For uptake at the lowest partial pressure measured ($\sim 0.01 P/P_0$)



O_2 (red) and N_2 (blue) adsorption isotherms measured at 77K on pristine Cu-BTC and Mn-, Fe-, and Co-substituted samples

77 K: All Samples have *Higher* O₂ Loadings over N₂

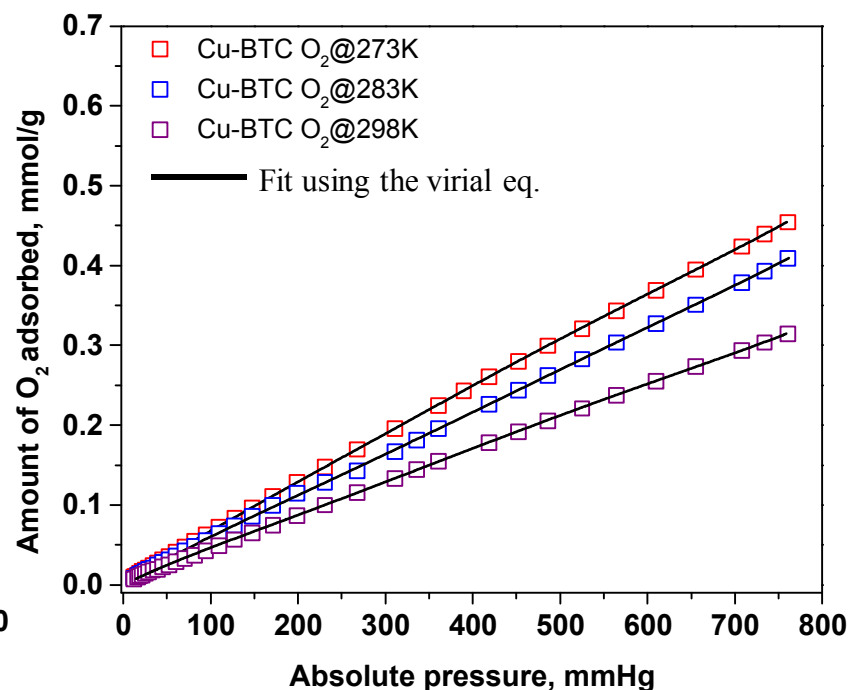
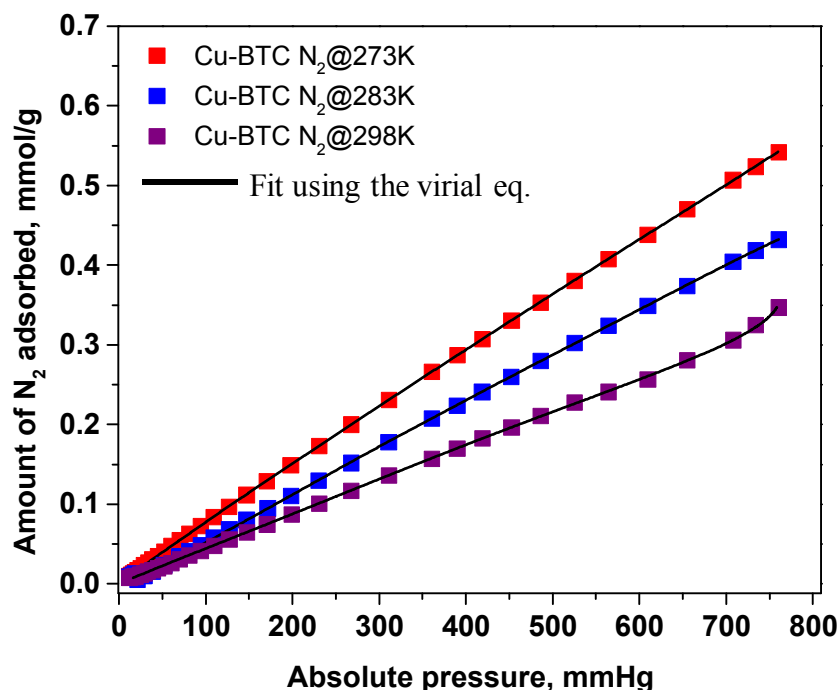


The highest O₂/N₂ selectivity is observed for the Mn/Cu-BTC sample

273-298 K: As Temperature Increases, O₂ Loadings Decrease Relative to N₂

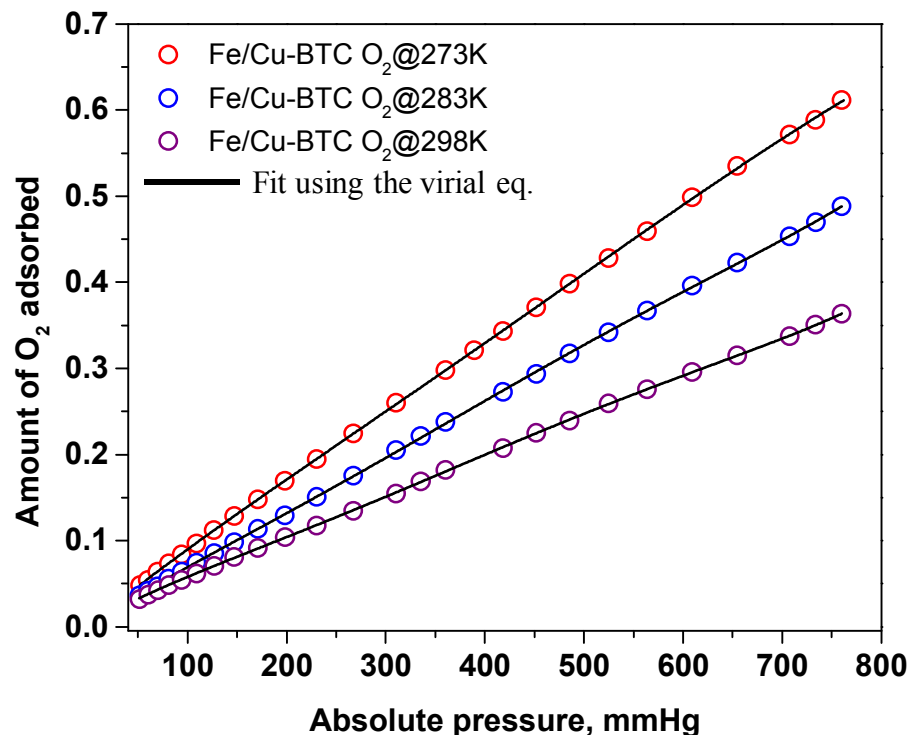
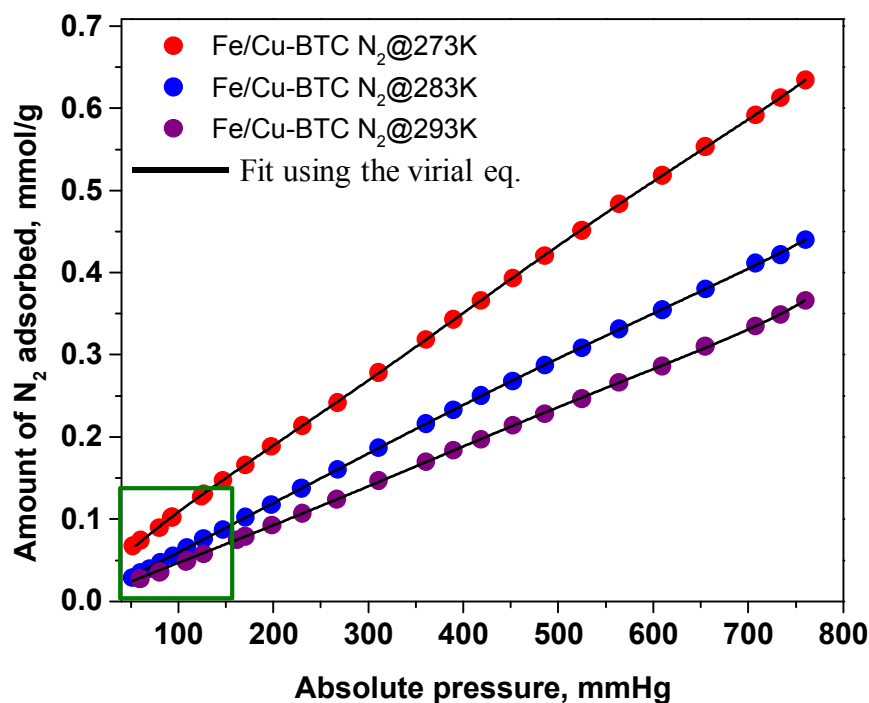
Isotherms in the 273-298K range, *independently* fitted using a modified virial equation:

$$\ln P = \ln N + \frac{1}{T} \sum_{i=0}^m a_i N^i$$



Similar behavior noted for the Mn- and Co/Cu-BTC samples

N_2 @273 K in Fe/Cu-BTC Trend Deviation: Slightly Higher N_2 Uptake at Lowest Loading Levels (at lowest pressures)

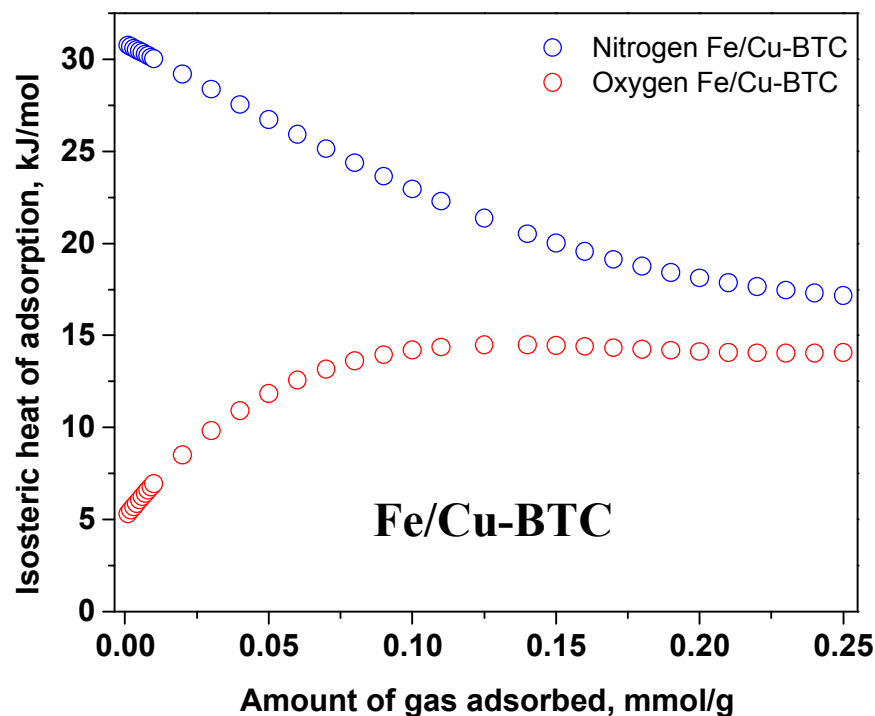
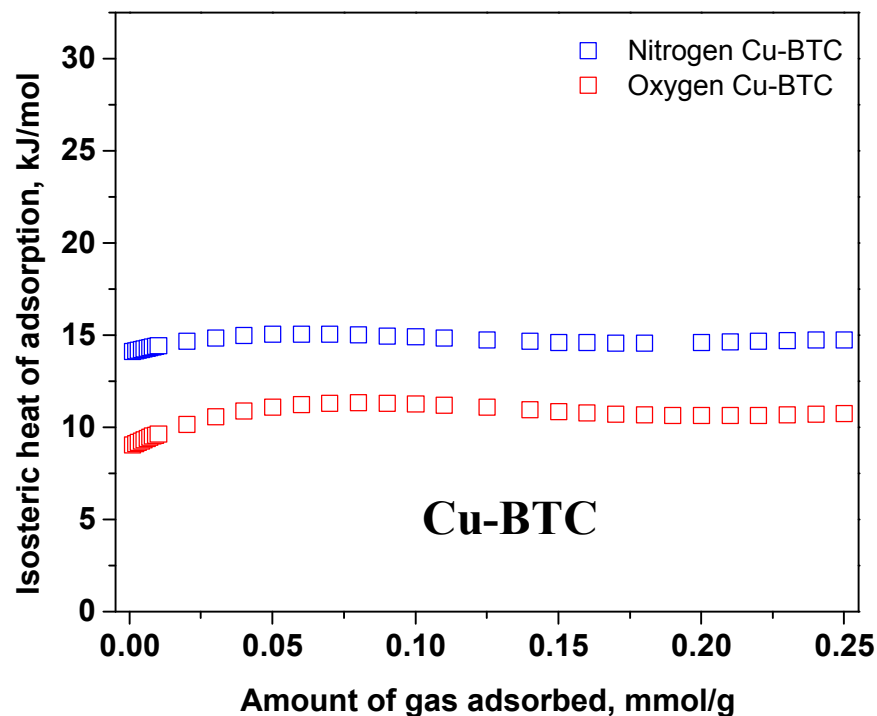


N_2 and O_2 adsorption isotherms measured at 273, 283, and 298K on Fe/Cu-BTC

Similar N_2 and O_2 uptake for Fe/Cu-BTC in the room temperature range

Isosteric Heats of Adsorption for O₂ (red) and N₂ (blue)

Comparison of Cu-BTC vs Fe/Cu-BTC Data

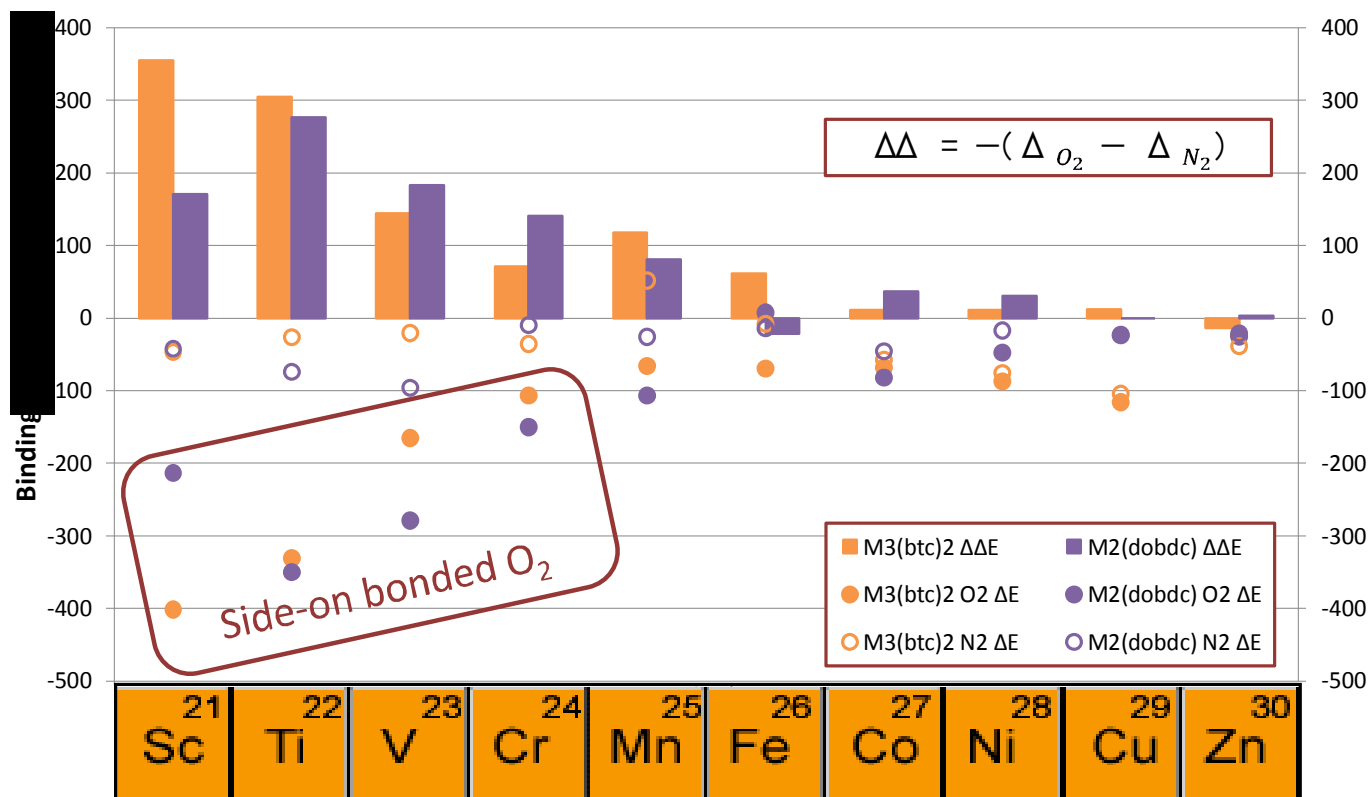


The 0 K DFT *binding energy* calculations **do not correlate** as well with experimental data from **273-298 K**

Is it the framework morphology / channel structure or the choice of metal center?

Transition to Quantum Calculations to Estimate Metal-Oxygen Binding Energy

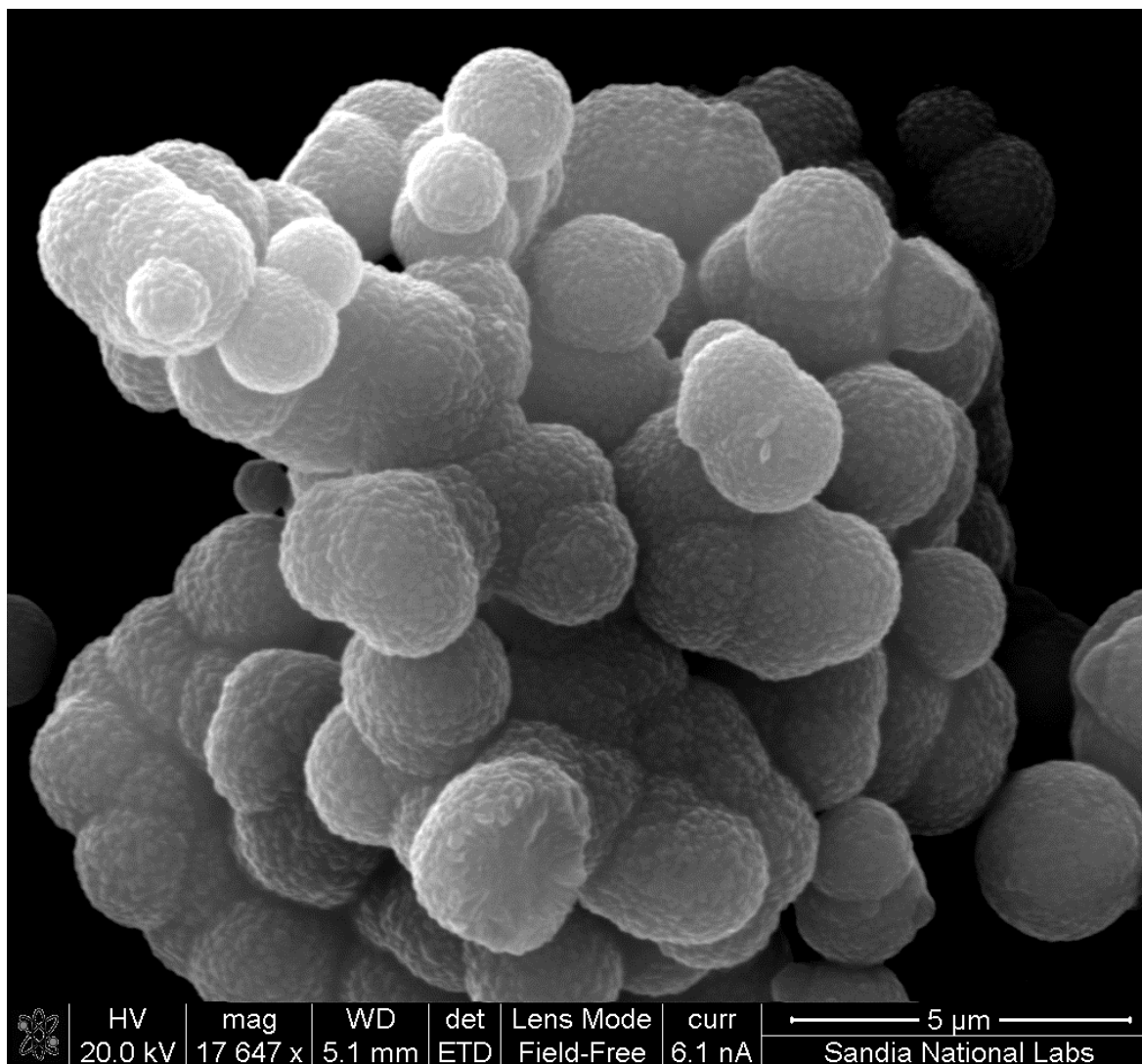
Binding Energy Calculated as a Function of Metal Site



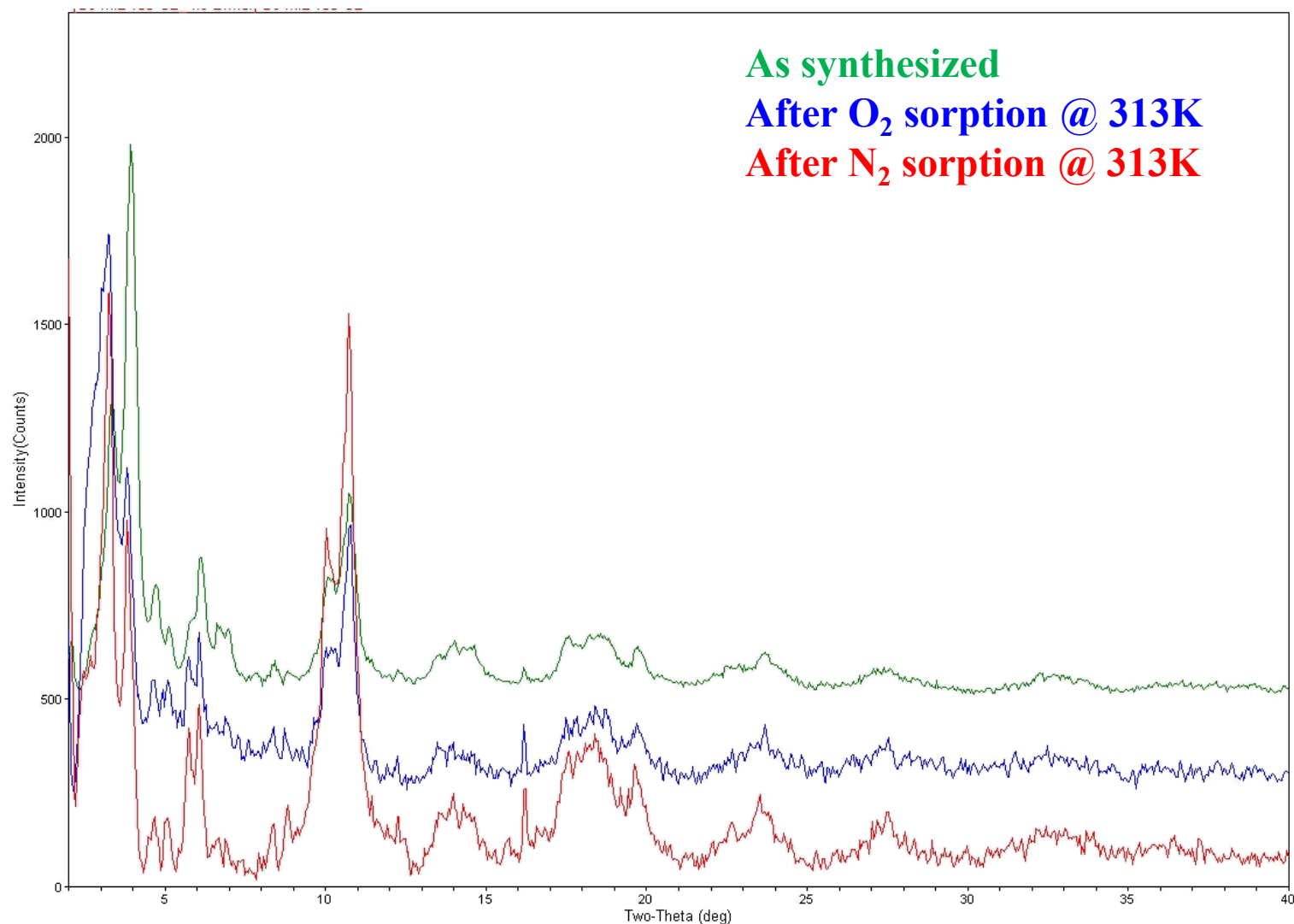
Parkes, M.; Sava Gallis, D. F.; Greathouse, J.A.; Nenoff, T.M.
 "Screening MOFs for O₂/N₂ Separations: Role of MOF Metal Center",
J. Phys Chem C, **2015**, 119, 6556.

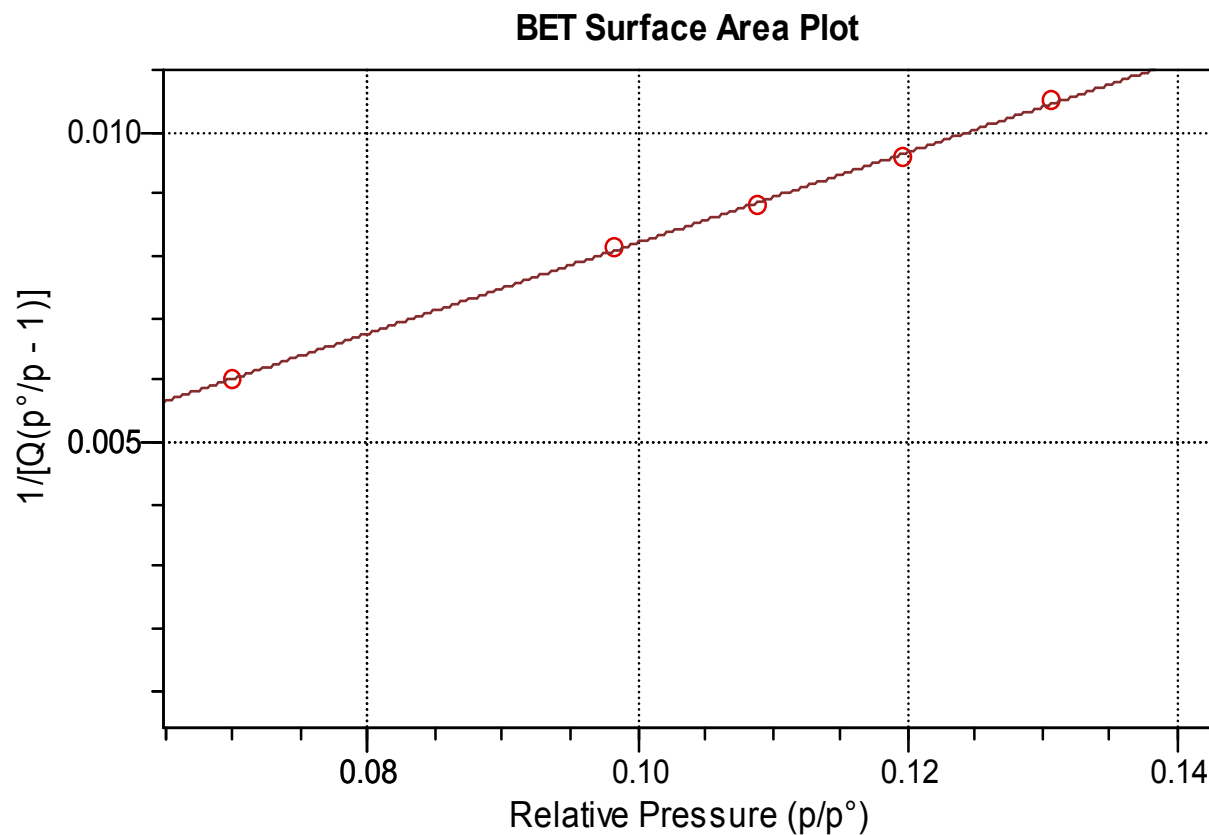
Marie Parkes, Sanibel Conference, Top Prize - Poster, 2014

SMOF-8



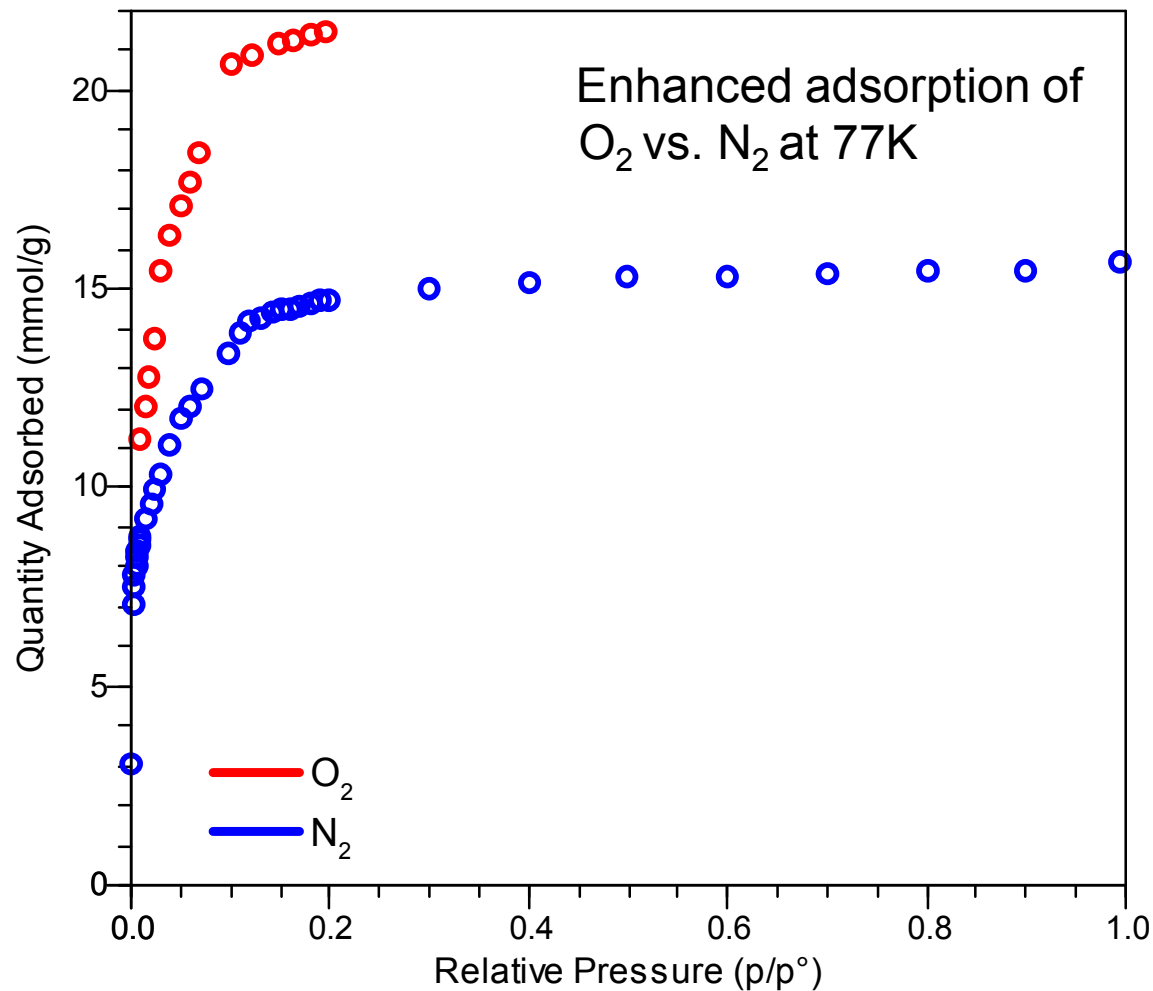
SMOF-8: Stable MOF framework over Wide Temperature Range and with Exposure to Variety of Gases





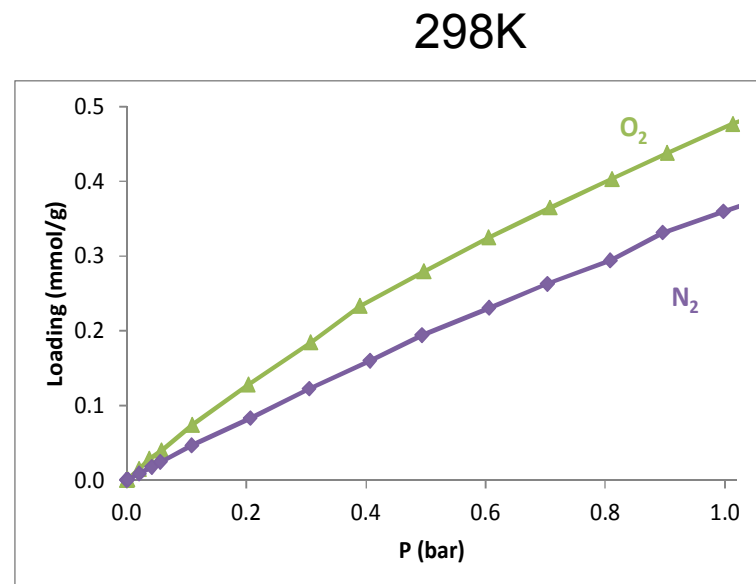
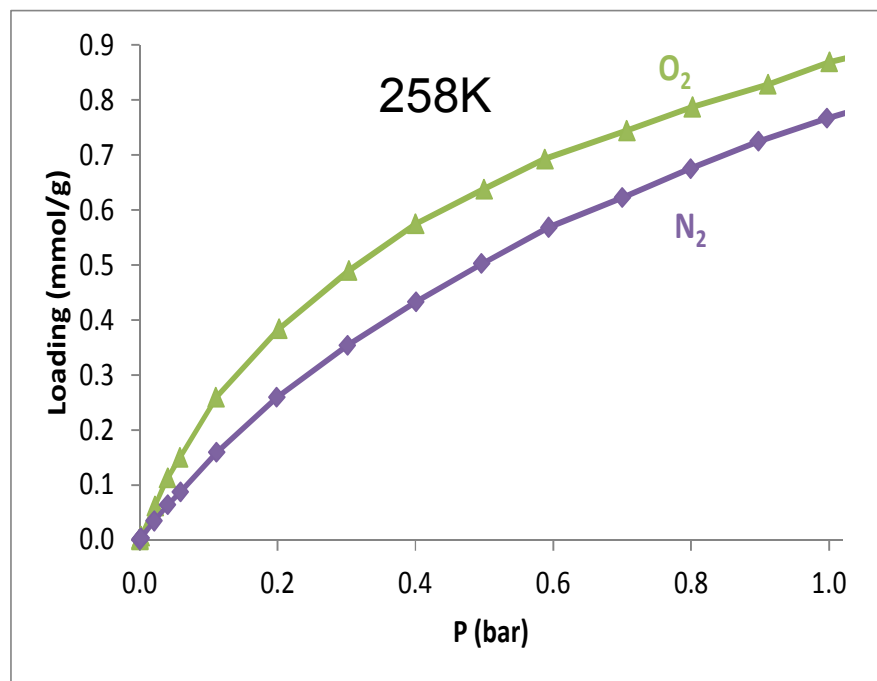
BET surface area: $1321.7194 \pm 24.4623 \text{ m}^2/\text{g}$

SMOF-8: Metal-Center has a role at 77K



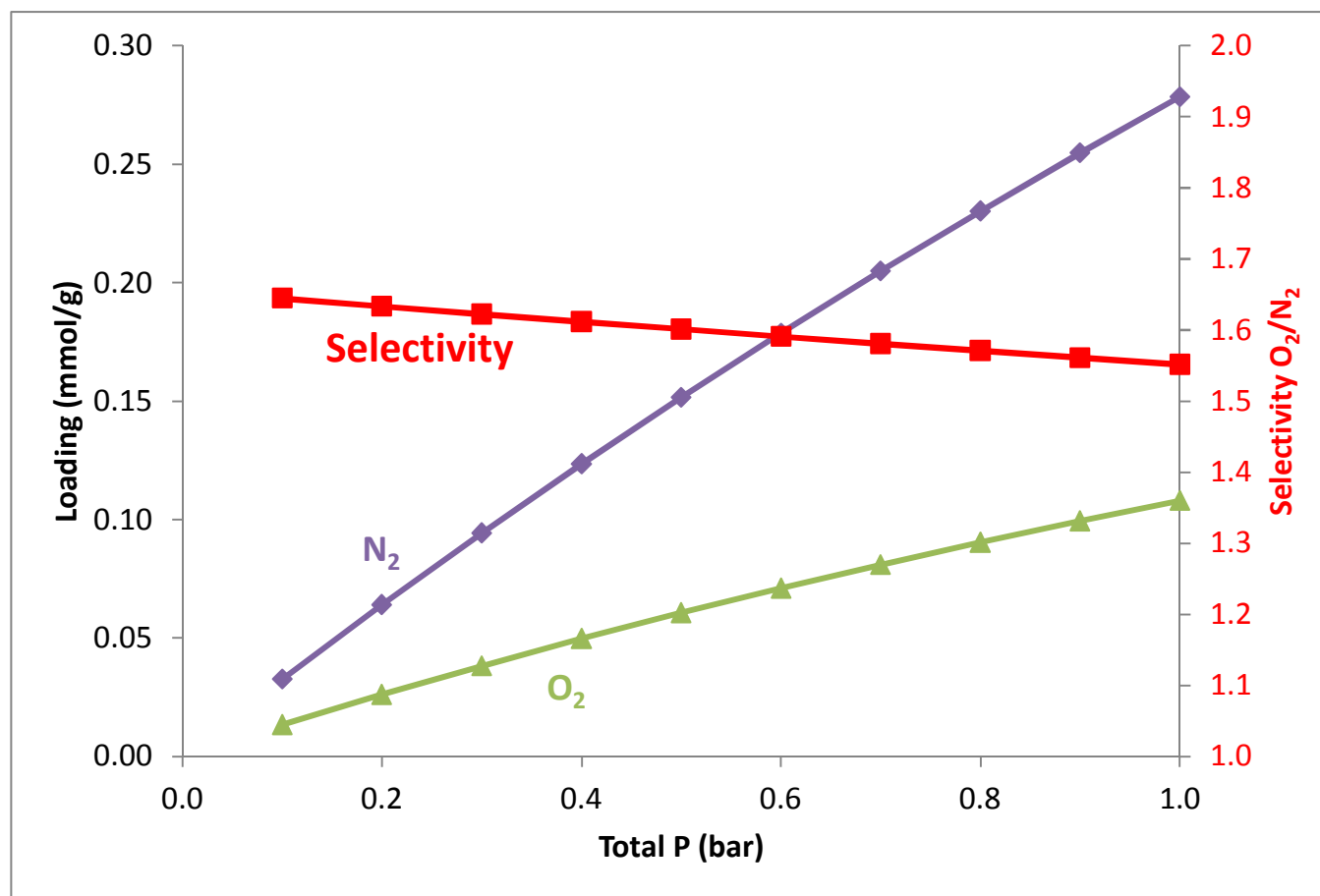
How does SMOF-8 behave at more realistic operational temperatures?

- **Grand Canonical Monte Carlo (GCMC) Simulations**
- Pure gas (N_2 or O_2) adsorption over pressure range 0 - 1 bar.
- Temperature range matched with experiment: 258 K, 298 K, 313 K.
- Grand canonical ensemble (constant chemical potential, temperature, volume) using the Towhee code (Martin, *Mol. Sim.* **2013**, 39, 1212).
- Gas-gas and MOF-gas interaction energies include van der Waals and electrostatic interactions.
- Framework atoms kept at their crystallographic coordinates.



Preferred O_2 uptake but O_2/N_2 selectivity increases between 258K and 298K

Simulations of Competitive Gas Adsorption: based on GCMC data, 298K



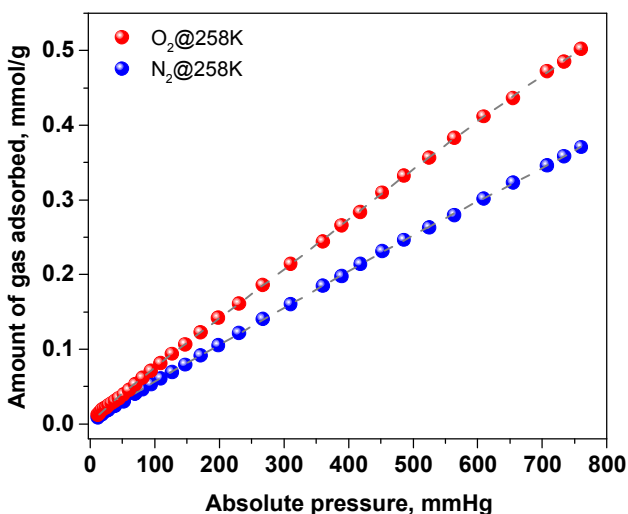
Ideal Adsorbed Solution Theory (IAST) used to calculate mixture adsorption
and O₂/N₂ selectivity for **20:80 mixture (O₂:N₂)**.

SMOF-8: Enhanced Quantity of O₂ vs N₂ Adsorbed over Wide Temperature Range (at least to 313K)

— Fit using the virial eq.

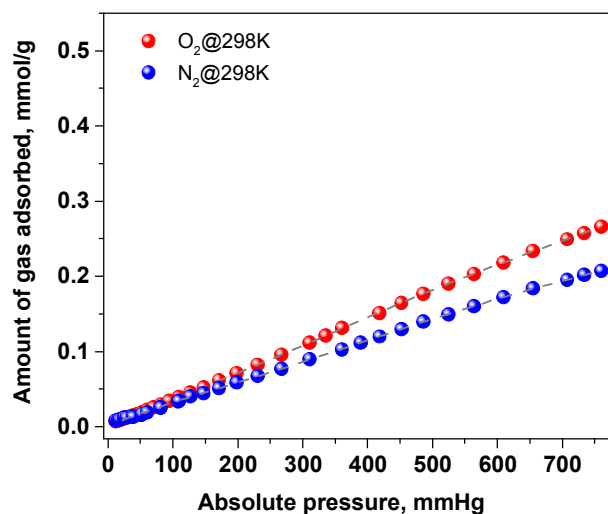
SMOF-8

O₂ vs. N₂ @258K



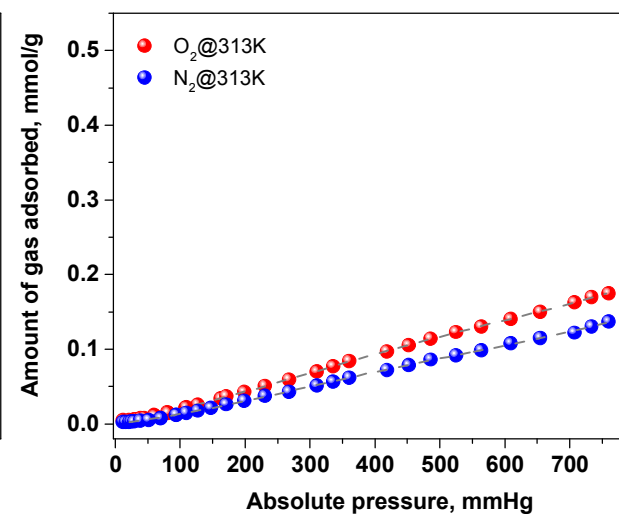
SMOF-8

O₂ vs. N₂ @298K



SMOF-8

O₂ vs. N₂ @313K



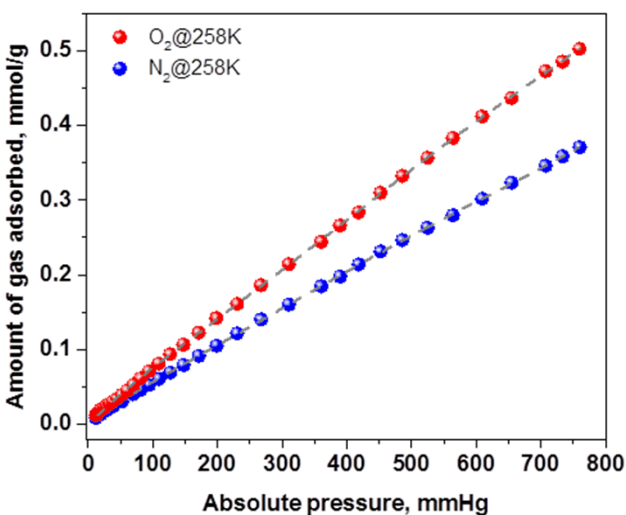
Isotherm trends mimic those predicted by GCMC

SMOF-8: Enhanced Quantity of O₂ vs N₂ Adsorbed over Wide Temperature Range (at least to 313K)

— Fit using the virial eq.

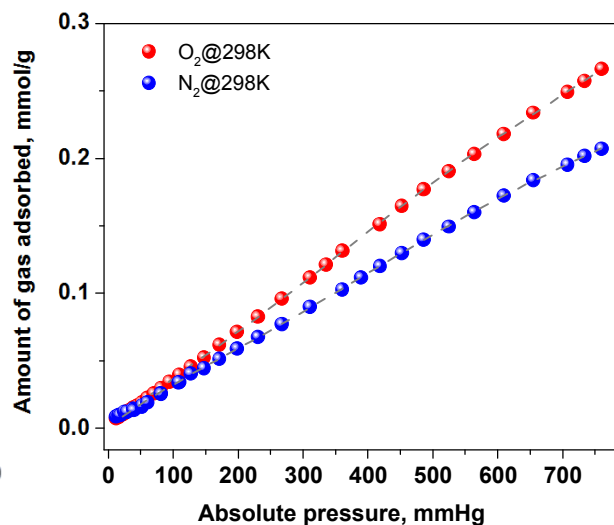
SMOF-8

O₂ vs. N₂ @258K



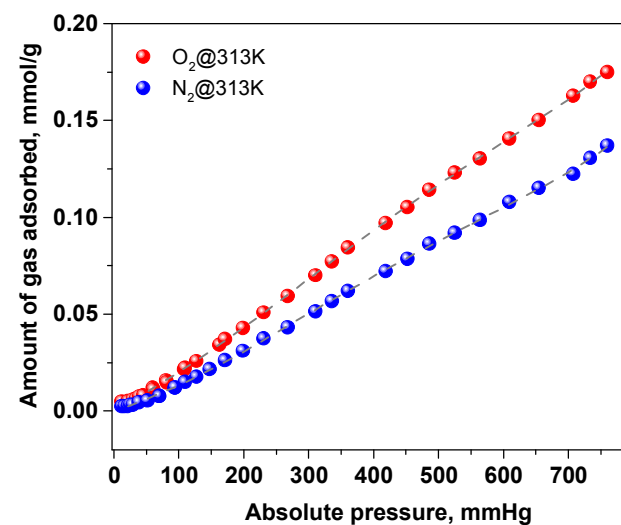
SMOF-8

O₂ vs. N₂ @298K



SMOF-8

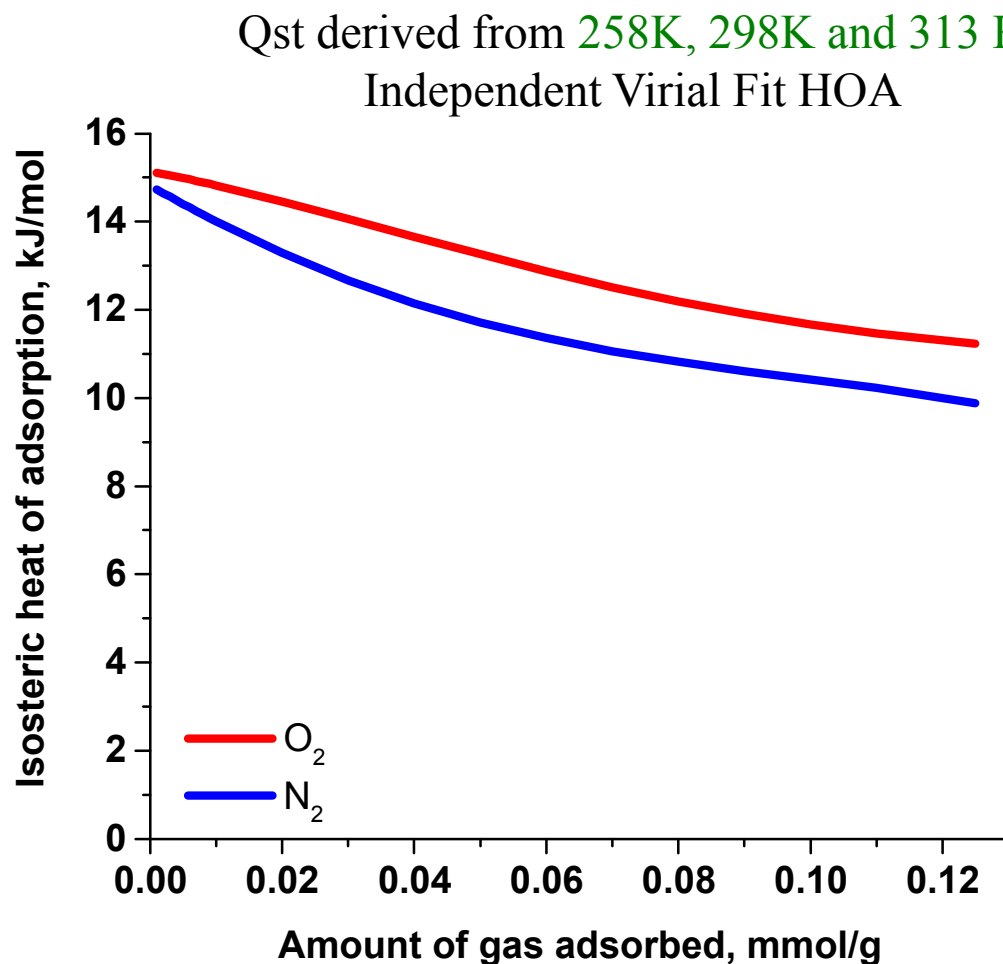
O₂ vs. N₂ @313K



Isotherm trends mimic those predicted by GCMC

SMOF-8: Isosteric Heat of Adsorption (kJ/mol)

Higher Binding Energy in SMOF-8 for O₂ vs N₂



- Successfully synthesized partially substituted
Co-, Fe- and Mn- analogues of Cu-BTC
- Assessed the effect on metal substitution on the O₂ and N₂ adsorption capacity at both cryogenic and close to room temperature ranges
- For the Co-, Mn- and original Cu-BTC, O₂ preferentially adsorbs over N₂ at 77K. **However**, the trend is reversed at 298K, where N₂ preferentially adsorbs over O₂
- Based on predictive modeling, we studied early transition metal metal-center MOFs for enhanced O₂ sorption.
- **SMOF-8**: Early transition metal MOFs show preference for O₂ vs N₂ over wide temperature range (up to at least 313K), as confirmed by isosteric heats of adsorption.
- **Next Steps**: Data transfer to *Technoeconomic Analysis* and *Burner Design* for Oxyfuel combustion applications

Thank You

Sandia National Laboratories' Sites



Albuquerque, New Mexico



**Kauai Test Facility
Hawaii**



**Tonopah Test
Range,
Nevada**



**Yucca Mountain
Nevada**



**WIPP,
New Mexico**



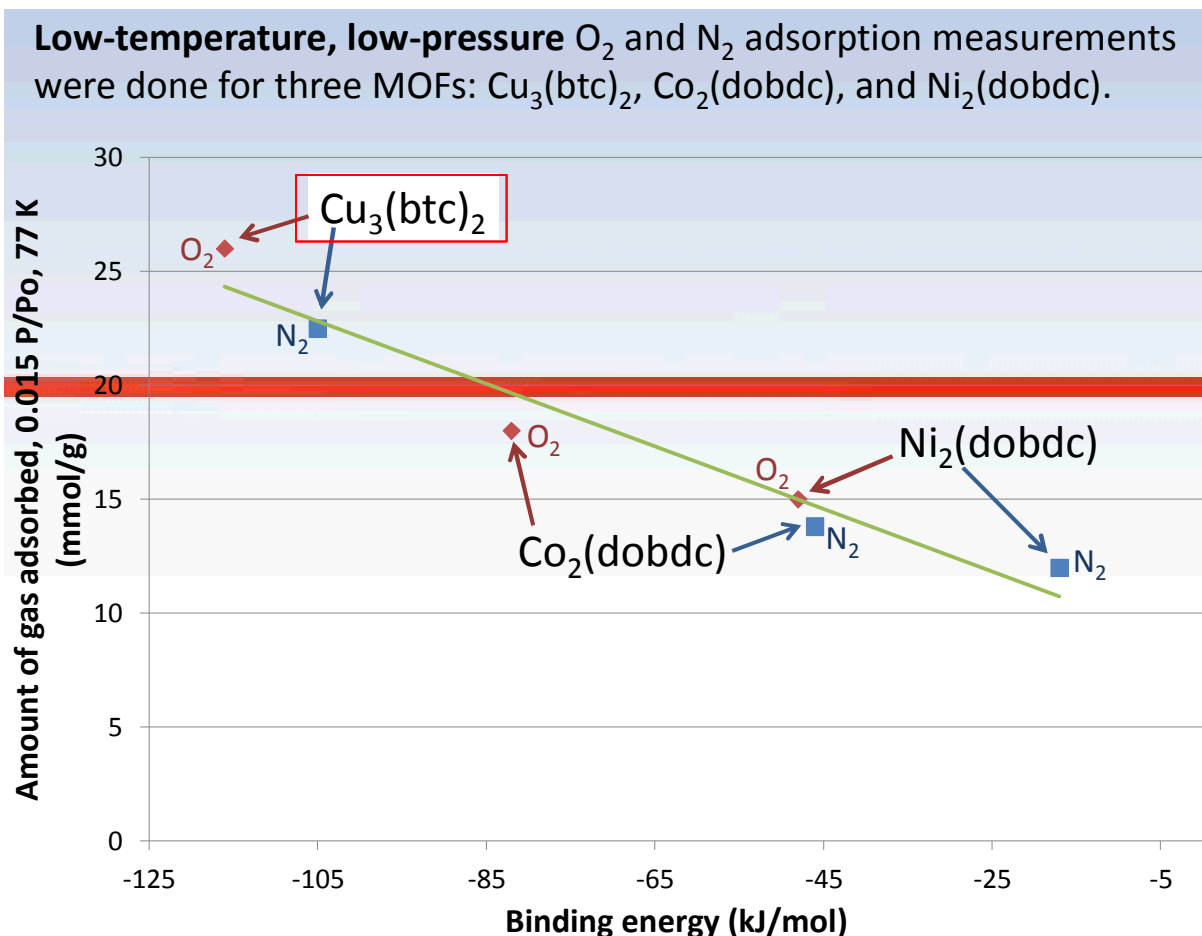
Pantex, Texas



Livermore, California

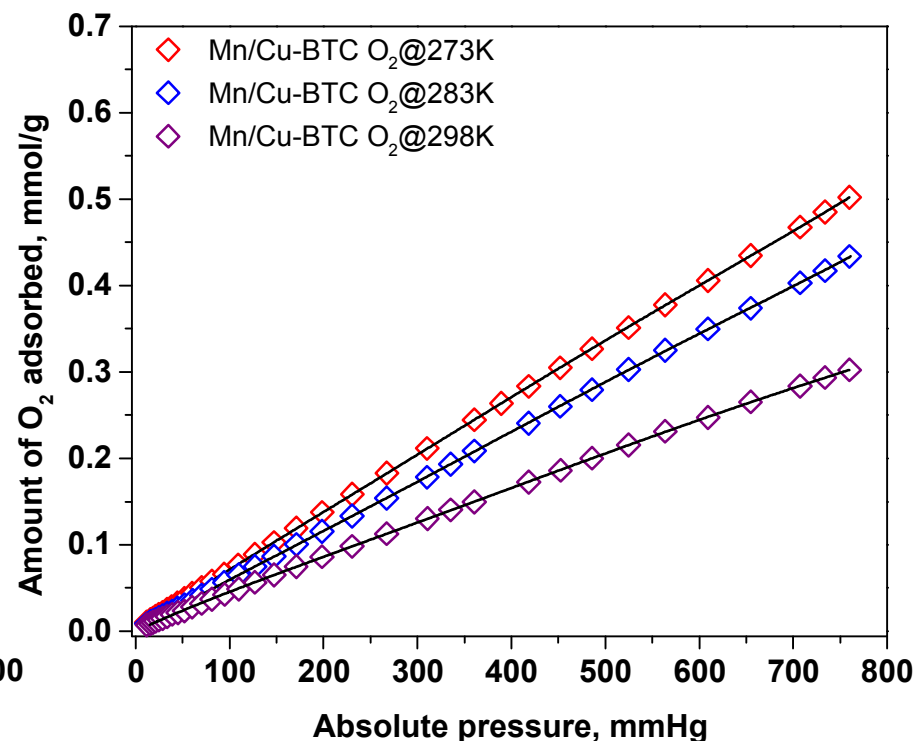
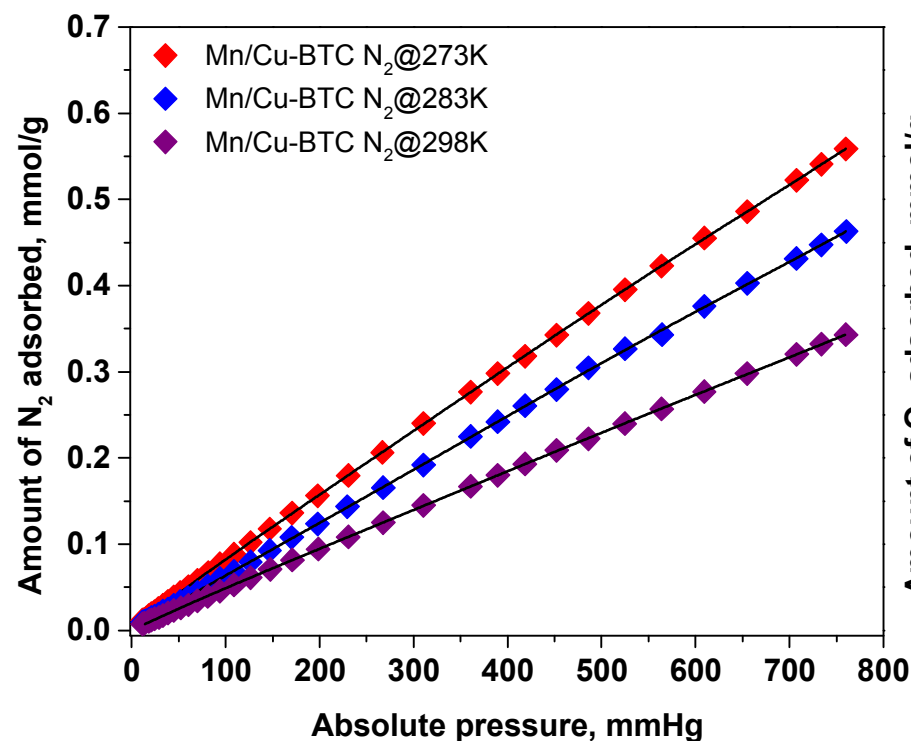
Extra slides

Transition to Quantum Calculations to Estimate Metal-Oxygen Binding Energy



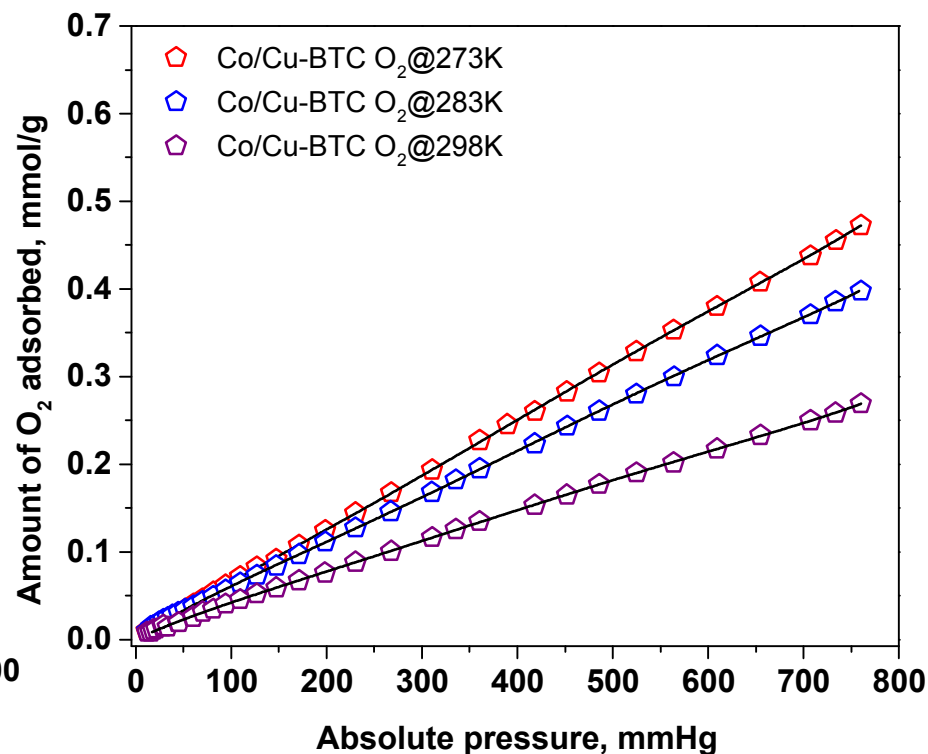
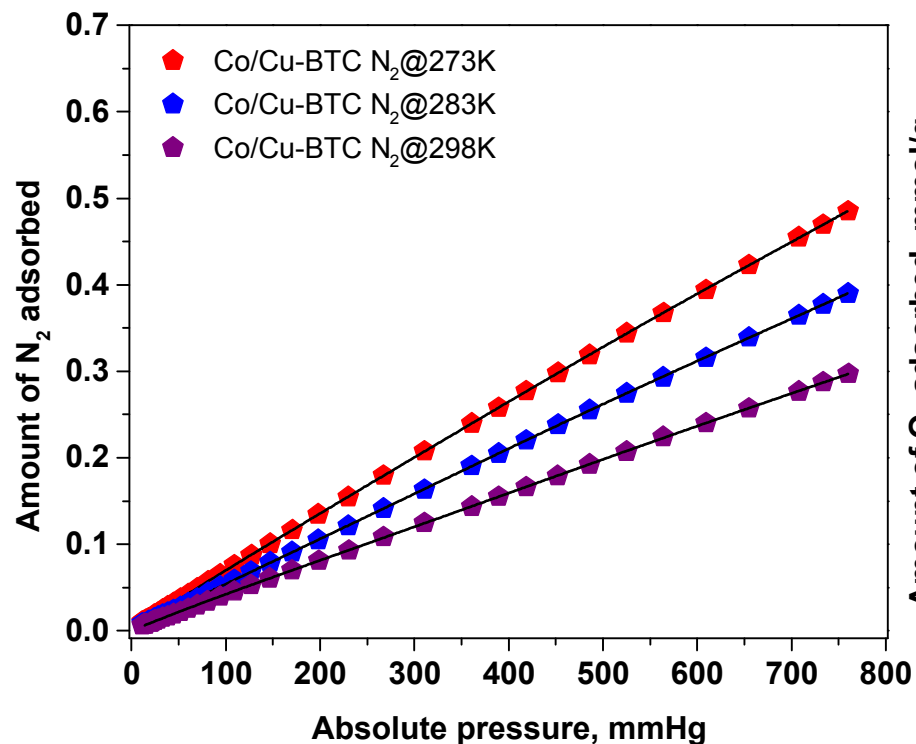
Excellent correlation between simulated binding energies and low-temperature, low-pressure experimental gas uptake.

N_2 and O_2 adsorption isotherms measured at 273, 283, and 298K on pristine Mn/Cu-BTC



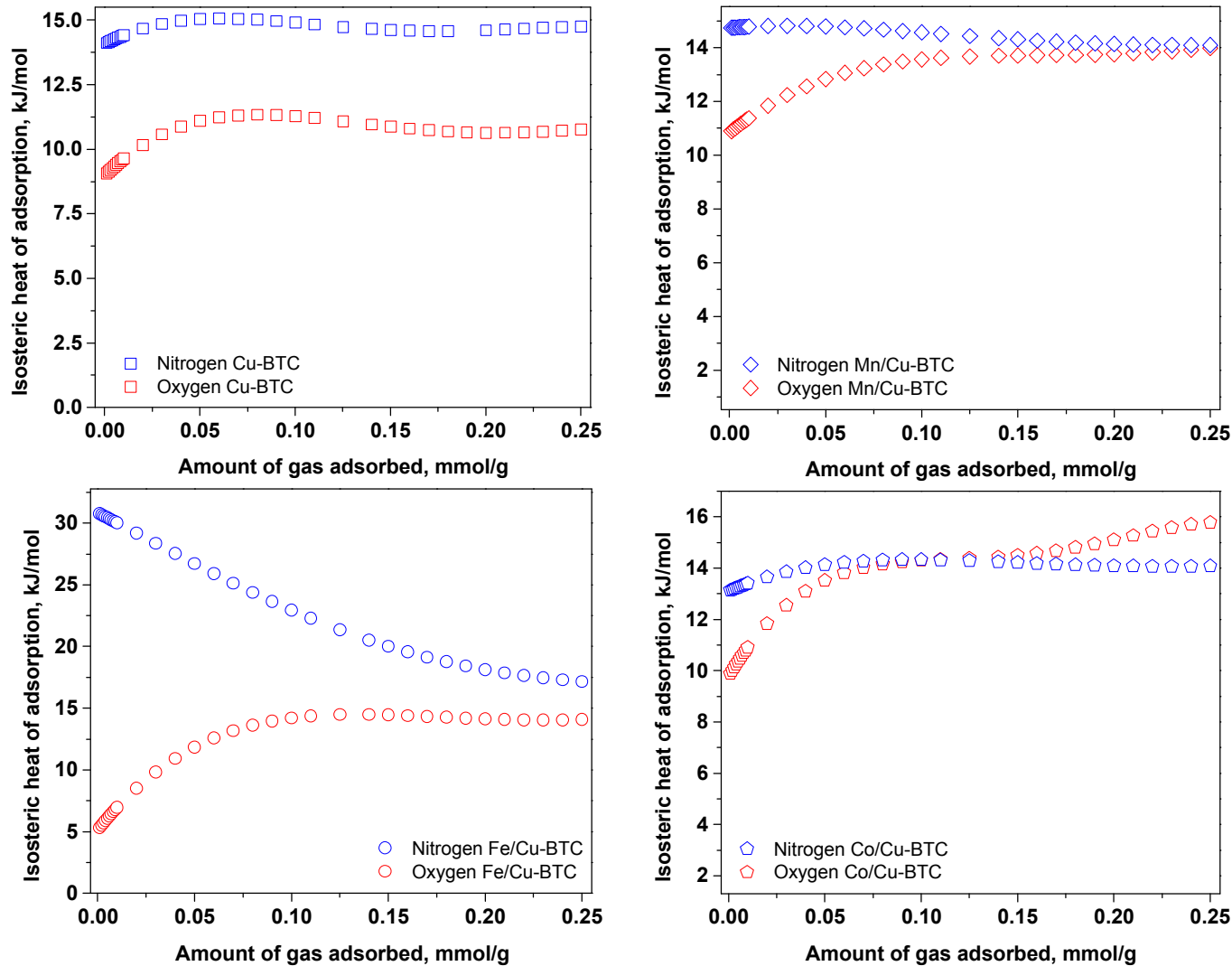
In the room temperature range, slightly higher affinity for N_2 over O_2 is noted

N_2 and O_2 adsorption isotherms measured at 273, 283, and 298K on pristine Co/Cu-BTC

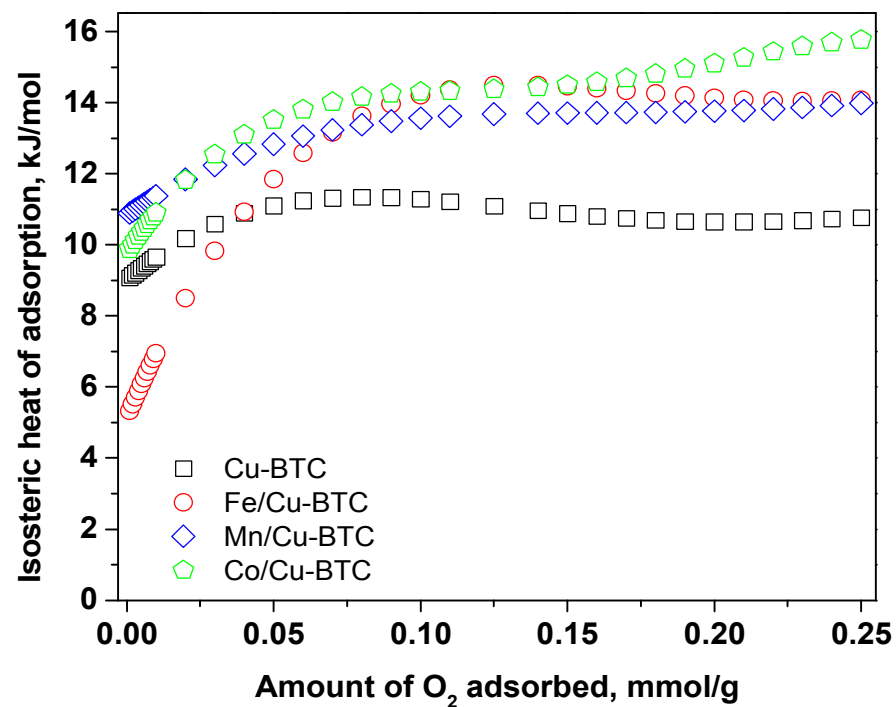
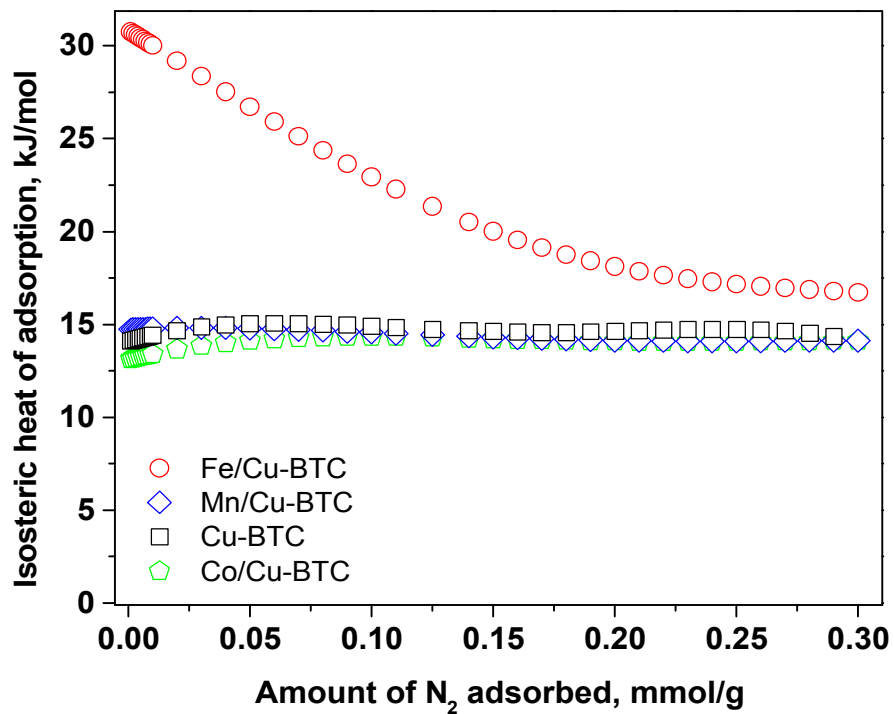


In the room temperature range, slightly higher affinity for N_2 over O_2 is noted

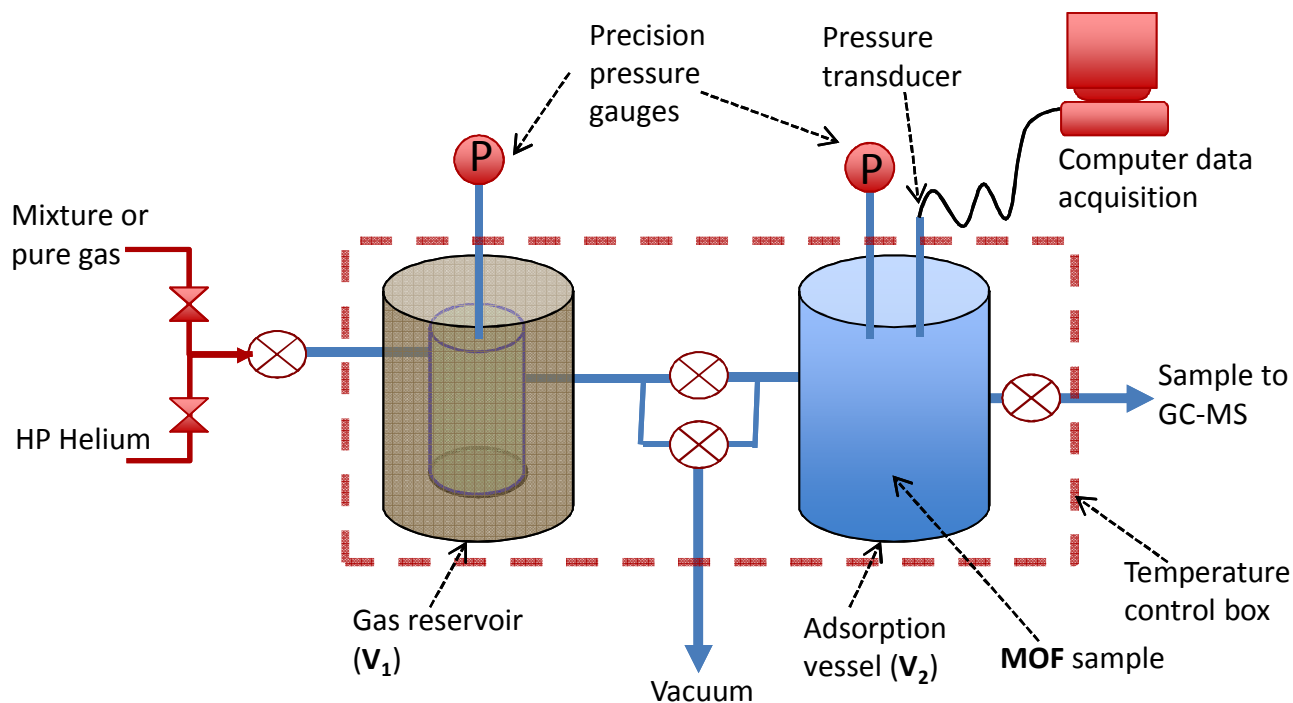
Significantly higher binding energy of N_2 over O_2 is noted for the Fe/Cu-BTC sample



Isosteric heats of adsorption for O_2 (red) and N_2 (blue) obtained from the fitted 273, 283 and 298K adsorption isotherms



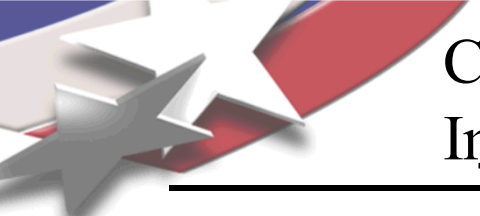
O₂/N₂ Gas mixture adsorption measurements containing 20% O₂ and 80% N₂



Room temperature (294K) in pressure range of 1.77 to 5.2 bars.

Samples tested for adsorption of O₂/N₂ mixture containing 20% O₂ and 80% N₂ at 21, 35, and 48.5°C, respectively.

P _{eq} , bar	Amount adsorbed., cm ³ (STP).g ⁻¹ .bar ⁻¹		aO ₂ /N ₂
	O ₂	N ₂	
1.77	6.568	7.109	0.924
3.50	5.910	6.384	0.926
5.00	5.346	5.558	0.962



Combustion Studies plus MOF O₂ Separations for Improved Combustion Process Efficiency

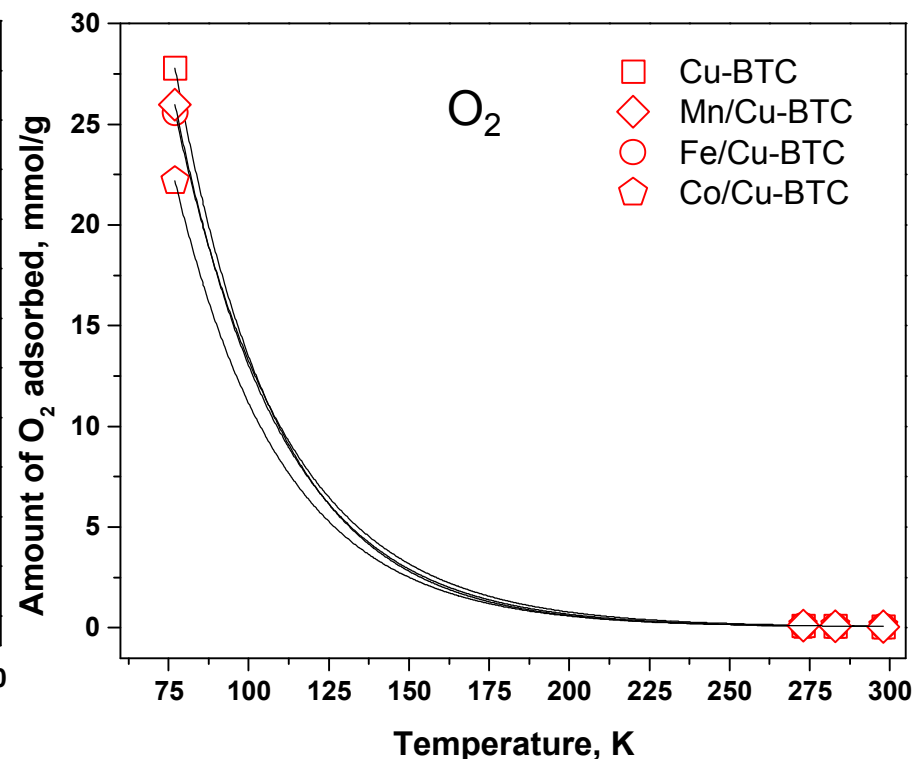
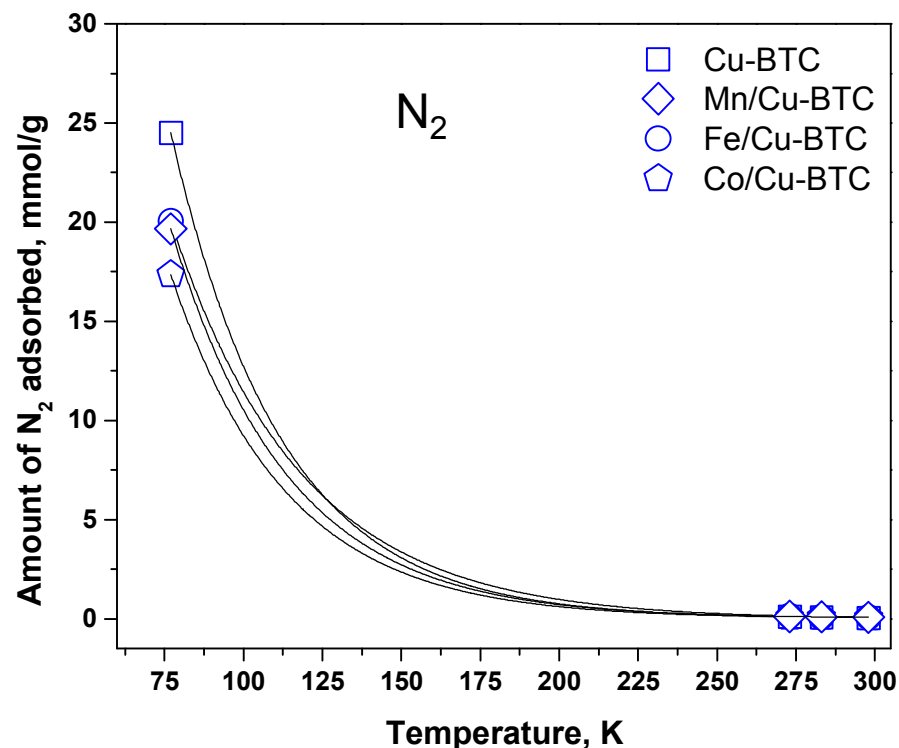
LDRD: Combine Experiment MOFs Gas Separations Data into Flame / Combustion Testing

5% improved efficiency ← heat/radiation improvement w/oxyfuel ← enhanced O₂/N₂ via MOF

- 1) Study of non-premixed oxygen-enriched and oxy-fuel flames using a non-premixed turbulent jet flame burner
- 2) Measurement of radiant flux for accurate determination of flame radiation
- 3) Measurement of soot concentration in flames planar laser-induced incandescence measurements (LII)
- 4) Allow for the calculation of the contribution of the soot to total radiant heat transfer of the flames
- 5) Data input to Systems Analysis for calculations of efficiency improvements of combined developed MOFs into Oxyfuel Process Stream**

At 77K, Metal Sites Play an Important Role, while at 273 - 298 K Metal Sites have a *Smaller Effect*

The temperature dependency of the N₂ and O₂ uptake at ~ 0.2 atm and 77, 273, 283, and 298 K

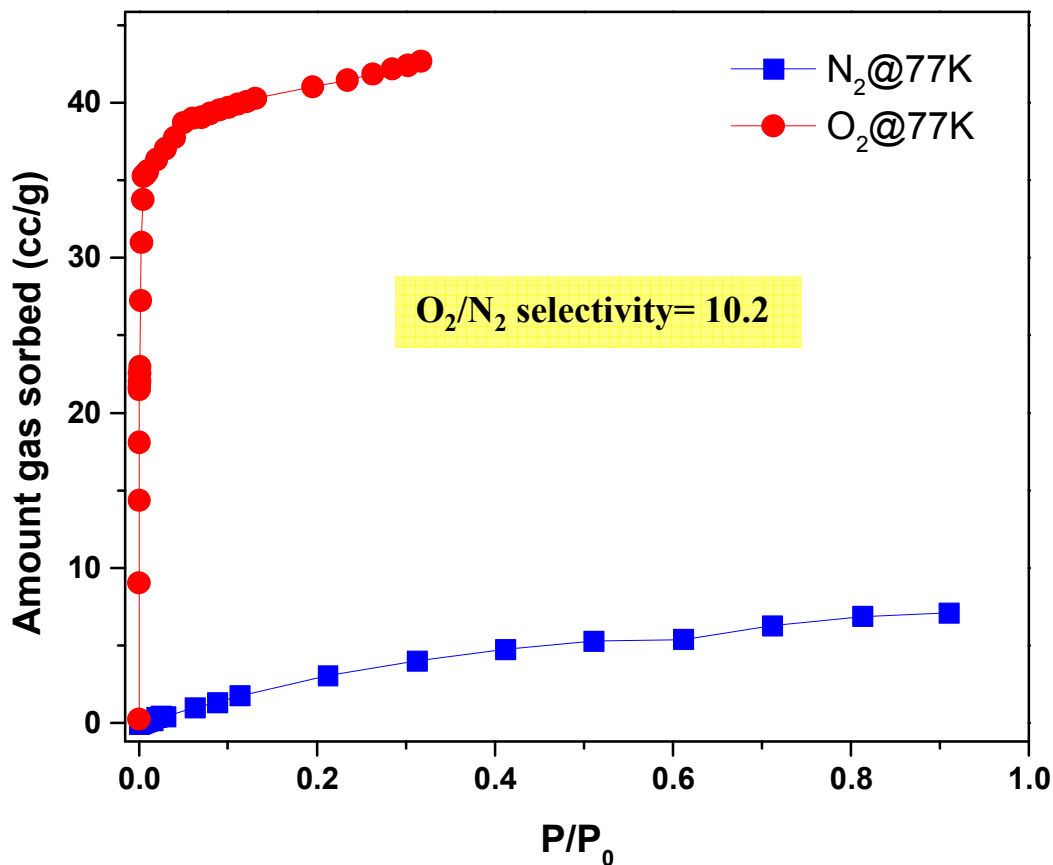
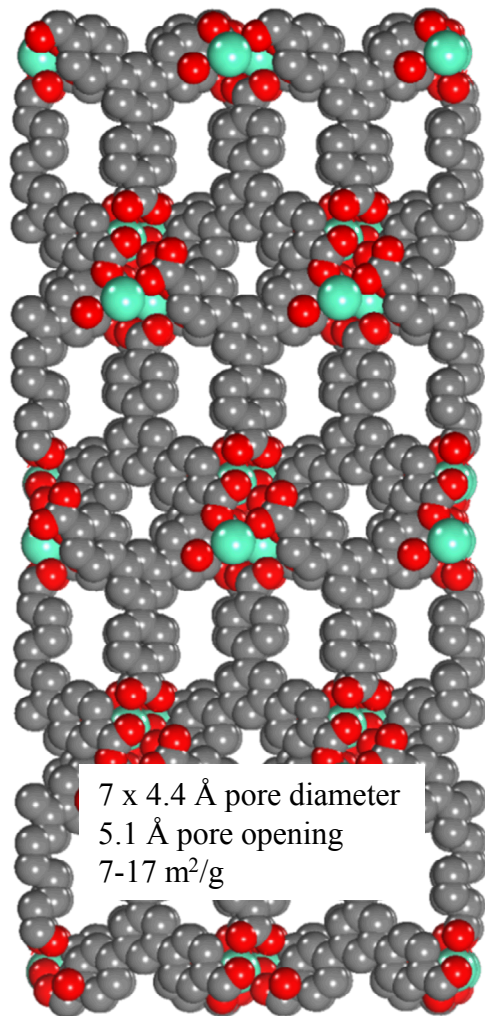


Distinct transition point temperature where the metal sites dependence on the O₂ and N₂ uptake is inverted

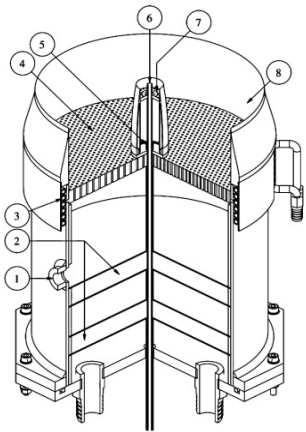
SMOF-7: O₂ vs. N₂ Single Gas Sorption Isotherm, at 77K

D. Sava Gallis, T. M. Nenoff,
US Patent Pending, 2014

SMOF-7



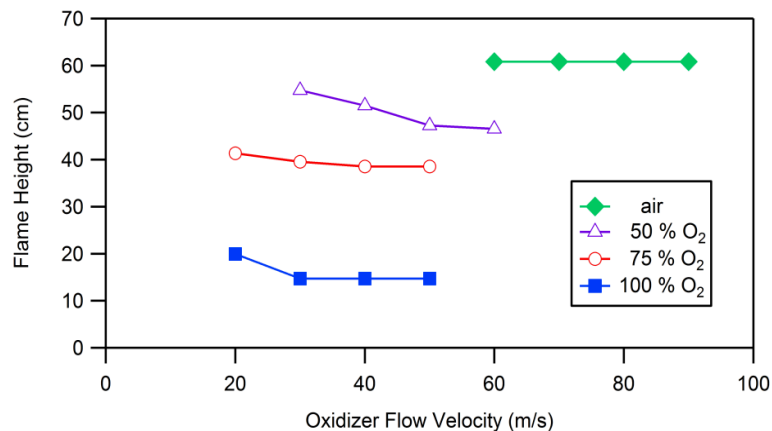
Coupling of Burner design and Oxy-fuel Combustion to Radiant Heat Transfer



Balloon number	Description
1	Flashback over-pressure sensing port
2	Glass bead filled cavities
3	Cooling water coil
4	Collow perforated baseplate
5	Pilot mixture feed exit
6	Central jet exit
7	Pilot perforated baseplate
8	Collow collar



- Newly designed and constructed burner with smaller diameter inside tube for CH_4 into oxidizer jet flow
- Allows either premixed or non-premixed methane-air flame
- Designed specifically for pure O_2 and enriched O_2 stream as determined by gas separations data from MOFs and economic life cycle analyses



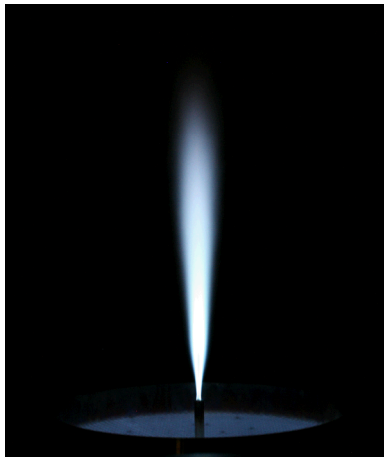
LDRD calculated/predicted flame heights when using a 1/8", 0.020 wall stainless steel tube to deliver methane to the Dunn burner.

The volumetric flow of methane is always equal to $\frac{1}{2}$ the flow of oxygen, to maintain stoichiometric combustion conditions.

Preliminary Investigation of Oxygen-Enriched NG Flames

Performed preliminary testing performed with oxidizers of pure oxygen and with 50% O₂ in N₂, using an overall equivalence ratio of 1, with a constant methane flow

- Velocity (Re) of oxidizer flow is 50% lower when using pure O₂, making for taller flame (slower mixing)
- Soot formation is enhanced when using pure O₂ (higher temperatures, slower mixing)



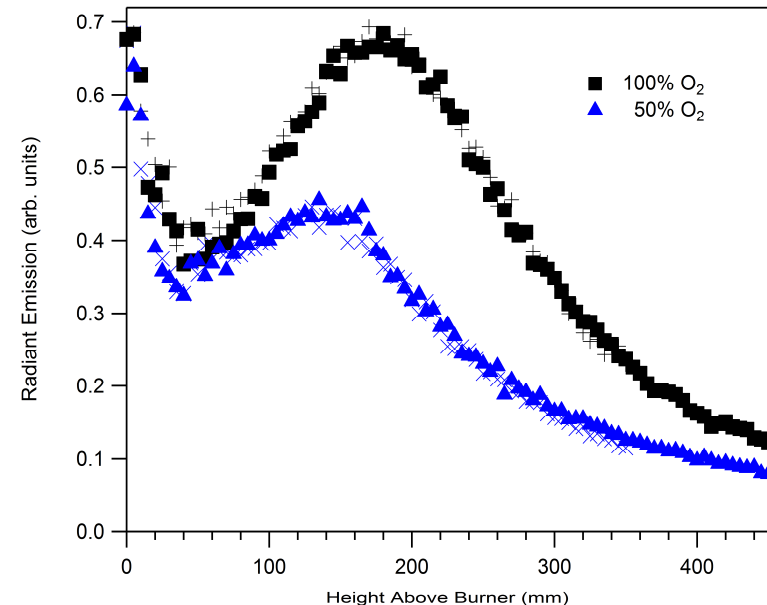
50% O₂ in N₂



100% O₂

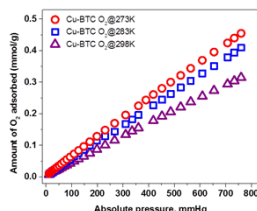
Radiant emission measurements have been performed along the flame centerline

- Data for 100% O₂ shows significantly more thermal radiation
- Flame temperatures are higher when using pure O₂ (more radiation from flame products)
- Some soot is formed in the 100% O₂ flame

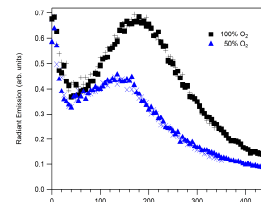
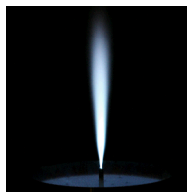


Systems Analysis of MOF-based Air Separation

MOF adsorption
isotherms (N_2 & O_2)
(from MOF team)



Optimal $O_2:N_2$ ratio
for combustion
(from combustion team)



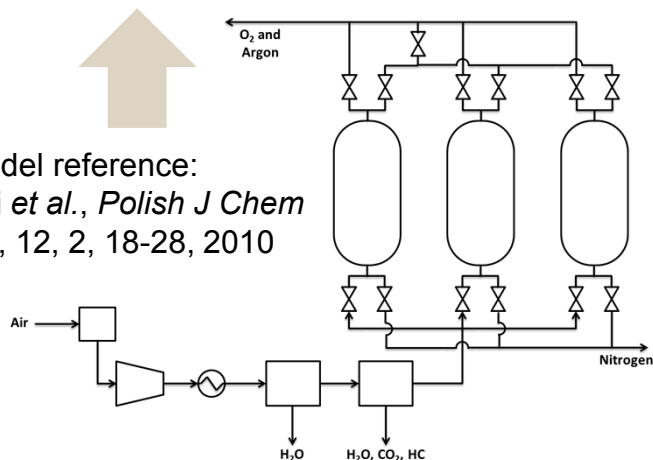
*Can MOF-based
PSA reduce energy
consumption by 5%
vs. conventional PSA
air separation?*

Construct and
validate model of
PSA process

Adjust PSA model
parameters to yield
desired $O_2:N_2$ ratio

Estimate energy
consumption based
on PSA parameters

PSA model reference:
Beeyani *et al.*, *Polish J Chem
Technol*, 12, 2, 18-28, 2010

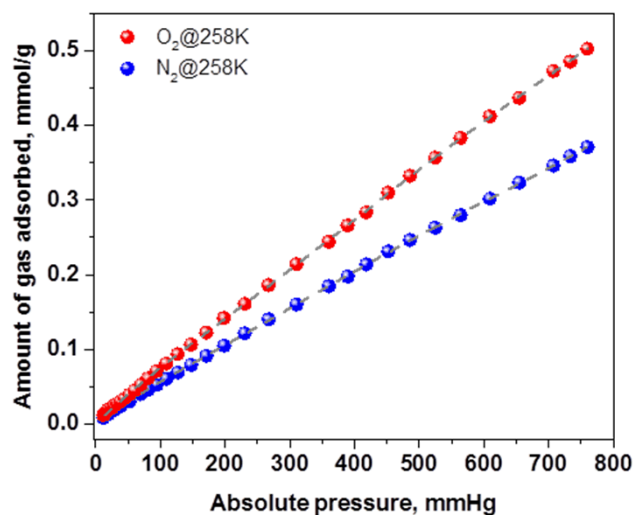


Key PSA model
parameters:

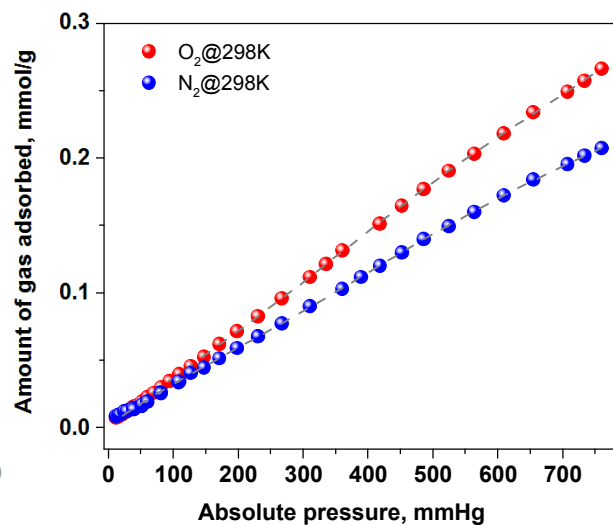
- Vessel dimensions
- Operating pressures
- Cycle time
- Feed rate

PSA energy consumption is
dominated by compressor(s)
→ Operating pressures and
flow rates are primary
drivers

SMOF-8
O₂ vs. N₂@258K



SMOF-8
O₂ vs. N₂@298K



SMOF-8
O₂ vs. N₂@313K

