



# Leveraging Flexibility in Energy Minimization Algebraic Multigrid

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# Outline

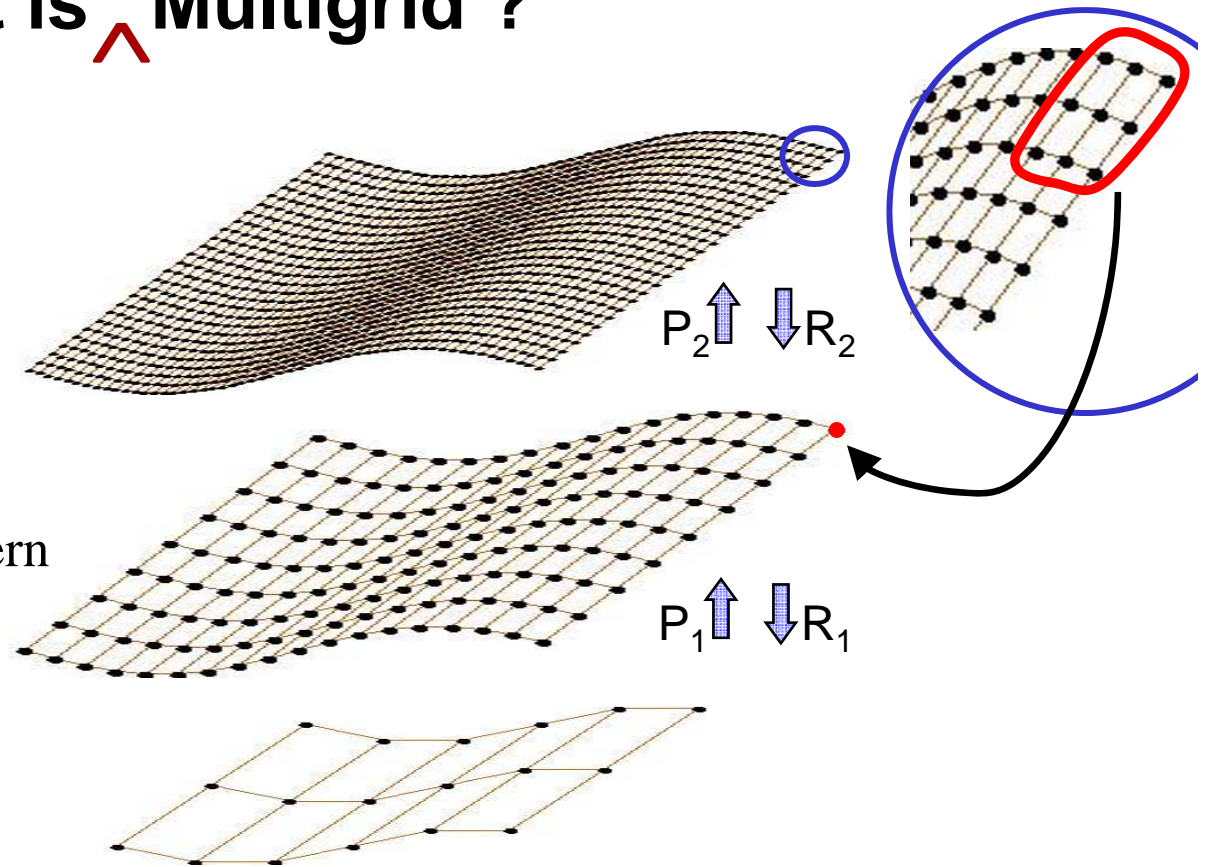
- Energy minimization AMG
  - Motivation: arbitrary coarsening, flexible coarse basis function support, accurate interpolation of arbitrary important modes, flexible choice of norm for minimization & search space
  - $A \neq A^T$  & Krylov Methods
- Leveraging flexibility of energy minimization AMG
  - weakly constrained & over-constrained
  - anisotropic elasticity
    - Flexible sparsity pattern & accurate rigid body mode interpolation
  - extended finite elements & fracture
    - Flexible pattern, flexible norm choice



# *Algebraic* What is <sup>^</sup>Multigrid ?

Solve  $A_3 u_3 = f_3$

- Construct Graph & Coarsen
- Determine  $P_i$  &  $R_i$  sparsity pattern
- Determine  $P_i$  &  $R_i$ 's coefs
- Project:  $A_i = R_i A_{i+1} P_i$



$$\min_{e_H} \|e - Pe_H\|_2^2 \leq \beta \|e\|_A^2$$

$$\|Se\|_A^2 \leq \|e\|_A^2 - \alpha \|e\|_{A^2}^2$$

$\Rightarrow$

$$\|ST_{2-level}\|_A \leq \sqrt{1 - \frac{\alpha}{\beta}}$$



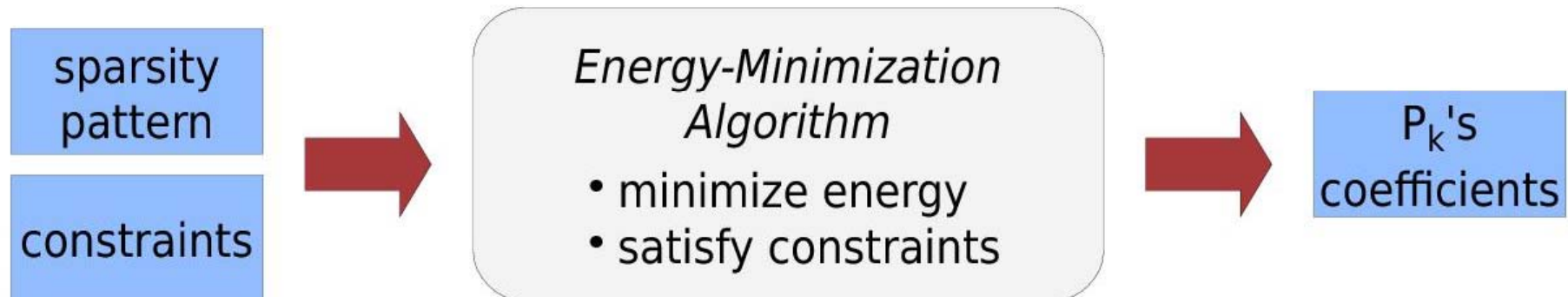
# Algorithm

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$\min \sum \|p_i\|_e^2$  where  $p_i$  gives the  $i^{\text{th}}$  column of a prolongator

Idea: construct the grid transfer operator  $P$  by minimizing the energy of each column, while enforcing constraints (sparsity pattern and specified modes).

Input / output of energy-minimization algorithm:



Advantages:

- Flexibility (input):
  - arbitrary coarsening
  - accept any sparsity pattern (arbitrary basis function support)
  - enforce constraints: important modes requiring accurate interpolation
  - choice of norm for minimization and search space
- Robustness



# Energy-Minimization

Find  $P = [p_1 \ p_2 \ \cdots \ p_m]$  that

minimizes  $\sum_i \|p_i\|_e$  in some space subject to  $X \begin{pmatrix} p_1 \\ \vdots \\ p_m \end{pmatrix} = g$

if  $e = A \Rightarrow$

$$\hat{A} \left( \begin{array}{c} A \\ A \\ A \\ A \\ X \end{array} \right) X^T \begin{pmatrix} p_1 \\ p_2 \\ p_3 \\ p_4 \\ \lambda \end{pmatrix} = \begin{pmatrix} 0 \\ g \end{pmatrix}$$

Constraints enforce exact interpolation of null space, e.g.  $A B = 0 \rightarrow B \in \text{Range}(P)$

$\gg P \ll$

“Solve”  $AP = 0$

- 1) with minimization algorithm
- 2) in space satisfying constraints

$$A (P_0 - \Delta P) = 0 \text{ with } X \gg P_0 \ll = g$$

$$X \gg \Delta P \ll = 0$$

$$Q \hat{A} \gg P_0 \ll, (Q \hat{A})^2 \gg P_0 \ll, \dots$$

$$Q = (I - X^T (X X^T)^{-1} X)$$



# CG minimization

Lemma: Let  $A$  be SPD and apply CG to

$$Q^T A Q \gg \Delta P \ll = Q^T A Q \gg P_0 \ll$$

with 0 initial guess, then CG computes

$$\gg \Delta P_i \ll = \arg \min_{\gg \Delta P_i \ll \in \mathcal{K}_i} \|\gg P_i \ll\|_{\hat{A}}^2 \text{ where } P_i = P_0 - \Delta P_i$$

*Proof.*

$$\begin{aligned} \gg \Delta P_i \ll &= \arg \min_{\gg \Delta P_i \ll \in \mathcal{K}_i} \|\gg P_* \ll - \gg \Delta P_i \ll\|_{Q^T A Q}^2 \\ &= \arg \min_{\gg \Delta P_i \ll \in \mathcal{K}_i} \|\gg P_* \ll\|_{Q^T A Q}^2 + \|\gg \Delta P_i \ll\|_{Q^T A Q}^2 - 2 \langle \gg \Delta P_i \ll, \gg P_0 \ll \rangle_{\hat{A}} \\ &= \arg \min_{\gg \Delta P_i \ll \in \mathcal{K}_i} \|\gg P_0 \ll\|_{Q^T A Q}^2 + \|\gg \Delta P_i \ll\|_{Q^T A Q}^2 - 2 \langle \gg \Delta P_i \ll, \gg P_0 \ll \rangle_{\hat{A}} \\ &= \arg \min_{\gg \Delta P_i \ll \in \mathcal{K}_i} \|\gg P_0 \ll - \gg \Delta P_i \ll\|_{\hat{A}}^2 \end{aligned}$$

*Corollary: CG solution is unique*



# GMRES minimization

Lemma: Let  $A$  be nonsingular and apply GMRES to

$$Q \hat{A} \gg \Delta P \ll = Q \hat{A} \gg P_0 \ll \quad (*)$$

with 0 initial guess, then GMRES computes

$$\gg \Delta P_i \ll = \arg \min_{\gg \Delta P_i \ll \in \mathcal{K}_i} \left\| \gg P_i \ll \right\|_{\hat{A}^T Q \hat{A}} \text{ where } P_i = P_0 - \Delta P_i$$

which is unique.

*Proof.*

Define  $S$  and  $S_\perp$  such that

$$QS = 0, \quad S_\perp S_\perp^T = Q, \quad S_\perp^T S_\perp = I, \quad S^T S = I, \quad S^T S_\perp = I$$

Use properties of GMRES applied to nonsingular system

$$S_\perp^T \hat{A} S_\perp y = S_\perp^T \hat{A} \gg P_0 \ll \quad (**)$$

Pre-multiplication of  $(**)$  & associated Krylov space by  $S_\perp$  reveal equivalence with  $(*)$ .

$$\left\| \gg \Delta P_i \ll \right\|_Q$$





## $\mathbf{A} \neq \mathbf{A}^T$ (weakly constrained)

- Use GMRES to “solve”  $\mathbf{A}\mathbf{P} = \mathbf{0}$  with only constraint  $\mathbf{P} = [\mathbf{P}_f \ \mathbf{I}_c]^T$
- Use GMRES to “solve”  $\mathbf{R}\mathbf{A} = \mathbf{0}$  with only constraint  $\mathbf{R} = [\mathbf{R}_f \ \mathbf{I}_c]$

Consider

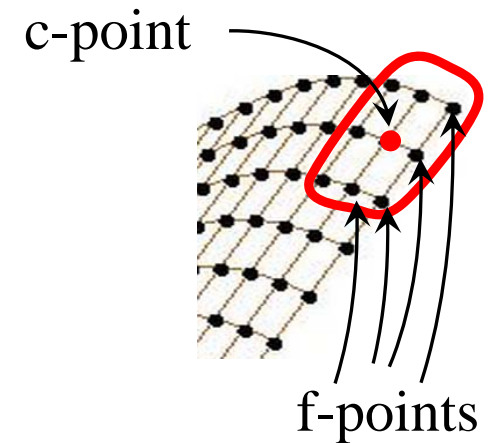
$$\begin{pmatrix} \mathbf{A}_{ff} & \mathbf{A}_{fc} \\ \mathbf{A}_{cf} & \mathbf{A}_{cc} \end{pmatrix} \begin{pmatrix} \mathbf{u}_f \\ \mathbf{u}_c \end{pmatrix} = \begin{pmatrix} \mathbf{b}_f \\ \mathbf{b}_c \end{pmatrix}$$

Then

$$\underbrace{\begin{pmatrix} \mathbf{I}_f & \mathbf{0} \\ \mathbf{R} & \end{pmatrix} \begin{pmatrix} \mathbf{A}_{ff} & \mathbf{A}_{fc} \\ \mathbf{A}_{cf} & \mathbf{A}_{cc} \end{pmatrix} \begin{pmatrix} \mathbf{I}_f & \mathbf{P} \\ \mathbf{0} & \end{pmatrix}}_{\begin{pmatrix} \mathbf{A}_{ff} & \mathbf{E}_{fc} \\ \mathbf{E}_{cf} & \mathbf{A}_H \end{pmatrix}} \begin{pmatrix} \mathbf{y}_f \\ \mathbf{y}_c \end{pmatrix} = \begin{pmatrix} \mathbf{b}_f \\ \mathbf{R}\mathbf{b} \end{pmatrix}$$

Decouples if  $\mathbf{E}_{fc} = \begin{pmatrix} \mathbf{A}_{ff} & \mathbf{A}_{fc} \end{pmatrix} \mathbf{P}$  &  $\mathbf{E}_{cf} = \mathbf{R} \begin{pmatrix} \mathbf{A}_{ff} \\ \mathbf{A}_{cf} \end{pmatrix}$  are 0.

$= \mathbf{Q} \gg \mathbf{A}\mathbf{P} \ll$   $= \gg \mathbf{R}\mathbf{A} \ll \mathbf{Q}$







# Exploiting Flexibility

Coarsening, sparsity pattern,  $p_{ij}$  choice are often tied together within many **AMG methods**

Example: smoothed aggregation

1) **Aggregate:**  $\mathcal{A}_i \cup \mathcal{A}_j = \{1, \dots, |V|\}$ ,  $\mathcal{A}_i \cap \mathcal{A}_j = \emptyset$ ,  $\text{diam}(\mathcal{A}_i) \approx 3$

2)  $P_0 = \text{BlkDiag}(\mathcal{R}_i B) =$  
$$\begin{bmatrix} \mathcal{B}_1 & & \\ & \mathcal{B}_2 & \\ & & \ddots \end{bmatrix}$$
 Graph of  $\tilde{A}$

3)  $P = P_0 + \omega D^{-1} \tilde{A} P_0$

- $\text{ColDim}(B) = \text{ColDim}(\mathcal{B}_i)$
- sparsity pattern is  $|\tilde{A}| P_0$
- Should have  $\tilde{A} P_0 B_c = 0$  where  $B_c$  is coarse representation of  $B$  (modes requiring accurate interpolation)  
 $\Rightarrow \tilde{A} B = 0$  (as  $P_0 B_c = B$ )

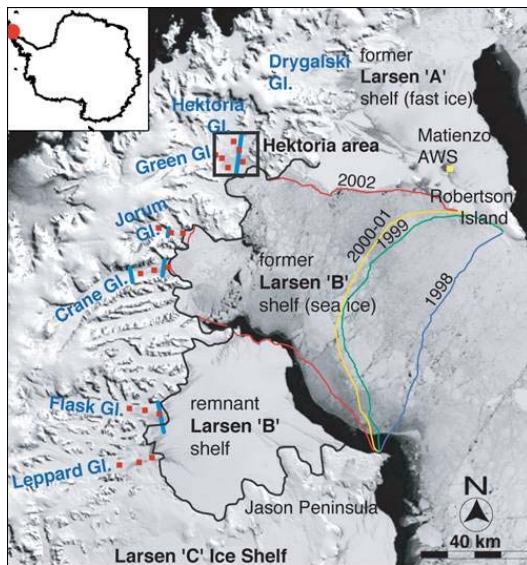
We will also exploit ability to change norm.

## Motivation: Importance of Ice Fracture

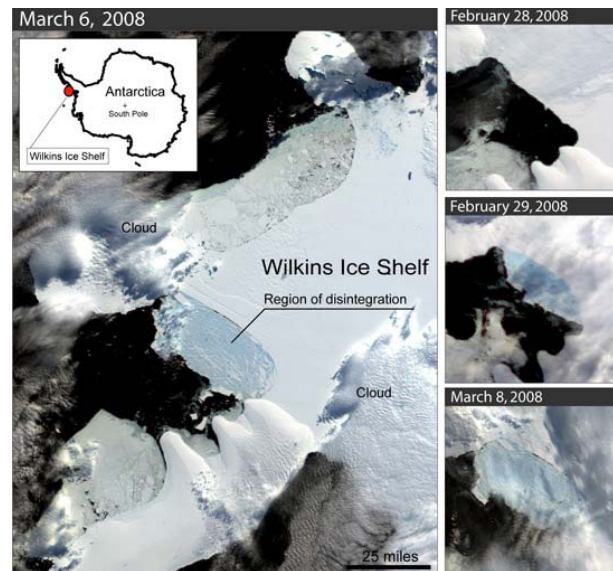
**Objective:** Employ parallel computers to study the fracture of land ice to better understand how it affects global climate change. In particular

- the collapse mechanism of ice shelves,
- the calving of large icebergs, and
- the role of fracture in the delivery of water to the bed of ice sheets.

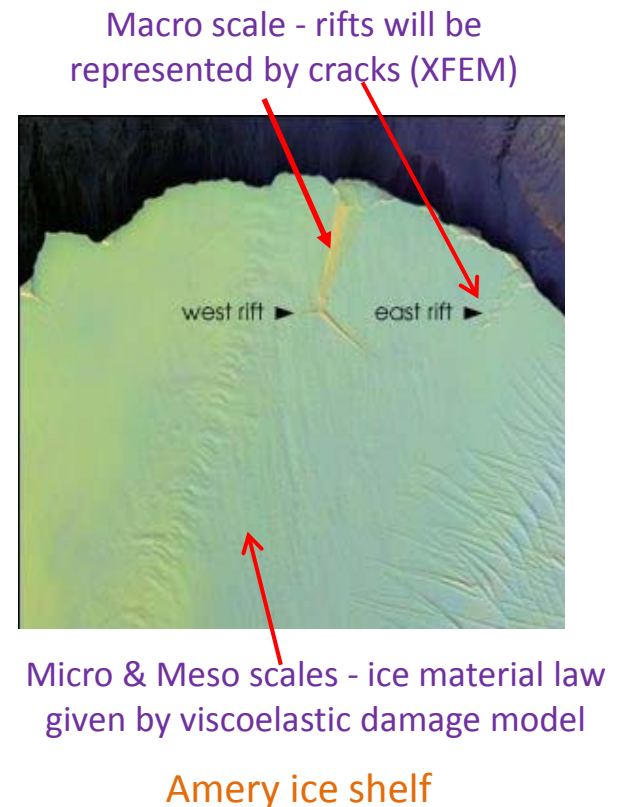
ice shelves in Antarctica



Larsen B diminishing shelf  
1998-2002

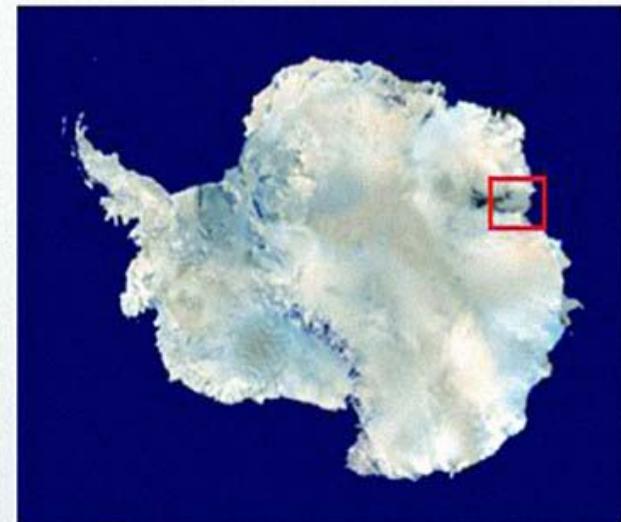
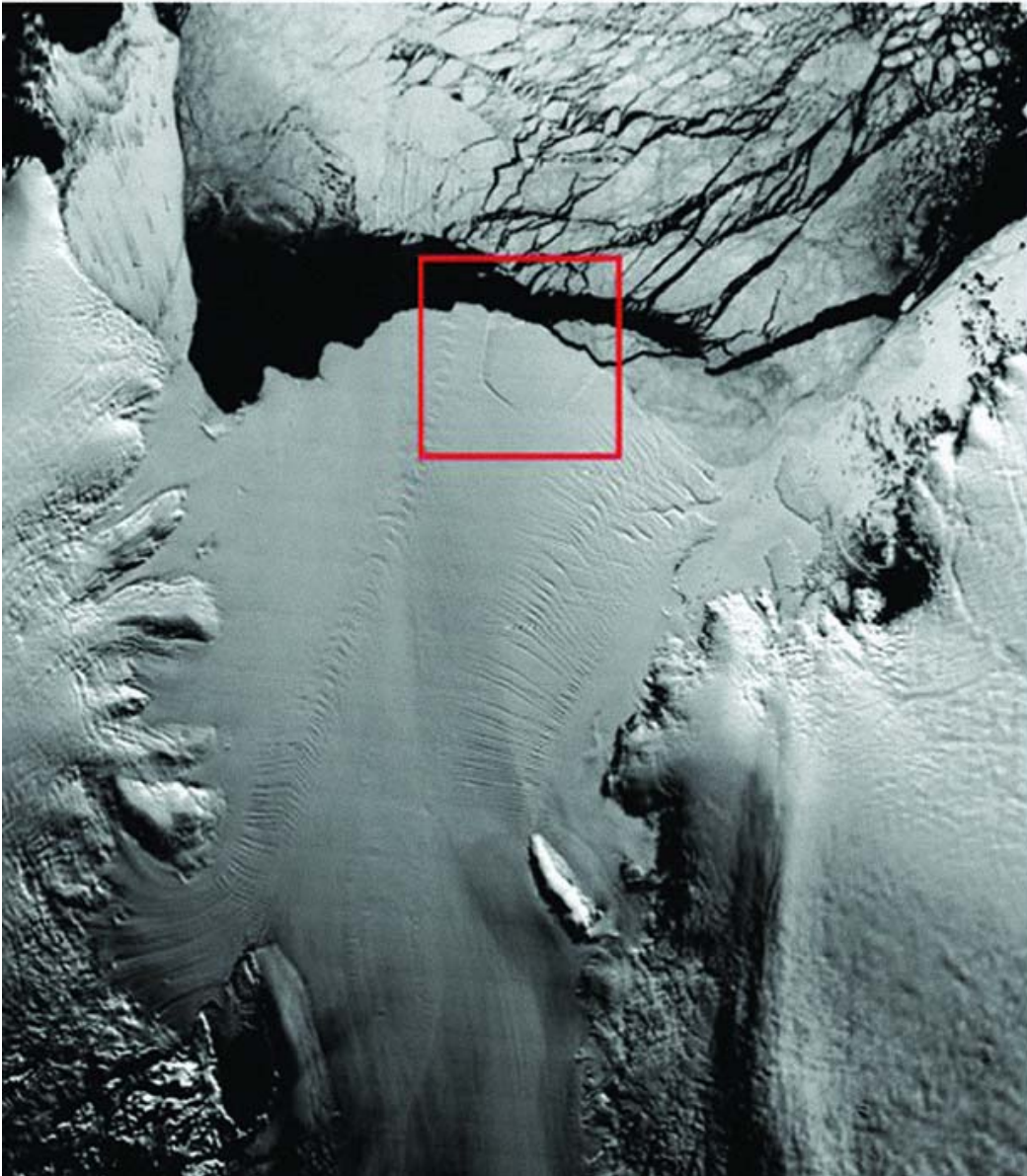


Wilkins ice shelf  
Recent 2008 collapse





## Amery ice shelf







# Computational Modeling of Fracture

## Classical FEM approach to fracture mechanics

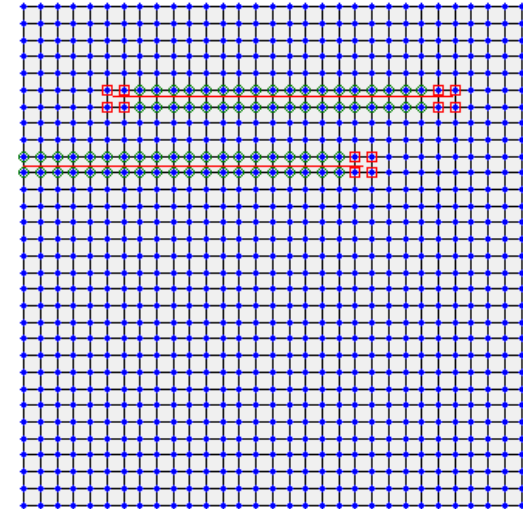
- Mesh conforms to crack boundaries
- Crack propagation → remeshing at each step
  - Requires double-nodes for crack opening and fine mesh for tip singularities

## eXtended Finite Element Method (XFEM)\*

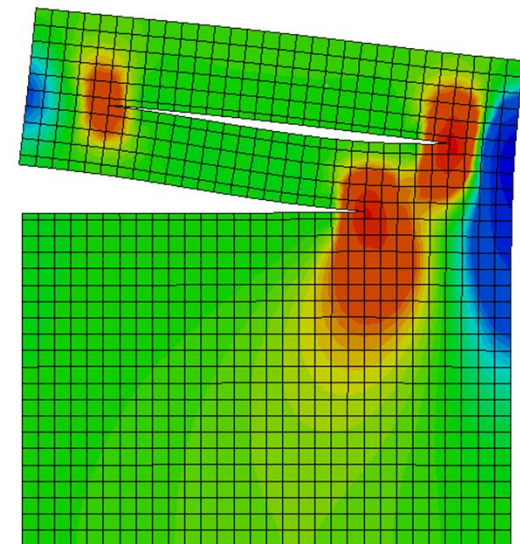
- Base mesh independent of crack geometry
- Crack propagation → adding “enriched” DOF with special basis functions to existing nodes
  - Crack geometry defined through levelsets
  - Discontinuities and singularities captured through special basis functions (enrichments)
  - Enrichments have local support

\* Belytschko & Black (1999), Moes et al. (1999)

XFEM mesh



Stresses in y direction when bottom edge fixed and uniform traction applied on top edge in y direction

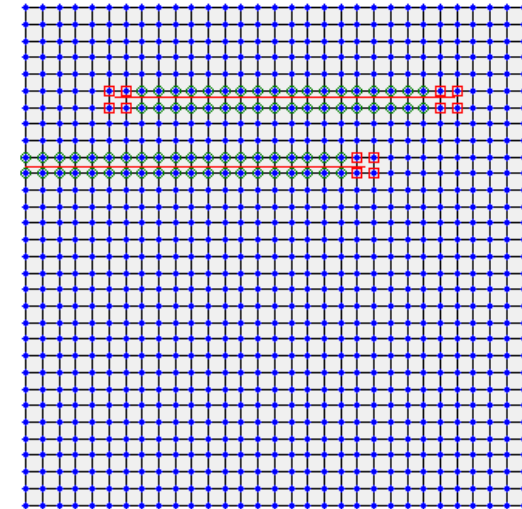




# XFEM Formulation

**Displacement trial function (shifted basis form.):**

$$\begin{aligned}
 u^h(\mathbf{x}) = & \sum_{I=1}^n N_I(\mathbf{x}) u_I \\
 & \blacksquare + \sum_{i=1}^{n_h} N_{I_i}(\mathbf{x}) (H(\mathbf{x}) - H(\mathbf{x}_{I_i})) a_{I_i} \\
 & \blacksquare + \sum_{i=1}^{n_f} N_{\hat{I}_i}(\mathbf{x}) \sum_{J=1}^{n_J} \left( F_J(\mathbf{x}) - F_J(\mathbf{x}_{\hat{I}_i}) \right) b_{\hat{I}_i J}
 \end{aligned}$$



■ **Jump enrichment:**

$$H(\mathbf{x}) = \begin{cases} 1 & \text{above } \Gamma_{c+} \\ -1 & \text{below } \Gamma_{c-} \end{cases}$$

■ **Tip enrichments:**

$$F_J(r, \theta) = \left\{ \overbrace{\sqrt{r} \sin\left(\frac{\theta}{2}\right)}^{J=1}, \overbrace{\sqrt{r} \cos\left(\frac{\theta}{2}\right)}^{J=2}, \overbrace{\sqrt{r} \sin\left(\frac{\theta}{2}\right) \sin(\theta)}^{J=3}, \overbrace{\sqrt{r} \cos\left(\frac{\theta}{2}\right) \sin(\theta)}^{J=4} \right\}$$



# XFEM Linear system

## Strain-displacement relations:

$$\mathbf{B}_{enr}^e = \nabla_{sym} \mathbf{N}_{enr}^e$$

- Symmetric gradient operator applied to enriched basis-function matrix



## Stiffness matrix:

$$\mathbf{A}_e = \int_{\Omega_e} (\mathbf{B}_{enr}^e)^T \mathbf{D} \mathbf{B}_{enr}^e d\Omega_e$$

- Numerical quadrature for stiffness matrix

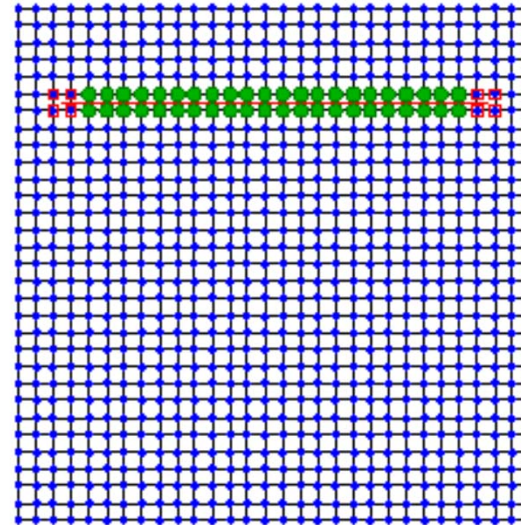


## XFEM Linear System:

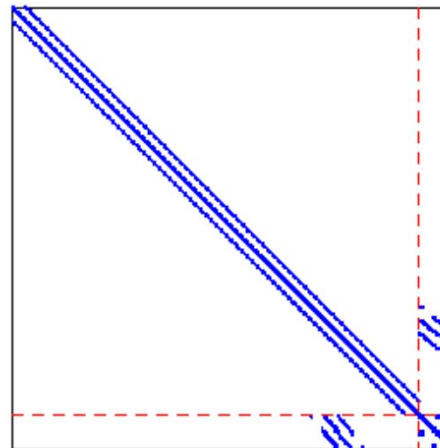
$$\begin{bmatrix} A_{rr} & A_{rx} \\ A_{xr} & A_{xx} \end{bmatrix} \begin{bmatrix} u_r \\ u_x \end{bmatrix} = \begin{bmatrix} \tilde{f}_r \\ \tilde{f}_x \end{bmatrix}$$

- Enriched DOF grouped together at the end in  $u_x$
- $A_{xx}$  small compared to  $A_{rr}$  for relatively small number of cracks
- Dense blocks in  $A_{xx}$  correspond to tip functions

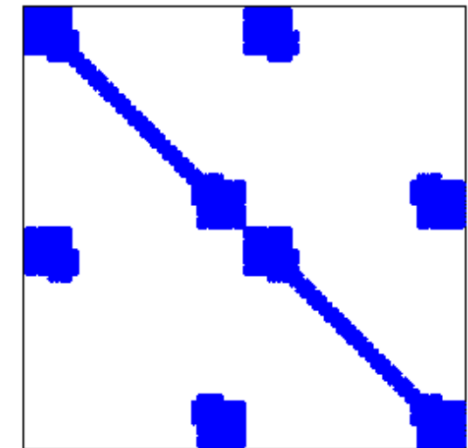
XFEM mesh



Sparsity pattern of  $A$

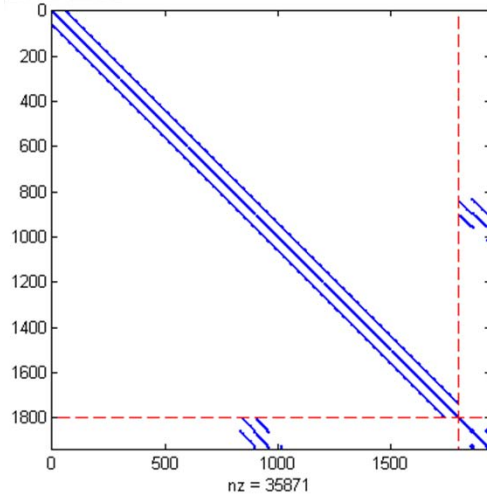


Sparsity pattern of  $A_{xx}$



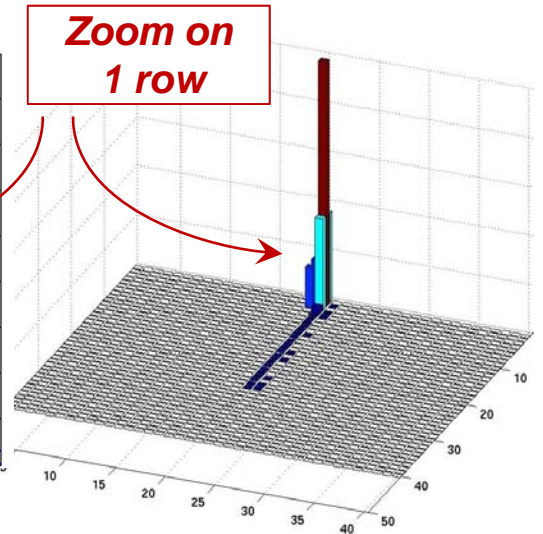
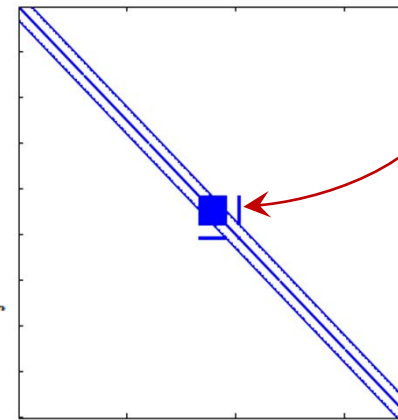


# Schur Complement



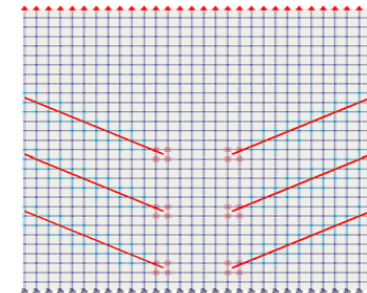
$$A = \begin{pmatrix} A_{rr} & A_{rx} \\ A_{xr} & A_{xx} \end{pmatrix}$$

$$S = A_{rr} - A_{rx} A_{xx}^{-1} A_{xr}$$



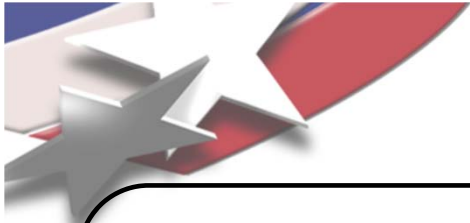
## AMG Applied to S

- $\hat{S}$ : small entries dropped from S
- Aggregation & SparsityPattern(  $A_{rr} \cdot \hat{S}$  )
- Standard AMG (energy min.)



Mesh	Scalar AMG	Variable Block AMG	AMG on Schur Complement
30×30	180	89	10
60×60	-	103	11
90×90	-	114	11
120×120	-	126	12





# Implicit Schur complement

**Lemma:** Schur complement/projection commutativity. Let  $P$  be interpolation associated with a 2-level AMG method applied to  $S$ . Define a 2-level AMG method for the full 2x2 system by

$$\bar{P} = \begin{bmatrix} P & 0 \\ 0 & I \end{bmatrix}$$

Then, projected Schur complement & Schur complement of projected full system are equivalent.

## Coarsening of Schur Complement

$$\begin{aligned}
 S &= A_{rr} - A_{rx}A_{xx}^{-1}A_{xr} \\
 \Rightarrow P^T S P &= P^T (A_{rr} - A_{rx}A_{xx}^{-1}A_{xr}) P \\
 &= P^T A_{rr} P - P^T A_{rx} A_{xx}^{-1} A_{xr} P
 \end{aligned}$$

## Schur Complement of Coarse-level 2x2 matrix

$$\begin{aligned}
 \bar{P} &= \begin{bmatrix} P & 0 \\ 0 & I \end{bmatrix} \\
 \Rightarrow \bar{P}^T A \bar{P} &= \begin{bmatrix} P & 0 \\ 0 & I \end{bmatrix}^T \begin{bmatrix} A_{rr} & A_{rx} \\ A_{xr} & A_{xx} \end{bmatrix} \begin{bmatrix} P & 0 \\ 0 & I \end{bmatrix} \\
 &= \begin{bmatrix} P^T A_{rr} P & P^T A_{rx} \\ A_{xr} P & A_{xx} \end{bmatrix} \\
 \Rightarrow \bar{S} &= P^T A_{rr} P - P^T A_{rx} A_{xx}^{-1} A_{xr} P
 \end{aligned}$$

Can be generalized for multilevel via recursion.



# Implicit Schur complement

Lemma: Let relaxation on Schur complement & on full 2x2 system be defined by

reduced system:

$$u_r \leftarrow u_r + M_{rr}^{-1} r_r$$

full system:

$$\tilde{u}_x \leftarrow A_{xx}^{-1}(\tilde{f}_x - A_{xr}\tilde{u}_r)$$

$$\begin{bmatrix} \tilde{u}_r \\ \tilde{u}_x \end{bmatrix} \leftarrow \begin{bmatrix} \tilde{u}_r \\ \tilde{u}_x \end{bmatrix} + \begin{bmatrix} M_{rr} & 0 \\ A_{xr} & A_{xx} \end{bmatrix}^{-1} \begin{bmatrix} \tilde{r}_r \\ \tilde{r}_x \end{bmatrix}$$

Then, iterates are equivalent if initial guesses and rhs chosen consistently.

Thm: Recursively define interpolation & relaxation as in 2 previous Lemma to construct two AMG methods: one applied to  $S$  and one applied to the full 2x2 system.

Then, AMG iterates are equivalent if fine level initial guess and rhs chosen consistently.

→ Multigrid solver can use implicit Schur complement, and never form  $S$  explicitly.

$$\text{Recall } \bar{P} = \begin{bmatrix} P & 0 \\ 0 & I \end{bmatrix}$$

Caveat:  $P$  &  $M_{rr}$  must be computable without an explicit form of  $S$  !!

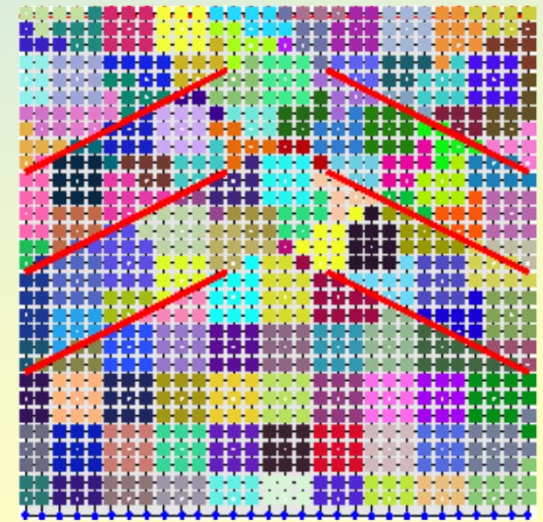


## Approximation & Implicit Schur Complements

Avoid explicit  $S$  when building  $P$

- using levelsets & coordinates define  $\hat{A}_{rr}(i, j) = \begin{cases} 0 & \text{if crack crossing} \\ A_{rr}(i, j) & \text{otherwise} \end{cases}$

$\Rightarrow$  run standard energy minimization, but  
Use  $\hat{A}_{rr}$  for aggregation & sparsity pattern  
Use  $A_{rr}$  for energy definition



Less expensive smoother

- Approximate  $(A_{xx}^{[k]})^{-1}$  via Gauss-Seidel
- Approximate  $(M_{rr}^{[k]})^{-1}$  via Gauss-Seidel

$\Rightarrow$

- One GS sweep on  $A_{xx}u_x = f_x - A_{xr}u_r$
- One GS sweep on  $A_{rr}u_r = f_r - A_{rx}u_x$
- One GS sweep on  $A_{xx}u_x = f_x - A_{xr}u_r$



# Approximating AMG on $S$

$P(C, G) =$  Prolongator generated via energy minimization

Definition of energy

Sparsity Pattern

$\hat{G}$  :  $G$  with crack crossings removed

$M_{rr}$  : Relaxation smoother for Schur complement

$R_r$  : Smoother for regular dof

$R_r$  : Smoother for enriched dof

	Schur		Hybrid		
	$P(S, \hat{S})$	$P(\underline{A_{rr}}, \hat{S})$	$P(A_{rr}, \underline{\hat{A_{rr}}})$	$P(A_{rr}, \hat{A_{rr}})$	$P(A_{rr}, \hat{A_{rr}})$
Mesh	$M_{rr} = \text{GS on } S$		$R_r = \text{GS on } S$	$R_r = \text{GS on } \underline{A_{rr}}$	$R_r = \text{GS on } A_{rr}$
			$R_x = \text{Direct Solve}$	$R_x = \text{Direct Solve}$	$R_r = \text{GS on } \underline{A_{xx}}$
$30 \times 30$	10	11	14	18	18
$60 \times 60$	11	11	13	17	17
$90 \times 90$	11	11	13	17	17
$120 \times 120$	12	11	13	17	17

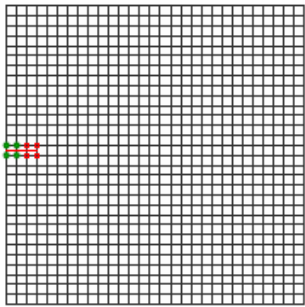


# Numerical Results...

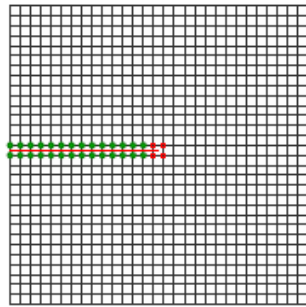
## Test Cases:

- Both edge cracks and interior cracks considered
- CG preconditioned with AMG
- VBlk AMG: block form of standard AMG with 1 pre + 1 post **block** sym(GS)
- Hybrid Standard AMG:  $P(A_{rr}, A_{rr})$  with 1 pre + 1 post sym(GS) on 2x2 system
- Quasi-AMG:  $P(A_{rr}, \hat{A}_{rr})$  with 1 pre + 1 post sym(GS) on 2x2 system

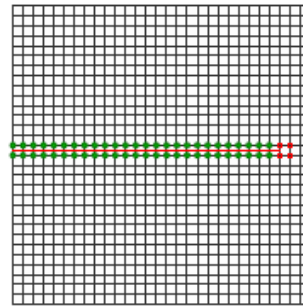
### Single Propagating Crack



(a) Case 1a

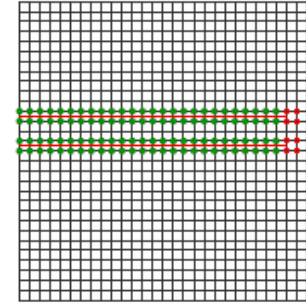


(b) Case 1b

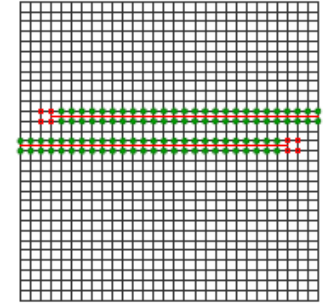


(c) Case 1c

### Two Cracks

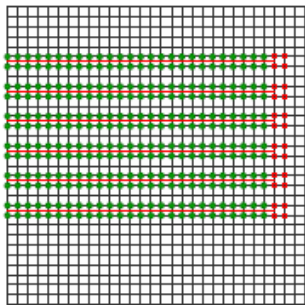


(d) Case 2a

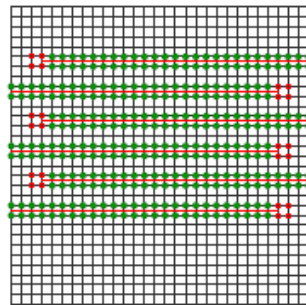


(e) Case 2b

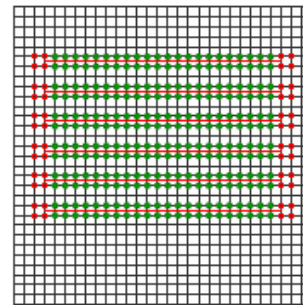
### Six Cracks



(f) Case 3a

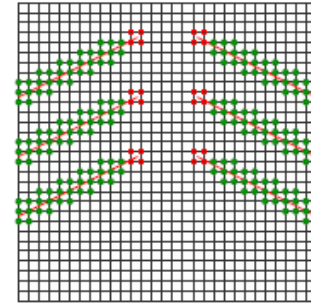


(g) Case 3b

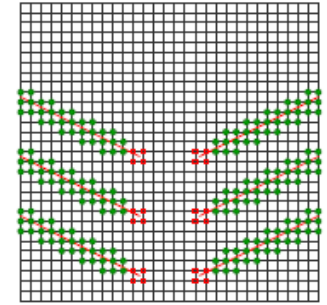


(h) Case 4

### Inclined Cracks



(i) Case 5a



(j) Case 5b



# Numerical Results...

Case	VBlk AMG	Hybrid Standard AMG	Quasi AMG	Mesh	Case	VBlk AMG	Hybrid Standard AMG	Quasi AMG
1a	28	13	11	$30^2$	3a	154	-	16
	29	15	10	$60^2$		127	-	14
	37	17	12	$90^2$		-	-	25
	37	19	12	$120^2$		-	-	21
1b	24	22	11	$30^2$	3b	-	-	18
	24	29	12	$60^2$		-	-	21
	36	35	14	$90^2$		-	-	28
	35	41	13	$120^2$		-	-	22
1c	31	31	13	$30^2$	4	116	107	15
	32	43	14	$60^2$		102	154	21
	47	53	16	$90^2$		142	190	23
	45	61	15	$120^2$		151	-	22
2a	64	57	15	$30^2$	5a	80	76	12
	52	80	14	$60^2$		91	107	13
	87	98	20	$90^2$		124	131	15
	92	113	18	$120^2$		140	151	15
2b	73	59	16	$30^2$	5b	89	81	16
	72	81	17	$60^2$		103	116	15
	97	104	21	$90^2$		134	143	17
	95	122	19	$120^2$		151	165	16

# of levels	full complexity	(1,1) complexity
2	1.673	1.607
3	1.815	1.716
3	1.65	1.583
4	1.699	1.621





# Exploiting Flexibility

Coarsening, sparsity pattern,  $p_{ij}$  choice are often tied together within many **AMG methods**

Example: smoothed aggregation

1) **Aggregate:**  $\mathcal{A}_i \cup \mathcal{A}_j = \{1, \dots, |V|\}$ ,  $\mathcal{A}_i \cap \mathcal{A}_j = \emptyset$ ,  $\text{diam}(\mathcal{A}_i) \approx 3$

2)  $P_0 = \text{BlkDiag}(\mathcal{R}_i B) =$

ColDim( $P$ ) =  $3 N_{\mathcal{A}}$   
 $\Rightarrow$  smaller search space  
 $\Rightarrow$  lower  $\text{nnz}(A_H)$

Graph of  $\tilde{A}$

3)  $P = P_0 + \omega D^{-1} \tilde{A} P_0$

~~• ColDim( $B$ ) = ColDim( $\mathcal{B}_i$ )  $\Rightarrow$  ColDim( $P$ ) = ColDim( $B$ ) \*  $N_{\mathcal{A}} = 6 * N_{\mathcal{A}}$~~

• sparsity pattern is  $|\tilde{A}| P_0$

• Should have  $\tilde{A} P_0 B_c = 0$  where  $B_c$  is coarse representation of  $B$  (modes requiring accurate interpolation)

$\Rightarrow \tilde{A} B = 0$  (as  $P_0 B_c = B$ )

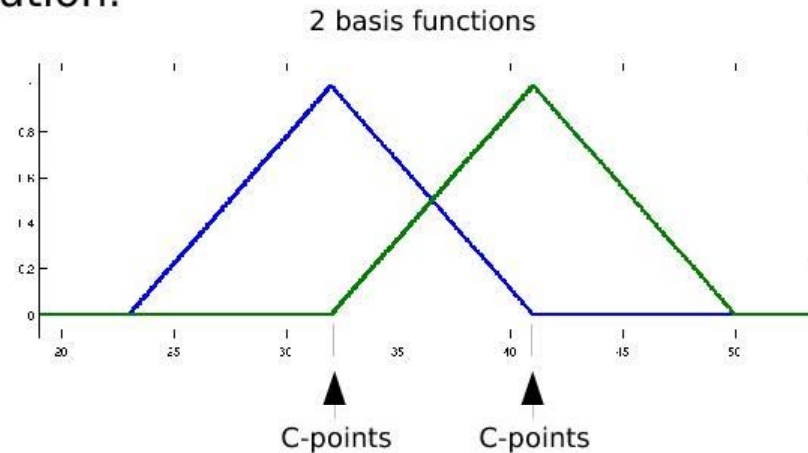
We will also exploit ability to change norm.



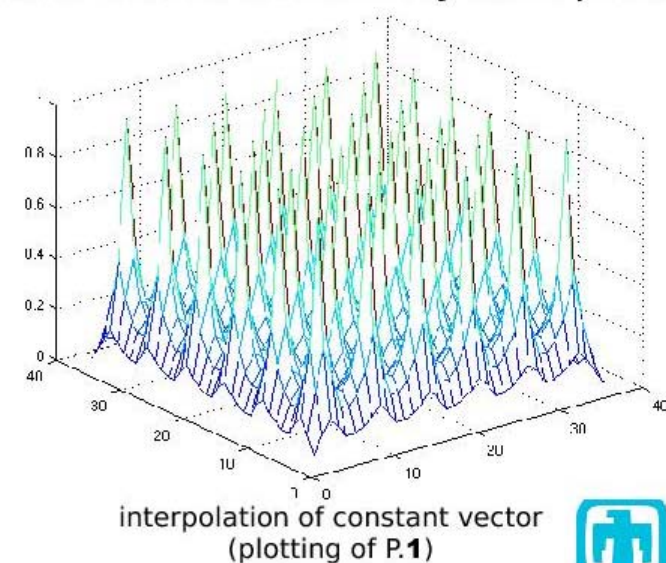
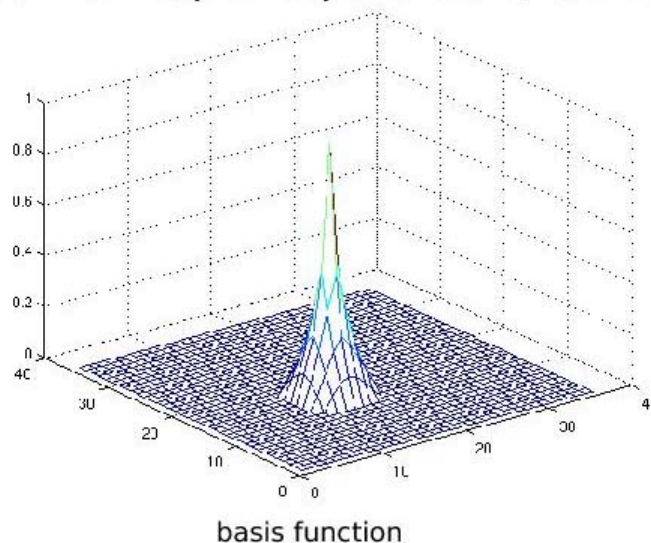


## Weakly Constrained Case

- For 1D Laplace problems, constraining only at root points corresponds to linear interpolation:



- For 2D Laplace problems, constant vector is not accurately interpolated:





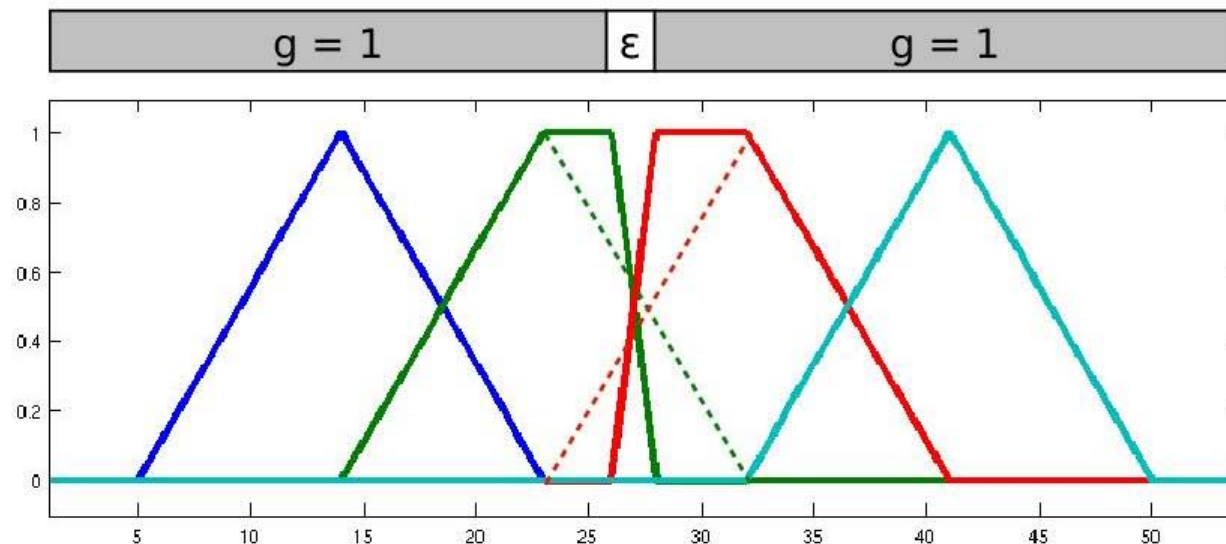
## Fully constrained

### Problematic if constraints do not capture physics

Example:  $(g(x) u_x)_x = f$  with two constraints. If  $B_{.,1}=1, B_{.,2}=x$ , then constants and linears are exactly interpolated

exact  
interpolation  
vectors

$\text{nnz}(P_i) \leq 2 \Rightarrow \text{fully constrained} \Rightarrow \text{linear interpolation independent of } g(x)$



*Problem:* fully constraining ignores energy:

- Jumps are not captured in  $P$
- Left and right regions connected within coarse level due to interpolation across epsilon region



# Smoothed Aggregation & General Energy Minimization

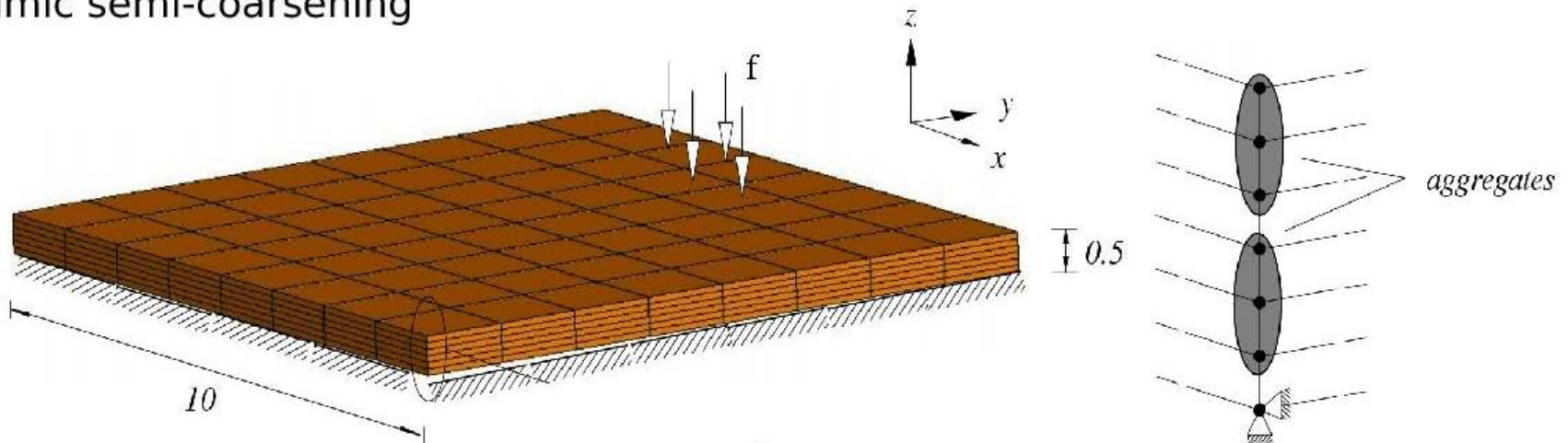
## Smoothed Aggregation

- 1 step minimization
- No need to apply  $Q$  ...  
... but  $A P_0 B_c$  must equal 0.
- *almost* fixed sparsity pattern governed by  $|A| |P_0|$
- # DOFs per node =  $\dim\{N\}$

## General Energy Minimization

- multi-step minimization
- No restriction on  $A P_0$ .
- Any sparsity pattern
- Arbitrary # DOFs per node

- Anisotropic problems require anisotropic coarsening and sparsity pattern to mimic semi-coarsening



This is normally accomplished by defined  $\tilde{A}$  where small (weak entries) are dropped during prolongator construction





# Smoothed Aggregation & General Energy Minimization

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## Smoothed Aggregation

- 1 step minimization
- No need to apply  $Q$  ...  
... but  $\tilde{A} P_0 B_c$  must equal 0.
- *almost* fixed sparsity pattern  
governed by  $[\tilde{A} \mid P_0]$
- # DOFs per node =  $\dim\{N\}$

## General Energy Minimization

- multi-step minimization
- No restriction on  $\tilde{A} P_0$ .
- Any sparsity pattern
- Arbitrary # DOFs per node

For elasticity:

- Proper  $\tilde{A}$  such that  $\tilde{A} P_0 B_c = 0$  with weak connections dropped is non-obvious
- Anisotropic coarsening gives small aggregates  $\Rightarrow$  high operator complexities
- 3 DOFs/node on finest level ...  
... but  $\dim\{N\} = 6$  for 3D elasticity  $\Rightarrow$  6 DOFs/node  $\Rightarrow$  even higher complexities



# Energy-minimization - Elasticity

---

Lots of choices. We focus on:

3 DOFs/nodes on the coarse grid



Does smaller search space limit quality of interpolation?

- N: 6 rigid body modes (3 translations & 3 rotations)
- CG to solve  $A P = 0$  (effectively defines energy)
- $P_0$  & sparsity pattern are smoothed aggregation inspired
  - Coarse nullspace defined by injection of fine nullspace @ root nodes
  - Initial Guess:  $P_{sa0} + X^T (X X^T)^{-1} (\hat{B} - X P_{sa0})$   
where  $P_{sa0}$  is smoothed aggregation  $P_0$  for just translations
  - Sparsity Pattern:  $|\tilde{A}| |P_{sa0}|$  except @ root points which are constrained to have only 1 nnz/row associated with injection
    - Avoids linear dependency issues
- $\tilde{A}$  defined using distance Laplacian + dropping for sparsity pattern
- No need for  $\tilde{A} B = 0$
- A is still used to define energy (as opposed to  $\tilde{A}$ )



## Experiments

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- 3D Linear Elasticity, plan stress
- AMG accelerate by CG, stopping criterion  $\|r_{\text{relative}}\| < 10^{-10}$
- Influence of the number of energy-minimization steps to the convergence.

Problem size:  $30^3$ . Stretch factor:  $\varepsilon$

# iter.	$\varepsilon = 1$	$\varepsilon = 10$	$\varepsilon = 100$
0	17	19	21
1	12	12	14
2	11	12	13
5	11	12	13
20	11	12	13



## Experiments

- Comparison with Smoothed-Aggregation:
  - SA: 6 DOFs/node
  - Energy-Minimization: 3 DOFs/node, 6 nullspace vectors

Mesh	$\epsilon = 1$		$\epsilon = 10$		$\epsilon = 100$	
	SA	Emin	SA	Emin	SA	Emin
$10^3$	6 1.30	7 1.07	8 2.81	8 1.22	9 3.21	8 1.24
$15^3$	8 1.19	9 1.05	10 2.32	10 1.15	12 2.54	12 1.16
$20^3$	8 1.24	9 1.06	10 2.59	9 1.18	13 3.05	10 1.20
$25^3$	9 1.26	8 1.07	11 2.76	9 1.20	14 3.04	10 1.20
$30^3$	10 1.22	11 1.05	12 2.52	12 1.17	15 3.06	13 1.19
$35^3$	10 1.24	10 1.06	12 2.66	12 1.18	16 3.03	13 1.19
$40^3$	10 1.26	9 1.06	12 2.77	12 1.19	16 3.21	11 1.21

Tab. : Iteration count and complexity (lower complexity = faster run time) for SA and energy minimization for various mesh sizes and stretch factors.

$$\text{complexity: } \frac{\sum_i \text{nnz}(A_i)}{\text{nnz}(A)}$$





# Conclusions

- Krylov minimization can be used to generate “energy” minimizing prolongators/restrictors for symmetric & non-symmetric systems
  - CG, GMRES
- Some linear algebra issues ...
- Flexibility
  - Coarsening, e.g. F/C aggregation, irregular
  - Grid transfer sparsity patterns
  - Norms defining energy
- \* sparsity pattern & energy norm flexibility used to XFEM ice fracture problem
- \* sparsity pattern and dimension of P flexibility used for anisotropic elasticity