



IFE First-Wall Materials Response to Repeated High-Energy Pulsed Ions*

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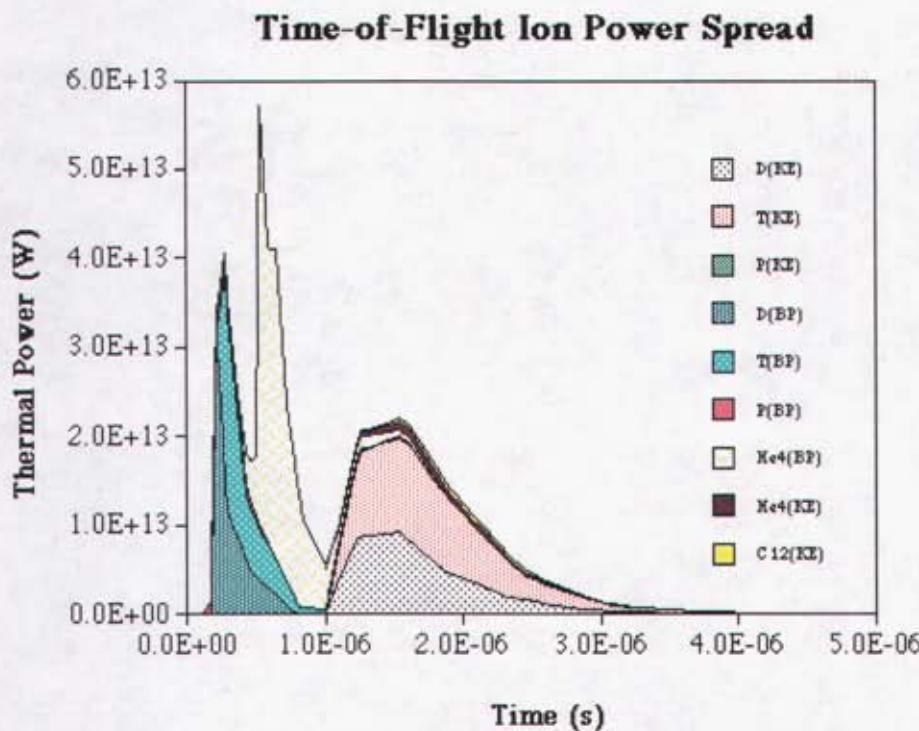


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Laser IFE Direct Drive Threat Spectra

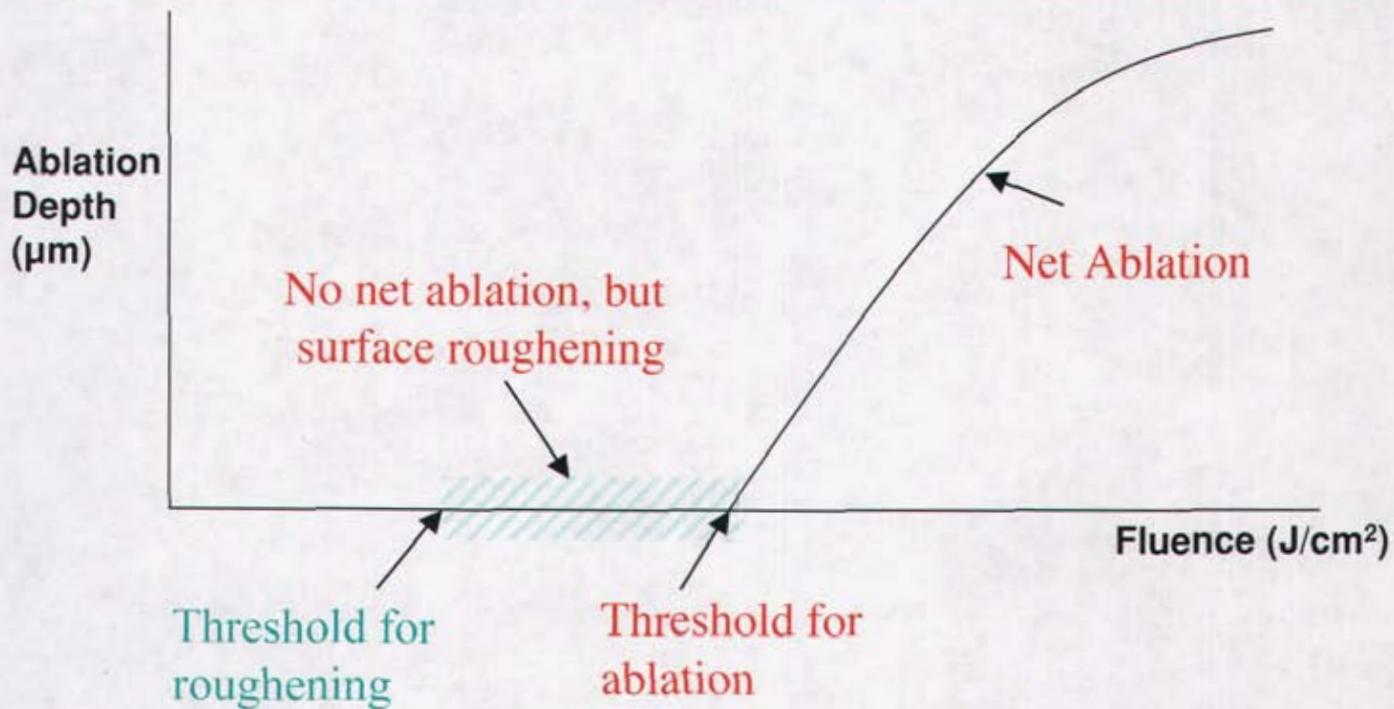


Simulation: Thermal Power to Wall in Ions
from 154 MJ Yield. Wall Radius: 6.5 m

- For Direct-drive Laser IFE:
 - ~70% neutrons
 - 1-2% x-rays
 - 30% ions (50-50 fusion and 'debris')
- Ions: several MeV, ~ few μ sec each, 8-20 J/cm^2 fluence, judged Significant Threat
- X-rays: ~ 1 J/cm^2 , up to 10 keV energies, judged less significant threat
- RHEPP-1: 700 keV N, higher for N^{+2} , 100-150 ns pulselength
- RHEPP-1 energy delivery too short, but otherwise good fidelity with reactor ion threat



Regimes of IFE Materials Response to Ions



Goals (for each material): examine net ablation to validate codes
find threshold for ablation

DONE

Area of Interest

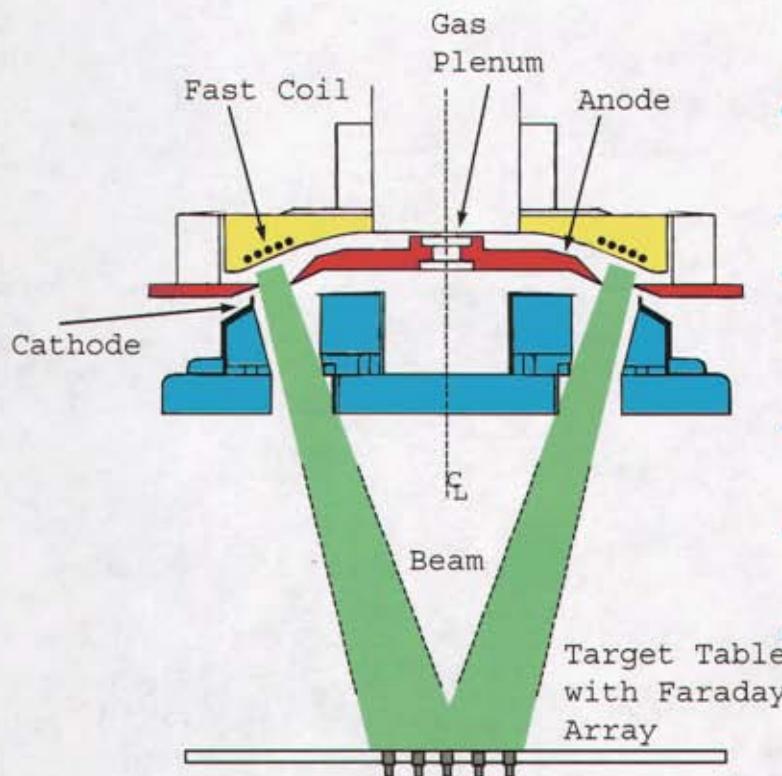
Understand roughening. Is there mass loss?
Find threshold for roughening
(Fluence/pulse, No. of pulses)



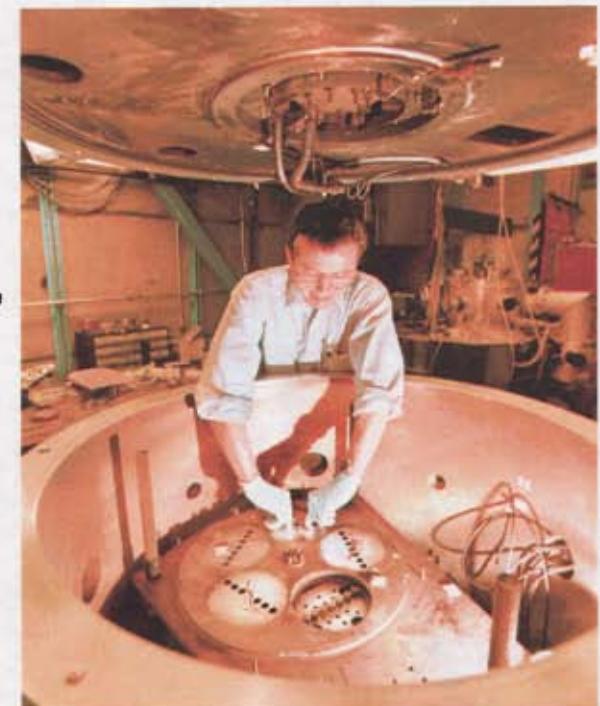
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Overall View of RHEPP-1 vacuum chamber and treatment area

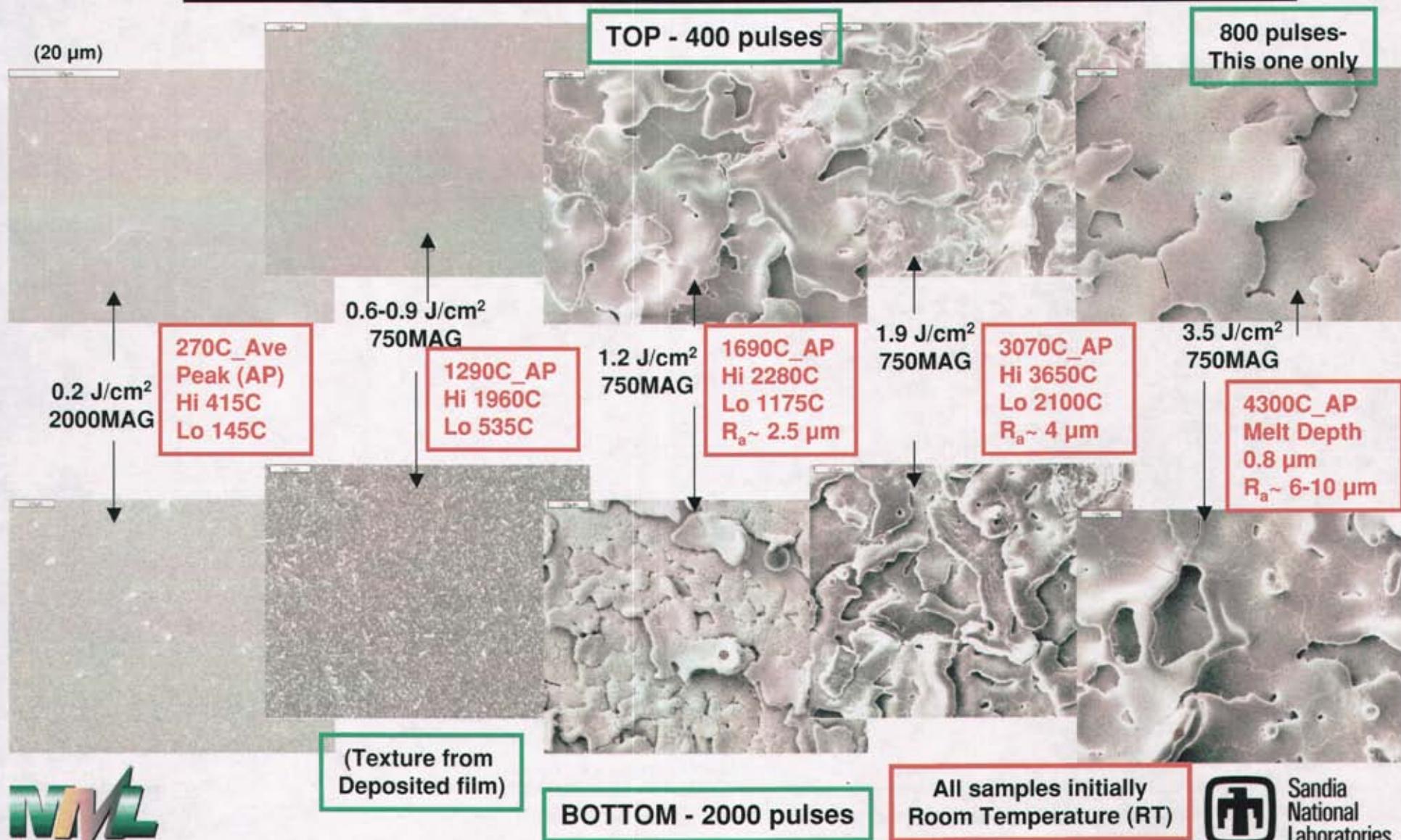


- 600-800 kV. Pulse Width ~ 100-200 ns
- $< 250 \text{ A/cm}^2$
- Beams from H, He, N₂, O₂, Ne, Ar, Xe, Kr, CH₄
- N beam reported on here
- Overall treatment area ~ 100 cm²
- Diode vacuum
- 10^{-5} Torr



Tray shown here replaced
by 'scalloped' holder that avoids
Beam center

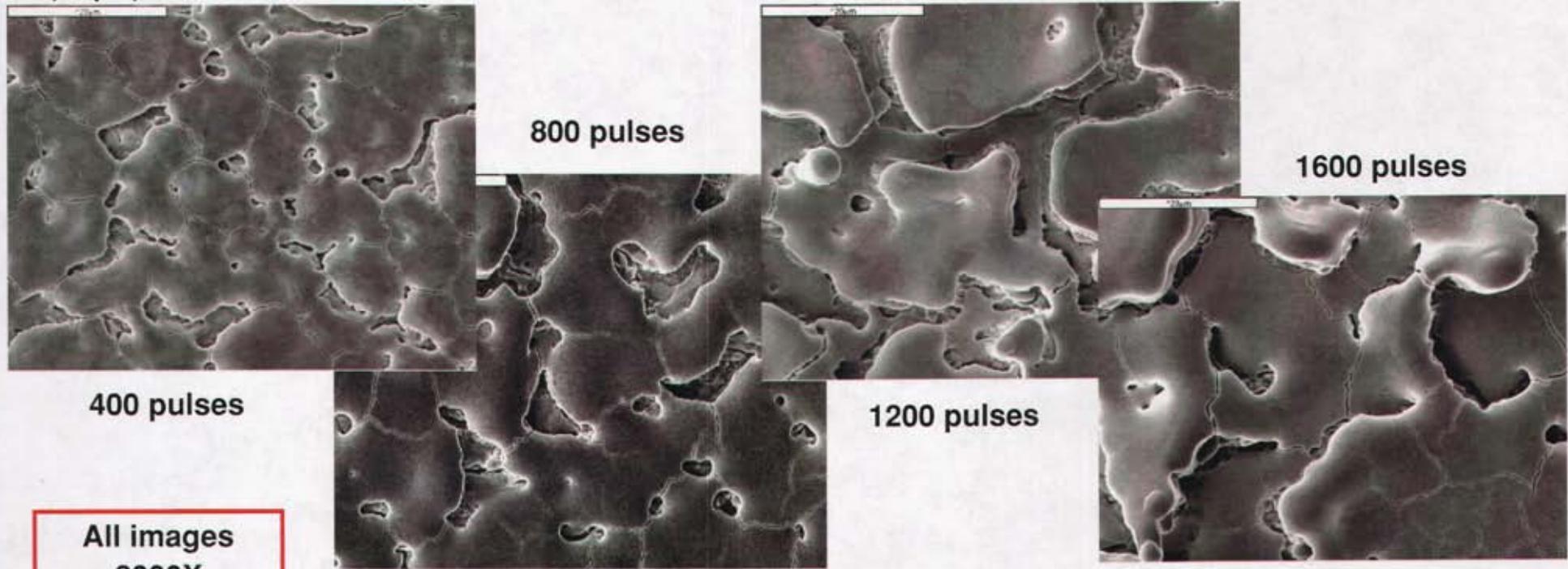
SEMs of Polycrystalline (PM) Tungsten Roughening: Threshold at $\sim 1 \text{ J/cm}^2$, roughening saturates after ~ 400 pulses





SEMs of lightly deformed PM Tungsten (non-melt): appears stress cracking starts, then exfoliation, forming 'valleys'

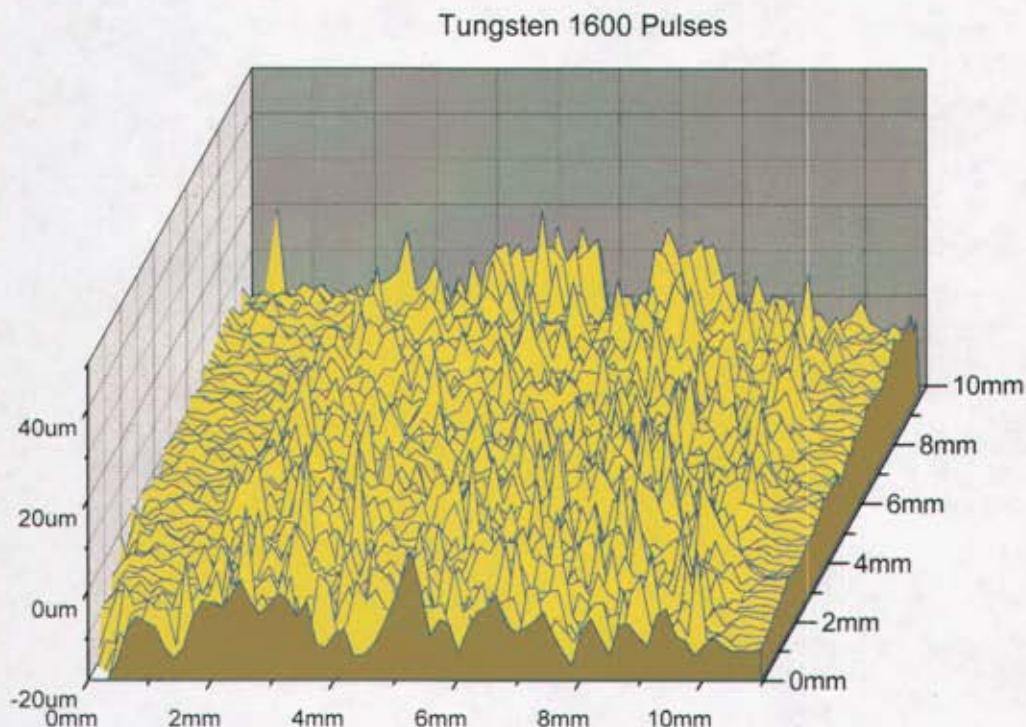
(20 μm)



- Heated PM Tungsten (600C) exposed to Nitrogen beam at $\sim 1.5 \text{ J/cm}^2$ - peak temp $\sim 3300\text{K}$
- Rounded 'knobs' are actually high points. **Surface rises during treatment.**



PM Tungsten after 1600 pulses (non-melting): Mostly mountains up to $\sim 30 \mu\text{m}$ height

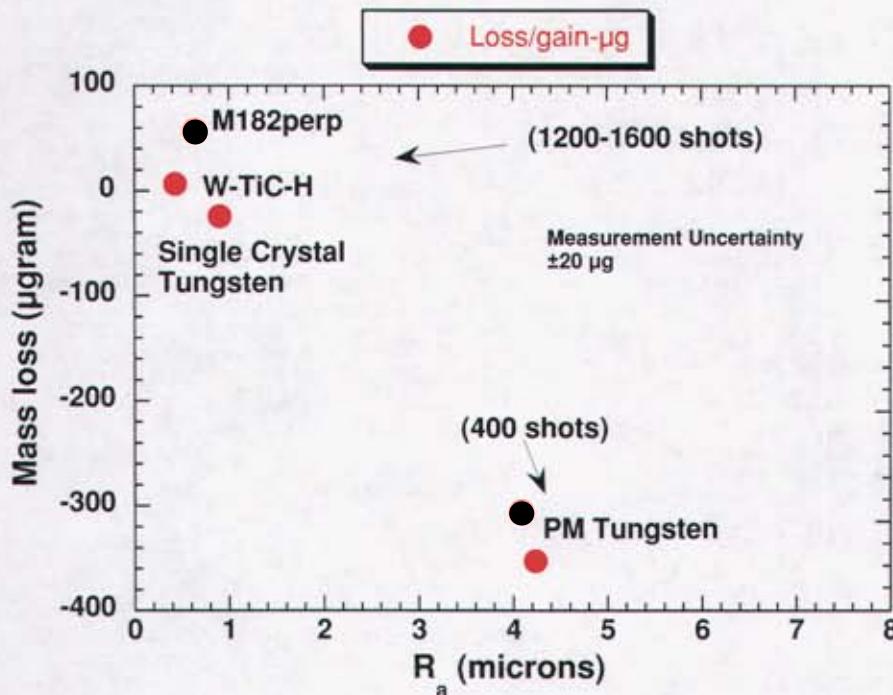


Cannot confirm mass loss by height study. Must weigh before/after exposure

- Heated/treated PM Tungsten examined with NEXIV laser interferometry
- Comprehensive line-out scan: max height $30 \mu\text{m}$, min height $< 10 \mu\text{m}$ compared to untreated
- Very deep microcracking not visible here
- Hypothesis: mountains are due to CTE expansion that does not recover



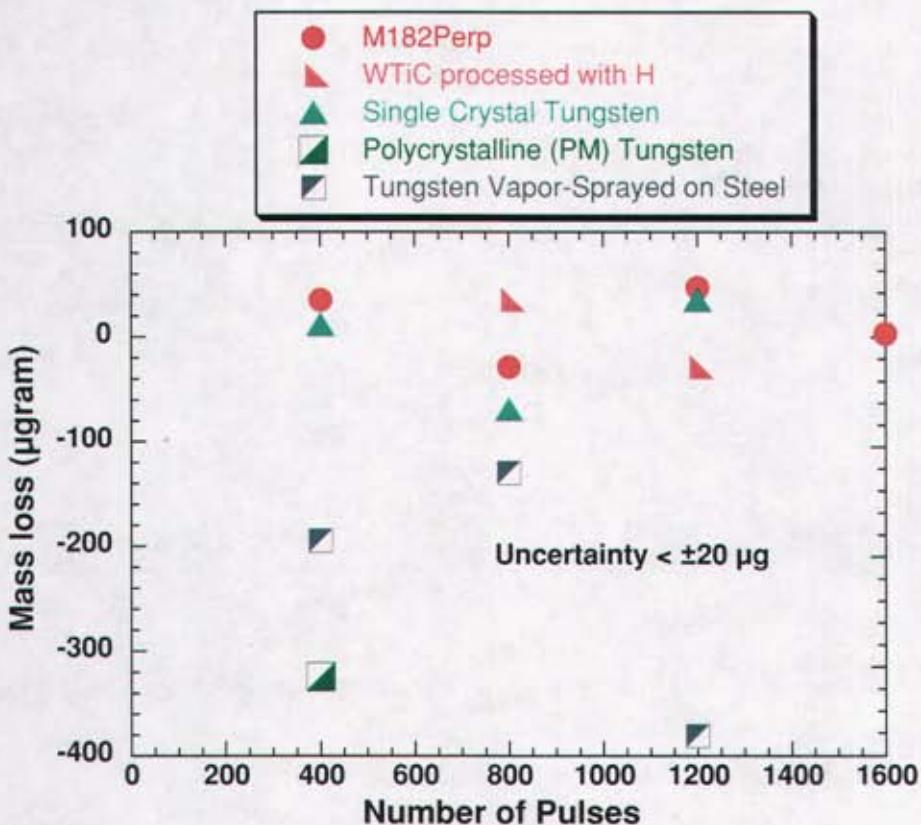
SNL Metrology weight measurements support connection between roughening and Mass Loss



- Samples of each listed material exposed for multiple 400-shot series, and weighed pre-and post-shot
- Exposure level/pulse: 1.2 - 1.7 J/cm²
Measurement Uncertainty < $\pm 20 \mu\text{g}$
- Two samples of polycrystalline (PM) Tungsten lost $\sim 350 \mu\text{g}$ in 400 pulses, with Surface Roughness Ra $\sim 4 \mu\text{m}$
- M182Perp, W-TiC-H, and Single Crystal Tungsten remained $< 1 \mu\text{m}$ Ra, and suffered little mass loss.



Mass Loss with Shot Number: M182Perp, WTiC-H, Single Crystal W show almost no loss



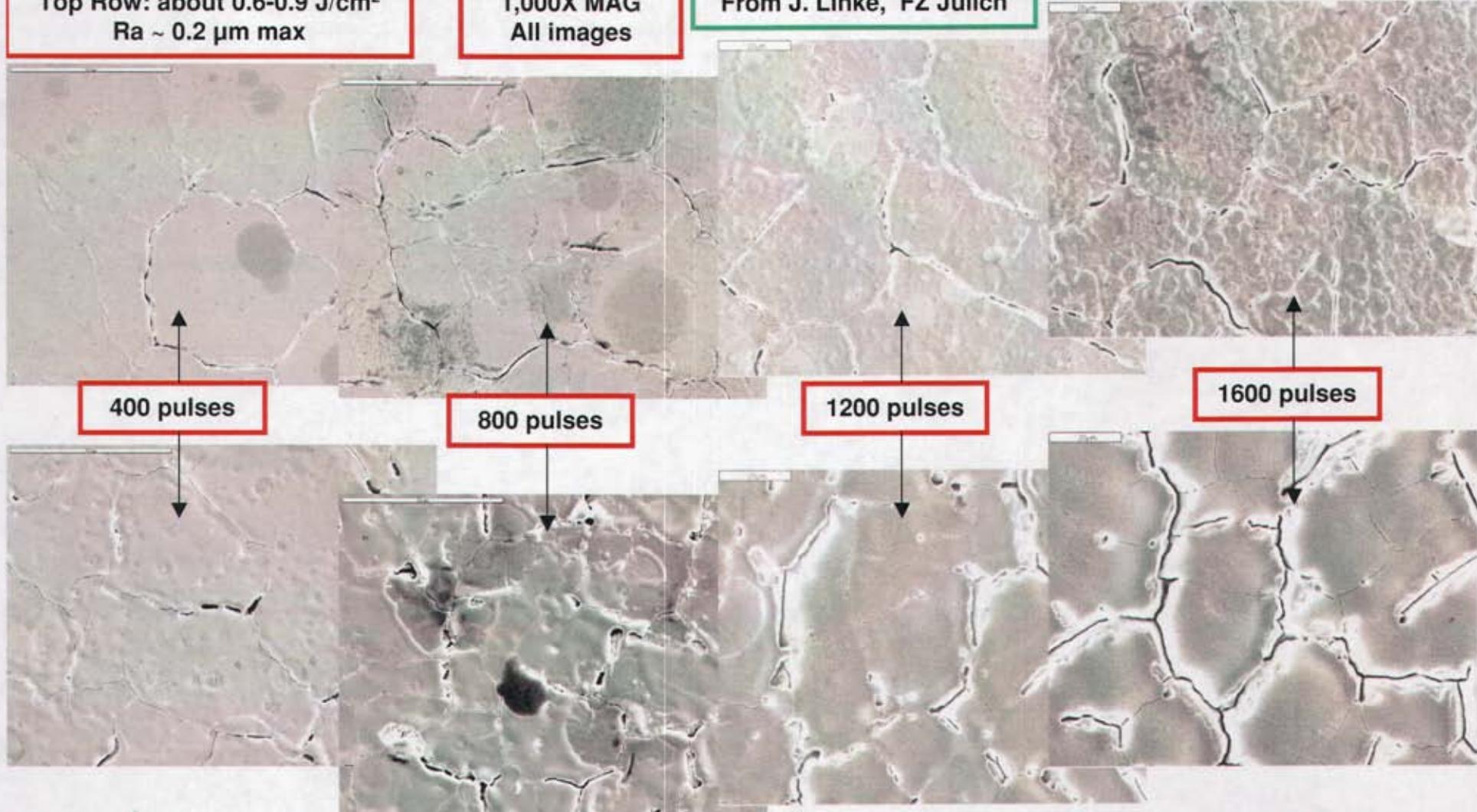
- Mass loss for PM Tungsten only for 400 pulses - exposure terminated
- Vapor-Sprayed Tungsten (on Ferritic Steel) loses up to 400 μg per 400 pulses
- Mass Gain due to entrained material (Cu) from diode region

SEMS of Tungsten M182 perp after 1600 pulses: Little topology change below 1 J/cm², some roughening w/ pulse number at ~ 1-1.2 J/cm²

Top Row: about 0.6-0.9 J/cm²
Ra ~ 0.2 μ m max

1,000X MAG
All images

From J. Linke, FZ Julich



Bottom Row: ~ 1 - 1.5 J/cm²
Ra ~ 0.35-0.45 μ m

Little or no mass loss to 1600 pulses



M182 Plansee Tungsten, cut with grains parallel to surface
(SEMs): surface-lying grains become unzipped with increasing fluence

No Treat

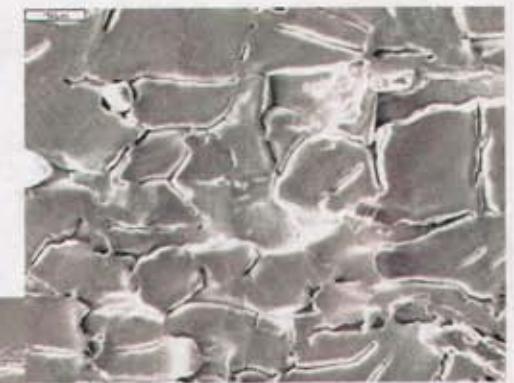


1,000X MAG



~ 0.7
J/cm²

All treated images 300X MAG.



About 1.3
J/cm²

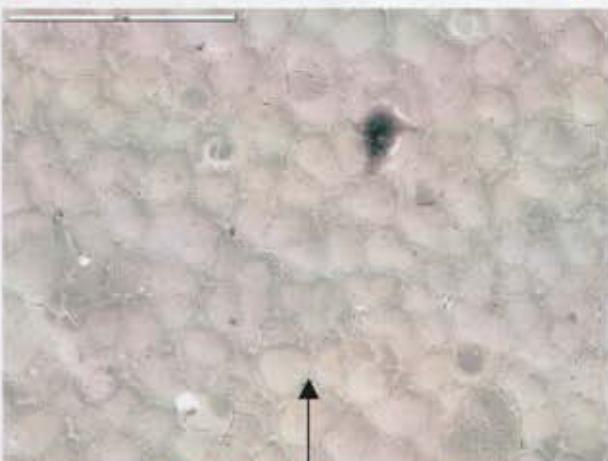


R_a : reaches 4 - 4.5 μm at 1.3 J/cm² (same as PM Tungsten)
Only apparent AFTER 400 pulses (these images)



W-TiC-A 'pre-stressed*' 2.5 cm-wide sample (SEMs): (presumed) stress-relief seems to restrict grain corner exfoliation

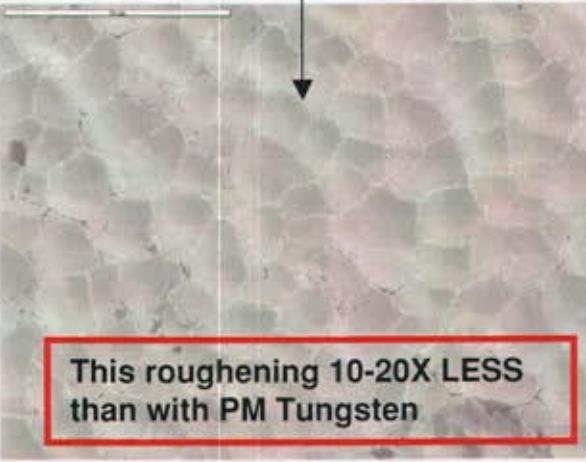
Top Row~ 1.0 J/cm Ra ~ 0.16 μ m



400 pulses



800 pulses



1200 pulses

This roughening 10-20X LESS
than with PM Tungsten

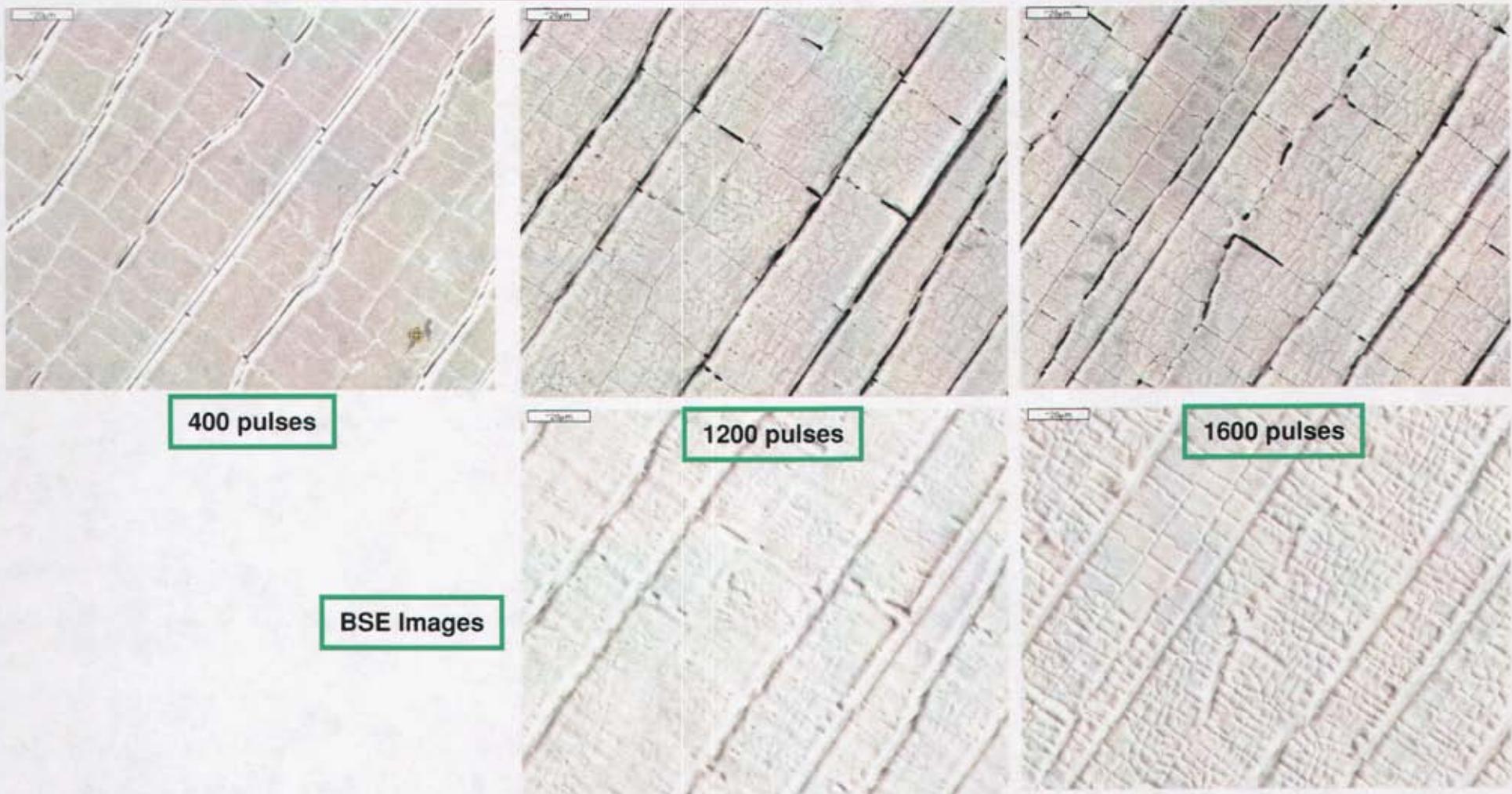
~ 1.4 J/cm²

All images -
1,000X MAG

Right Two ~ 1.7 J/cm²
Ra ~ 0.28 μ m

RHEPP-1 Surface Roughening, KS2000 Series

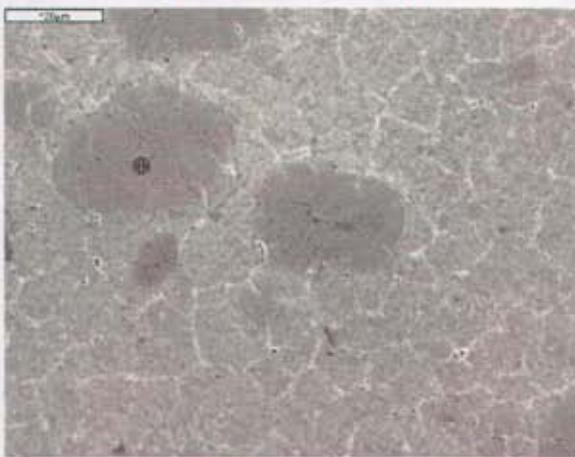
SEM, SingXtal RT, $\sim 1.1 \text{ J/cm}^2$: longitudinal cracks form, width stays constant, settling in between





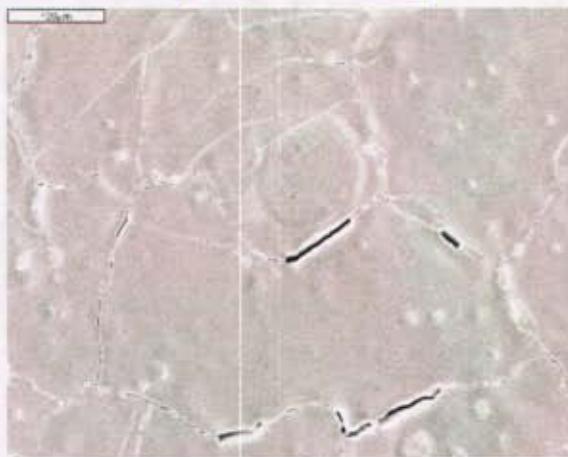
Three forms of Tungsten, treated at ~ same fluence (400 pulses):
Grain-refinement/strengthening, or below-surface burial
seem to restrict roughening/mass-loss.

1,000X MAG



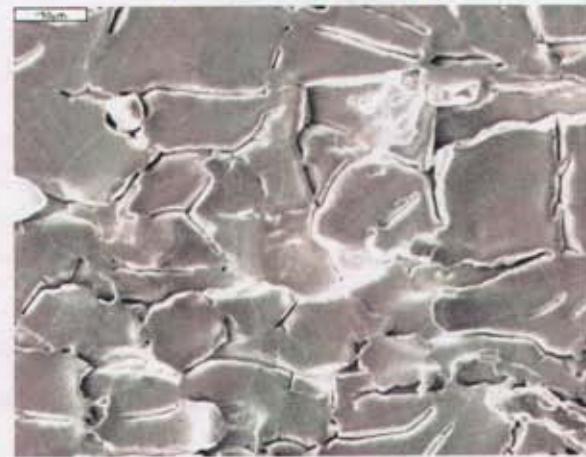
W-0.5%TiC 1.5 J/cm².
Ra = 0.04 μ m

1,000X MAG



M182Perp ~ 1.25 - 1.5 J/cm²
Ra ~ 0.15 μ m

300X MAG



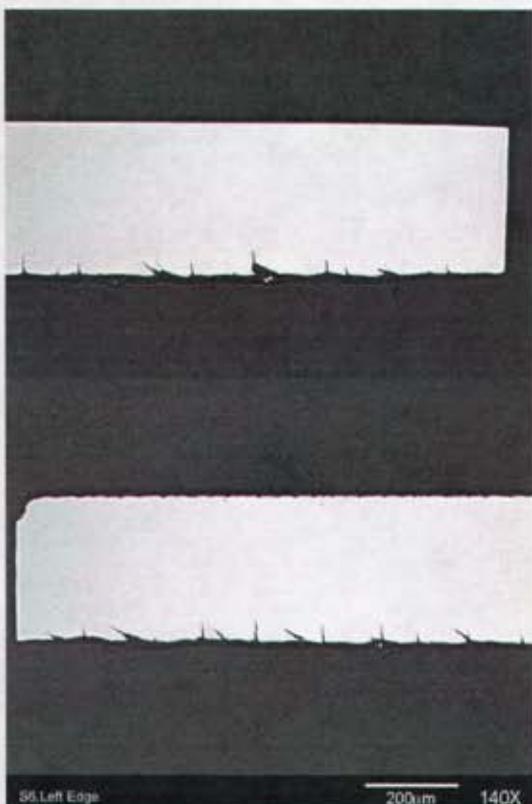
M182Parallel ~ 1.3 J/cm²
Ra ~ 4.5 μ m

Two on right are SAME material

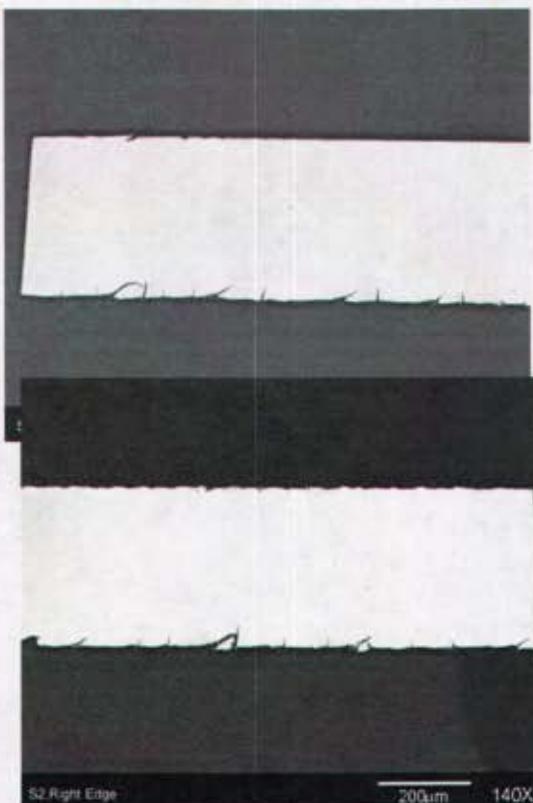


Single-Crystal Tungsten, 400 and 1600 pulses: No fatigue-cracking in-depth

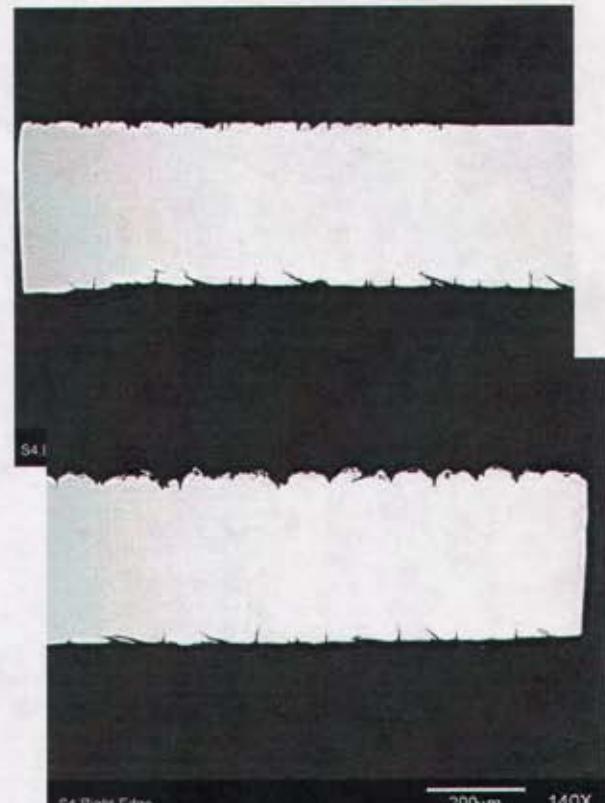
1.2 J/cm² 400X Upper 1600X lower



1.9 J/cm² 400 pulses



3.5 J/cm² 400 pulses



All 140X MAG

1600 pulses

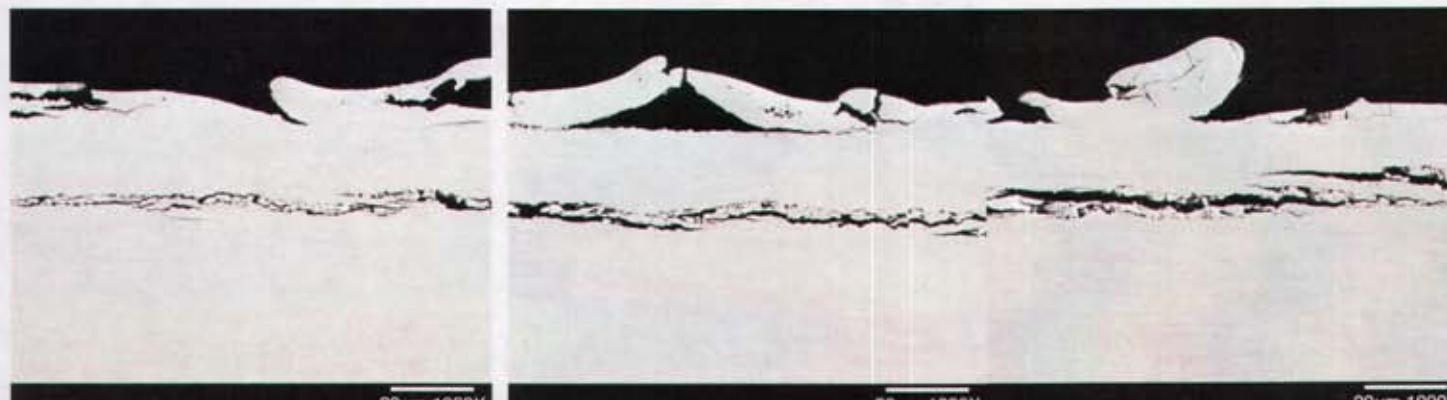
1600 pulses

Top surface is treated in all cases
Cuts on bottom surface look like sample prep



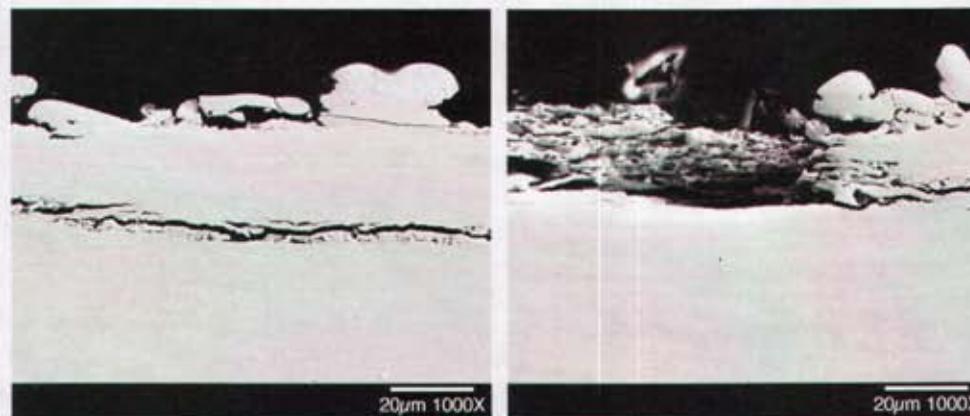
RHEPP-1 Surface Roughening

PM Tungsten, 1.9 J/cm² RT, sectioned SEMs (near Melt):
Large distortions in near-surface zone



400 pulses

Increasing pulse number



All images BEI 1000X MAG



1600 pulses

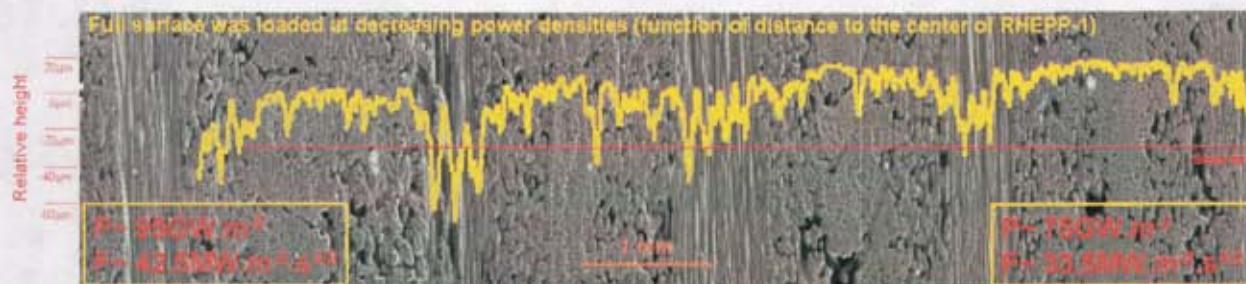
Preferential erosion of carbon-carbon composites

Same type of preferential erosion under different conditions
(particles, pulse duration, deposited energy)



Electron beam loading in JUDITH facility:
120kV, 2.4 GW/m², 5 ms
Forschungszentrum Juelich, Germany

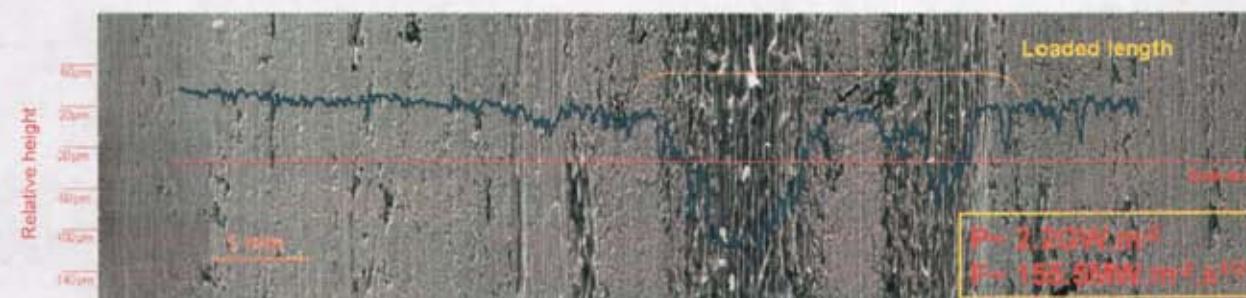
Ion beam loading in RHEPP-1 facility:
700kV, 75-95 GW/m², 200 ns
Sandia National Laboratories



DMS704 loaded in RHEPP-1
for 400 pulses

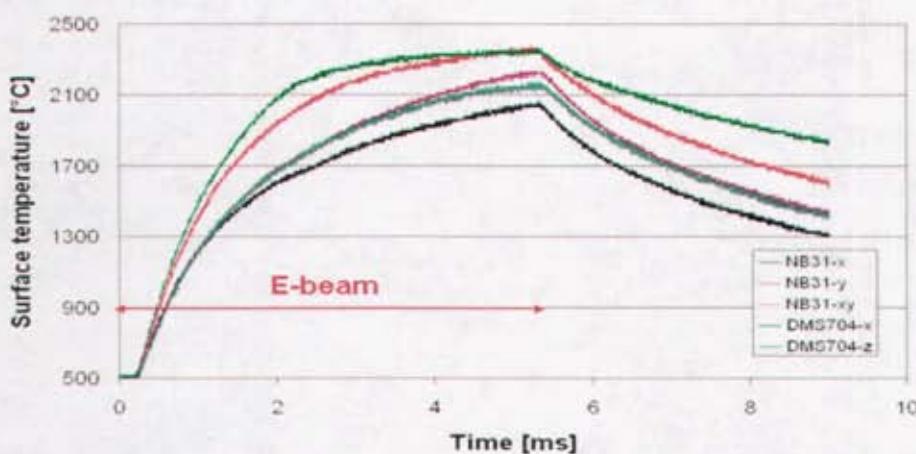
$F = P * \sqrt{t}$: High Heat Flux conditions
with Heat Diffusion effect included.
Comparison:

ITER ELMs (est):
 $22.4 - 67.1 \text{ MW m}^{-2} \text{s}^{1/2}$
RHEPP-1:
 $33 - 42 \text{ MW m}^{-2} \text{s}^{1/2}$



DMS704 loaded in JUDITH,
single pulse

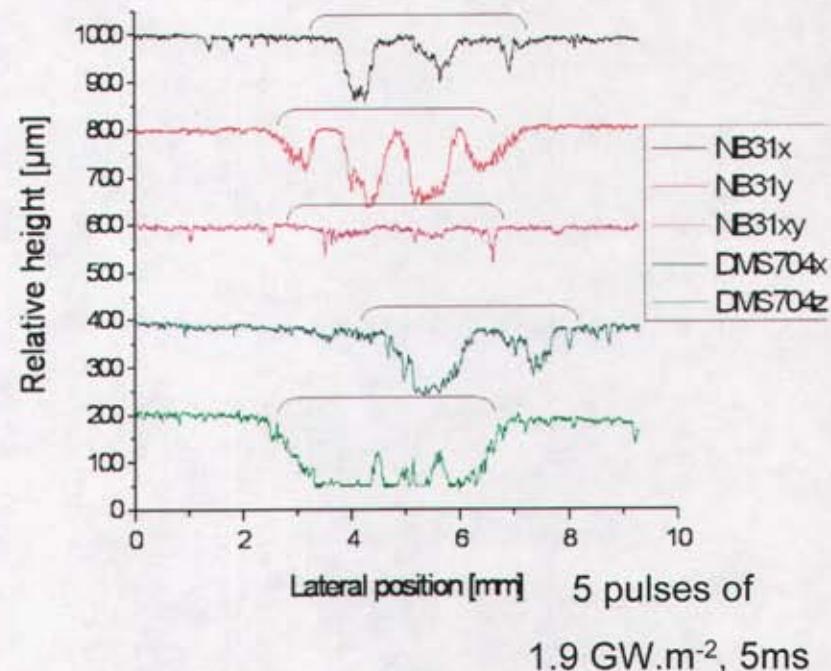
Preferential erosion can be reduced by aligning less fibers perpendicular to heat flow



NB-31, DMS704 mounted in different orientations and exposed to 5 JUDITH pulses each

Results

- Higher Measured Surface Temperature (left) and
- More Erosion (Below) in **RED** and **GREEN** directions with greater fiber alignment perpendicular to heat input



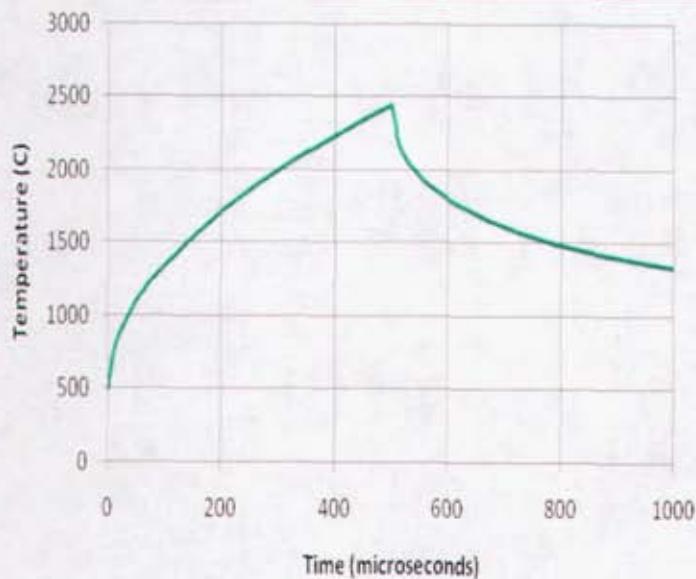
Optimal material orientation is essential

This allows:

- Maintaining good thermal conductivity (x direction)
- Limiting of local overheating (y and z directions)
- More homogeneous mechanical attachment of all the fibers

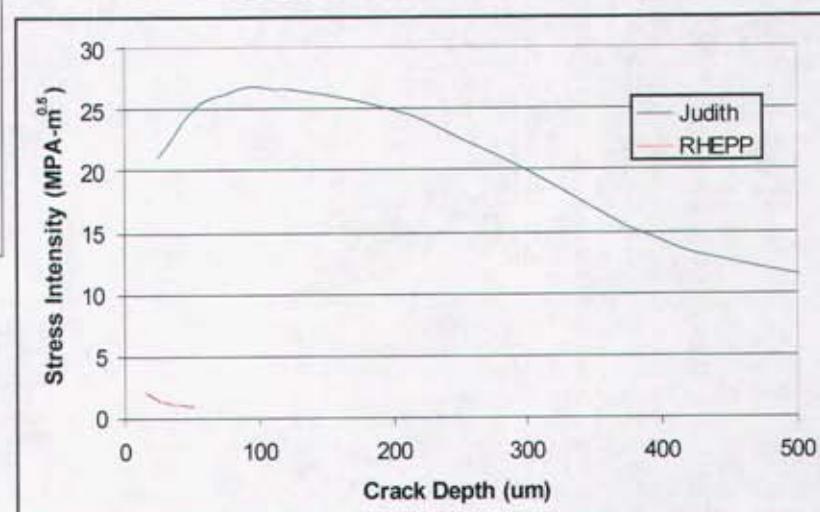
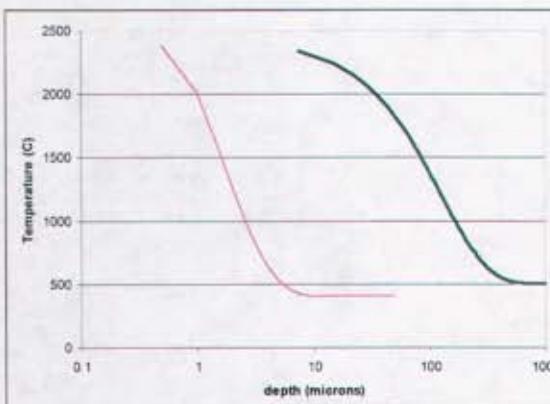


Fracture Modeling: Comparison of Tungsten exposed to IFE and MFE ELM Conditions



- 3 mm Tungsten on ferritic steel exposed to single heat pulse.
Fluence: 0.7 MJ/m^2 over $500 \mu\text{sec}$.
 $T_{\text{initial}} = 500\text{C}$, Tungsten properties from ITER Material Properties Handbook.
- Heat deposited at surface
- (Top Left): Surface temp reaches $\sim 2500\text{C}$
- (Bottom Left): Plastic Strain reaches 1%, gradient to $>250 \mu\text{m}$ depth

Unlike RHEPP heating, the ELM-like pulse produces fracture stresses at the fatigue crack threshold after one pulse



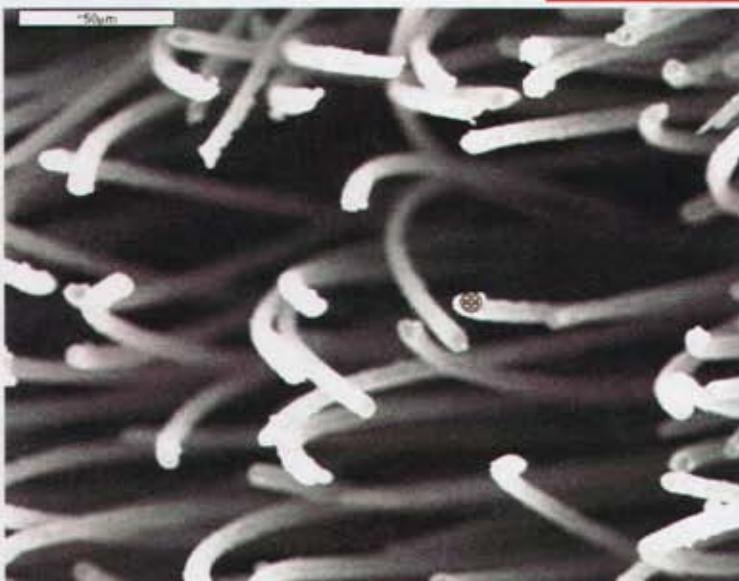
- (Top Left) RHEPP pulses with fluence chosen to reach same surface maximum temperature - 2500C
- (Mid Left) Plastic Strain Curves: Both effects MUCH deeper for the ELM case
- Bottom: Stress Intensity for the 'ELM' case at 25 MPa-m^{0.5} - at fatigue cracking threshold for tungsten (20-40 MPa-m^{0.5}). RHEPP at ~ 2 MPa-m^{0.5}
- This could explain why RHEPP thermomechanical effects take hundreds of pulses to develop.



RHEPP-1 Surface Roughening

Tungsten-coated Carbon Velvet survives 1600 pulses amazingly well

From T. Knowles, ESLI

Carbon PAN fibers w/ 1.6 μm W coating,
2% areal coverage

(ABOVE)

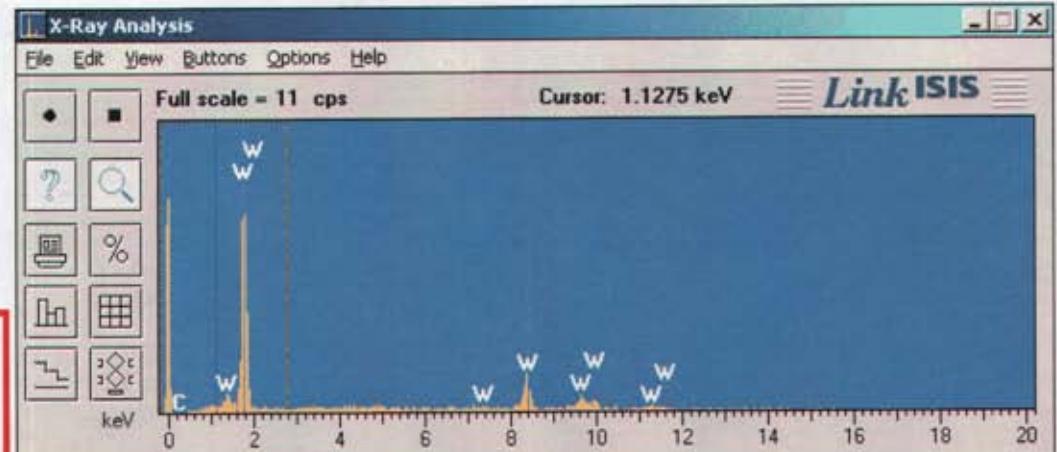
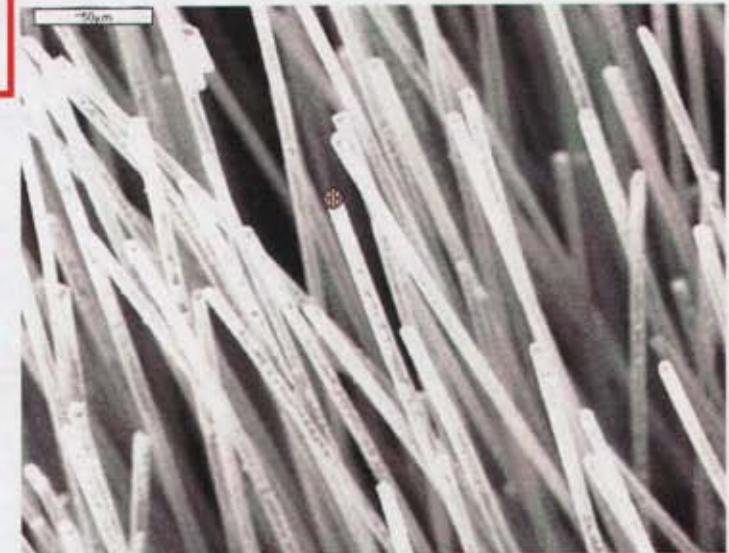
RT @ $\sim 2.8 \text{ J/cm}^2$, 1600 pulses

NOTE: bent tips, flat ends have W removed, rounded ends still have W

This reinforces recent JUDITH result:
Mechanical strength of PAN fibers may
more than make up for their lower Thermal
Conductivity compared to PITCH

(RIGHT)
520C (nominal), 1600
pulses, 1.5 $\text{J/cm}^2/\text{pulse}$

NOTE: W remaining
on tips (see below)
and sides



EDS scan of tip (cross): W rich



Exposure Results Summary_1

- **Tungsten:**

- Surface roughens due to thermomechanical stress, occurs **BELOW** the melt point. Relief develops over hundreds of pulses. Heating to 500C, i.e. above the DBTT, delays but does not stop this process.
- Roughening Threshold for multi-pulse exposure $\sim 1 - 1.2 \text{ J/cm}^2$ - corresponds to $\sim 1400 - 1700\text{C}$ maximum surface temperature.
- Grain size and orientation very important. Worst form is polycrystalline lightly-deformed, - develops high relief ($5+ \mu\text{m } R_a$, up to $100 \mu\text{m } P-V$). This relief is linked to confirmed mass loss.
- Deformed tungsten with grains perpendicular to surface (M182) suffers much less roughening, as does W-25Re alloy (not shown).
- W-0.5%TiC (Kurishita) - fine grain Tungsten shows robust survivability, low roughening. Processing with Hydrogen seems to improve grain boundary strength compared to Argon, as predicted.



Exposure Results Summary_2

- Graphite:
 - CFCs perform best when fiber direction is oriented to conduct maximum heat below the surface, and when minimal fibers are parallel to surface, independent of whether they are PAN or PITCH fibers.
 - Some forms of graphite, e.g. R6650, MFC-1, 149A, show little/no mass loss at 1 J/cm^2 , i.e. at higher than roughening threshold for tungsten. This corresponds to surface temperature of 1800K, according to 1-D BUCKY modeling of high-thermal conductivity graphite.
 - Above this point, however, ablation/sublimation result in significant roughening and rapid mass loss.
 - These values are WELL below BUCKY modeling of sublimation threshold for high-conductivity graphite, $- 3.5 \text{ J/cm}^2$.
- ‘Engineered’ surfaces like ‘Velvet’ may represent the best solution for surface survivability. Robust PAN fiber survivability consistent with recent JUDITH findings that use of PAN limits brittle destruction (seen in PITCH fibers).
- Fracture Modeling indicates 1) single RHEPP pulses are well below threshold for Tungsten surface cracking, and 2) single ELM-like pulses produce much deeper strain and are at or near the Tungsten fracture threshold.