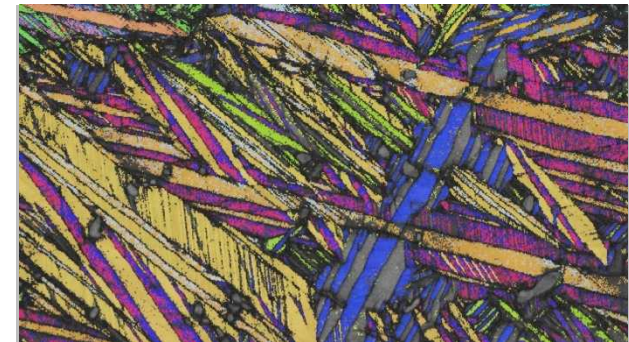
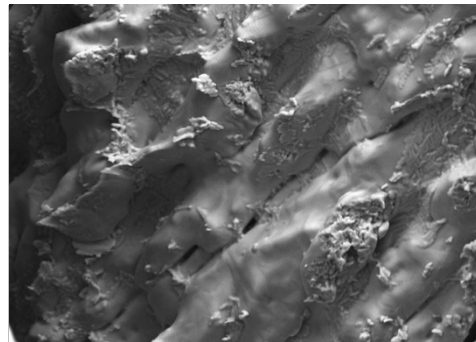
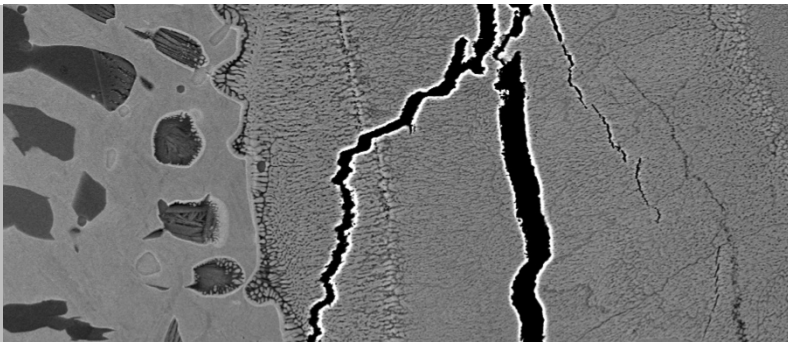


Exceptional service in the national interest



Weldability of Advanced Shape Memory Alloys

J. M. Rodelas

Sandia National Laboratories, Albuquerque NM

Materials Science & Technology 2014

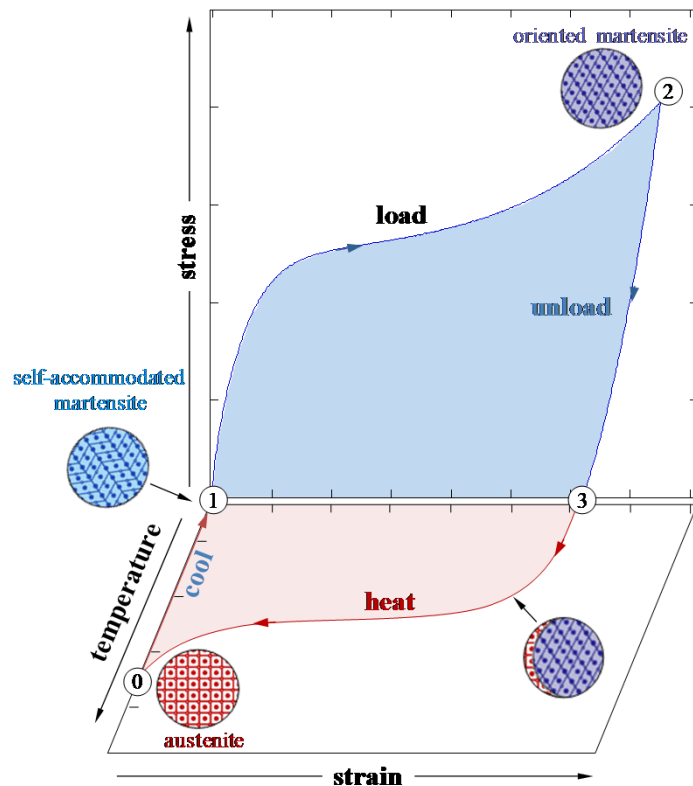
Oct. 13th, 2014



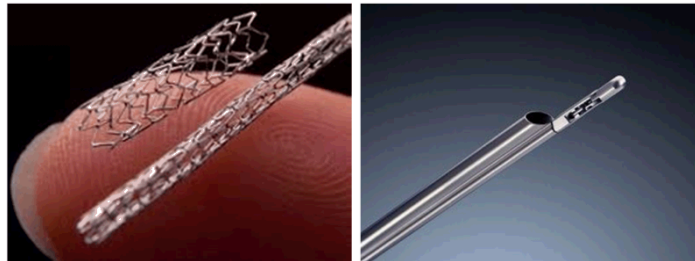
Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000. SAND NO. 2011-XXXXP

What is a Shape Memory Alloy (SMA)?

- Unique class of intermetallic alloys that changes shape using a 1st order transformation
- Widely used conventional NiTi intermetallic SMA has functional limitations of $\sim 100^{\circ}\text{C}$
- New high temperature (HT) SMAs being developed to perform $>100^{\circ}\text{C}$.



Biomedical Devices



(HT)SMA Compact Actuators



Habe et al., Proc of SPIE Vol. 6525 6525C-1 (2007)

SMA anti-scald device



Image source: Bouge R. *Assembly Automation*. 29:3 pp214-19 (2009)

Morphing Aircraft Structures



Image source: Habe et al., Proc of SPIE Vol. 6525 6525C-1 (2007)

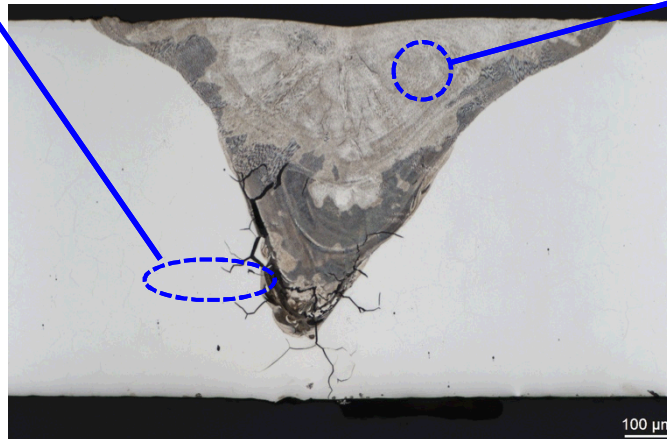
Why Explore the Weldability of Shape Memory Alloys?

- Weld metallurgical phenomena that determine material weldability has received little attention for SMAs
- Eventual development of robust welded high-temperature (HT) SMAs in real-world applications requires understanding of weld metallurgy

Heat Affected Zone Weldability Concerns

- Liquation cracking
- Sub-solidus HAZ embrittlement
- Liquid metal embrittlement
- Reheat/Strain-age cracking
- HAZ sensitization
- Lamellar cracking

Fabrication Weldability Considerations for Engineering Alloys



Weld Metal Weldability Concerns

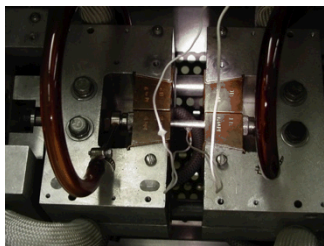
- Solidification cracking
- Weld metal liquation*
- WM Ductility dip cracking*
- Hydrogen-induced cracking

*multi-pass welds

Weldability of SMAs/HTSMAs: A Multi-Technique Approach

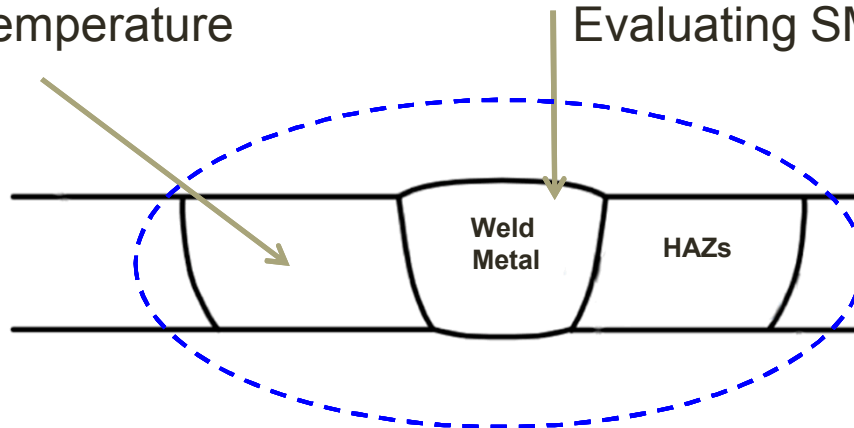
- True assessment of SMA weldability will require an understanding metallurgical behavior governing SMA cracking during welding
- Simplified Ni-Ti binary provides insight into new Ni-Ti-X HTSMAs

#1:
Heat Affected Zone Cracking
Evaluating elevated temperature ductility



Gleeble Thermomechanical Simulator

#2:
WM Solidification Cracking
Evaluating SMA/HTSMA susceptibility

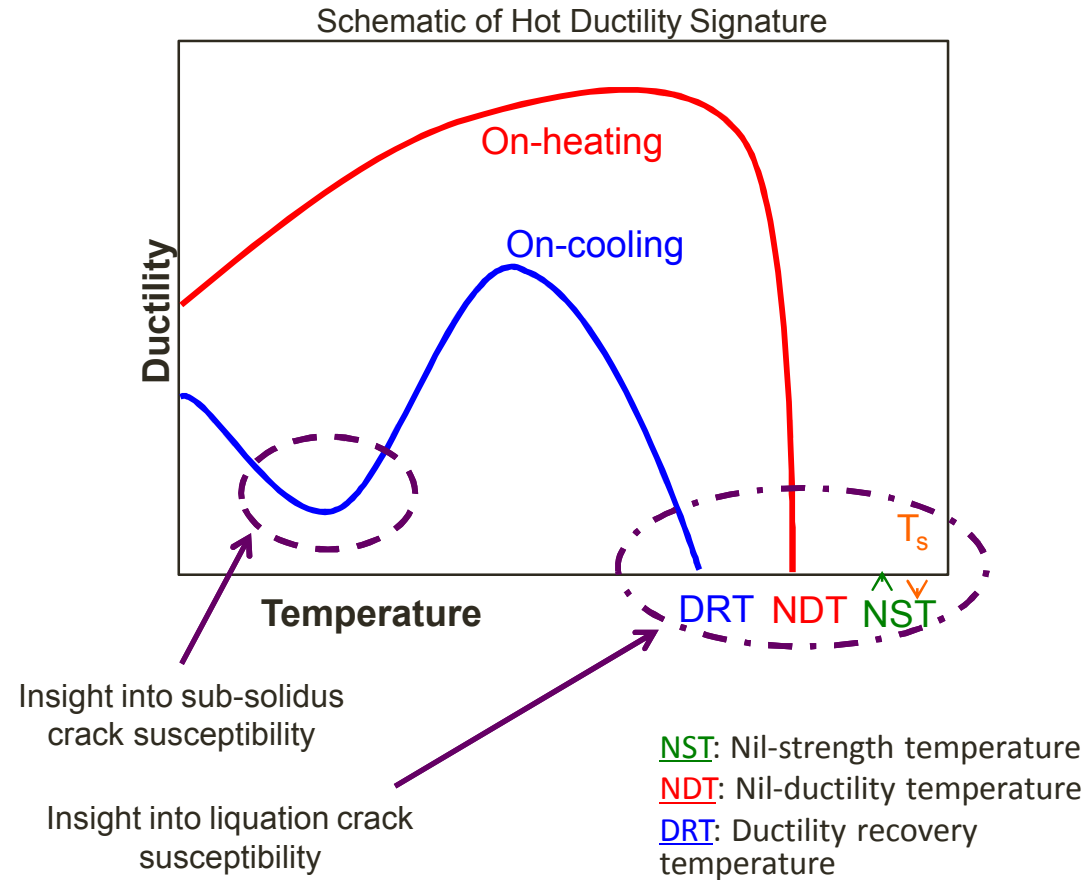
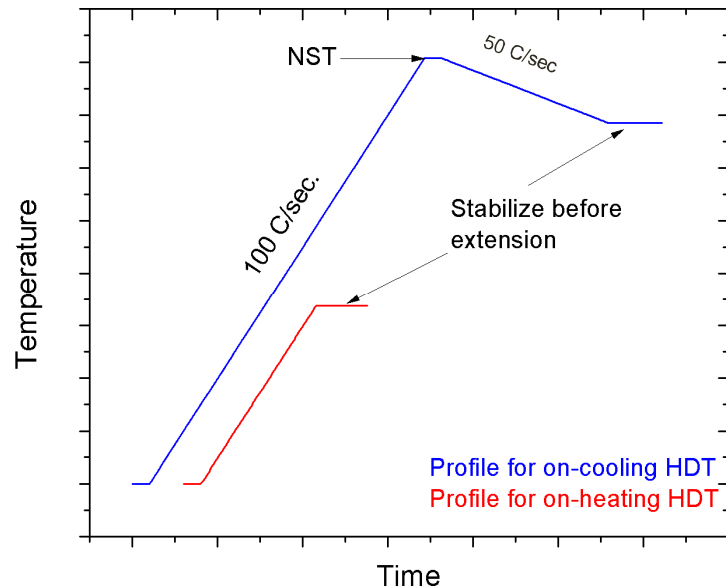
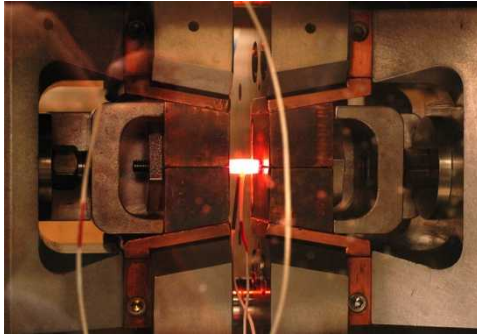


Cast Pin Tear Test Sample

Existing SMA welding studies examine
behavior of all weld zones combined

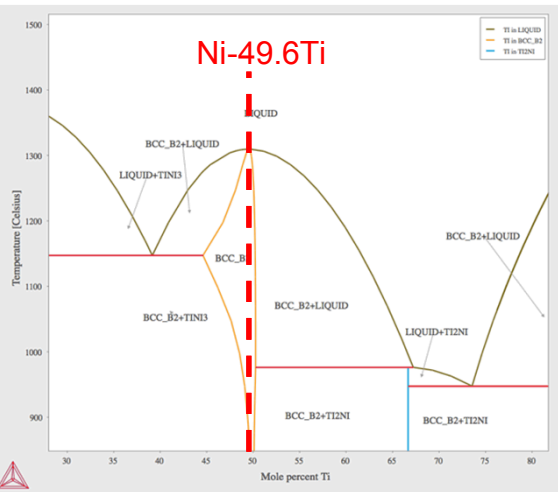
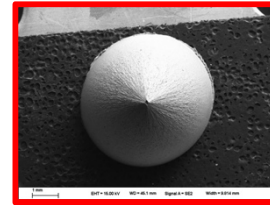
#1: Hot Ductility of SMA HAZs

- High-temperature ductility response of material provides insight into material weldability
- HAZ cracking generally associated with exhaustion of available ductility

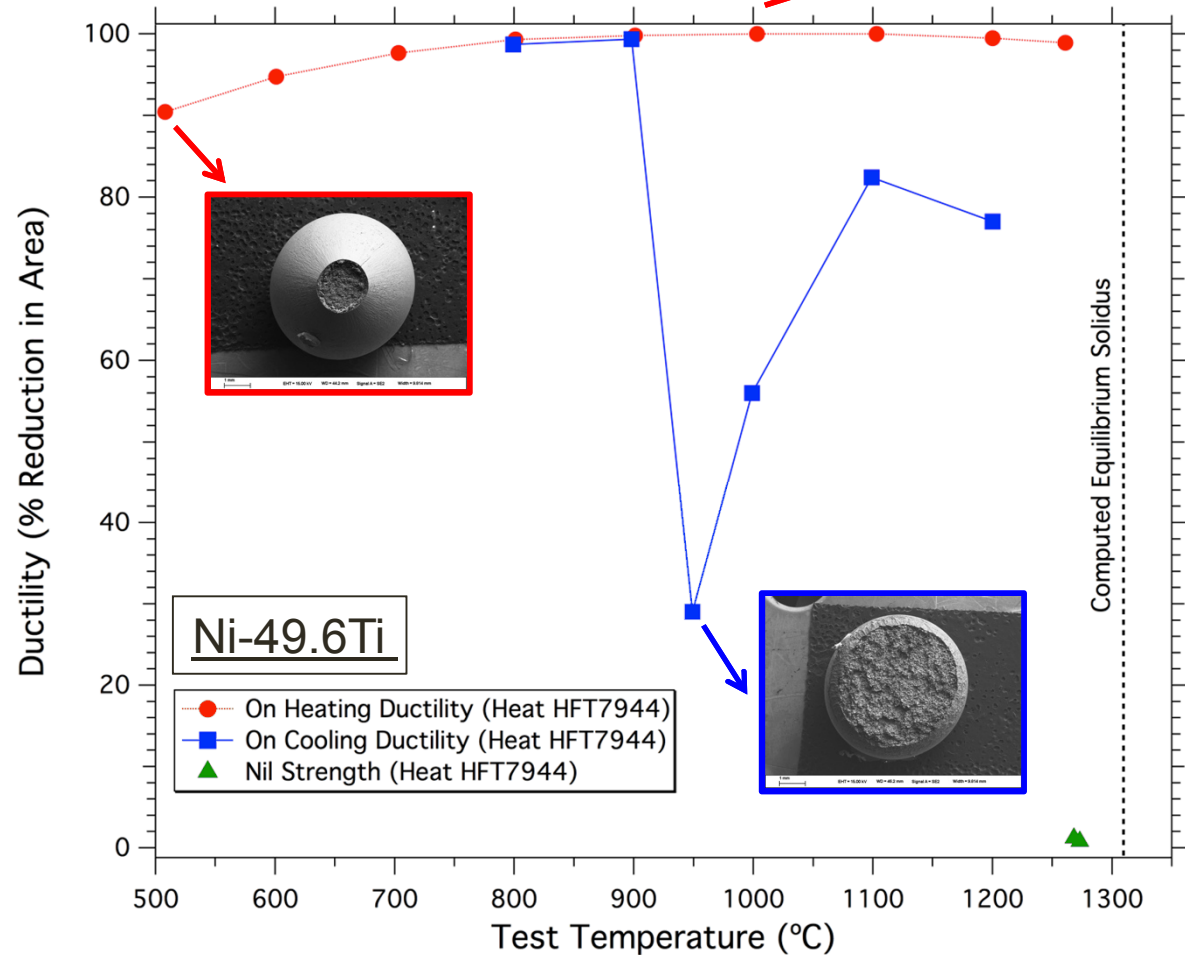
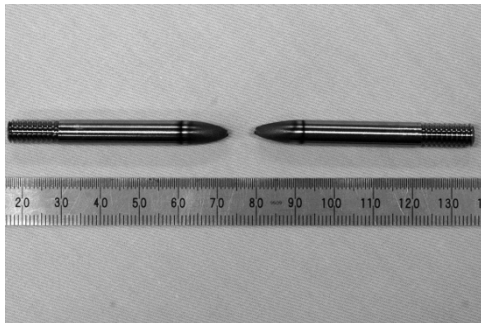


Understanding SMA Heat Affected Zone (HAZ) Behavior

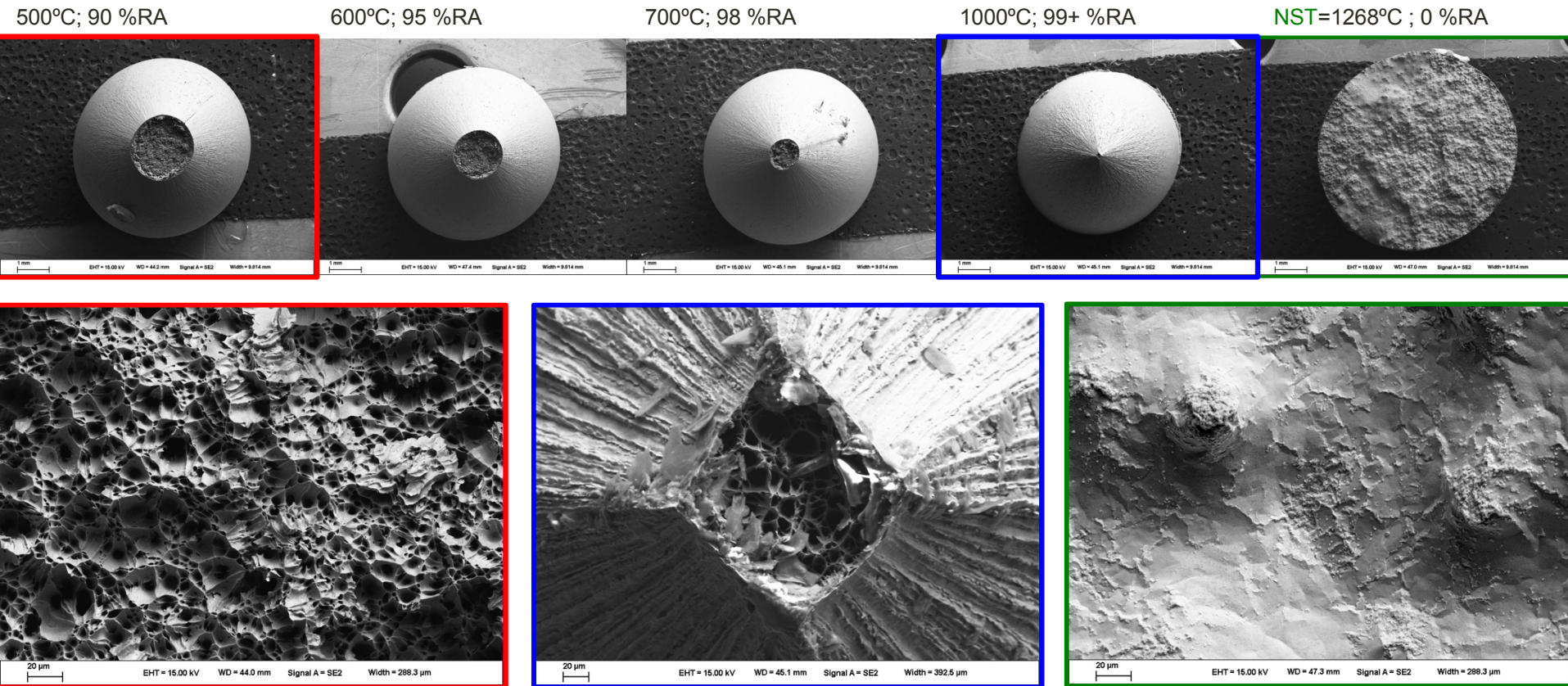
- Ni-49.6Ti demonstrates negligible HAZ liquation cracking susceptibility
- Sharp drop in ductility ~950°C on cooling



Calculated Ni-Ti Binary



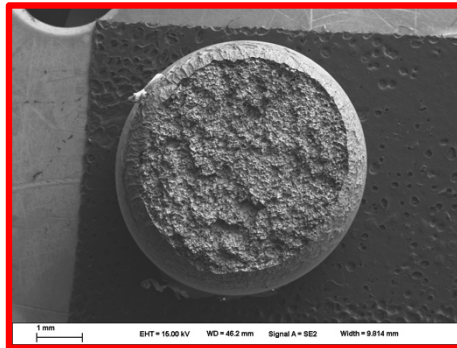
- On heating HDT samples exhibit ductile rupture up to NST temperature
 - NST exhibits flat/intergranular fracture with some solidification features



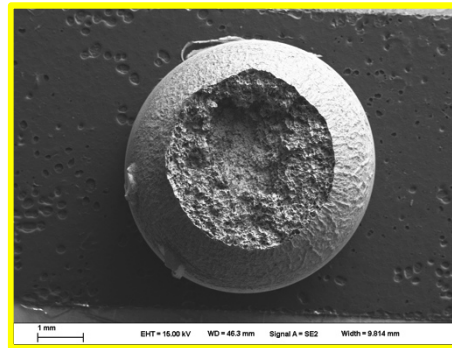
HDT Fractography: On Cooling: Ni-49.6Ti

- Precipitous drop in ductility centered $\sim 950^{\circ}\text{C}$ on cooling characterized by mixed sample failure mode: ductile rupture + smooth intergranular fracture

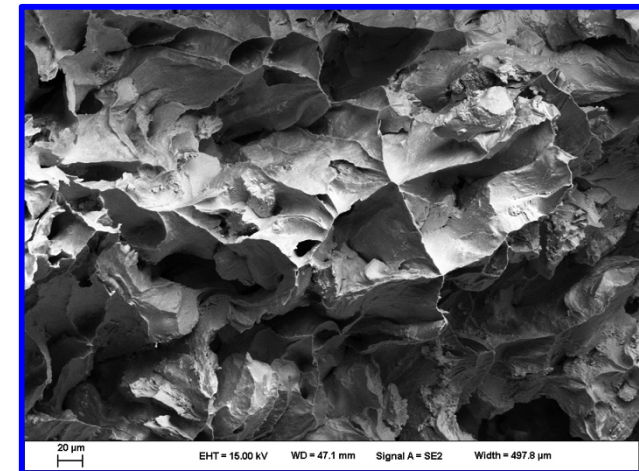
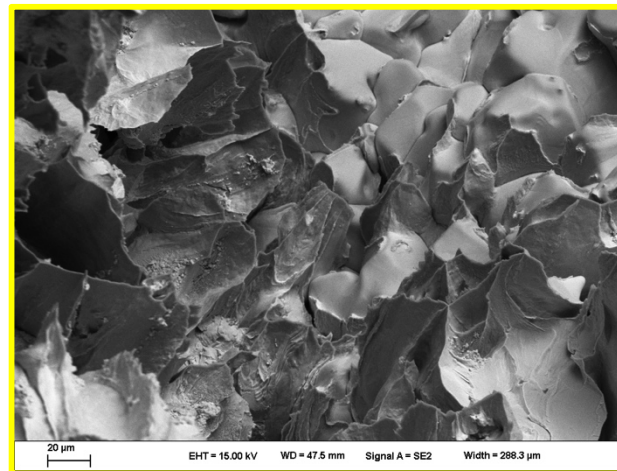
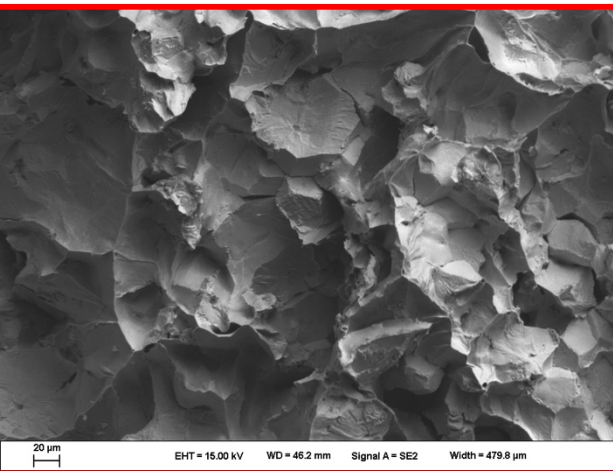
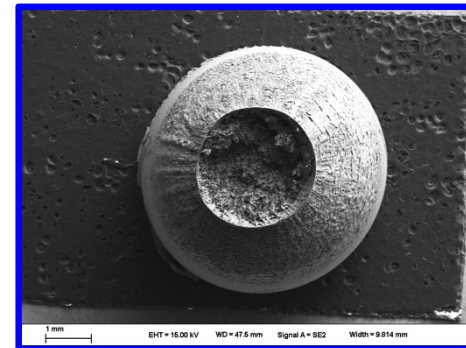
950°C; 29 %RA



1000°C; 56 %RA

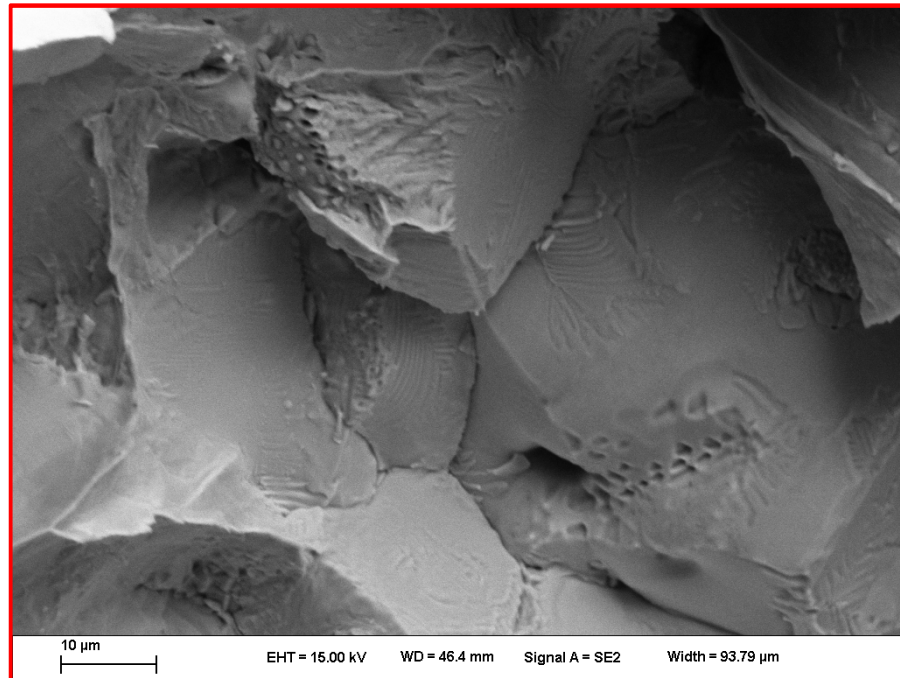


1100°C; 82 %RA



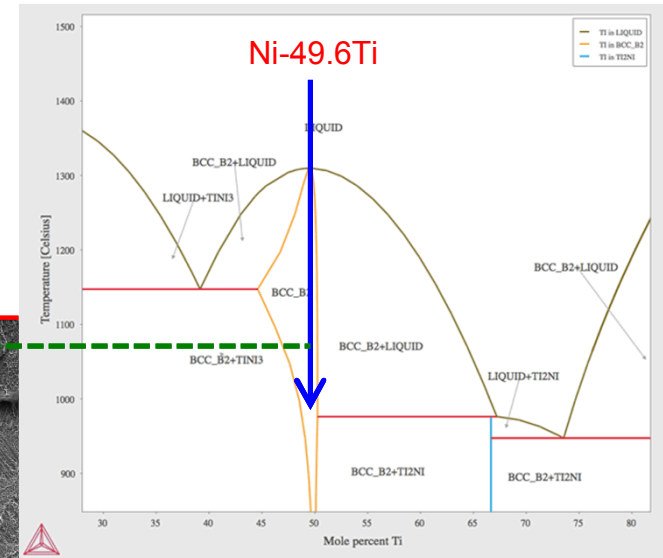
Further work required to understand on-cooling ductility dip for Ni-49.6Ti

Ni-49.6Ti
950°C; 29% RA

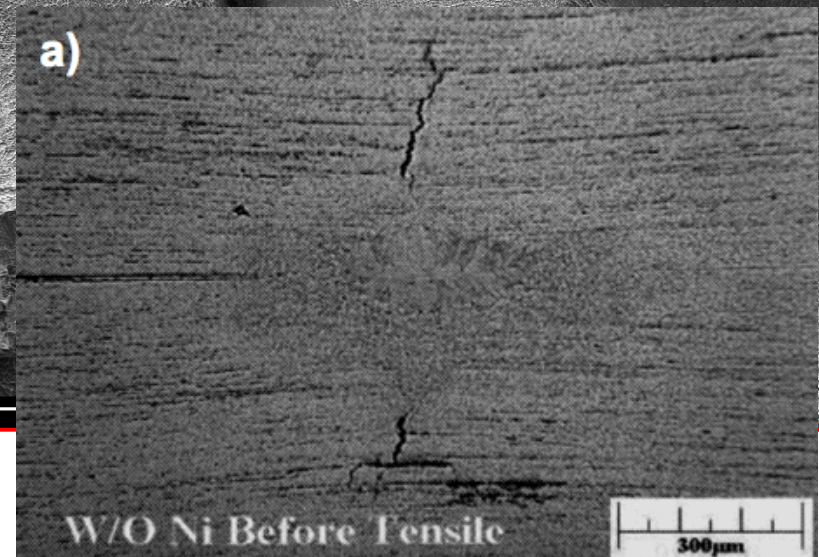


Little evidence of local ductility at grain boundaries

950°C



1-4V
RA

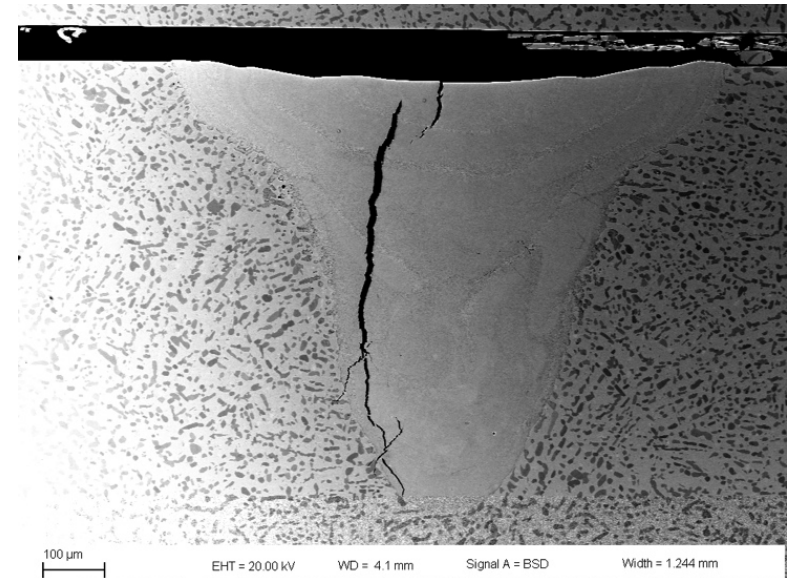
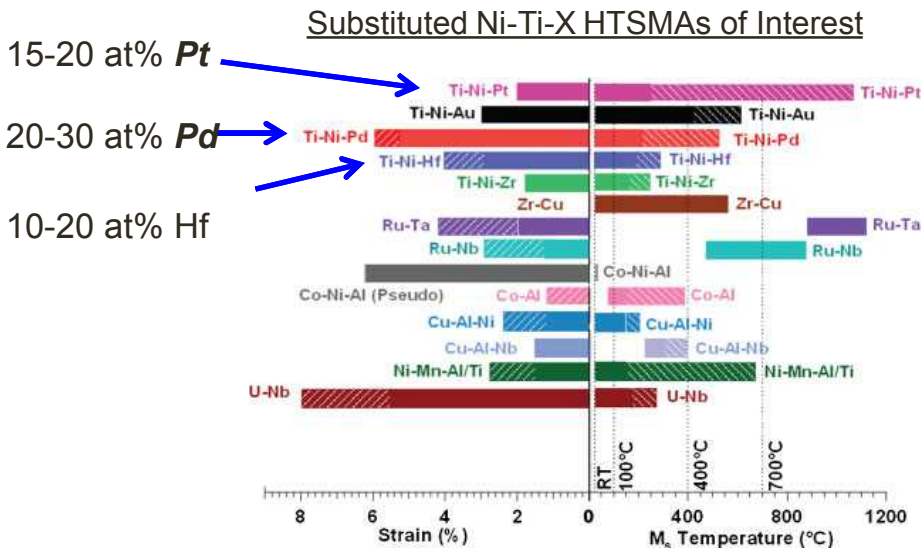


Further characterization will provide insight into
HAZ cracking observed in other studies

9

#3 SMA Solidification Crack Susceptibility

- Cost and manufacturability issues for SMA/HTSMA preclude the use of conventional solidification crack susceptibility evaluation techniques (e.g., Varestraint)

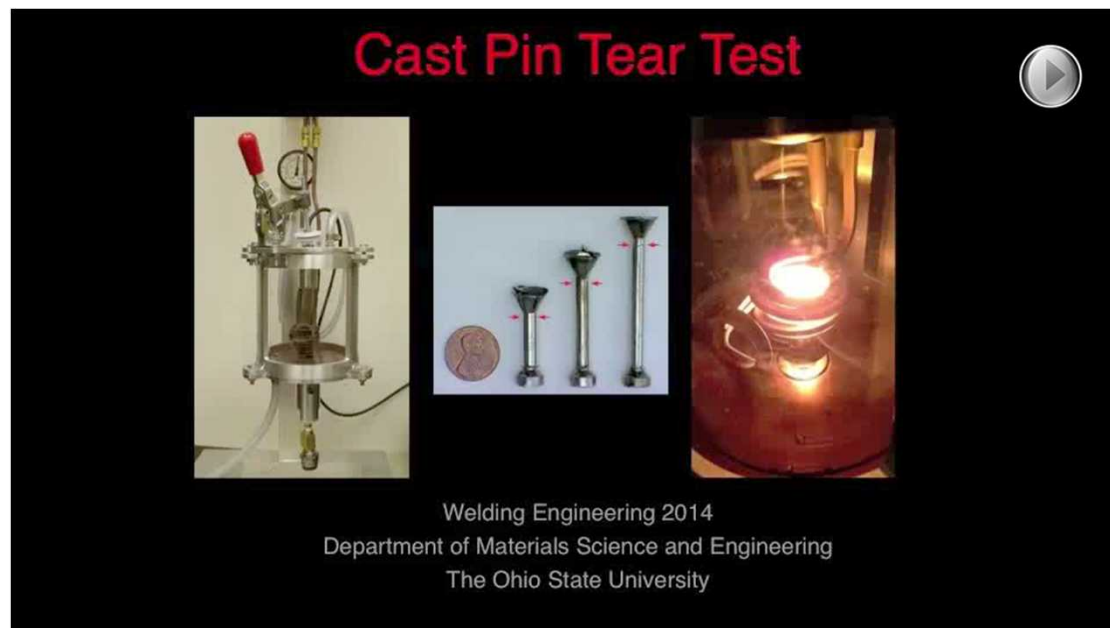
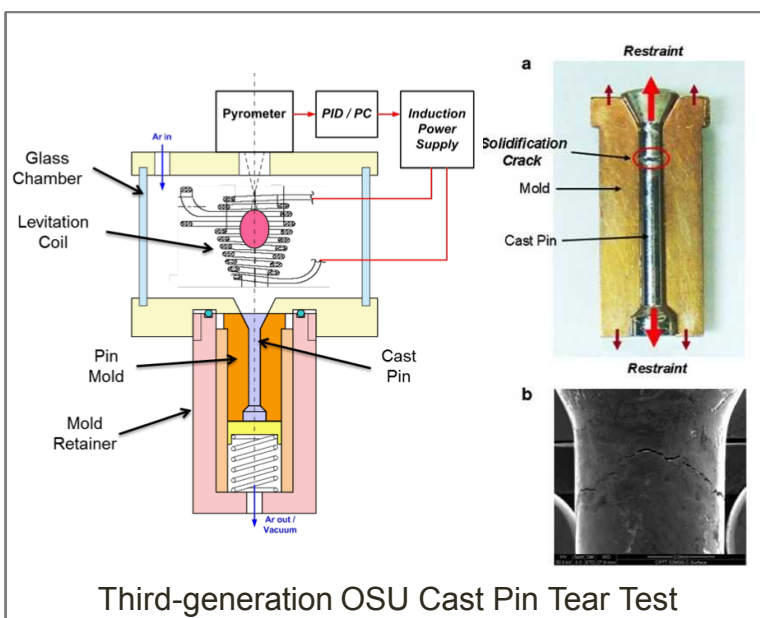


Solidification crack in Ni-Ti-Pt HTSMA laser weld

- Large quantities of testable product forms is cost prohibitive

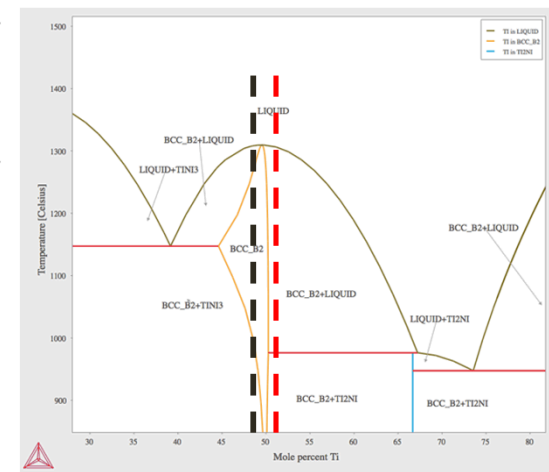
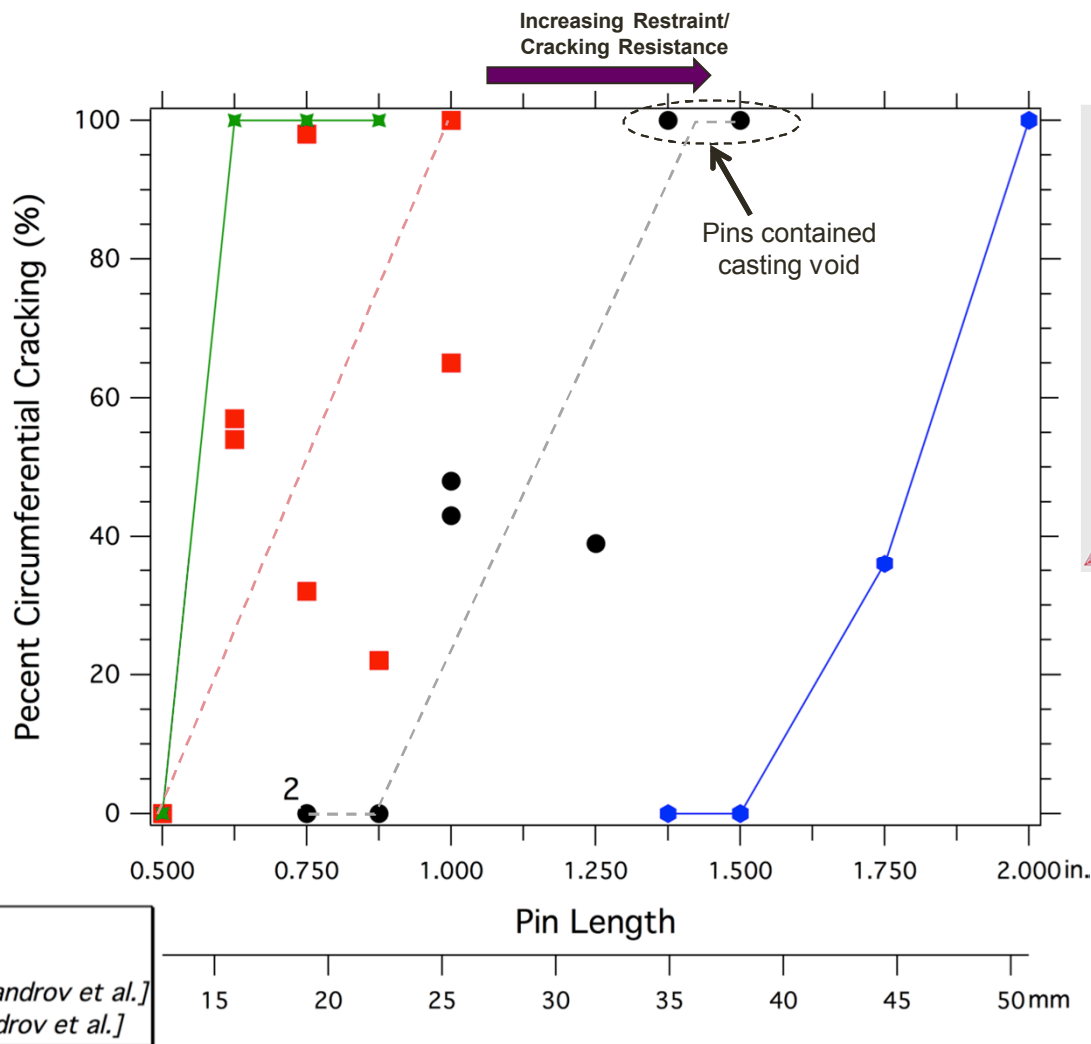
University Partnership Enables Evaluation of SMA Solidification Cracking Susceptibility

- Cast pin tear testing (CPTT) only requires small amount of material: 10-15 g per test sample
- Good qualitative agreement with established augmented strain test methods, e.g., Varestraint



SMA CPTT Results

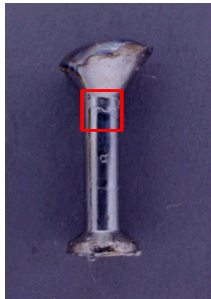
- SMA alloys in general are moderately crack susceptible
 - Ti-rich SMA alloys comparatively more solidification crack sensitive compared to Ni-rich



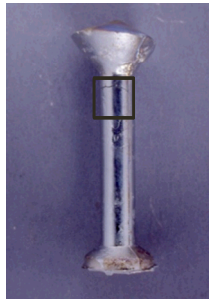
- Non-equilibrium (Scheil) solidification temperature ranges:
 - 161°C (Ni-49Ti)
 - 335°C (Ni-51Ti)

Solidification features on CPTT fracture surface consistent with solidification cracking

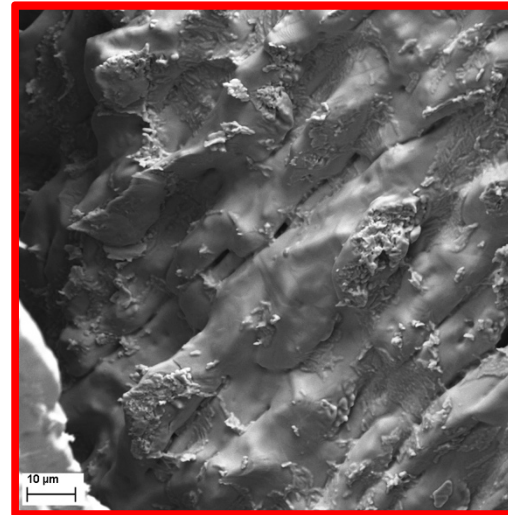
'Ti-rich'
Ni-51Ti



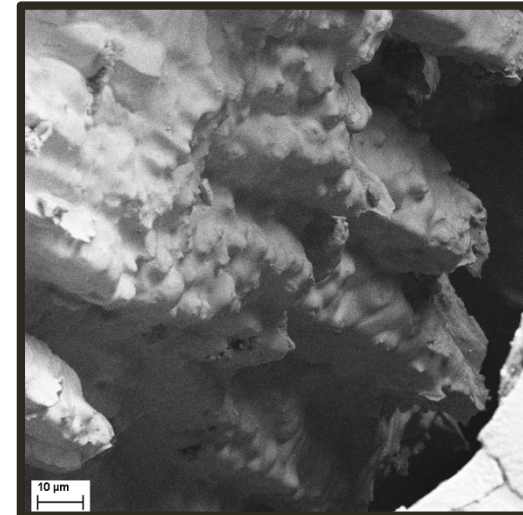
'Ni-rich'
Ni-49Ti



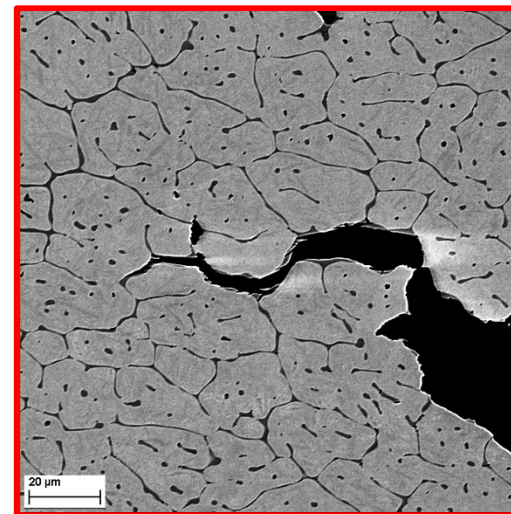
10 mm



Terminal eutectic phase decorates fracture surface of Ni-51Ti CPTT



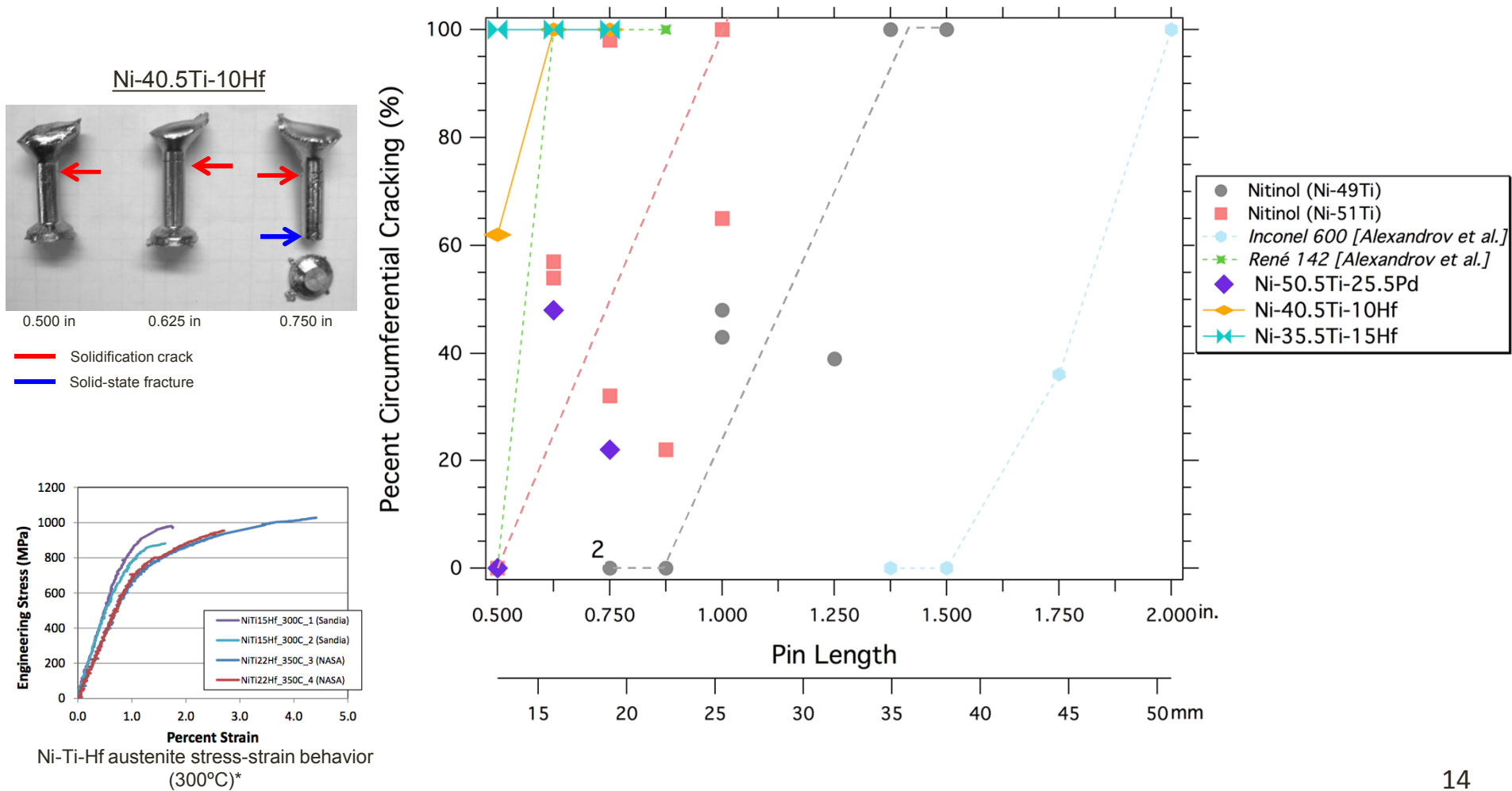
Fracture surface of Ni-49Ti largely free of terminal microconstituent on fracture surface



Cross section of Ni-51Ti CPTT reveals fracture along NiTi-Ti₂Ni eutectic

Preliminary HTSMA CPTT Results

- Ni-Ti-Hf alloys exhibit extensive cracking even for smallest pin mold length
- Ni-Ti-Pd alloy (24.0 Ni – 50.5 Ti – 25.5 Pd) qualitatively similar CPTT response as Ti-rich NiTi

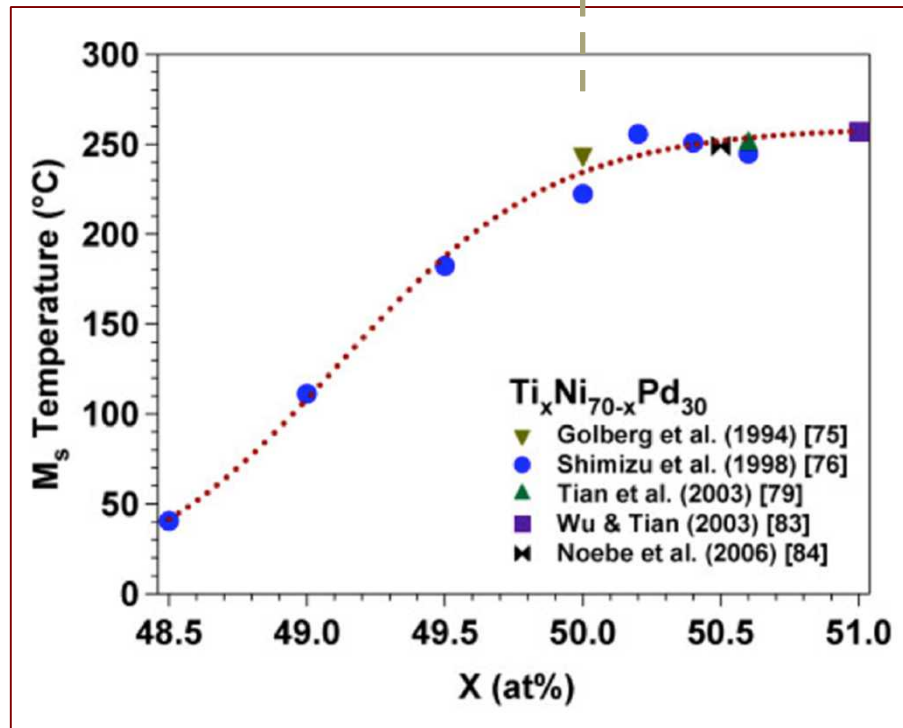


HTSMA Practical Implications

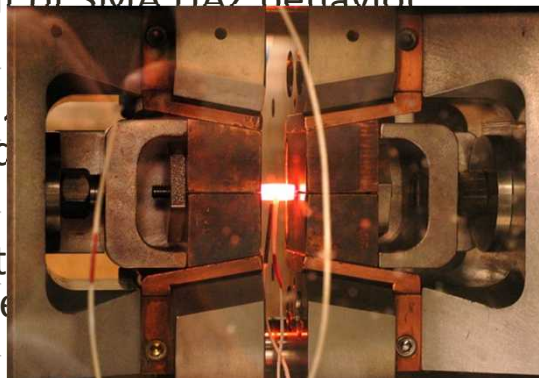
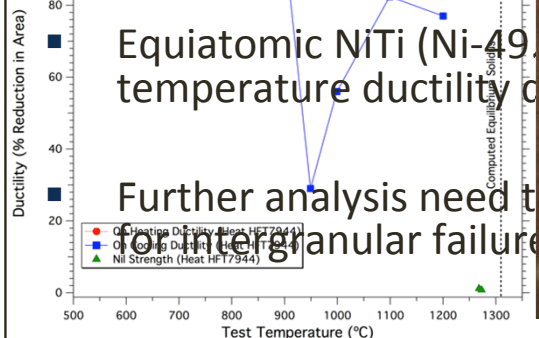
- Ti-rich ternary Ni-Ti-X HTSMAs ideal for compositional robustness with respect to transformation temperature may not be ideal selection for fusion welding applications

Ni-rich
Ti-rich
Highly composition-dependent transformation temperature
Composition-independent transformation temperature

←
→

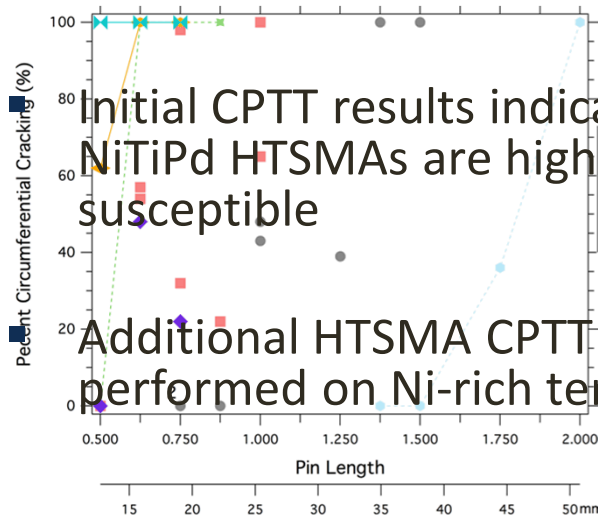


- Gleeble hot ductility experiments provide basis for meaningful assessment of SMA HAZ behavior



- Ranking assessment of SMA solidification crack susceptibility achieved via CPTT
- Compositionally dependent predicted STR in agreement with CPTT results for Ti vs. Ni-rich NiTi SMAs

10 μ m



Initial CPTT results indicate Ti-rich NiTiHf and NiTiPd HTSMAs are highly solidification crack susceptible

Additional HTSMA CPTT testing will be performed on Ni-rich ternary compositions



Acknowledgments

- The work has been funded wholly by SNL Laboratory Directed Research & Development (LDRD)

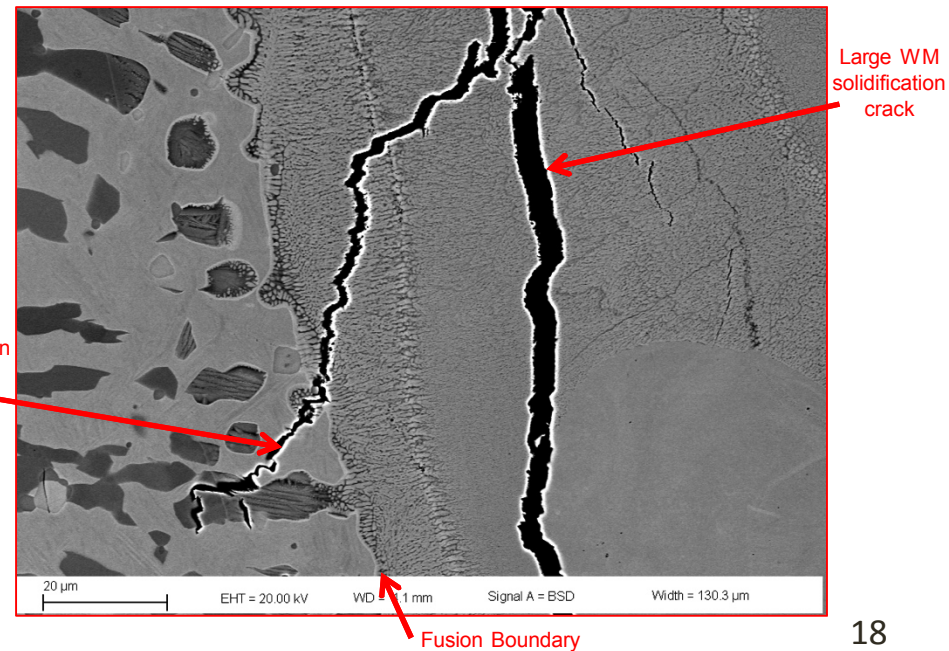
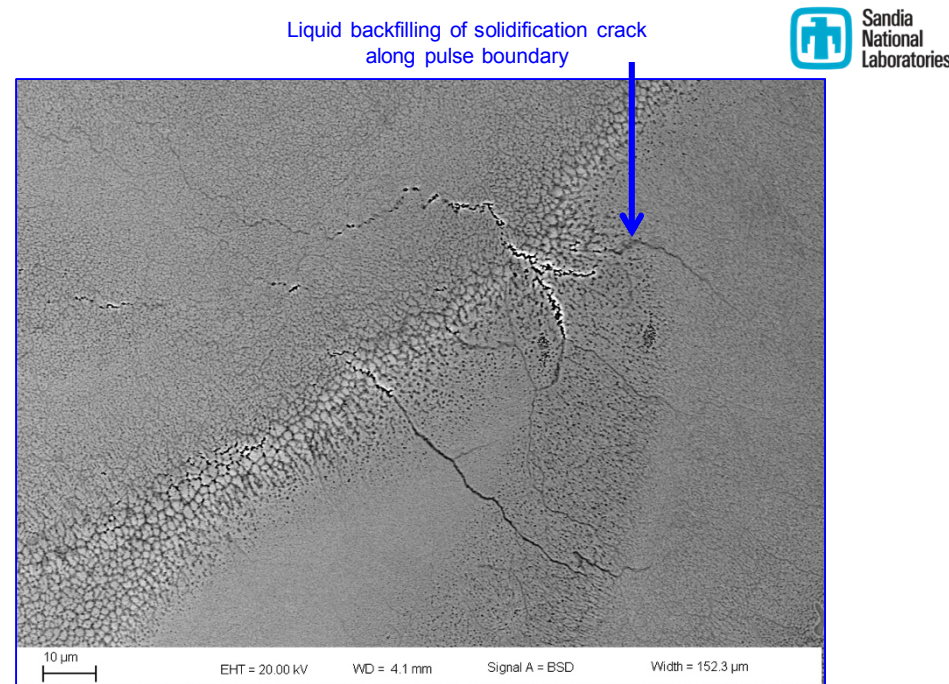
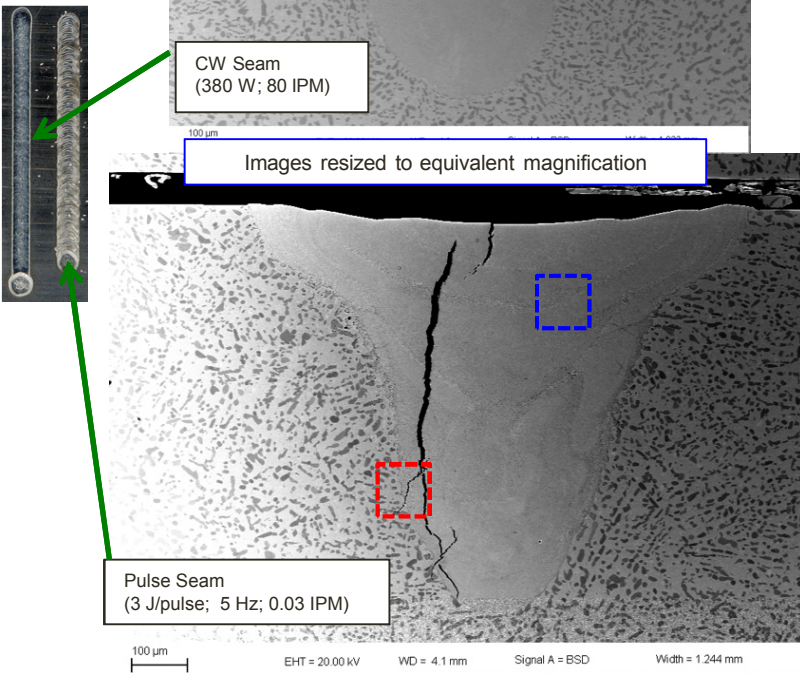
- Special thanks to:
 - The Ohio State University: Welding & Joining Metallurgy Group
 - Dr. Boian Alexandrov
 - Tyler Payton
 - Peter Duran
 - Don Susan
 - Charlie Robino
 - Alice Kilgo
 - Bonnie McKenzie
 - Amy Allen



HTSMA Laser Beam Weld

- Autogenous laser welds can be successfully be made on cast Ni-Ti-Pt HTSMAs
- Cracking in pulsed laser welds highlights material process sensitivity

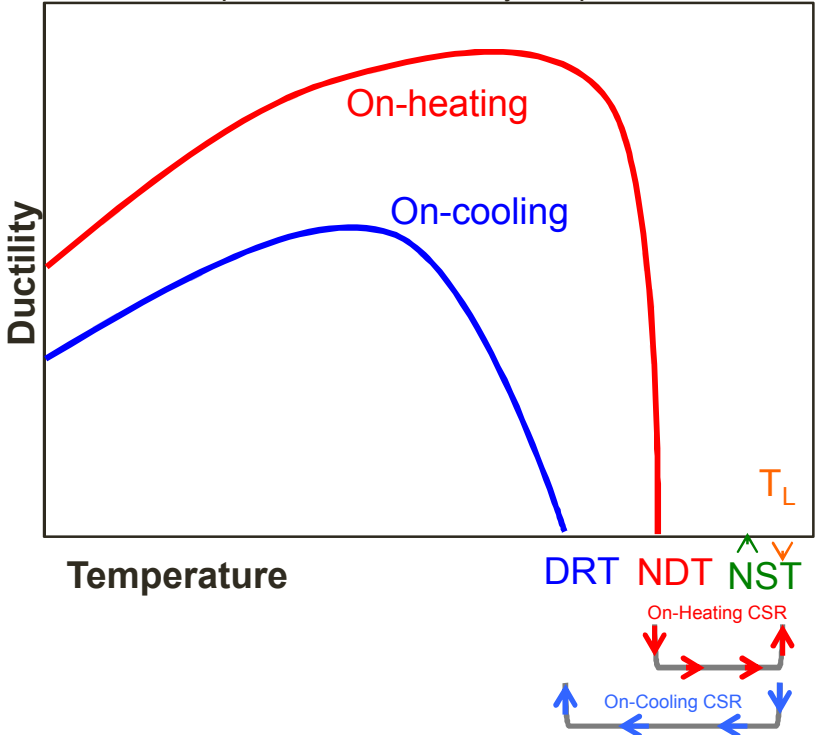
HTSMA: 31.5Ni-50.5Ti-18Pt



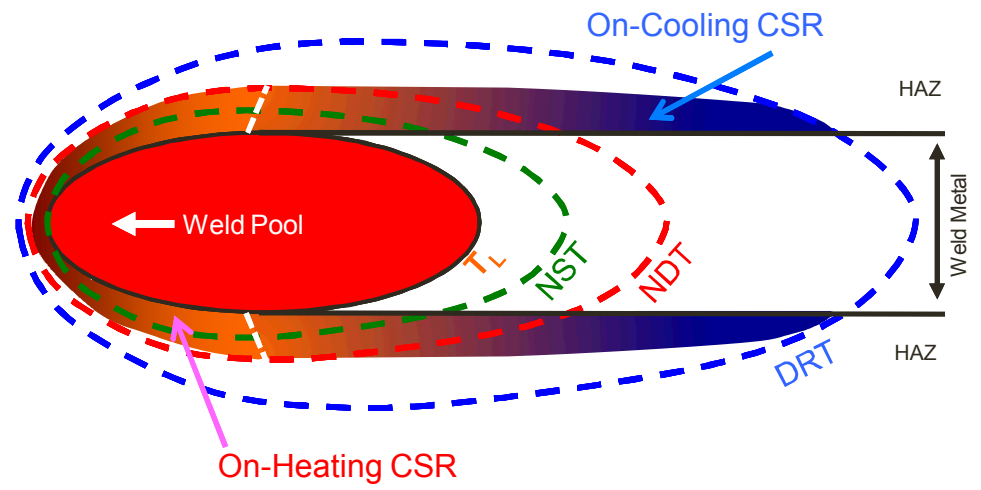
Understanding SMA Heat Affected Zone (HAZ) Behavior

- Material ductility is related to cracking susceptibility
- Hot ductility test (HDT) measures material ductility as a function of HAZ-relevant temperatures/heating rates

Example: Measured Ductility Response



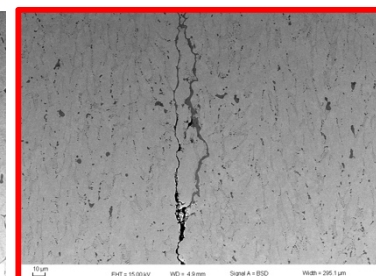
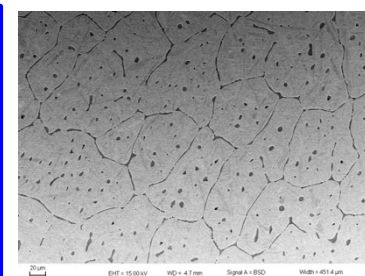
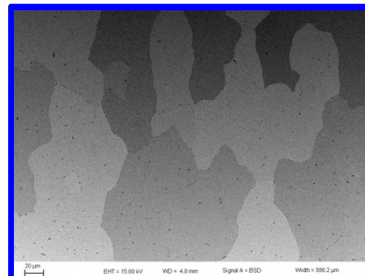
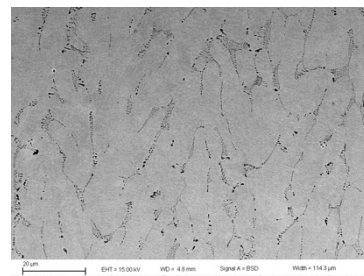
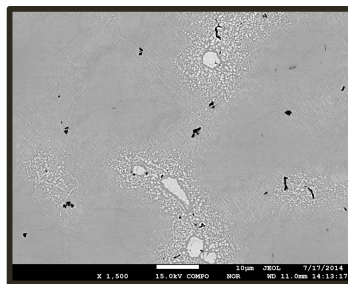
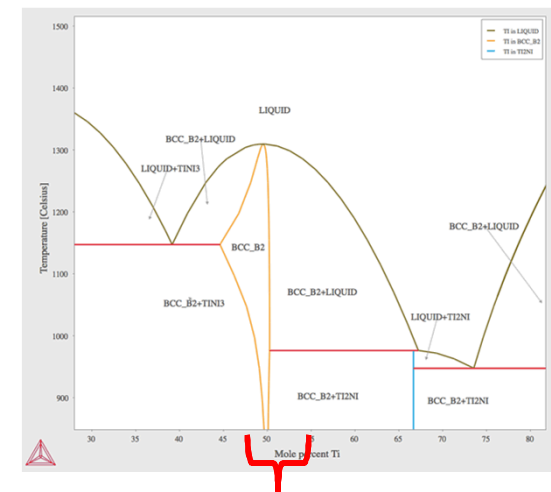
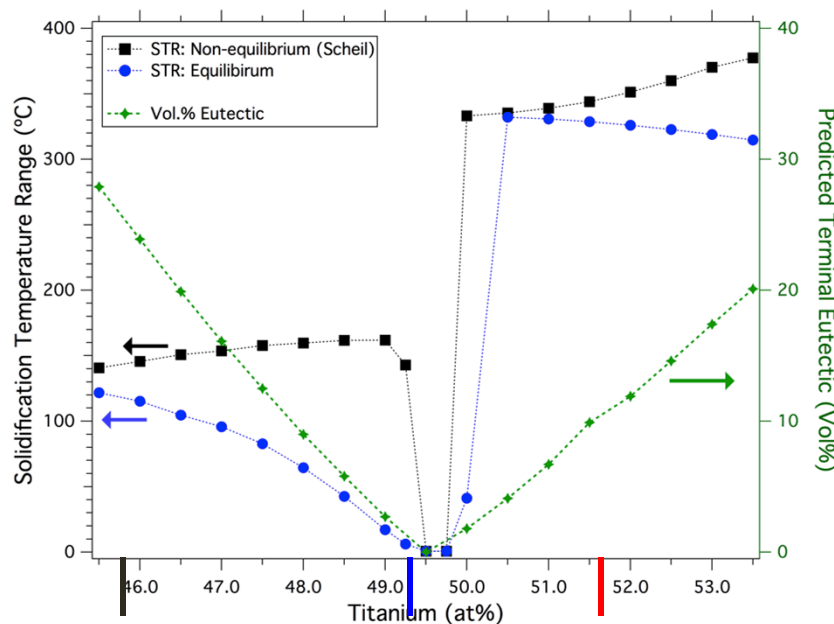
- NST:** Nil-strength temperature
 - T at which material cannot support load
- NDT:** Nil-ductility temperature
 - T at which material fails with no ductility
- DRT:** Ductility recovery temperature
 - T at which ductility recovered on cooling



Translation of Measured HDT Temperatures to HAZ Crack Susceptible Regions (CSR)

Significant Solidification Temperature Range Compositional Dependence for NiTi SMAs

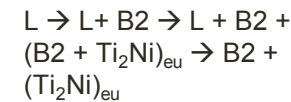
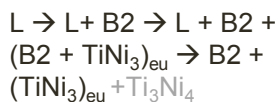
- Ti-rich alloys show large predicted solidification temperature range (STR).
 - Qualitatively agrees with preliminary CPTT tests
- Near-equiatomic and Ni-rich SMAs less prone to solidification cracking



Ni-Rich

Near-equiatomic

Ti-Rich



Understanding SMA Heat Affected Zone (HAZ) Behavior: Functional Behavior

- Technique is informative regarding how joining process alters functional behavior of specific regions surrounding weld
- Simulated Ni-49.6Ti HAZ shows apparent shift in A_p with increasing HAZ peak temperature
- On-cooling SMA behavior altered as a result of HAZ thermal cycles
 - 2-stage transformation destroyed with peak HAZ temperatures 700°C and greater

