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Modeling the Mechanical Behavior of Additively Manufactured 304L Stainless Steel

Benjamin Reedlunn¹, David Adams¹, Jay Carroll¹, Bo Song¹,
Michael Maguire¹, Jack Wise¹, Joseph Bishop¹, Joseph
Michael¹, Jonathan Madison¹, Theron Rodgers¹, Donald
Brown², Bjorn Clausen², Todd Palmer³

1: Sandia National Laboratories

2: Los Alamos National Laboratories

3: Pennsylvania State University



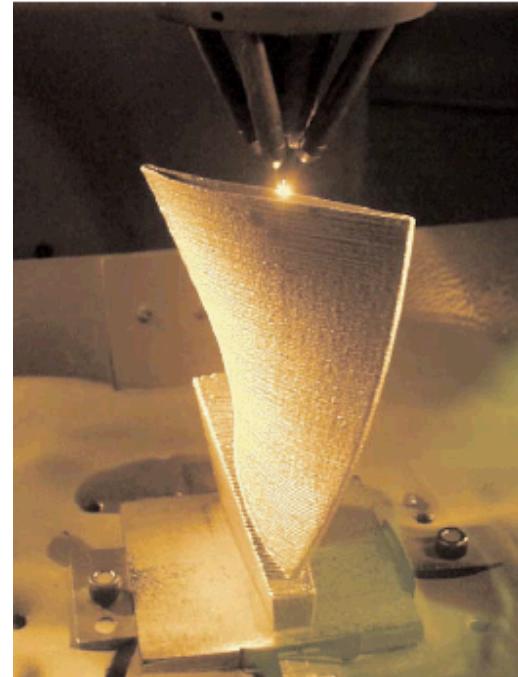
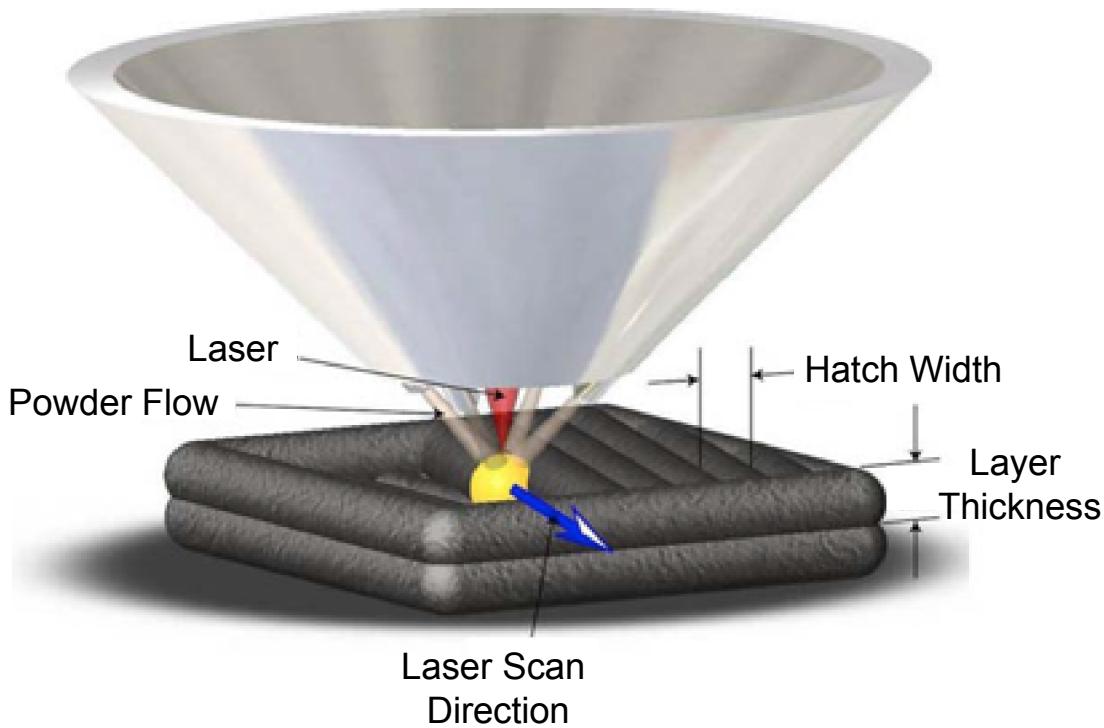
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Outline

- Introduction
- Experimental Characterization
- Simulations
 - Model Construction
 - Preliminary Results

INTRODUCTION

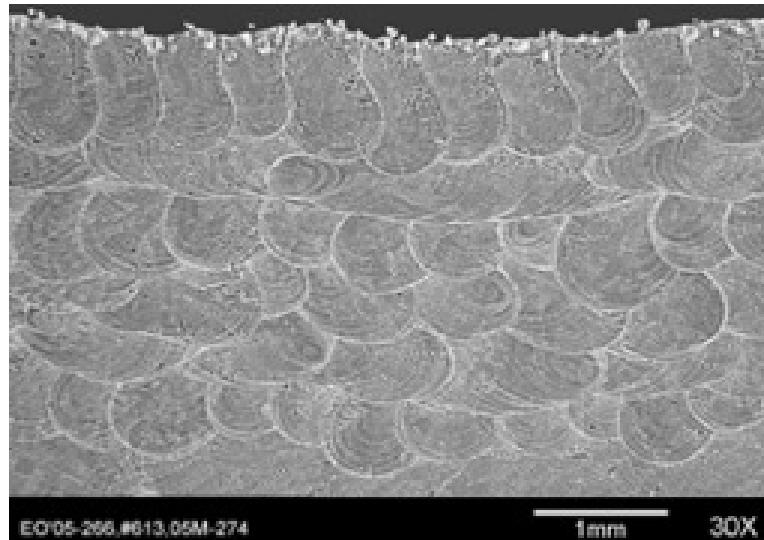
Laser Engineered Net Shaping (LENS™)



- Pros
 - Complex part geometries
 - Rapid design to production
- Cons
 - Speed
 - Finishing required
 - Open scientific questions

Fundamental Questions

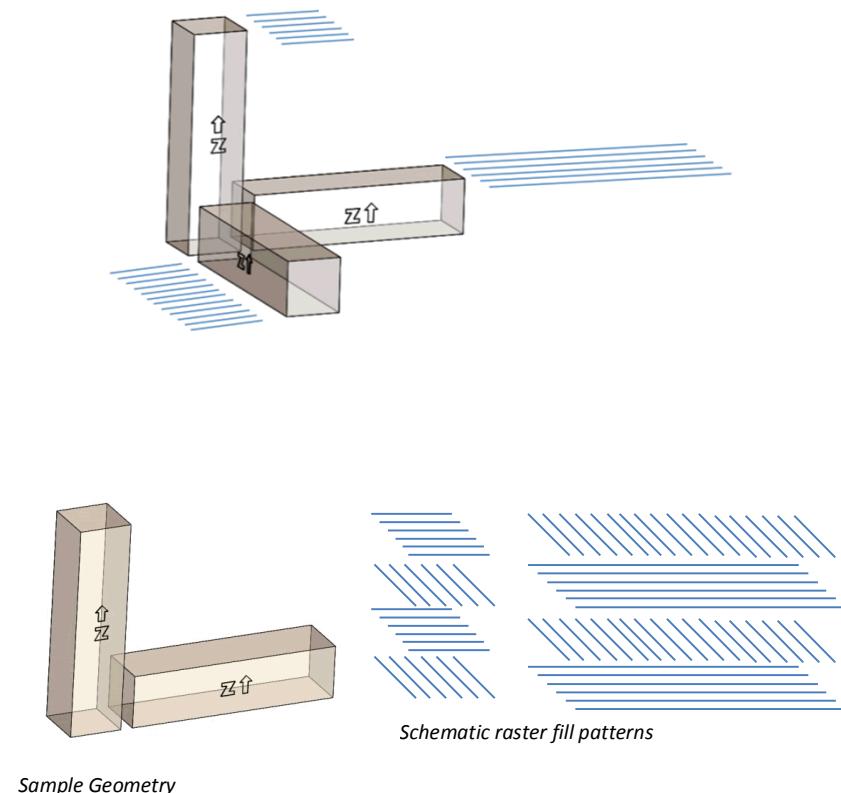
- How does the mechanical response of a LENS material compare to that of a wrought material.
 - What role does the exotic microstructure play?
 - Variability?



- How do we predict the response?
 - What level of sophistication do we need in our simulations?
 - Loss of 'scale separation'?

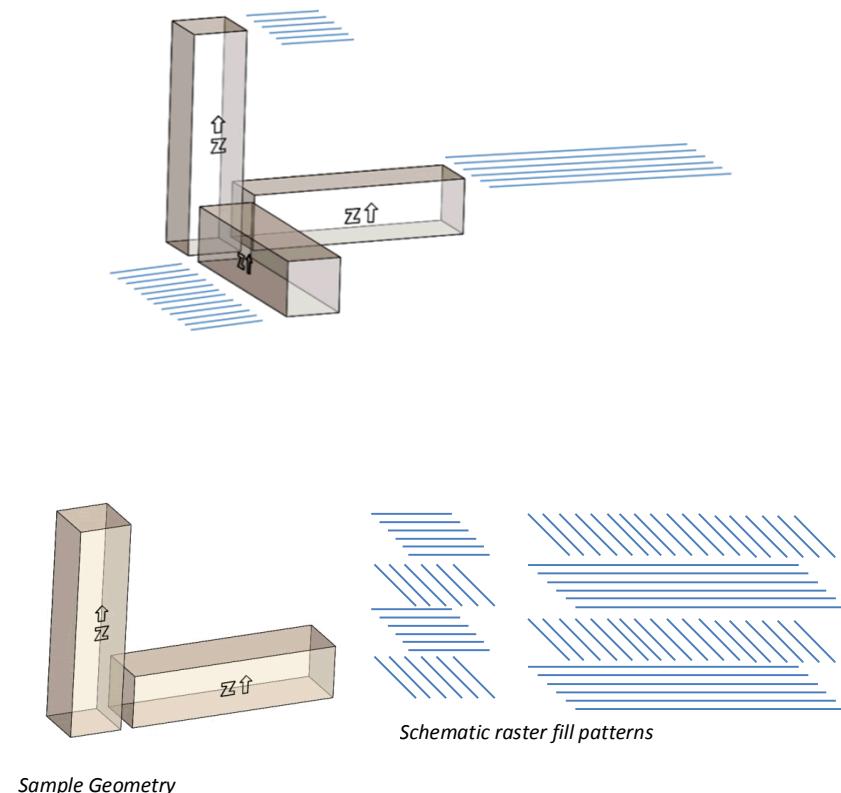
Parameter Sensitivities

- Laser power
 - 3.8 kW, 2 kW, 0.5 kW
- Parallel Hatch vs. Cross Hatch
- As-Deposited vs. Annealed
- Anisotropy
 - X vs. Y vs. Z
- Center vs. Edge
- Strain Rate
 - 10^{-5} s^{-1} to 10^9 s^{-1}
- Temperature
 - 20°C to 300°C



Parameter Sensitivities

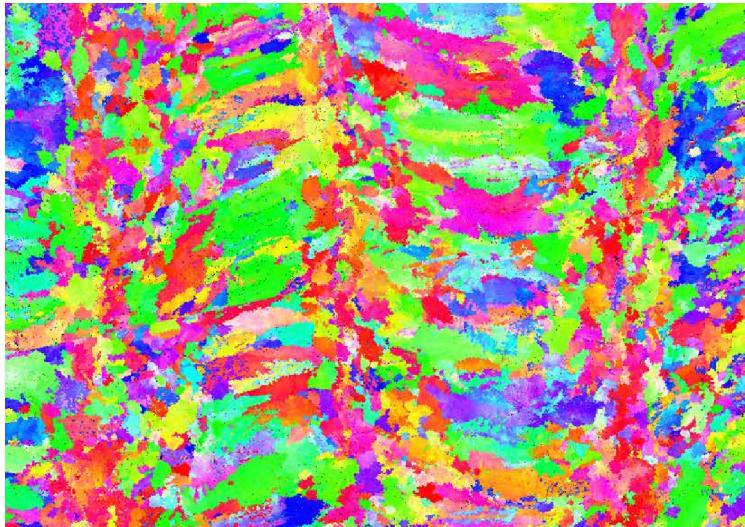
- Laser power
 - 3.8 kW, 2 kW, 0.5 kW
- Parallel Hatch vs. Cross Hatch
- As-Deposited vs. Annealed
- Anisotropy
 - X vs. Y vs. Z
- Center vs. Edge
- Strain Rate
 - 10^{-5} s^{-1} , 10⁻³ s⁻¹, to 10^9 s^{-1}
- Temperature
 - 20 °C to 300 °C



EXPERIMENTS

LENS Microstructure Orthographic Projections

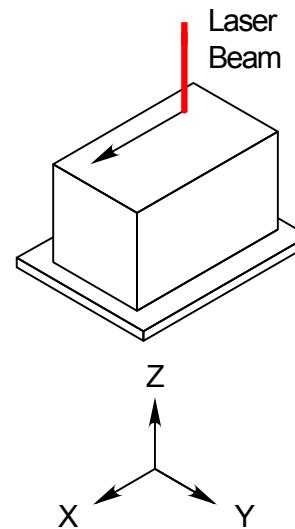
Z-Plane (Z-direction)



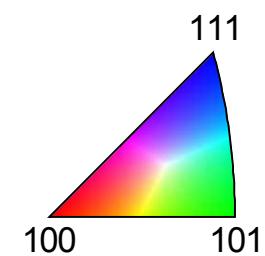
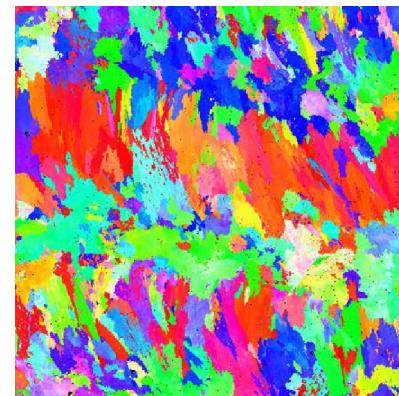
X-Plane (X-direction)



1.0 mm

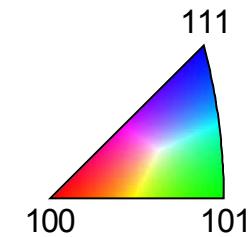
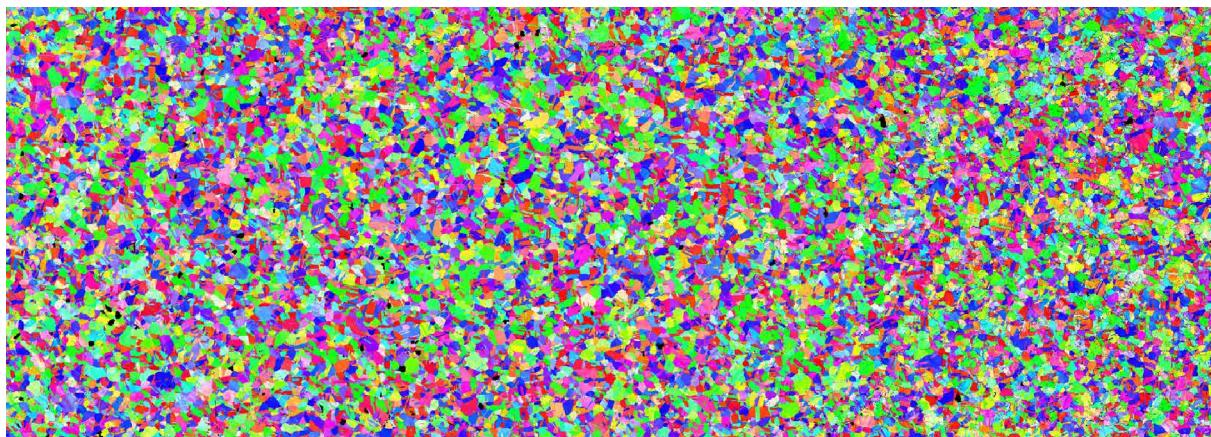


Y-Plane (Y-direction)



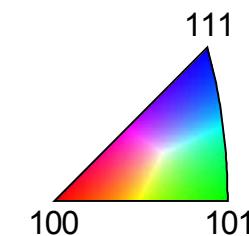
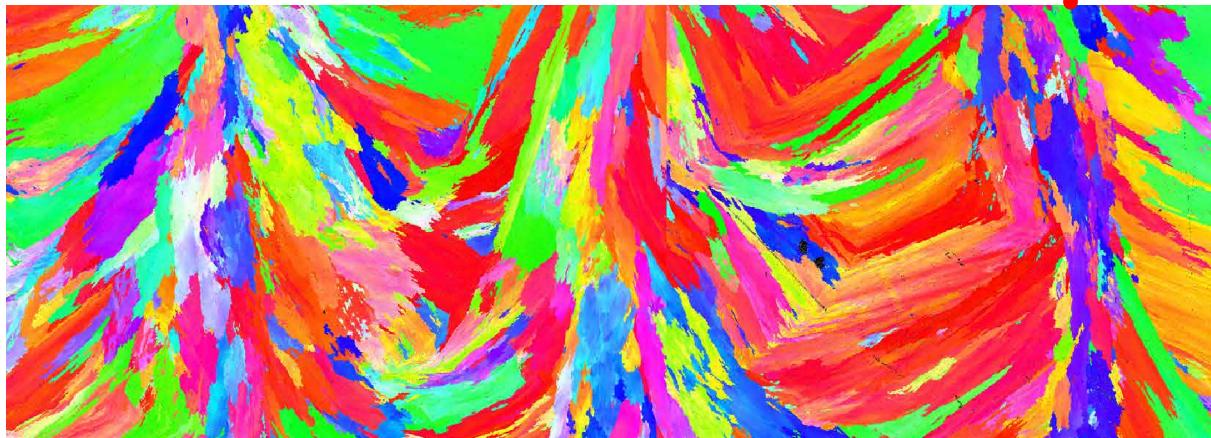
Wrought vs. LENS Microstructure

Wrought



1.0 mm

3.8 kW LENS



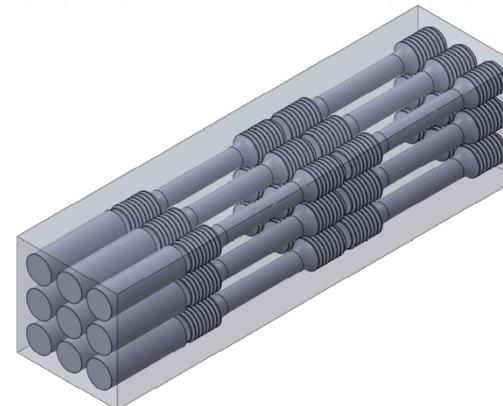
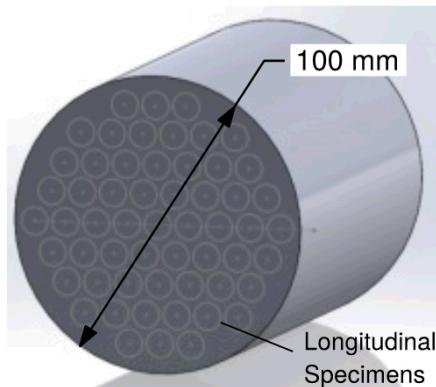
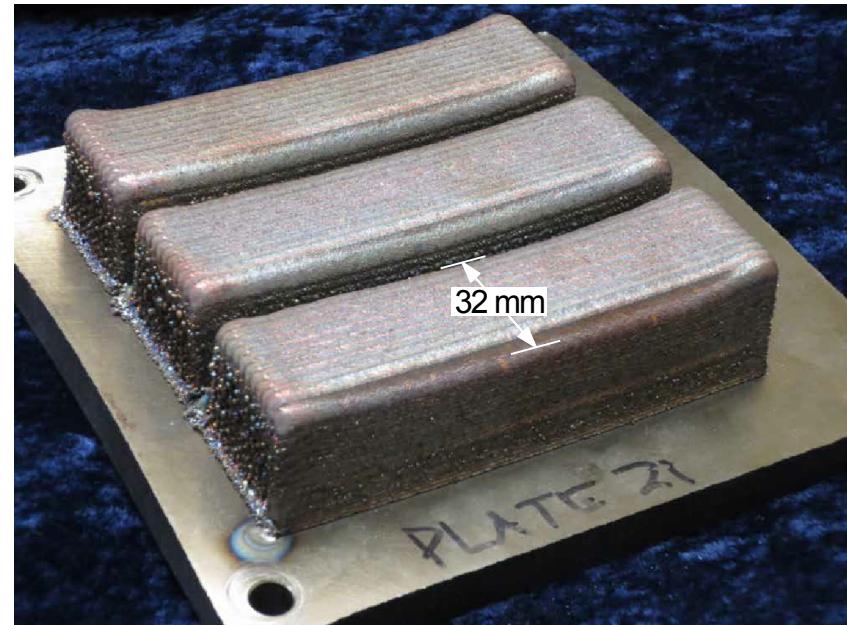
1.0 mm

Base Material

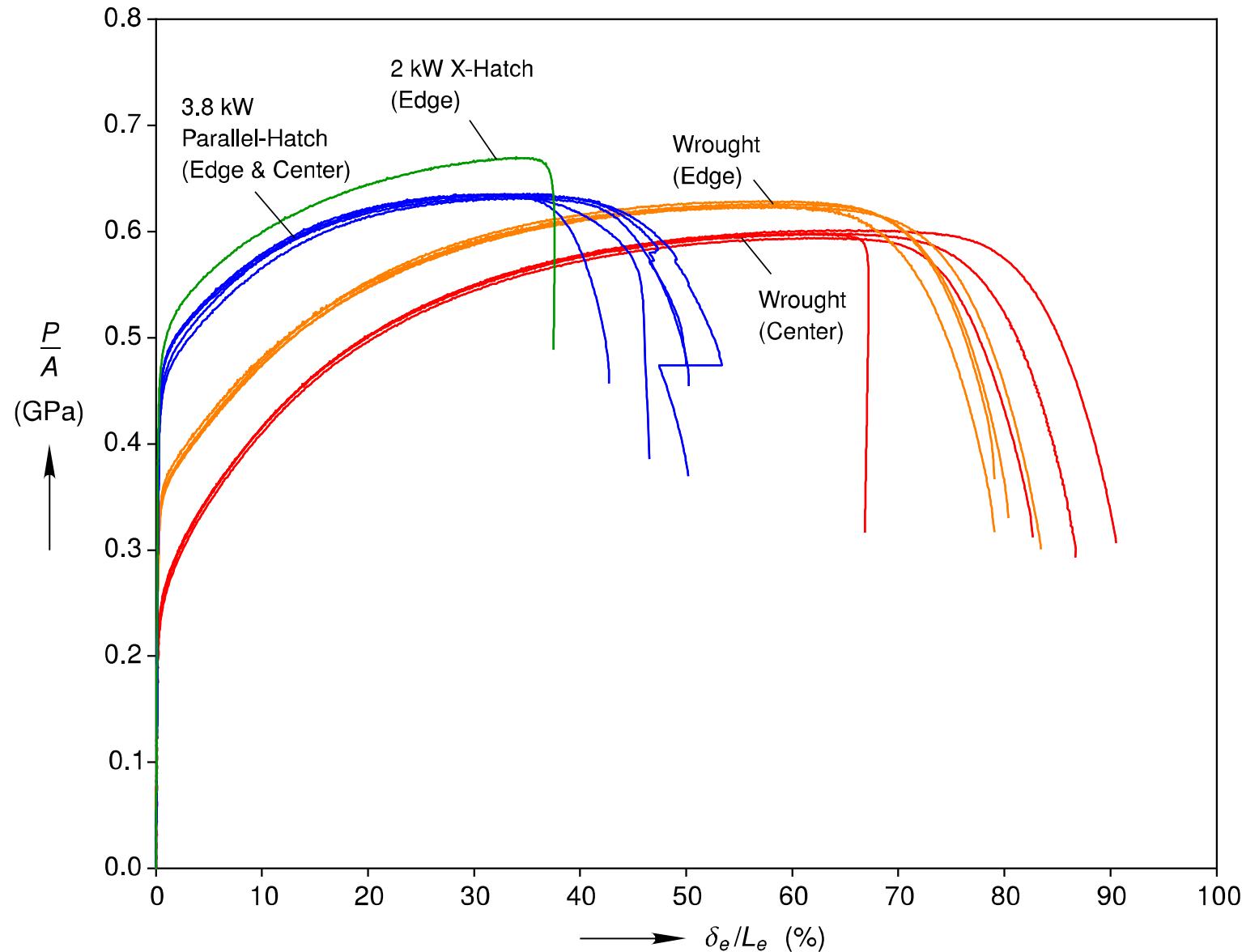
Wrought Bar



LENS Bars (“Twinkies”)

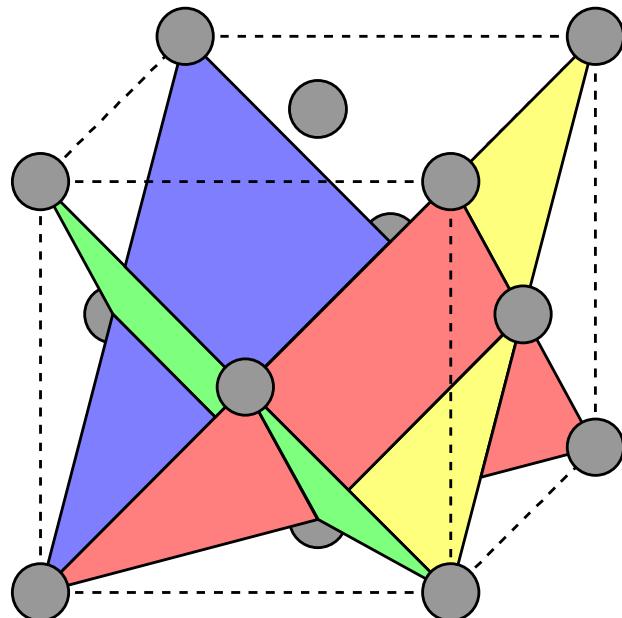


Tensile Tests



SIMULATIONS

Crystal Plasticity Model



$$\tau^\alpha = \mathbf{n}^\alpha \cdot \boldsymbol{\sigma} \cdot \mathbf{m}^\alpha$$

$$\dot{\gamma}^\alpha = \dot{\gamma}_0 \left(\frac{\tau^\alpha}{g} \right)^{1/m} \text{sign}(\tau^\alpha)$$

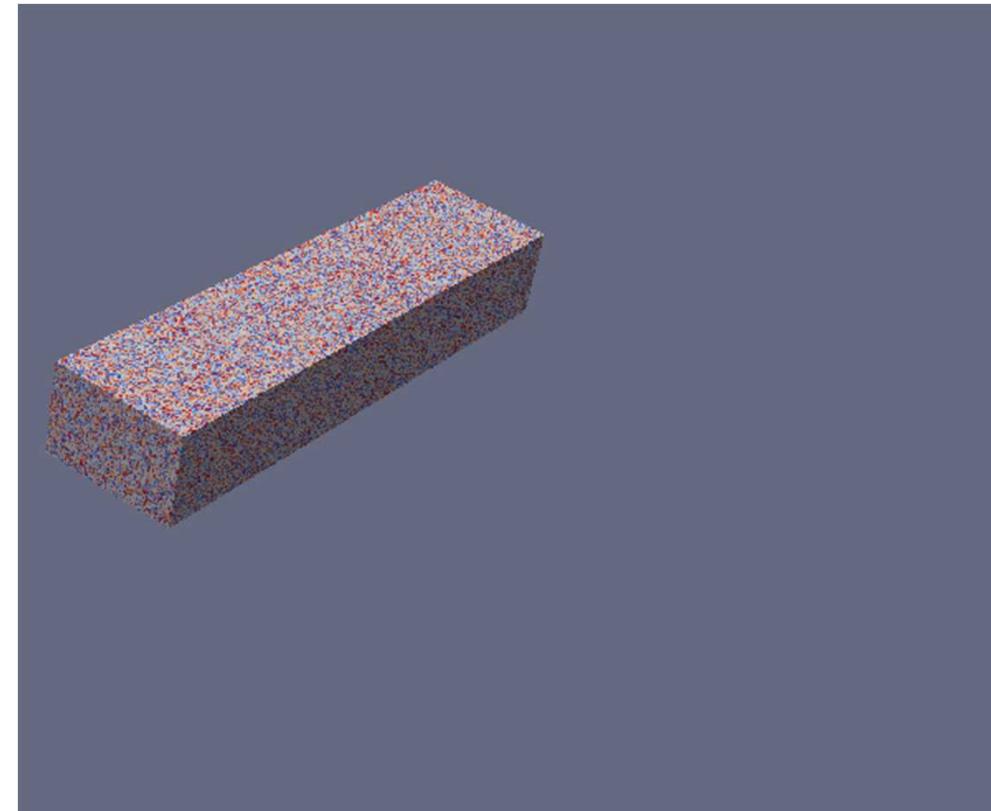
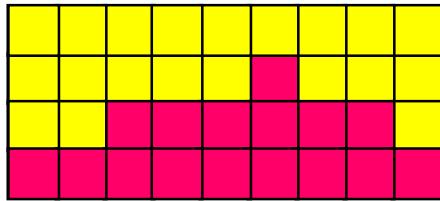
$$\gamma = \sum_{\alpha}^N |\dot{\gamma}^\alpha| \quad (\text{sum over slip systems})$$

$$g = g_0 + (g_{s0} - g_0) \left[1 - \exp \left(-\frac{G_0 \gamma}{g_{s0} - g_0} \right) \right]$$

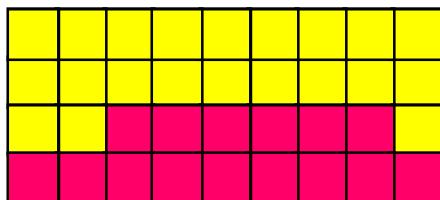
Matous, K. and Maniatty, A., Finite element formulation for modeling large deformations in elasto-viscoplastic polycrystals. *Int. J. Numerical Methods in Engineering.* 2004; **60**:2313-2333.

Synthetic Microstructure Generation

Potts grain growth model with a moving heat source

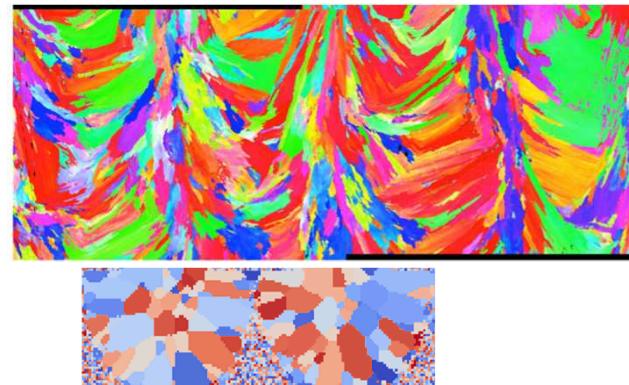


$$P = \begin{cases} 1 & \text{for } E \leq 0 \\ \exp\left(\frac{-\Delta E}{kT}\right) & \text{for } E > 0 \end{cases}$$

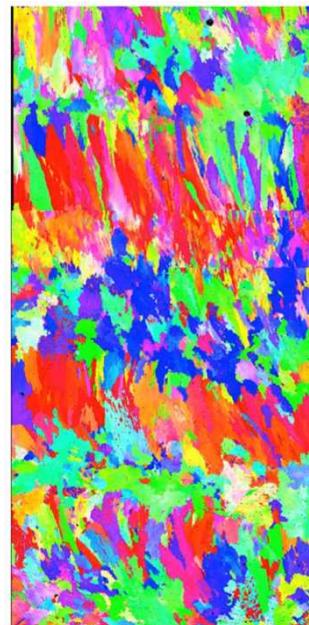


Synthetic Microstructure Generation

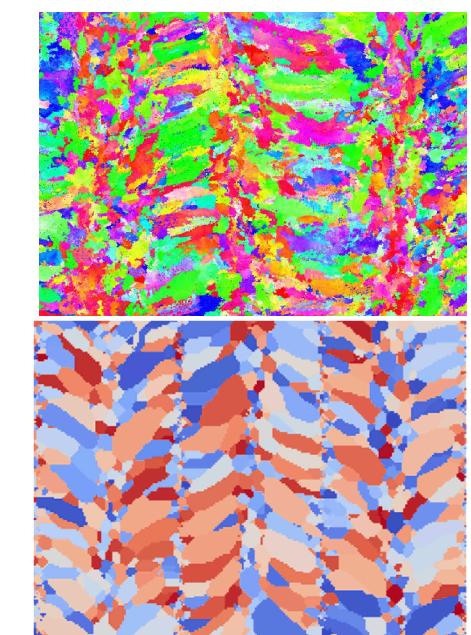
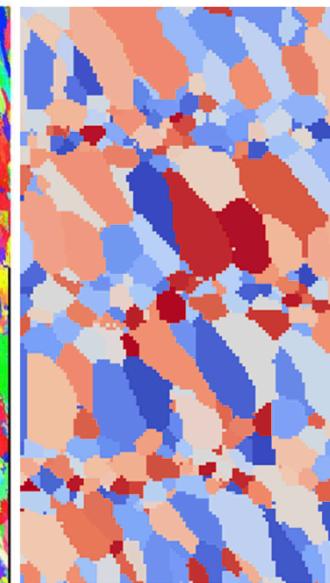
X-Plane



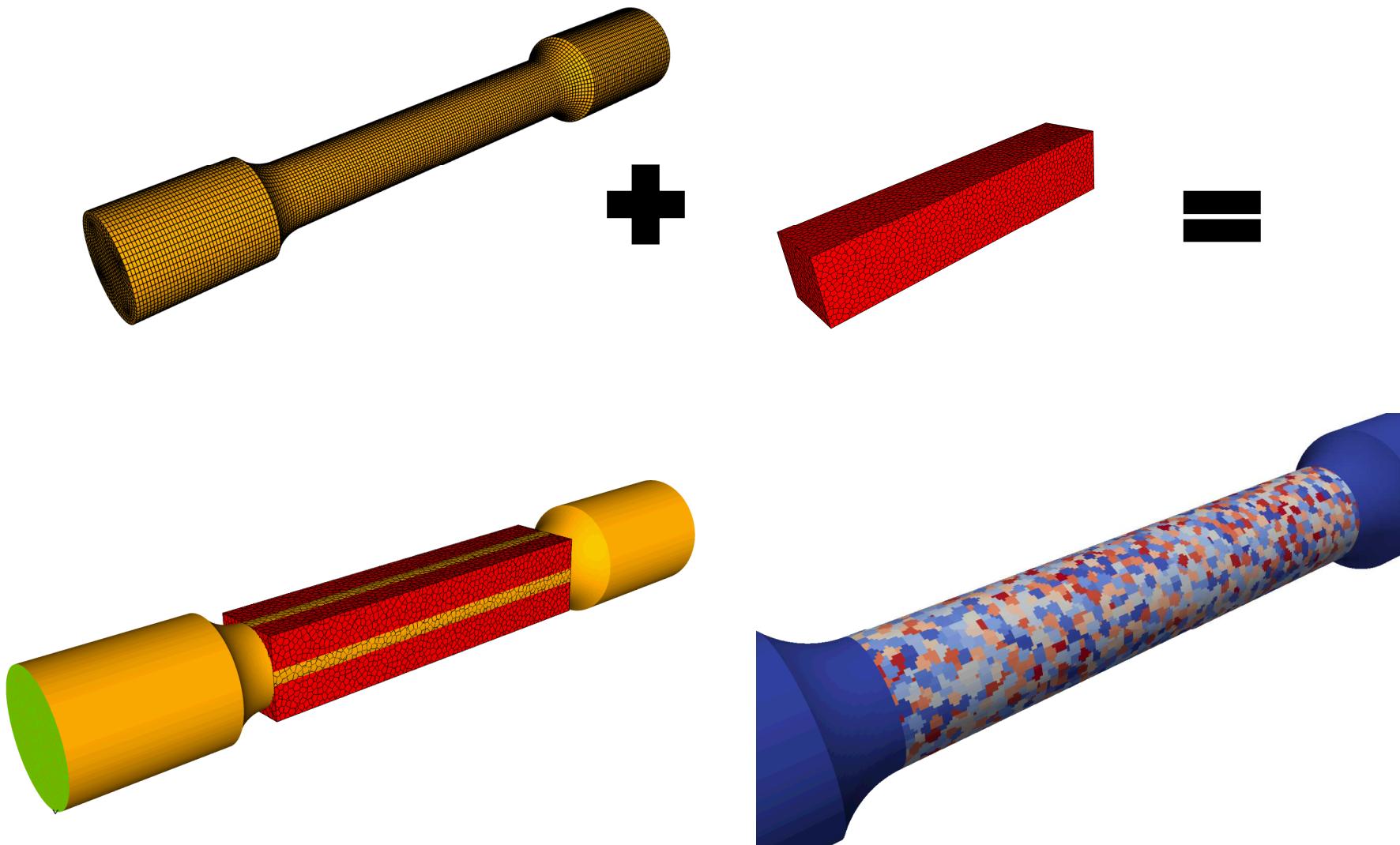
Y-Plane



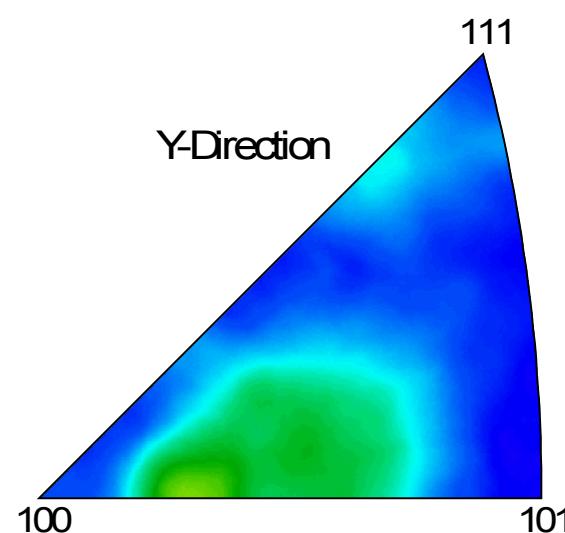
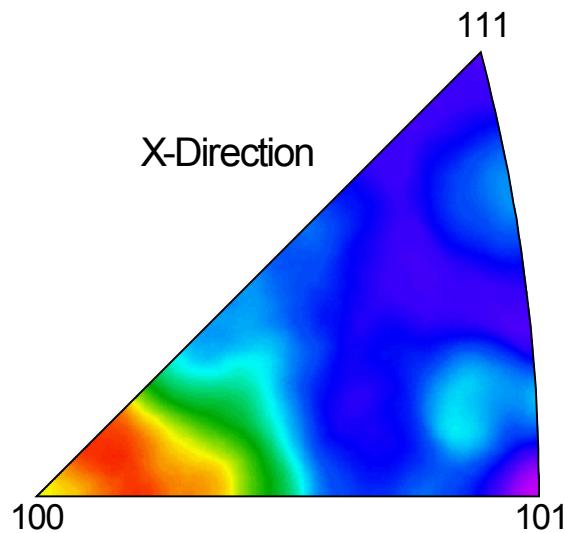
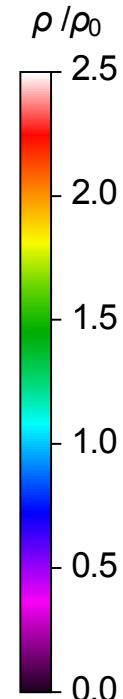
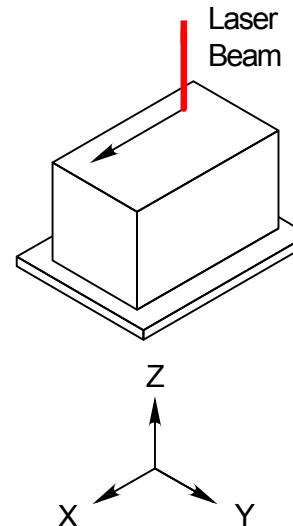
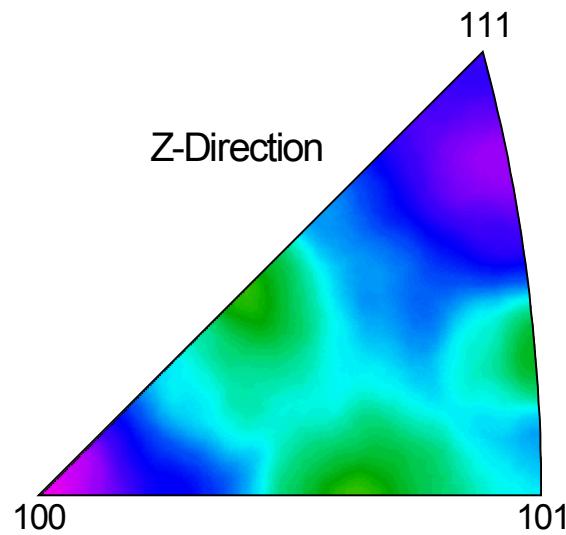
Z-Plane



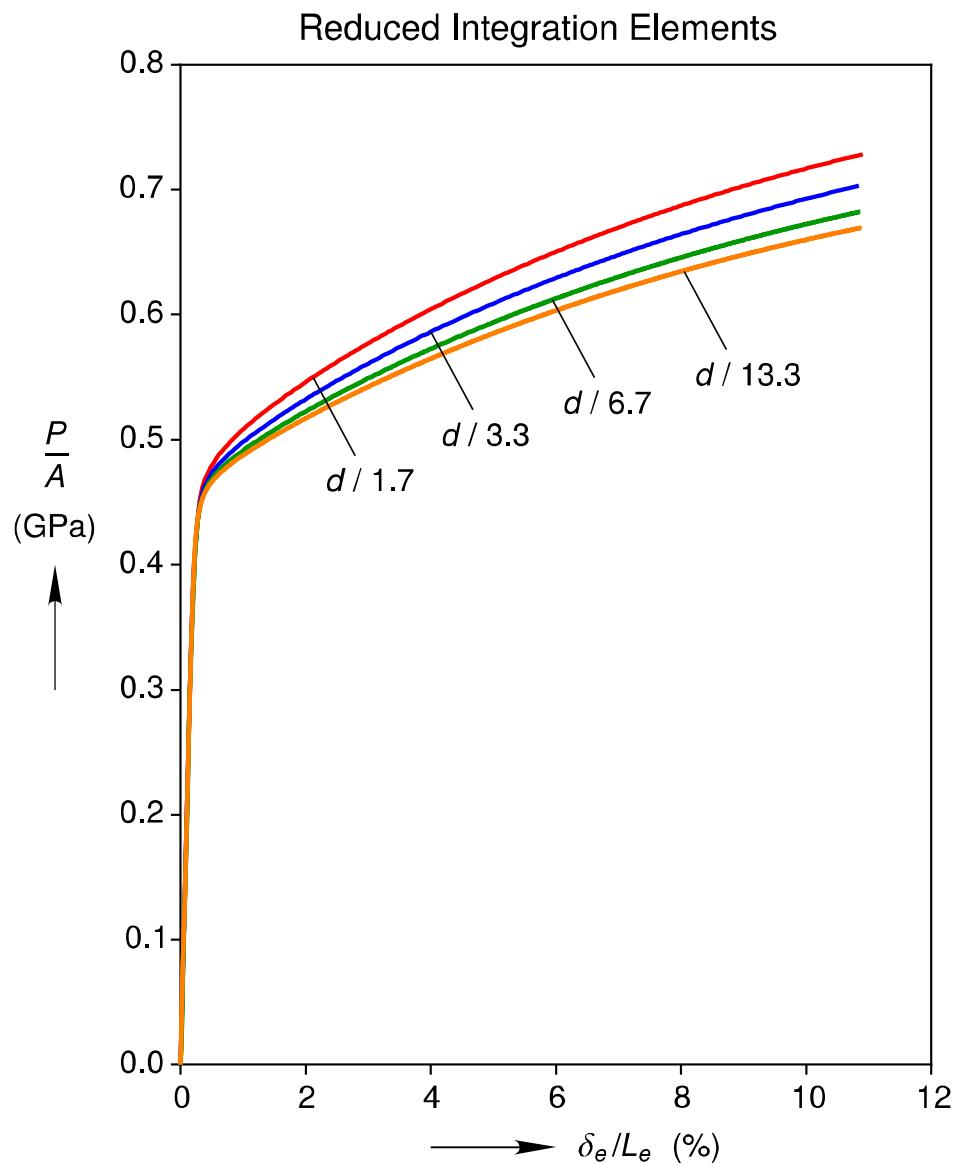
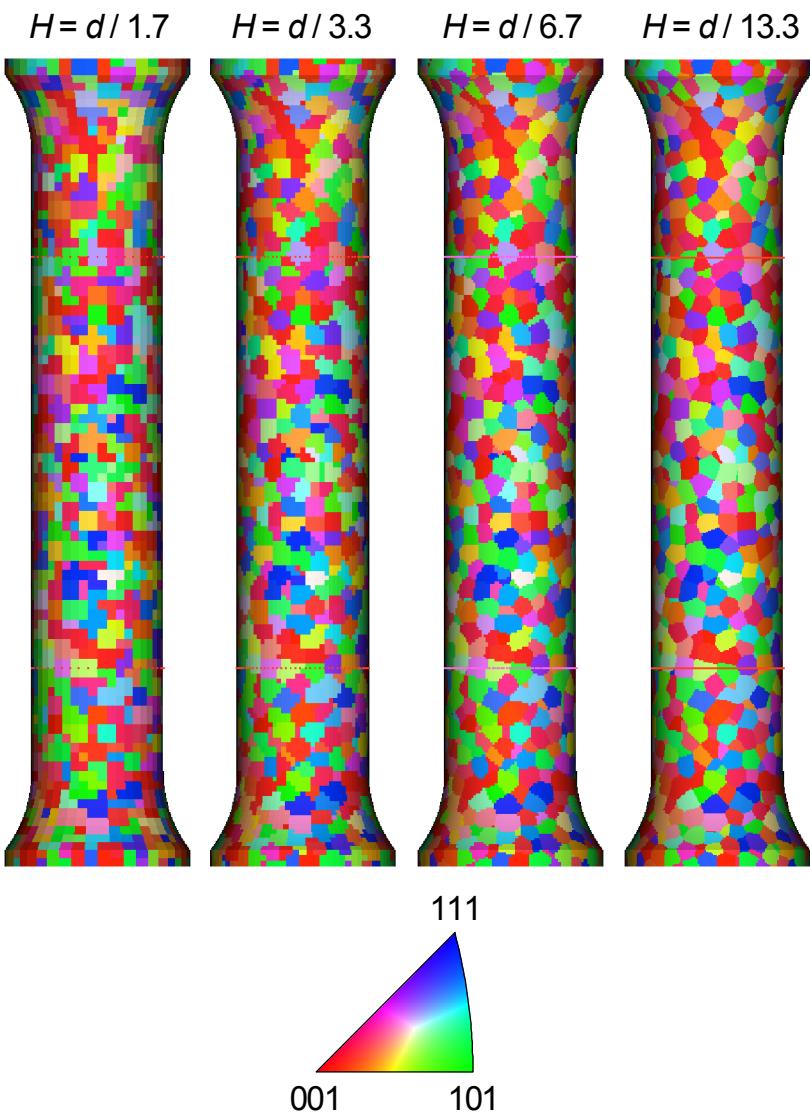
Voronoi Overlay on a Hexahedral Mesh



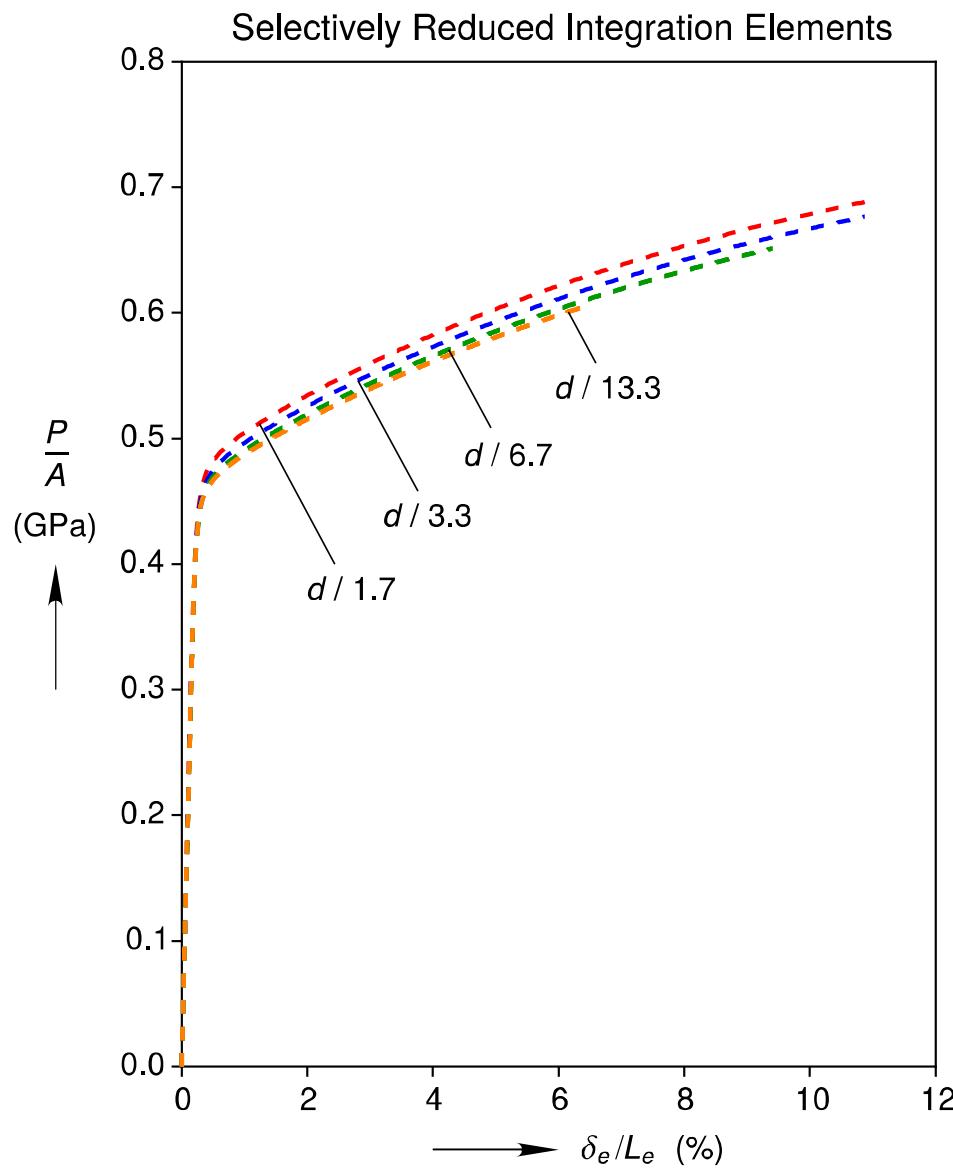
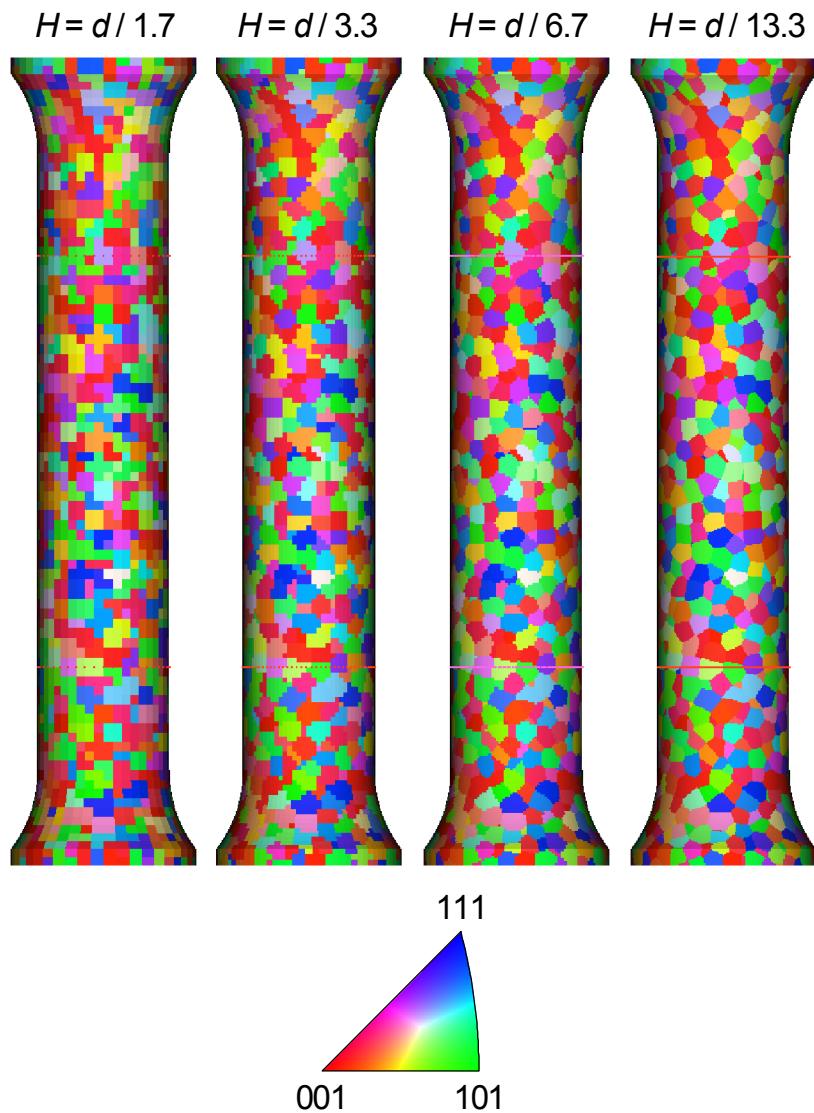
Inverse Pole Figures



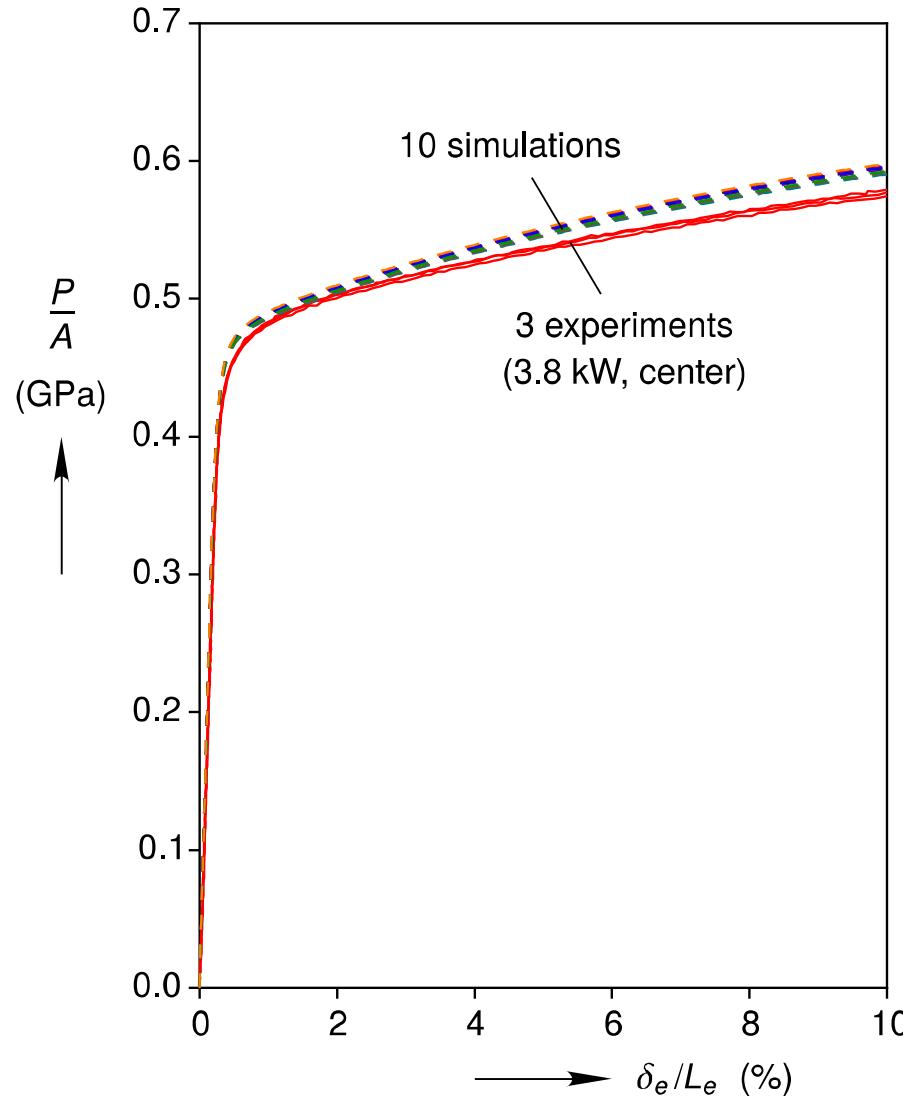
Mesh Convergence



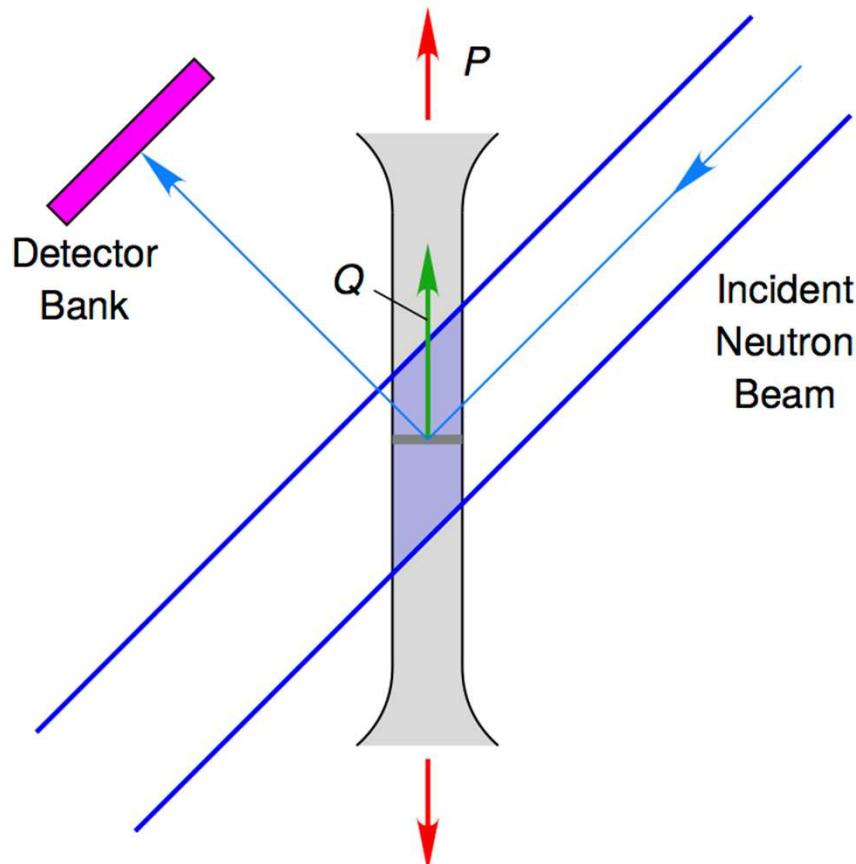
Mesh Convergence



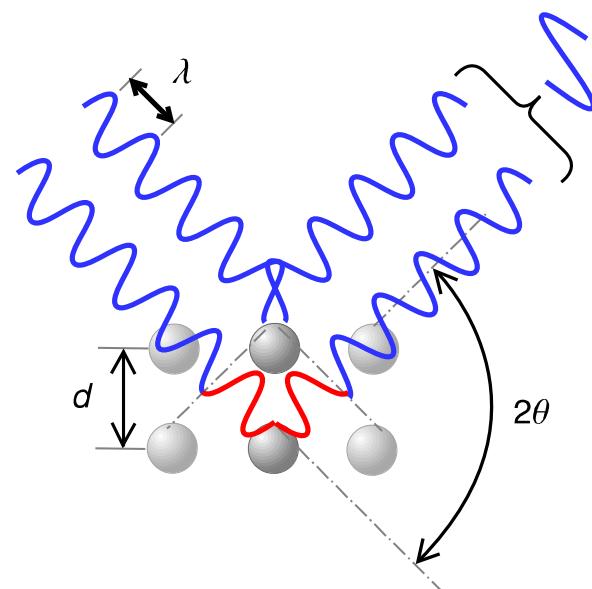
Calibration and Statistical Consistency



Neutron Diffraction



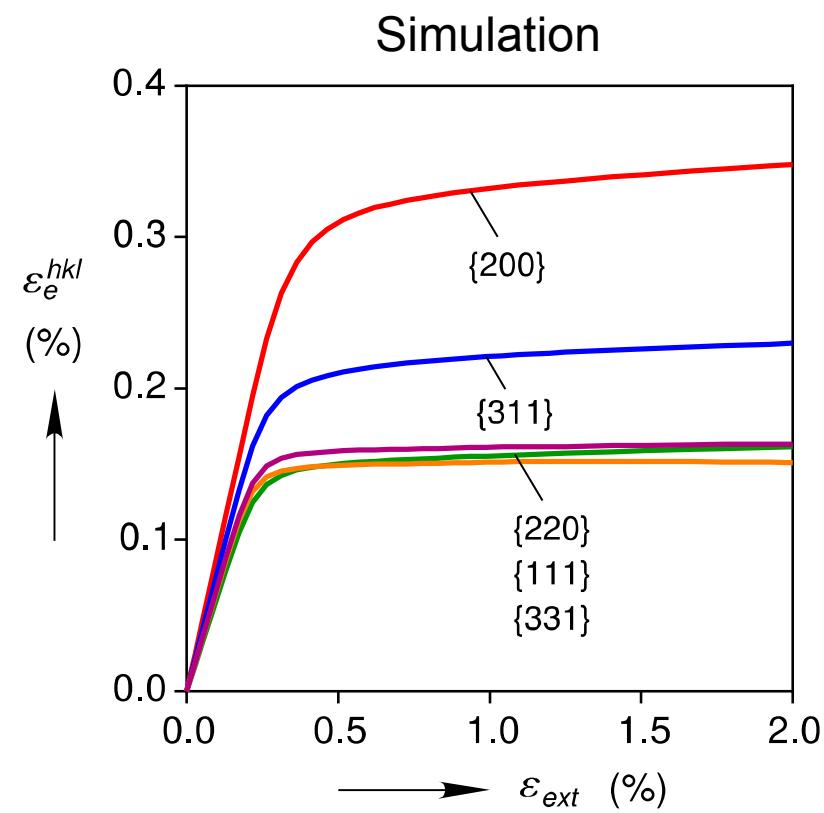
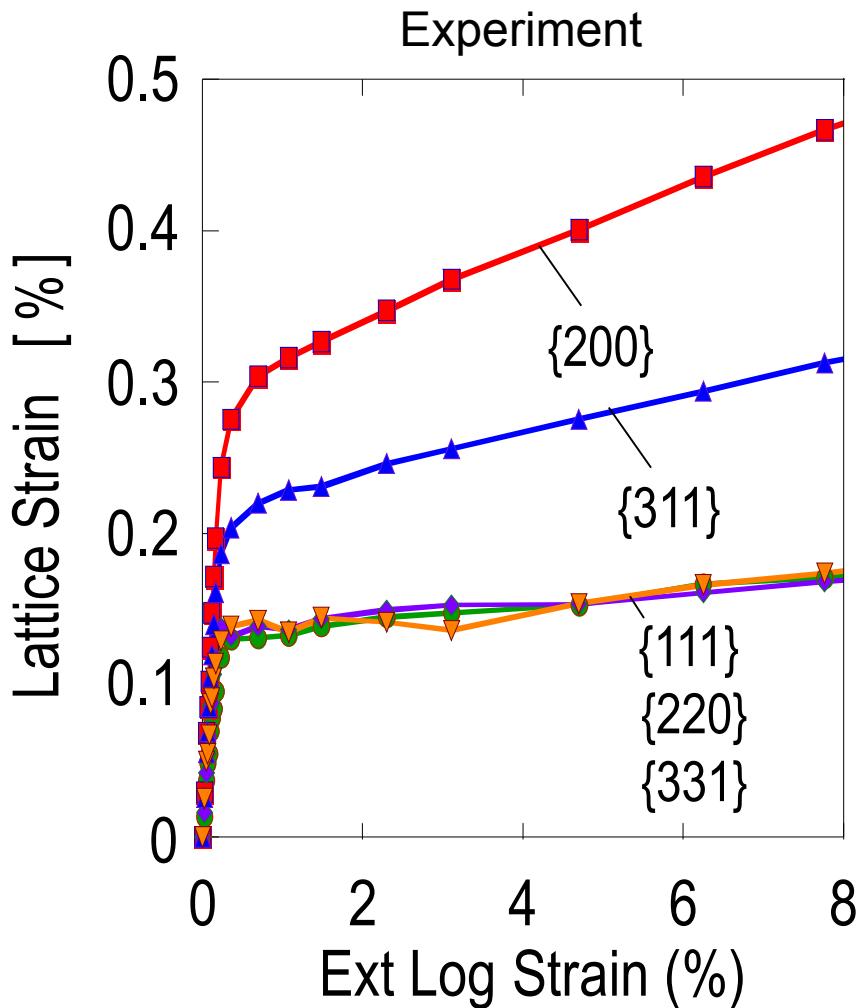
Bragg's Law



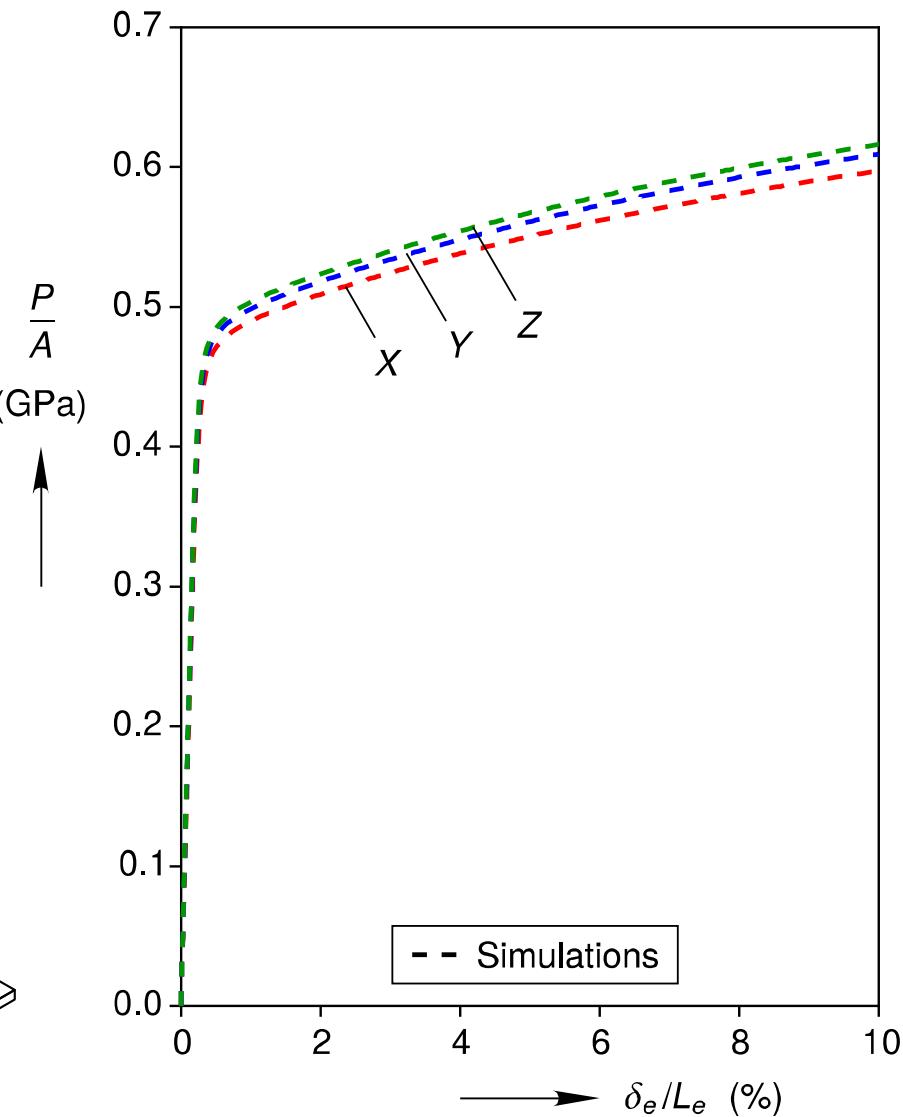
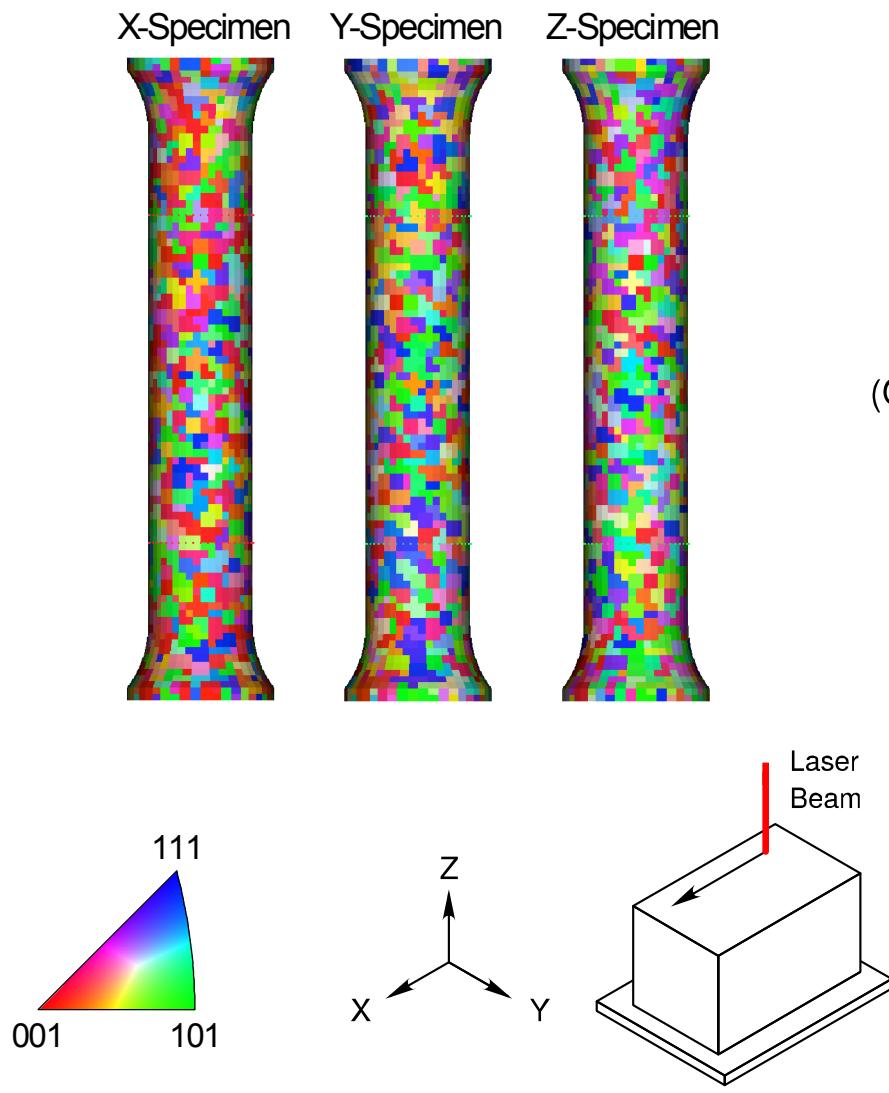
$$2d \sin \theta = n \lambda$$

http://en.wikipedia.org/wiki/Bragg's_law (modified)

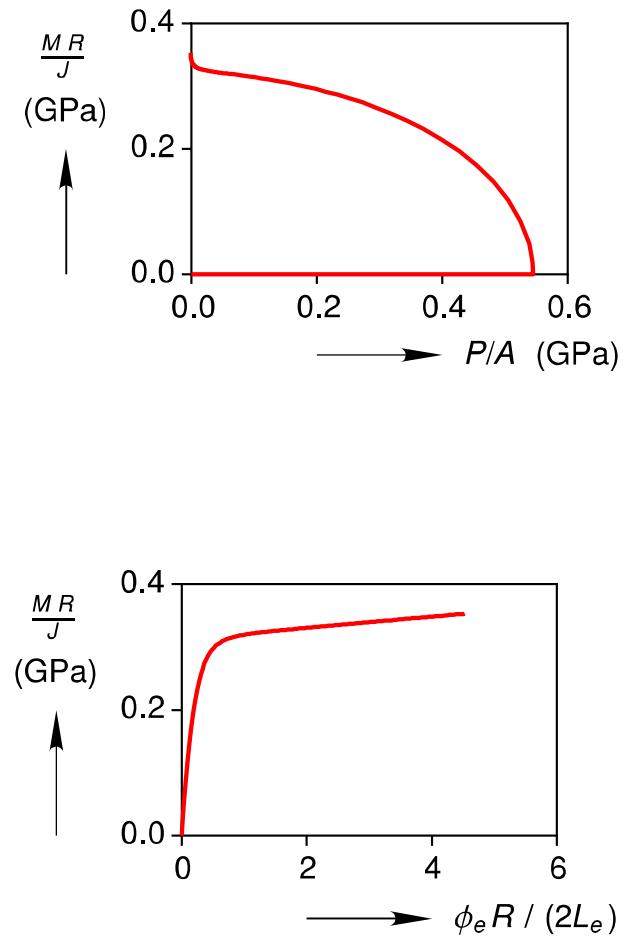
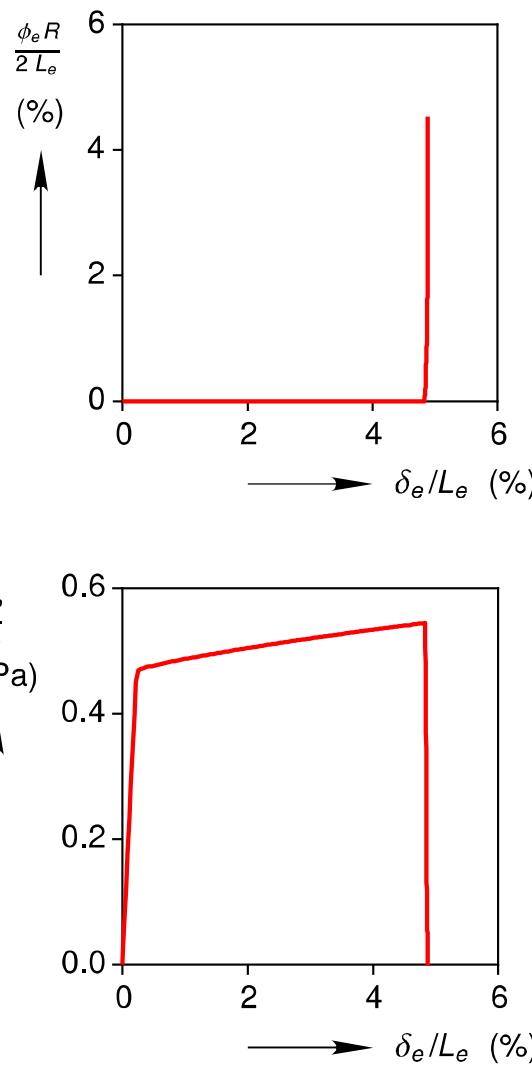
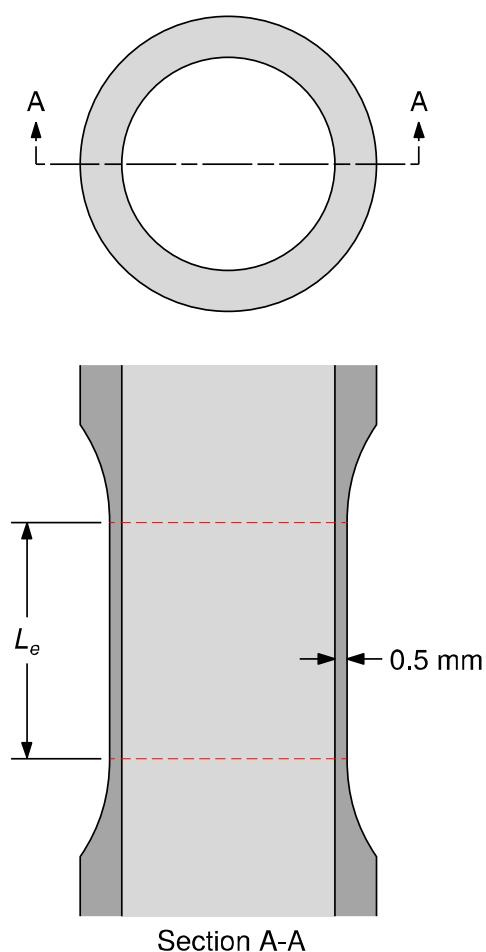
Lattice Strains



Anisotropy Predictions



Validation Simulations

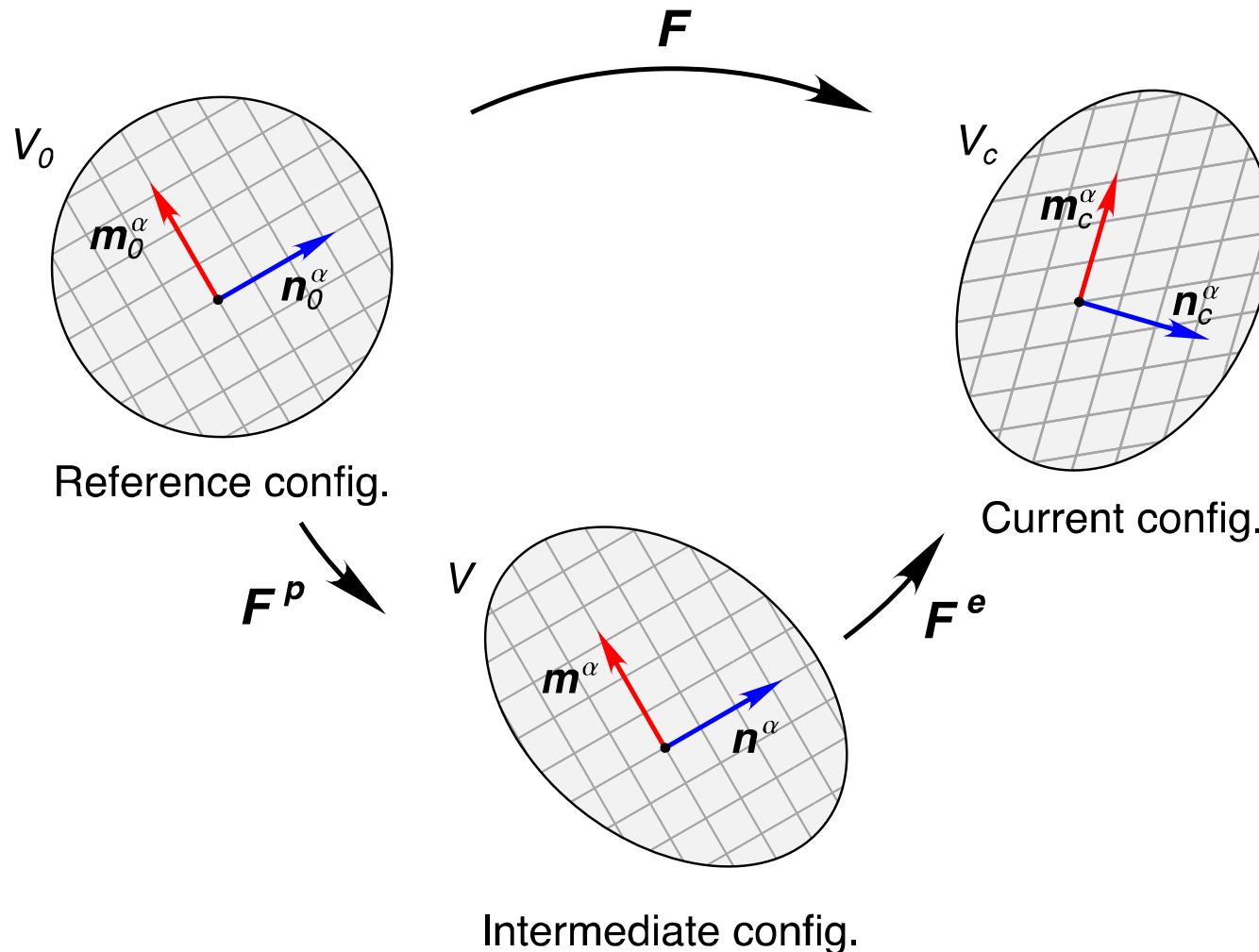


Summary

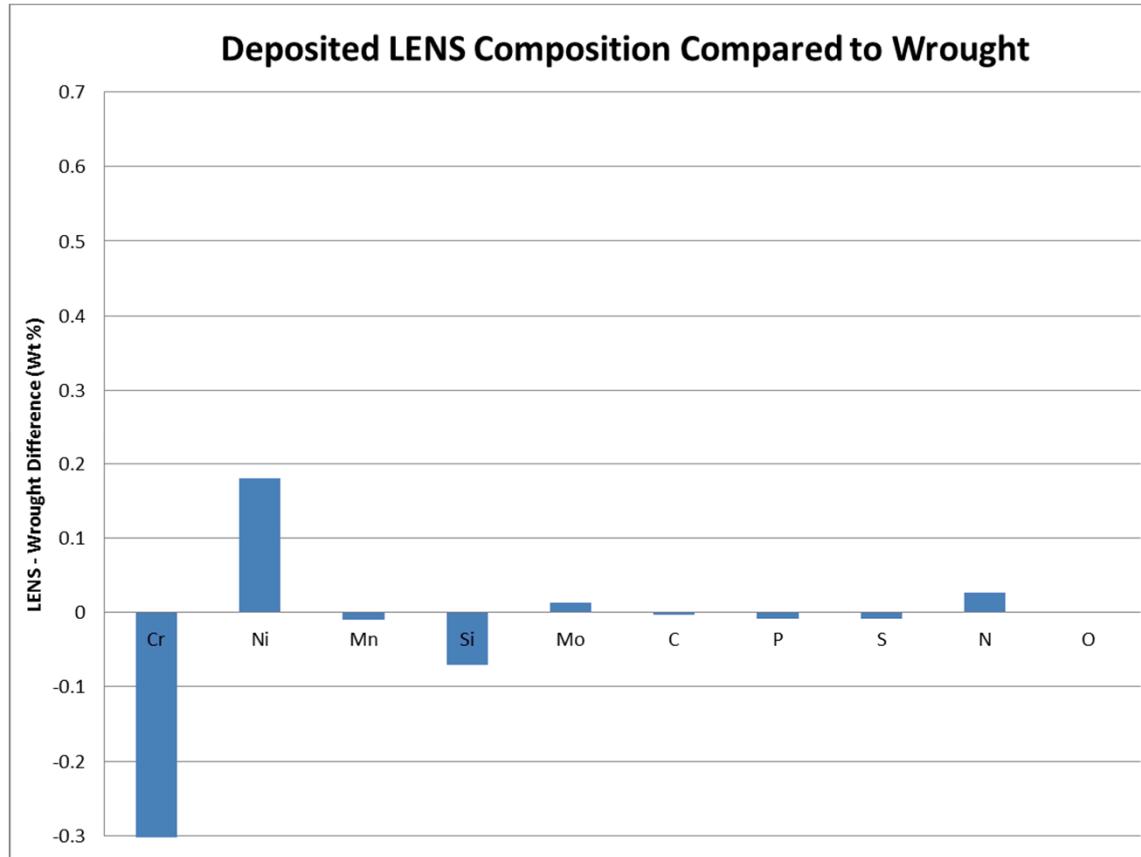
- Experiments
 - Additively manufactured 304L is 50-100% stronger and less ductile than comparable wrought 304L
- Simulations
 - Synthetic microstructures generated
 - Mesh convergence is difficult to obtain
 - Qualitatively validated the model against neutron diffraction measurements
 - Predicted mild anisotropy in yield and hardening

Questions?

Crystal Plasticity

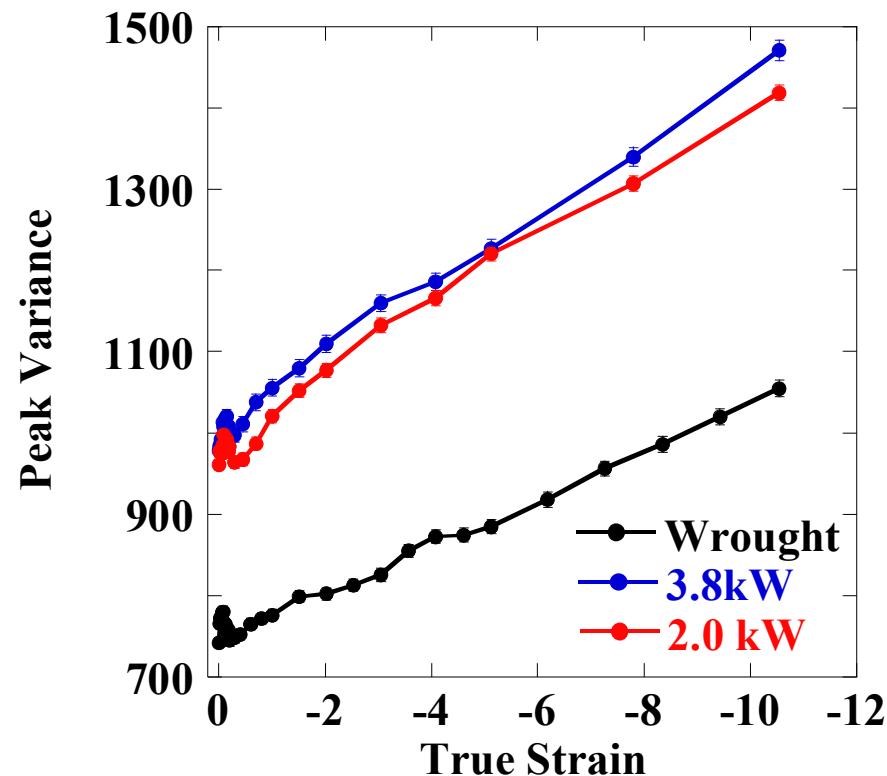
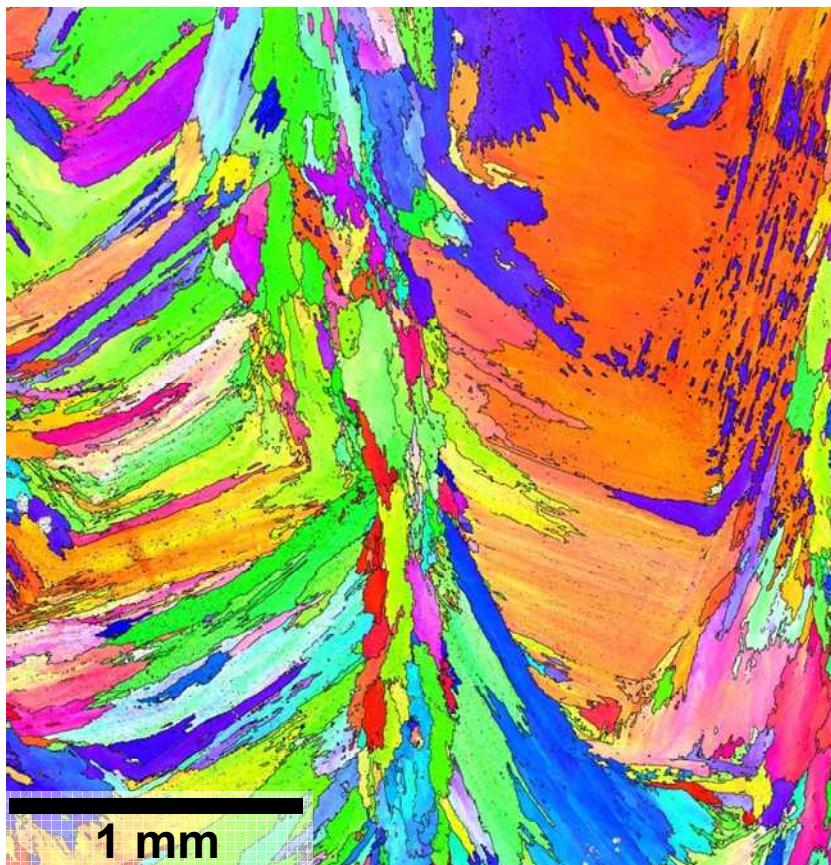


Composition Differences



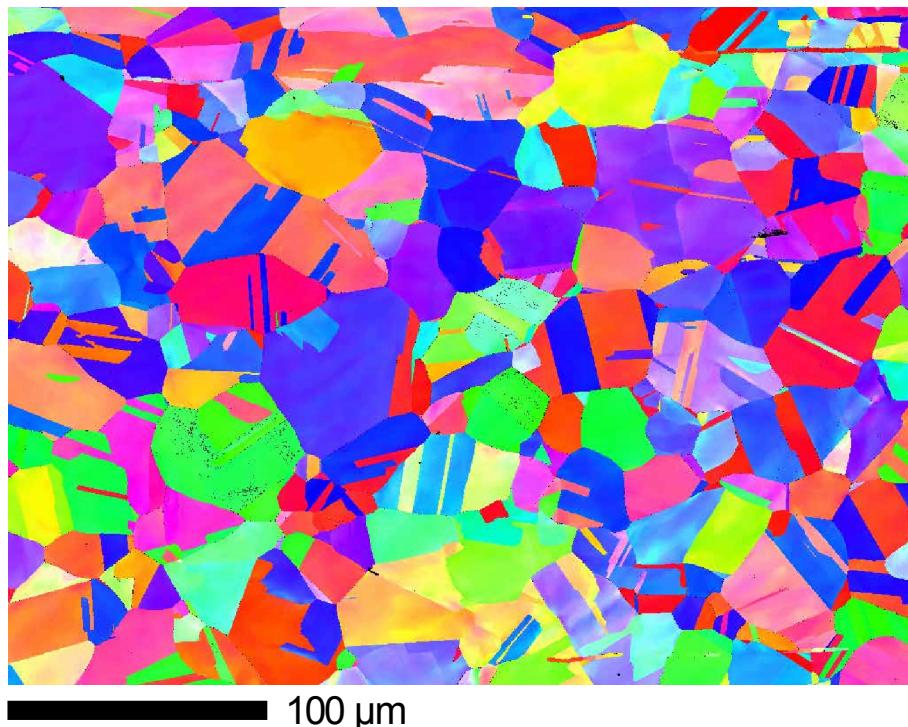
	Fe	Cr	Ni	Mn	Si	Mo	N	Co	P	S	C	O
Wrought	bal (68.2)	19.5	10.1	1.5	0.58	0.027	0.049	0.029	0.015	0.015	0.013	0
LENS Deposited	bal (68.8)	18.8	10.28	1.49	0.51	0.04	0.075	0	0.007	0.007	0.01	0.023

Indicators of Dislocation Density

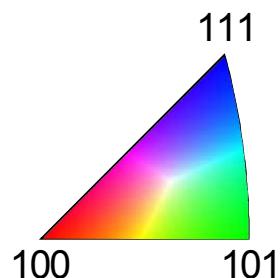
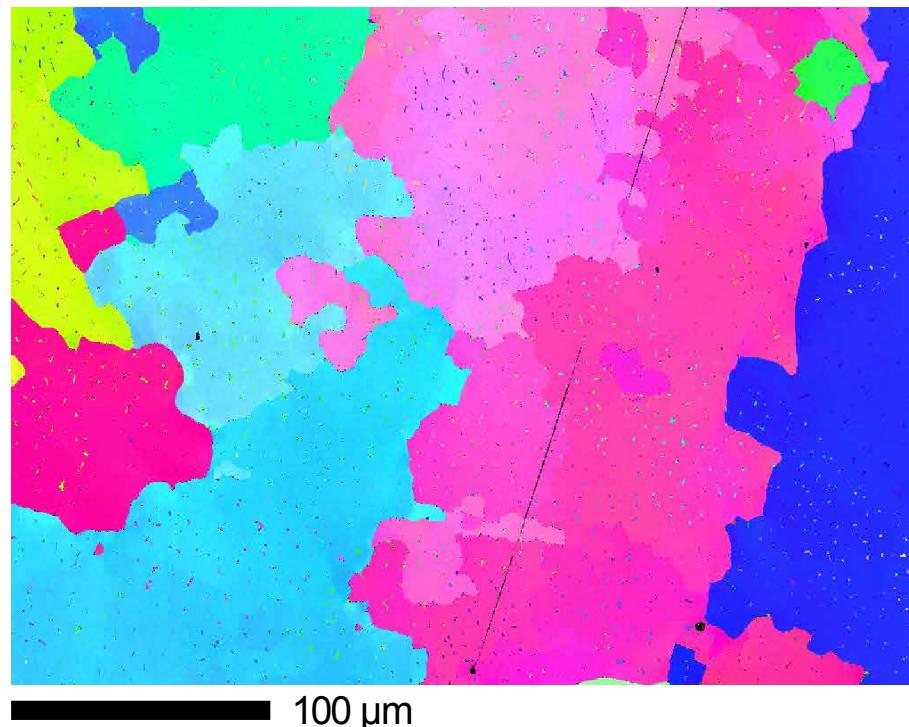


Ferrite / Martensite

Wrought
1.2 % Ferrite/Martensite (Ferrite Scope)

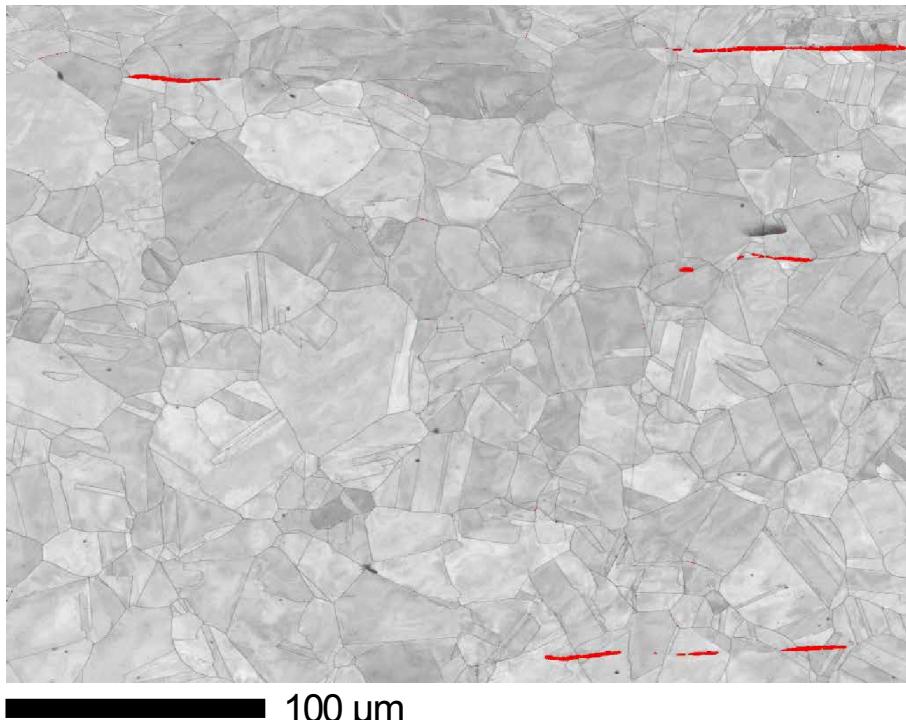


LENS 2 kW
2.3 % Ferrite/Martensite (Ferrite Scope)

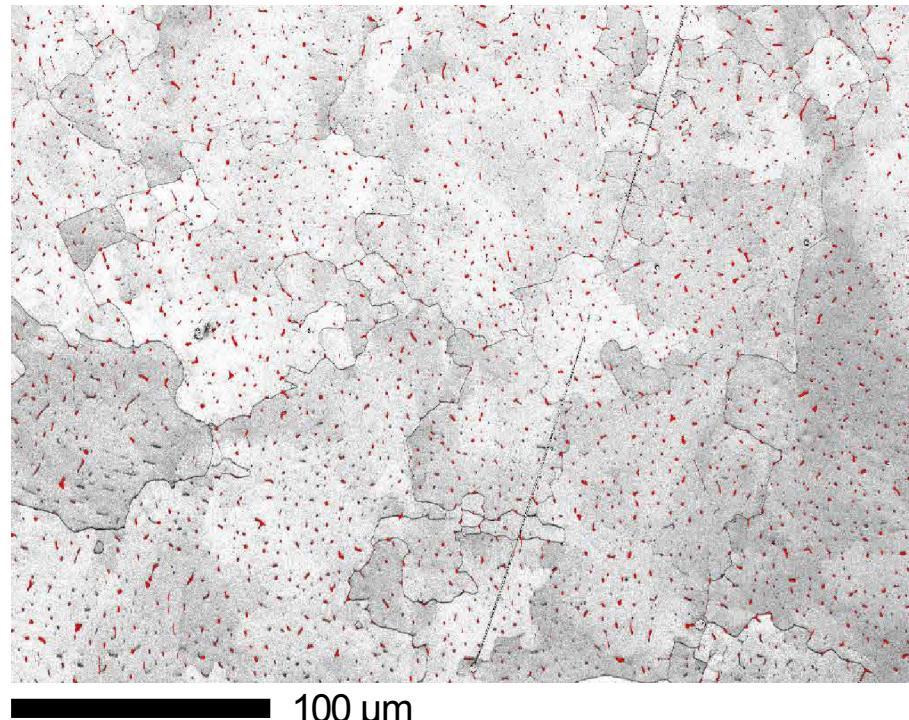


Ferrite / Martensite

Wrought
1.2 % Ferrite/Martensite (Ferrite Scope)



LENS 2 kW
2.3 % Ferrite/Martensite (Ferrite Scope)

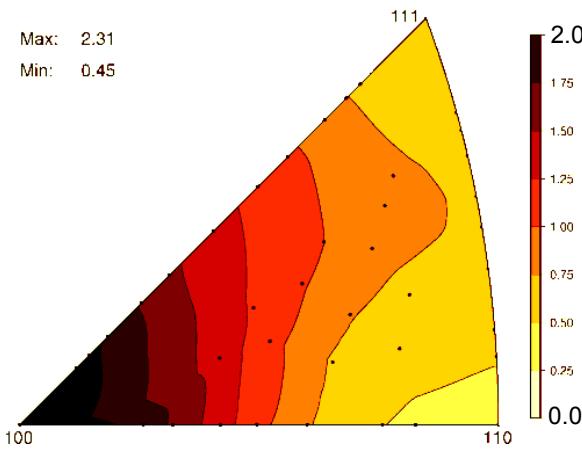


Gray = Austenite, Red = Ferrite

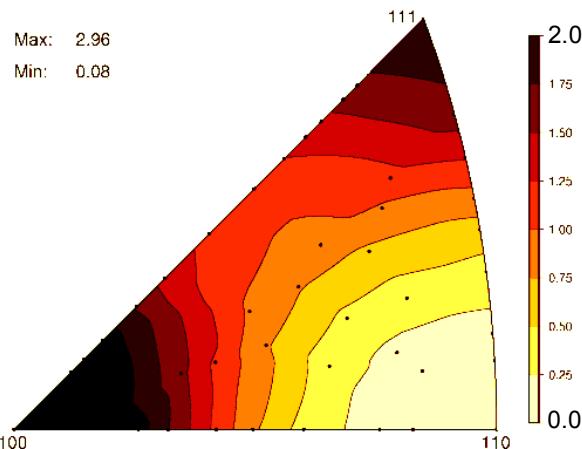
Deformation Induced Texture

Experiment

0 % Strain

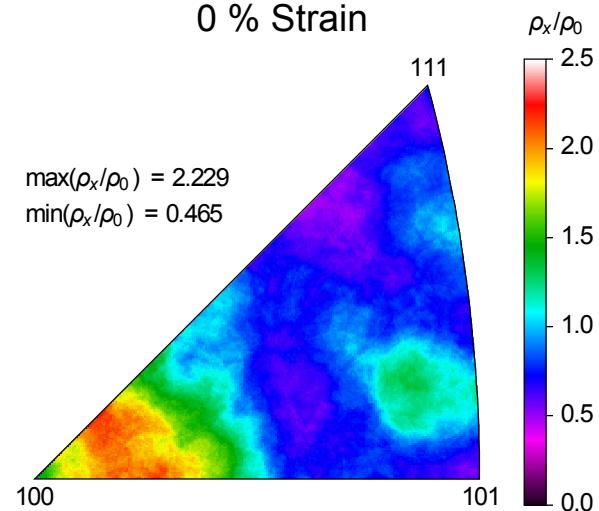


32 % Strain

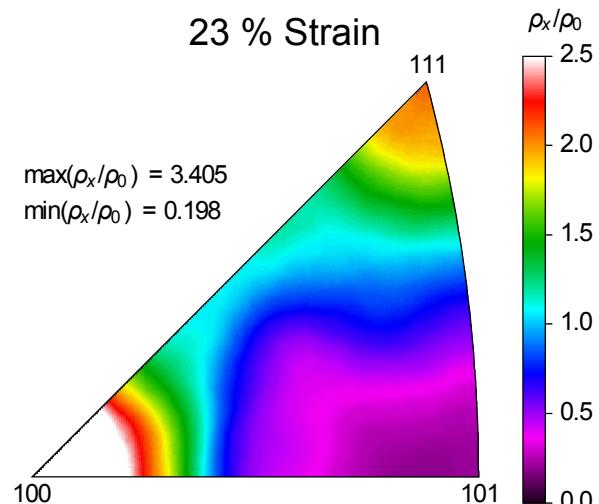


Simulations

0 % Strain



23 % Strain



Modeling Strategy

- Homogeneous Plasticity Models
 - Isotropic, Von Mises
 - Anisotropic, Hill
- Crystal Plasticity Finite Element Models
 - Textured microstructure with equiaxed grains of uniform size
 - Textured microstructure with approximate grain morphology
- Other material models?