

Using Nanoparticles to Stabilize Thin Polymer Films

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Division of Polymeric Materials: Science & Engineering,
Nanotechnology Applications in Coatings**

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Presentation Outline

- **Wetting/dewetting behavior of polymer films**
- **Addition of nanoparticles to polymer films, and the resulting wetting/dewetting behaviors**
- **Potential application for this technology – chemical sensors**



Thin Polymer Films

- **Thin polymeric films are used in many new and emerging technologies:**
 - Dielectric coatings
 - Fuel cells
 - Nanolithography resist layers
 - Chemical and biological sensors
- **Films must be continuous, of uniform thickness and remain stable on a variety of substrates**
- **Often, however, the substrate is lower in energy than the polymer causing it to dewet under the appropriate conditions.**

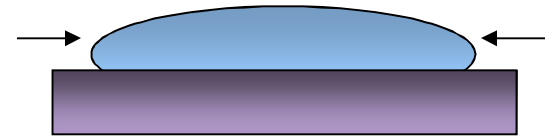
The Problem of Dewetting

- When a liquid is spread out over a solid, the stability of the system depends upon the surface energy of the substrate (γ_S), the surface tension of the liquid (γ_L) and the interfacial energy between the two (γ_{LS})
- The spreading parameter (S) dictates if a liquid will wet the surface or not

$$S = \gamma_S - \gamma_L - \gamma_{LS}$$



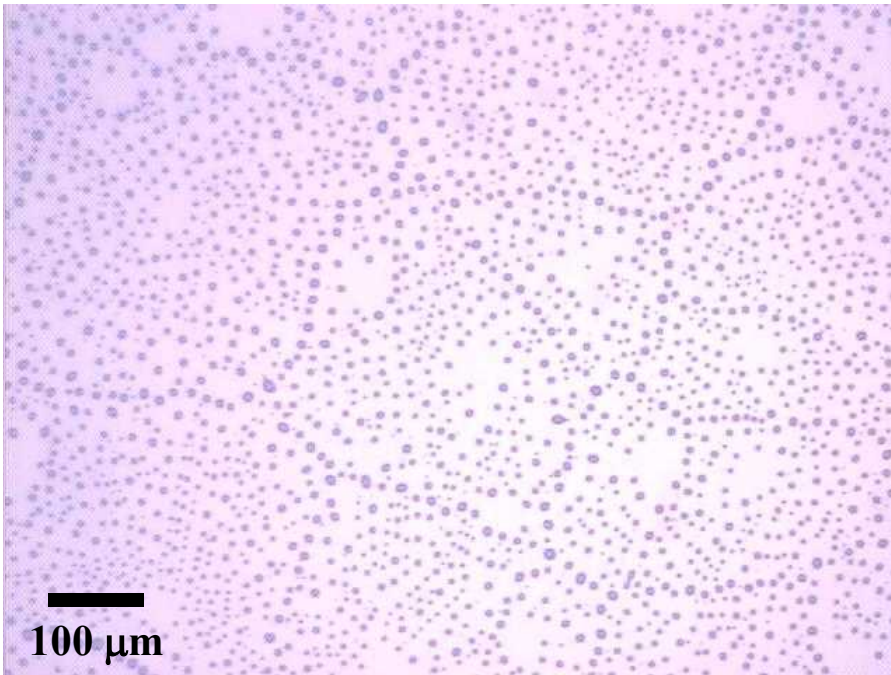
$S > 0$, wetting



$S < 0$, dewetting

Dewetting of Polymer Films

Pure Polystyrene film (33 nm) annealed under a saturated toluene atmosphere



50 minutes

- **Glass Transition Temperature (T_g)**
 - Above this temperature, polymer is mobile
 - Induce dewetting
 - Heat the sample
 - Expose the sample to a plasticizing agent
- **Types of dewetting**
 - Spinodal
 - Nucleation and hole growth



Film Equilibrium

- Bulk experiments were performed to determine the equilibrium concentration of solvent absorbed into the polymer
 - Polystyrene was weighed out and placed in a saturated toluene atmosphere
 - Sample was reweighed until there was no change to ensure equilibrium – one week
 - Final concentration of the sample was ~600 mg PS/ml solution
- For a thin film, the equilibration time is expected to be much shorter:

$$\frac{D\tau}{\Delta^2} > 1$$

$$D \sim 10^{-6} \text{ cm}^2/\text{s}, \Delta = 30 \text{ nm} \rightarrow \tau \sim 10 \text{ } \mu\text{s}$$

• Bird, R. B.; Stewart, W. E.; Lightfoot, E. N., *Transport Phenomena*. J. Wiley: New York, 1960.

• Rauch, J.; Kohler, W., Collective and thermal diffusion in dilute, semidilute, and concentrated solutions of polystyrene in toluene. *Journal of Chemical Physics* **2003**, 119, (22), 11977-11988.



Film Viscosity

- Using the Martin Equation we can estimate the viscosity of the film during annealing which will relate to the rate of dewetting:

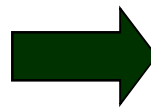
$$\frac{\eta_{sp}}{c[\eta]} = e^{k'[\eta]c}$$

$$\eta_0 = 0.56 \text{ cP}$$

$$c = 600 \text{ mg/ml}$$

$$[\eta] \sim 38 \text{ ml/g}$$

$$k' \sim 0.33$$



$$\eta = 23 \text{ Pa-s}$$

~ pure PS at 250 °C

•Gandhi, K. S.; Williams, M. C., Solvent Effects on Viscosity of Moderately Concentrated Polymer Solutions. *Journal of Polymer Science Part C-Polymer Symposium* **1971**, (35), 211.

•McCabe, W.; Smith, J.; Harriott, P., *Unit operations of chemical engineering*. McGraw-Hill: New York, 1993.

•Brandrup, J.; Immergut, E. H., *Polymer Handbook*. John Wiley & Sons: New York, 1989.



Effective Glass Transition Temperature

- The Fox Equation can be used to determine the effective T_g of the film during annealing:

$$\frac{1}{T_g} = \frac{w}{T_g^P} + \frac{1-w}{T_g^S}$$

Mass fraction of polymer, $w = 0.60$, $T_g^P = 379$ K, $T_g^S = 117$ K

↳ $T_g = 200$ K or -73 °C

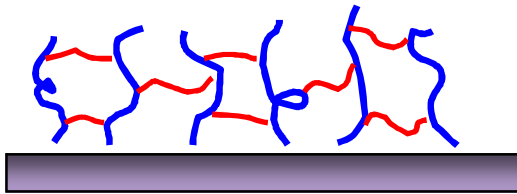
- Therefore, rapid dewetting is expected at room temperature

• Rauch, J.; Kohler, W., Collective and thermal diffusion in dilute, semidilute, and concentrated solutions of polystyrene in toluene. *Journal of Chemical Physics* **2003**, 119, (22), 11977-11988.

• Wiedersich, J.; Surovtsev, N. V.; Rossler, E., A comprehensive light scattering study of the glass former toluene. *Journal of Chemical Physics* **2000**, 113, (3), 1143-1153.



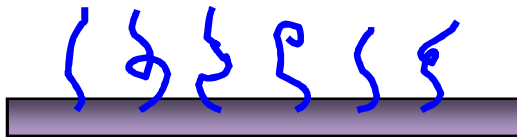
Ways to Stop Dewetting



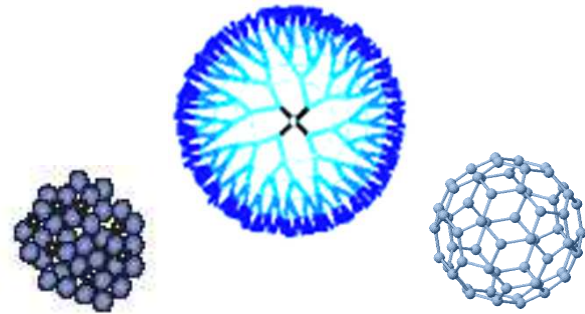
Crosslinking *X*



Surface Treatment *X*



Grafting *X*

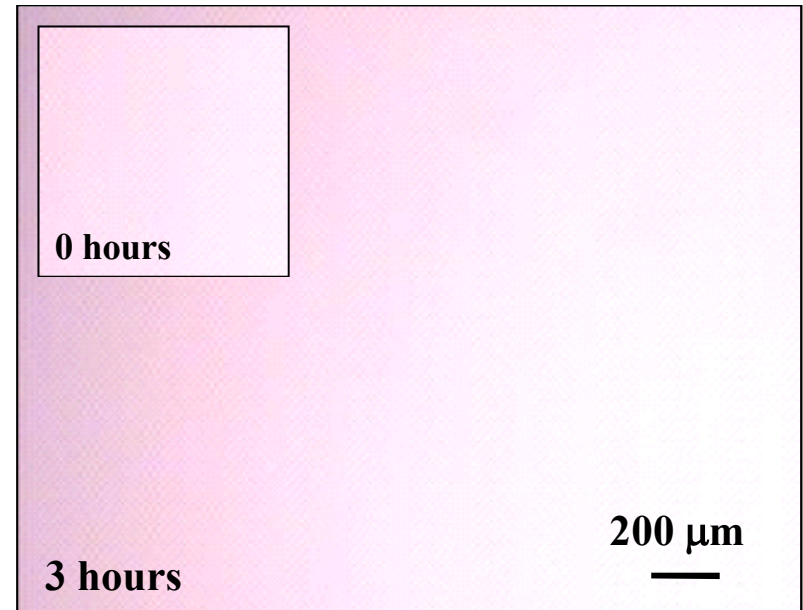


Nanoparticles ✓

Addition of Fullerenes

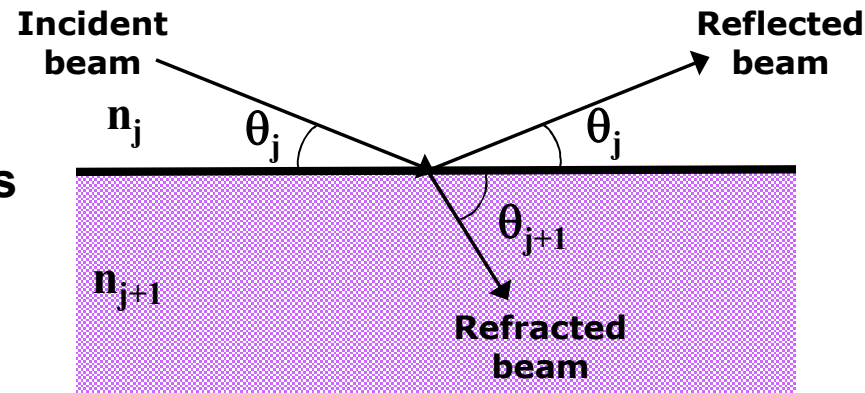
- A solution of PS with 3 wt% C₆₀ was spin-coated on a piranha-cleaned wafer
 - Film thickness = 33 nm
- Sample was annealed for 3 hours under a saturated toluene atmosphere
 - No dewetting seen!
 - The fullerenes appear to eliminate dewetting just as they do for high temperature annealing
- Previous studies suggest that the elimination of dewetting is due to the location of the nanoparticles in the film
 - Neutron reflectivity

PS + 3 wt% C₆₀ film (33 nm) annealed under a saturated toluene atmosphere



Neutron Reflection

- Neutron reflection is a technique that can be used to determine the depth-composition profile of thin planar samples
 - A beam of neutrons strike the sample surface at a glancing angle (θ)
 - The beam is either reflected or refracted
 - The angle of the refracted beam is dependent on the neutron refractive index of the material
- The neutron refractive index for a material is dependent on its scattering length density (ρ_z)
- By using materials with sufficient contrast in their scattering length densities, it is possible to determine their location in the sample

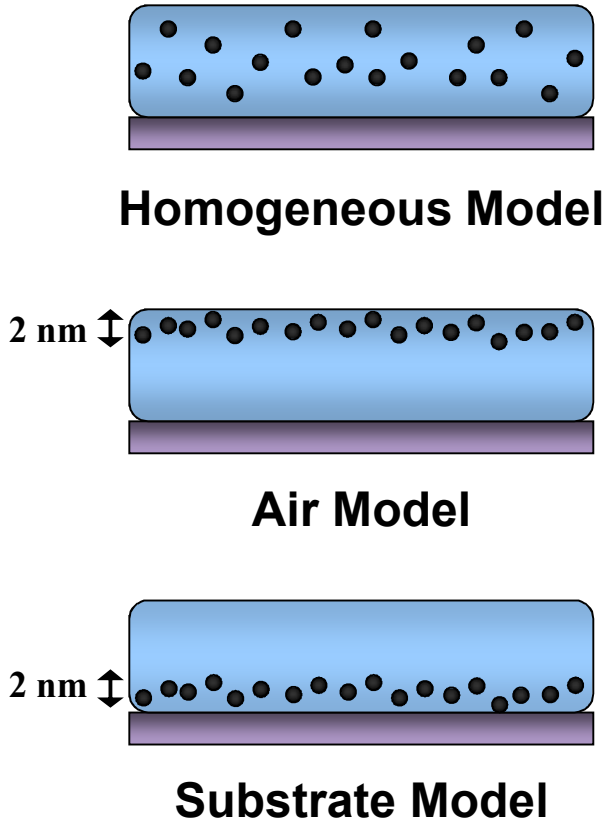


Snell's law: $n_j \cos\theta_j = n_{j+1} \cos\theta_{j+1}$

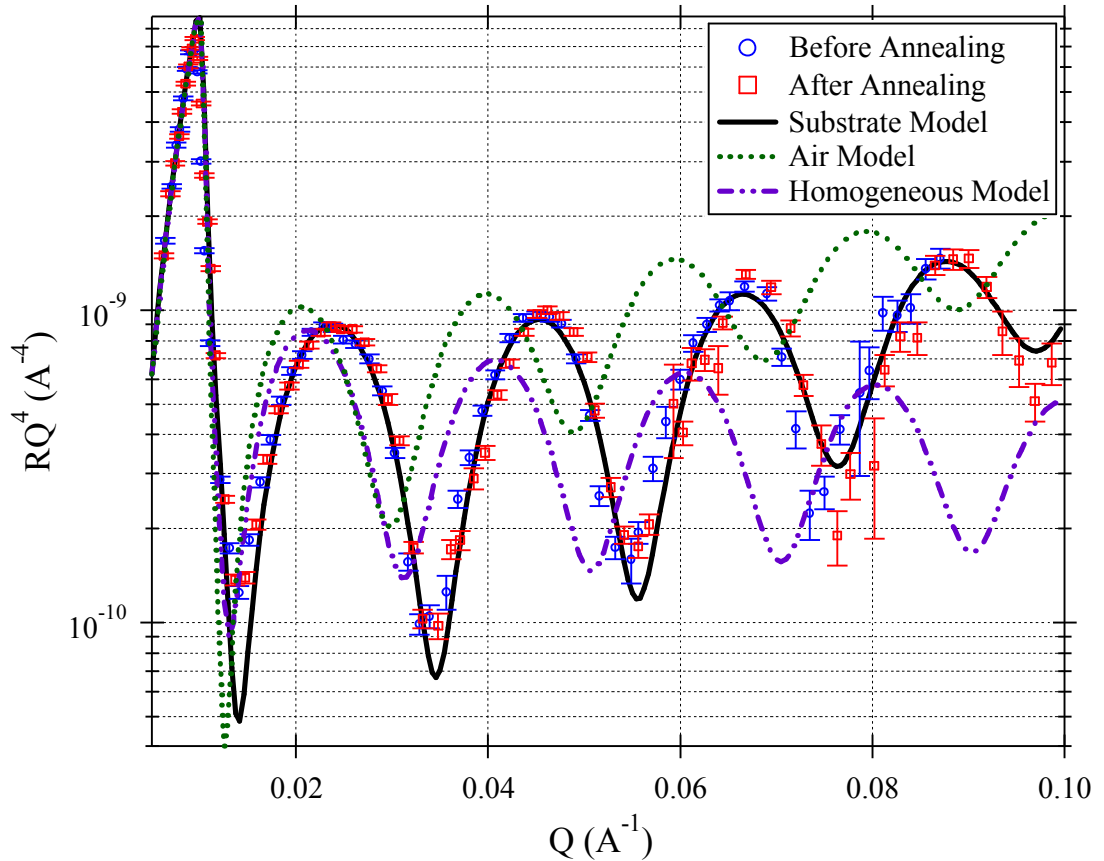
Scattering length densities for materials used in this work

Material	$\rho_z (\text{\AA}^{-2}) \times 10^6$
Silicon	2.07
C ₆₀	5.73
PS	1.41
dPS	6.47

Reflectivity Data



Reflectivity of 75k PS + 3 wt% C60 Film (31.5 nm)



Sample was annealed 3 hours under a saturated toluene atmosphere

Modeling Reflectivity Data

Model	Layer	Thickness (Å)	SLD (10^6 Å^{-2})
Substrate	1	295	1.41
	2	20	2.66
	wafer	-	2.07
Air	1	20	2.66
	2	295	1.41
	wafer	-	2.07
Homogeneous	1	315	1.49
	wafer	-	2.07

- From reflectivity model:

$$\phi_{C60,L} = \frac{\rho_L - \rho_{PS}}{\rho_{C60} - \rho_{PS}}$$

$$\phi_{C60,L} \sim 0.29$$

- 3 wt% $\rightarrow \phi_{C60} = 0.018$

- From mass balance:

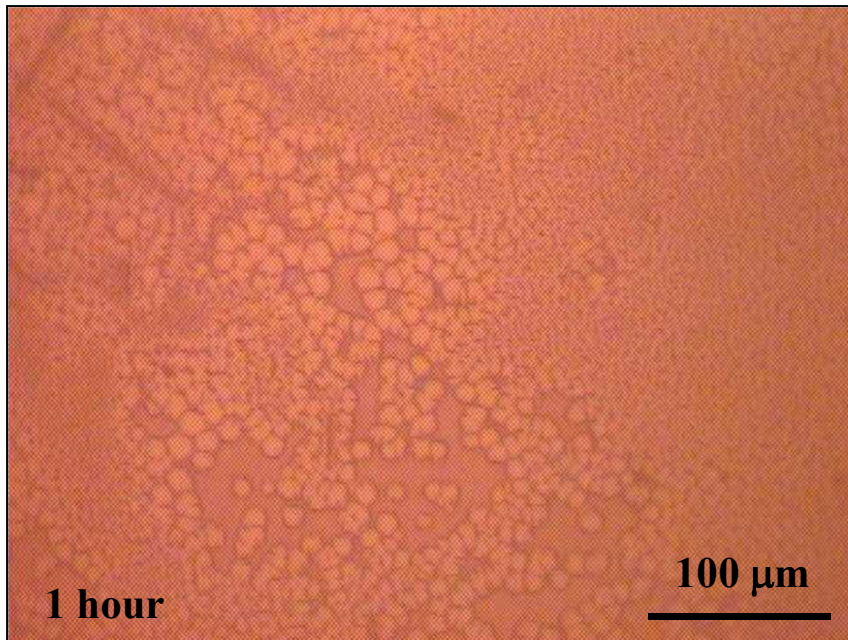
$$\phi_{C60,L} = \frac{\Delta}{\delta} \times \phi_{C60}$$

$$\phi_{C60,L} = 0.28$$

Good agreement!

Fullerenes First

PS film (30 nm) floated onto a fullerene layer and annealed under a saturated toluene atmosphere



- A film was placed onto a fullerene layer and then solvent annealed
 - Dewetting of the film still occurred!
- Therefore can not attribute inhibition of dewetting solely to nanoroughness or a change in surface energy

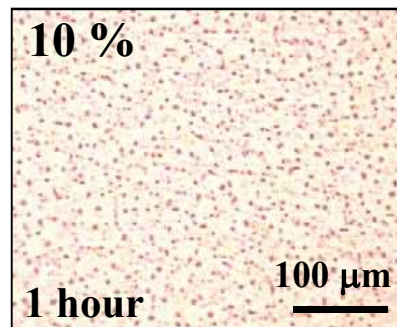
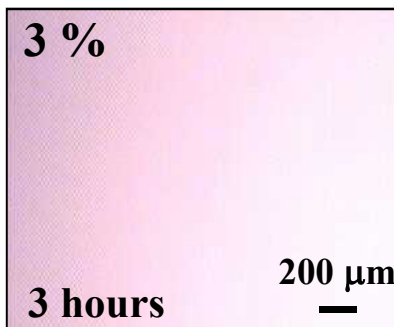
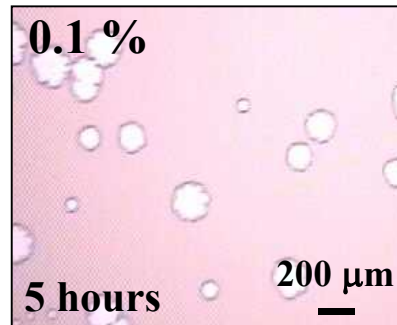
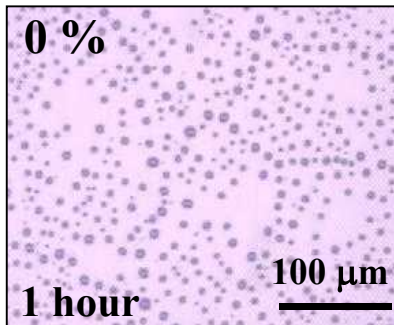


How Dewetting is Inhibited

- From reflectivity, we know the fullerene-enriched layer at the substrate is ~ 2 nm thick, which is 2-3 fullerenes high
 - Layer forms during the spin-coating process due to phase separation from the poor solubility of fullerenes in the solvent
- The fullerenes create a gel-like network 2 nm thick that shields the adverse van der Waals forces emanating from the substrate

Concentration Dependence

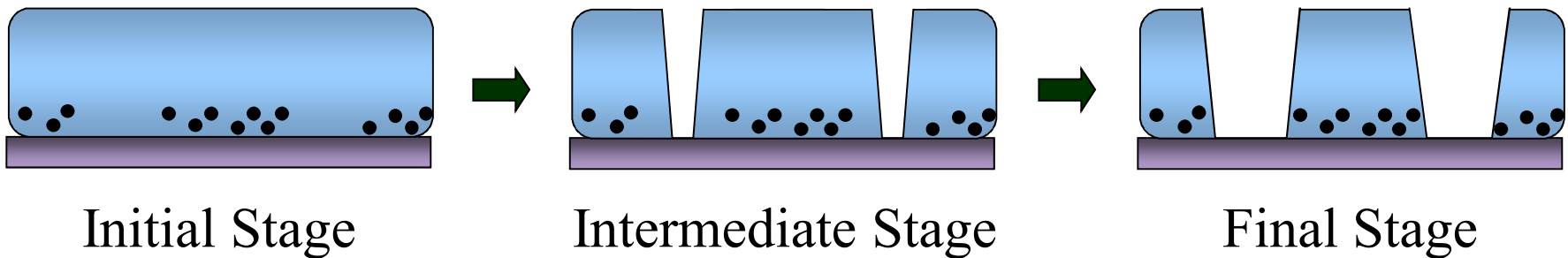
PS films with varying C_{60} concentrations (~ 30 nm) annealed under a saturated toluene atmosphere



- The concentration of C_{60} dictates the ability of the film to resist dewetting
- There is an optimum concentration needed to fully retard dewetting
 - Below this concentration, holes form but eventually stop growing
 - Above this concentration, dewetting is seen again

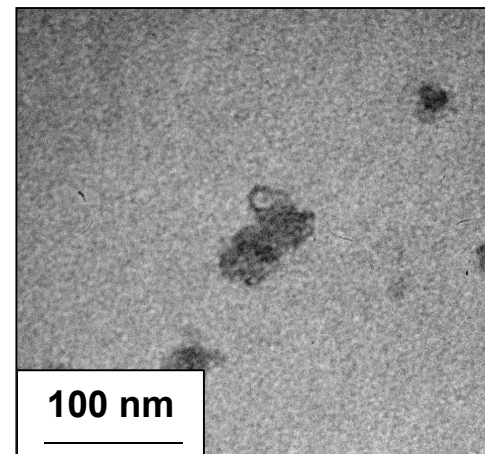
0.1 wt% C₆₀ in 30 nm PS film

- Partial dewetting occurs when the concentration of C₆₀ is too low
 - Holes form where there are no or few nanoparticles
 - The holes grow until they reach an area where there are sufficient nanoparticles to inhibit dewetting

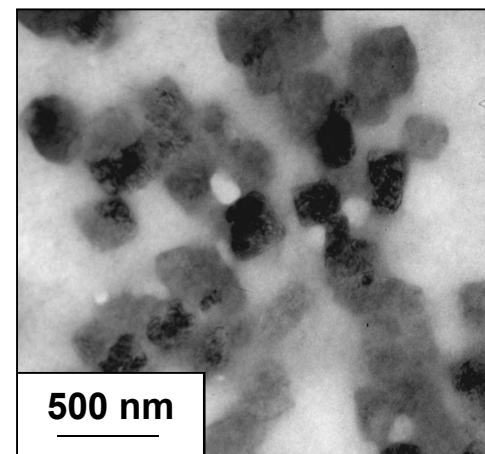


TEM for Comparison of 10 wt% Samples

- TEM was used to check for agglomeration of the fullerenes
 - Very few agglomerates were seen in the 3 wt% film
 - All agglomerates were <100 nm in size
 - Large clusters of agglomerates were seen throughout the 10 wt% film
 - Agglomerates were on the order of 200-300 nm in size, with micron sized clusters
- Particles of this size act as nucleating sites as seen in colloidal-sized particle systems



3 wt% C₆₀

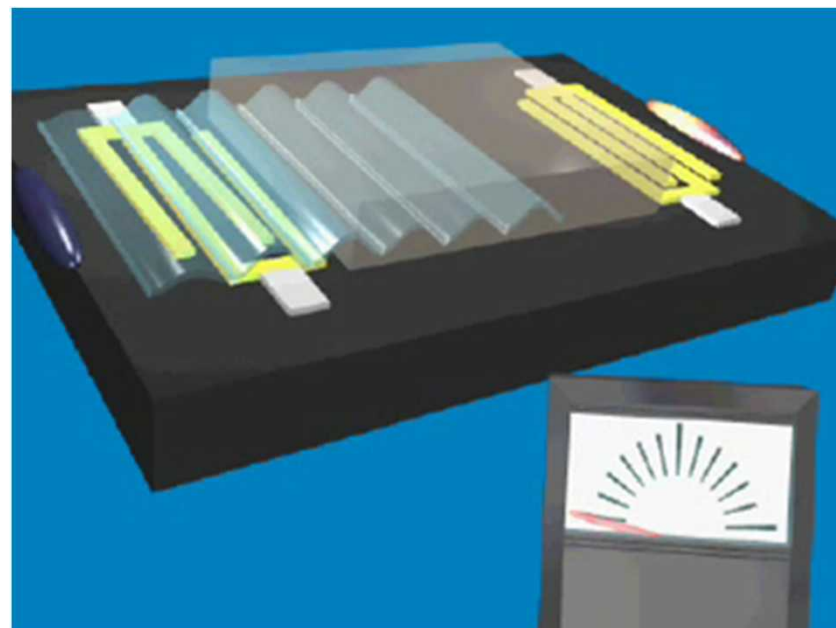


10 wt% C₆₀



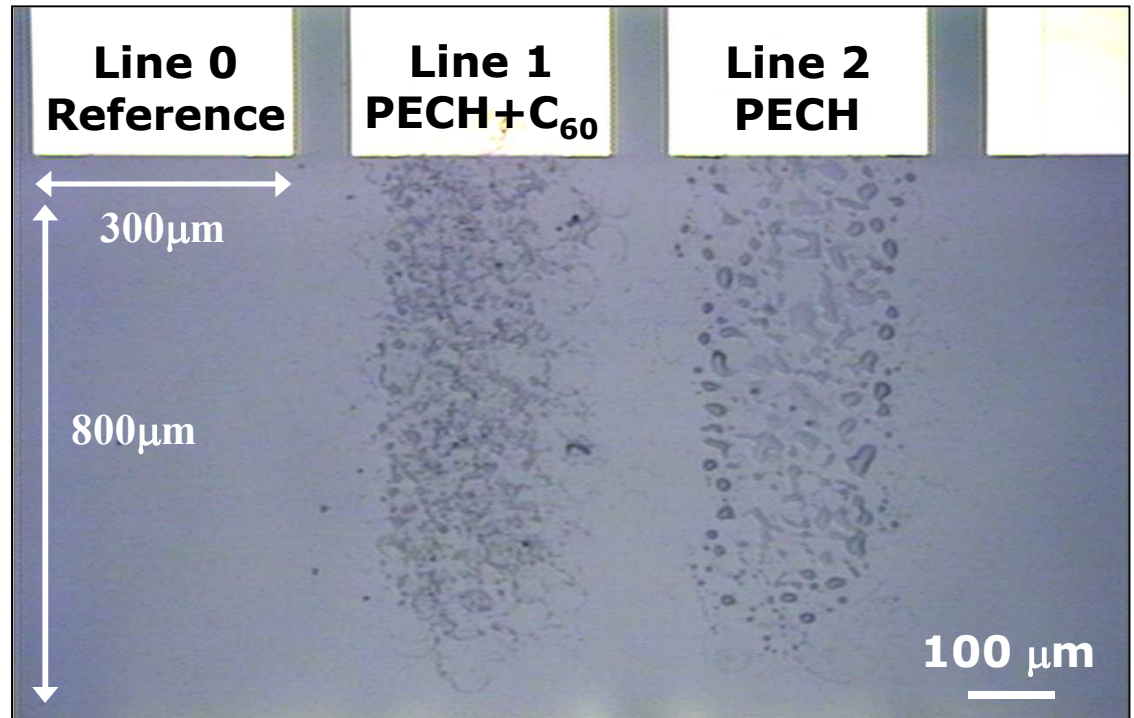
Application: Sandia's μ ChemLab – Detection Stage

- **Surface Acoustic Wave (SAW) Sensor**
 - Quartz substrate
 - IDTs
 - Polymer film
- **Analyte absorbed into film**
 - Small increase in mass results in a change in the velocity of the SAW
- **Difficulty consistently depositing a stable polymer film on sensor surface**
 - Addition of fullerenes gives a more stable response to challenges



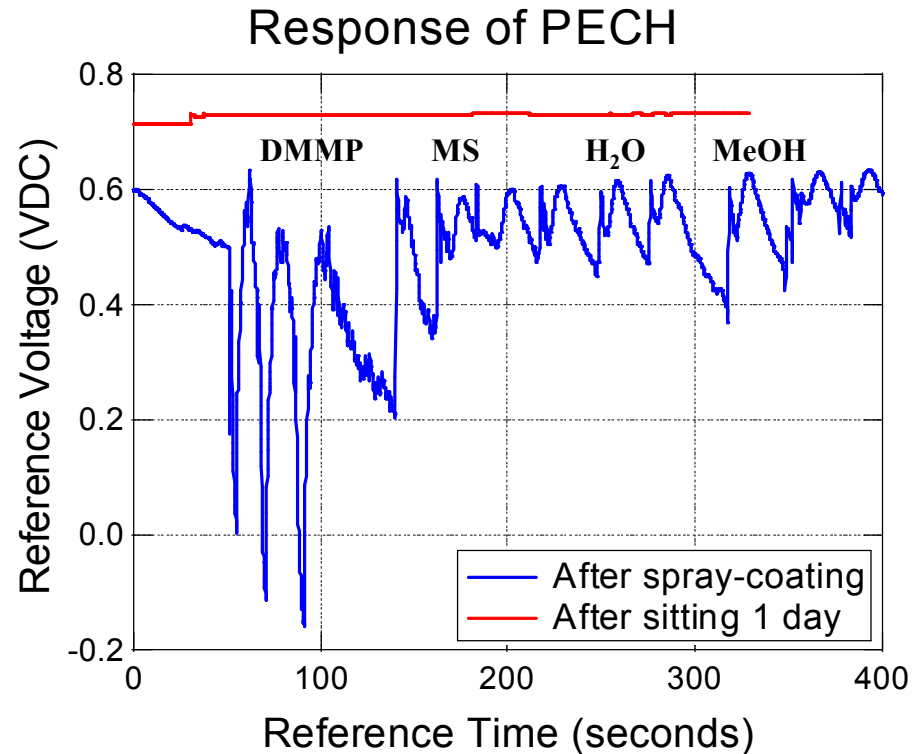
Live SAW Sensor

- A live SAW sensor was sprayed with PECH (polyepichlorohydrin) and PECH + C₆₀
- The sensor was then challenged with various solvent vapors to test its response



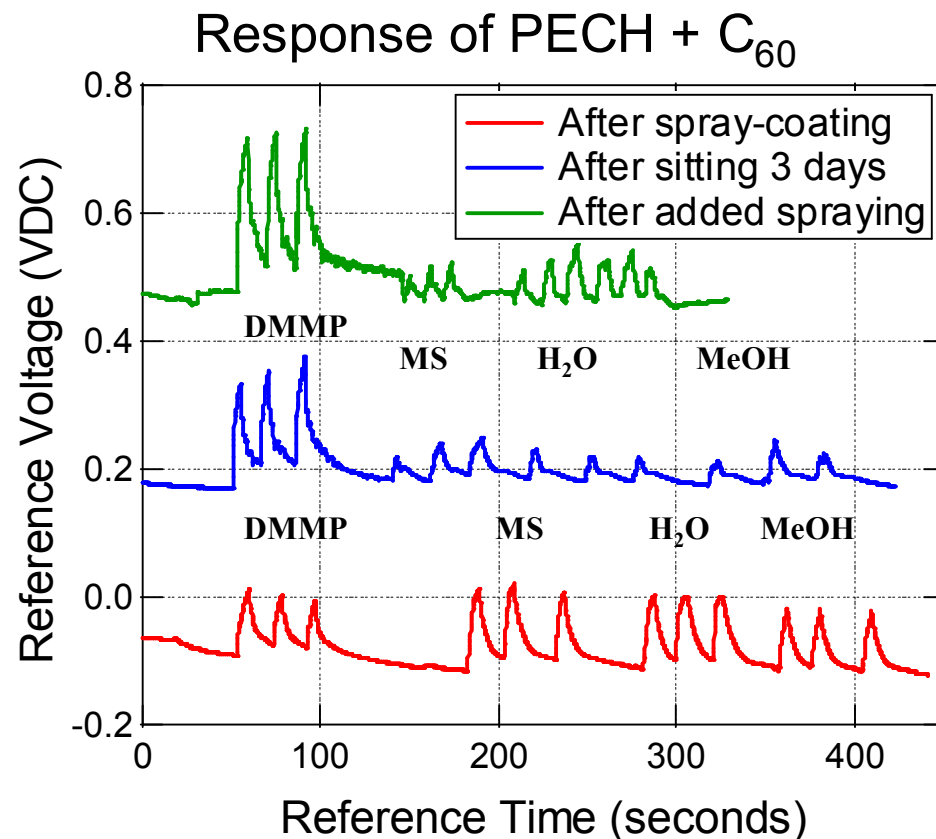
Sensor Response: PECH

- The sensor response of pure PECH upon challenging is very erratic with an unstable baseline
 - Possible dewetting
- After one day, the sensor was challenged again giving no response
 - Sensor inoperable



Sensor Response: PECH + C₆₀

- Upon addition of fullerenes, the sensor gives a stable response with a stable baseline when challenged after spray-coating
- After several days and even the addition of more polymer, the sensor response remains stable





Conclusion

- **Thin polystyrene films will dewet from a silicon substrate upon exposure to a saturated toluene atmosphere**
- **The addition of fullerenes to the polymer solution before spin-coating can inhibit dewetting of the film**
- **The inhibition of dewetting is caused by the fullerenes forming a gel-like layer at the substrate**
- **This technique is very appealing due to the fact that it does not alter the properties of the polymer or the substrate**
- **This technique can be used in sensor applications to manufacture more robust and reliable sensors.**

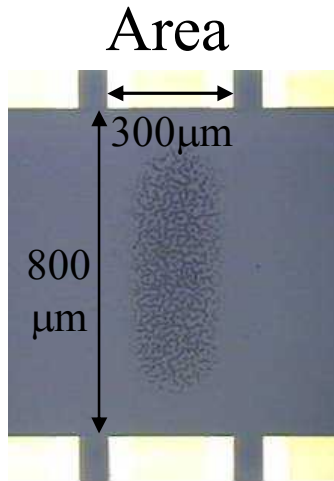


Thank you!

Questions?

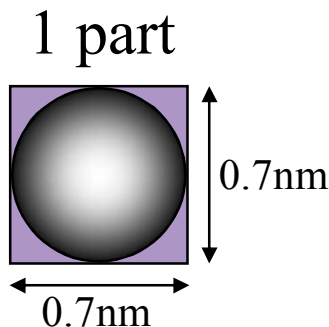
Why Fullerenes?

- Cheap and readily available!



$$Area = 300 \mu m \times 800 \mu m = 2.4 \times 10^{11} nm^2$$

$$\frac{1 part}{(0.7 nm)^2} \times \frac{3 \times 10^{-22} g}{1 part} = 6.1 \times 10^{-22} g/nm^2$$



$$(2.4 \times 10^{11} nm^2) \times (6.1 \times 10^{-22} g/nm^2) = 1.5 \times 10^{-10} g$$

$$(1.5 \times 10^{-10} g) \times (\$250/g) = \text{n\$}37.5/\text{sensor}$$



Neutron Reflection

- By using materials with sufficient contrast in their scattering length densities, it is possible to determine their location in the sample

$$\rho_z = \frac{(\sum b_i)DN_A}{M_m}$$

$$n_m = 1 - \frac{\lambda \rho_z}{2\pi}$$

- The specular reflection (R) is measured as a function of the neutron wave vector transfer (Q)

$$Q = \frac{4\pi}{\lambda} \sin \theta$$

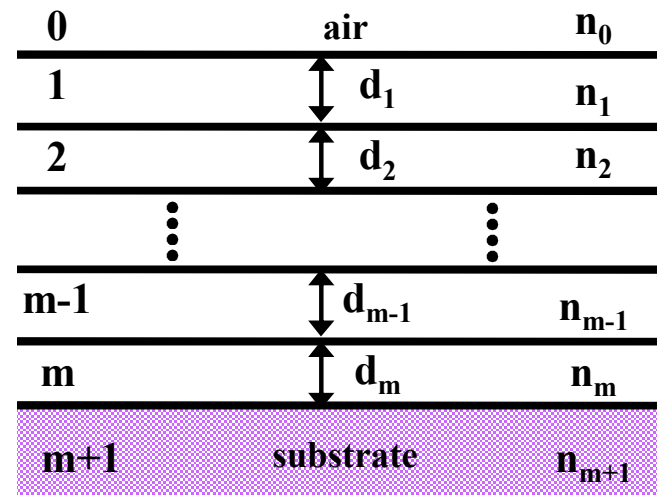
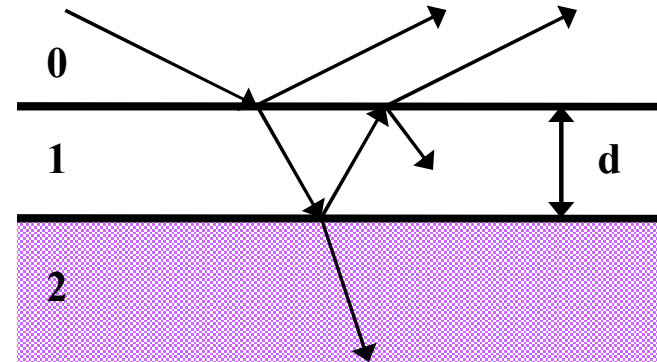
$$R(Q) = \frac{I_{ref}(Q)}{I_{inc}(Q)}$$

Reflectivity

- The reflectivity data can then be modeled using layers of different scattering length densities to determine the depth-composition profile

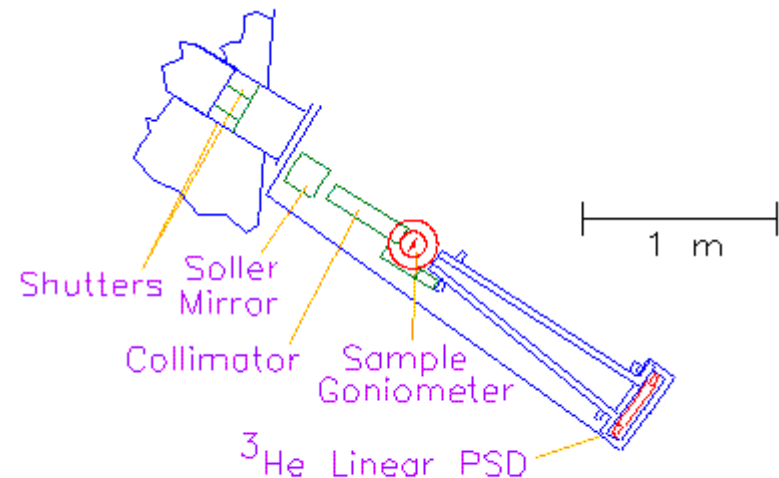
$$r_{m,m+1} = \frac{n_m \sin \theta_m - n_{m+1} \sin \theta_{m+1}}{n_m \sin \theta_m + n_{m+1} \sin \theta_{m+1}}$$

$$R = r_{m,m+1}^2$$



POSY2

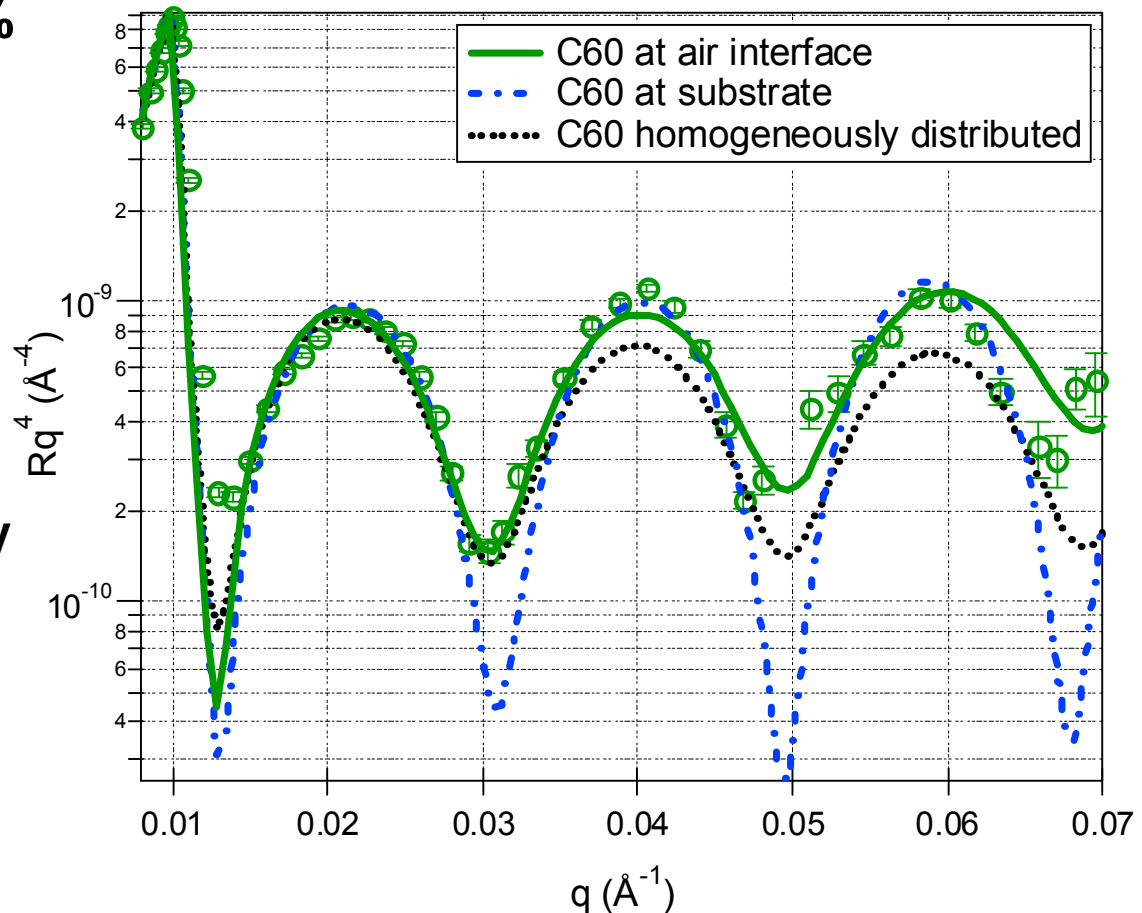
- The primary pulsed beam contains all wavelengths in the spectrum moderated to 20 K by a solid methane moderator. The intensity reflected at one angle q is measured as a function of the wavelength. The reflectivity is calculated by normalizing the intensities reflected to those of the direct beam. This measurements covers a range of q 's defined by the largest and the shortest wavelengths available. To extend the range of q measurements are taken at different angles. Reflectivity curves taken at different angles are spliced together by fitting the data in the partially overlapping q ranges. The data are put on an absolute basis by assuming that at the lowest q part of the q range covers the region of total reflection ($R=1$). The procedure assumes that the resolution function $\Delta q/q$ is constant.



Beam Size	Neutrons/pulse	$\Delta q/q$	θ range	λ range
5×0.3 cm	100	3-5%	0-3°	1-16 Å

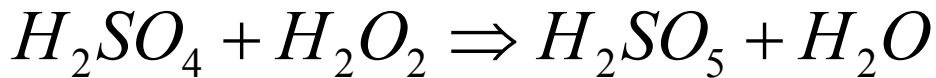
Reflectivity of “Flipped” Films

- A polystyrene with 3 wt% fullerenes was spin-coated onto freshly cleaved mica and “flipped” onto a Sigmacote silanized wafer
 - Expect fullerene enriched layer to initially be at air interface
- Was not able to perform reflectivity on annealed film because dewetting occurred!

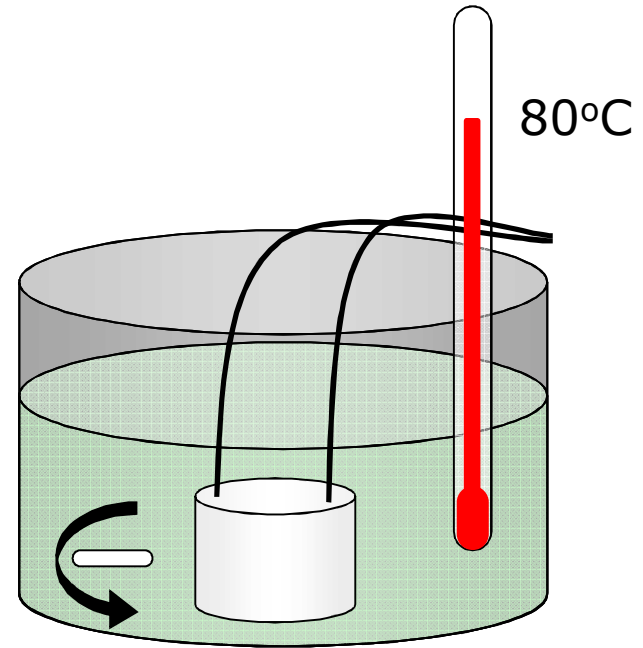


Piranha Cleaning

- Wafers are placed in a Teflon holder and placed in a beaker with 70% H_2SO_4 and 30% H_2O_2 by volume
- The solution is stirred continuously and kept at 80°C for 1 hour



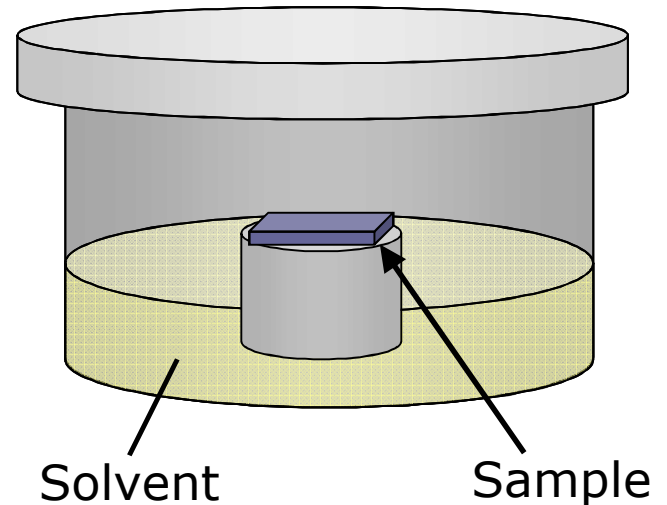
- The piranha oxidizes the organic contaminants making them soluble in the solution so they may be washed away
- The wafers are then rinsed in filtered DI water and used immediately



$$\gamma_S^d \approx 34.8 \frac{mN}{m}; \gamma_S^p \approx 35.8 \frac{mN}{m}$$
$$\Rightarrow \gamma_S \approx 70.6 \frac{mN}{m}$$

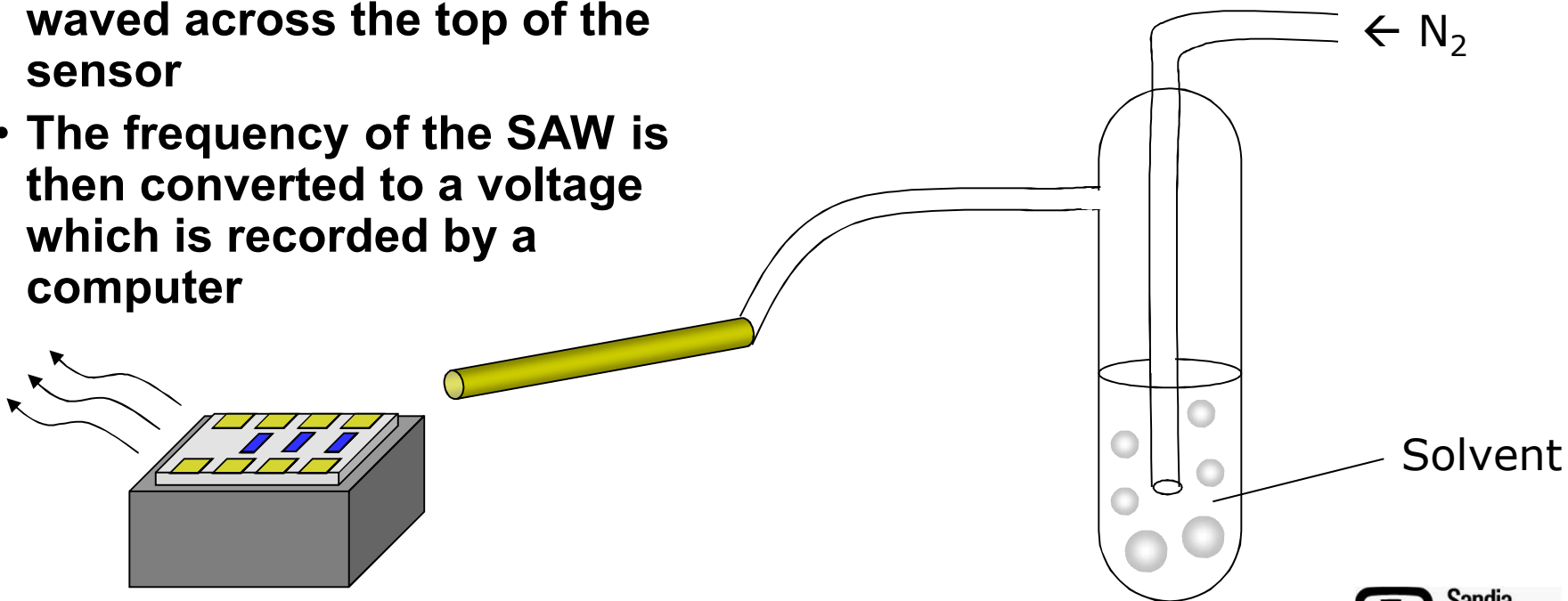
Solvent Annealing

- Sample is suspended above the solvent in a tightly sealed container
- Solvent and its vapor reach equilibrium and also the solvent is absorbed into the film reaching equilibrium



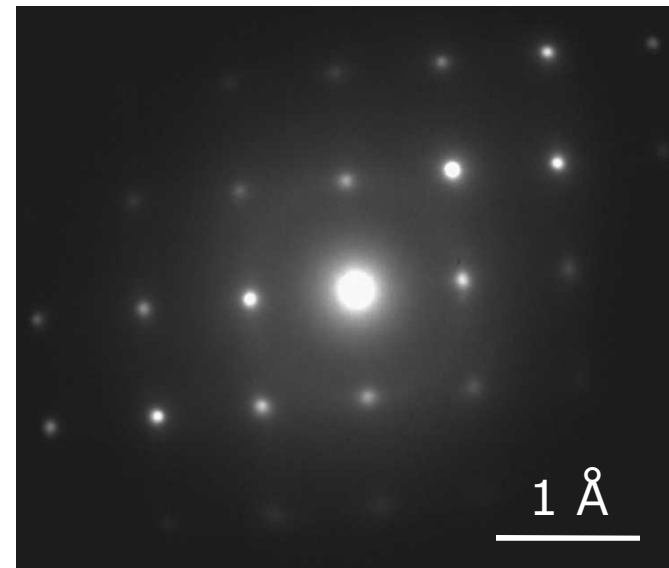
Challenging the Sensor

- Nitrogen is fed to a bubbler which is filled with the solvent
- It bubbles through and creates a saturated vapor stream which is fed through a nozzle and waved across the top of the sensor
- The frequency of the SAW is then converted to a voltage which is recorded by a computer



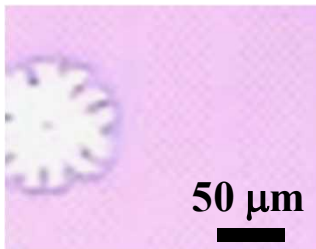
TEM Diffraction

- Diffraction was done on a fullerene agglomeration
- Diffraction pattern shows crystalline structure of the fullerenes
- More experiments would need to be done tilting the sample in different orientations to determine the exact structure

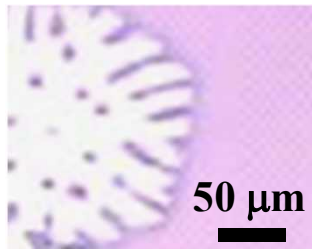


Fingering Instability

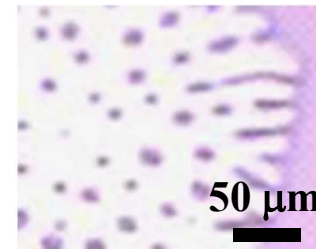
- Similar to patterns seen in Hele-Shaw flow where a lower viscosity fluid is forced into a region of higher viscosity fluid
- Fingers form and eventually break off into droplets through Rayleigh instabilities
- Other explanation is from dewetting of water on mica
 - due to viscosity the water collects in the rim at a thickness higher than the equilibrium thickness which is sensitive to longitudinal periodic fluctuations leading to finger creation



10 minutes



15 minutes



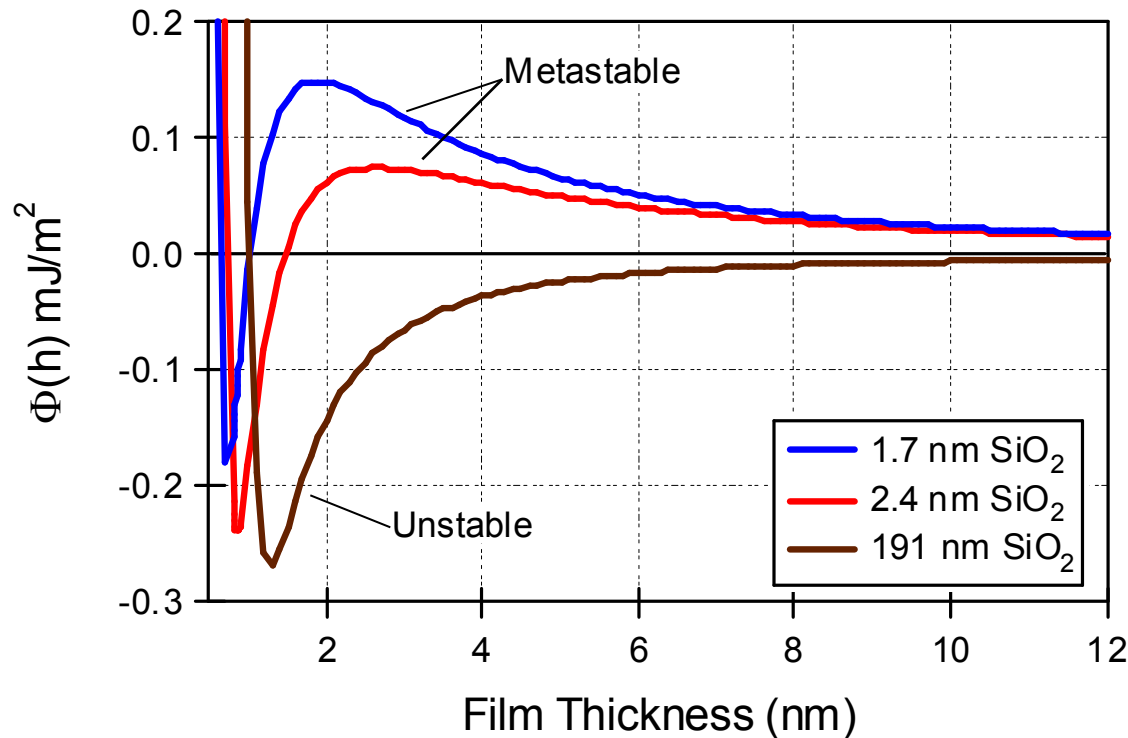
20 minutes

Interfacial Potential

$$\phi_{vdW}(h) = \frac{c}{h^8} - \frac{A_{SiO}}{12\pi h^2} + \frac{A_{SiO} - A_{Si}}{12\pi (h + d)^2}$$

$$A_{SiO} = 1.8(3)E^{-20} \text{ J}$$

$$A_{Si} = -2.2(5)E^{-20} \text{ J}$$



Surface Energy: Fullerenes vs. PSNPs

- Stronger forces due to the lower surface energy of the substrate
 - 2 nm fullerene layer not thick enough to retard forces
 - PSNPs are larger in diameter and it is possible to have more than a monolayer at the substrate

