

# Mixing-controlled reactive transport at the pore scale and its impact on flow field and upscaling of reactive transport



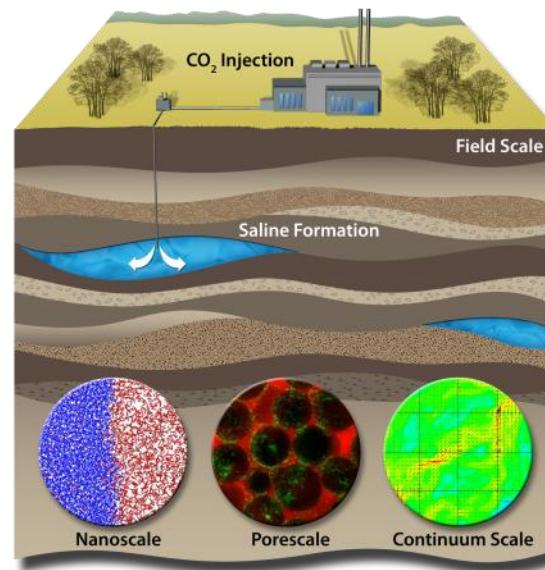
Hongkyu Yoon

August 20, 2015

Collaborators:

Thomas Dewers (SNL)

Jon Major, Peter Eichhubl (UT)



Sandia  
National  
Laboratories

*Exceptional  
service  
in the  
national  
interest*

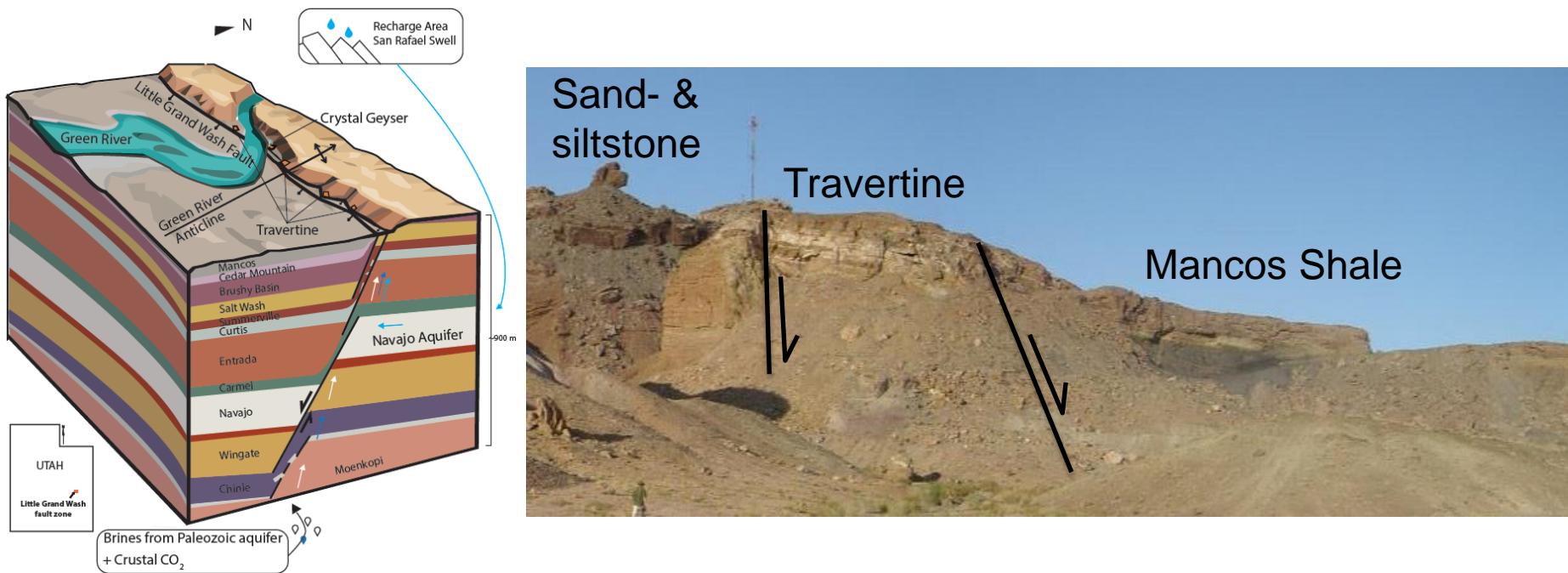
**Acknowledgment:** This work is supported as part of the Center for Frontiers of Subsurface Energy Security, an Energy Frontier Research Center funded by the U.S. Department of Energy, Office of Science, Office of Basic Energy Sciences under Award Number DE-SC0001114.



Sandia National Laboratories is a multi-program laboratory managed and operated by Sandia Corporation, a wholly owned subsidiary of Lockheed Martin Corporation, for the U.S. Department of Energy's National Nuclear Security Administration under contract DE-AC04-94AL85000.

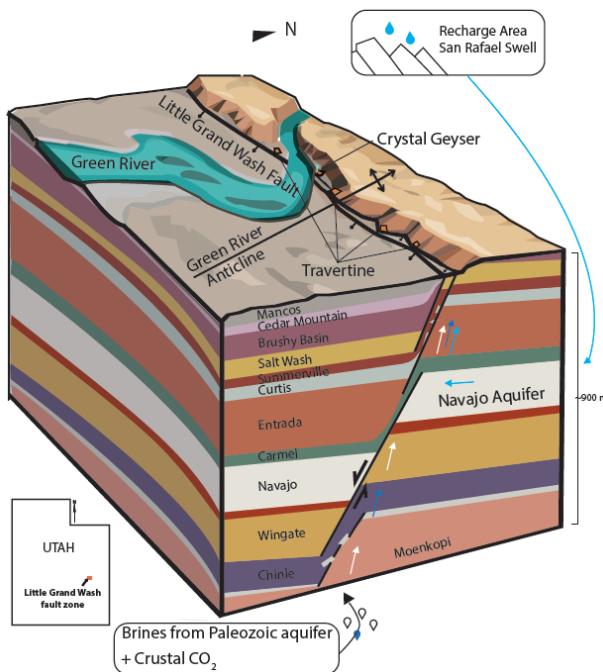
# Little Grand Wash Fault, Crystal Geyser, Utah

- Observations along the surface exposure of the Grand Wash fault indicate alteration zones of 10-50 m width with spacing on the order of 100 m
- Locations of conduits controlled by fault-segment intersections and topography
- Sandstone permeability reduced by 3 to 4 orders of magnitude in alteration zones by carbonate cementation

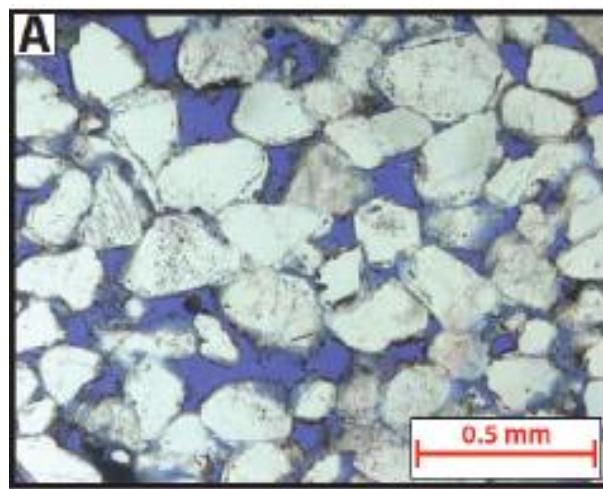


# Little Grand Wash Fault, Crystal Geyser, Utah

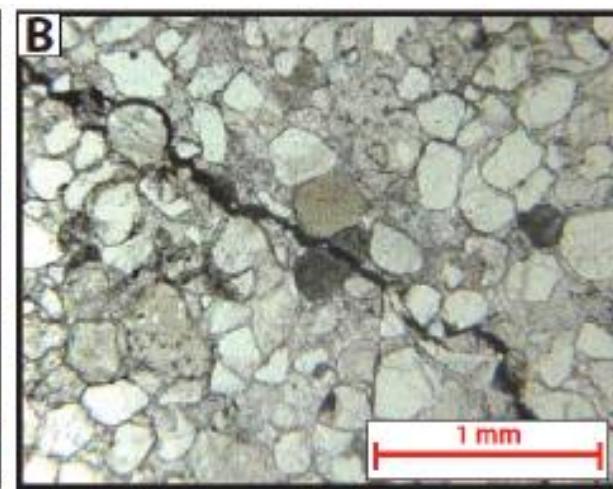
- Observations along the surface exposure of the Grand Wash fault indicate alteration zones of 10-50 m width with spacing on the order of 100 m
- Locations of conduits controlled by fault-segment intersections and/or topography
- Sandstone permeability reduced by 3 to 4 orders of magnitude in alteration zones by carbonate cementation



Far from fault



Near fault



U.S. DEPARTMENT OF  
**ENERGY**

Office of  
Science



Center for Frontiers of Subsurface Energy Security

THE UNIVERSITY OF  
**TEXAS**  
AT AUSTIN

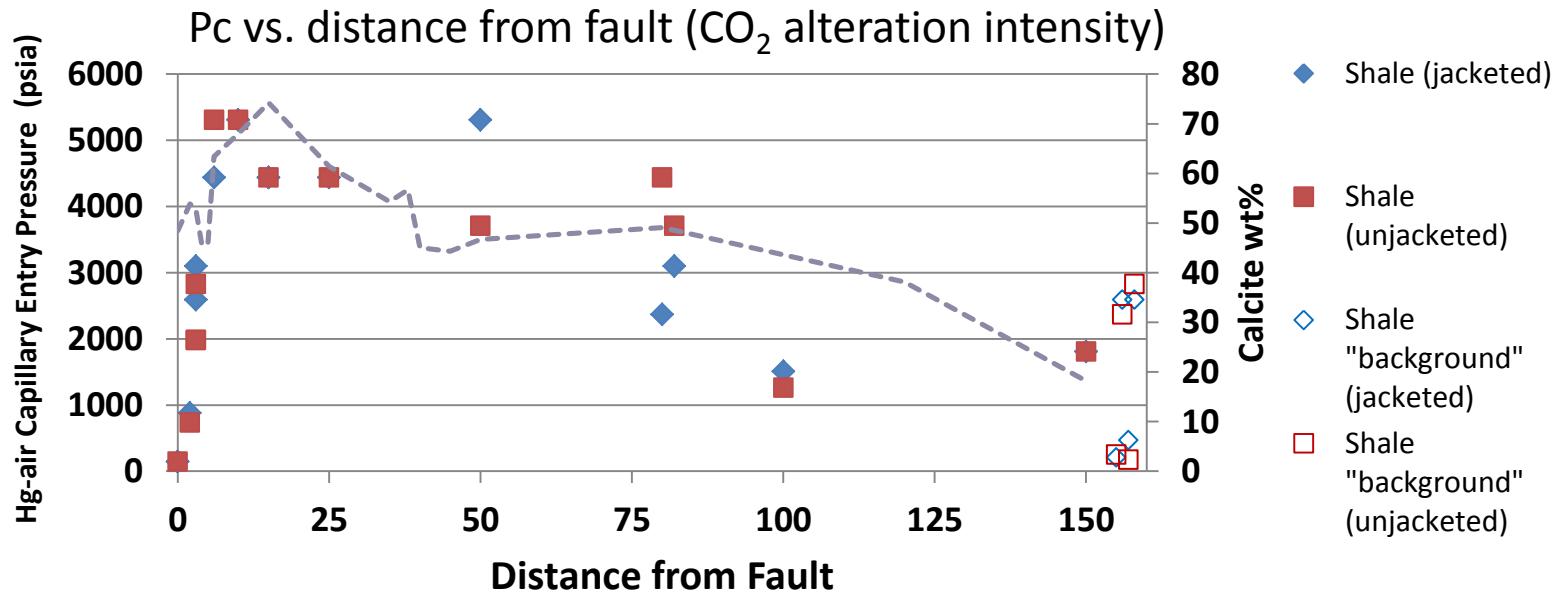


**Sandia**  
National  
Laboratories

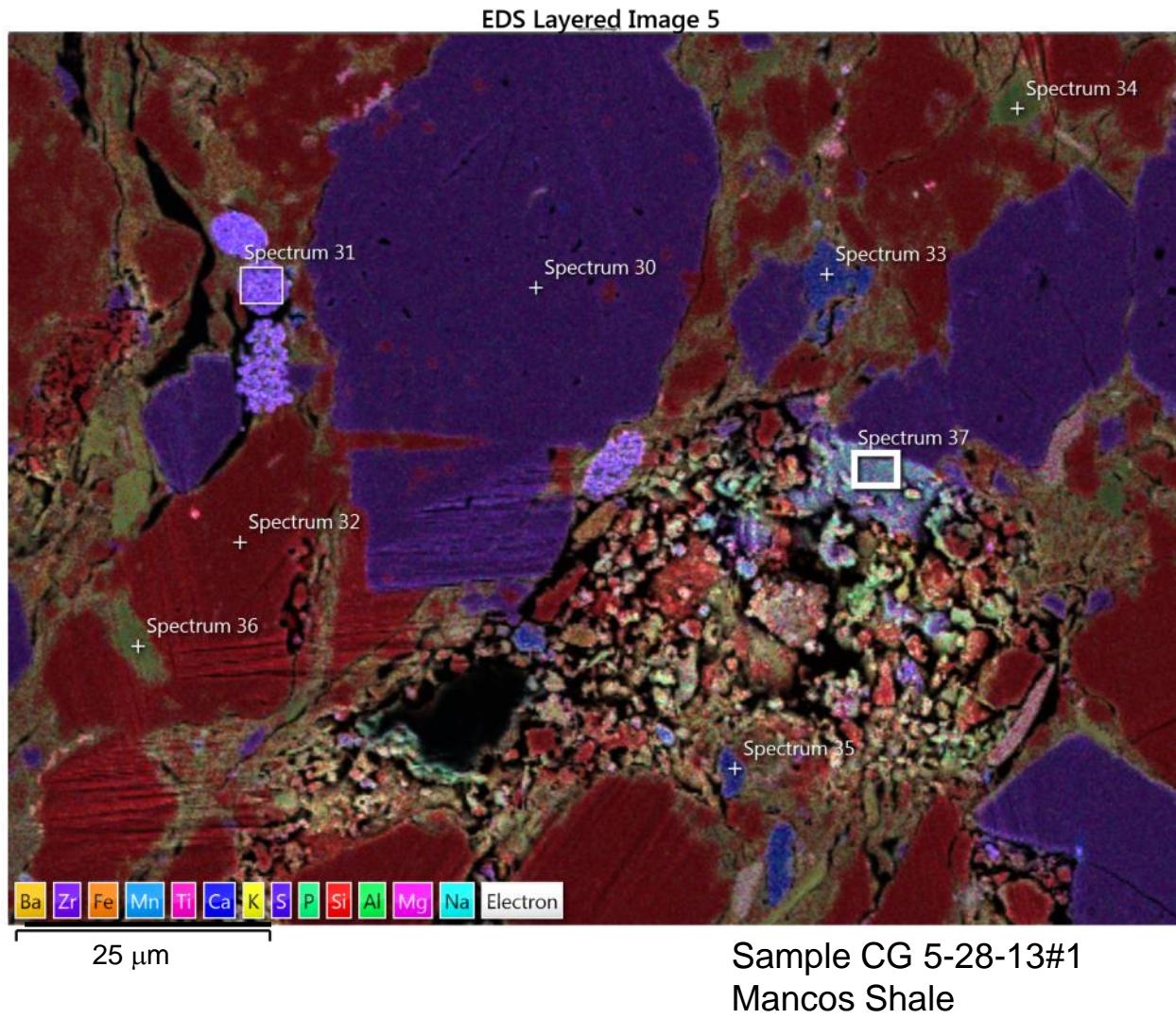
# Natural CO<sub>2</sub> alteration and shale seal capacity



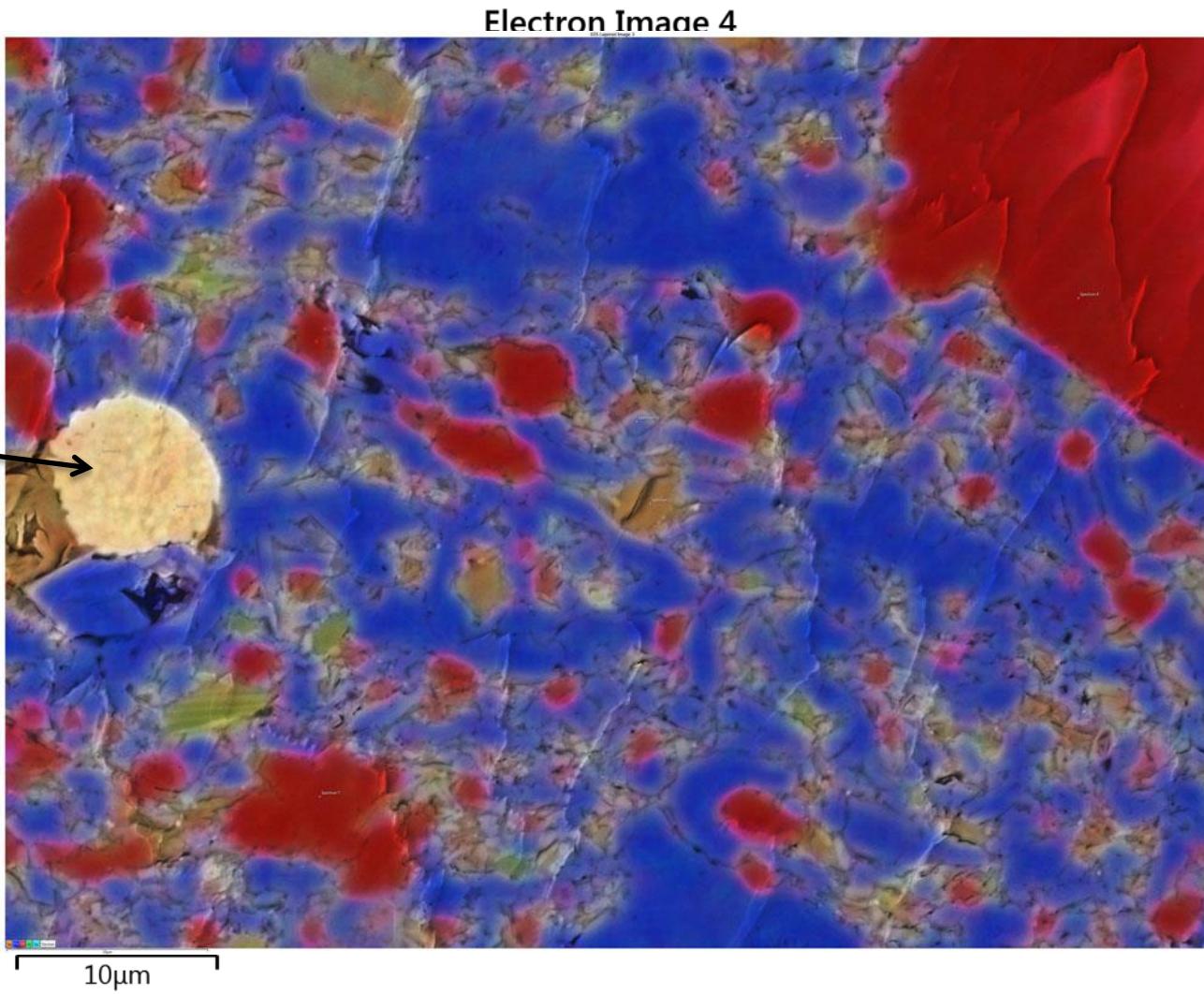
## Mancos Shale Transect



# SEM images of unaltered shale (< 10 wt% carbonate)

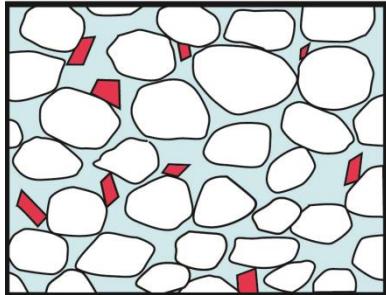


# SEM images of CO<sub>2</sub>-altered shale (~60 wt% carbonate)

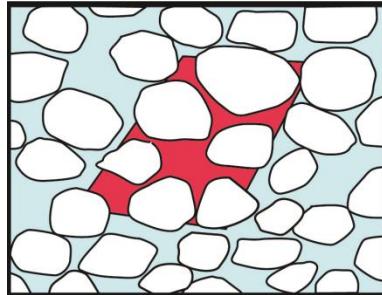


# Conceptual Model of Cementation Patterns

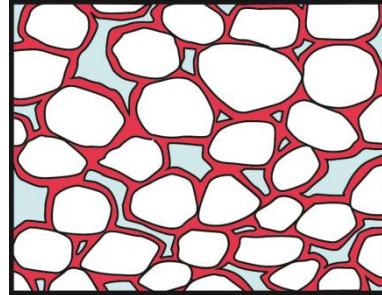
## Thin-Section Scale Spatial Distribution



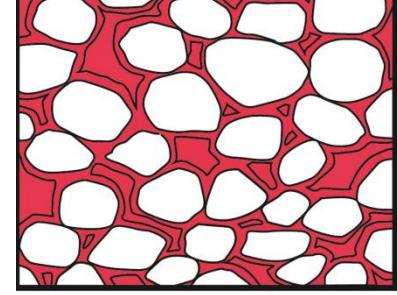
Disseminated



Poikilotopic

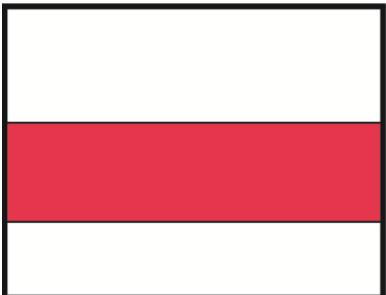


Circumgranular

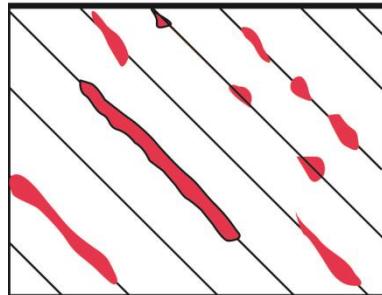


Pore filling

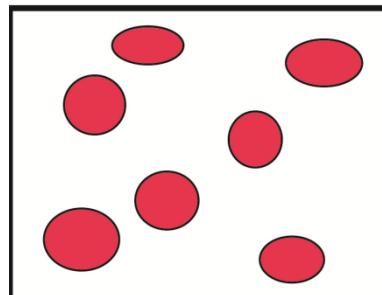
## Lithofacies Scale Spatial Distribution



Cemented  
Layers



Textually  
Selective  
Concretions



Non-Textually  
Selective  
Concretions



Equal  
Distribution

Peter Mozley (NMT), Unpublished

# Reactive Transport Modeling Framework

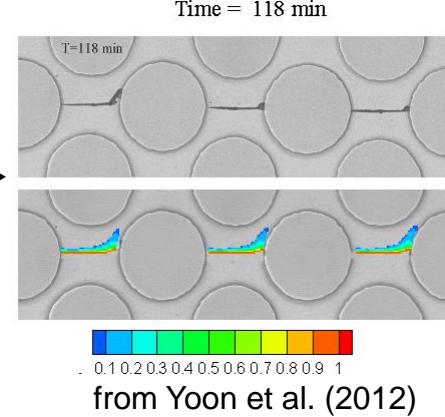
- Pore scale reactive transport model can provide a tool to develop functional forms of reaction rates for  $\text{CaCO}_3$  precipitation and dissolution as a function of system parameters based on fundamental principles without model assumptions
- Pore-scale modeling results will be able to develop the response functional forms of permeability, porosity, and surface area changes as a function of pore structures, volume, Pe, Da number, mineral types, and influent solution chemistry
- Response surface results can be used as input for continuum scale reactive transport modeling

## System parameters

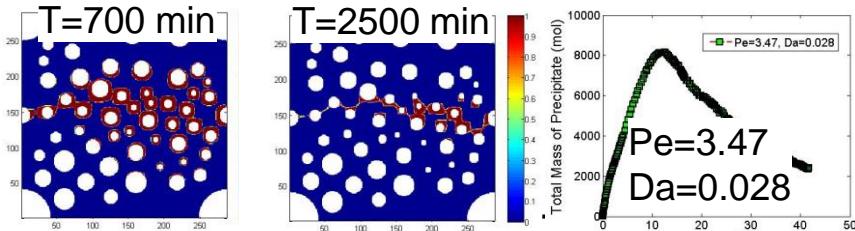
Flow rate, Mineral type



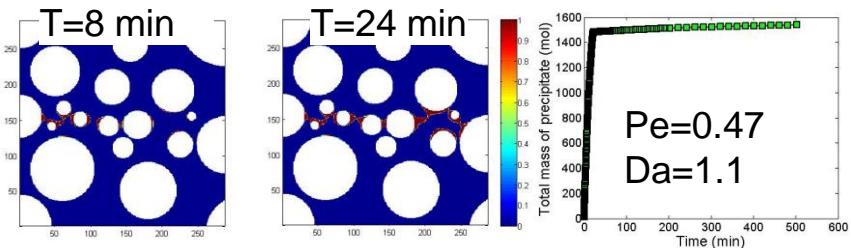
Chemistry (e.g., pH &  $\text{CO}_3$  conc)



Not far from equilibrium ( $\log Q = \sim 0.7$ )

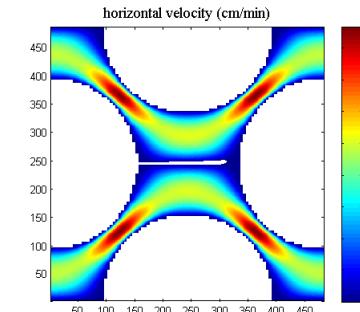


Far from equilibrium ( $\log Q = \sim 3.7$ )



# Pore Scale Model Framework

Lattice Boltzmann Method:  
Velocity field ( $u$ ) at pore scale



Velocity at 1 micron resolution

Finite Volume Method: Reactive transport at pore scale

$\Delta t$

$\Psi_j = C_j + \sum_{i=1}^{N_{eq}} v_{ji} C_i$  Chemical equilibrium in bulk fluid (e.g.,  $\text{H}^+$ ,  $\text{HCO}_3^-$ , ...)  
Extended Debye-Hückel Equation for activity coefficients

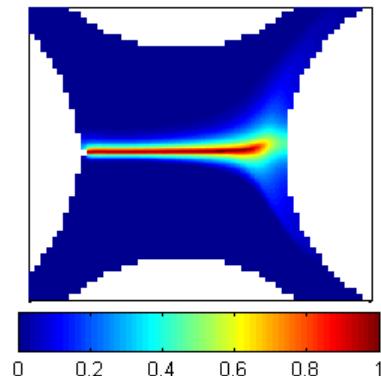
$$D \frac{\partial \Psi_j}{\partial \mathbf{n}} = -I_m \quad \text{on reactive surface}$$

$$I_m = k_{cc} ([\Omega]^n - 1)^m \quad \Omega = \frac{Q_{cc}}{K_{sp}} \text{ or } \ln \left( \frac{Q_{cc}}{K_{sp}} \right)$$

Update of  $\text{CaCO}_3$  volumetric content ( $V_m$ )

$$\frac{\partial V_m}{\partial t} = \overline{V_m} s_m k_{cc} \left( \left[ \frac{a_{\text{Ca}^{2+}} a_{\text{CO}_3^{2-}}}{K_{sp}} \right]^n - 1 \right)^m$$

Yoon et al. (WRR, 2012)



Mineral phase  
volumetric content

# Functional Relationships based on Pore Scale Simulations

- Pe & Da numbers

$$Pe(uL/D) = 0.08, 0.8, 8$$

$$Da(kL/(K_{sp}^{0.5} \times D)) = 0.002, 0.02, 0.1$$

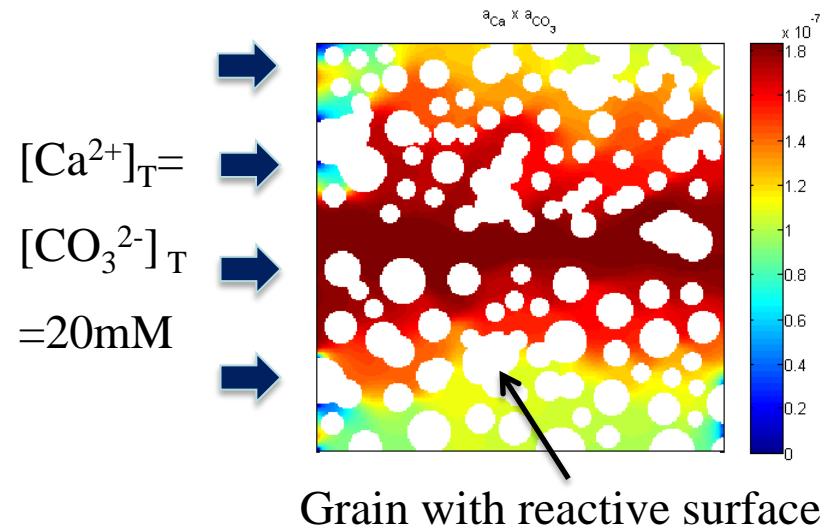
$$(K_{sp, \text{calcite}} = 3.3 \times 10^{-9} \text{ M}^2)$$

- Chemical speciation

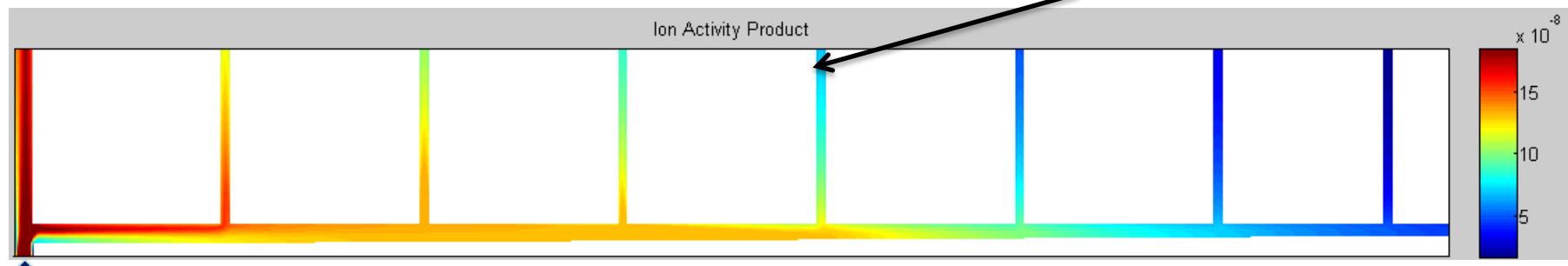
Speciation:  $\text{Ca}^{2+}$ ,  $\text{H}^+$ ,  $\text{CO}_3^{2-}$ ,  $\text{HCO}_3^-$ ,  $\text{H}_2\text{CO}_3$

No speciation:  $\text{Ca}^{2+}$ ,  $\text{CO}_3^{2-}$

- Pore structures



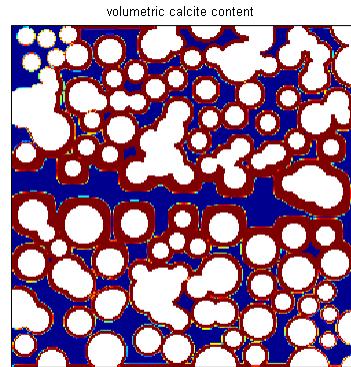
fracture network with varying apertures and patterns



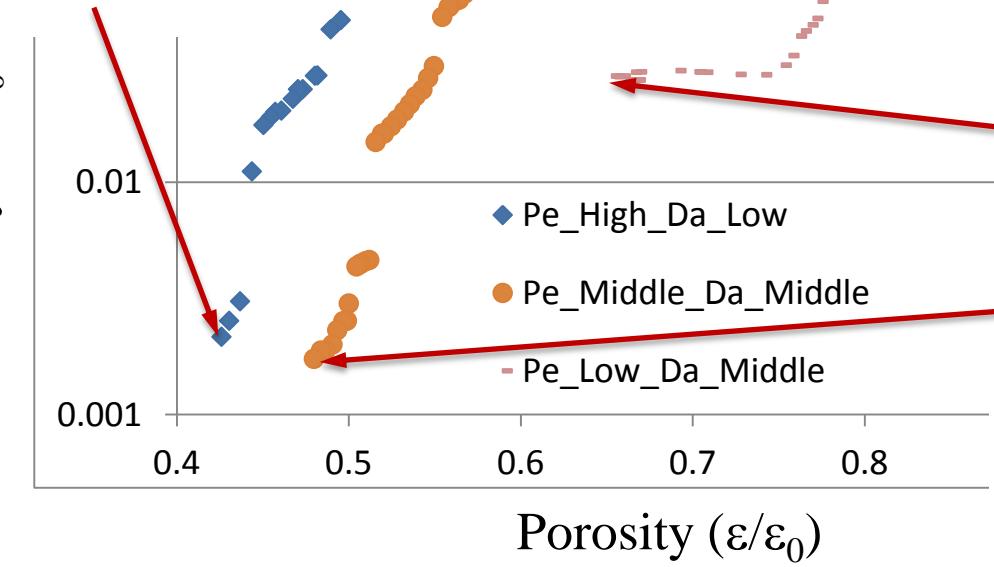
Yoon et al. (in prep)

# Permeability-Porosity Relationships

High Pe; Low Da

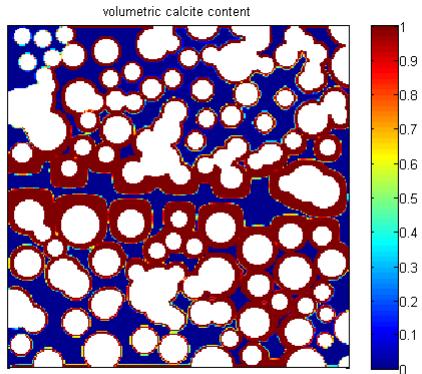
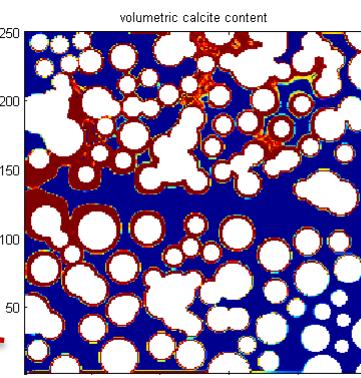


Permeability ( $k/k_0$ )



Carbonate speciation

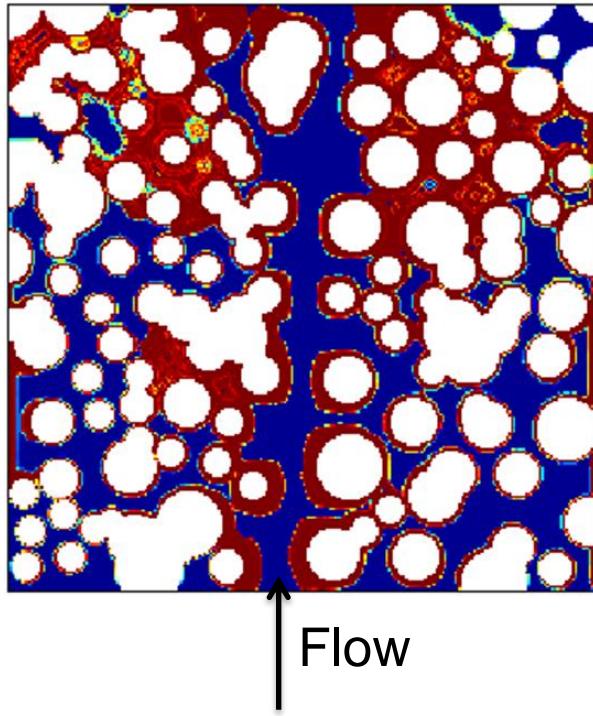
Low Pe;  
Medium Da



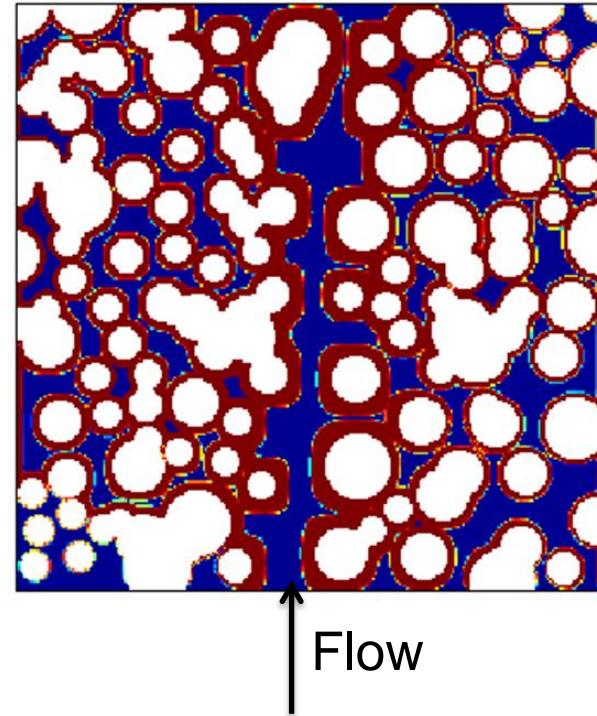
Medium Pe; Medium Da

# Direction of precipitation and pore clogging

Medium Pe & High Da



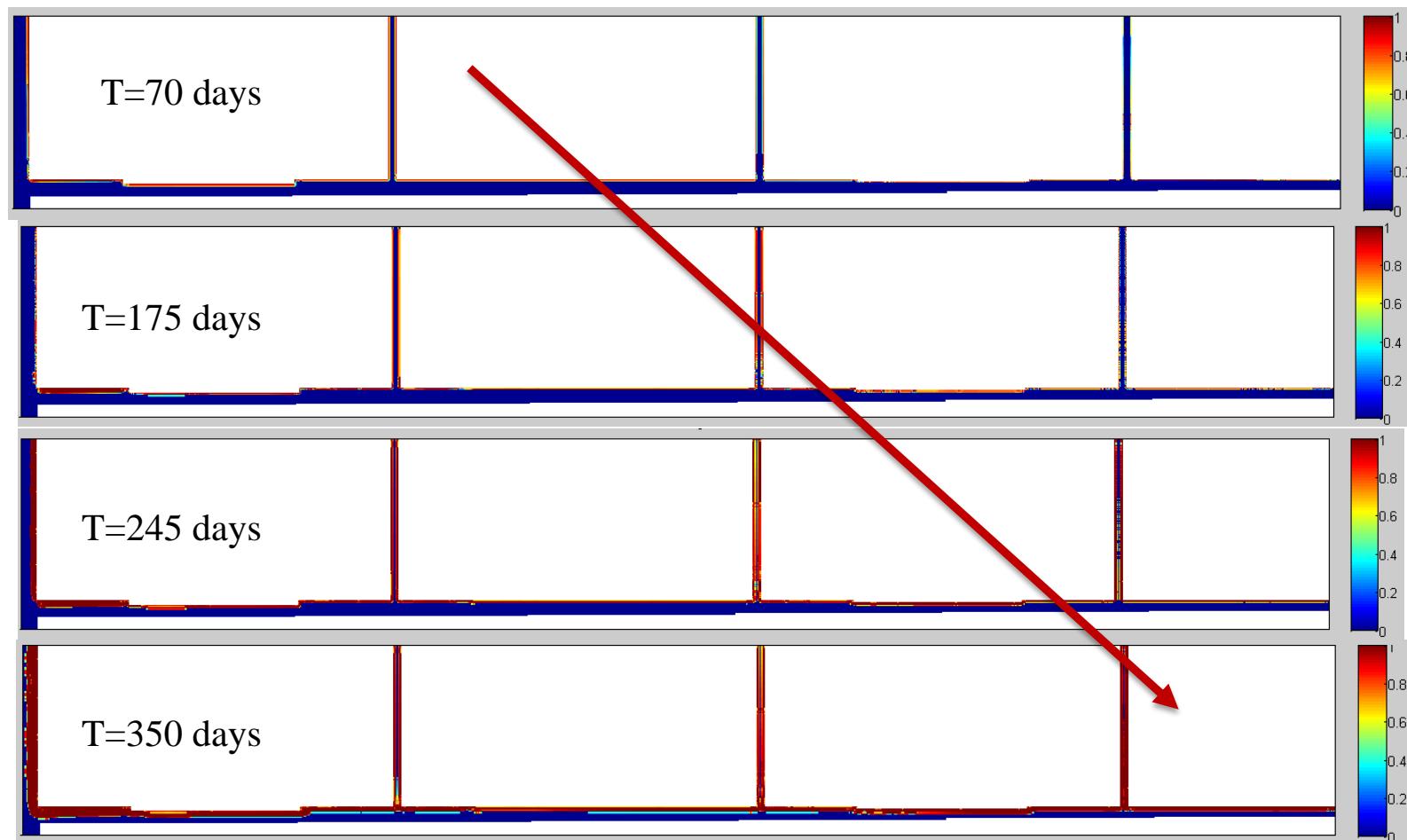
High Pe & Low Da



- Simulation results under two different Pe and Da regimes show fast precipitation from the top – this example show multiple possible pathways for field observations

# High Pe & High Da

CaCO<sub>3</sub> volumetric content



$$[\text{Ca}^{2+}]_T = [\text{CO}_3^{2-}]_T = 20 \text{ mM}$$

- Precipitation occurs near the main fault and clogging of fracture networks moves away from the main fault conduit as observed in the outcrop

# Summary

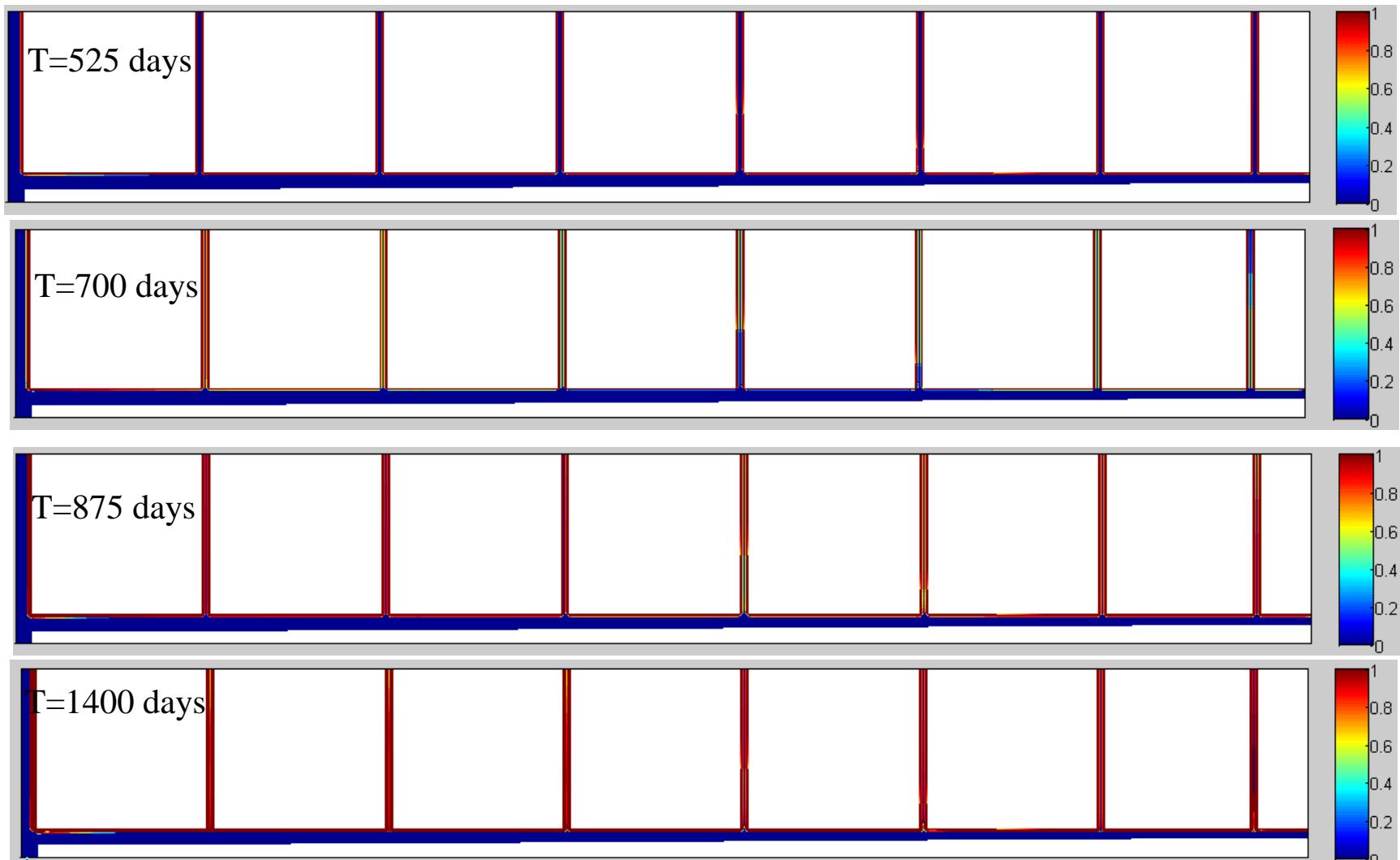
- Fault-controlled CO<sub>2</sub> leakage conduits are sites of preferred carbonate pore and fracture cementation
- Carbonate cementations significantly increases caprock sealing capacity
- Vigorously tested pore-scale model was used to develop a permeability and porosity ( $k-\varepsilon$ ) relationship for continuum-scale model
- Pore scale model was able to qualitatively capture pore clogging patterns in a simple fracture network model mimicking the Little Grand Wash fault
- An adaptive strategy to couple pore- and continuum scale will be tested against cement precipitation patterns observed in the Little Grand Wash fault
- Algorithms developed in this work will be implemented into a continuum scale reactive transport model

# Questions?

# Back-Up Slides

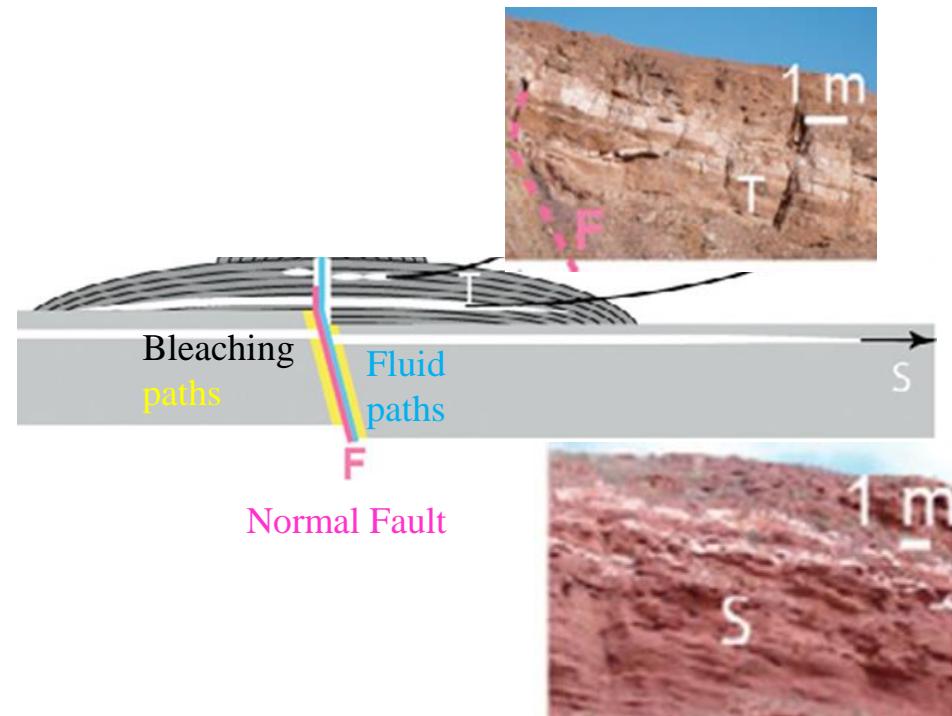
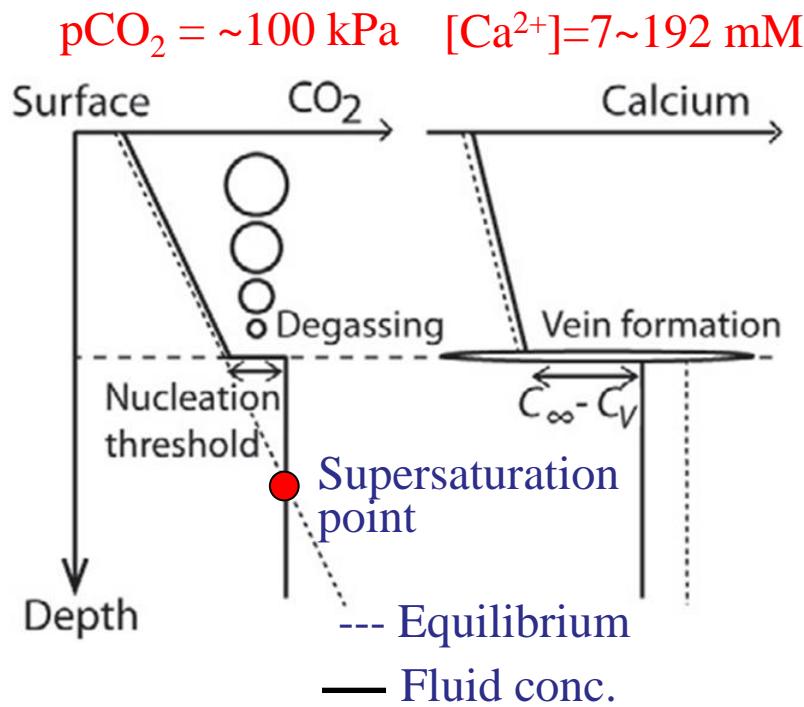
# High Pe & Medium Da

$\text{CaCO}_3$  volumetric content



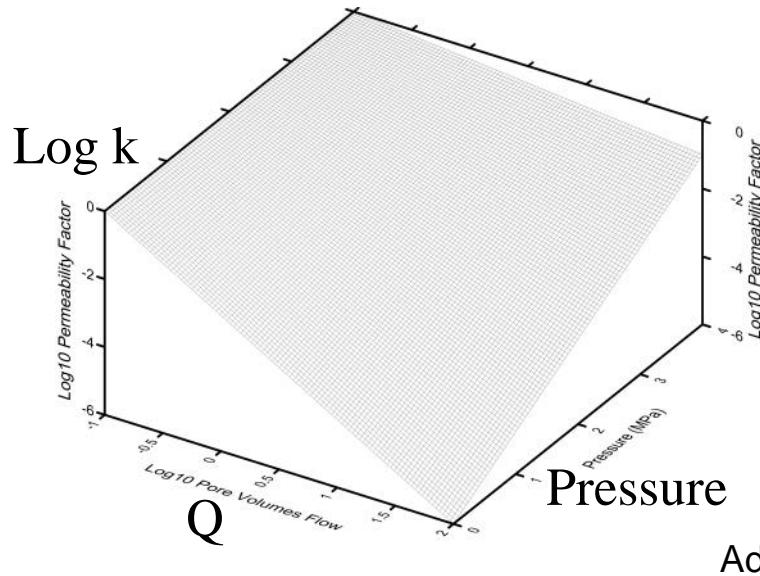
# Simple chemistry & mineralogy

- Spring water: Low temperature and Mg concentrations; high concentrations of dissolved  $\text{CO}_2$  ( $\text{pCO}_2 = \sim 100 \text{ kPa}$ )
- Aragonite precipitation indicates large, sudden increase of supersaturation with respect to  $\text{CaCO}_3$  in solution  $\rightarrow$  high  $\text{CO}_2$  degassing rate
- Both calcite and aragonite are present



# Continuum Scale Reactive Transport Modeling

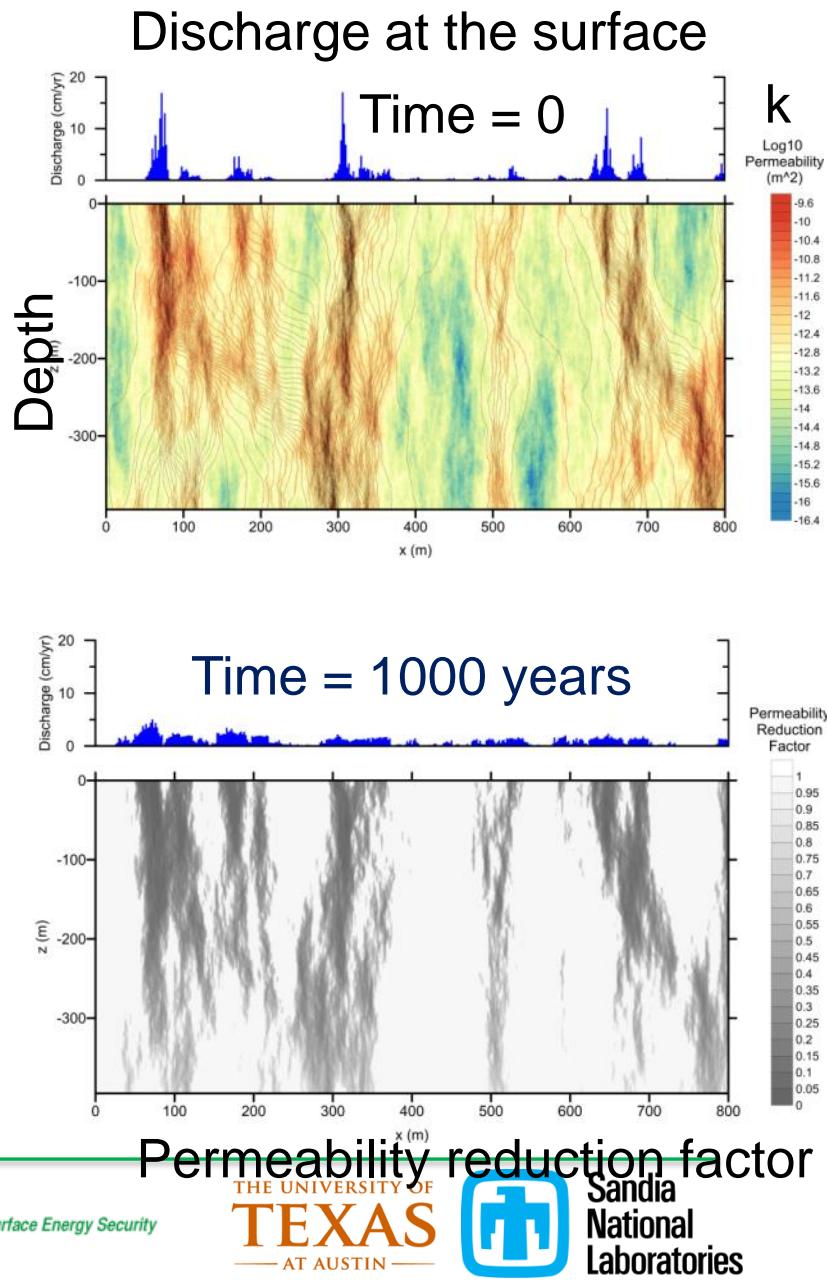
- Simplified, two-dimensional response surface
- Permeability reduction due to  $\text{CaCO}_3$  precipitation is a function of cumulative pore volume ( $Q$ ) of groundwater and fluid pressure ( $P$ )
- Fluid pressure is taken as a gross proxy for chemical conditions in which higher  $\text{CaCO}_3$  solubility is associated with higher fluid pressure (greater depth)



Adapted from Mehmani et al. (2012)

# Crystal Geyser Site: Grand Wash Fault Modeling

- Unconditional geostatistical simulation
- Initial simulated steady-state flow pattern is qualitatively similar to the spacing of seeps along the Grand Wash fault (~100's of m between locations of groundwater discharge)
- Transient flow simulation includes explicit updating of permeability ( $k$ ) at each time step using the response surface (FEHM)
- $k$  is reduced by several orders of magnitude by calcite precipitation, primarily in the shallower high-flow channels
- Evolution of the flow field results in more dispersed groundwater discharge at the surface



# Functional relationships based on Pore Scale Simulations

- Vigorously tested pore-scale model can be used to develop a response function (or dimension reduction model) for continuum-scale permeability and porosity ( $k$ - $\varepsilon$ ) relationships
- $k$ - $\varepsilon$  and surface area- $\varepsilon$  relationships will be developed over a range of solution chemistry, chemical reaction, and pore structure configurations in addition to Pe and Da numbers

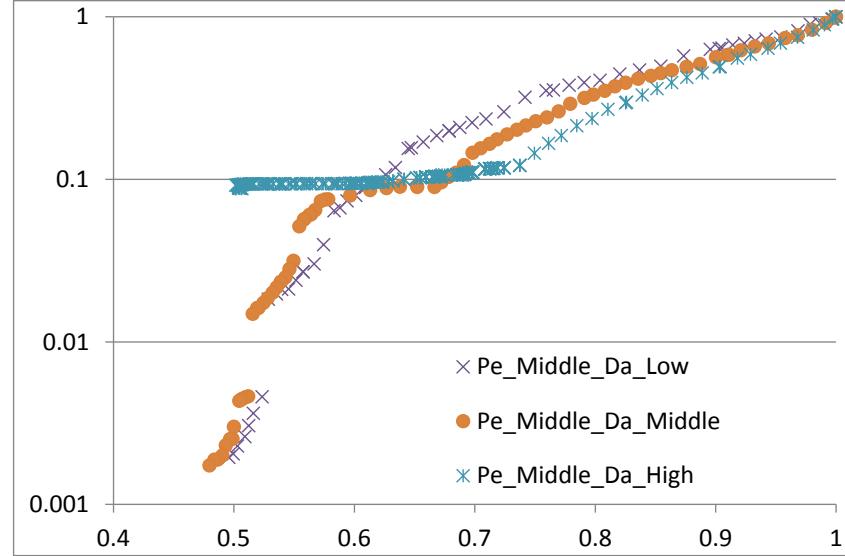
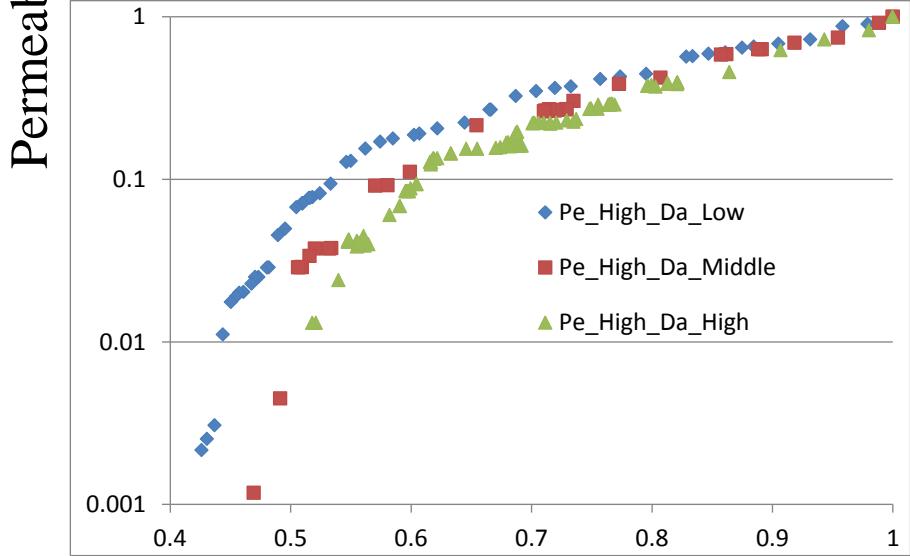
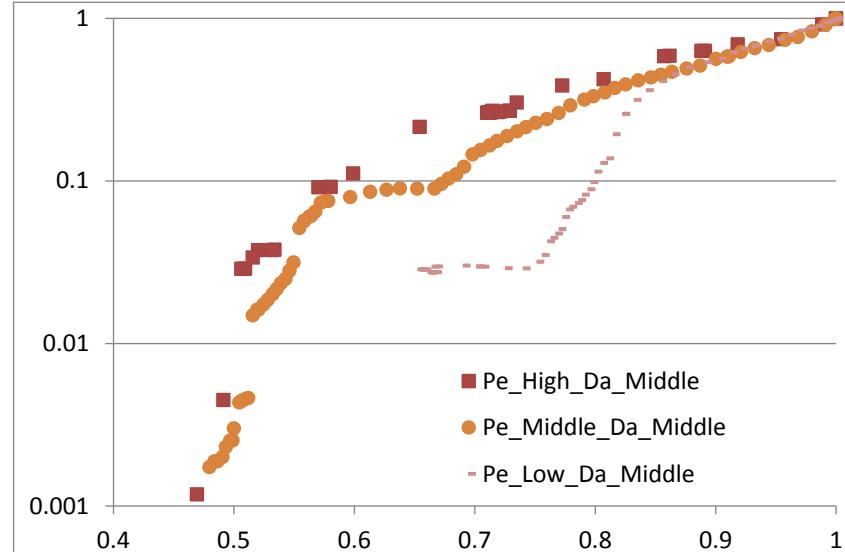
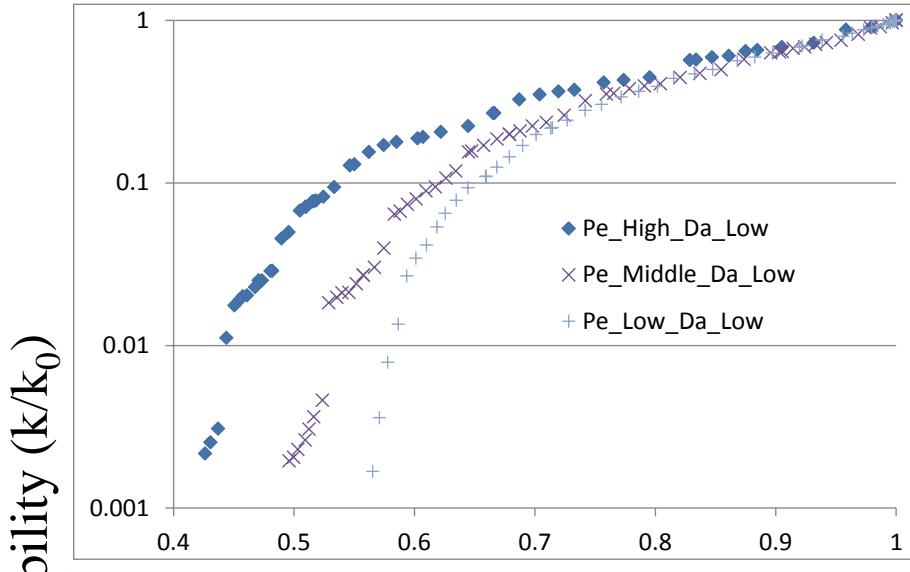
**Changes in porosity due to precipitation ~tortuosity and permeability by phenomenological power law relations**

$$\tau(\varphi) = \tau_0 \left( \frac{\varphi}{\varphi_0} \right)^n$$

$$k(\varphi) = k_0 \left( \frac{\varphi}{\varphi_0} \right)^n$$

$$a_{cc} = a_{cc}^0 \left( \frac{\varphi}{\varphi_0} \right)^{2/3}$$

# Permeability-Porosity Relationships



# Field Observations

