

Evaluation of a Six-DOF Electrodynamic Shaker System

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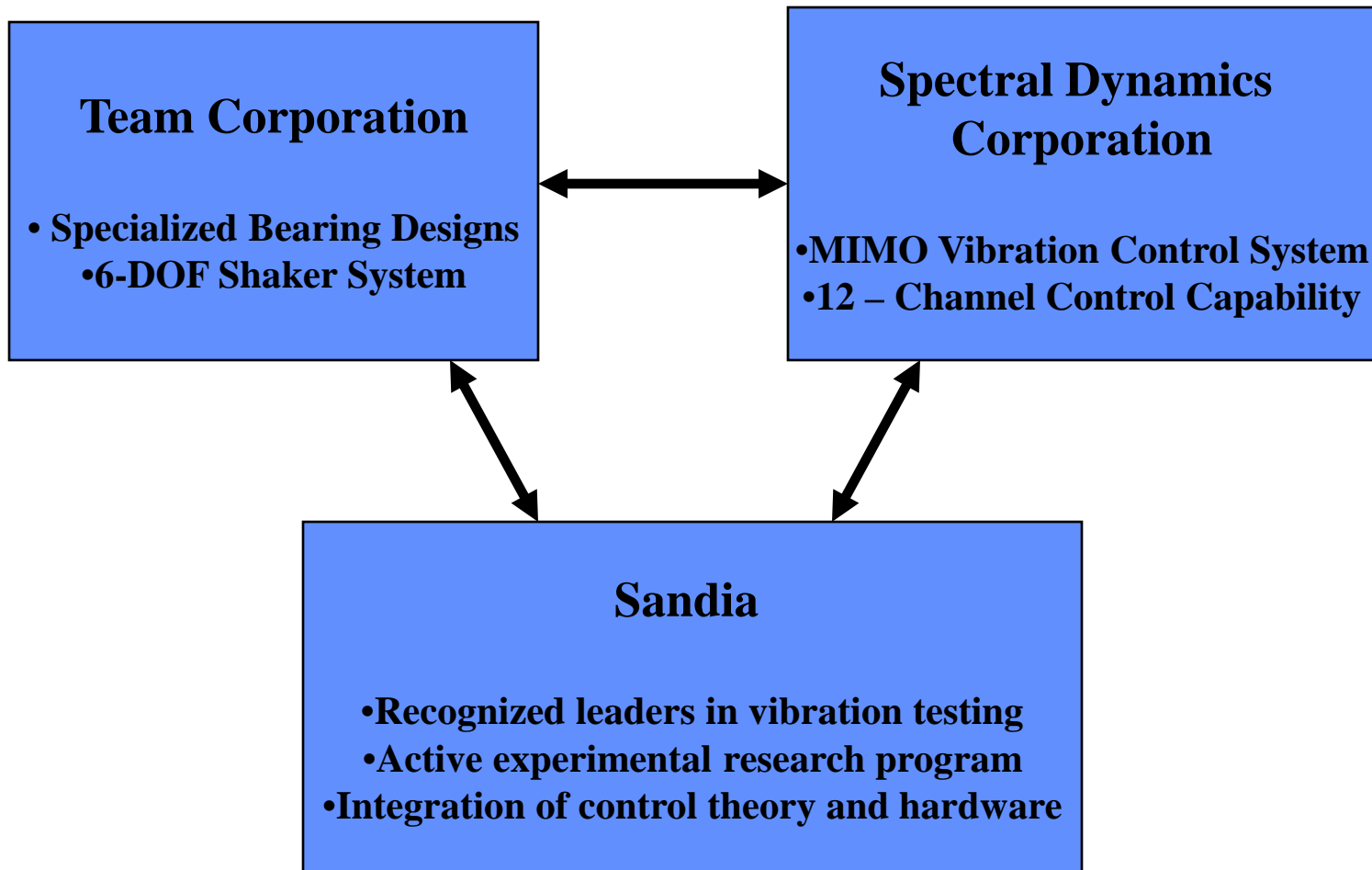


Why is it important?

- Real shock and vibration environments are multidimensional (6 degrees-of-freedom)
 - 3 translations and 3 rotations
- Single axis testing will not excite the modes of the system (or component) the same way they are excited in the real environment
 - Resulting stress states are not the same
 - Failure modes of system may be missed
 - The assumption that sequential testing in three axes is equivalent is not correct!
- Improved model validation experiments
 - Improved control of boundary conditions (multiple exciters)
 - Forces and moments available to tailor boundary conditions
 - Approach idealized boundary conditions used in models such as fixed-free
 - Single axis shaker tests are not really single axis
 - Selectively provide single or coupled loadings to structure
 - Full definition of input including rotations
 - Ignored in the past



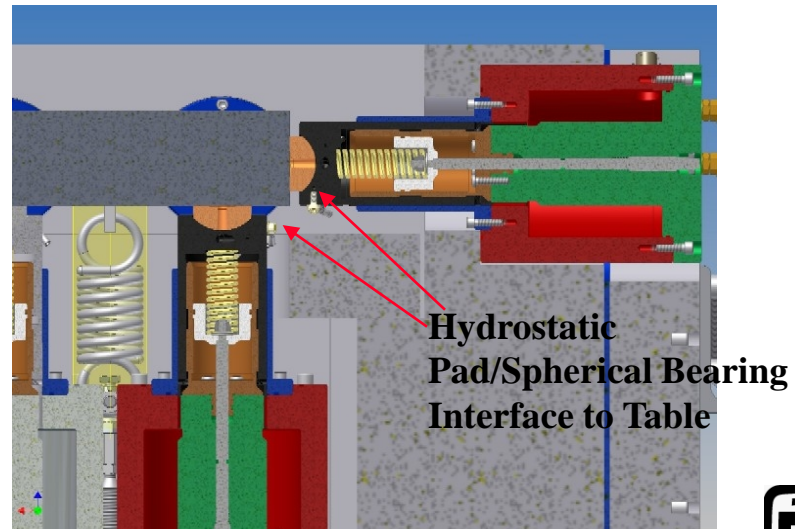
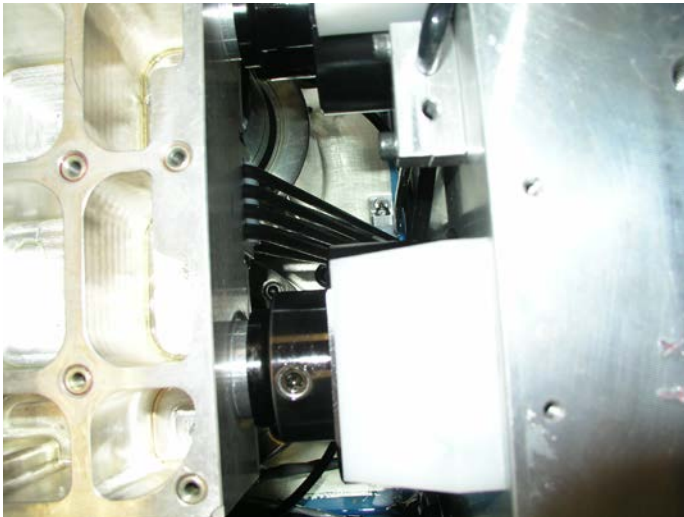
Collaboration for Theory, Hardware, Environmental Specification and Control



Team Tensor TE6-900 6-DOF Shaker System



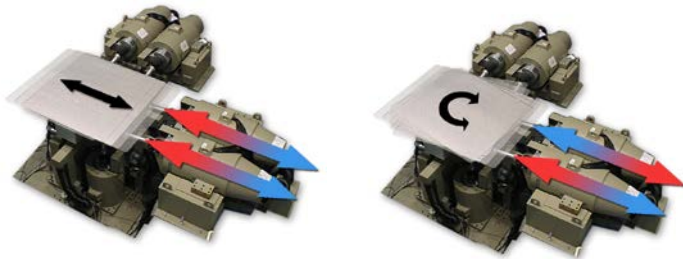
TE6-900 Specifications		
	English Units	SI Units
STROKE	+/-0.25 inch	+/-6.4 mm
ROTATION	+/-5.0 deg.	.09 rad.
VELOCITY	60 in/sec	1525 mm/sec
FORCE	200 lbf	890 N
TABLE WT.	9.02 lbs	4.09 kg



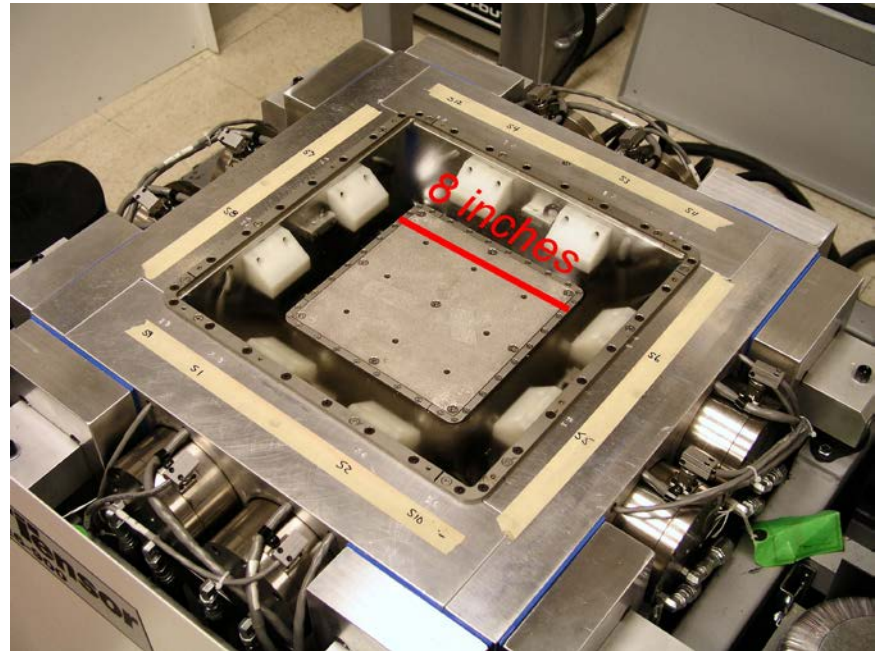
6- DOF System with Top Cover Removed

Utilizes 12 Independent Electrodynamic Exciters with Hydraulic Bearing Assemblies:

- 4 - Vertical Shakers
- 8 - Horizontal Shakers (4 per axis)



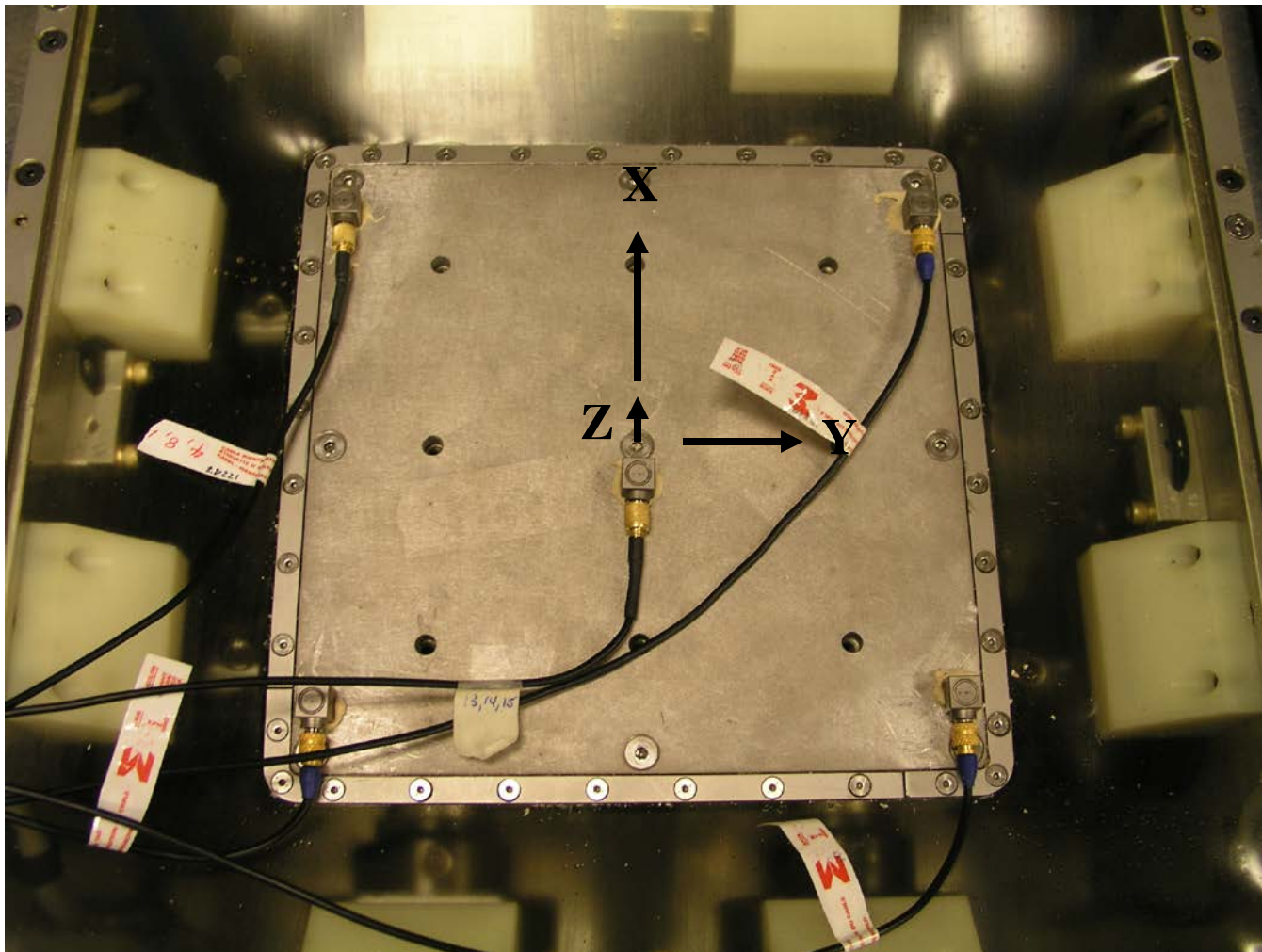
Selecting phase relationships between exciters will generate translations and/or rotations



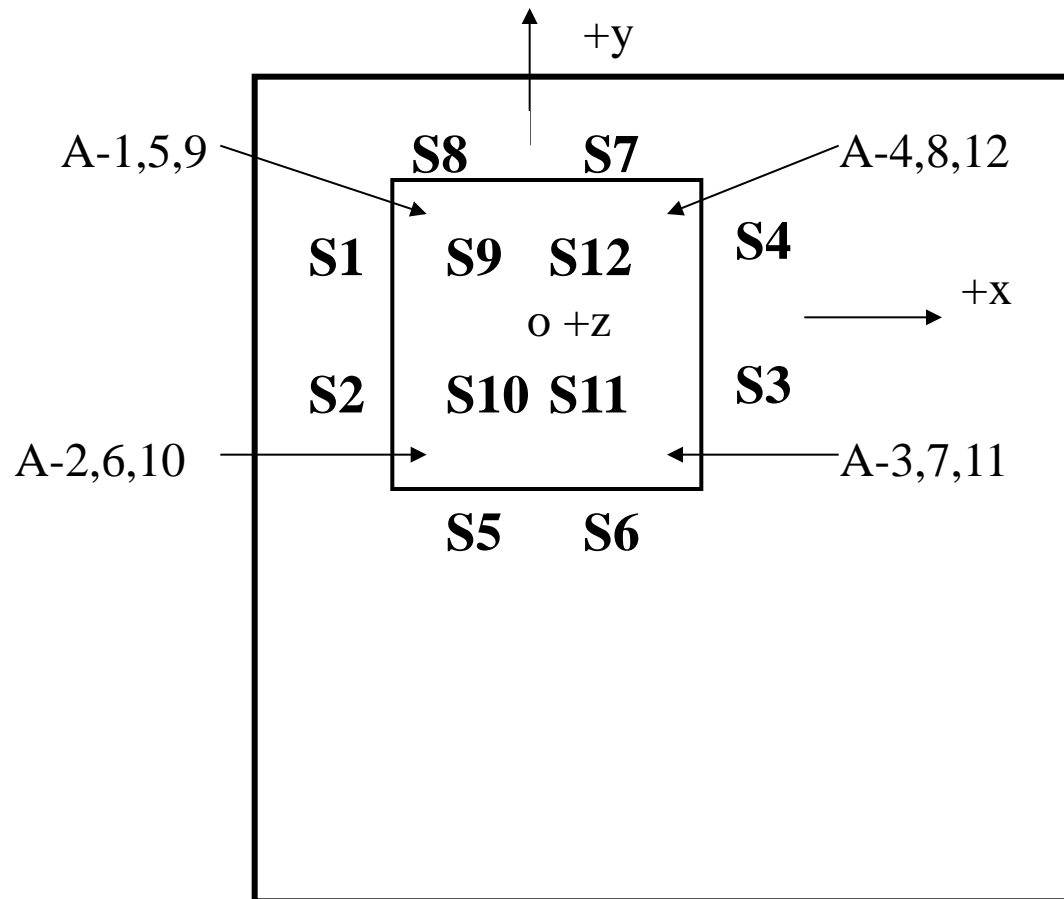
12-actuators/6-DOF's

- Provides Over-determined system
- Versatility to specify control methods tailored to test objectives

Location of control accelerometers



Accelerometer and Shaker Numbering Convention





Input/output transformation matrices were used to convert 12 accelerometers and 12 shakers to a 6x6 rigid body control matrix

Accel to mode

$1/4$	$1/4$	$1/4$	$1/4$	0	0	0	0	0	0	0	0
0	0	0	0	$1/4$	$1/4$	$1/4$	$1/4$	0	0	0	0
0	0	0	0	0	0	0	0	$1/4$	$1/4$	$1/4$	$1/4$
0	0	0	0	0	0	0	0	$1/4$	$-1/4$	$-1/4$	$1/4$
0	0	0	0	0	0	0	0	$1/4$	$1/4$	$-1/4$	$1/4$
$-1/8$	$1/8$	$1/8$	$-1/8$	$-1/8$	$-1/8$	$1/8$	$1/8$	0	0	0	0



Input/output transformation matrices were used to convert 12 accelerometers and 12 shakers to a 6x6 rigid body control matrix

Output transformation matrix (Mode to Shaker)⁻¹

1/4	1/4	-1/4	-1/4	0	0	0	0	0	0	0	0
0	0	0	0	1/4	1/4	-1/4	-1/4	0	0	0	0
0	0	0	0	0	0	0	0	1/4	1/4	1/4	1/4
0	0	0	0	0	0	0	0	1/4	1/4	-1/4	-1/4
0	0	0	0	0	0	0	0	1/4	1/4	-1/4	1/4
-1/8	1/8	-1/8	1/8	-1/8	1/8	-1/8	1/8	0	0	0	0

Typical impedance function

0.2v/g
x-translation

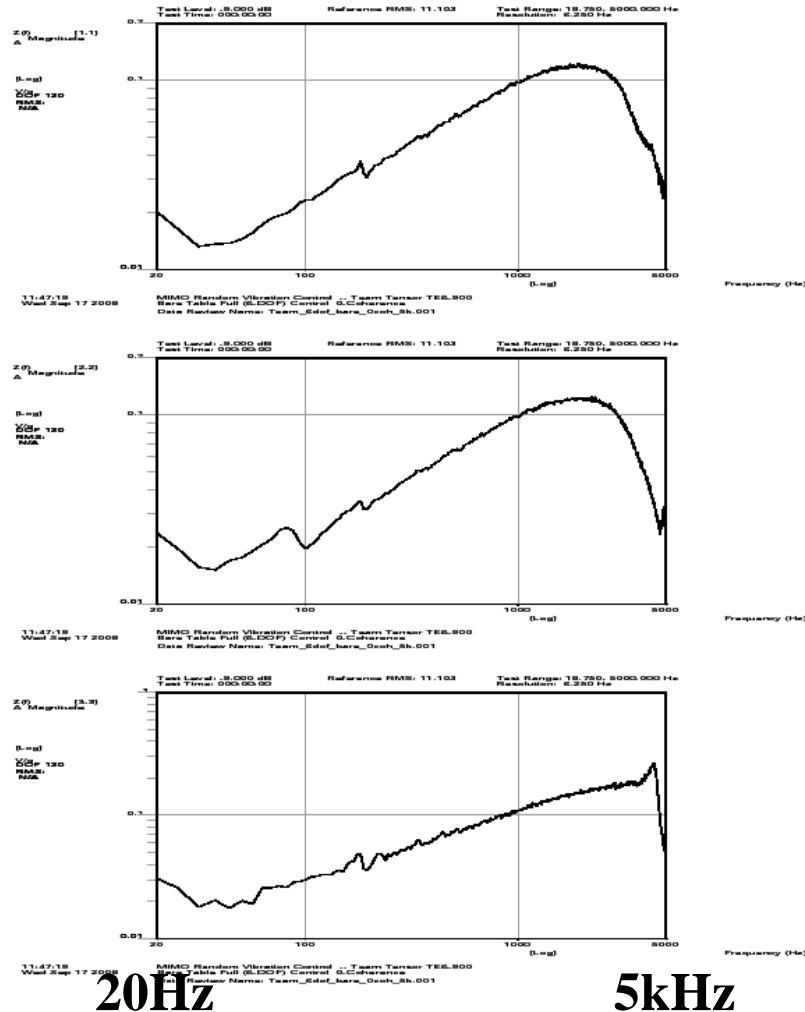
0.01v/g

0.2v/g
y-translation

0.01v/g

1 v/g
z-translation

0.01v/g



Rotation impedance functions

0.2v/g

rotation about x

0.01v/g

0.2v/g

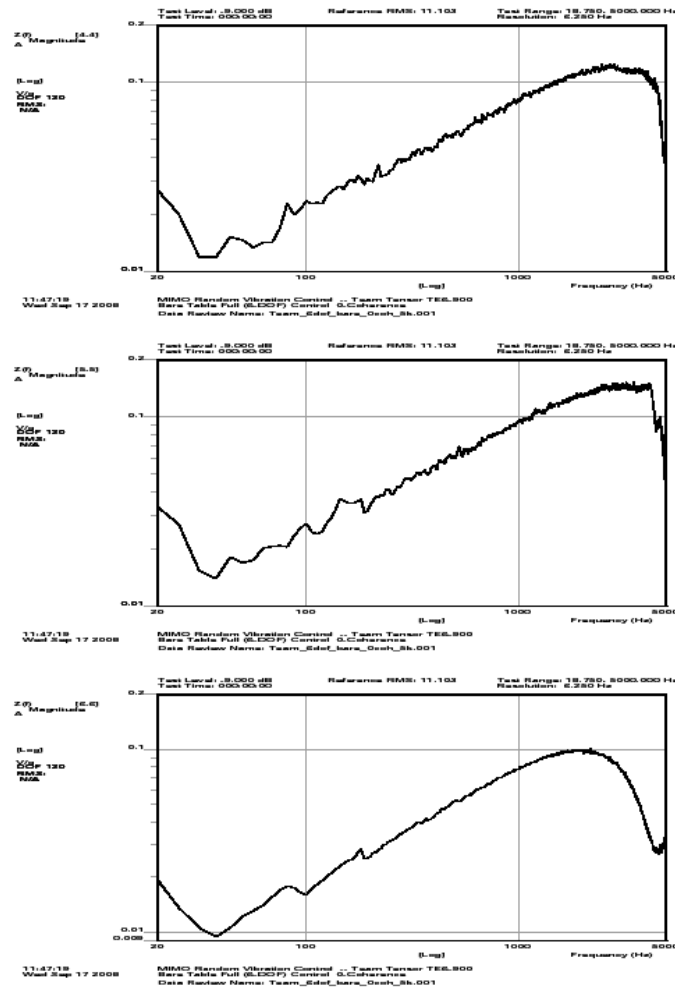
rotation about y

0.01v/g

0.2 v/g

rotation about z

0.01v/g



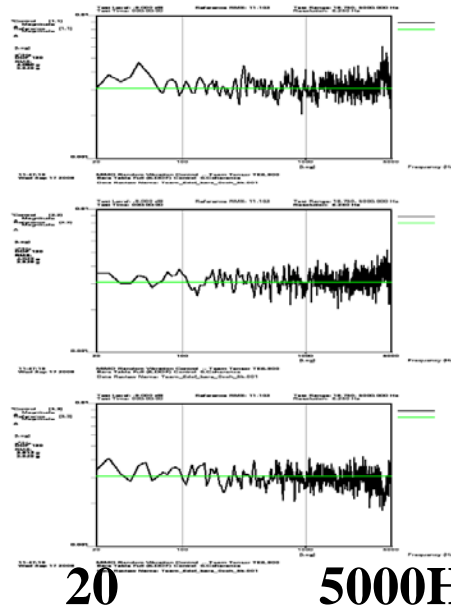
20Hz

5kHz

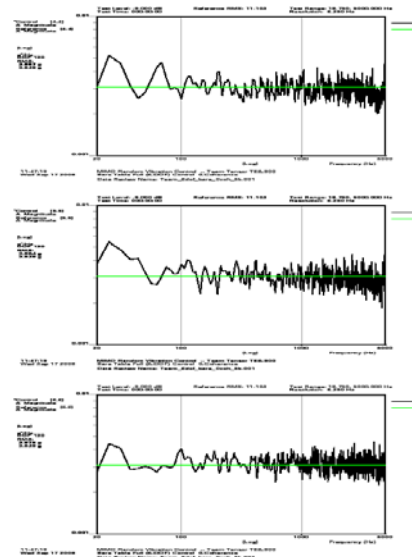
Results

- **Successful Demonstration of full 6-Dof closed loop random vibration test**
 - Independent power spectrums controlled for three translations and three rotations
 - **First time 12 shakers have been simultaneously controlled to 5000 Hz**
 - **4grms**

Translations



Rotations



All vertical
scales
 g^2/Hz

0.01

0.001

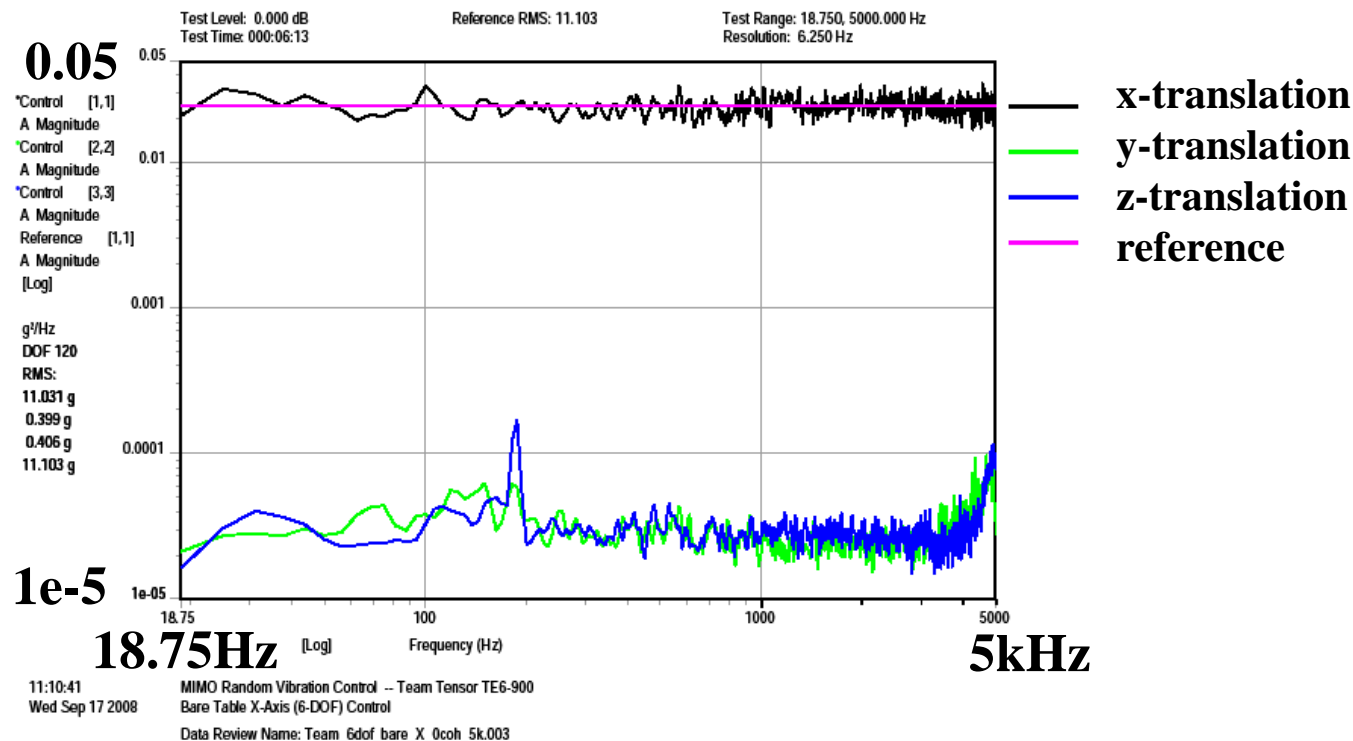
20

5000Hz

All frequency axes

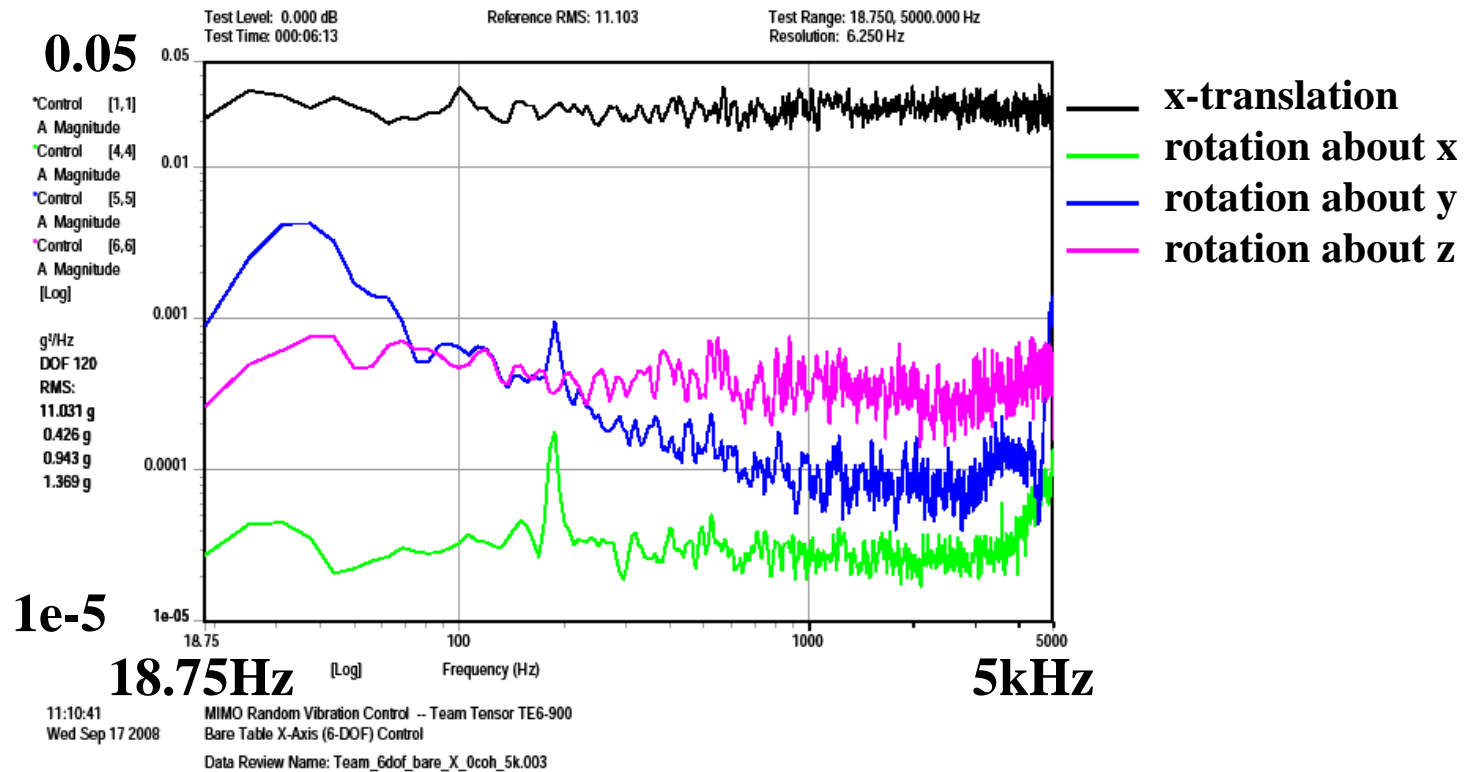
X-axis test with other degrees of freedom restrained

g^2/Hz

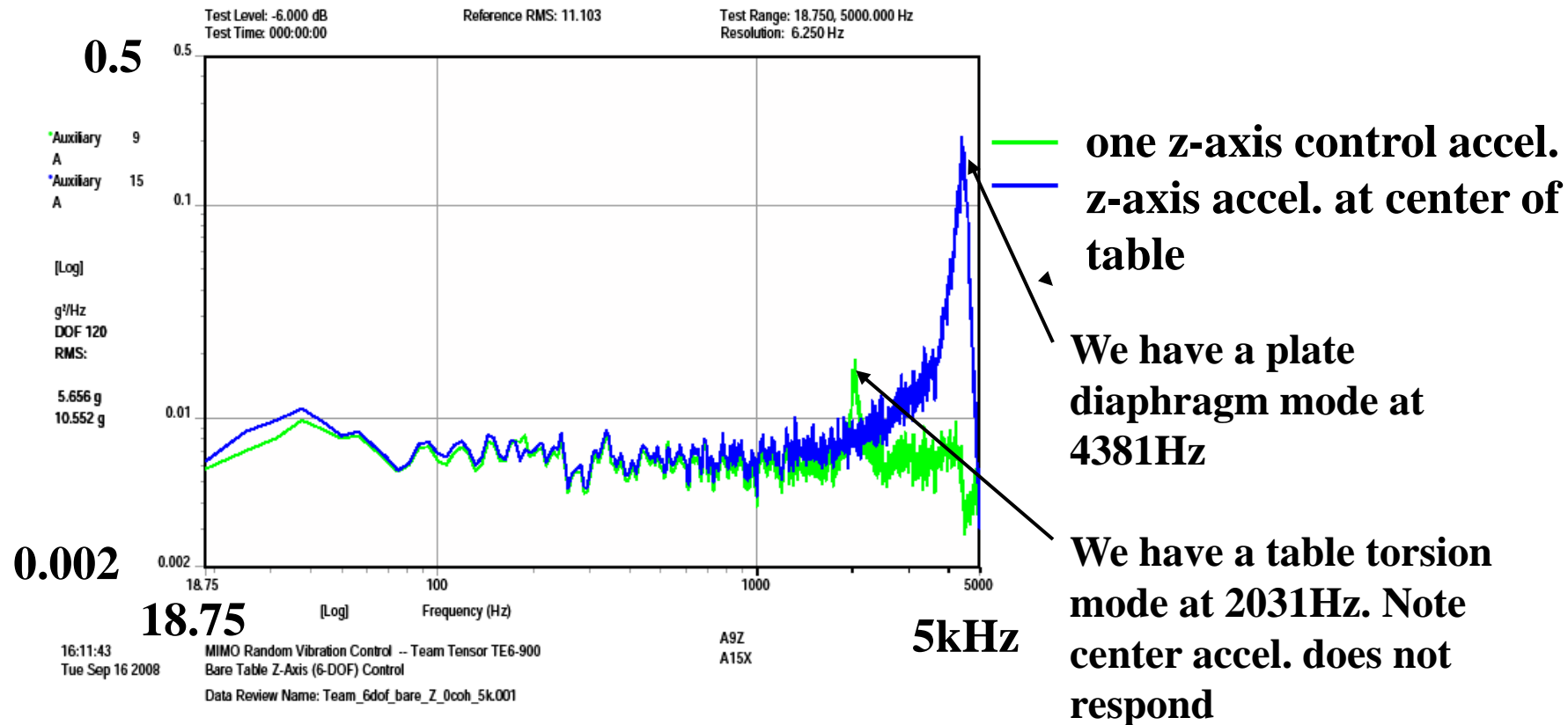


X-axis test with other degrees of freedom restrained

g^2/Hz

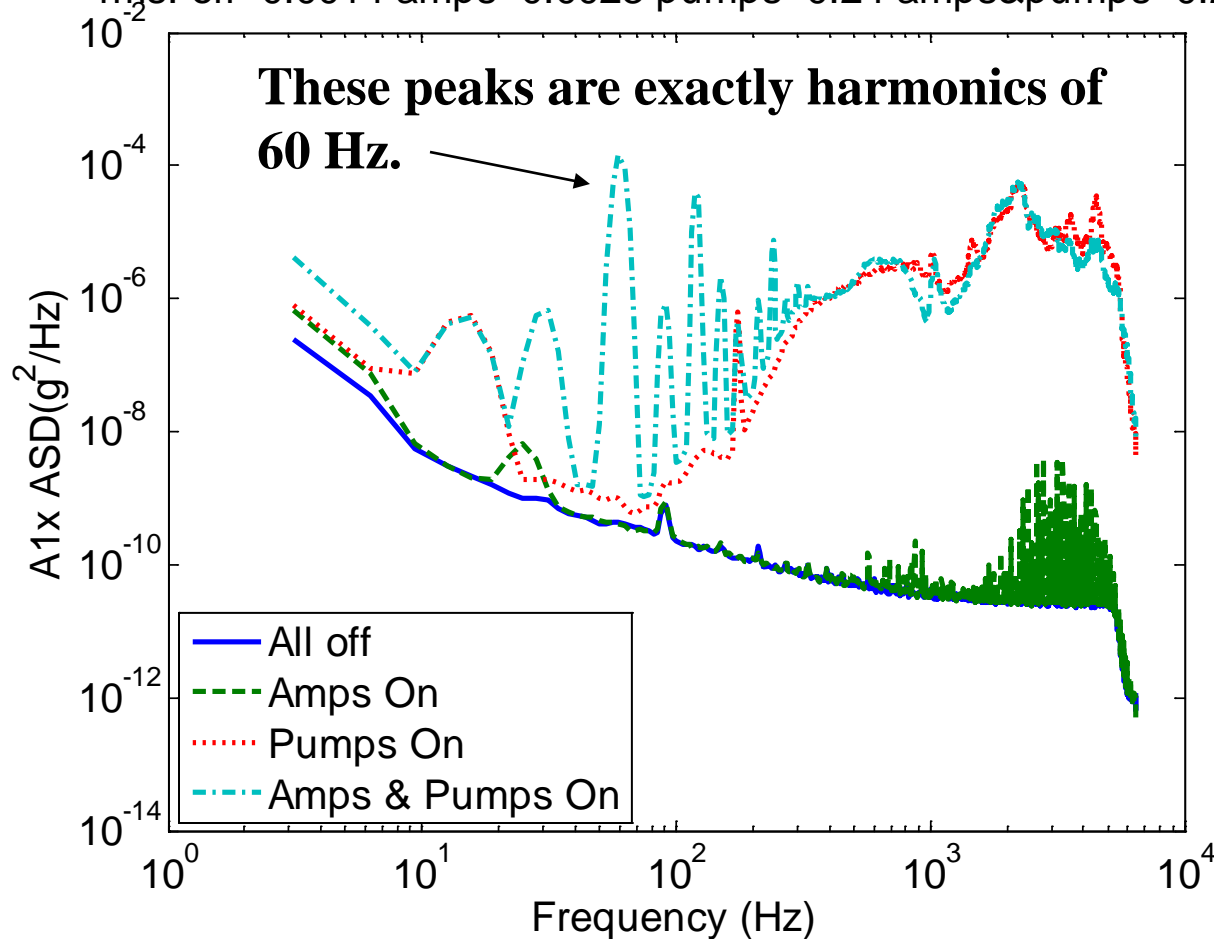


We have identified two table modes below 5kHz



Noise Floor Measurement

rms: off=0.0014 amps=0.0023 pumps=0.24 amps&pumps=0.22



Every thing looks pretty good until we turn the pumps on.

We are actively searching for the source.

It suggests a ground loop somewhere.

In spite of the noise control was pretty good.



Desired Shaker Design Improvements

- **Output current and voltage signals available**
 - Very difficult to access system capability without these measurements
 - Assist in optimizing the control strategy
- **Master gain control on each amplifier**
 - Balance the control system drive outputs
- **Separate hydraulic power supply from shaker cabinet**
 - Reduce system noise
- **Improved access to all electrical connectors to allow better trouble-shooting**
- **Interlock to prevent field current when pumps are off**
- **Improved technique for establishing cord tensions to achieve desired preload/position**
- **BIGGER SYSTEM (Same Cost---- Fat Chance!)**



Desired Control System Improvements

- Improved diagnostic tools to verify system integrity
 - State of health checks
 - Comparison of impedance functions from previous tests
 - Ability to view FRF's (Inverse of Impedance) directly---More intuitive
 - Other
 - Export FRF's and Impedance for offline computations
- Ability to specify any set of accelerometers as controls (not necessarily starting with channel one)
 - Re-patching channels increases chances for error
- Improved description of error messages



Lessons Learned

- **Correct Setup is Critical**
 - Inoperative accelerometer or shaker is deadly
 - Accelerometers
 - Sensitivities, polarity, location
- **Careful thought must be given to design of the experiment**
 - Selection and definition of control strategy can greatly affect the results



Summary

- **Team 6-Dof system is installed and operational**
- **System performance evaluated**
 - All six degrees of freedom have been achieved
 - 5 kHz closed loop random vibration control has been demonstrated for all three translations and three rotations
- **6-Dof system shows great promise for the future**



Publications Regarding Benefits of Realistic Multi-axis Environments

- **Multi-axis testing excites all modes simultaneously with a more realistic stress loading** (Berman, M.B. “Inadequacies in Uniaxial Stress Screen Vibration Testing.” *Journal of the IEST*. Vol. 44, No. 4, Fall 2001: 20-23)
- **Test objects may pass uni-axial testing but fail under operating conditions** (Freeman, M.T. “3-axis Vibration Test System Simulates Real World” *Test Engineering and Management*. Dec/Jan 1990-91: 10-14)
- **Rate of fatigue damage is increased by a factor of two with three axis excitation** (Himmelblau, H. and M.J. Hine. “Effects of Triaxial and Uniaxial Random Excitation on the Vibration Response and Fatigue Damage of Typical Spacecraft Hardware”. *Proceedings of the 66th Shock and Vibration Symposium*. Arlington, VA: SAVIAC 1995)
- **Durability of objects vary when exposed to sequential vs. simultaneous excitation** (French, M. “*Comparison of Simultaneous and Sequential Single Axis Durability*”: To be published in *Experimental Techniques*, November 2006)