

# Modeling the Mechanical Behavior of Additively Manufactured 304L Stainless Steel

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1: Sandia National Laboratories

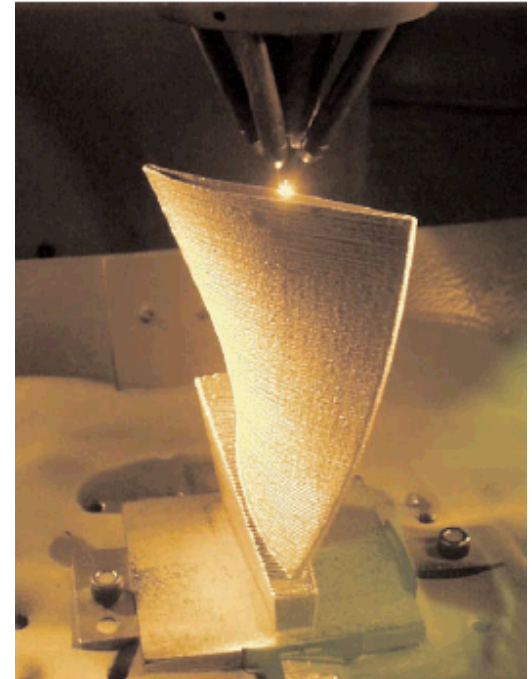
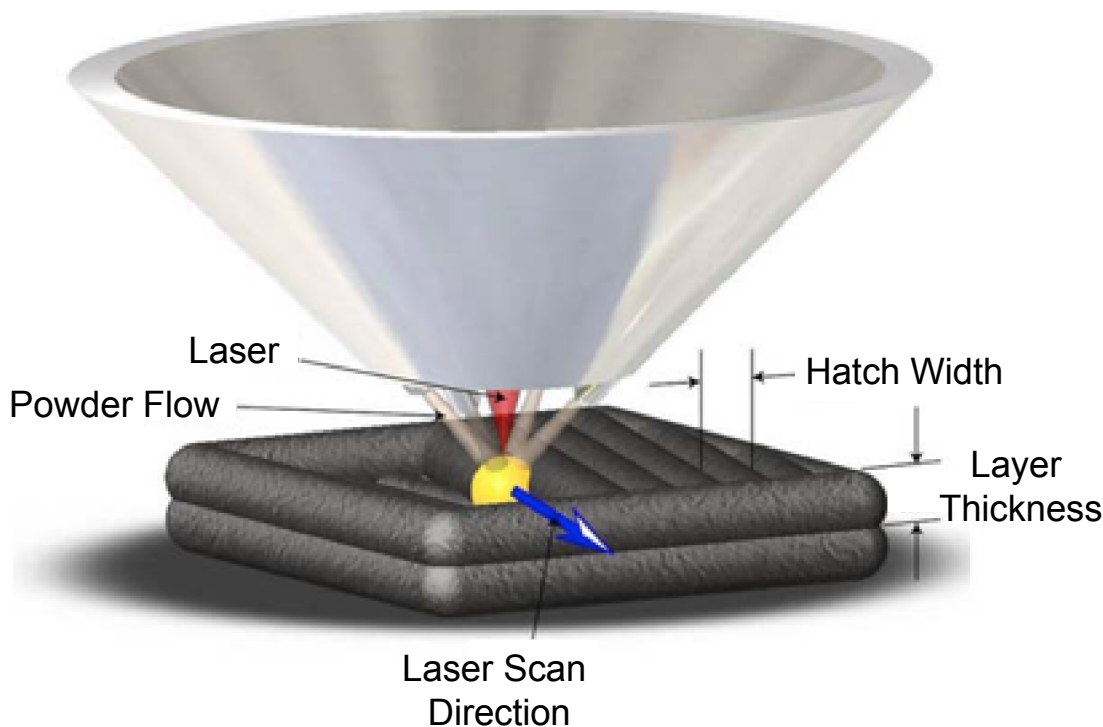
2: Los Alamos National Laboratories

3: Pennsylvania State University

- Introduction
- Experimental  
Characterization
- Simulations
  - Model Construction
  - Preliminary Results

# INTRODUCTION

# Laser Engineered Net Shaping (LENS™)

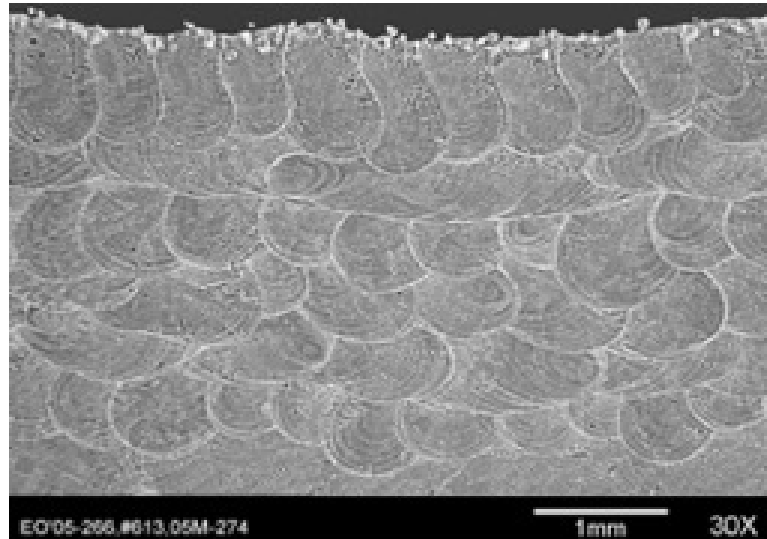


- Pros
  - Complex part geometries
  - Rapid design to production
- Cons
  - Speed
  - Finishing required
  - Open scientific questions



# Fundamental Questions

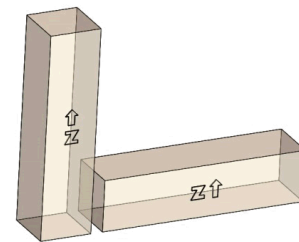
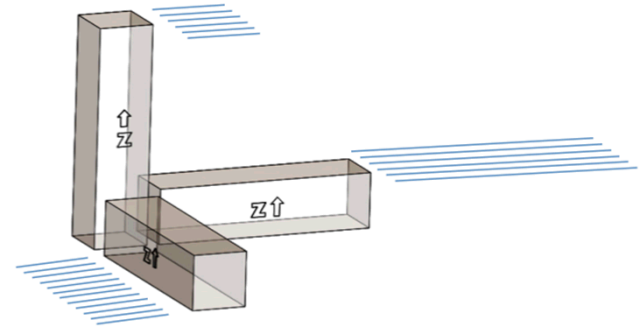
- How does the mechanical response of a LENS material compare to that of a wrought material.
  - What role does the exotic microstructure play?
  - Variability?



- How do we predict the response?
  - What level of sophistication do we need in our simulations?
  - Loss of 'scale separation'?

# Parameter Sensitivities

- Laser power
  - 3.8 kW, 2 kW, 0.5 kW
- Parallel Hatch vs. Cross Hatch
- As-Deposited vs. Annealed
- Anisotropy
  - X vs. Y vs. Z
- Center vs. Edge
- Strain Rate
  - $10^{-5} \text{ s}^{-1}$  to  $10^9 \text{ s}^{-1}$
- Temperature
  - 20 °C to 300 °C



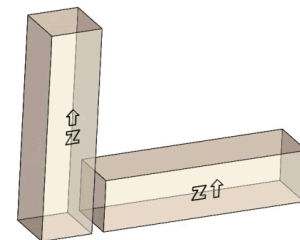
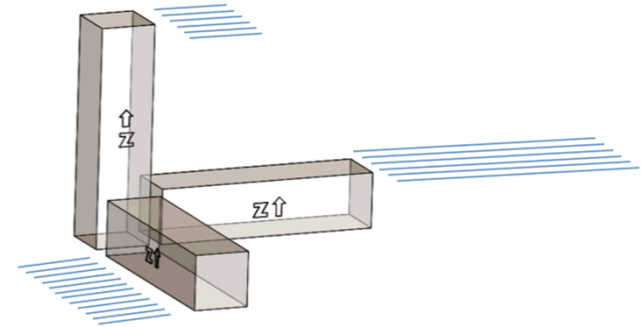
Sample Geometry



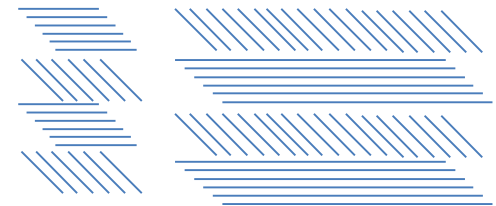
Schematic raster fill patterns

# Parameter Sensitivities

- Laser power
  - 3.8 kW, 2 kW, 0.5 kW
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- Anisotropy
  - X vs. Y vs. Z
- Center vs. Edge
- Strain Rate
  - $10^{-5} \text{ s}^{-1}$ ,  $10^{-3} \text{ s}^{-1}$ , to  $10^9 \text{ s}^{-1}$
- Temperature
  - 20 °C to 300 °C



Sample Geometry

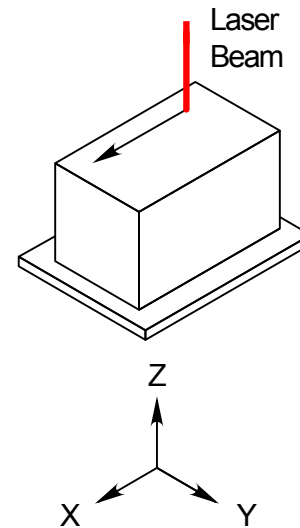
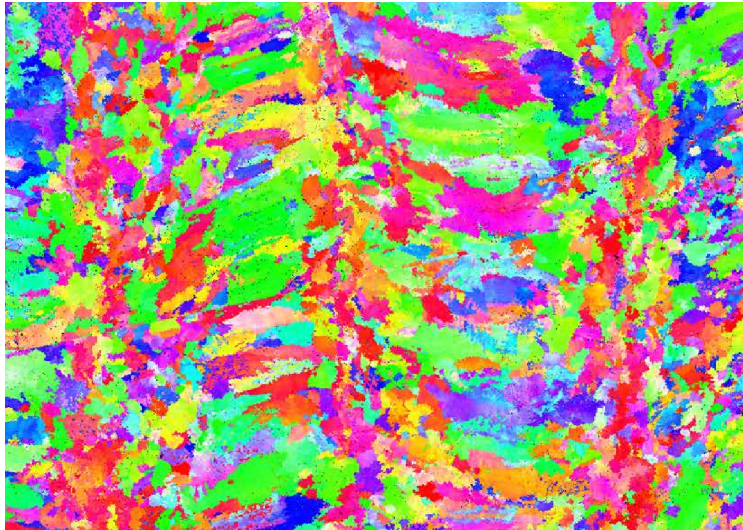


Schematic raster fill patterns

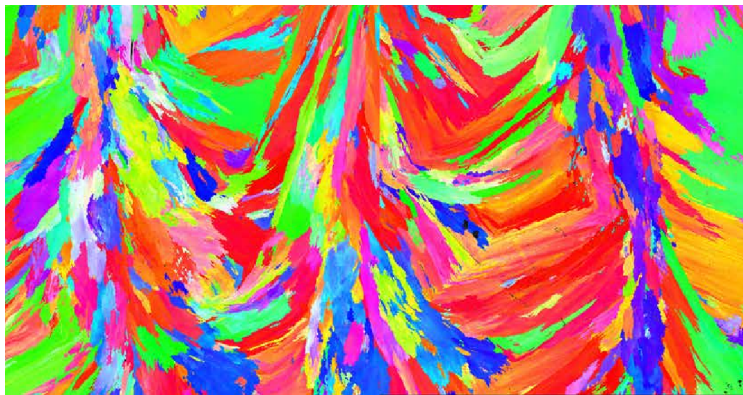
# EXPERIMENTS

# LENS Microstructure Orthographic Projections

Z-Plane (Z-direction)

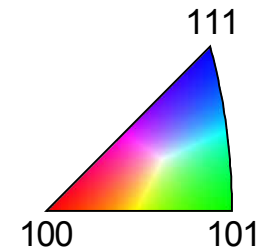
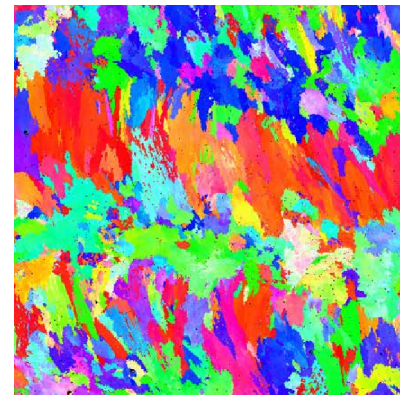


X-Plane (X-direction)



1.0 mm

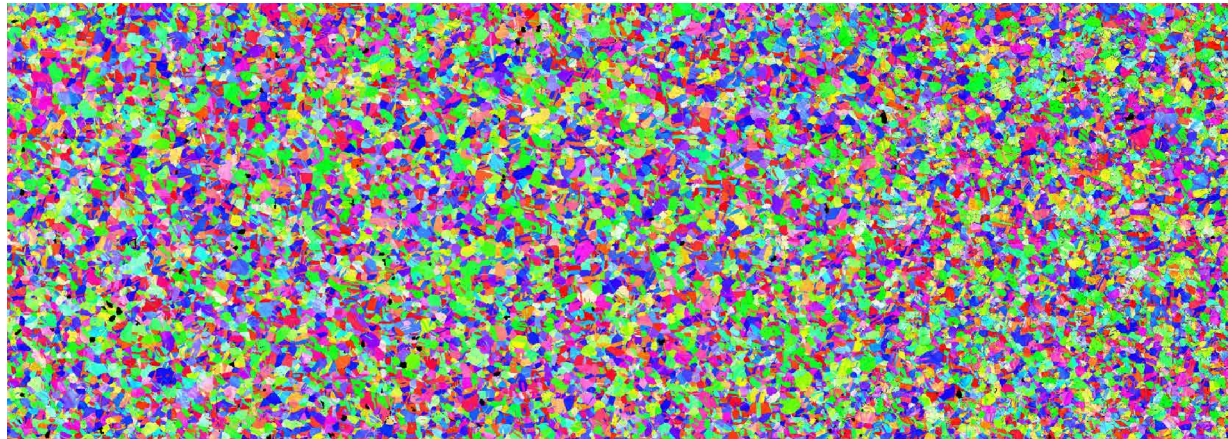
Y-Plane (Y-direction)



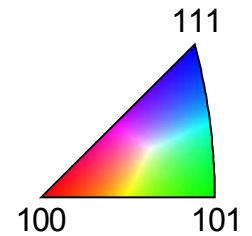


# Wrought vs. LENS Microstructure

Wrought

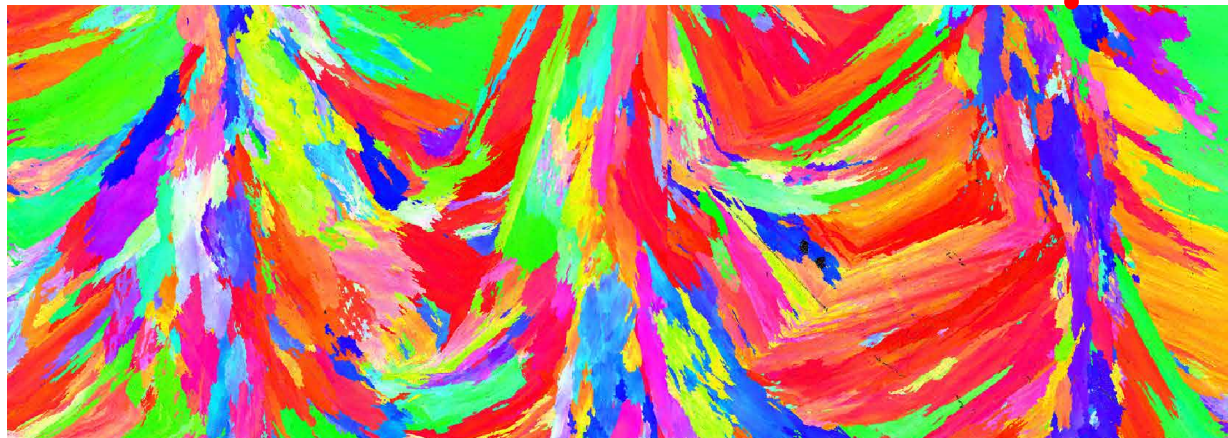


1.0 mm

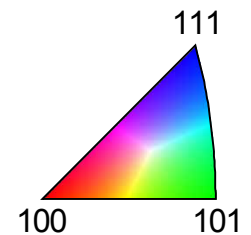


3.8 kW LENS

Laser Beam



1.0 mm

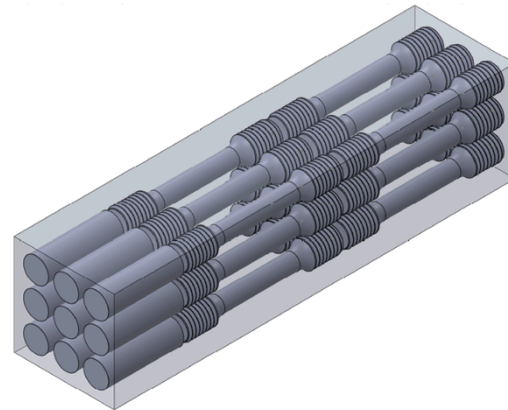
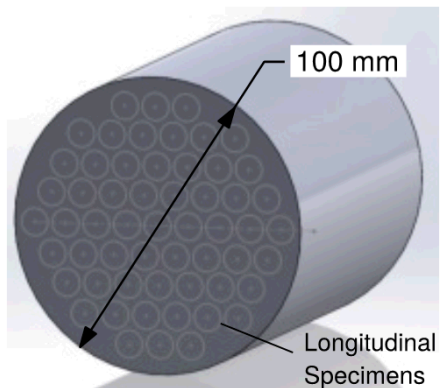
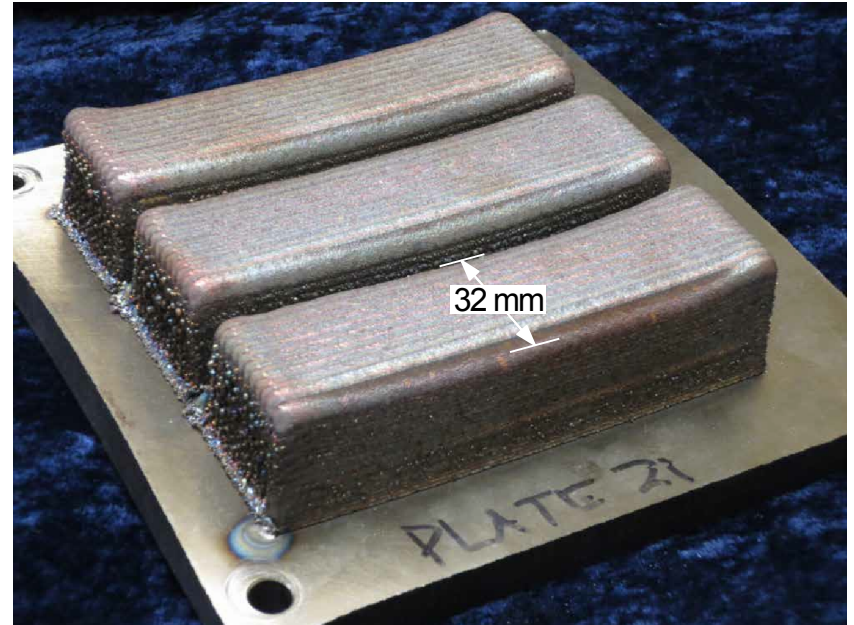


# Base Material

Wrought Bar

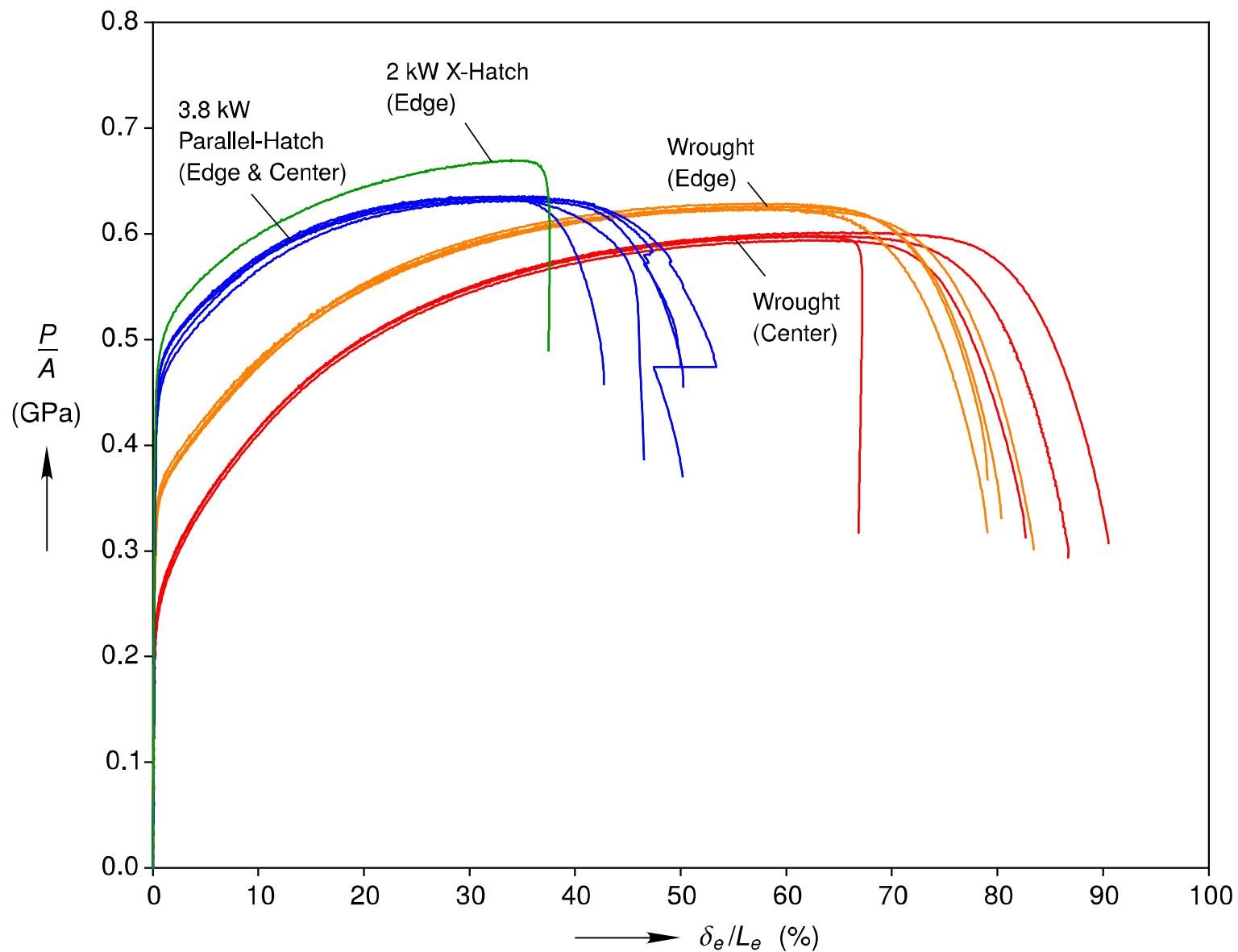


LENS Bars ("Twinkies")





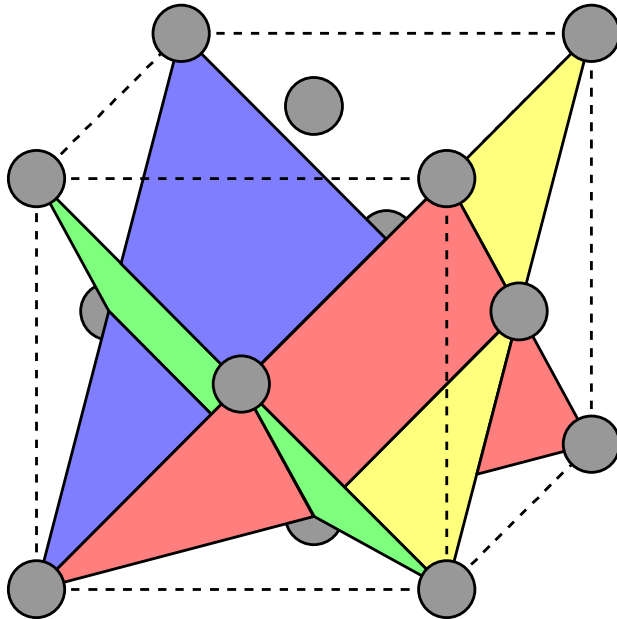
# Tensile Tests





# SIMULATIONS

# Crystal Plasticity Model



$$\tau^{\alpha} = \mathbf{n}^{\alpha} \cdot \boldsymbol{\sigma} \cdot \mathbf{m}^{\alpha}$$

$$\dot{\gamma}^{\alpha} = \dot{\gamma}_0 \left( \frac{\tau^{\alpha}}{g} \right)^{1/m} \text{sign}(\tau^{\alpha})$$

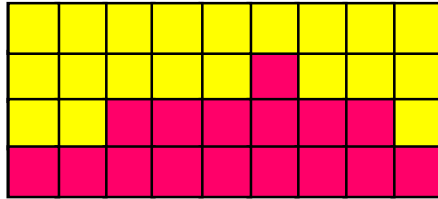
$$\gamma = \sum_{\alpha}^N |\gamma^{\alpha}| \quad (\text{sum over slip systems})$$

$$g = g_0 + (g_{s0} - g_0) \left[ 1 - \exp \left( -\frac{G_0 \gamma}{g_{s0} - g_0} \right) \right]$$

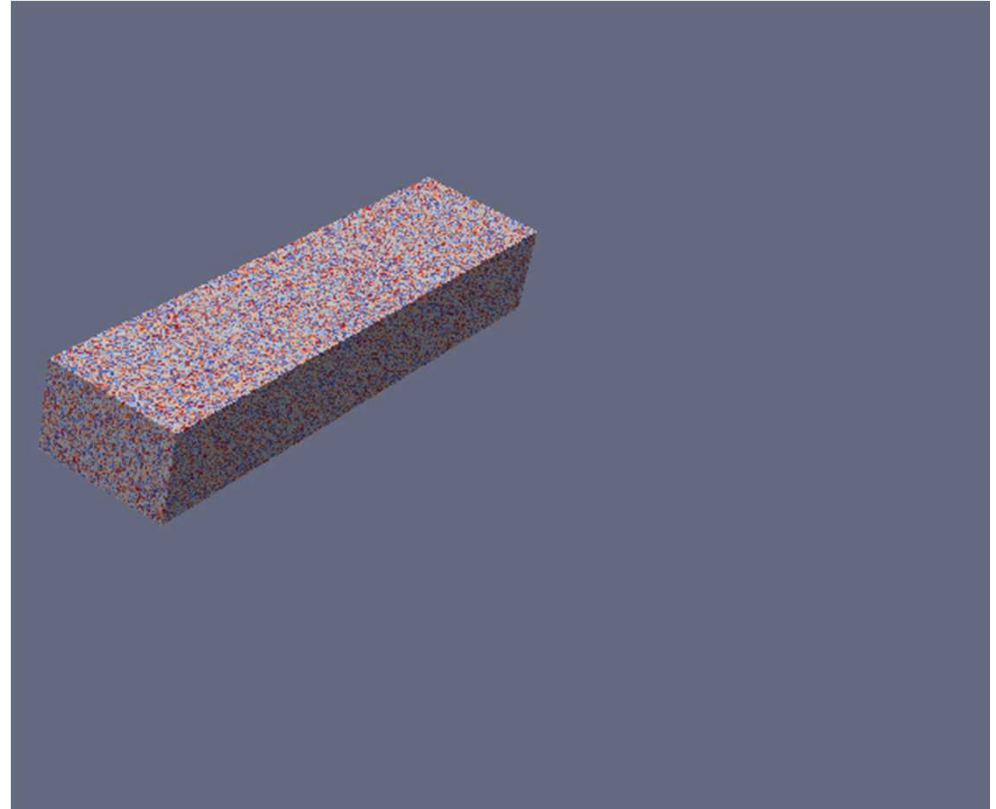
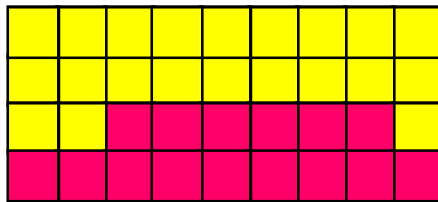
Matous, K. and Maniatty, A., Finite element formulation for modeling large deformations in elasto-viscoplastic polycrystals. *Int. J. Numerical Methods in Engineering*. 2004; **60**:2313-2333.

# Synthetic Microstructure Generation

Potts grain growth model with a moving heat source

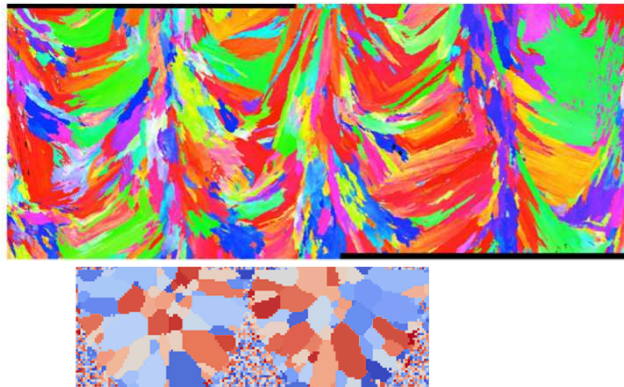


$$P = \begin{cases} 1 & \text{for } E \leq 0 \\ \exp\left(\frac{-\Delta E}{kT}\right) & \text{for } E > 0 \end{cases}$$

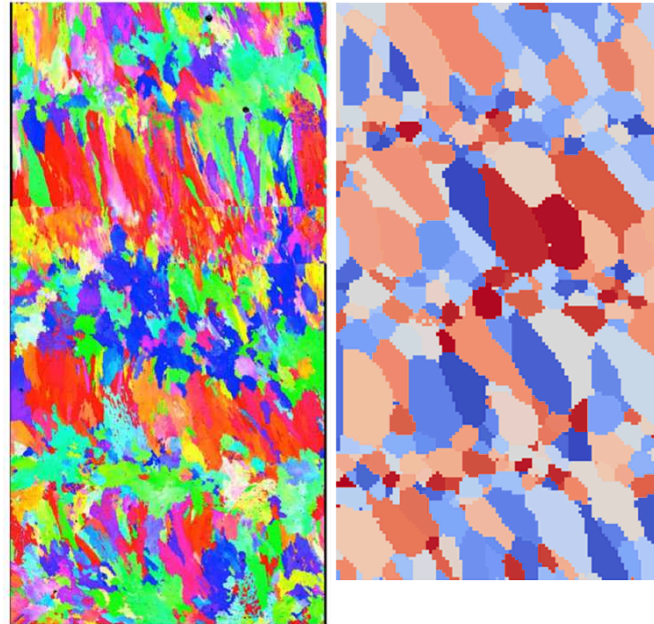


# Synthetic Microstructure Generation

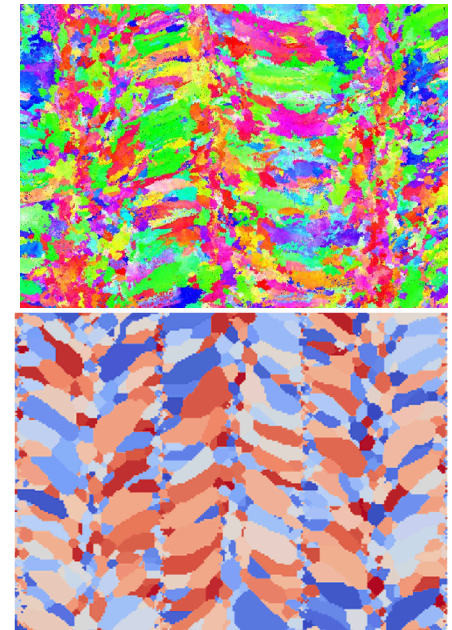
X-Plane



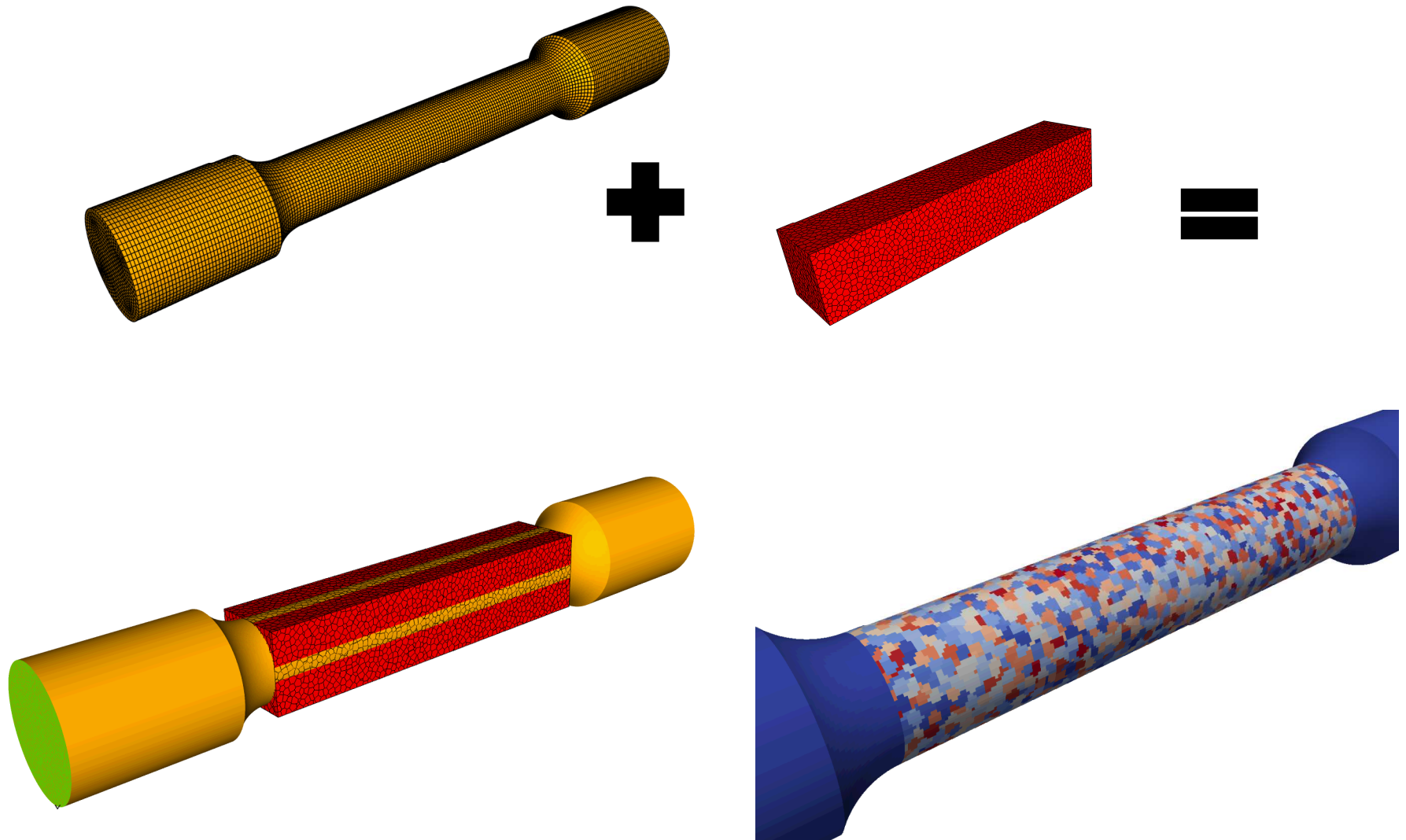
Y-Plane



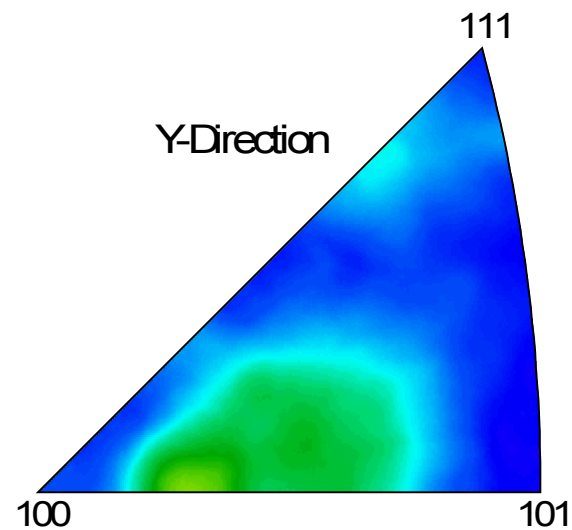
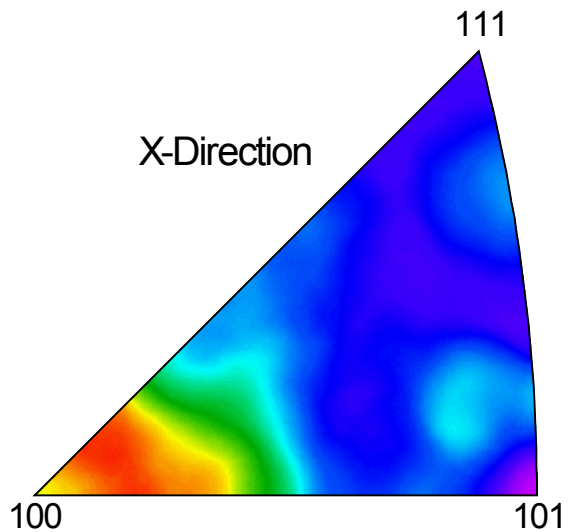
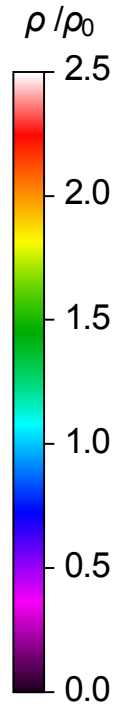
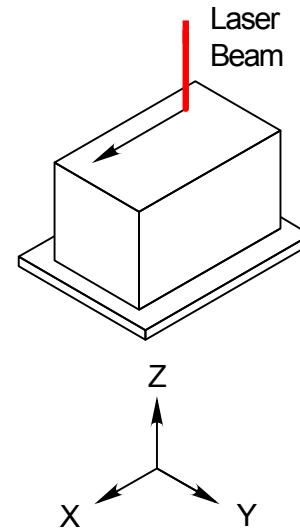
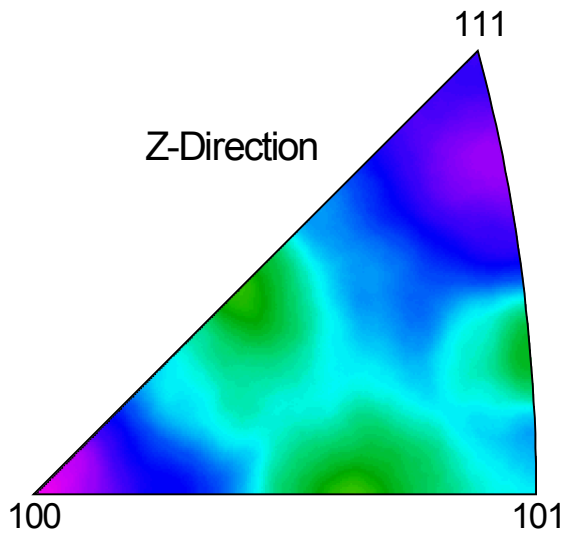
Z-Plane



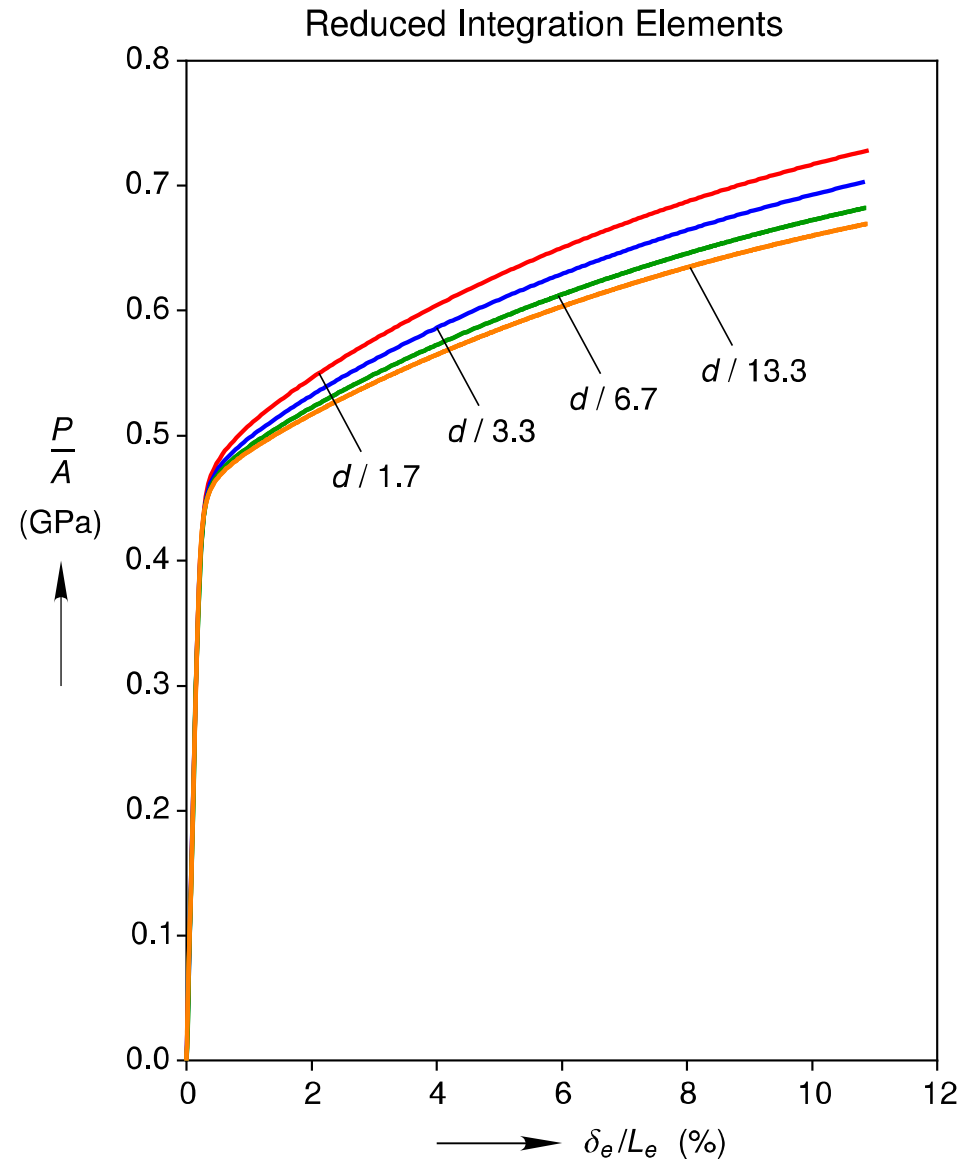
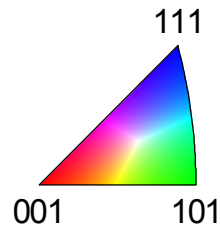
# Voronoi Overlay on a Hexahedral Mesh



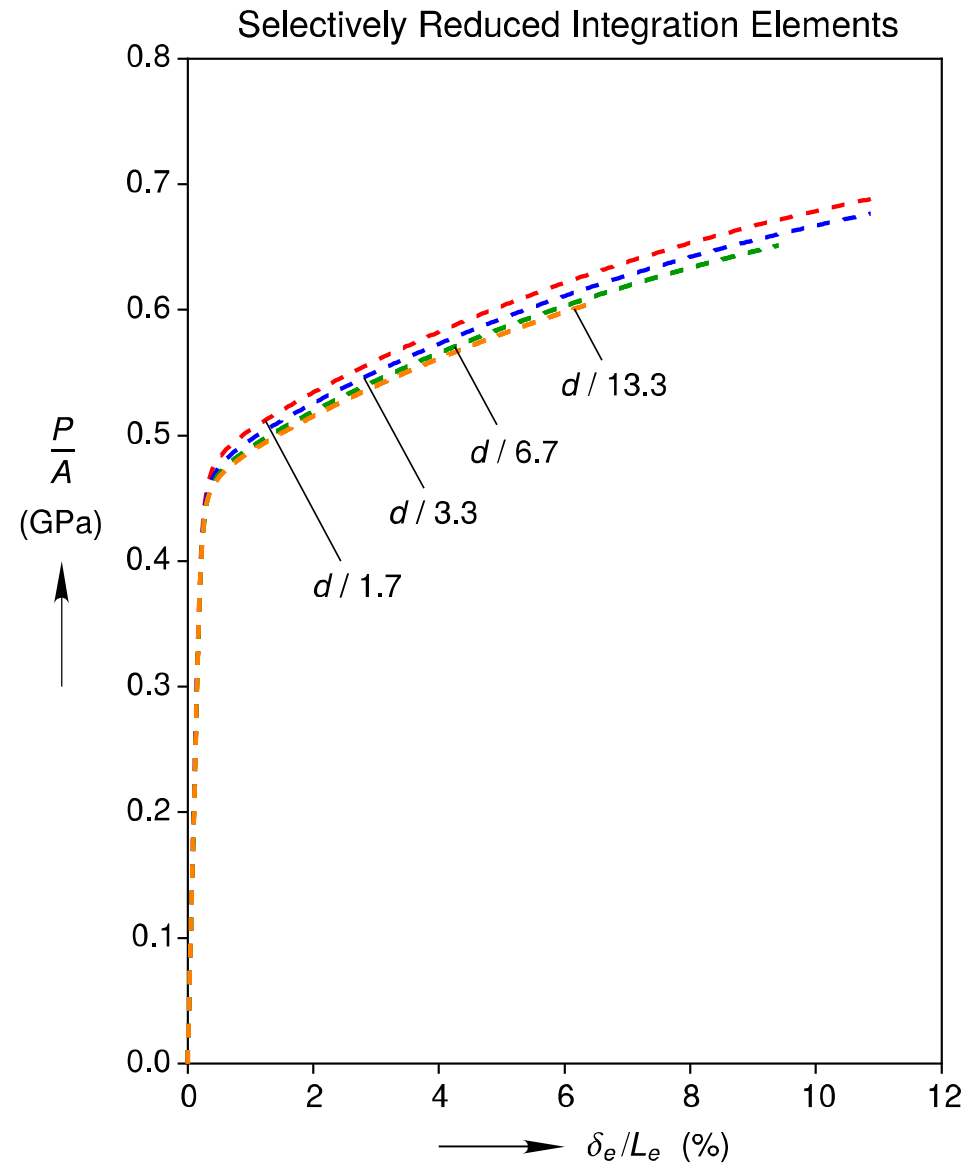
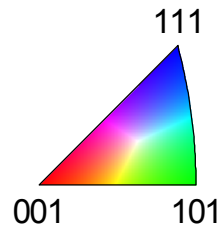
# Inverse Pole Figures



# Mesh Convergence

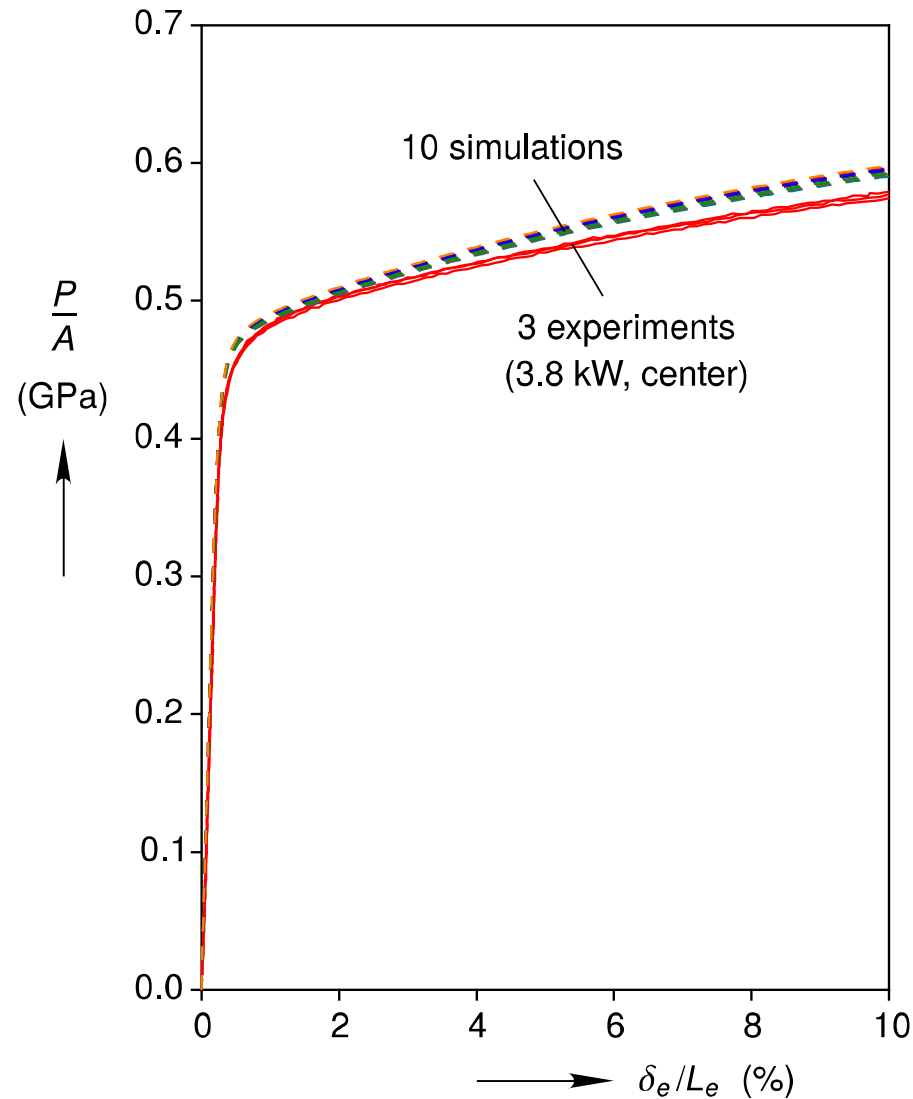


# Mesh Convergence

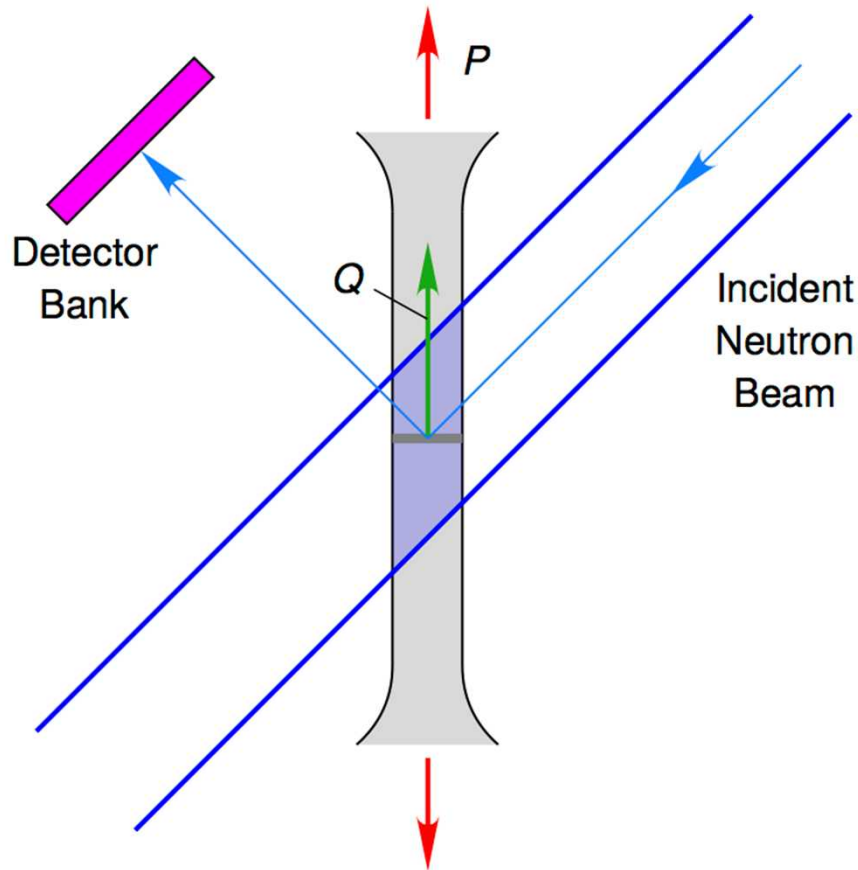




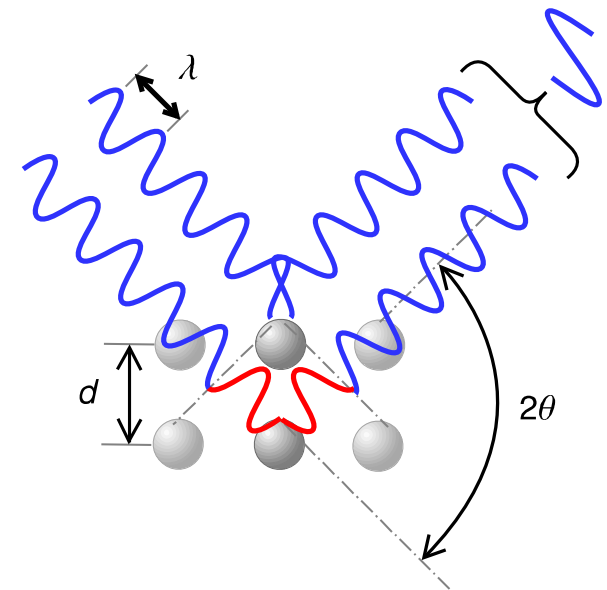
# Calibration and Statistical Consistency



# Neutron Diffraction



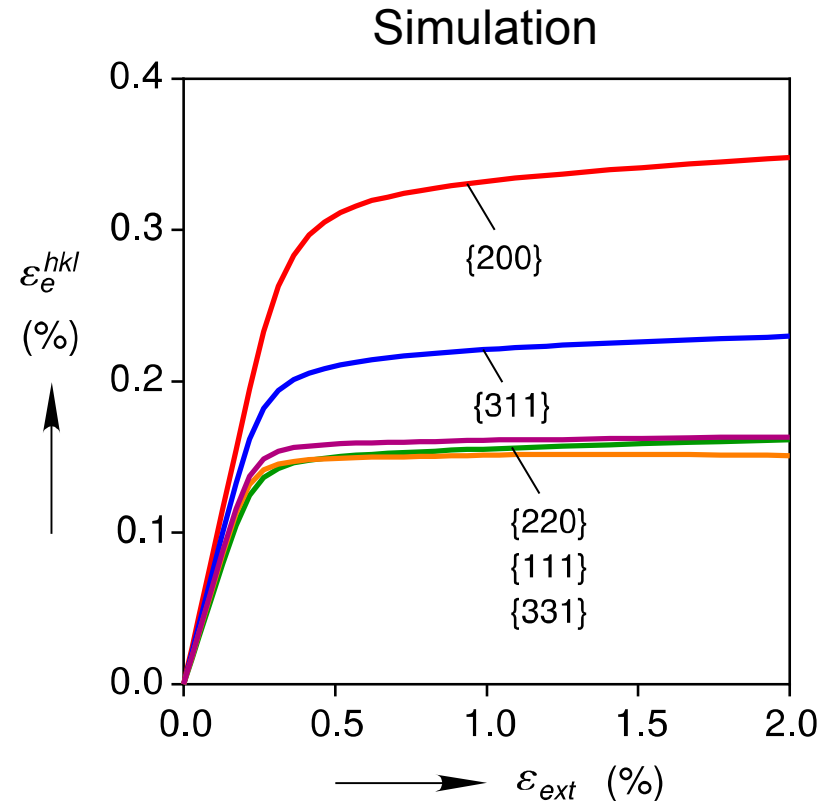
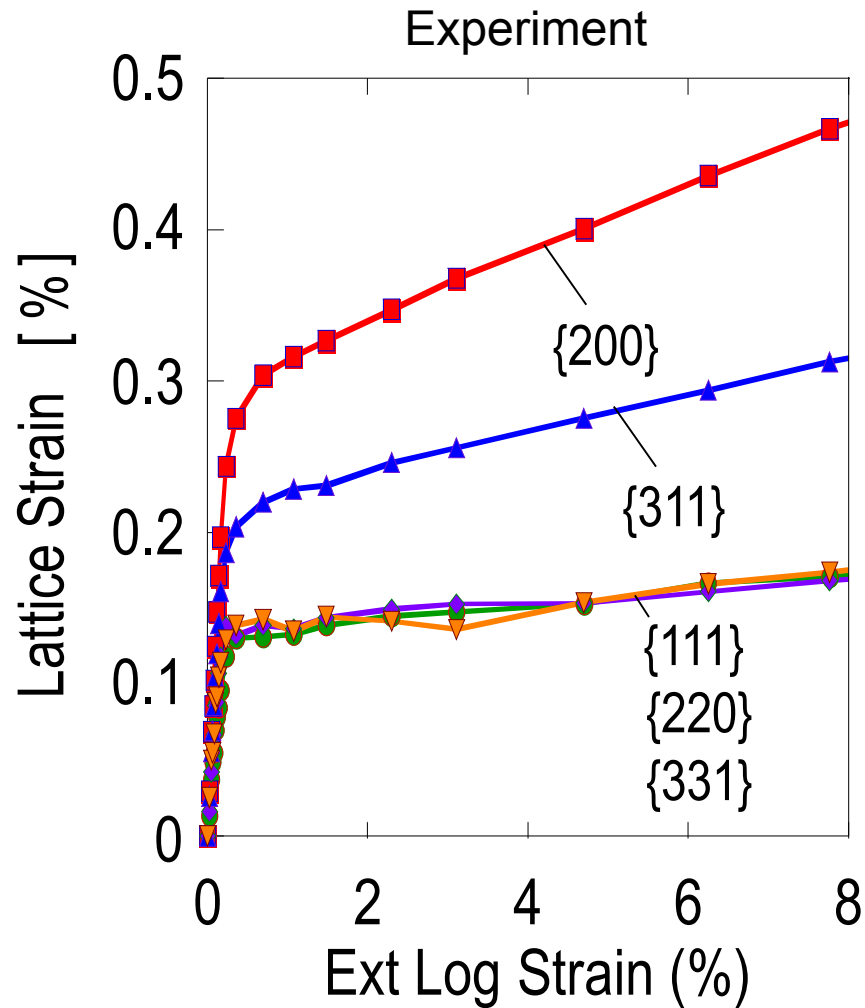
## Bragg's Law



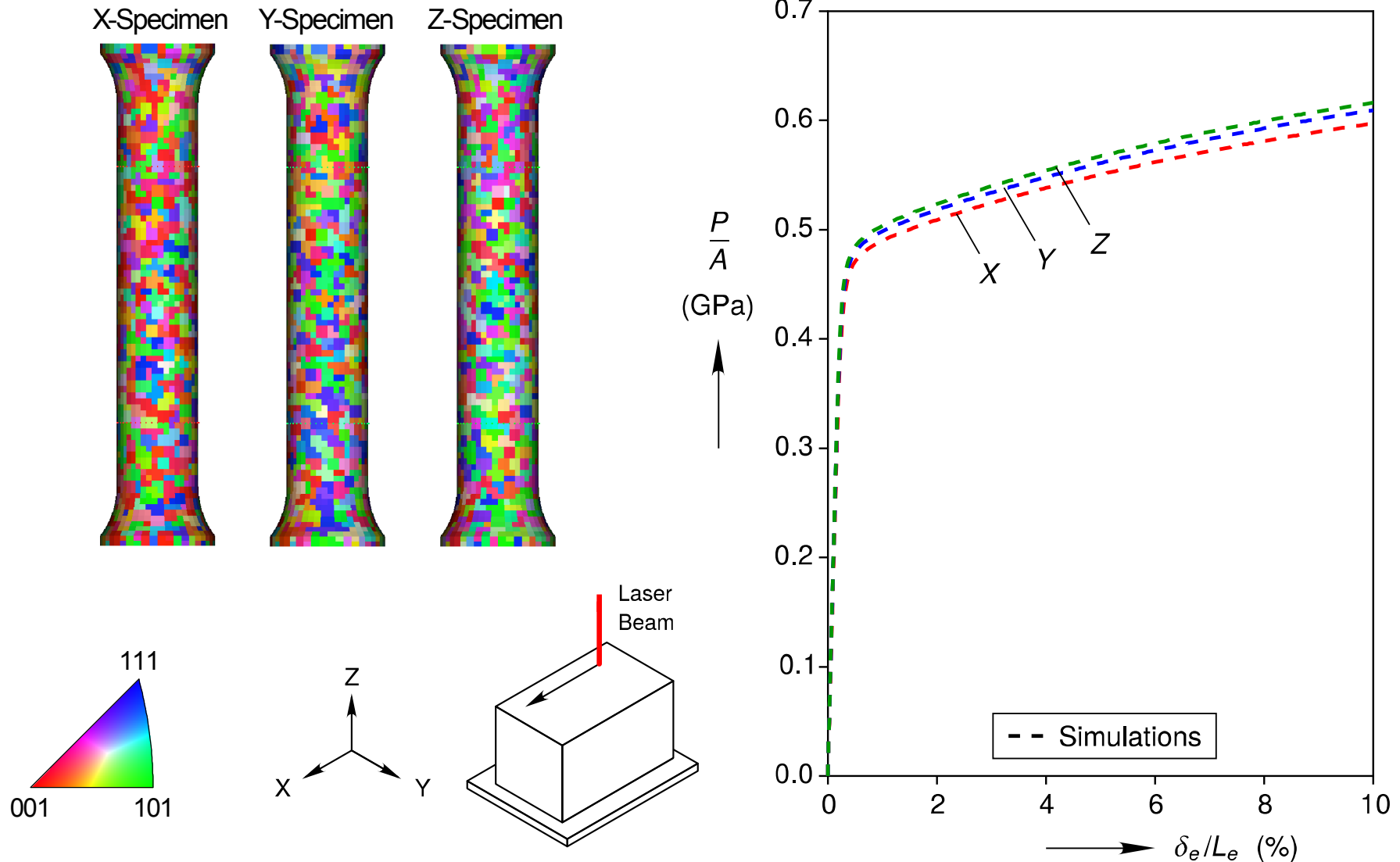
$$2d \sin \theta = n \lambda$$

[http://en.wikipedia.org/wiki/Bragg's\\_law](http://en.wikipedia.org/wiki/Bragg's_law) (modified)

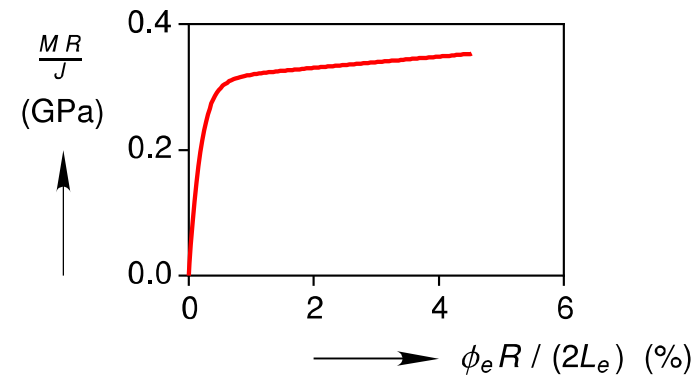
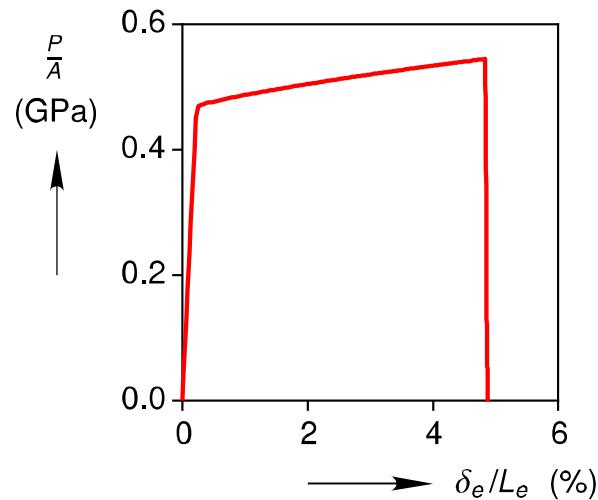
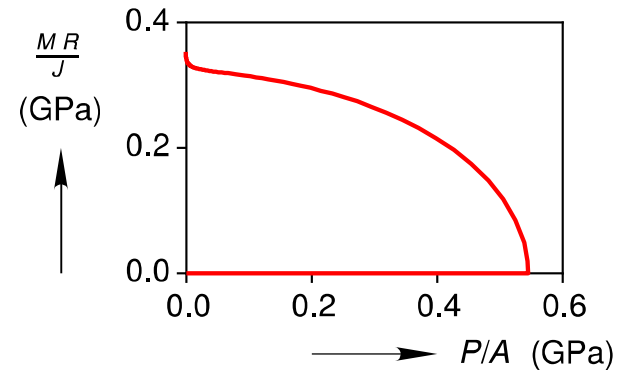
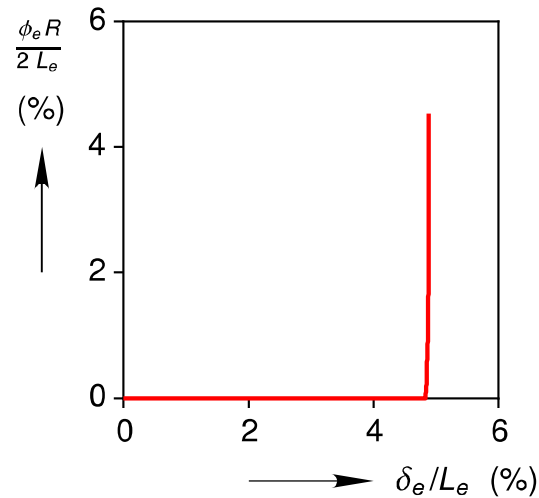
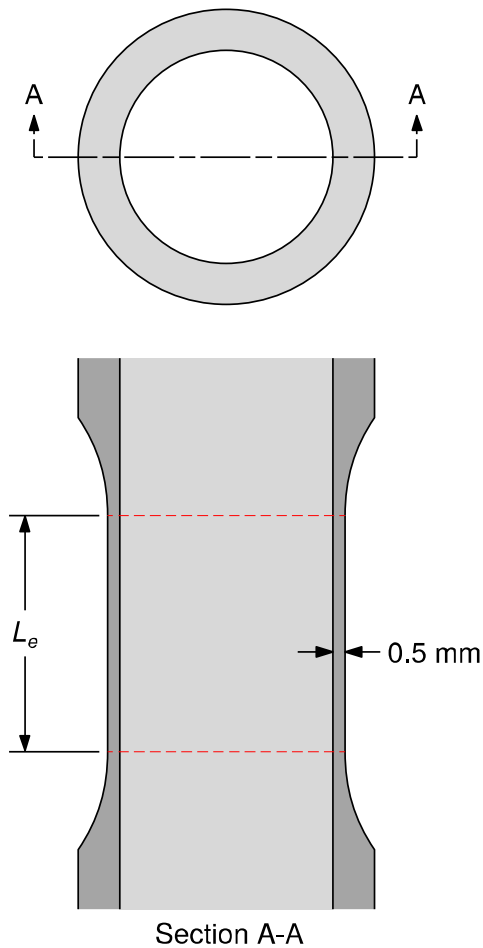
# Lattice Strains



# Anisotropy Predictions



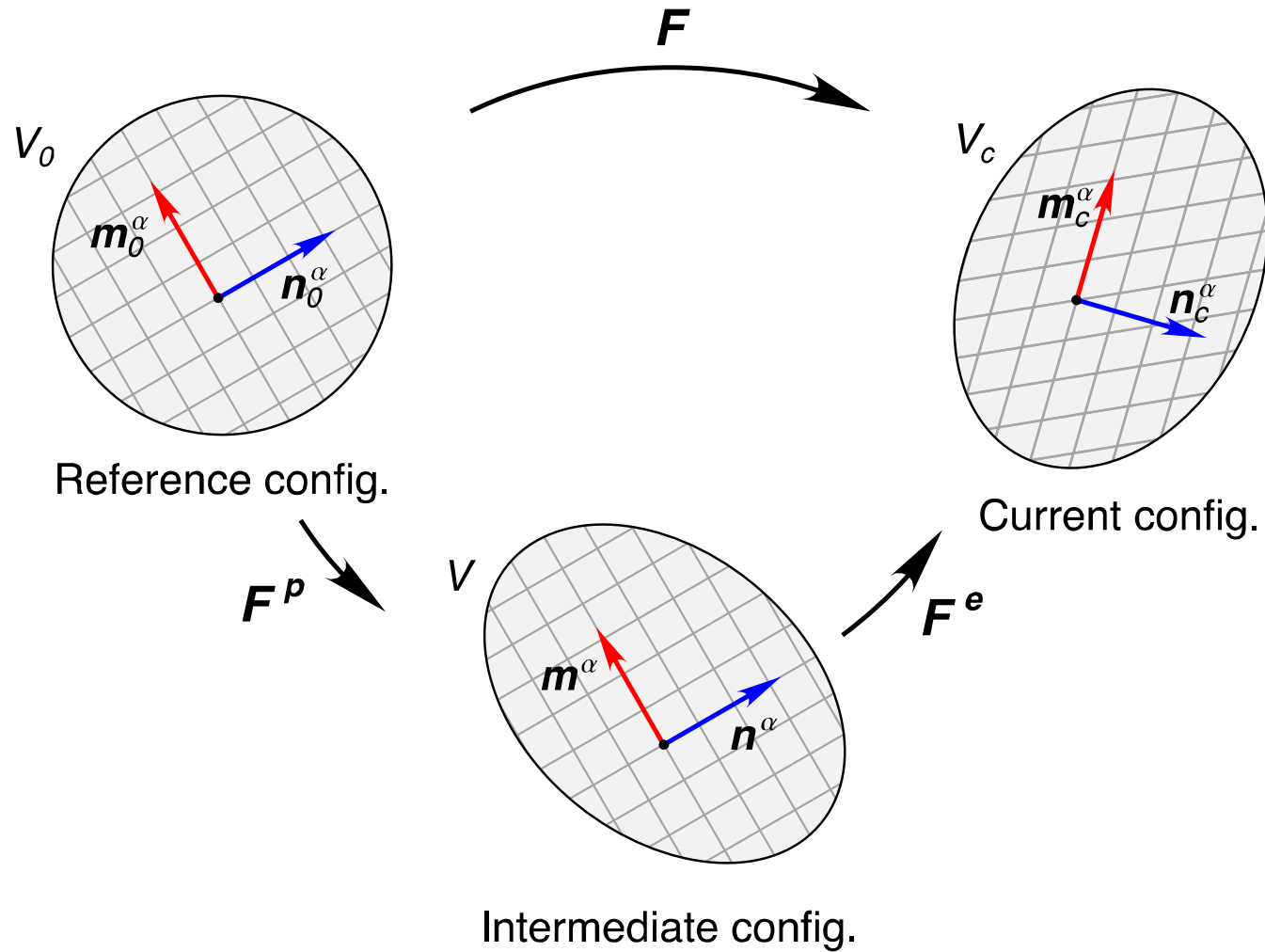
# Validation Simulations



- Experiments
  - Additively manufactured 304L is 50-100% stronger and less ductile than comparable wrought 304L
- Simulations
  - Synthetic microstructures generated
  - Mesh convergence is difficult to obtain
  - Qualitatively validated the model against neutron diffraction measurements
  - Predicted mild anisotropy in yield and hardening

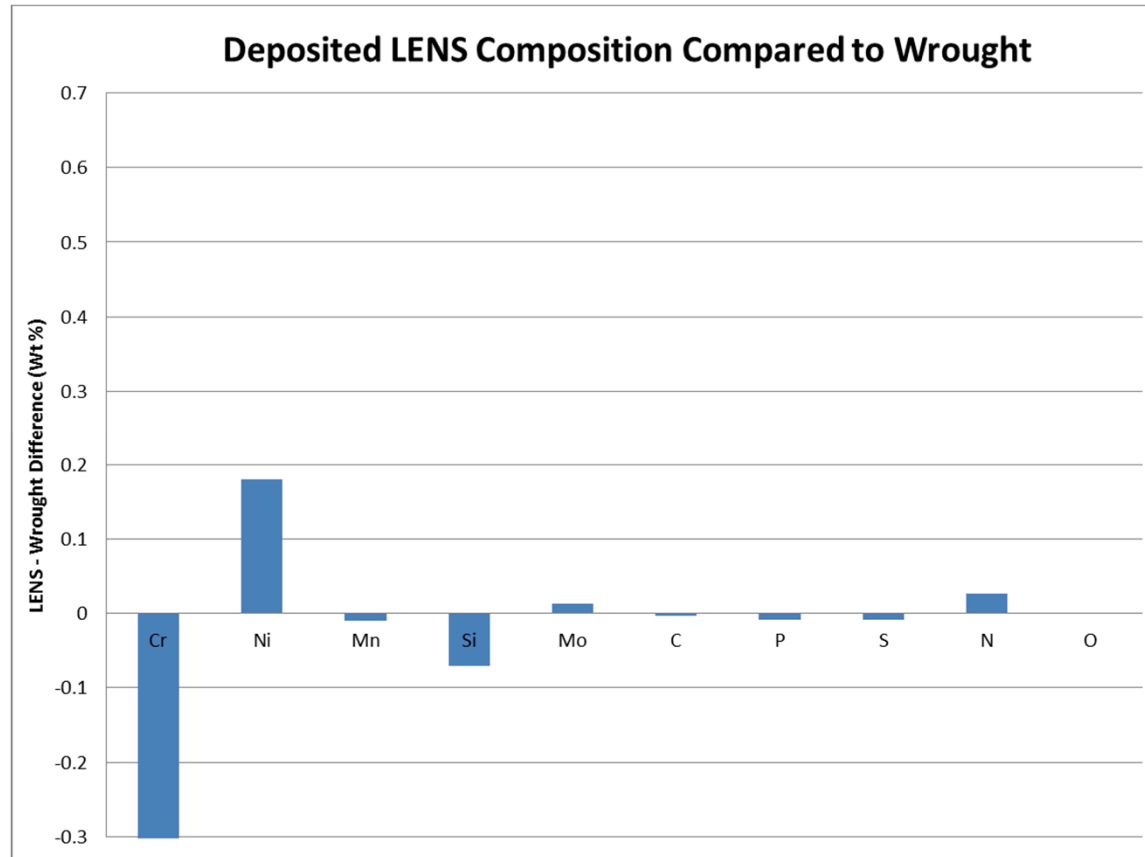
# Questions?

# Crystal Plasticity



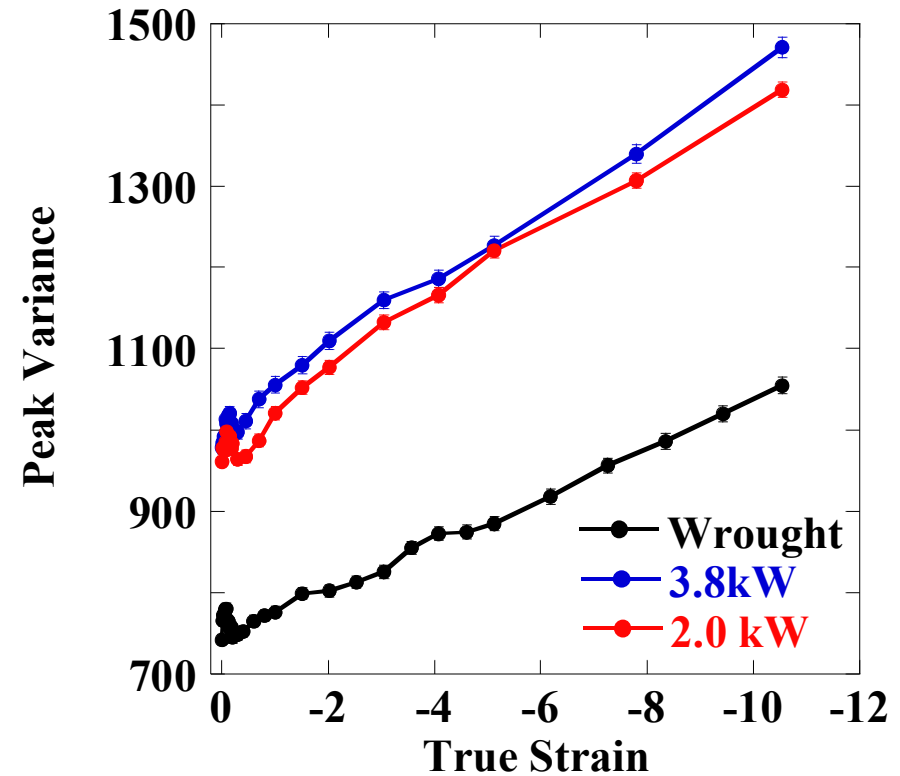
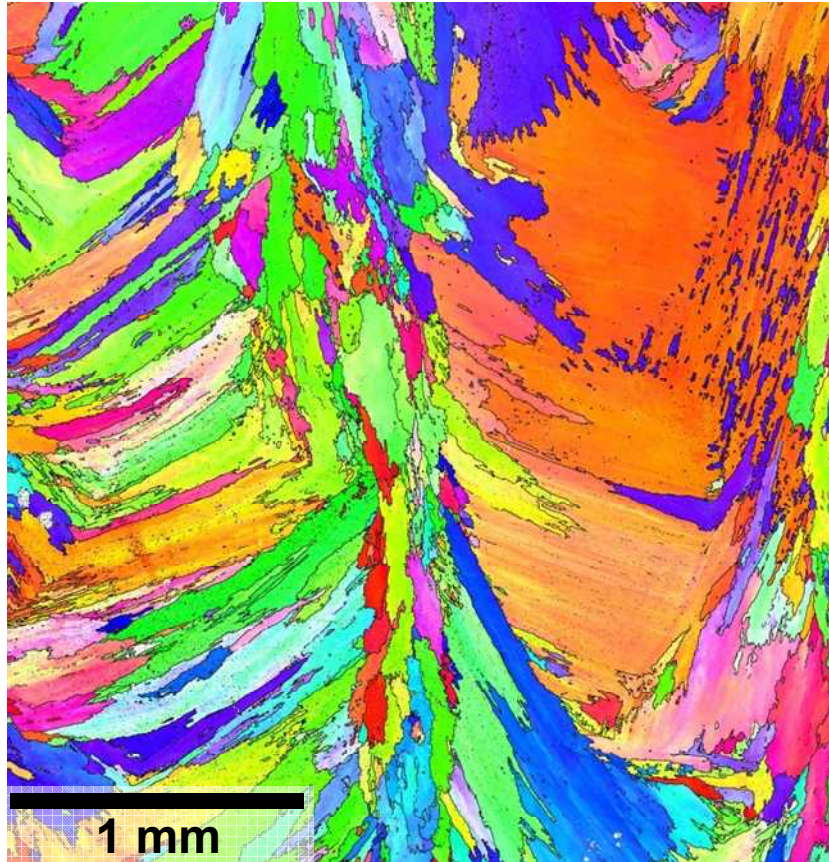


# Composition Differences



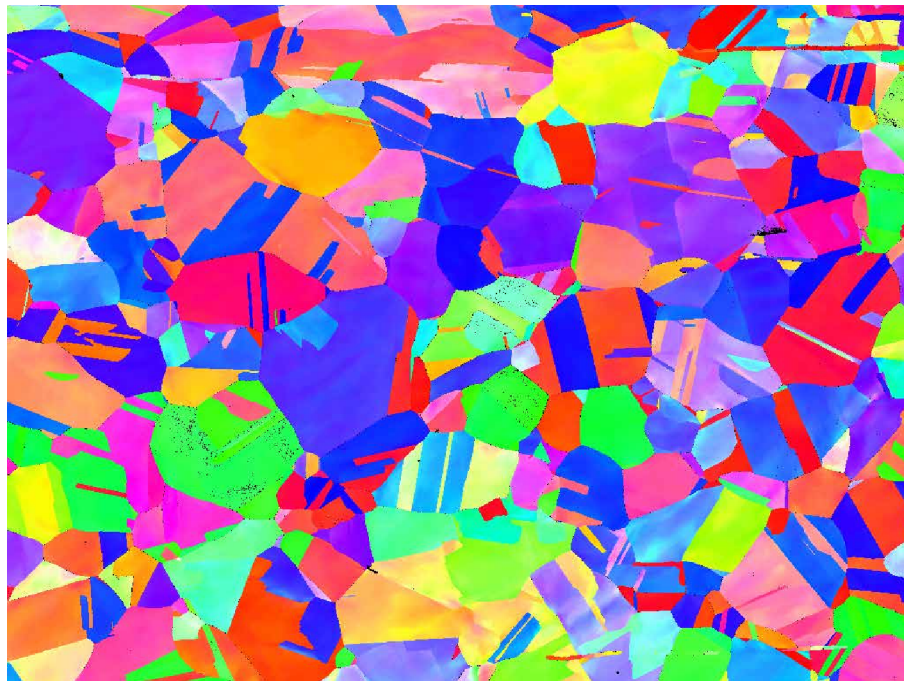
	Fe	Cr	Ni	Mn	Si	Mo	N	Co	P	S	C	O
Wrought	bal (68.2)	<b>19.5</b>	<b>10.1</b>	1.5	0.58	0.027	0.049	0.029	0.015	0.015	0.013	0
LENS Deposited	bal (68.8)	<b>18.8</b>	<b>10.28</b>	1.49	0.51	0.04	0.075	0	0.007	0.007	0.01	0.023

# Indicators of Dislocation Density

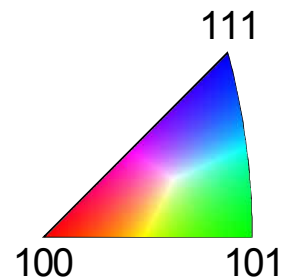


# Ferrite / Martensite

Wrought  
1.2 % Ferrite/Martensite (Ferrite Scope)



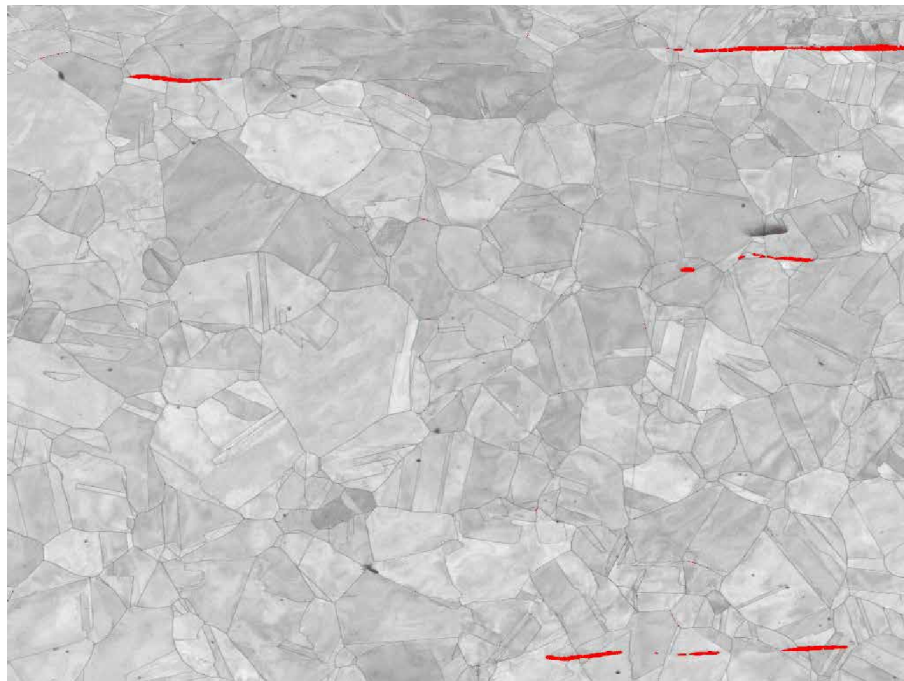
LENS 2 kW  
2.3 % Ferrite/Martensite (Ferrite Scope)





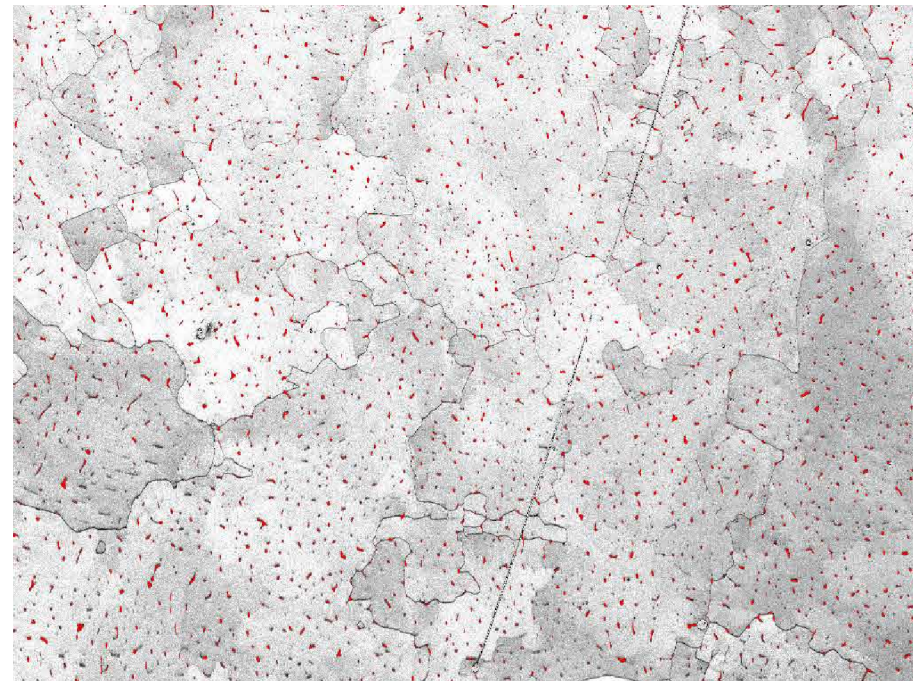
# Ferrite / Martensite

Wrought  
1.2 % Ferrite/Martensite (Ferrite Scope)



100  $\mu\text{m}$

LENS 2 kW  
2.3 % Ferrite/Martensite (Ferrite Scope)



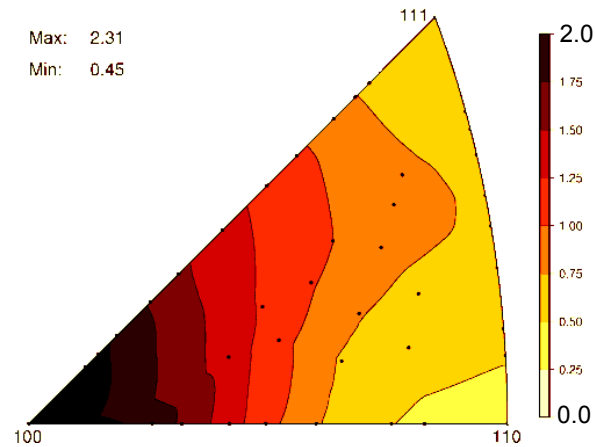
100  $\mu\text{m}$

Gray = Austenite, Red = Ferrite

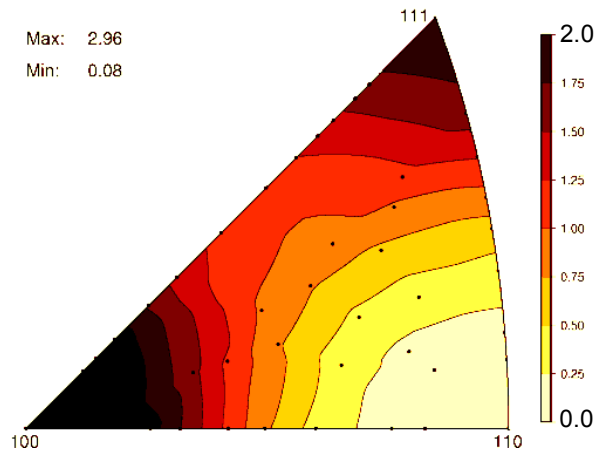
# Deformation Induced Texture

## Experiment

0 % Strain

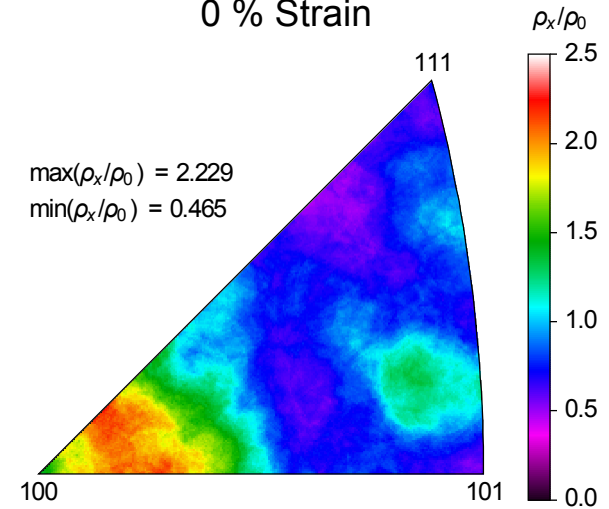


32 % Strain

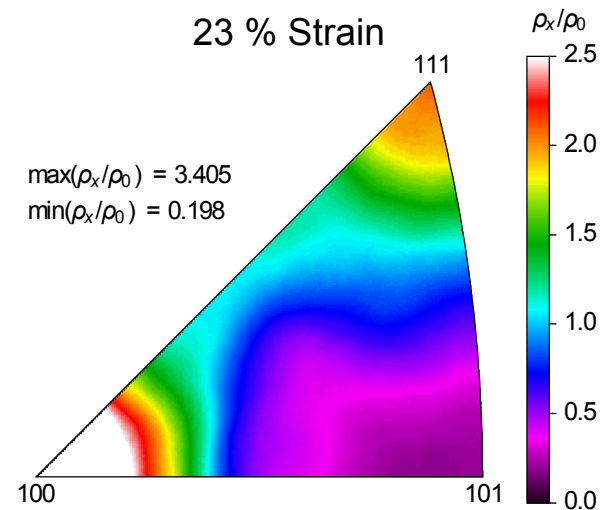


## Simulations

0 % Strain



23 % Strain



# Modeling Strategy

- Homogeneous Plasticity Models
  - Isotropic, Von Mises
  - Anisotropic, Hill
- Crystal Plasticity Finite Element Models
  - Textured microstructure with equiaxed grains of uniform size
  - Textured microstructure with approximate grain morphology
- Other material models?