

Simulating Rectified Motion in a Piston Assembly Subjected to Vibrational Acceleration

**Jonathan Clausen, J.R. Torczynski,
L.A. Romero, and T.J. O'Hern**

*American Physical Society Division of Fluid Dynamics 67th Annual
Meeting; San Francisco, California
November 23-25, 2014*

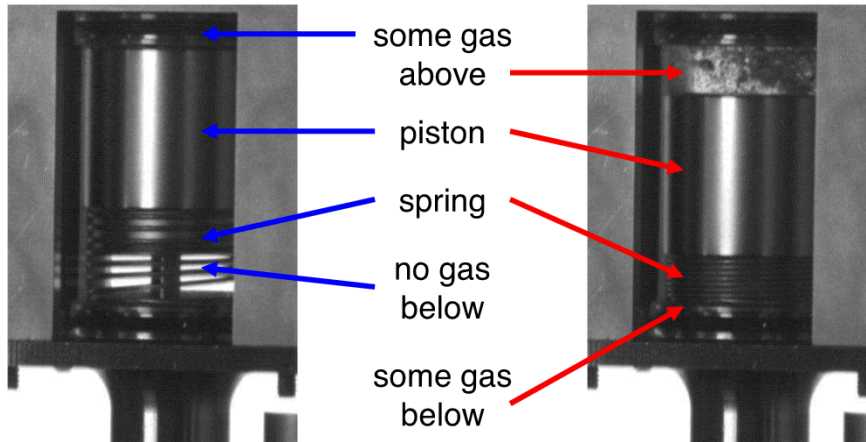


*Exceptional
service
in the
national
interest*



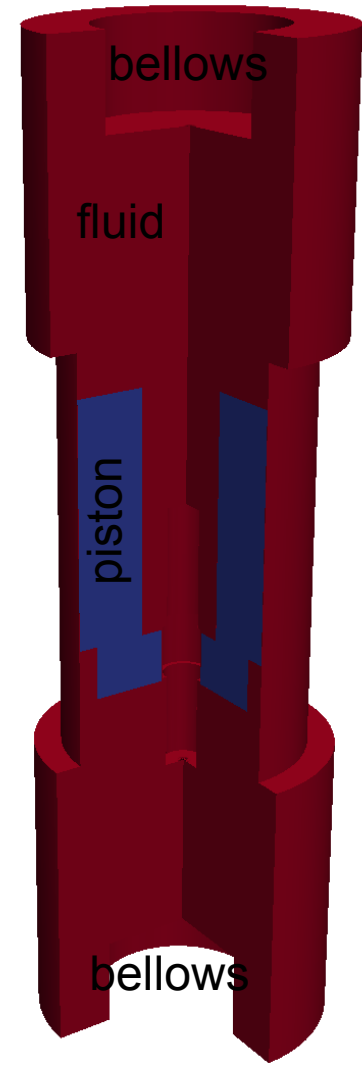
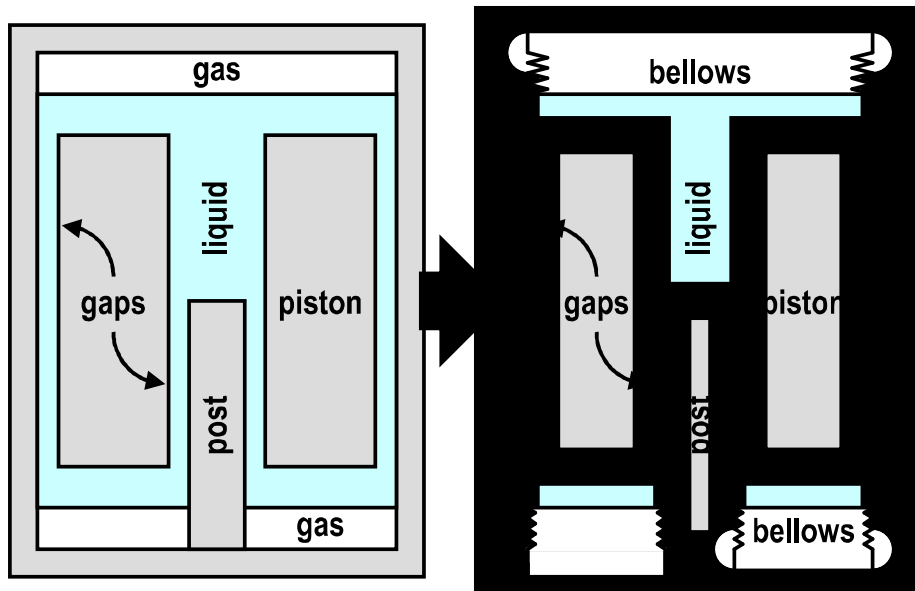
Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000. SAND NO. 2011-XXXXP

Piston Assembly



Vibration **off**
Spring supports piston

Vibration **on**
Piston compresses spring



axisymmetric

Summary of Theory

Piston	$M_P \ddot{Z}_P = -K_P Z_P - M_{PG} g_V + F_P, \quad M_{PG} = M_P - M_{LP}$
Bellows	$M_B \ddot{Z}_B = -K_B Z_B - M_{BG} g_V + F_B - \rho g (1 - \kappa) A_B Z_B$
	$Z_{BU} = Z_B, \quad Z_{BL} = \kappa Z_B, \quad \kappa = A_{BU} / A_{BL}, \quad A_B = A_{BU}, \quad g_V = g_1 \cos \omega t$
	$M_B = M_{BU} + \kappa^2 M_{BL}, \quad K_B = K_{BU} + \kappa^2 K_{BL}, \quad M_{BG} = M_{BU} + \kappa M_{BL} + \rho L_B A_B$
Liquid Forces	$F_P = \hat{\mathbf{e}}_z \cdot \int_{S_P} \boldsymbol{\sigma} \cdot \hat{\mathbf{n}} dS, \quad F_B = \hat{\mathbf{e}}_z \cdot \int_{S_{BU}} \boldsymbol{\sigma} \cdot \hat{\mathbf{n}} dS + \kappa \hat{\mathbf{e}}_z \cdot \int_{S_{BL}} \boldsymbol{\sigma} \cdot \hat{\mathbf{n}} dS$

Liquid	$\frac{\partial}{\partial \mathbf{x}} \cdot \mathbf{u} = 0$
	$\rho \left(\frac{\partial}{\partial t} + \mathbf{u} \cdot \frac{\partial}{\partial \mathbf{x}} \right) \mathbf{u} = \frac{\partial}{\partial \mathbf{x}} \cdot \boldsymbol{\sigma}$
	$\boldsymbol{\sigma} = -p \mathbf{I} + \mu \left(\frac{\partial \mathbf{u}}{\partial \mathbf{x}} + \frac{\partial \mathbf{u}^T}{\partial \mathbf{x}} \right)$
	$\mathbf{u} = \mathbf{u}_{\text{surface}} \text{ on walls}$

Quasi-steady theory

Two modes of motion

■ Poiseuille

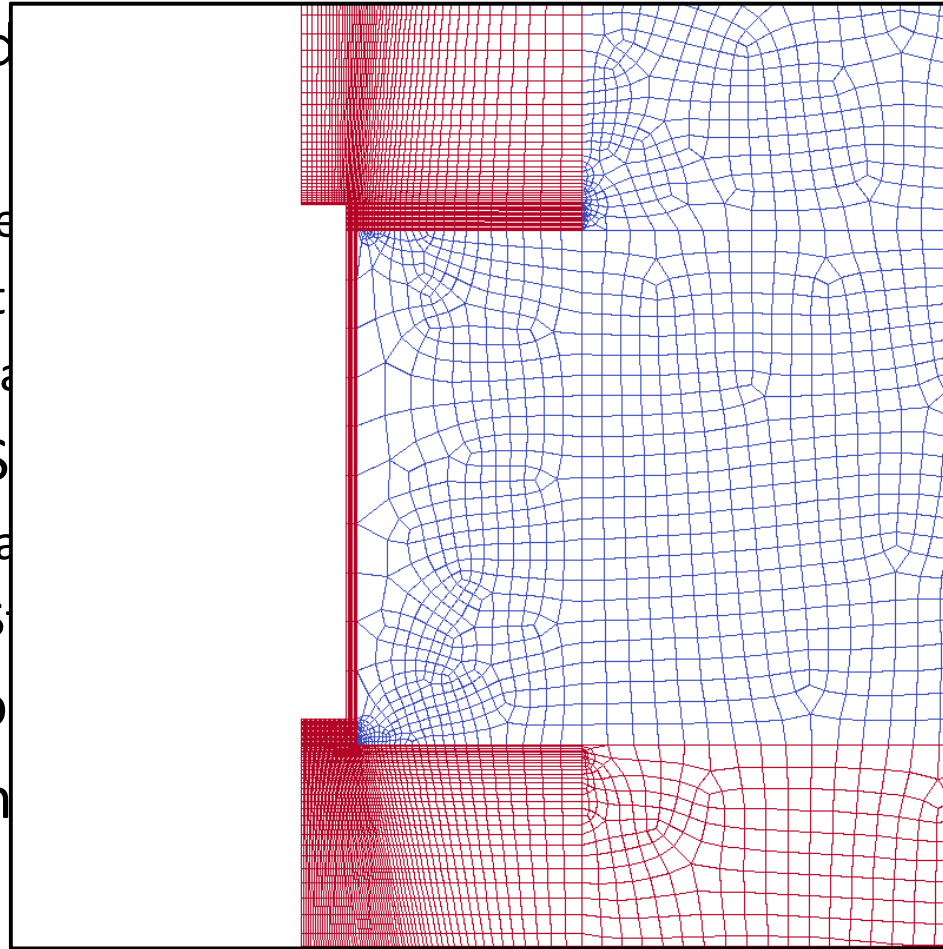
- high dissipation; high added mass
- high pressure difference

■ Couette

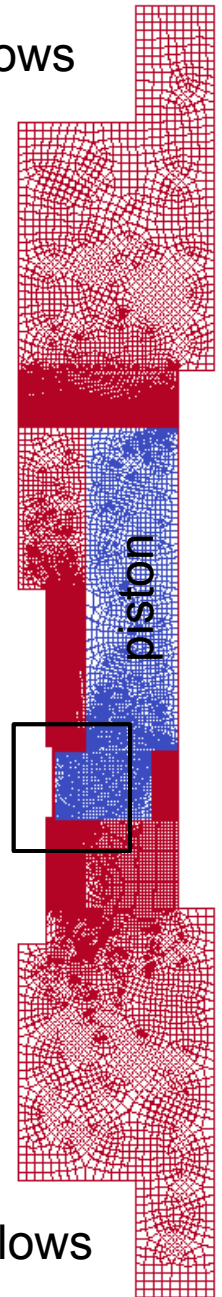
- lower dissipation
- less drag on piston
- piston and bellows motion dictated by area ratio
- resonance behavior

Simulation Details

- Quasi-steady
- Sierra/TF
 - Q1 finite e
 - Full sensit
 - ALE simulat
- Equations S
 - Solid Dyna
 - Navier—S
- Bellows mo
- Piston sprin

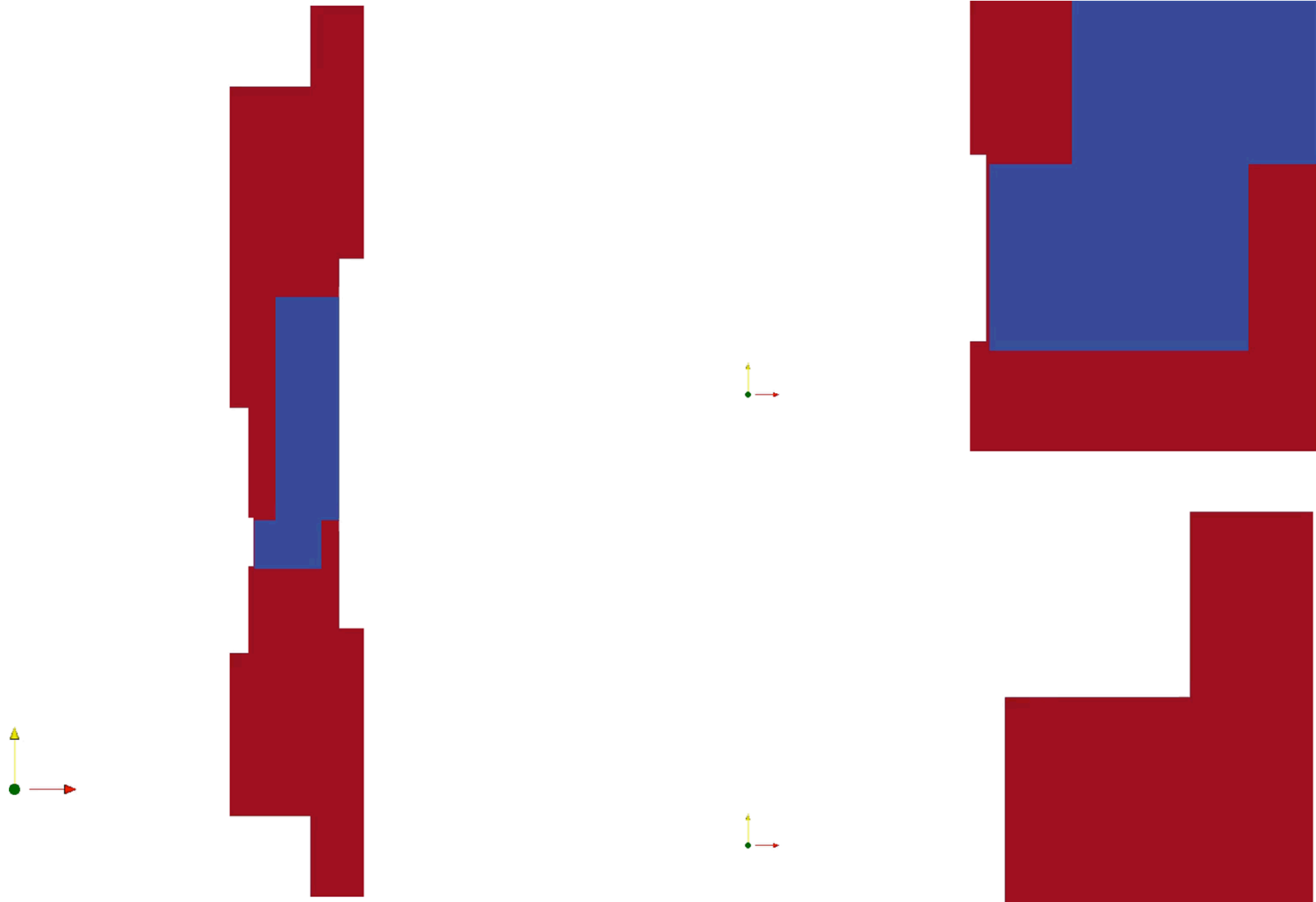


bellows

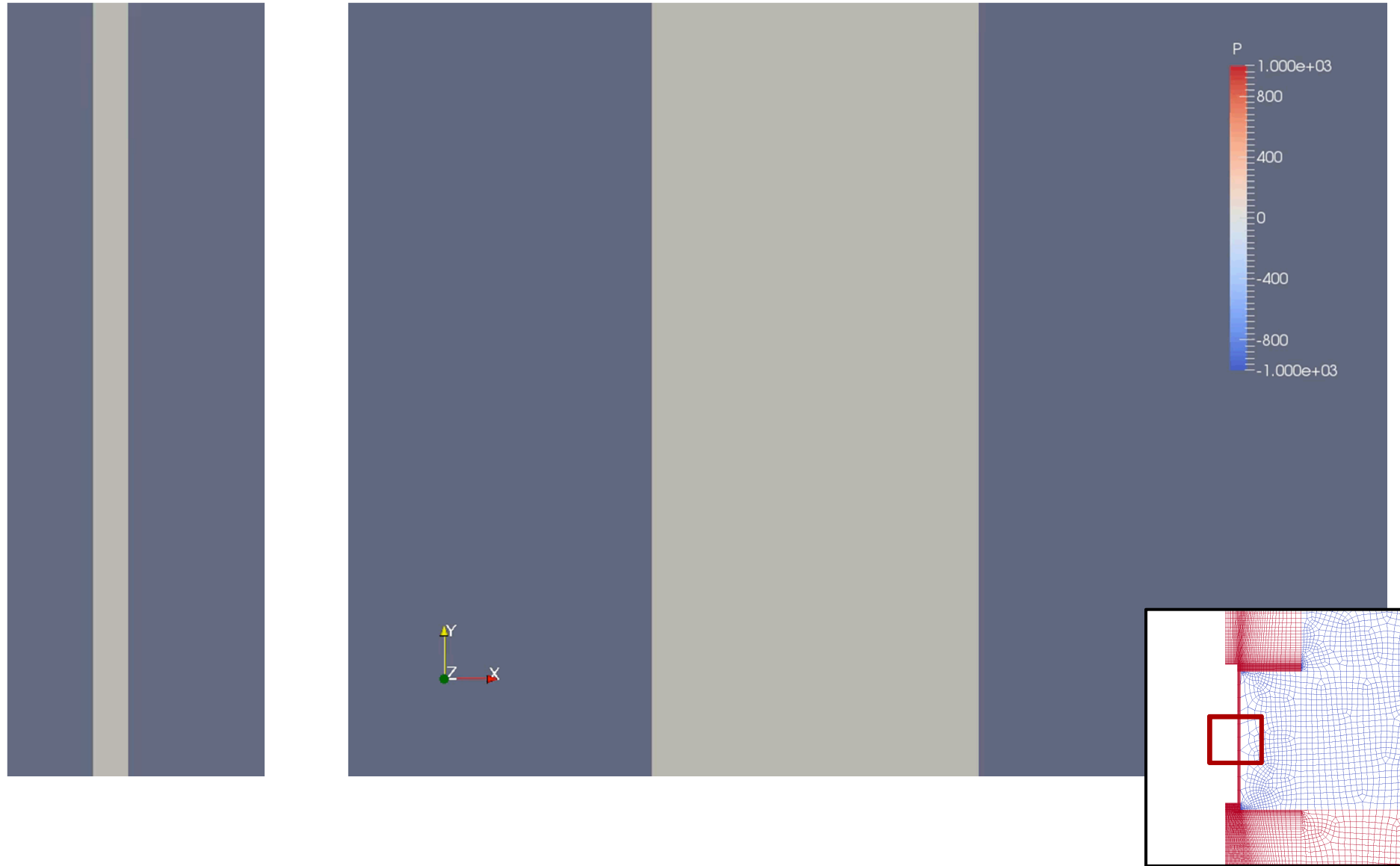


bellows

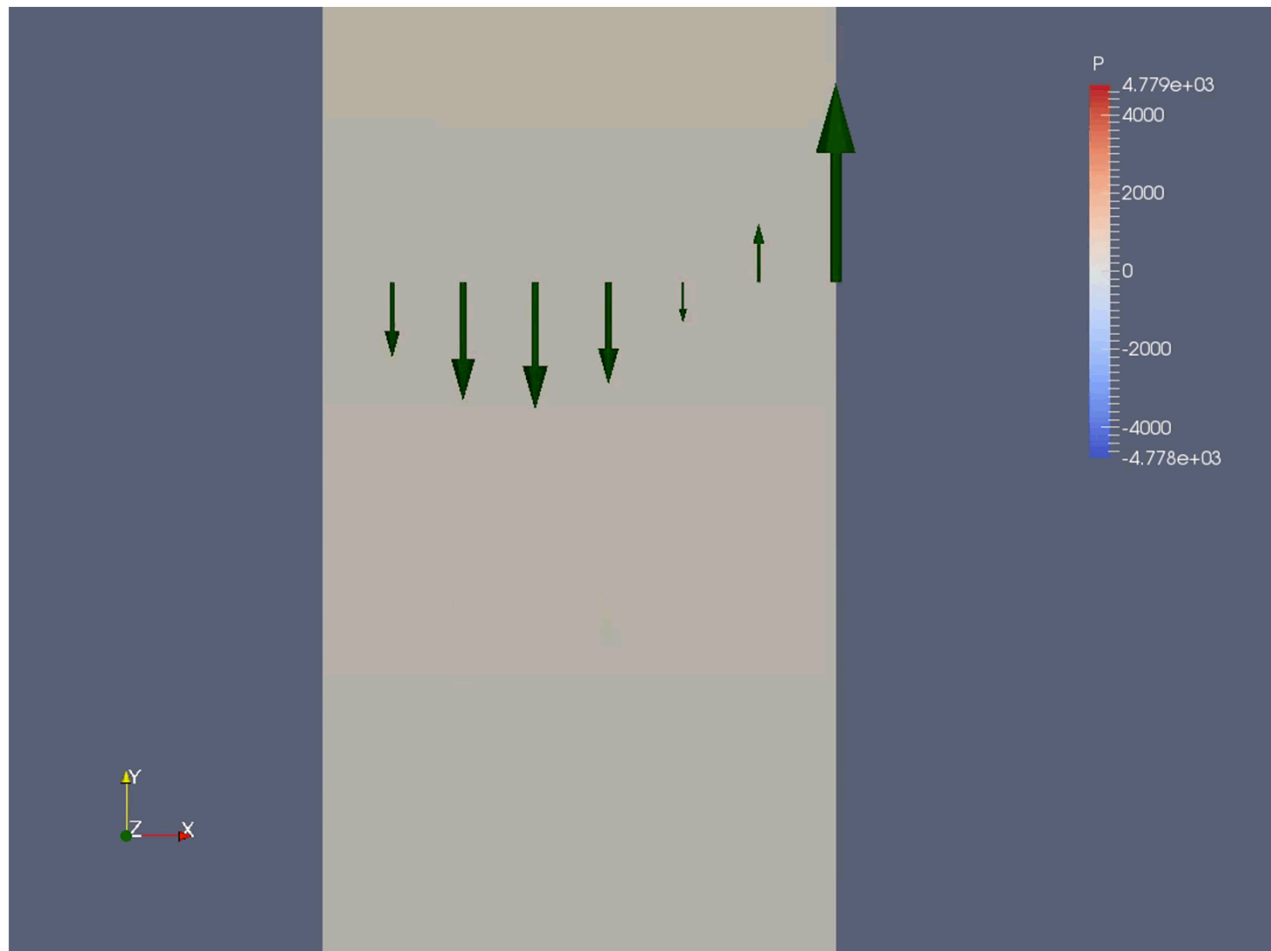
ALE Simulation of Piston



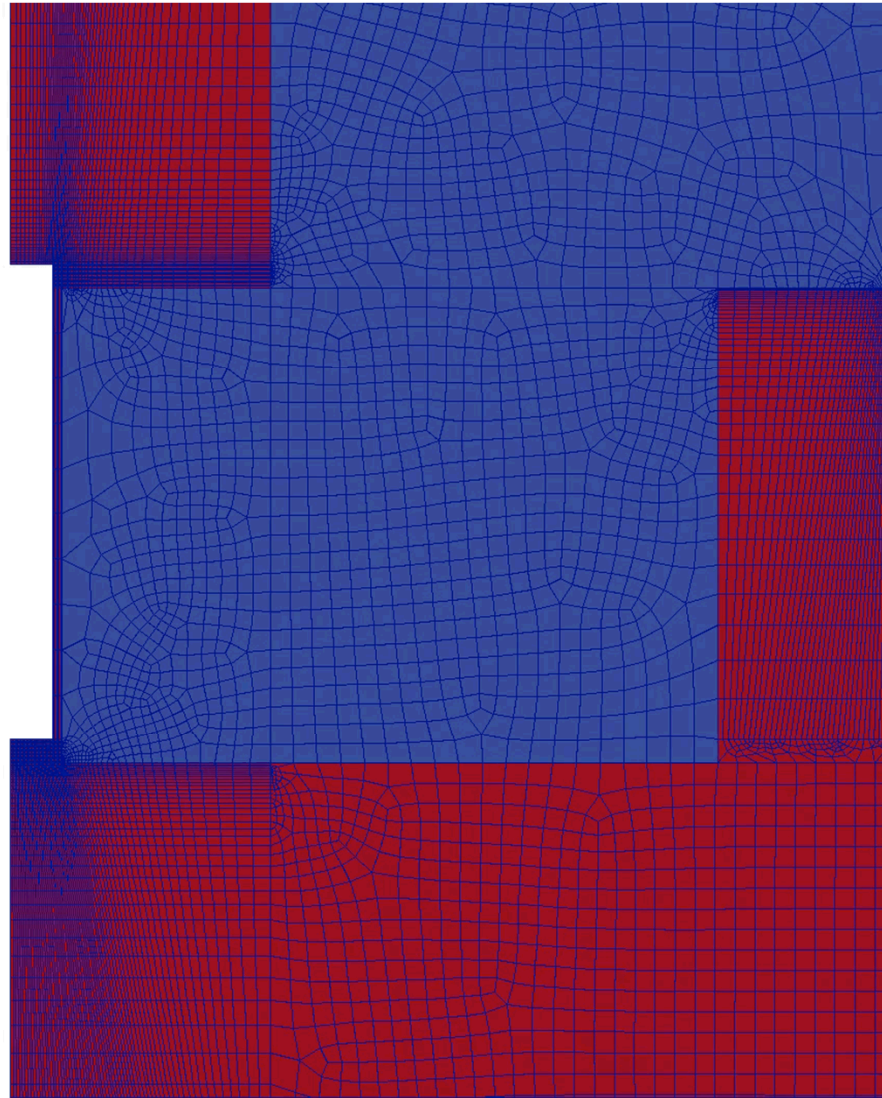
ALE Simulation of Piston

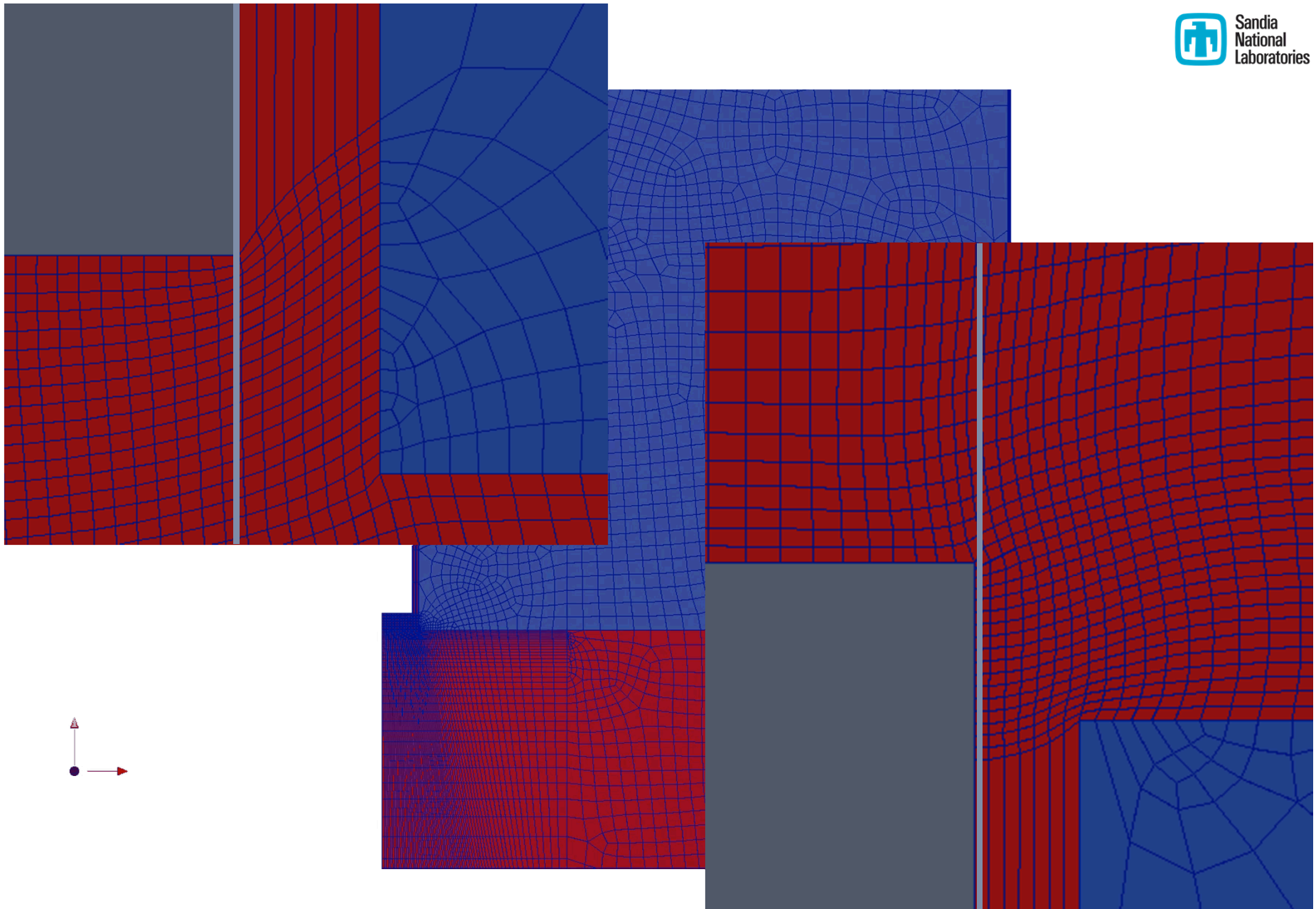


Flow modes

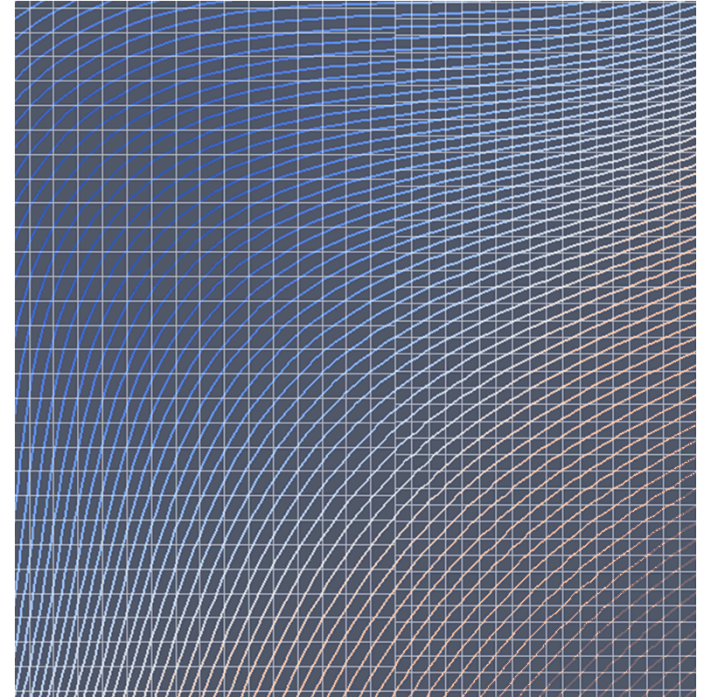
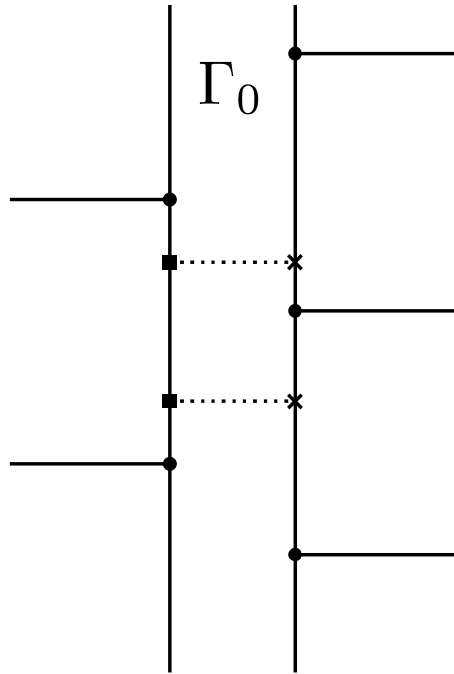


ALE Simulation of Piston





Sliding Mesh Scheme

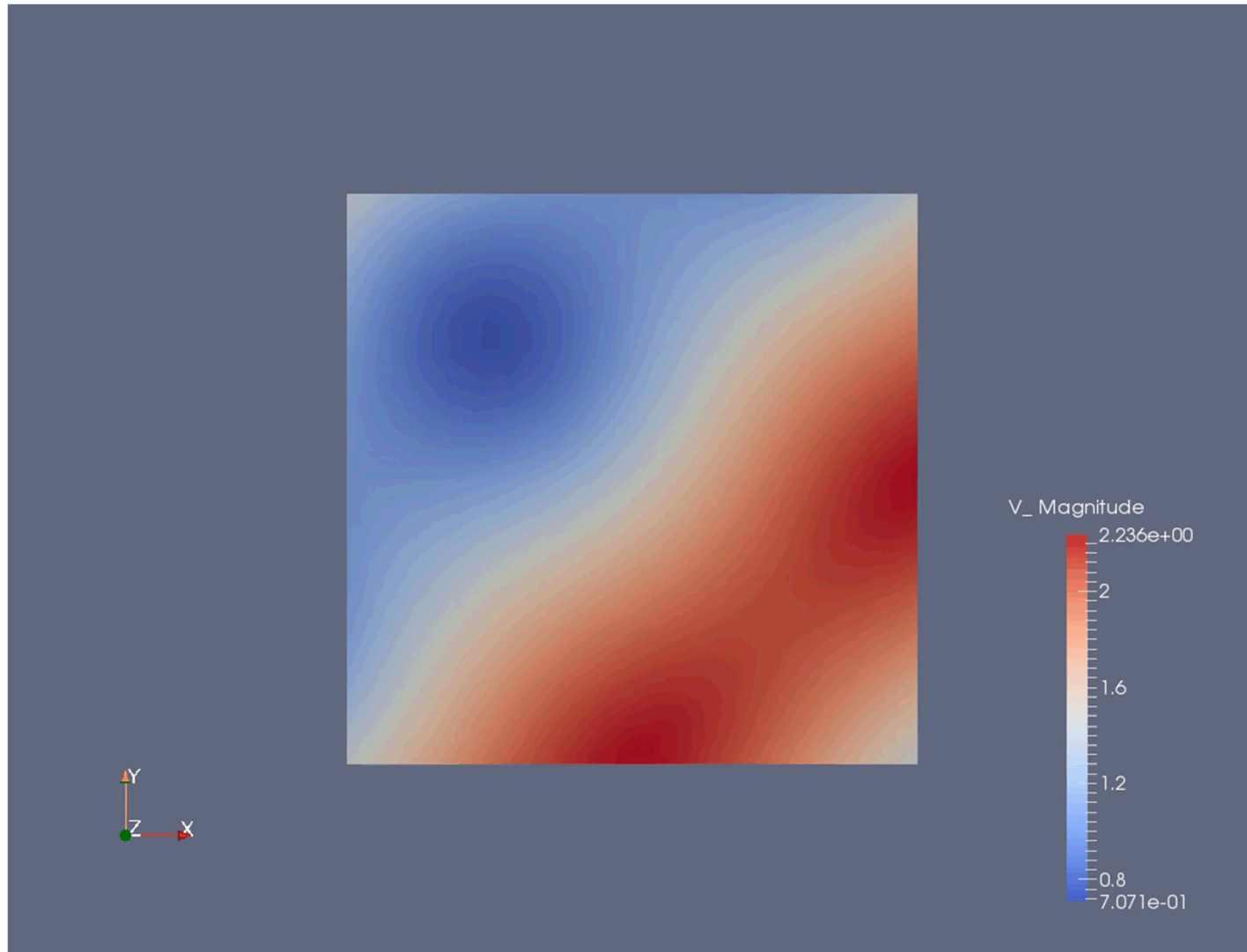


$$\nabla \cdot \boldsymbol{\sigma} \rightarrow - \int_{\Omega} \nabla \boldsymbol{w} : \boldsymbol{\sigma} \, dx + \sum_{k \in \mathcal{T}_h} \int_{\Gamma_0} \boldsymbol{w} \cdot \hat{\boldsymbol{\sigma}} \cdot \boldsymbol{n} \, ds$$

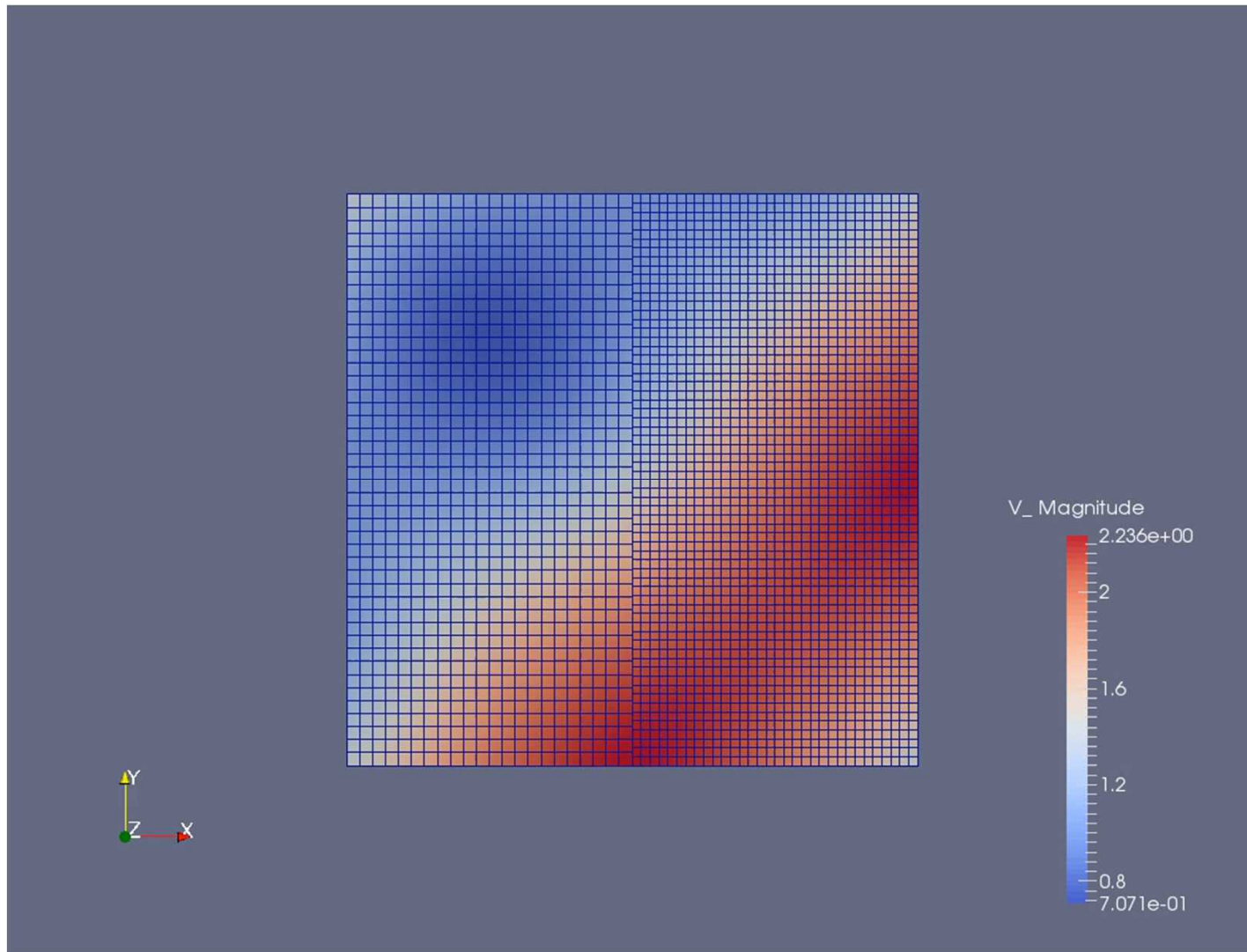
$$\sum_{k \in \mathcal{T}_h} \int_{\Gamma_0} \boldsymbol{w} \cdot \hat{\boldsymbol{\sigma}} \cdot \boldsymbol{n} \, ds = \int_{\Gamma_0} \{ \hat{\boldsymbol{\sigma}} \} \cdot \llbracket \boldsymbol{w} \rrbracket \, ds$$

$$\{ \hat{\boldsymbol{\sigma}} \} = \{ \boldsymbol{\sigma} \} - \alpha(\llbracket \boldsymbol{u}_h \rrbracket)$$

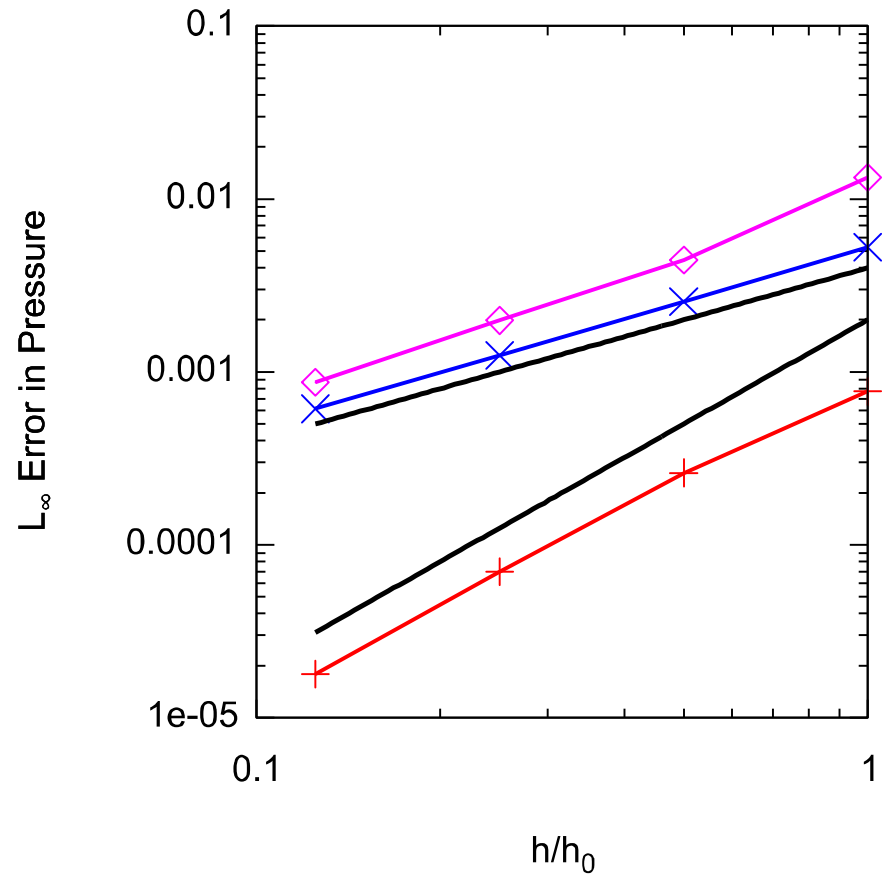
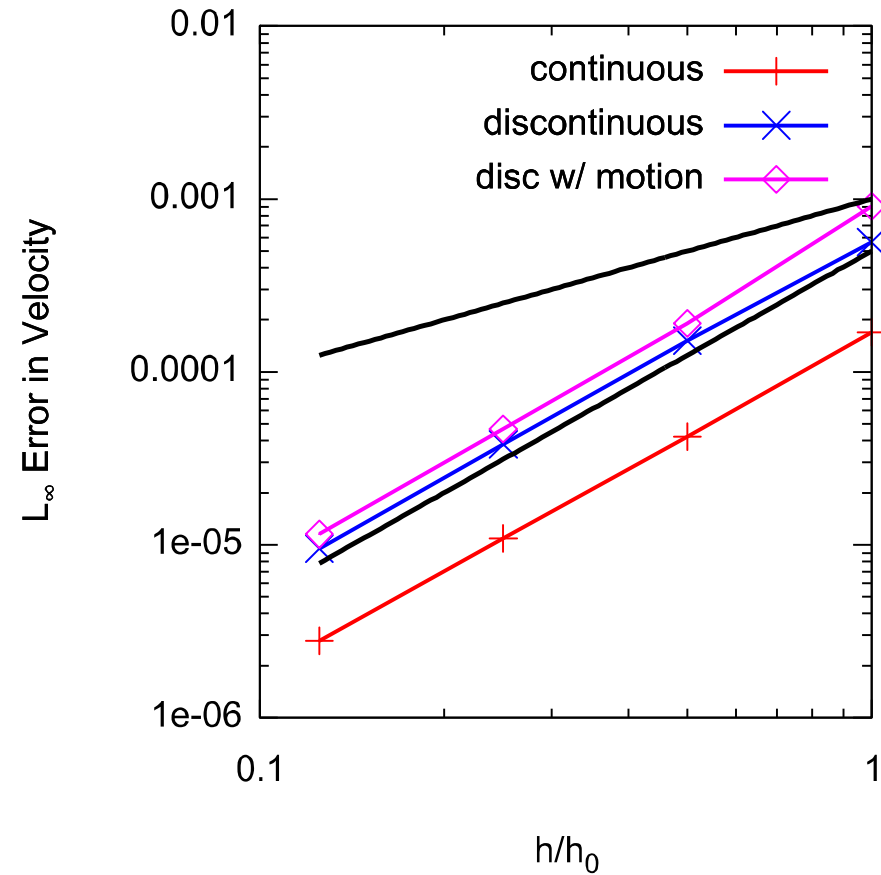
Taylor Vortex Verification



Taylor Vortex Verification



Taylor Vortex Verification



Conclusions

- resonance
 - Poiseuille
 - Couette
- rectified motion
- dynamic model
- ALE simulations
 - modes
 - amplitude limited
- sliding mesh scheme

