

# **Evaluation of a Six-DOF Electrodynamic Shaker System**

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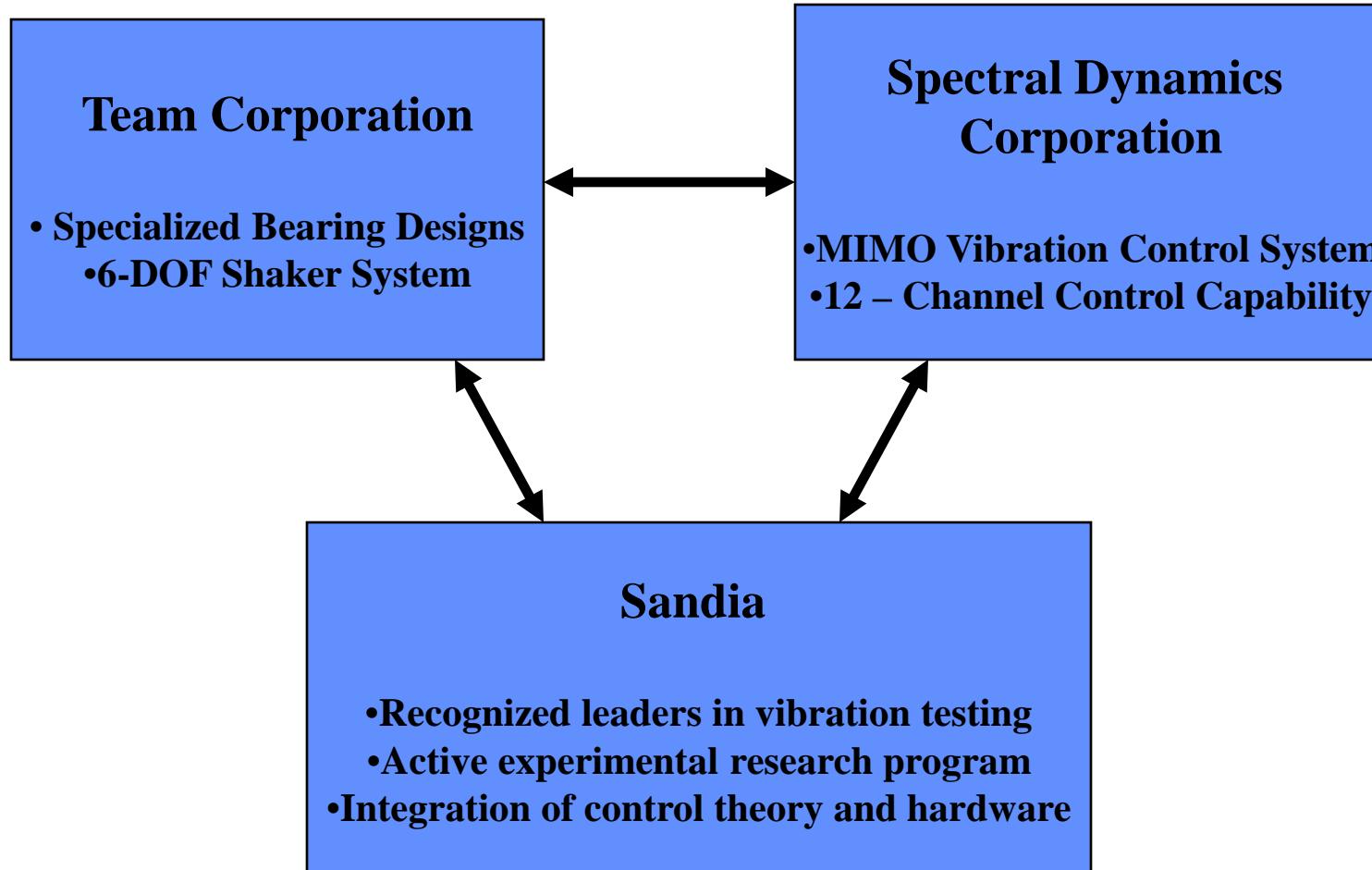


# Why is it important?

- Real shock and vibration environments are multidimensional (6 degrees-of-freedom)
  - 3 translations and 3 rotations
- Single axis testing will not excite the modes of the system (or component) the same way they are excited in the real environment
  - Resulting stress states are not the same
  - Failure modes of system may be missed
    - The assumption that sequential testing in three axes is equivalent is not correct!
- Improved model validation experiments
  - Improved control of boundary conditions (multiple excitors)
    - Forces and moments available to tailor boundary conditions
      - Approach idealized boundary conditions used in models such as fixed-free
        - Single axis shaker tests are not really single axis
  - Selectively provide single or coupled loadings to structure
    - Full definition of input including rotations
      - Ignored in the past



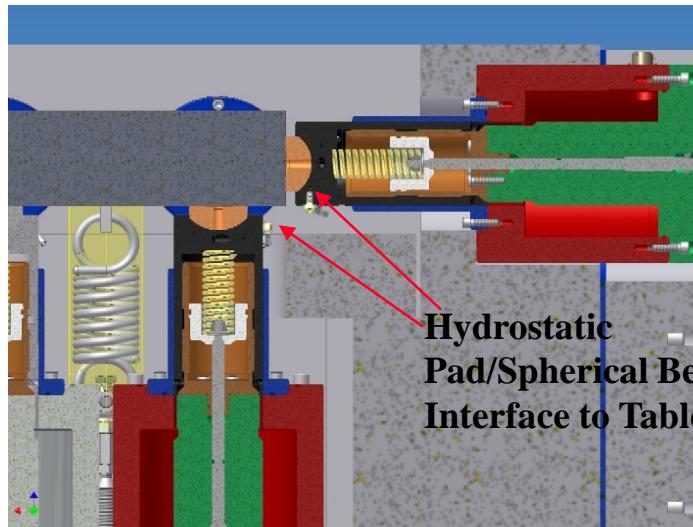
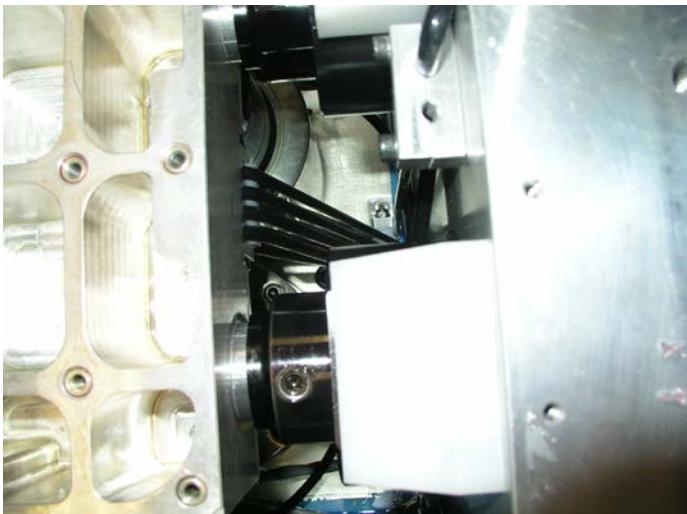
# Collaboration for Theory, Hardware, Environmental Specification and Control



# Team Tensor TE6-900 6-DOF Shaker System



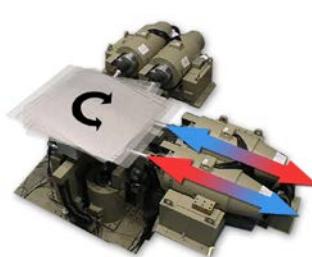
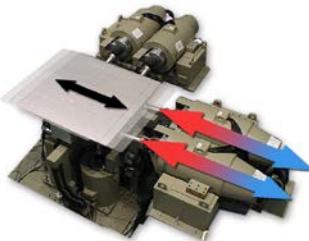
TE6-900 Specifications		
	English Units	SI Units
<b>STROKE</b>	+/-0.25 inch	+/-6.4 mm
<b>ROTATION</b>	+/-5.0 deg.	.09 rad.
<b>VELOCITY</b>	60 in/sec	1525 mm/sec
<b>FORCE</b>	200 lbf	890 N
<b>TABLE WT.</b>	9.02 lbs	4.09 kg



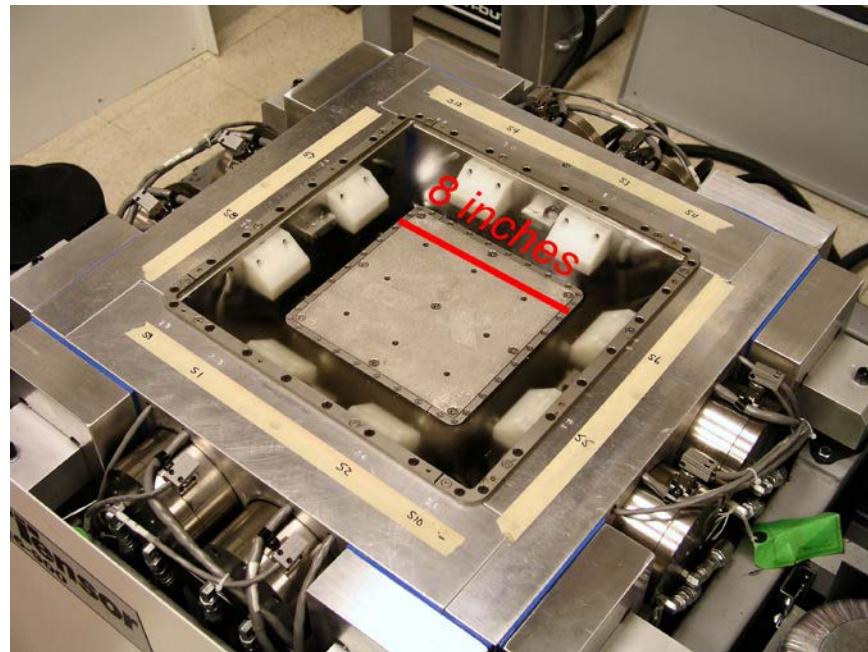
# 6- DOF System with Top Cover Removed

Utilizes 12 Independent Electrodynmaic  
Exciters with Hydraulic Bearing  
Assemblies:

- 4 - Vertical Shakers
- 8 - Horizontal Shakers (4 per axis)



Selecting phase relationships  
between exciters will generate  
translations and/or rotations

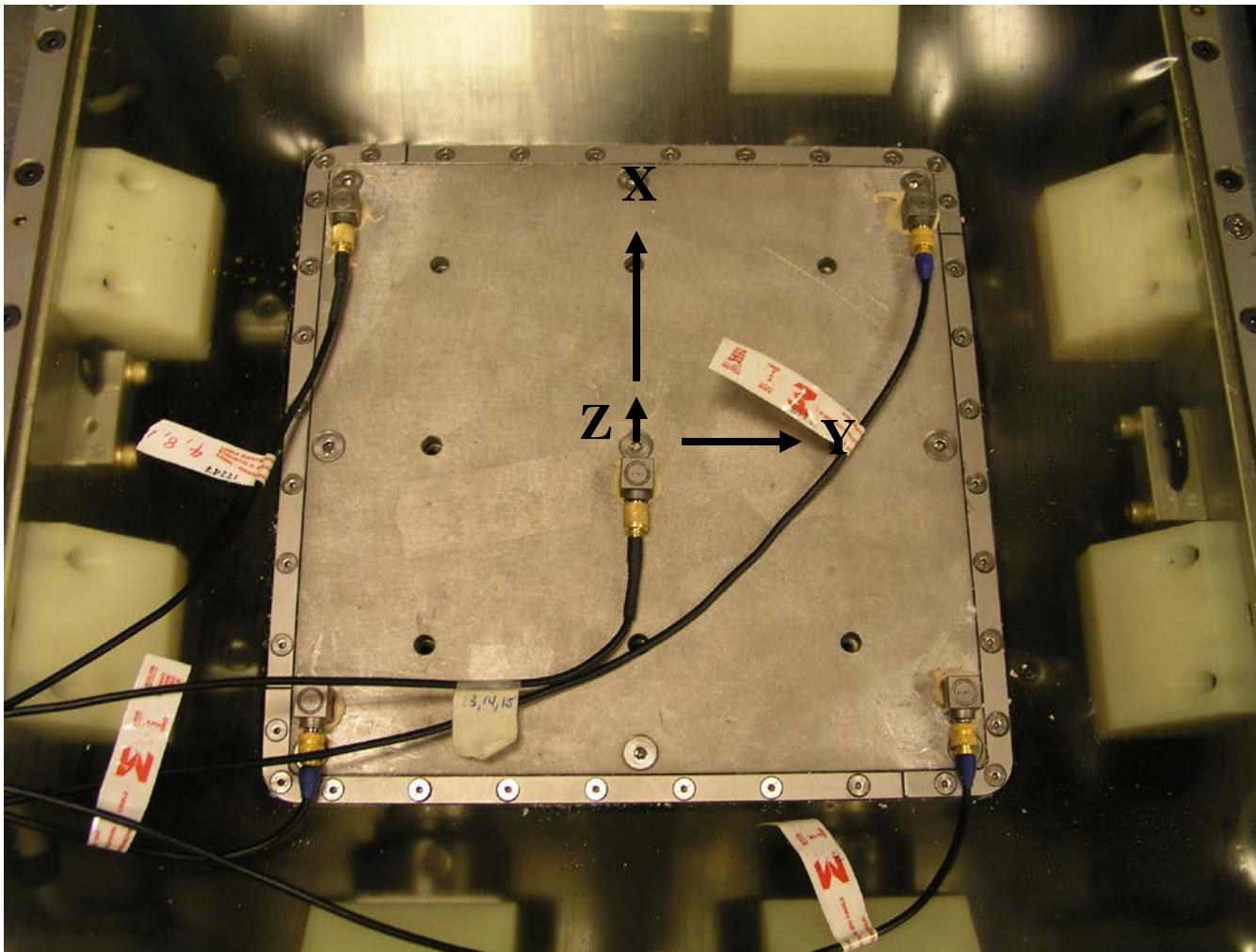


## 12-actuators/6-DOF's

- Provides Over-determined system
- Versatility to specify control methods tailored to test objectives

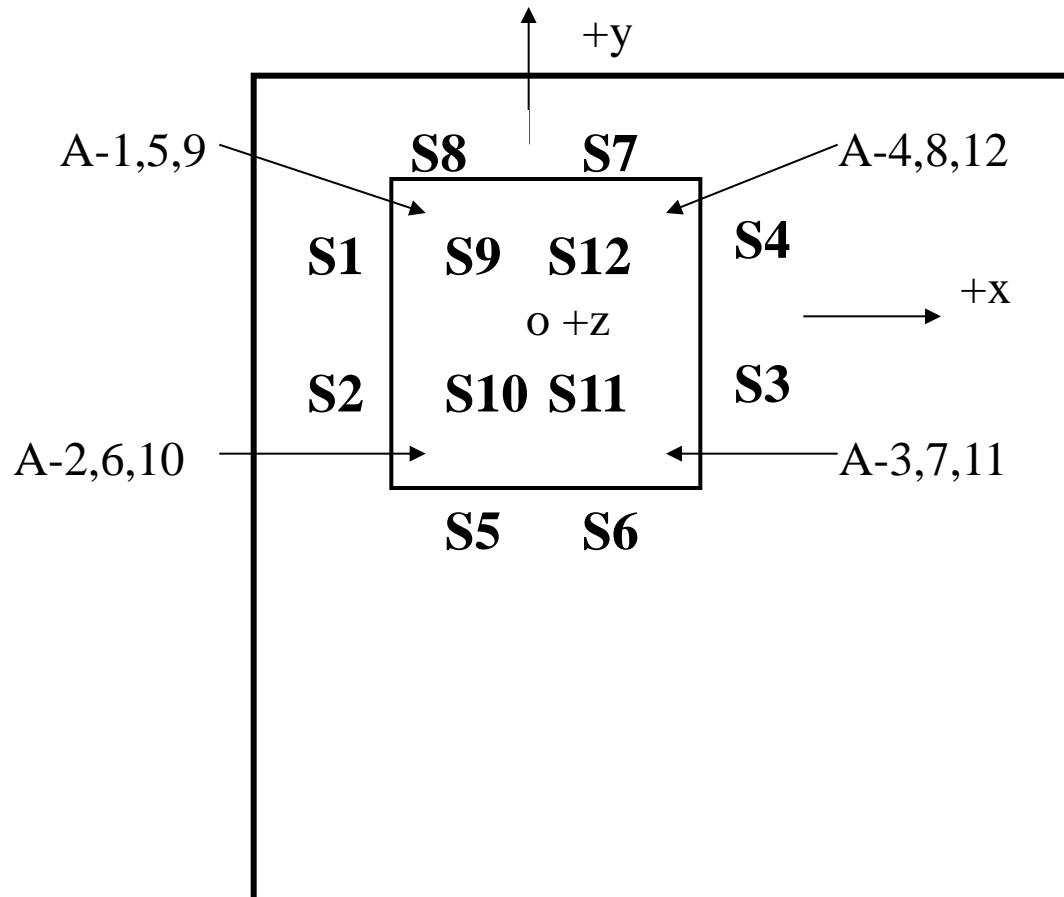


# Location of control accelerometers





# Accelerometer and Shaker Numbering Convention





**Input/output transformation matrices were used to convert 12 accelerometers and 12 shakers to a 6x6 rigid body control matrix**

**Accel to mode**

1/4	1/4	1/4	1/4	0	0	0	0	0	0	0	0	0
0	0	0	0	1/4	1/4	1/4	1/4	0	0	0	0	0
0	0	0	0	0	0	0	0	1/4	1/4	1/4	1/4	1/4
0	0	0	0	0	0	0	0	1/4	-1/4	-1/4	-1/4	1/4
0	0	0	0	0	0	0	0	1/4	1/4	-1/4	1/4	1/4
-1/8	1/8	1/8	-1/8	-1/8	-1/8	1/8	1/8	0	0	0	0	0



**Input/output transformation matrices were used to convert 12 accelerometers and 12 shakers to a 6x6 rigid body control matrix**

**Output transformation matrix (Mode to Shaker)<sup>-1</sup>**

1/4	1/4	-1/4	-1/4	0	0	0	0	0	0	0	0	0
0	0	0	0	1/4	1/4	-1/4	-1/4	0	0	0	0	0
0	0	0	0	0	0	0	0	1/4	1/4	1/4	1/4	1/4
0	0	0	0	0	0	0	0	1/4	1/4	-1/4	-1/4	-1/4
0	0	0	0	0	0	0	0	1/4	1/4	-1/4	1/4	1/4
-1/8	1/8	-1/8	1/8	-1/8	1/8	-1/8	1/8	0	0	0	0	0

# Typical impedance function

$0.2v/g$

x-translation

$0.01v/g$

$0.2v/g$

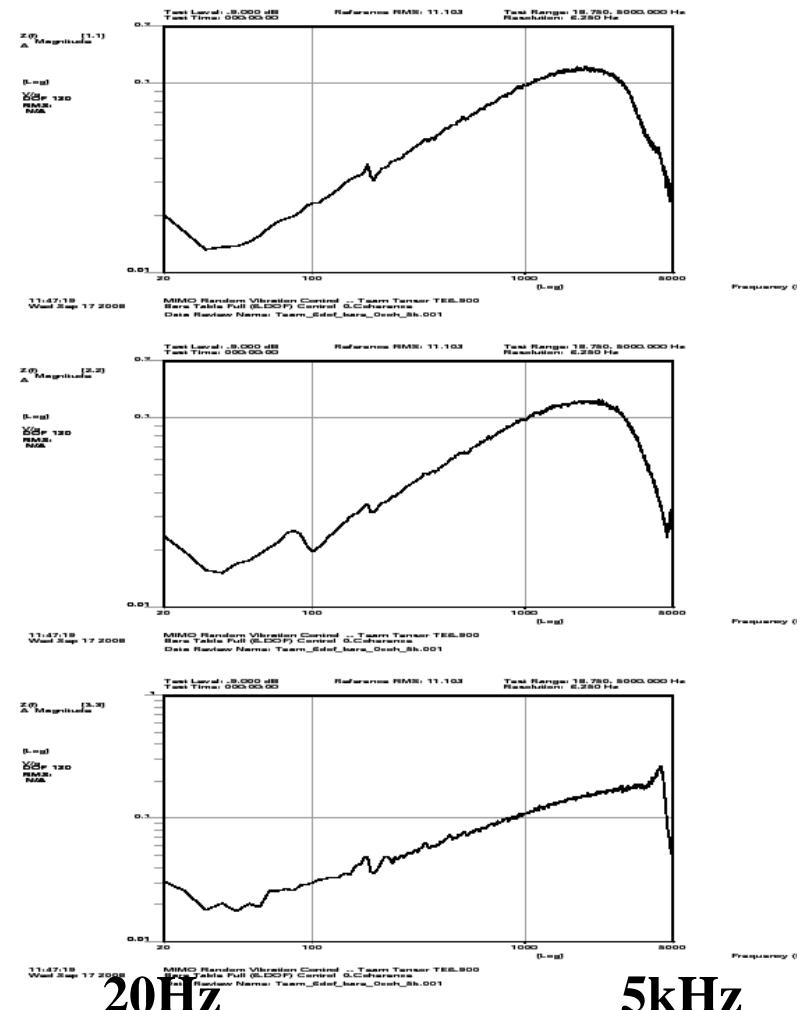
y-translation

$0.01v/g$

$1 v/g$

z-translation

$0.01v/g$



# Rotation impedance functions

0.2v/g

rotation about x

0.01v/g

0.2v/g

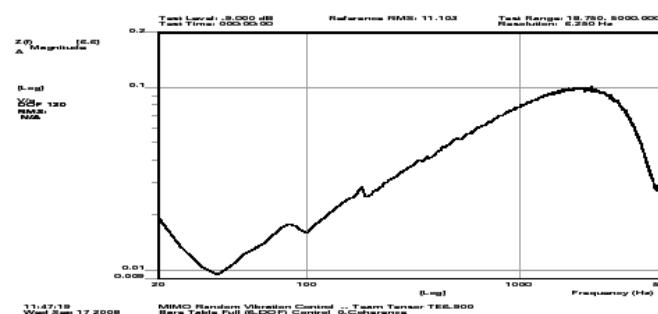
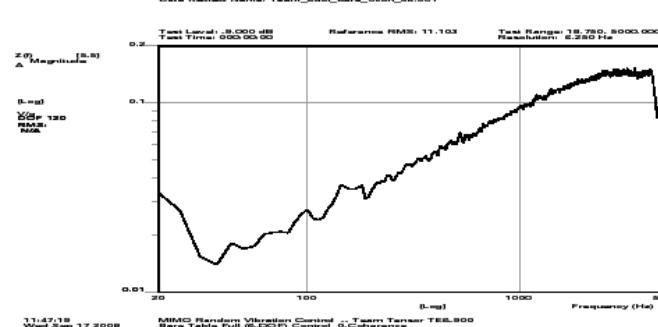
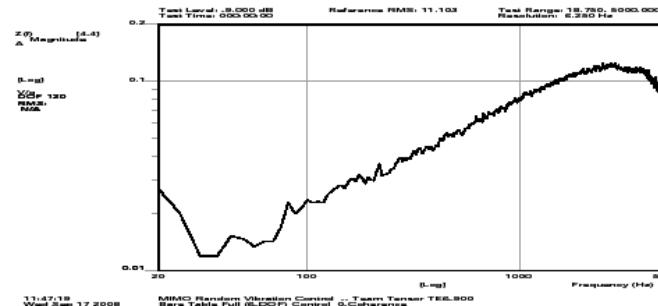
rotation about y

0.01v/g

0.2 v/g

rotation about z

0.01v/g



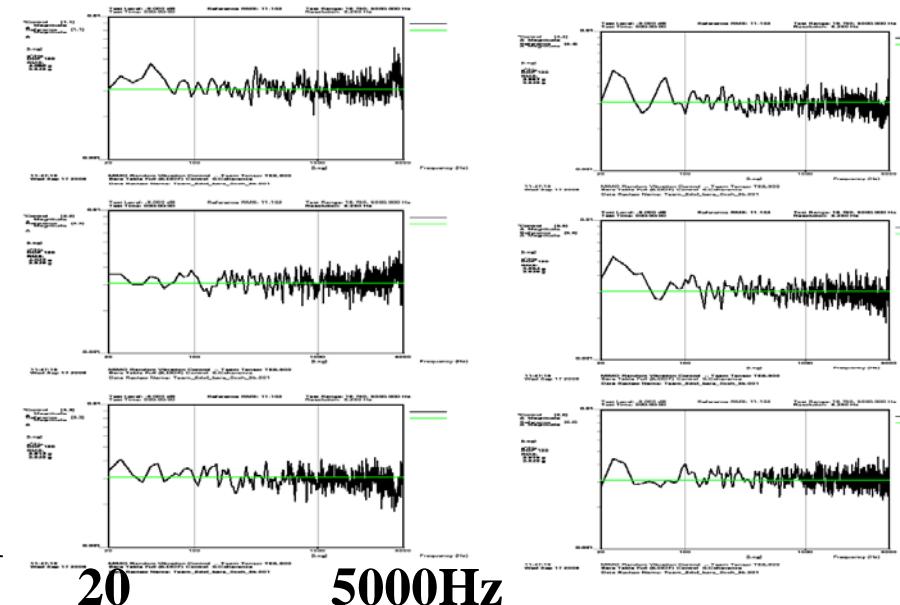
20Hz

5kHz

# Results

- Successful Demonstration of full 6-Dof closed loop random vibration test
  - Independent power spectrums controlled for three translations and three rotations
  - First time 12 shakers have been simultaneously controlled to 5000 Hz
  - 4grms

## Translations



## Rotations

All vertical  
scales  
 $g^2/Hz$

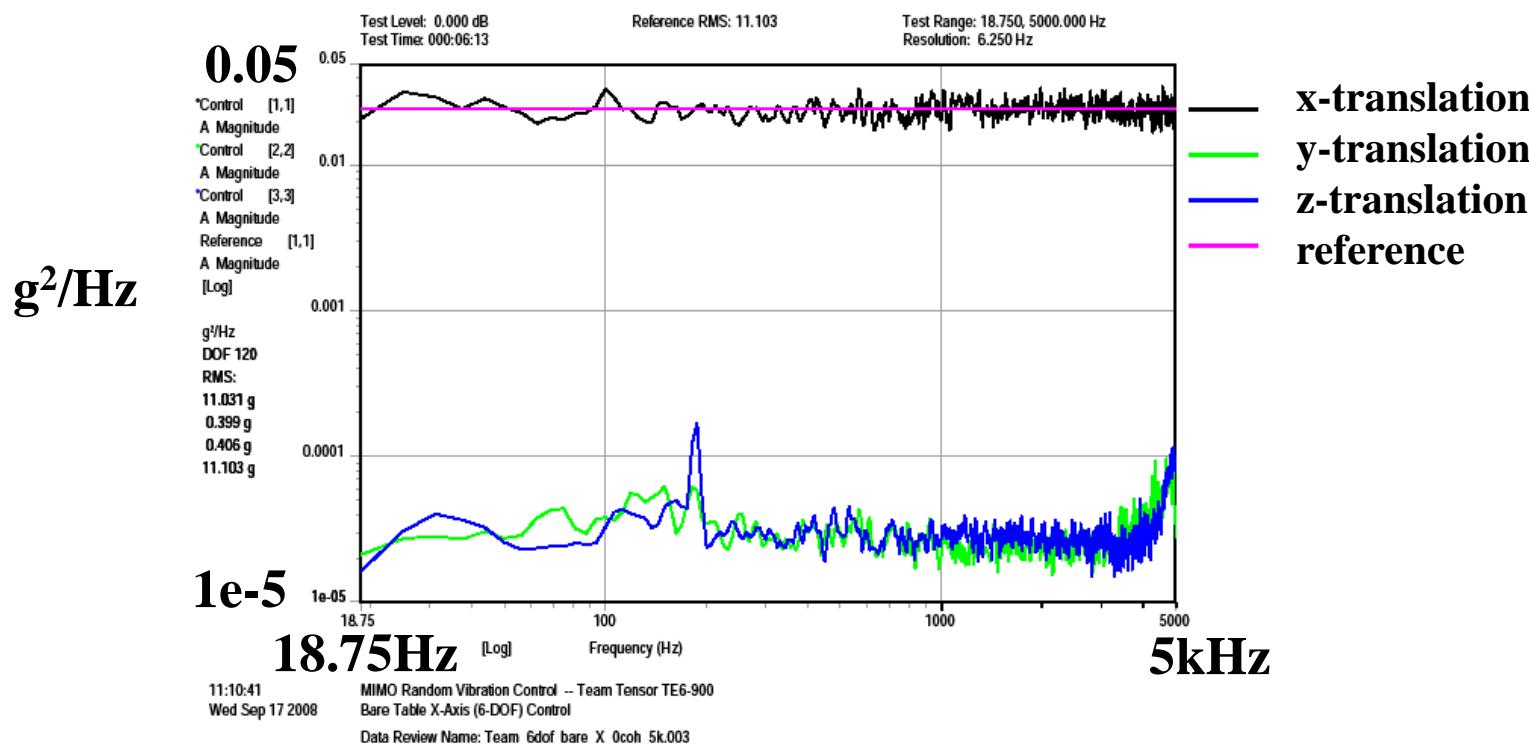
0.01

0.001

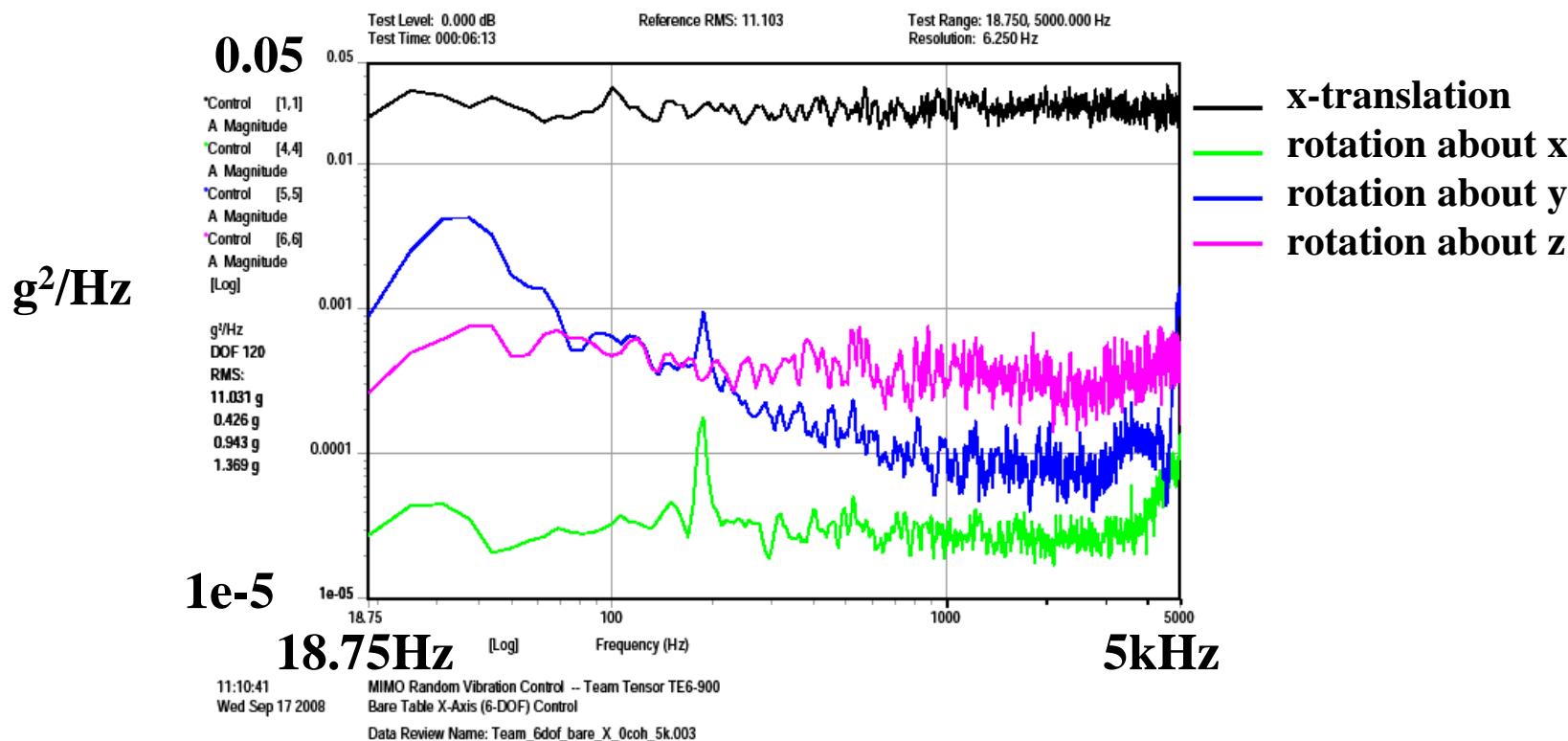
20

5000Hz

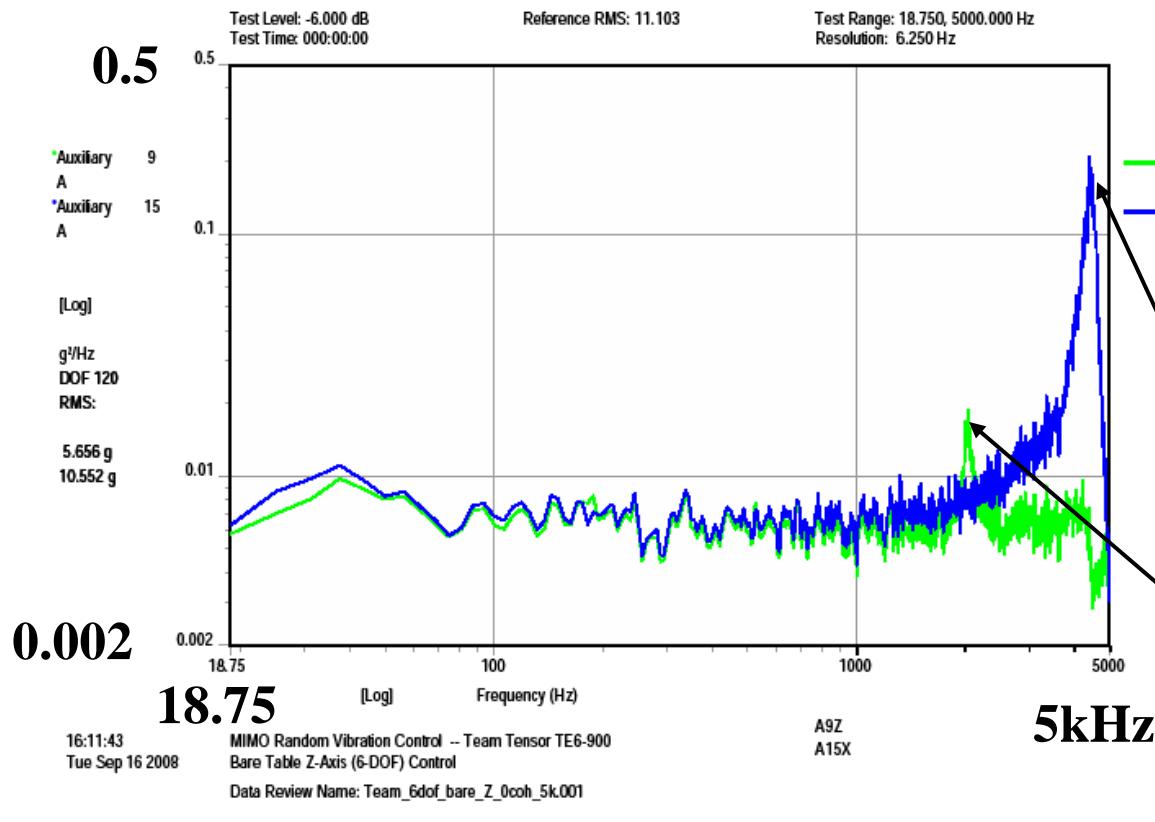
# X-axis test with other degrees of freedom restrained



# X-axis test with other degrees of freedom restrained



# We have identified two table modes below 5kHz

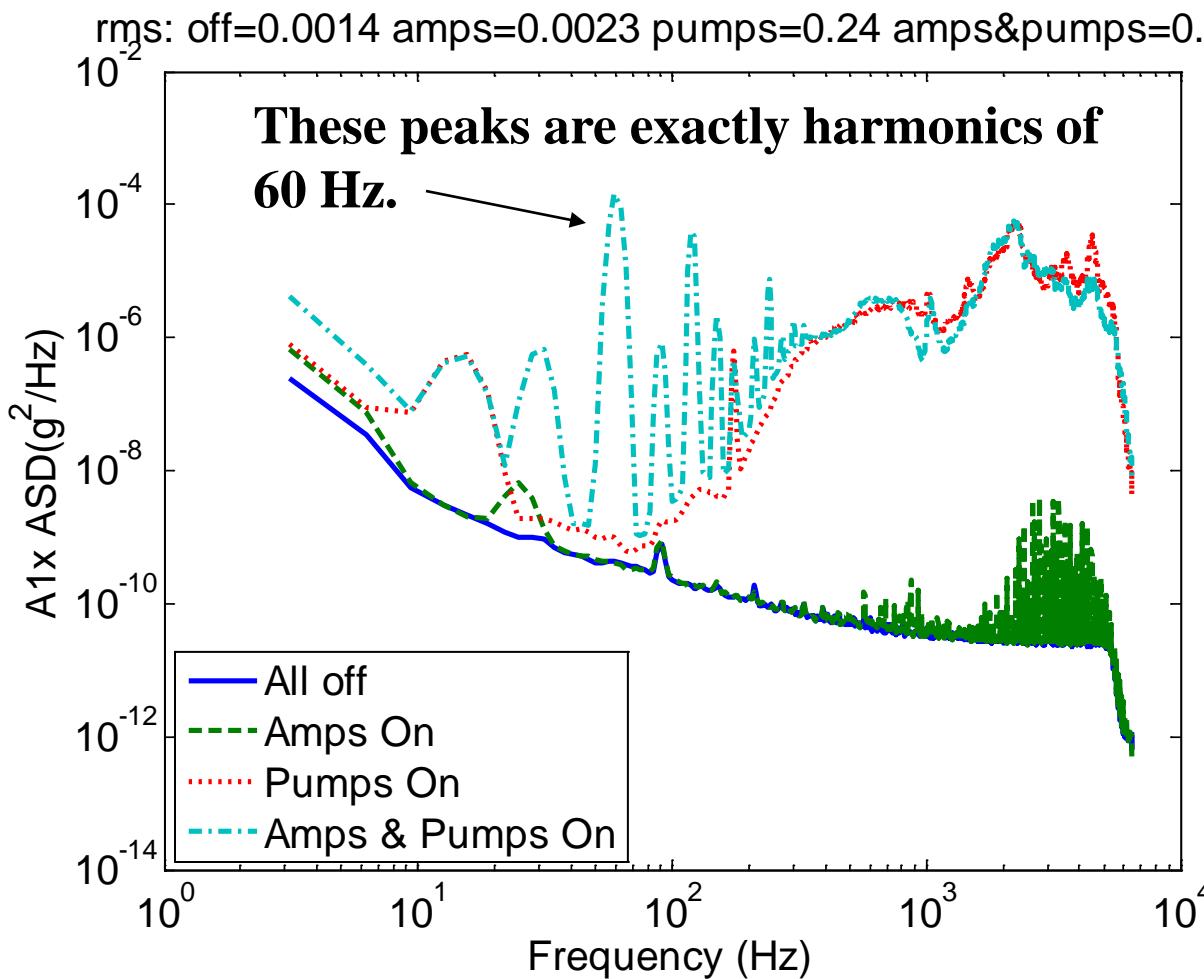


one z-axis control accel.  
z-axis accel. at center of table

We have a plate diaphragm mode at 4381Hz

We have a table torsion mode at 2031Hz. Note center accel. does not respond

# Noise Floor Measurement



Every thing looks pretty good until we turn the pumps on.

We are actively searching for the source.

It suggests a ground loop somewhere.

In spite of the noise control was pretty good.



# Desired Shaker Design Improvements

- **Output current and voltage signals available**
  - Very difficult to access system capability without these measurements
  - Assist in optimizing the control strategy
- **Master gain control on each amplifier**
  - Balance the control system drive outputs
- **Separate hydraulic power supply from shaker cabinet**
  - Reduce system noise
- **Improved access to all electrical connectors to allow better trouble-shooting**
- **Interlock to prevent field current when pumps are off**
- **Improved technique for establishing cord tensions to achieve desired preload/position**
- **BIGGER SYSTEM (Same Cost---- Fat Chance!)**



# Desired Control System Improvements

- Improved diagnostic tools to verify system integrity
  - State of health checks
    - Comparison of impedance functions from previous tests
    - Ability to view FRF's (Inverse of Impedance) directly---More intuitive
    - Other
  - Export FRF's and Impedance for offline computations
- Ability to specify any set of accelerometers as controls (not necessarily starting with channel one)
  - Re-patching channels increases chances for error
- Improved description of error messages



# Lessons Learned

- **Correct Setup is Critical**
  - Inoperative accelerometer or shaker is deadly
  - Accelerometers
    - Sensitivities, polarity, location
- **Careful thought must be given to design of the experiment**
  - Selection and definition of control strategy can greatly affect the results



## Summary

- Team 6-Dof system is installed and operational
- System performance evaluated
  - All six degrees of freedom have been achieved
  - 5 kHz closed loop random vibration control has been demonstrated for all three translations and three rotations
- 6-Dof system shows great promise for the future



# Publications Regarding Benefits of Realistic Multi-axis Environments

- **Multi-axis testing excites all modes simultaneously with a more realistic stress loading** (Berman, M.B. "Inadequacies in Uniaxial Stress Screen Vibration Testing." *Journal of the IEST*. Vol. 44, No. 4, Fall 2001: 20-23)
- **Test objects may pass uni-axial testing but fail under operating conditions** (Freeman, M.T. "3-axis Vibration Test System Simulates Real World" *Test Engineering and Management*. Dec/Jan 1990-91: 10-14)
- **Rate of fatigue damage is increased by a factor of two with three axis excitation** (Himelblau, H. and M.J. Hine. "Effects of Triaxial and Uniaxial Random Excitation on the Vibration Response and Fatigue Damage of Typical Spacecraft Hardware". *Proceedings of the 66<sup>th</sup> Shock and Vibration Symposium*. Arlington, VA: SAVIAC 1995)
- **Durability of objects vary when exposed to sequential vs. simultaneous excitation** (French, M. "Comparison of Simultaneous and Sequential Single Axis Durability": To be published in *Experimental Techniques*, November 2006)