



Leveraging Flexibility in Energy Minimization Algebraic Multigrid

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Outline

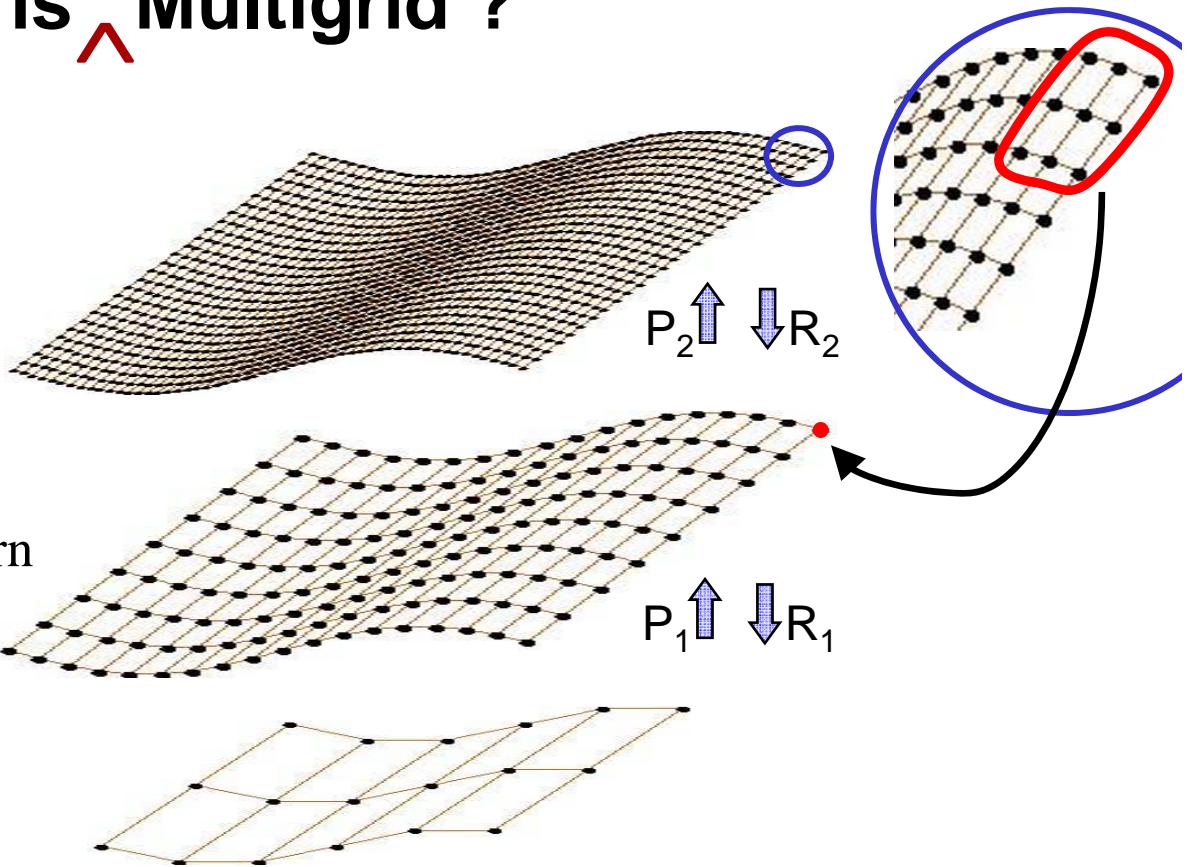
- Energy minimization AMG
 - Motivation: arbitrary coarsening, flexible coarse basis function support, accurate interpolation of arbitrary important modes, flexible choice of norm for minimization & search space
 - $A \neq A$ & Krylov Methods
- Leveraging flexibility of energy minimization AMG
 - weakly constrained & over-constrained
 - anisotropic elasticity
 - Flexible sparsity pattern & accurate rigid body mode interpolation
 - extended finite elements & fracture
 - Flexible pattern, flexible norm choice



Algebraic What is \wedge Multigrid ?

Solve $A_3 u_3 = f_3$

- Construct Graph & Coarsen
- Determine P_i & R_i sparsity pattern
- Determine P_i & R_i 's coeffs
- Project: $A_i = R_i A_{i+1} P_i$



$$\min_{e_H} \| e - Pe_H \|_2^2 \leq \beta \| e \|_A^2$$

$$\| Se \|_A^2 \leq \| e \|_A^2 - \alpha \| e \|_{A^2}^2$$

$$\Rightarrow \| ST_{2-level} \|_A \leq \sqrt{1 - \frac{\alpha}{\beta}}$$

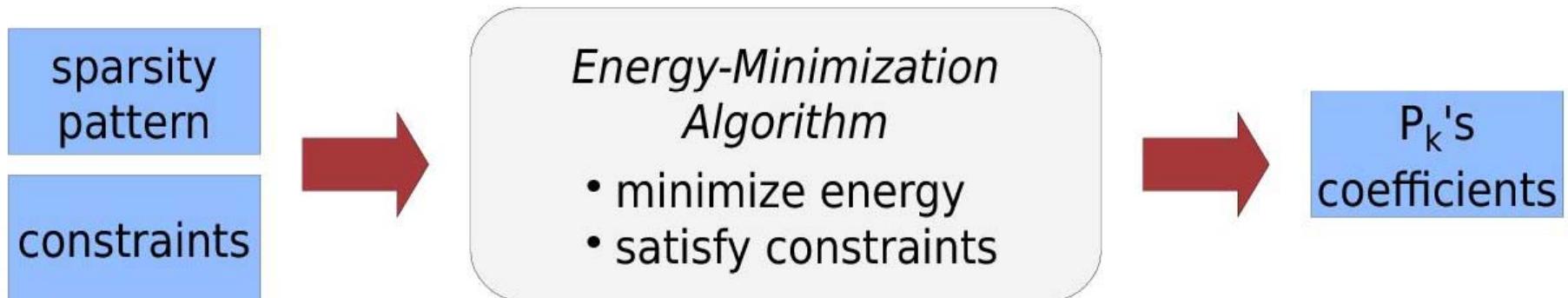


Algorithm

$$\min \sum \|p_i\|_e^2 \quad \text{where } p_i \text{ gives the } i^{\text{th}} \text{ column of a prolongator}$$

Idea: construct the grid transfer operator P by minimizing the energy of each column , while enforcing constraints (sparsity pattern and specified modes).

Input / output of energy-minimization algorithm:



Advantages:

- Flexibility (input):
 - arbitrary coarsening
 - accept any sparsity pattern (arbitrary basis function support)
 - enforce constraints: important modes requiring accurate interpolation
 - choice of norm for minimization and search space
- Robustness



Energy-Minimization

Find $P = [p_1 \ p_2 \ \cdots \ p_m]$ that

minimizes $\sum_i \|p_i\|_e$ in some space subject to $X \begin{pmatrix} p_1 \\ \vdots \\ p_m \end{pmatrix} = g$

if $e = A$ \Rightarrow

$$\hat{A} \begin{pmatrix} A & & & \\ & A & & \\ & & A & \\ & & & A \end{pmatrix} X^T \begin{pmatrix} p_1 \\ p_2 \\ p_3 \\ p_4 \\ \lambda \end{pmatrix} = \begin{pmatrix} 0 \\ \\ \\ \\ g \end{pmatrix}$$

Constraints enforce exact interpolation of null space,
e.g. $A B = 0 \rightarrow B \in \text{Range}(P)$

»P«

“Solve” $AP = 0$

- 1) with minimization algorithm
- 2) in space satisfying constraints

$$A (P_0 - \Delta P) = 0 \text{ with } X \gg P_0 \ll = g$$

$$X \gg \Delta P \ll = 0$$

$$Q \hat{A} \gg P_0 \ll, (Q \hat{A})^2 \gg P_0 \ll, \dots$$

$$Q = (I - X^T (X X^T)^{-1} X)$$



CG minimization

Lemma: *Let A be SPD and apply CG to*

$$Q \hat{A} Q \gg \Delta P \ll = Q \hat{A} Q \gg P_0 \ll$$

with 0 initial guess, then CG computes

$$\Delta P_i = \arg \min_{\Delta P_i \in \mathcal{K}_i} \left\| \Delta P_i \right\|_{\hat{A}} \quad \text{where} \quad P_i = P_0 \cdot \Delta P_i$$

Proof.

$$\begin{aligned}
\gg\Delta P_i \ll &= \arg \min_{\gg\Delta P_i \ll \in \mathcal{K}_i} \left\| \gg P_* \ll - \gg\Delta P_i \ll \right\|_{Q\hat{A}Q}^2 \\
&= \arg \min_{\gg\Delta P_i \ll \in \mathcal{K}_i} \left\| \gg P_* \ll \right\|_{Q\hat{A}Q}^2 + \left\| \gg\Delta P_i \ll \right\|_{Q\hat{A}Q}^2 - 2 \left\langle \gg\Delta P_i \ll, \gg P_0 \ll \right\rangle_{\hat{A}} \\
&= \arg \min_{\gg\Delta P_i \ll \in \mathcal{K}_i} \left\| \gg P_0 \ll \right\|_{Q\hat{A}Q}^2 + \left\| \gg\Delta P_i \ll \right\|_{Q\hat{A}Q}^2 - 2 \left\langle \gg\Delta P_i \ll, \gg P_0 \ll \right\rangle_{\hat{A}} \\
&= \arg \min_{\gg\Delta P_i \ll \in \mathcal{K}_i} \left\| \gg P_0 \ll - \gg\Delta P_i \ll \right\|_{\hat{A}}^2
\end{aligned}$$

Corollary: CG solution is unique





GMRES minimization

Lemma: *Let A be nonsingular and apply GMRES to*

$$Q \hat{A} \ll \Delta P \ll = Q \hat{A} \ll P_0 \ll \quad (*)$$

with 0 initial guess, then GMRES computes

$$\ll \Delta P_i \ll = \arg \min_{\ll \Delta P_i \ll \in \mathcal{K}_i} \ll \Delta P_i \ll \ll \hat{A}^T Q \hat{A} \ll \text{ where } P_i = P_0 \cdot \Delta P_i$$

which is unique.

Proof.

Define S and S_{\perp} such that

$$QS = 0, \quad S_{\perp} S_{\perp}^T = Q, \quad S_{\perp}^T S_{\perp} = I, \quad S^T S = I, \quad S^T S_{\perp} = I$$

Use properties of GMRES applied to nonsingular system

$$S_{\perp}^T \hat{A} S_{\perp} y = S_{\perp}^T \hat{A} \ll P_0 \ll \quad (**) \quad \text{with } \ll AP_i \ll \ll Q \ll$$

*Pre-multiplication of $(**)$ & associated Krylov space by S_{\perp} reveal equivalence with $(*)$.*



$\mathbf{A} \neq \mathbf{A}^T$ (weakly constrained)

- Use GMRES to “solve” $AP = 0$ with only constraint $P = [P_f \ I_c]^T$
- Use GMRES to “solve” $RA = 0$ with only constraint $R = [R_f \ I_c]$

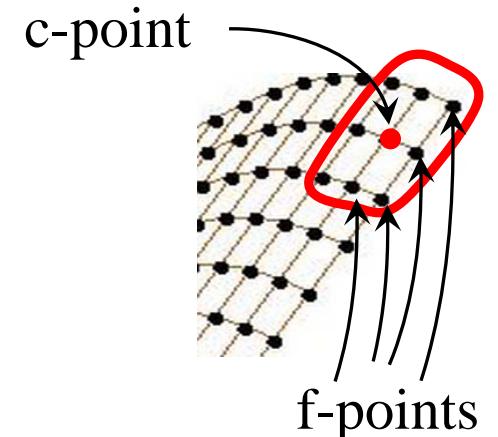
Consider

$$\begin{pmatrix} A_{ff} & A_{fc} \\ A_{cf} & A_{cc} \end{pmatrix} \begin{pmatrix} u_f \\ u_c \end{pmatrix} = \begin{pmatrix} b_f \\ b_c \end{pmatrix}$$

Then

$$\underbrace{\begin{pmatrix} I_f & 0 \\ R & \end{pmatrix} \begin{pmatrix} A_{ff} & A_{fc} \\ A_{cf} & A_{cc} \end{pmatrix} \begin{pmatrix} I_f & P \\ 0 & \end{pmatrix}}_{\begin{pmatrix} A_{ff} & E_{fc} \\ E_{cf} & A_H \end{pmatrix}} \begin{pmatrix} y_f \\ y_c \end{pmatrix} = \begin{pmatrix} b_f \\ Rb \end{pmatrix}$$

Decouples if $E_{fc} = (A_{ff} \ A_{fc})P$ & $E_{cf} = R \begin{pmatrix} A_{ff} \\ A_{cf} \end{pmatrix}$ are 0.
 $= Q \gg AP \ll$ $= \gg RA \ll Q$





Exploiting Flexibility

Coarsening, sparsity pattern, p_{ij} choice are often tied together within many **AMG methods**

Example: smoothed aggregation

1) **Aggregate:** $\mathcal{A}_i \cup \mathcal{A}_j = \{1, \dots, |V|\}$, $\mathcal{A}_i \cap \mathcal{A}_j = \emptyset$, $\text{diam}(\mathcal{A}_i) \approx 3$

2) $P_0 = \text{BlkDiag}(\mathcal{R}_i, B) = \begin{bmatrix} \mathcal{B}_1 & & \\ & \mathcal{B}_2 & \\ & & \ddots \end{bmatrix}$ Graph of $\tilde{\mathbf{A}}$

3) $P = P_0 + \omega D^{-1} \tilde{\mathbf{A}} P_0$

- $\text{ColDim}(B) = \text{ColDim}(\mathcal{B}_i)$
- sparsity pattern is $|\tilde{\mathbf{A}}| / P_0$
- Should have $\tilde{\mathbf{A}} P_0 B_c = 0$ where B_c is coarse representation of B (modes requiring accurate interpolation)
 $\Rightarrow \tilde{\mathbf{A}} B = 0$ (as $P_0 B_c = B$)

We will also exploit ability to change norm.

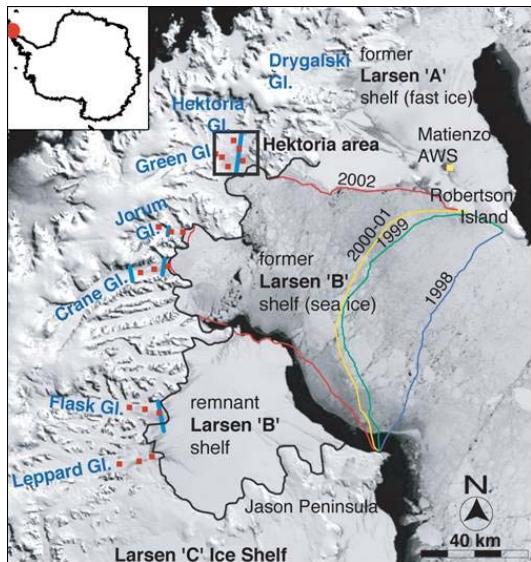


Motivation: Importance of Ice Fracture

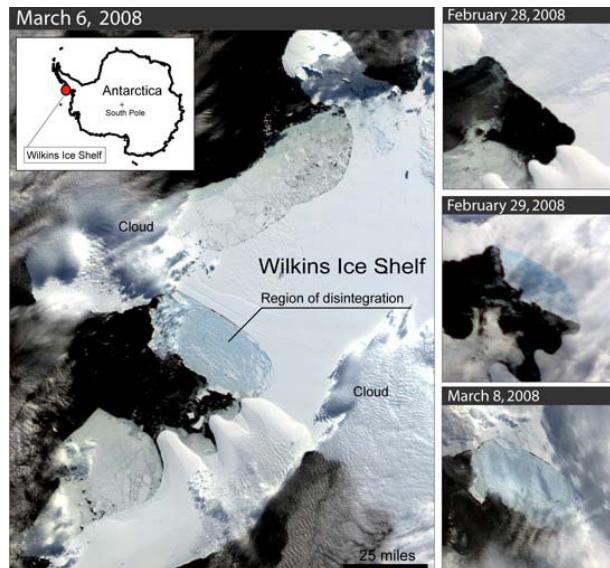
Objective: Employ parallel computers to study the fracture of land ice to better understand how it affects global climate change. In particular

- the collapse mechanism of ice shelves,
- the calving of large icebergs, and
- the role of fracture in the delivery of water to the bed of ice sheets.

ice shelves in Antarctica

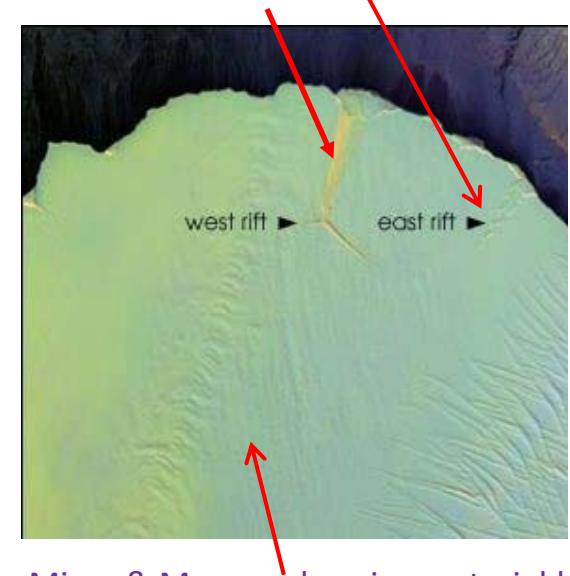


Larsen B diminishing shelf
1998-2002



Wilkins ice shelf
Recent 2008 collapse

Macro scale - rifts will be represented by cracks (XFEM)

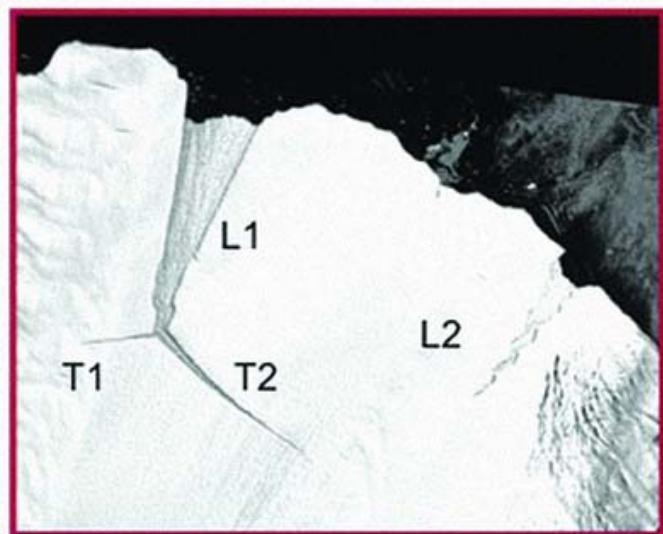
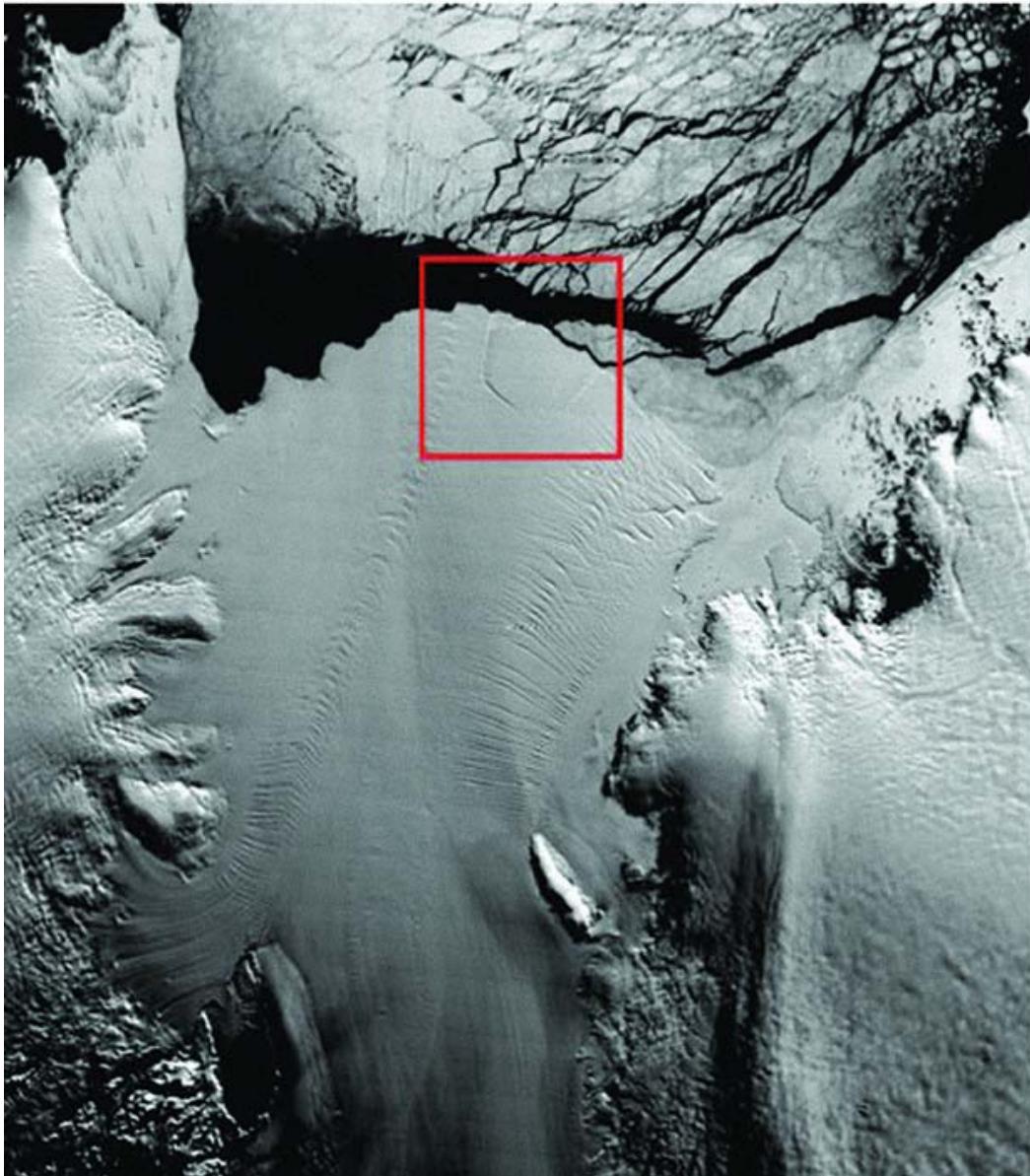


Micro & Meso scales - ice material law given by viscoelastic damage model

Amery ice shelf



Amery ice shelf





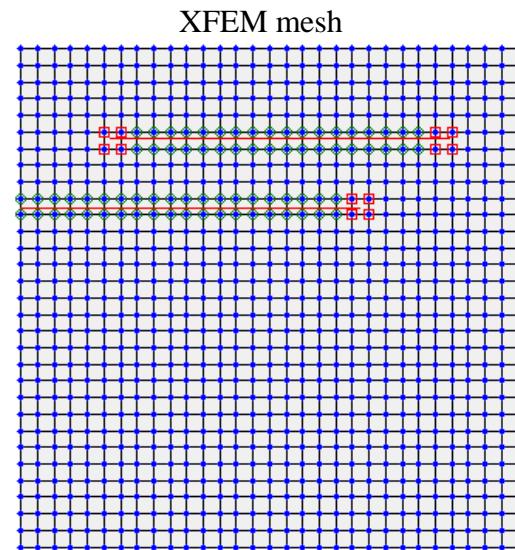
Computational Modeling of Fracture

Classical FEM approach to fracture mechanics

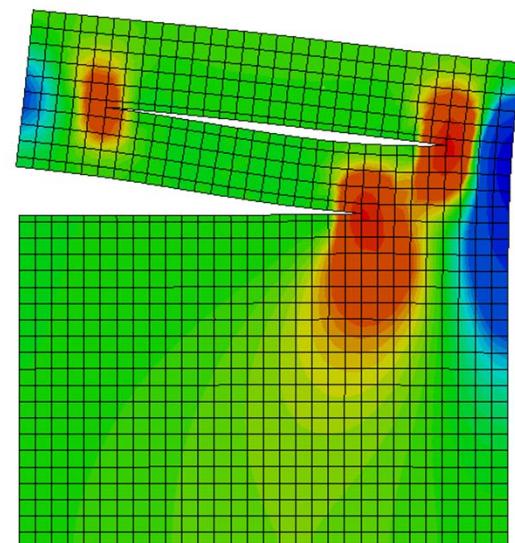
- Mesh conforms to crack boundaries
- Crack propagation → remeshing at each step
 - Requires double-nodes for crack opening and fine mesh for tip singularities

eXtended Finite Element Method (XFEM)*

- Base mesh independent of crack geometry
- Crack propagation → adding “enriched” DOF with special basis functions to existing nodes
 - Crack geometry defined through levelsets
 - Discontinuities and singularities captured through special basis functions (enrichments)
 - Enrichments have local support



Stresses in y direction when bottom edge fixed and uniform traction applied on top edge in y direction



* Belytschko & Black (1999), Moes et al. (1999)

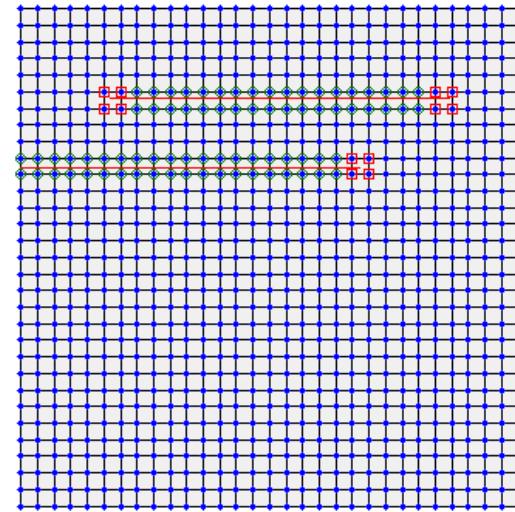


XFEM Formulation

Displacement trial function (shifted basis form.):

$$u^h(\mathbf{x}) = \sum_{I=1}^n N_I(\mathbf{x}) u_I$$

- $+ \sum_{i=1}^{n_h} N_{I_i}(\mathbf{x}) (H(\mathbf{x}) - H(\mathbf{x}_{I_i})) a_{I_i}$
- $+ \sum_{i=1}^{n_f} N_{\hat{I}_i}(\mathbf{x}) \sum_{J=1}^{n_J} (F_J(\mathbf{x}) - F_J(\mathbf{x}_{\hat{I}_i})) b_{\hat{I}_i J}$



■ Jump enrichment:

$$H(\mathbf{x}) = \begin{cases} 1 & \text{above } \Gamma_{c+} \\ -1 & \text{below } \Gamma_{c-} \end{cases}$$

■ Tip enrichments:

$$F_J(r, \theta) = \left\{ \overbrace{\sqrt{r} \sin\left(\frac{\theta}{2}\right)}^{J=1}, \overbrace{\sqrt{r} \cos\left(\frac{\theta}{2}\right)}^{J=2}, \overbrace{\sqrt{r} \sin\left(\frac{\theta}{2}\right) \sin(\theta)}^{J=3}, \overbrace{\sqrt{r} \cos\left(\frac{\theta}{2}\right) \sin(\theta)}^{J=4} \right\}$$



XFEM Linear system

Strain-displacement relations:

$$\mathbf{B}_{enr}^e = \nabla_{sym} \mathbf{N}_{enr}^e$$

- Symmetric gradient operator applied to enriched basis-function matrix



Stiffness matrix:

$$\mathbf{A}_e = \int_{\Omega_e} (\mathbf{B}_{enr}^e)^T \mathbf{D} \mathbf{B}_{enr}^e d\Omega_e$$

- Numerical quadrature for stiffness matrix

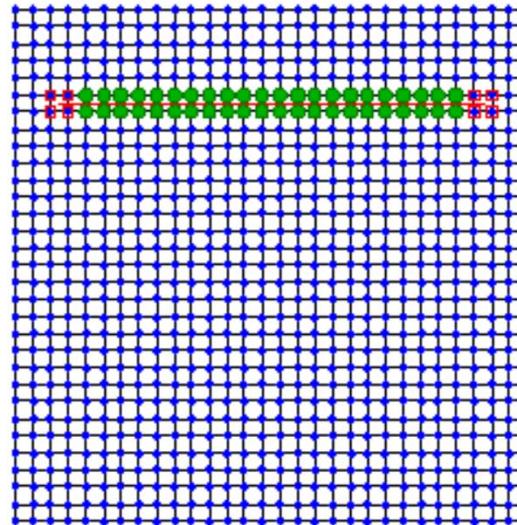


XFEM Linear System:

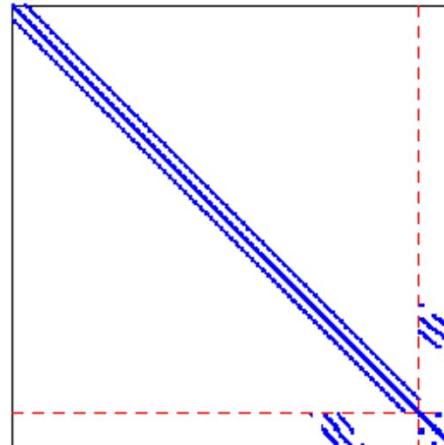
$$\begin{bmatrix} A_{rr} & A_{rx} \\ A_{xr} & A_{xx} \end{bmatrix} \begin{bmatrix} u_r \\ u_x \end{bmatrix} = \begin{bmatrix} \tilde{f}_r \\ \tilde{f}_x \end{bmatrix}$$

- Enriched DOF grouped together at the end in u_x
- A_{xx} small compared to A_{rr} for relatively small number of cracks
- Dense blocks in A_{xx} correspond to tip functions

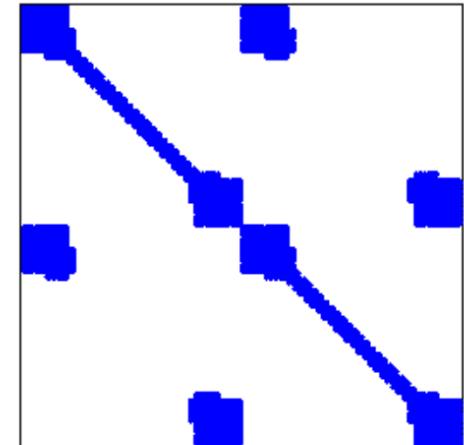
XFEM mesh



Sparsity pattern of A

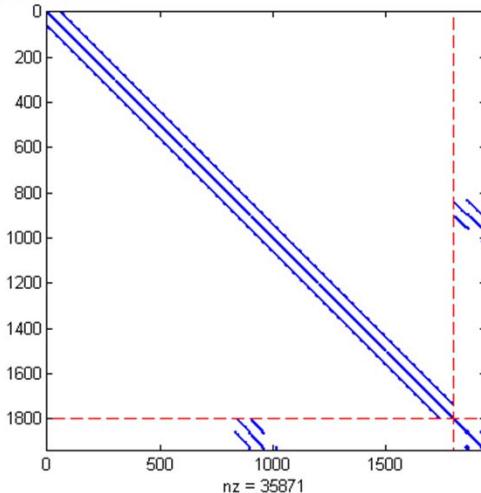


Sparsity pattern of A_{xx}

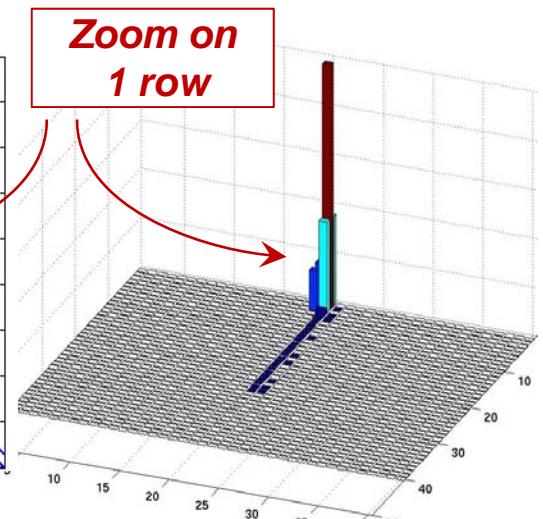
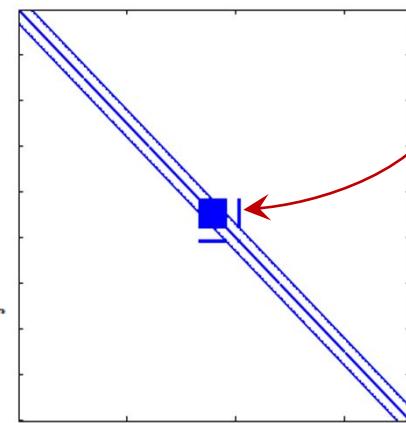




Schur Complement

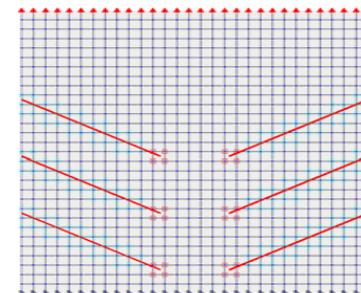


$$A = \begin{pmatrix} A_{rr} & A_{rx} \\ A_{xr} & A_{xx} \end{pmatrix}$$
$$S = A_{rr} - A_{rx} A_{xx}^{-1} A_{xr}$$



AMG Applied to S

- \hat{S} : small entries dropped from S
- Aggregation & SparsityPattern($A_{rr} \cdot \hat{S}$)
- Standard AMG (energy min.)



Mesh	Scalar AMG	Variable Block AMG	AMG on Schur Complement
30×30	180	89	10
60×60	-	103	11
90×90	-	114	11
120×120	-	126	12



Implicit Schur complement

Lemma: Schur complement/projection commutativity. Let P be interpolation associated with a 2-level AMG method applied to S . Define a 2-level AMG method for the full 2×2 system by

$$\bar{P} = \begin{bmatrix} P & 0 \\ 0 & I \end{bmatrix}$$

Then, projected Schur complement & Schur complement of projected full system are equivalent.

Coarsening of Schur Complement

$$\begin{aligned} S &= A_{rr} - A_{rx}A_{xx}^{-1}A_{xr} \\ \Rightarrow P^T S P &= P^T (A_{rr} - A_{rx}A_{xx}^{-1}A_{xr}) P \\ &= P^T A_{rr} P - P^T A_{rx}A_{xx}^{-1}A_{xr} P \end{aligned}$$

Schur Complement of Coarse-level 2×2 matrix

$$\begin{aligned} \bar{P} &= \begin{bmatrix} P & 0 \\ 0 & I \end{bmatrix} \\ \Rightarrow \bar{P}^T A \bar{P} &= \begin{bmatrix} P & 0 \\ 0 & I \end{bmatrix}^T \begin{bmatrix} A_{rr} & A_{rx} \\ A_{xr} & A_{xx} \end{bmatrix} \begin{bmatrix} P & 0 \\ 0 & I \end{bmatrix} \\ &= \begin{bmatrix} P^T A_{rr} P & P^T A_{rx} \\ A_{xr} P & A_{xx} \end{bmatrix} \\ \Rightarrow \bar{S} &= P^T A_{rr} P - P^T A_{rx}A_{xx}^{-1}A_{xr} P \end{aligned}$$

Can be generalized for multilevel via recursion.



Implicit Schur complement

Lemma: Let relaxation on Schur complement & on full 2x2 system be defined by

reduced system:

$$u_r \leftarrow u_r + M_{rr}^{-1} r_r$$

full system:

$$\tilde{u}_x \leftarrow A_{xx}^{-1} (\tilde{f}_x - A_{xr} \tilde{u}_r)$$

$$\begin{bmatrix} \tilde{u}_r \\ \tilde{u}_x \end{bmatrix} \leftarrow \begin{bmatrix} \tilde{u}_r \\ \tilde{u}_x \end{bmatrix} + \begin{bmatrix} M_{rr} & 0 \\ A_{xr} & A_{xx} \end{bmatrix}^{-1} \begin{bmatrix} \tilde{r}_r \\ \tilde{r}_x \end{bmatrix}$$

Then, iterates are equivalent if initial guesses and rhs chosen consistently.

Thm: Recursively define interpolation & relaxation as in 2 previous Lemma to construct two AMG methods: one applied to S and one applied to the full 2x2 system.

Then, AMG iterates are equivalent if fine level initial guess and rhs chosen consistently.

→ Multigrid solver can use implicit Schur complement, and never form S explicitly.

Recall $\bar{P} = \begin{bmatrix} P & 0 \\ 0 & I \end{bmatrix}$

Caveat: P & M_{rr} must be computable without an explicit form of S !!



Approximation & Implicit Schur Complements

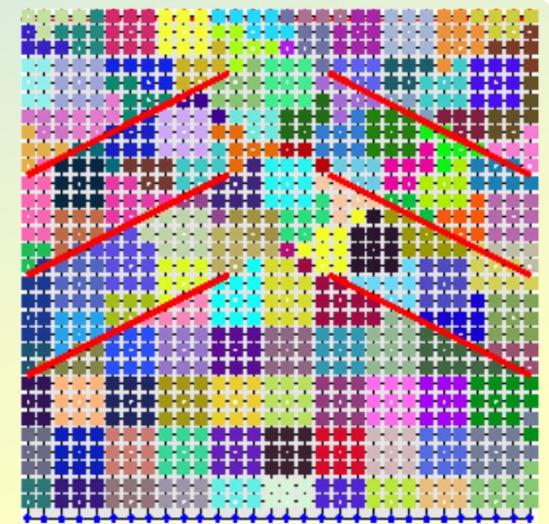
Avoid explicit S when building P

- using levelsets & coordinates define $\hat{A}_{rr}(i, j) = \begin{cases} 0 & \text{if crack crossing} \\ A_{rr}(i, j) & \text{otherwise} \end{cases}$

⇒ run standard energy minimization, but

Use \hat{A}_{rr} for aggregation & sparsity pattern

Use A_{rr} for energy definition



Less expensive smoother

- Approximate $(A_{xx}^{[k]})^{-1}$ via Gauss-Seidel
- Approximate $(M_{rr}^{[k]})^{-1}$ via Gauss-Seidel
 - One GS sweep on $A_{xx}u_x = f_x - A_{xr}u_r$
 - One GS sweep on $A_{rr}u_r = f_r - A_{rx}u_x$
 - One GS sweep on $A_{xx}u_x = f_x - A_{xr}u_r$



Approximating AMG on S

$P(C, G) =$ Prolongator generated via
energy minimization

Definition
of energy

Sparsity
Pattern

\hat{G} : G with crack crossings removed

M_{rr} : Relaxation smoother for Schur complement

R_r : Smoother for regular dof

R_r : Smoother for enriched dof

	Schur		Hybrid		
	$P(S, \hat{S})$	$P(\underline{A}_{rr}, \hat{S})$	$P(\underline{A}_{rr}, \hat{A}_{rr})$	$P(\underline{A}_{rr}, \hat{A}_{rr})$	$P(\underline{A}_{rr}, \hat{A}_{rr})$
Mesh	$M_{rr} = \text{GS on } S$		$R_r = \text{GS on } S$	$R_r = \text{GS on } \underline{A}_{rr}$	$R_r = \text{GS on } \underline{A}_{rr}$
30×30	10	11	14	18	18
60×60	11	11	13	17	17
90×90	11	11	13	17	17
120×120	12	11	13	17	17

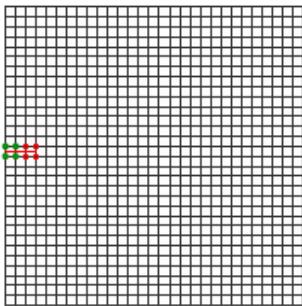


Numerical Results...

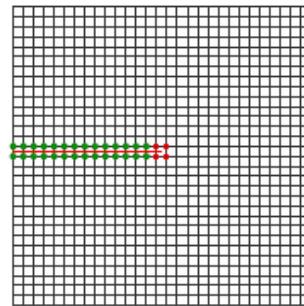
Test Cases:

- Both edge cracks and interior cracks considered
- CG preconditioned with AMG
- VBlk AMG: block form of standard AMG with 1 pre + 1 post **block** sym(GS)
- Hybrid Standard AMG: $P(A_{rr}, A_{rr})$ with 1 pre + 1 post sym(GS) on 2x2 system
- Quasi-AMG: $P(A_{rr}, \hat{A}_{rr})$ with 1 pre + 1 post sym(GS) on 2x2 system

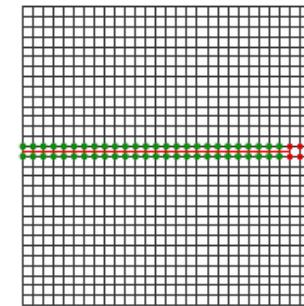
Single Propagating Crack



(a) Case 1a

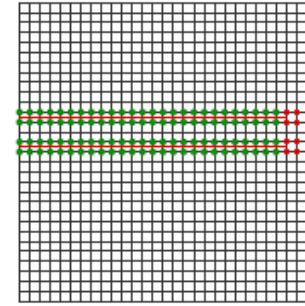


(b) Case 1b

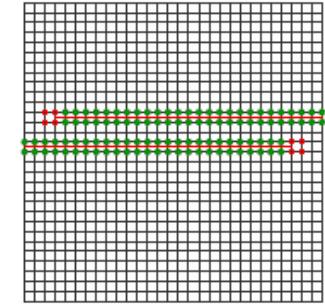


(c) Case 1c

Two Cracks

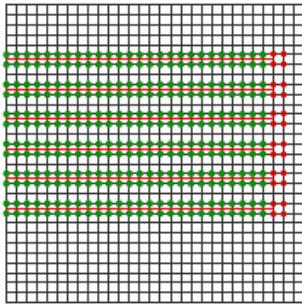


(d) Case 2a

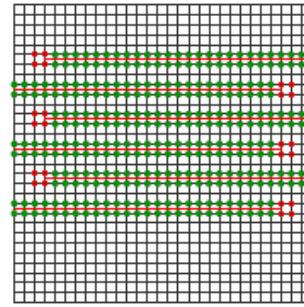


(e) Case 2b

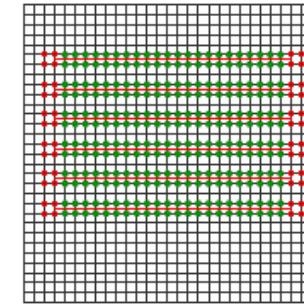
Six Cracks



(f) Case 3a

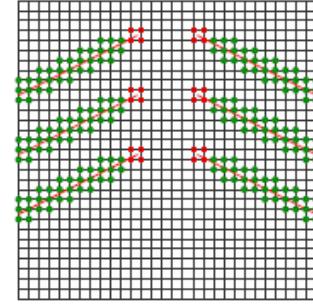


(g) Case 3b

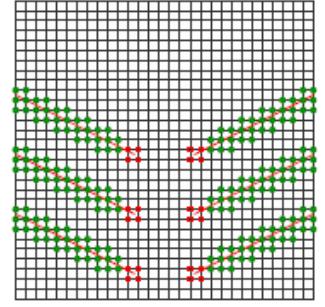


(h) Case 4

Inclined Cracks



(i) Case 5a



(j) Case 5b



Numerical Results...

Case	VBlk AMG	Hybrid Standard AMG	Quasi AMG	Mesh	Case	VBlk AMG	Hybrid Standard AMG	Quasi AMG	# of levels	full complexity	(1,1) complexity
1a	28	13	11	30^2	3a	154	-	16	2	1.673	1.607
	29	15	10	60^2		127	-	14	3	1.815	1.716
	37	17	12	90^2		-	-	25	3	1.65	1.583
	37	19	12	120^2		-	-	21	4	1.699	1.621
1b	24	22	11	30^2	3b	-	-	18			
	24	29	12	60^2		-	-	21			
	36	35	14	90^2		-	-	28			
	35	41	13	120^2		-	-	22			
1c	31	31	13	30^2	4	116	107	15			
	32	43	14	60^2		102	154	21			
	47	53	16	90^2		142	190	23			
	45	61	15	120^2		151	-	22			
2a	64	57	15	30^2	5a	80	76	12			
	52	80	14	60^2		91	107	13			
	87	98	20	90^2		124	131	15			
	92	113	18	120^2		140	151	15			
2b	73	59	16	30^2	5b	89	81	16			
	72	81	17	60^2		103	116	15			
	97	104	21	90^2		134	143	17			
	95	122	19	120^2		151	165	16			



Exploiting Flexibility

Coarsening, sparsity pattern, p_{ij} choice are often tied together within many **AMG methods**

Example: smoothed aggregation

1) **Aggregate:** $\mathcal{A}_i \cup \mathcal{A}_j = \{1, \dots, |V|\}$, $\mathcal{A}_i \cap \mathcal{A}_j = \emptyset$, $\text{diam}(\mathcal{A}_i) \approx 3$

2) $P_0 = \text{BlkDiag}(\mathcal{R}_i, B)$ =

3) $P = P_0 + \omega D^{-1} \tilde{A} P_0$

ColDim(P) = $3 N_{\mathcal{A}}$
⇒ smaller search space
⇒ lower $nnz(A_H)$

Graph of \tilde{A}

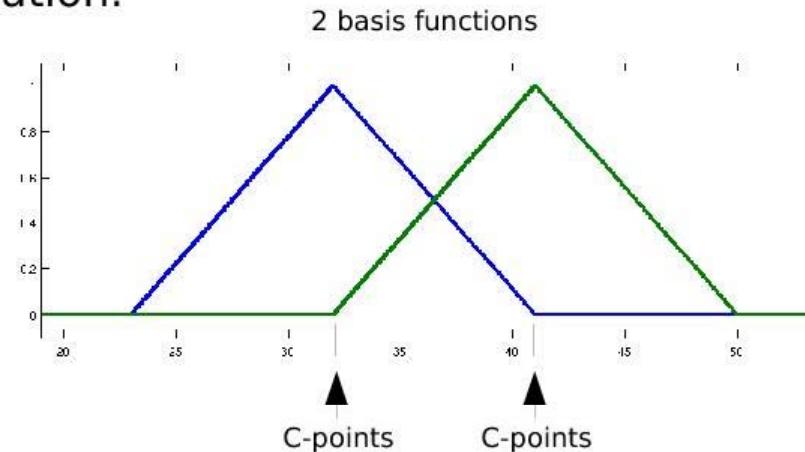
- $\text{ColDim}(B) = \text{ColDim}(\mathcal{B}_i) \Rightarrow \text{ColDim}(P) = \text{ColDim}(B) * N_{\mathcal{A}} = 6 * N_{\mathcal{A}}$
- sparsity pattern is $|\tilde{A}| / P_0$
- Should have $\tilde{A} P_0 B_c = 0$ where B_c is coarse representation of B (modes requiring accurate interpolation)
 $\Rightarrow \tilde{A} B = 0$ (as $P_0 B_c = B$)

We will also exploit ability to change norm.

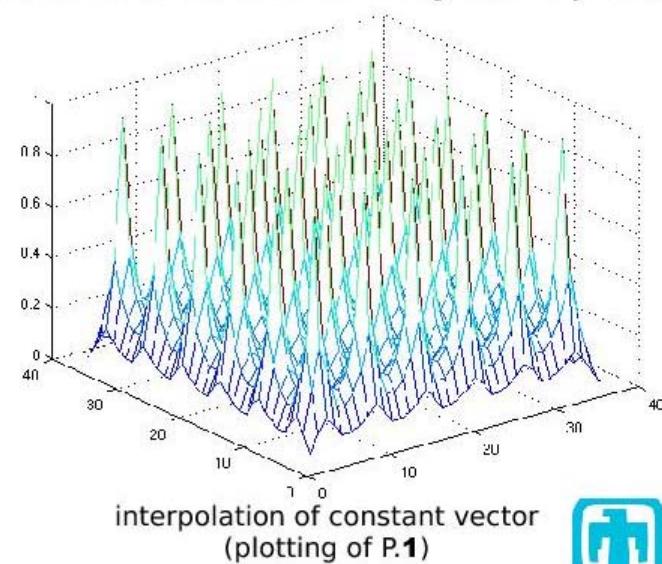
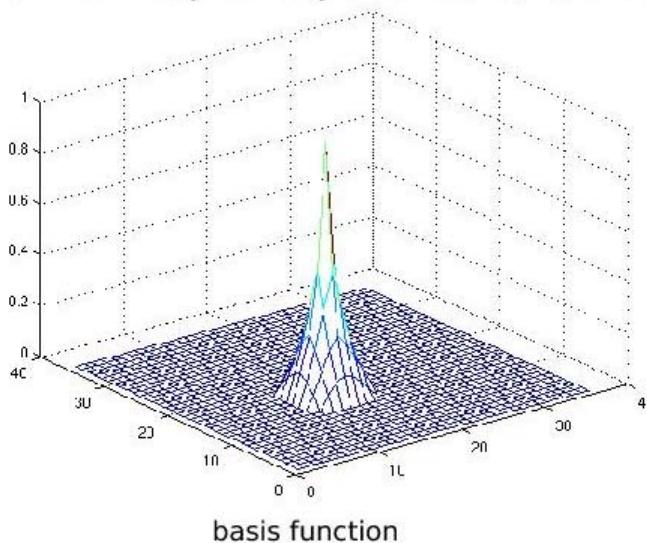


Weakly Constrained Case

- For 1D Laplace problems, constraining only at root points corresponds to linear interpolation:



- For 2D Laplace problems, constant vector is not accurately interpolated:





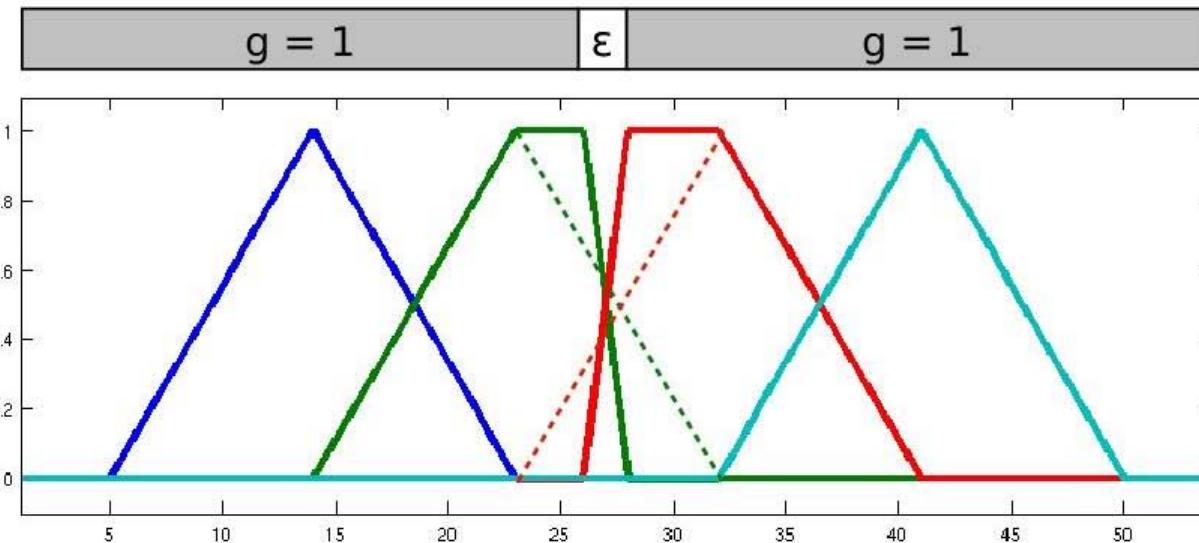
Fully constrained

Problematic if constraints do not capture physics

Example: $(g(x) u_x)_x = f$ with two constraints. If $B_{.,1} = 1, B_{.,2} = x$,
then constants and linears are exactly interpolated

exact
interpolation
vectors

$nnz(P_i) \leq 2 \Rightarrow$ fully constrained \Rightarrow linear interpolation independent of $g(x)$



Problem: fully constraining ignores energy:

- Jumps are not captured in P
- Left and right regions connected within coarse level due to interpolation across epsilon region

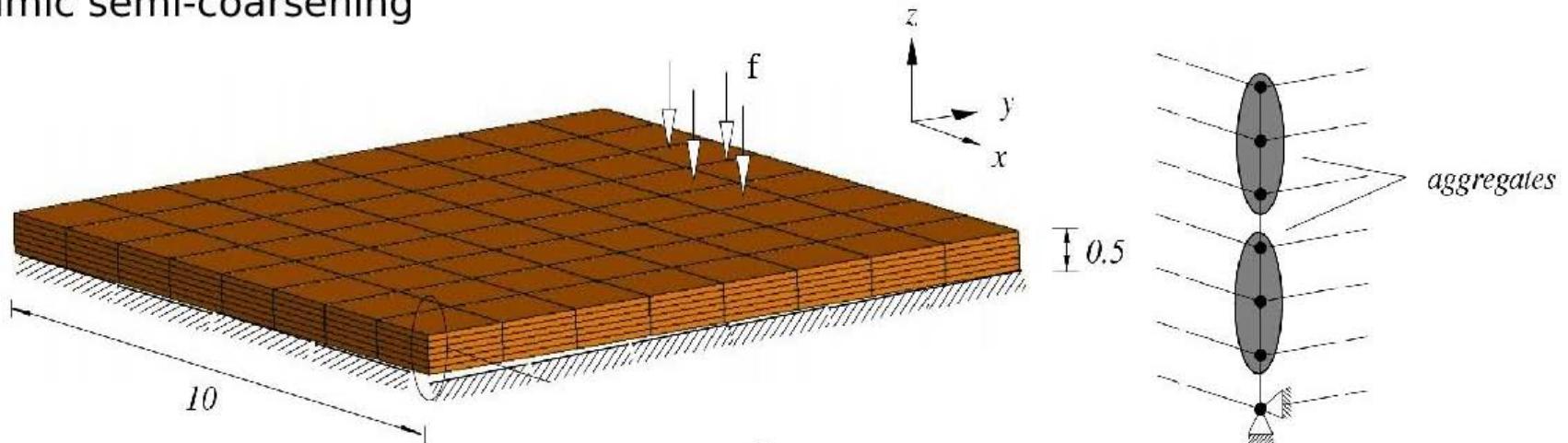


Smoothed Aggregation & General Energy Minimization

Smoothed Aggregation

- 1 step minimization
- No need to apply Q ...
... but $A P_0 B_c$ must equal 0.
- *almost* fixed sparsity pattern governed by $|A| |P_0|$
- # DOFs per node = $\dim\{N\}$

- Anisotropic problems require anisotropic coarsening and sparsity pattern to mimic semi-coarsening



This is normally accomplished by defined \tilde{A} where small (weak entries) are dropped during prolongator construction



Smoothed Aggregation & General Energy Minimization

Smoothed Aggregation

- 1 step minimization
- No need to apply $Q \dots$
... but $\tilde{A} P_0 B_c$ must equal 0.
- *almost* fixed sparsity pattern governed by $[\tilde{A} \parallel P_0]$
- # DOFs per node = $\dim\{N\}$

General Energy Minimization

- multi-step minimization
- No restriction on $\tilde{A} P_0$.
- Any sparsity pattern
- Arbitrary # DOFs per node

For elasticity:

- Proper \tilde{A} such that $\tilde{A} P_0 B_c = 0$ with weak connections dropped is non-obvious
- Anisotropic coarsening gives small aggregates \Rightarrow high operator complexities
- 3 DOFs/node on finest level ...
... but $\dim\{N\} = 6$ for 3D elasticity \Rightarrow 6 DOFs/node \Rightarrow even higher complexities



Energy-minimization - Elasticity

Lots of choices. We focus on:

3 DOFs/nodes on the coarse grid



Does smaller search space limit quality of interpolation?

- N: 6 rigid body modes (3 translations & 3 rotations)
- CG to solve $A P = 0$ (effectively defines energy)
- P_0 & sparsity pattern are smoothed aggregation inspired
 - Coarse nullspace defined by injection of fine nullspace @ root nodes
 - Initial Guess: $P_{sa0} + X^T (X X^T)^{-1} (\hat{B} - X P_{sa0})$
where P_{sa0} is smoothed aggregation P_0 for just translations
 - Sparsity Pattern: $|\tilde{A}| |P_{sa0}|$ except @ root points which are constrained to have only 1 nnz/row associated with injection
 - Avoids linear dependency issues
- \tilde{A} defined using distance Laplacian + dropping for sparsity pattern
- No need for $\tilde{A} B = 0$
- A is still used to define energy (as opposed to \tilde{A})



Experiments

- 3D Linear Elasticity, plan stress
- AMG accelerate by CG, stopping criterion $||r_{\text{relative}}|| < 10^{-10}$
- Influence of the number of energy-minimization steps to the convergence.
Problem size: 30^3 . Stretch factor: ε

# iter.	$\varepsilon = 1$	$\varepsilon = 10$	$\varepsilon = 100$
0	17	19	21
1	12	12	14
2	11	12	13
5	11	12	13
20	11	12	13



Experiments

- Comparison with Smoothed-Aggregation:
 - SA: 6 DOFs/node
 - Energy-Minimization: 3 DOFs/node, 6 nullspace vectors

Mesh	$\epsilon = 1$		$\epsilon = 10$		$\epsilon = 100$	
	SA	Emin	SA	Emin	SA	Emin
10^3	6 <i>1.30</i>	7 <i>1.07</i>	8 <i>2.81</i>	8 <i>1.22</i>	9 <i>3.21</i>	8 <i>1.24</i>
15^3	8 <i>1.19</i>	9 <i>1.05</i>	10 <i>2.32</i>	10 <i>1.15</i>	12 <i>2.54</i>	12 <i>1.16</i>
20^3	8 <i>1.24</i>	9 <i>1.06</i>	10 <i>2.59</i>	9 <i>1.18</i>	13 <i>3.05</i>	10 <i>1.20</i>
25^3	9 <i>1.26</i>	8 <i>1.07</i>	11 <i>2.76</i>	9 <i>1.20</i>	14 <i>3.04</i>	10 <i>1.20</i>
30^3	10 <i>1.22</i>	11 <i>1.05</i>	12 <i>2.52</i>	12 <i>1.17</i>	15 <i>3.06</i>	13 <i>1.19</i>
35^3	10 <i>1.24</i>	10 <i>1.06</i>	12 <i>2.66</i>	12 <i>1.18</i>	16 <i>3.03</i>	13 <i>1.19</i>
40^3	10 <i>1.26</i>	9 <i>1.06</i>	12 <i>2.77</i>	12 <i>1.19</i>	16 <i>3.21</i>	11 <i>1.21</i>

Tab. : Iteration count and complexity (lower complexity = faster run time) for SA and energy minimization for various mesh sizes and stretch factors.

$$\text{complexity: } \frac{\sum_i \text{nnz}(A_i)}{\text{nnz}(A)}$$



Conclusions

- Krylov minimization can be used to generate “energy” minimizing prolongators/restrictors for symmetric & non-symmetric systems
 - CG, GMRES
- Some linear algebra issues ...
- Flexibility
 - Coarsening, e.g. F/C aggregation, irregular
 - Grid transfer sparsity patterns
 - Norms defining energy

* sparsity pattern & energy norm flexibility used to XFEM
ice fracture problem

* sparsity pattern and dimension of P flexibility used for anisotropic elasticity