



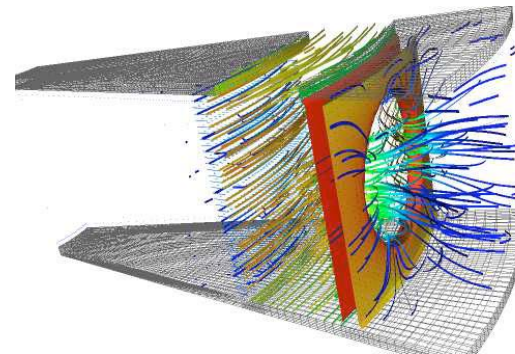
ALEGRA: An Arbitrary Lagrangian-Eulerian Multimaterial, Multiphysics Code

The ALEGRA Team

presented by Bill Rider

Sandia National Laboratories

**AIAA Aerospace Science Meeting,
Reno NV January 8, 2008**





A quote to start us off

“An expert is someone who knows some of the worst mistakes that can be made in his subject, and how to avoid them.”

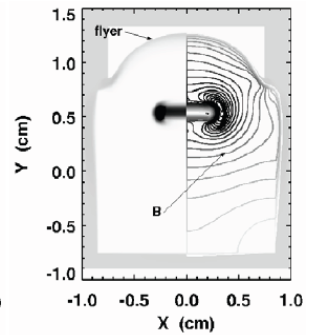
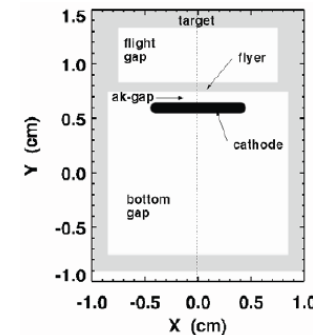
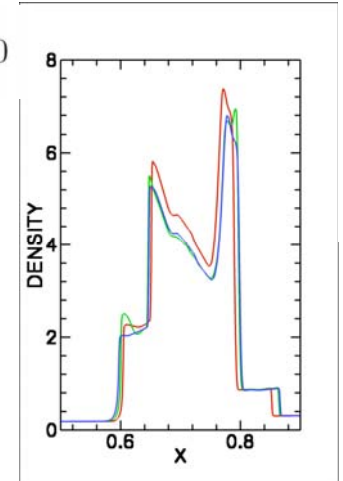
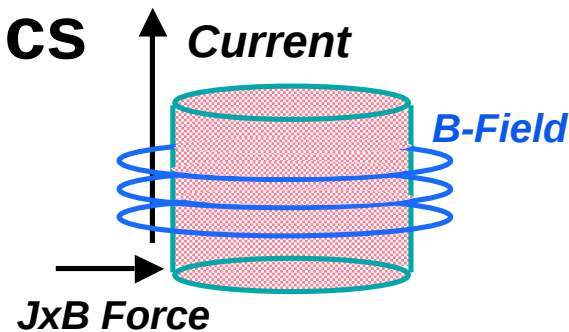
– Werner Heisenberg



Outline of the Talk

- A Brief history of ALEGRA
- Governing Equations
- Solution Procedure
- Multimaterial dynamics
 - Lagrangian step
 - Remap step
- MHD
- Applications
 - Code Verification
 - Z-pinch implosions
 - Advanced material modeling

$$\frac{\partial \mathbf{B}}{\partial t} + \nabla \times (\mathbf{B} \times \mathbf{u}) + \mathbf{u}(\nabla \cdot \mathbf{B}) = 0$$





A (very) brief history of ALEGA

- **The project began in 1988 to support the ICF program,**
- **Based on existing codes PRONTO & MMALE**
- **Major support and development under the DOE ASC program through the 1990's to today**
- **Developed in C++ for high-performance massively parallel computers**

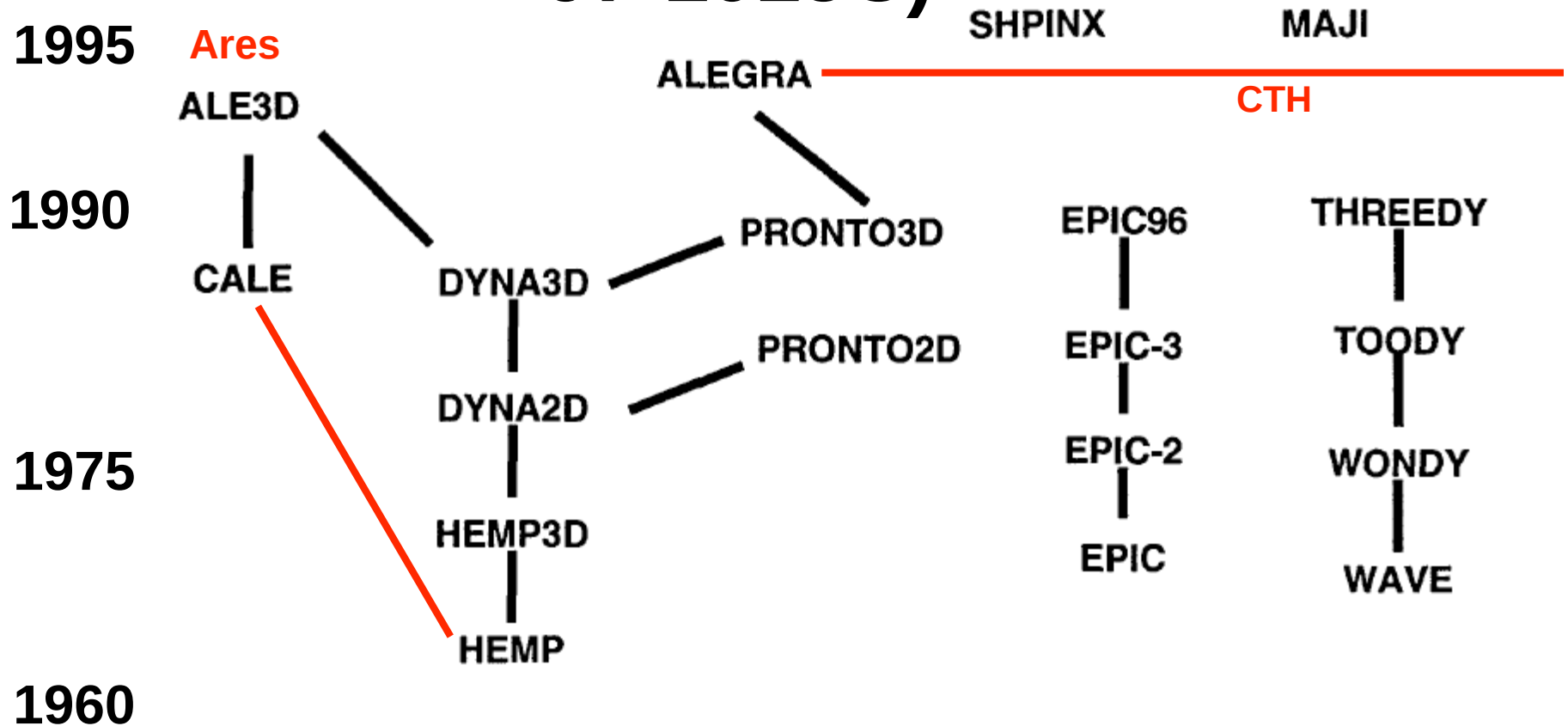


Historical Context

- **PRONTO is the basis (became PRESTO under ASC Sierra framework)**
 - The basic Lagrangian step is PRONTO plus the energy equation necessary for shocks (ala CTH!).
- **It's a finite element code (we're Sandia after all!).**
- **Other aspects of the method (i.e. the ALE remap) are based on (inspired by) CTH.**



Family tree of Lagrangian hydrocodes by Gene Hertel (SAND 97-1015C)





Governing Equations

- **Mass**

$$\frac{\partial f_k \rho_k}{\partial t} = -\nabla \cdot (f_k \rho_k (\mathbf{u} - \mathbf{u}_g))$$

- **Momentum**

$$\frac{\partial \rho \mathbf{u}}{\partial t} = -\nabla \cdot (\rho (\mathbf{u} - \mathbf{u}_g) \mathbf{u} - \mathbf{T} - \mathbf{T}^M + p_r \mathbf{I}) + \mathbf{b}$$

- **Energy**

$$\begin{aligned} \frac{\partial \rho (e + e_r + 1/2 \mathbf{u}^T \mathbf{u} + 1/2 \mathbf{B}^T \mathbf{B})}{\partial t} = \\ - \nabla \cdot [\rho (\mathbf{u} - \mathbf{u}_g) (e + e_r + 1/2 \mathbf{u}^T \mathbf{u} + 1/2 \mathbf{B}^T \mathbf{B})] \\ - \nabla \cdot [\mathbf{u} (\mathbf{T} + p_r) + (\mathbf{u} \mathbf{B}) \mathbf{B} - \mathbf{q}] + \mathbf{u}^T \mathbf{b} + S_e \end{aligned}$$

- **Magnetics - Faraday's law**

$$\frac{\partial \mathbf{B}}{\partial t} + \nabla \times (\mathbf{B} \times (\mathbf{u} - \mathbf{u}_g)) + (\mathbf{u} - \mathbf{u}_g) (\nabla \cdot \mathbf{B}) + \nabla \times \mathbf{E}' = 0$$

- **Involution constraint, Ampere's law**

$$\nabla \cdot \mathbf{B} = 0$$

$$\nabla \times \mathbf{H} = \mathbf{J}$$



Governing Equations: Radiation Included

- **Energy Equation**
$$\frac{\partial \left(\rho \epsilon + e_r + \frac{1}{2} \mathbf{u}^T \mathbf{u} + \frac{1}{2\mu_0} \mathbf{B}^T \mathbf{B} \right)}{\partial t} =$$

$$-\nabla \cdot \left(\rho (\mathbf{u} - \mathbf{u}_g) \left(\rho \epsilon + e_r + \frac{1}{2} \mathbf{u}^T \mathbf{u} + \frac{1}{2\mu_0} \mathbf{B}^T \mathbf{B} \right) \right)$$

$$+ \nabla \cdot (\mathbf{u} (\mathbf{T} + \mathbf{T}^M - p_r \mathbf{I}) - \mathbf{q}) + \mathbf{J} \cdot \mathbf{E}'$$

- **Ion-Electron Temperature**

$$\rho \frac{de_e}{dt} = \mathbf{T}_e : \nabla \mathbf{u} - \nabla \cdot \mathbf{q}_e + \mathbf{J} \cdot \mathbf{E}' + \rho C_{Ve} \frac{\theta_i - \theta_e}{\tau_{ei}} - \int_0^\infty (\kappa (4\pi B_\nu - c E_\nu)) d\nu,$$

$$\rho \frac{de_i}{dt} = \mathbf{T}_i : \nabla \mathbf{u} - \nabla \cdot \mathbf{q}_i + \rho C_{Ve} \frac{\theta_e - \theta_i}{\tau_{ei}}$$

- **Rad.**
$$\frac{1}{c} \frac{\partial I}{\partial t} + \boldsymbol{\Omega} \cdot \nabla w_e = -\sigma_t w_e + \frac{\sigma_s}{4\pi} \int_{4\pi} w_e \boldsymbol{\Omega}' + \sigma_a \frac{c B(T_m)}{4\pi} + S_I$$



Solution Procedure

- **ALEGRA uses operator splitting, the key is a Lagrangian-Remap sequence for the ALE**
 - 1. Lagrangian - MHD**
 - 2. Diffusion: Magnetic-Thermal**
 - 3. Remesh**
 - 4. Remap**
 - 5. Radiation**

– Repeat



Review of the two step method for (DOE) ALE codes.

1. Compute the solution to the equations in the **Lagrangian** frame (including **Q 's & hourglass** control)

$$\frac{d\vec{x}}{dt} = \vec{u}; \rho = \frac{m}{V_{ol}}; \frac{d\vec{u}}{dt} + \frac{1}{\rho} \nabla (p + Q) = 0; \frac{de}{dt} + \frac{1}{\rho} (p + Q) \nabla \vec{u} = 0$$

$$\text{or} \quad \frac{de}{dt} + (p + Q) \frac{dV}{dt} = 0$$

2. Figure out what mesh to remap to (**rezone**)
3. **Remap** the variable to the new zone

$$\frac{\partial \rho}{\partial t} = -(\vec{u} - \vec{u}_g) \nabla \rho; \frac{\partial \rho \vec{u}}{\partial t} = -(\vec{u} - \vec{u}_g) \nabla \rho \vec{u}; \frac{\partial \rho u e}{\partial t} = -(\vec{u} - \vec{u}_g) \nabla \rho e$$

4. Repeat



Lagrangian Equations

- Lagrangian frame in integral form

$$\frac{d}{dt} \int_{\Omega_t} \rho \, dv = 0 \quad \longrightarrow \quad \dot{\mathbf{x}} = \mathbf{u}$$

$$\frac{d}{dt} \int_{\Omega_t} \rho \dot{\mathbf{u}} \, dv = \int_{\Omega_t} \nabla \cdot (\mathbf{T} + \mathbf{T}^M) \, dv$$

$$\frac{d}{dt} \int_{\Omega_t} \rho e \, dv = \int_{\Omega_t} \mathbf{T} \cdot \nabla \mathbf{u} \, dv$$

$$\frac{d}{dt} \int_{\Gamma_t} \mathbf{B} \cdot \mathbf{n} \, dA = 0$$



Remesh-Remap

$$\frac{d\mathbf{x}}{dt} = \mathbf{u}_g - \mathbf{u}$$

Remesh

$$\frac{\partial f_k}{\partial t} = -(\mathbf{u} - \mathbf{u}_g) \cdot \nabla f_k$$

$$\frac{\partial \rho e}{\partial t} = -\nabla \cdot (\rho e (\mathbf{u} - \mathbf{u}_g))$$

$$\frac{\partial_r f_k \rho_k}{\partial t} = -\nabla \cdot (f_k \rho_k (\mathbf{u} - \mathbf{u}_g))$$

$$\frac{\partial \rho K}{\partial t} = -\nabla \cdot (\rho K (\mathbf{u} - \mathbf{u}_g))$$

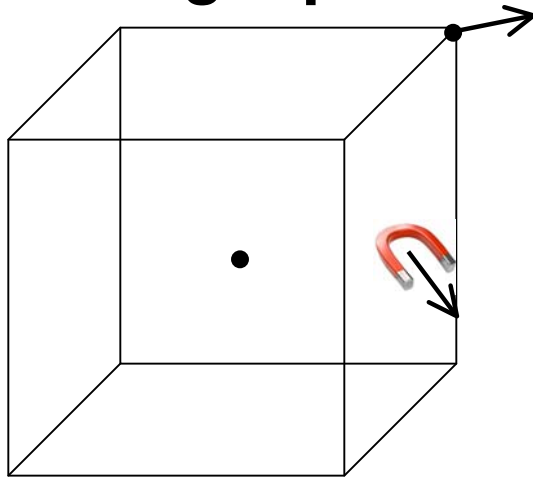
$$\frac{\partial \rho \mathbf{u}}{\partial t} = -\nabla \cdot (\rho \mathbf{u} (\mathbf{u} - \mathbf{u}_g))$$

$$\frac{\partial \mathbf{B}}{\partial t} = -\nabla \times (\mathbf{B} \times (\mathbf{u} - \mathbf{u}_g)) - (\mathbf{u} - \mathbf{u}_g) (\nabla \cdot \mathbf{B})$$



Centering of Variables

- **Vertex-Face staggered grid (unstructured hexs)**
 - Position, velocity, acceleration (nodal)
 - Density, energy, stress (element)
 - Magnetic field is face-centered
 - “Single point integration in space”





Multimaterial Lagrangian Hydro

- When the elements have more than one material, the treatment is more complex.
- Two choices:
 - The classical equal volume treatment (argued to be unphysical)
 - A more modern treatment which allows the materials to be treated as interacting adiabatically.



The modern multimaterial treatment

- Assumes the materials are interacting adiabatically. Could use a pressure relaxation as well.

- Changes the volume fraction and energy evolution

$$\frac{df_k}{dt} = f_k \left(\frac{\bar{B}}{B_k} - 1 \right) \frac{\partial u}{\partial x}$$
$$f_k \rho_k \frac{de_k}{dt} = -f_k \frac{\bar{B}}{B_k} \bar{p} \frac{\partial u}{\partial x}$$

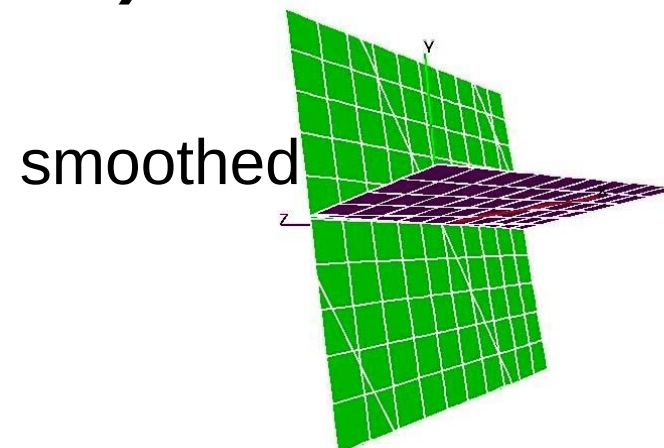
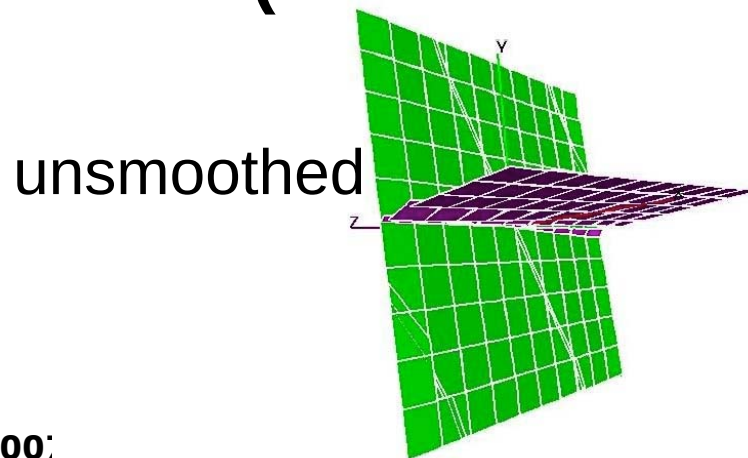
- Requires more complicated average properties

$$\bar{B} = \left(\sum_k \frac{f_k}{B_k} \right)^{-1} \quad \bar{p} = \bar{B} \left(\sum_k \frac{f_k p_k}{B_k} \right)$$



Multimaterial Remap

- The remap uses high resolution finite volume differencing for continuous fields
- Interface reconstruction with linearity preserving and automatic interface ordering (PIR) is used for discontinuous field (material interfaces).





Multimaterial Remap

- The remap process can create new mixed material elements which may be out of thermodynamic equilibrium.
- The elements should be brought into equilibrium before moving on from remap
 - This requires an adjustment of the volume

fractions
$$\Delta f_k = f_k \left(\frac{p_k - \bar{p}}{B_k} \right)$$

$$f_k^1 = f_k^0 + \Delta f_k; \rho_k^1 = \frac{f_k^0 \rho_k^0}{f_k^1}$$

$$f_k^1 \rho_k^1 e_k^1 = f_k^0 \rho_k^0 e_k^0 - \bar{p} \Delta f_k$$

- Any implementations requires limiters and renormalization

$$f_k := \frac{f_k}{\sum_k f_k} \quad \Delta f_k = \text{sign}(\Delta f_k) \min(\Delta f_k, 0.1)$$
$$f_k := \max[0, \min(f_k, 1)]$$



Kinetic energy remap & total energy conservation

- For some application (i.e. Z-pinch) this new feature is essential for good results.
- This adds a correction to the internal energy remap allowing energy

conservation, $K_{i,j,k} = \frac{1}{N_{\text{nodes}}} \sum_{\text{nodes of } i,j,k} 1/2 (u^2 + v^2 + w^2)$

$$\Delta e_{i,j,k}^{\text{remapped}} = \left(K_{i,j,k}^{\text{remapped}} - \frac{1}{N_{\text{nodes}}} \sum_{\text{nodes of } i,j,k} 1/2 (u^2 + v^2 + w^2)^{\text{remapped}} \right)$$

$q_j/p_j < 0.0001$ set $\Delta e_{i,j,k}^{\text{remapped}} = 0$

$\Delta e_{i,j,k}^{\text{remapped}} < -\beta e_{i,j,k}^{\text{remapped}}, \Delta e_{i,j,k}^{\text{remapped}} = -\beta e_{i,j,k}^{\text{remapped}}$

- **“fixes” are necessary for robust use!**



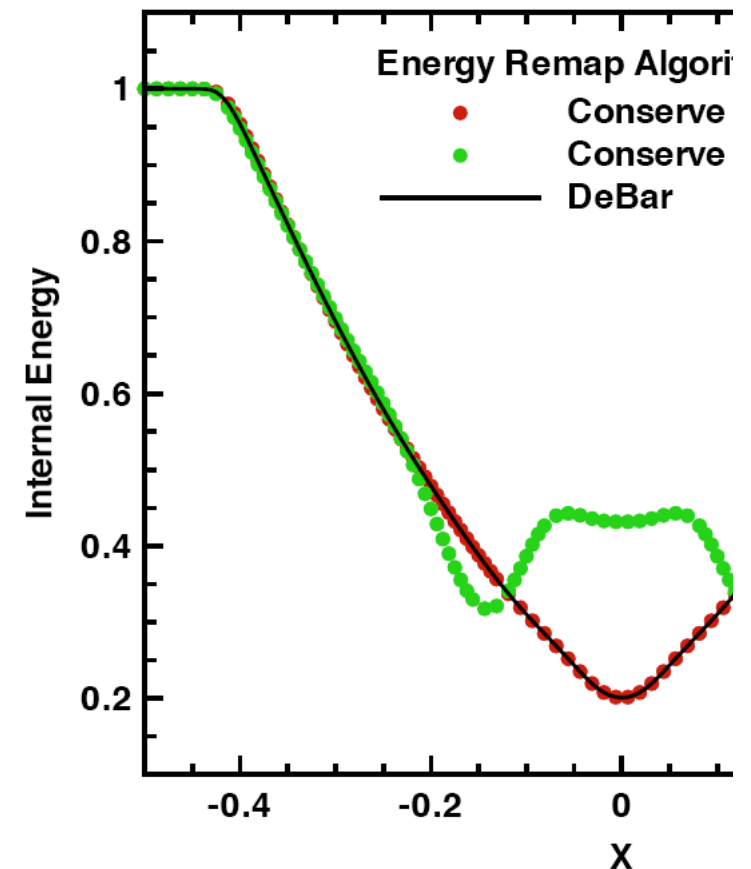
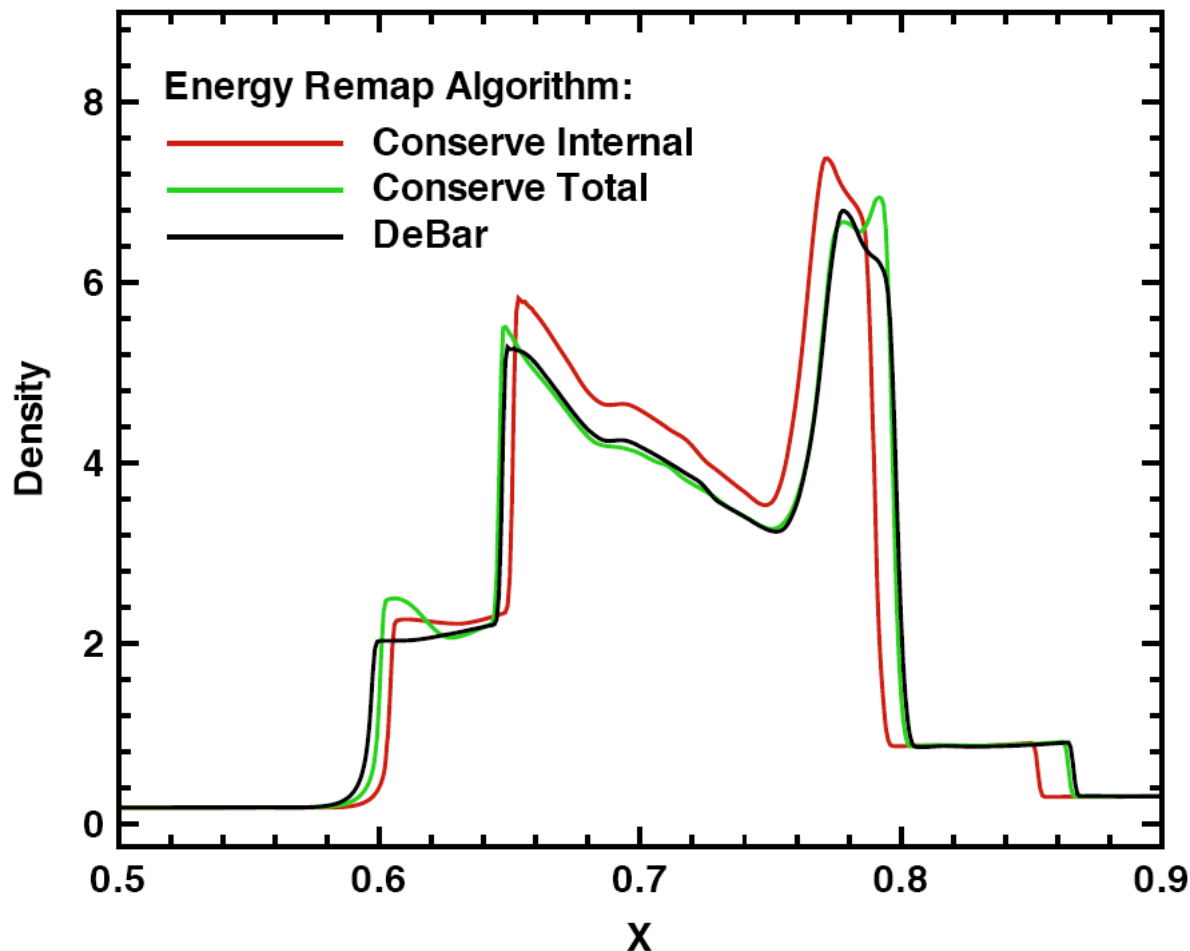
MHD

- **Uses a compatible formulation that preserves the divergence free magnetic field automatically.**
- **A software package, Intrepid, makes the implementation relatively seamless**
- **These properties are important to maintain through the remap as well.**
- **ALEGRA includes magnetic diffusion as well as ideal MHD**



Applications: Verification

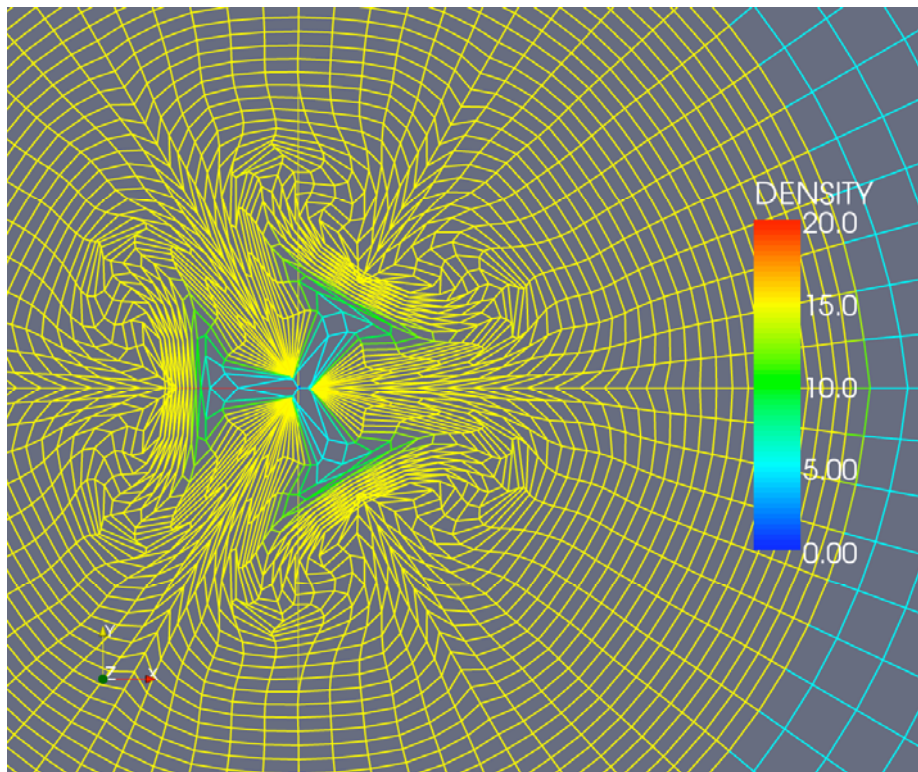
- Classic compressible flow problems
(we're also studying ideal MHD flows!)



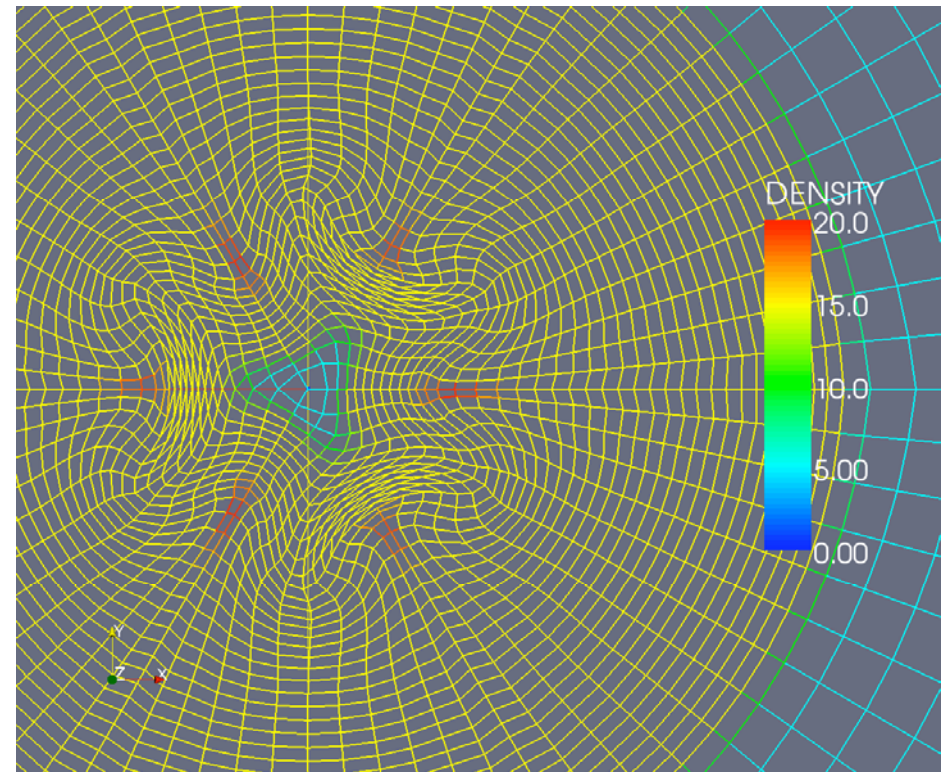


Cylindrical Noh Results

Scalar Q

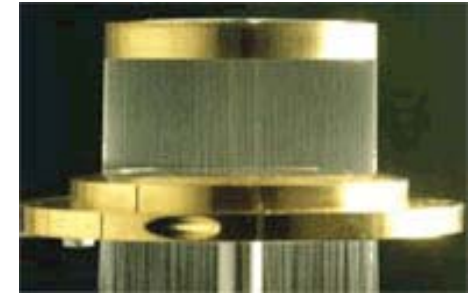


Tensor Q

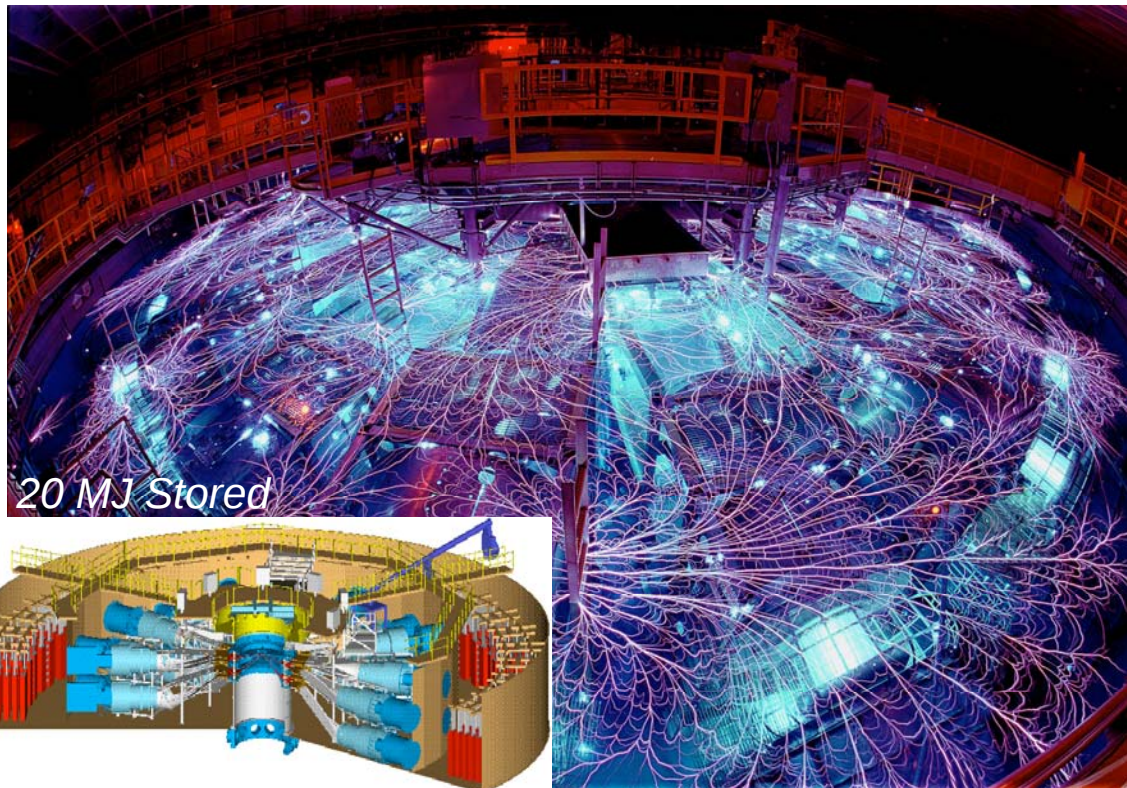




Applications: Z-Pinch

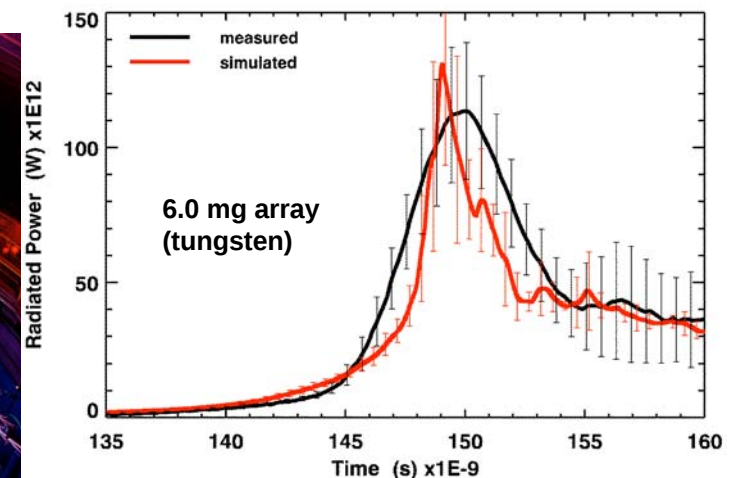


- ALEGRA has provided predictive simulations of magnetic flyers and wire array implosions conducted on SNL's Z-machine.

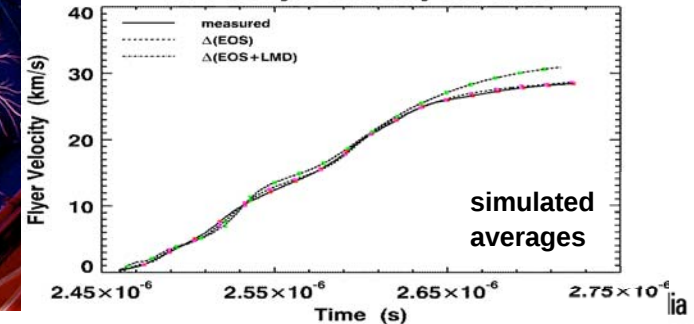


SAND-2007-????C

Radiated Power vs. Time



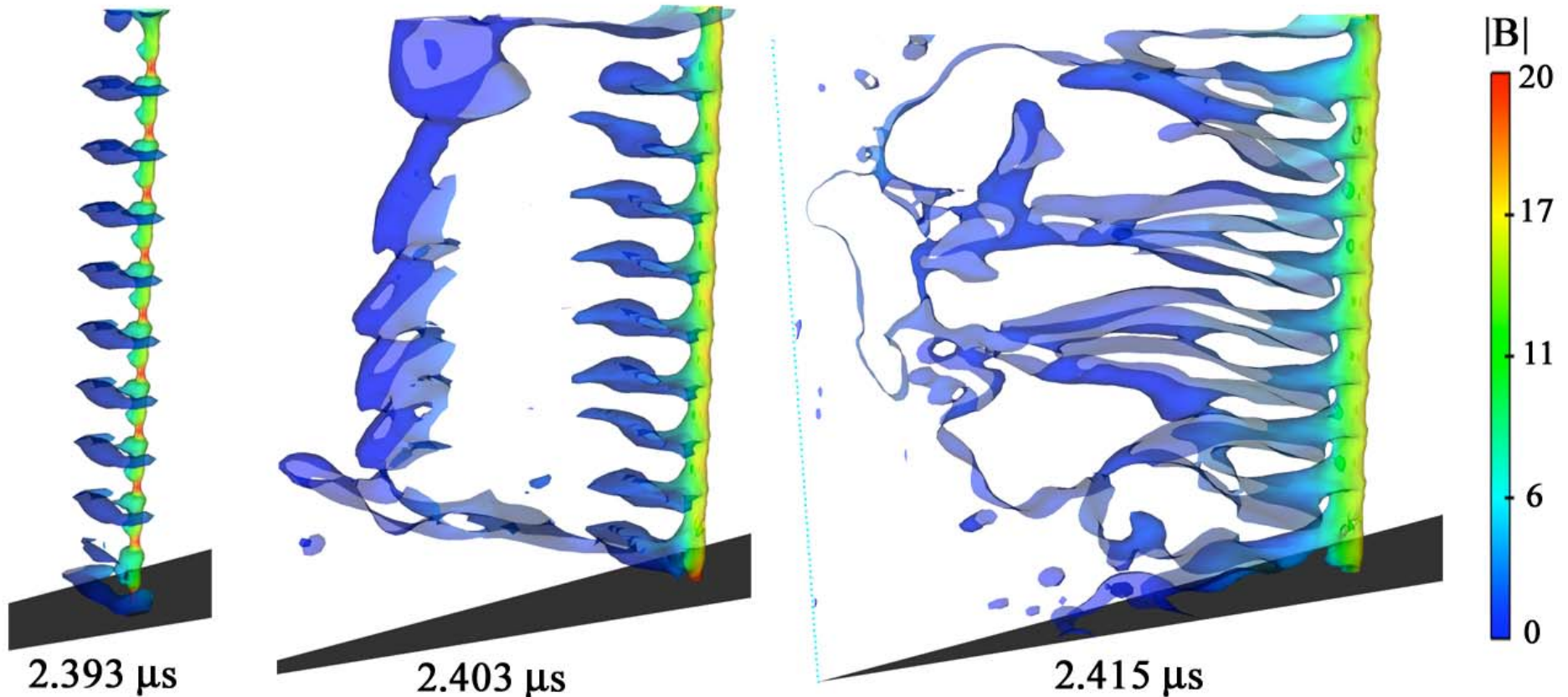
z1424 Flyer Velocity vs. Time





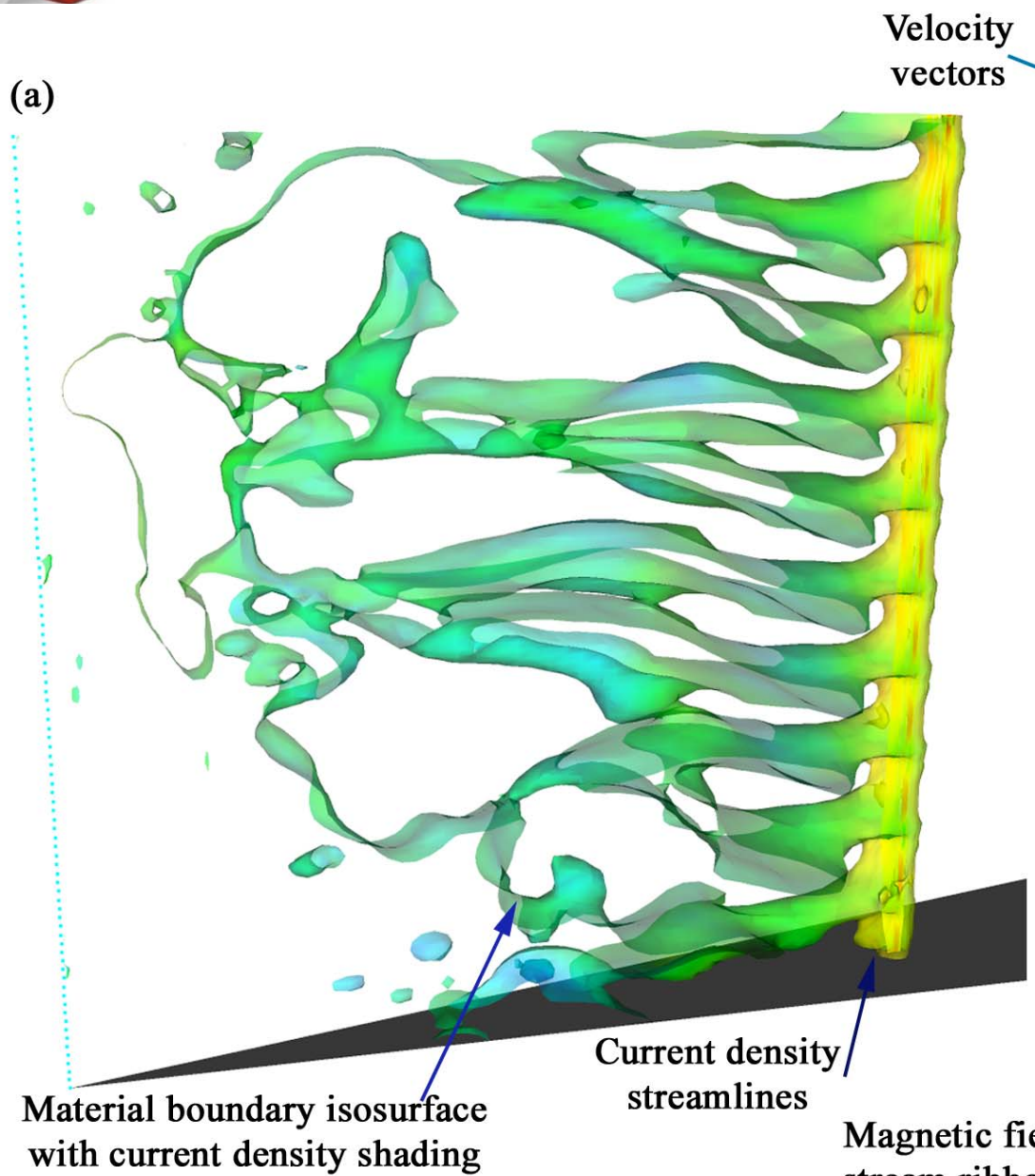
Sinusoidal Core Perturbation

Volume fraction isosurface with magnetic field strength

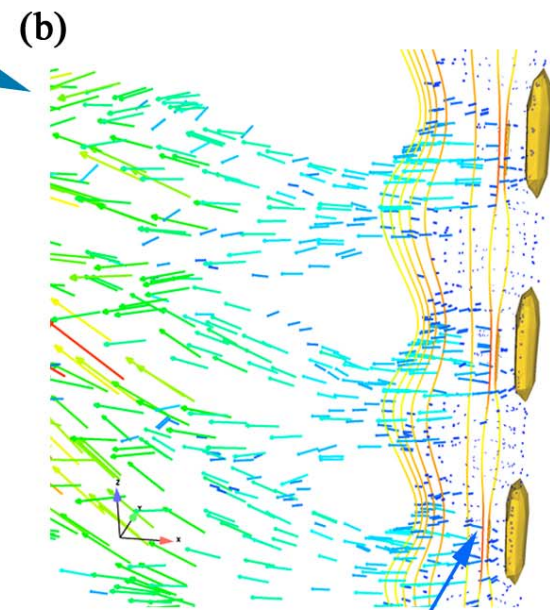


- Is this a variation of the $m=0$ instability for wire arrays?
- Are the local dynamics governed by the the strength of the local field versus the global?

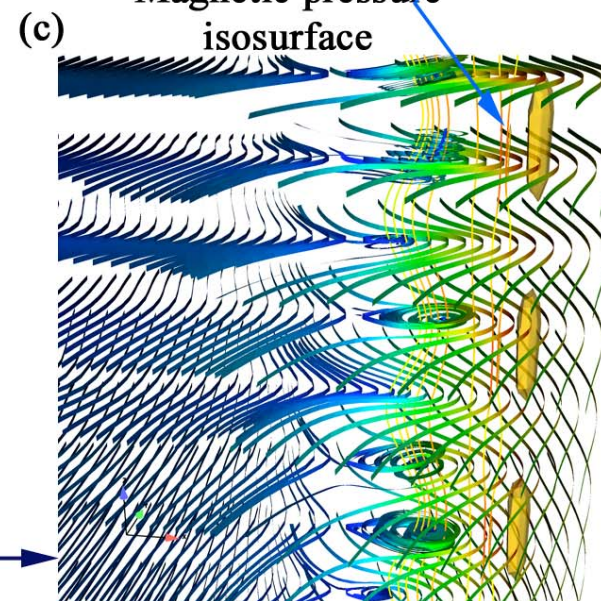
SAND-2007-????C



Velocity vectors



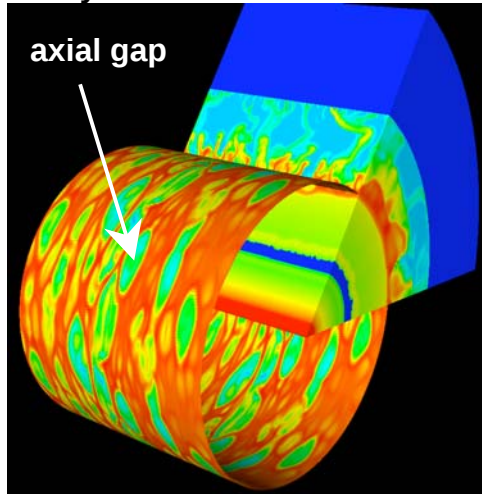
Magnetic pressure isosurface



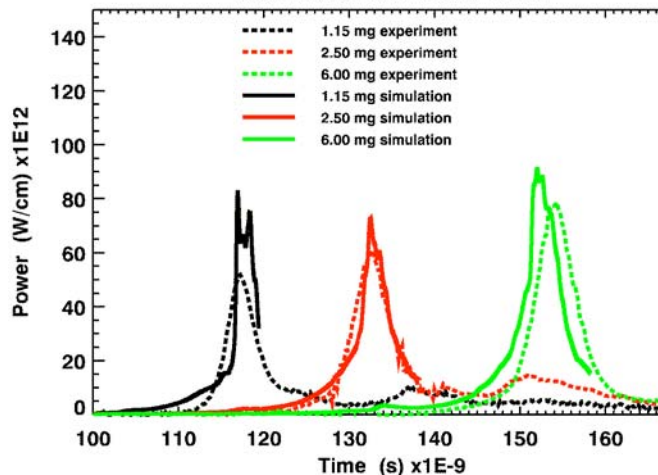


Wire Array Implosions require 3-D and all the physics!

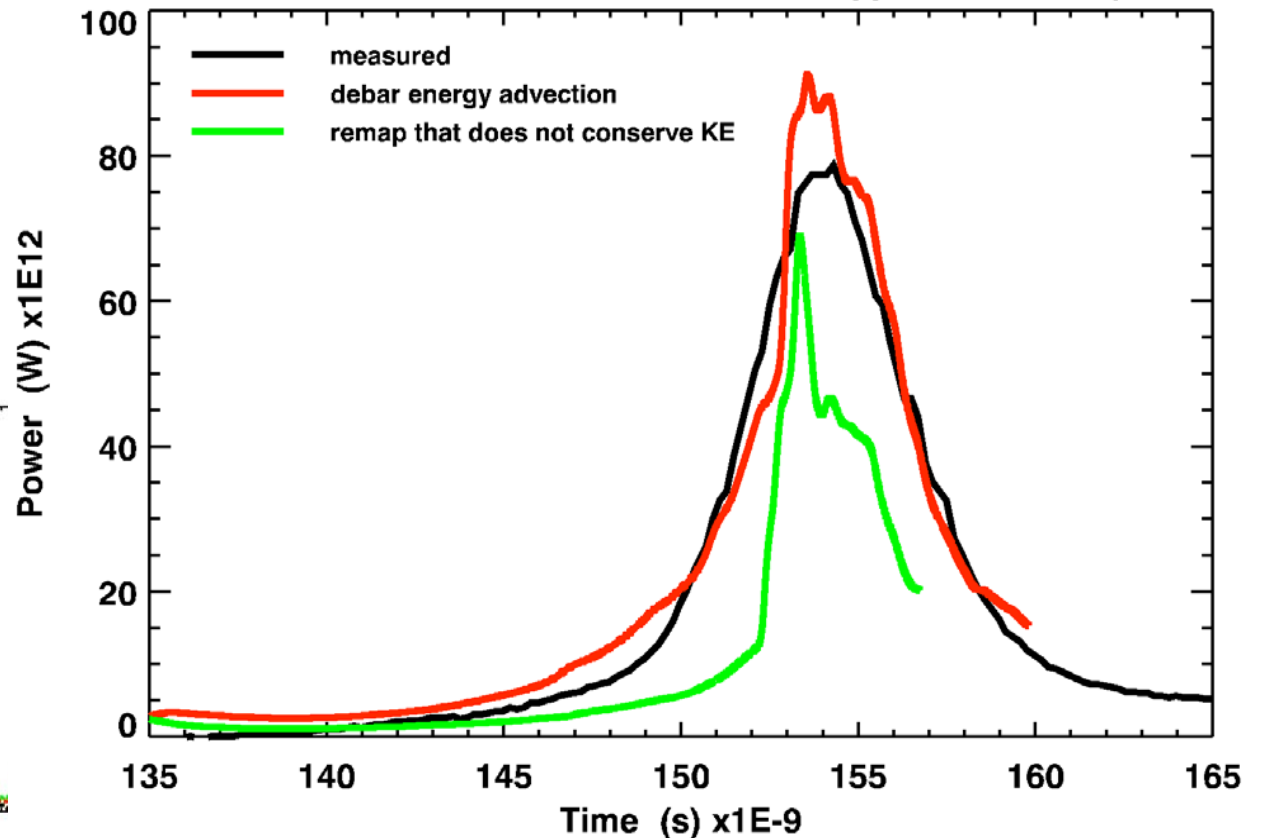
Density with 1.7% Correlation in θ



Radiated Power vs. Time



radiated power with and without energy conserving remap



Simulates a wide range of parameters

SAND-2007-????C



Applications: Advanced Material Modeling

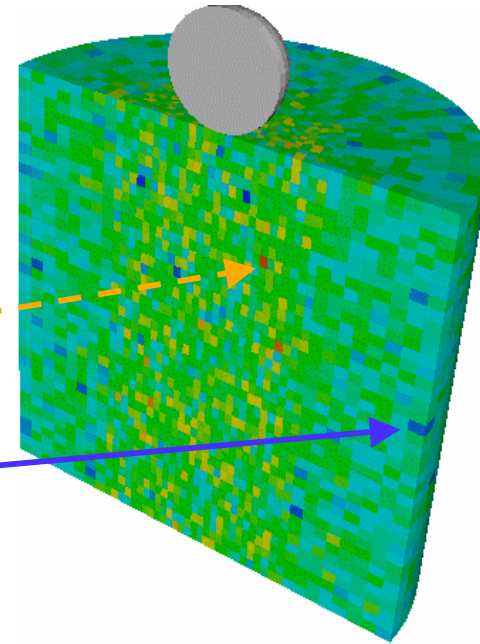
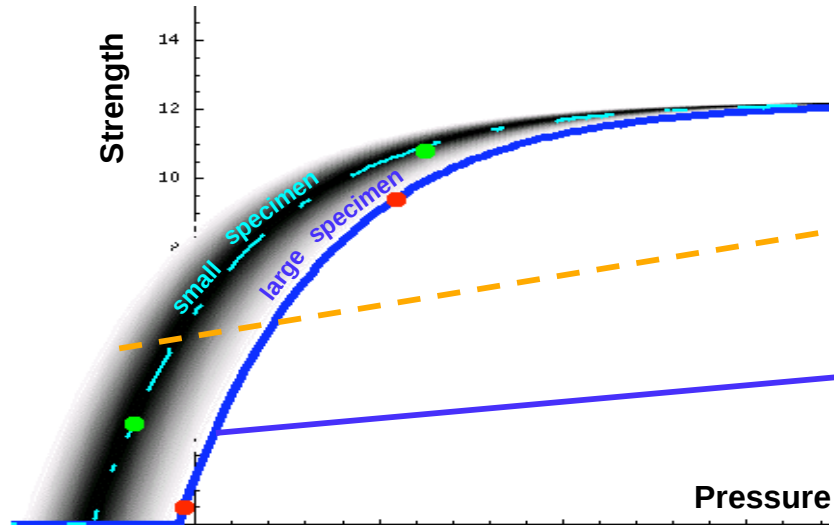


- Material modeling is important in many applications such as armor or anti-armor simulations.
- Among the most difficult aspect is fracture modeling which tends to be strongly size dependent –
 - Does not easily allow mesh independence
- ALEGRA has addressed this!

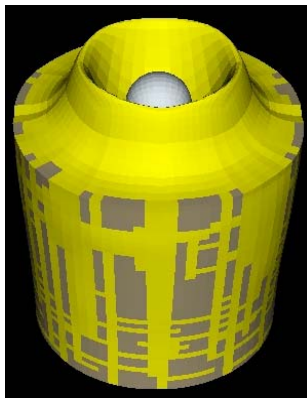


Material Heterogeneity is Crucial when Simulating Failure in Armor Systems

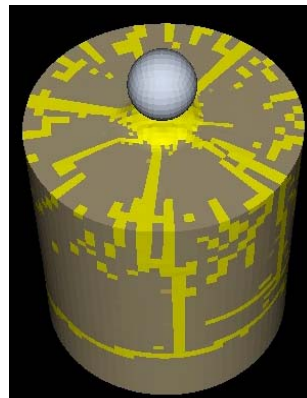
Spatially Variable (Fuzzy) Strength Profile for Ceramics



Initial state: small elements are stronger on average, but also more variable



Without Variability



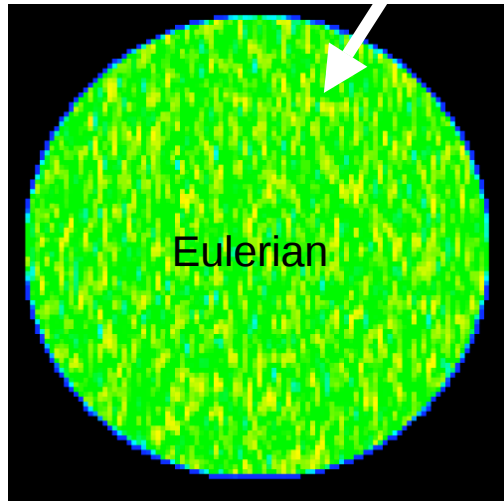
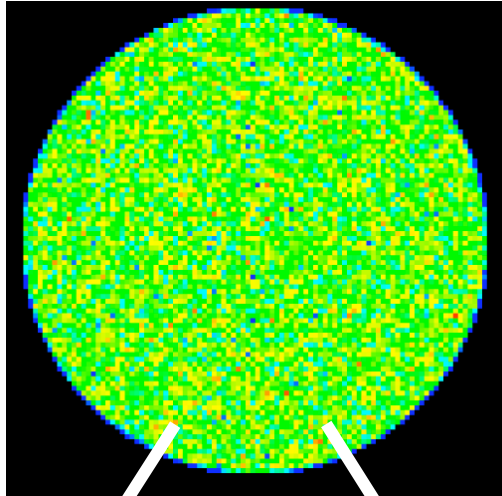
With Variability

**Key Collaboration: Brannon,
University of Utah**

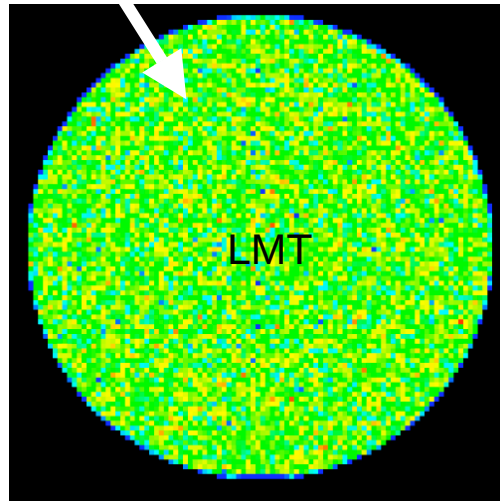


LMT Eliminates Smearing of Heterogeneity in Conventional Eulerian Algorithms

Initial State



Eulerian



LMT

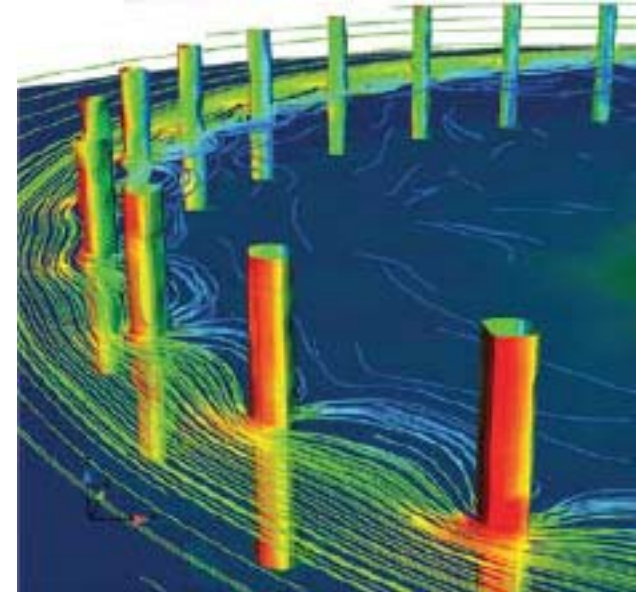
After Remap

Lagrangian Material Tracking (LMT):

- Standard Eulerian momentum solver
- Material internal state variables reside on Lagrangian tracers



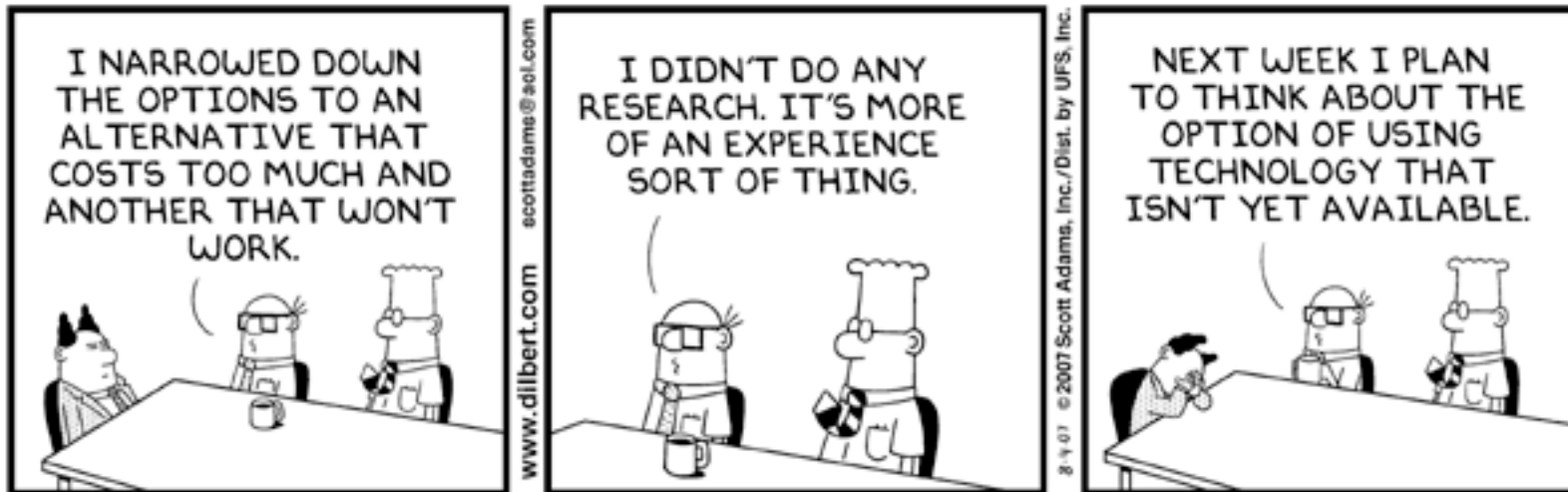
Conclusions



- **ALEGRA is a complex multiphysics code developed at SNL principally under the ASC program**
- **It has multimaterial capability**
- **MHD is an important aspect of many applications for ALEGRA**
- **Applications demonstrated are Z-pinch dynamics and complex material modeling.**



Scott Adams has an observation



© Scott Adams, Inc./Dist. by UFS, Inc.

“For the numerical analyst there are two kinds of truth; the truth you can prove, and the truth you see when you compute.” – Ami Harten