



Model Validation of Experimental Hardware: Design versus Reality

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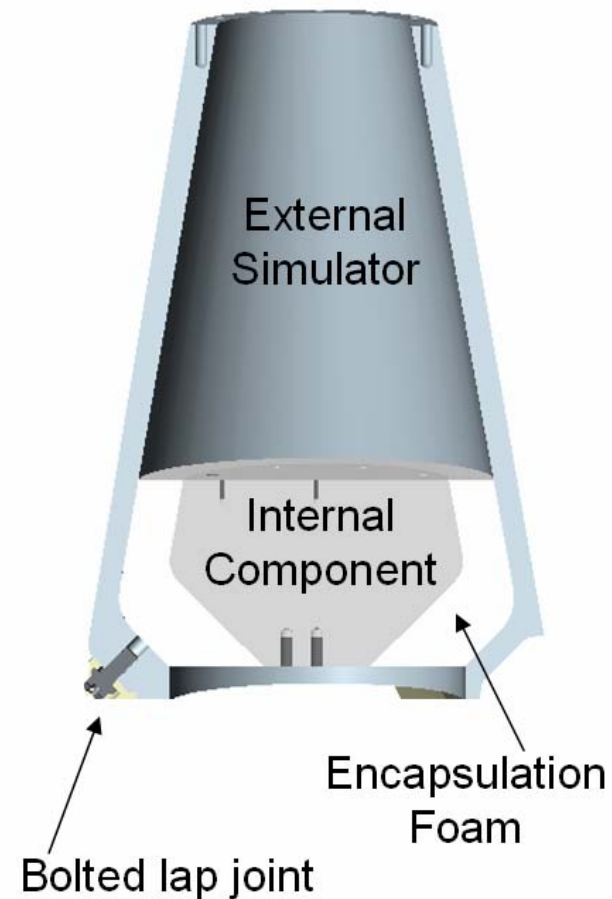




Introduction and Motivation

Model Validation Effort of Experimental Hardware

- Assess foam encapsulated components
- Bottom-up experimental approach
- Material → Subsystem validation levels
- Manufacturing process issues identified



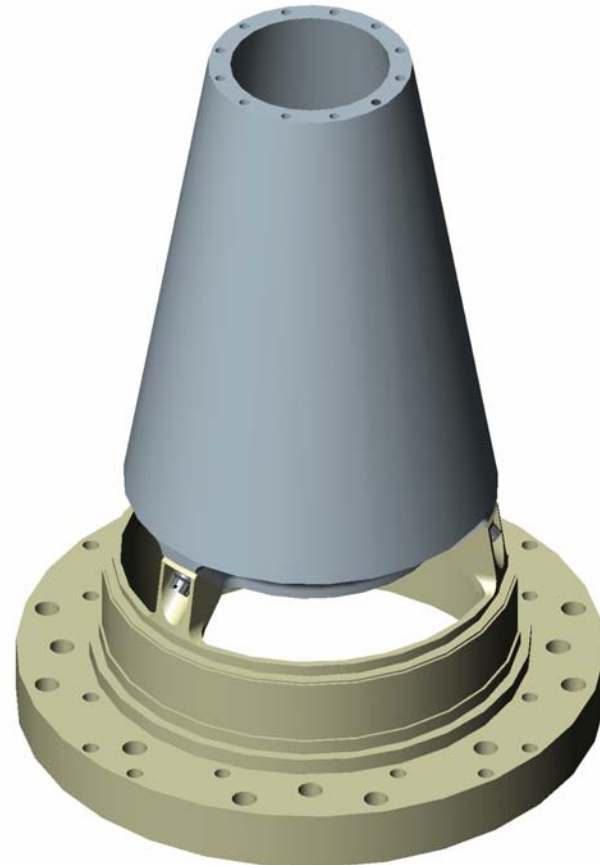


Introduction and Motivation

Model Development Considerations

- appropriate physics
- model form
- material parameters
- input loads
- boundary/loading conditions

Model Assumptions may be violated (reality $\neq$ design)





Introduction and Motivation

Formal Validation (triple-blind) Process

- **Experimentalist**
 - Collect validation data
 - No analytical model info
- **Analyst**
 - Develop FEA model
 - No experimental insight
- **Independent party**
 - Applied validation metrics

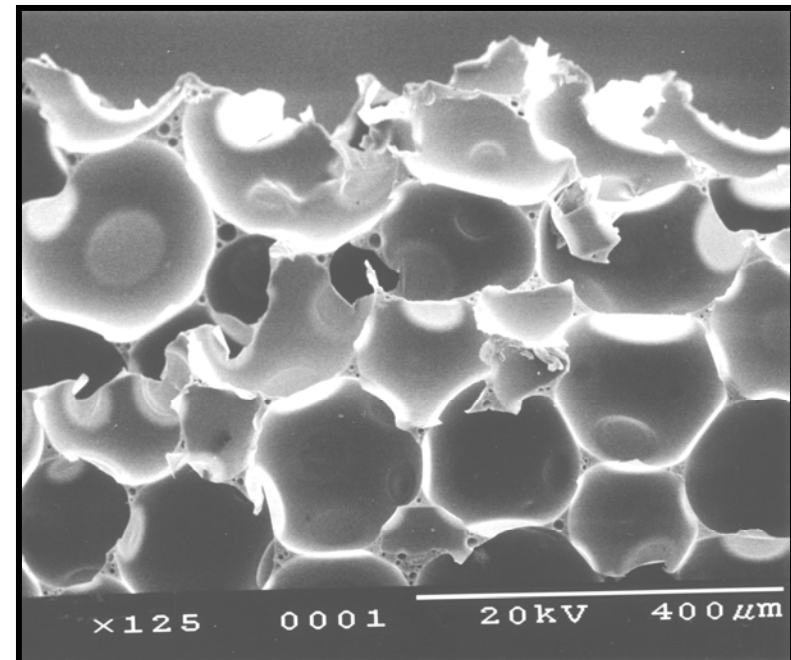




Introduction and Motivation

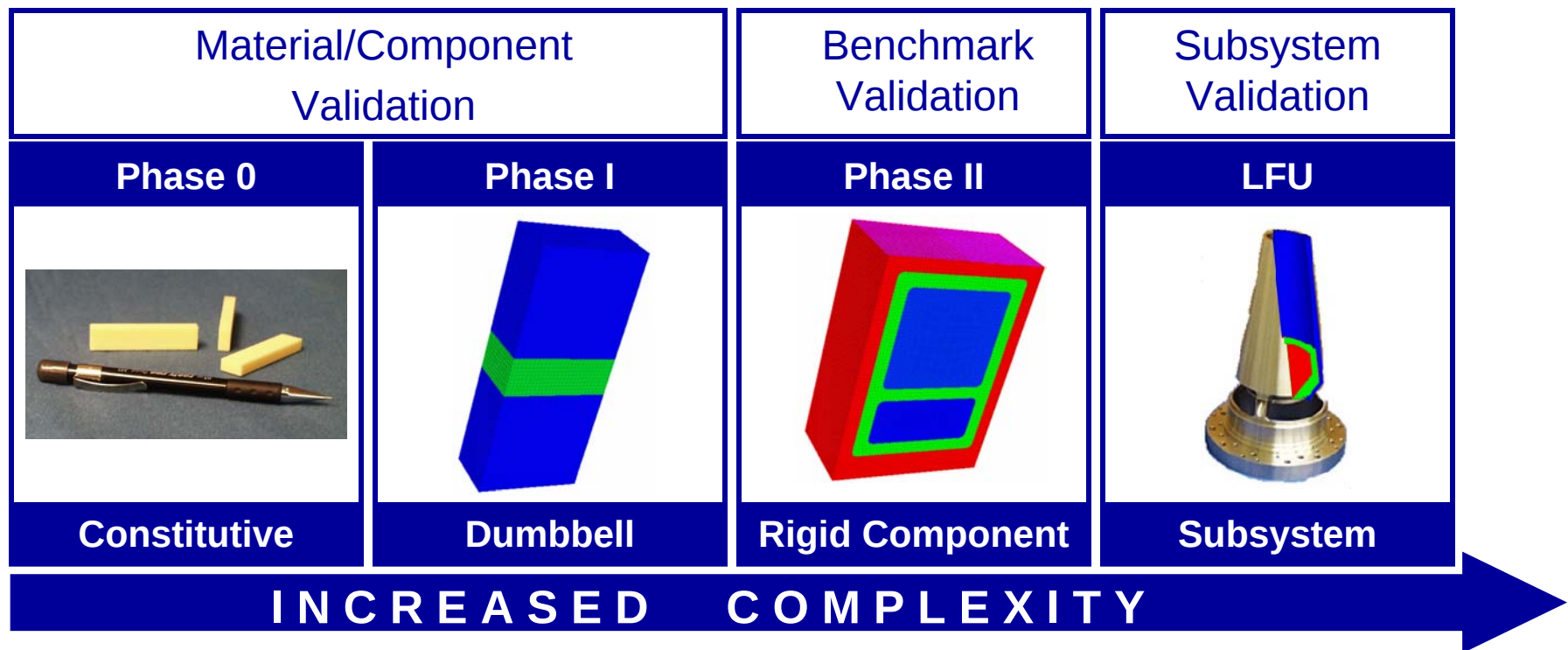
Foam Characteristics

- “rigid” epoxy foam
- closed-cell
- nominal density: 20 lb/ft³
- mitigate shock and vibration
- average cell diameter ~200 μm
- modeled as linear viscoelastic





Model Development/Validation Process

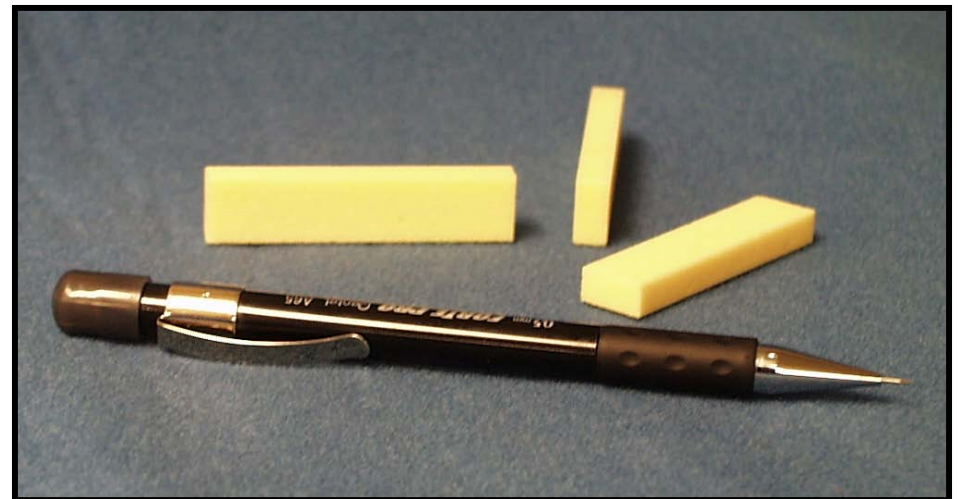
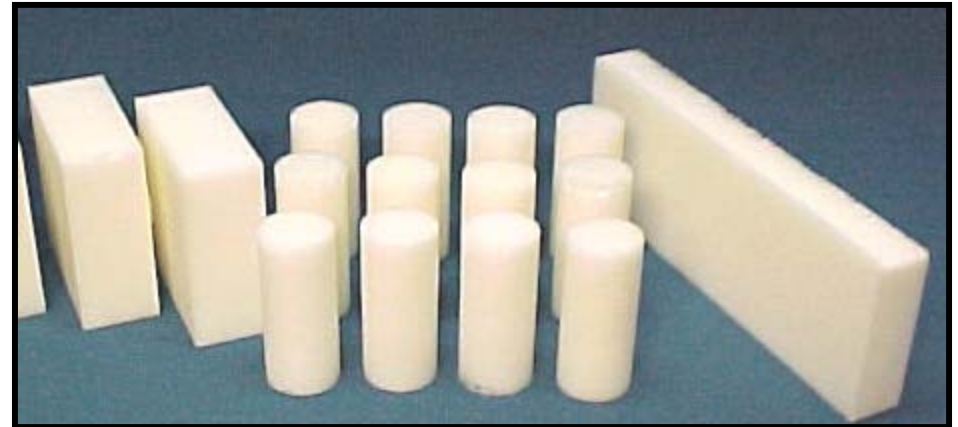




Material/Component Validation: Phase 0

Experimentally obtained material parameters

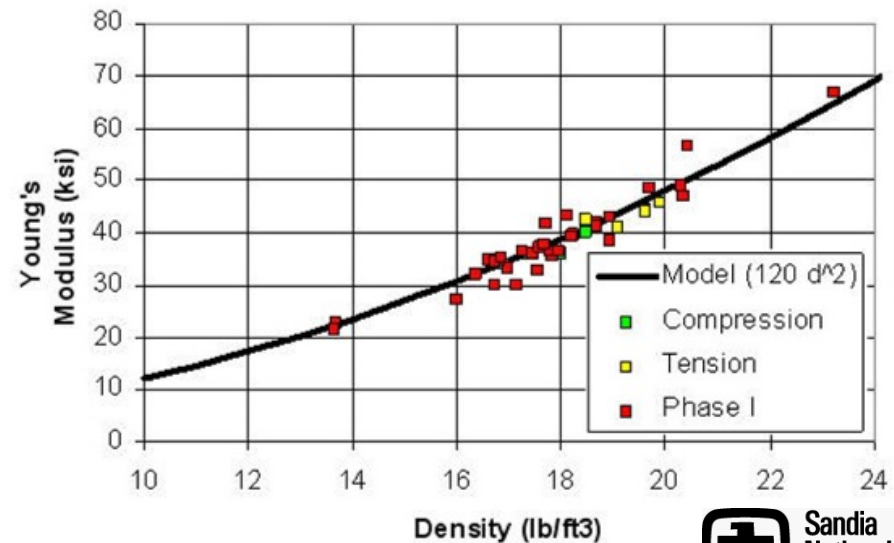
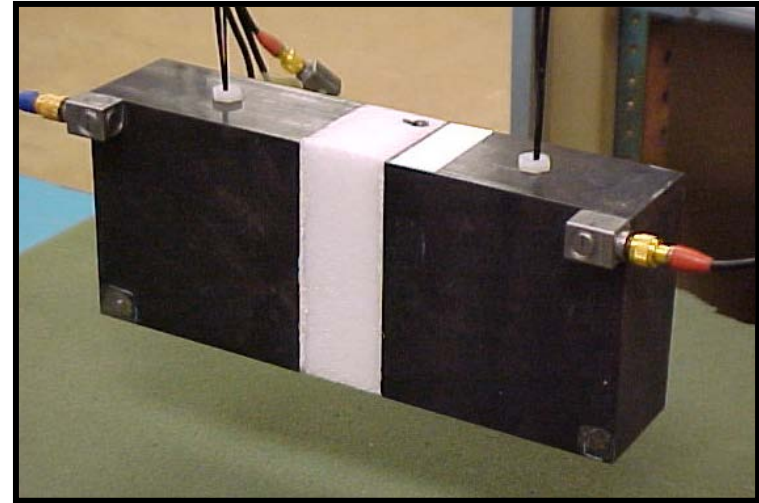
- Phase 0 geometry
- Quasi-static testing
 - tensile moduli
 - compressive moduli
- Temperature variation
 - glass transition (T_g)
 - rate dependence





Material/Component Validation: Phase I

- Linear viscoelastic model
- Phase I geometry
 - Modal analysis
 - Shaker vibration
 - Geometry variations
- Data used for both correlation and validation
- Model dependent upon density/gradient of foam
- Experimental E , ρ , $\zeta \rightarrow$ Probabilistic model





Benchmark Validation: Phase II

Phase II Geometry

- encapsulation foam
- outer aluminum mass
- stainless steel rigid interior masses
- natural adhesion of foam secured masses





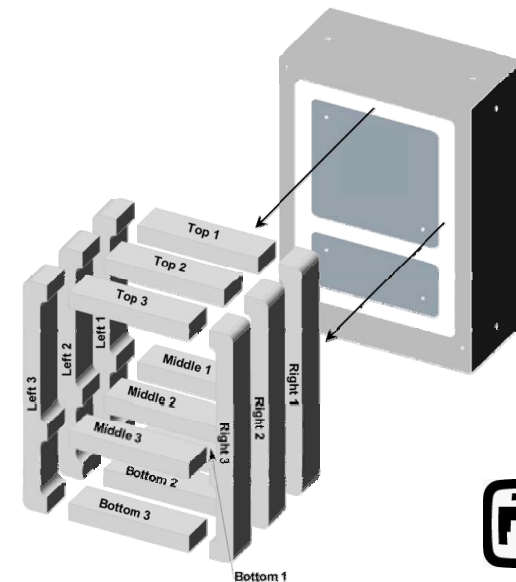
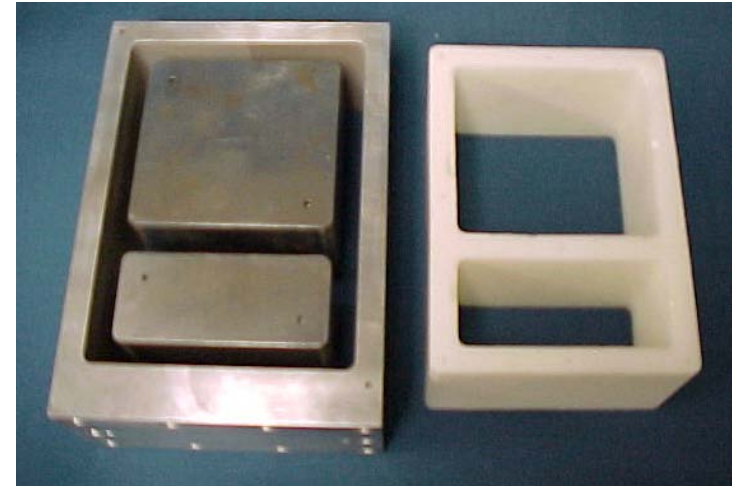
Benchmark Validation: Foam Development Study

Define foaming process

- Minimize density variation
- Preheating
- Curing temp/time

**Quantify average density
and density gradient**

- Mold release applied
- Density gradient observed
along foam rise direction
- Average density = 20.2 lb/ft^3
(desired = 20 lb/ft^3)

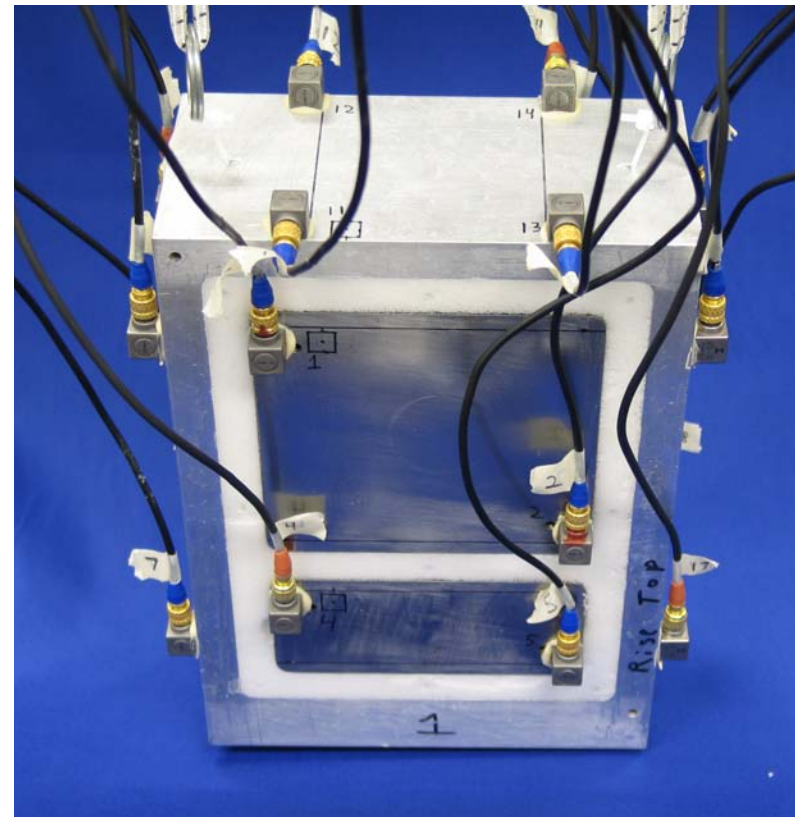




Benchmark Validation: Model Validation Data

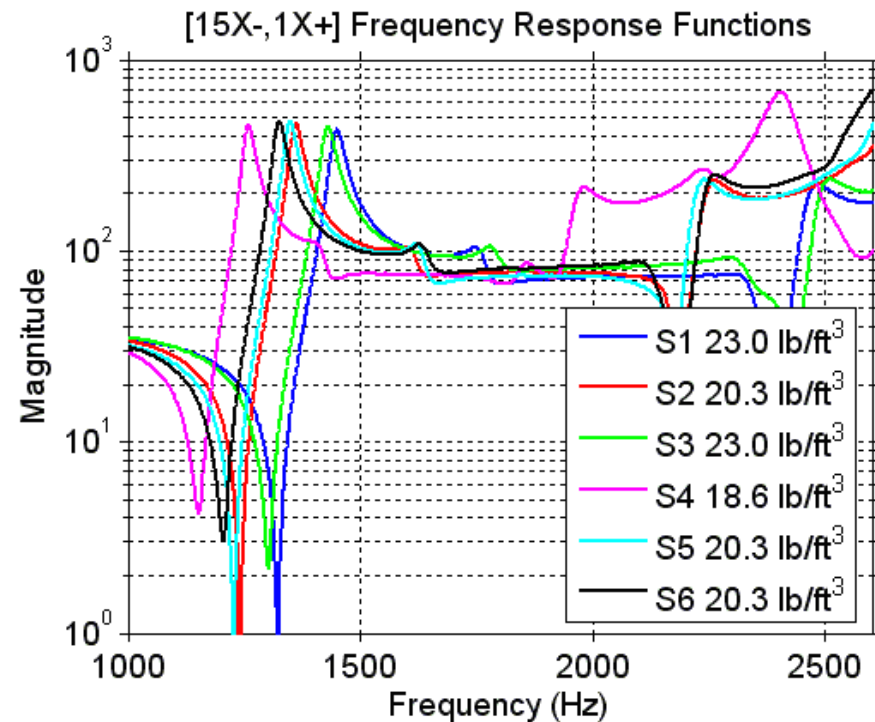
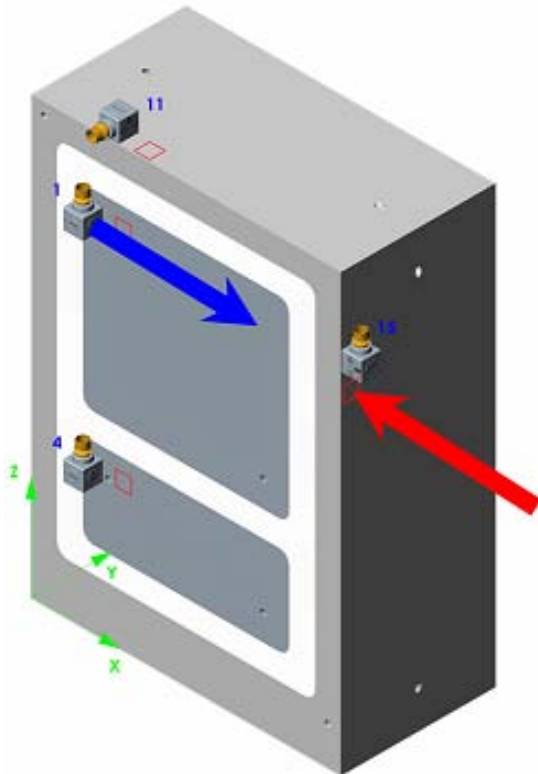
**Validation samples
created from studied
foaming procedure**

- Free-free modal
- Base-driven shaker
- Boundary conditions
- Input location effects
- Repeatability tests
- Mass loading effects examined





Benchmark Validation: Model Validation Data

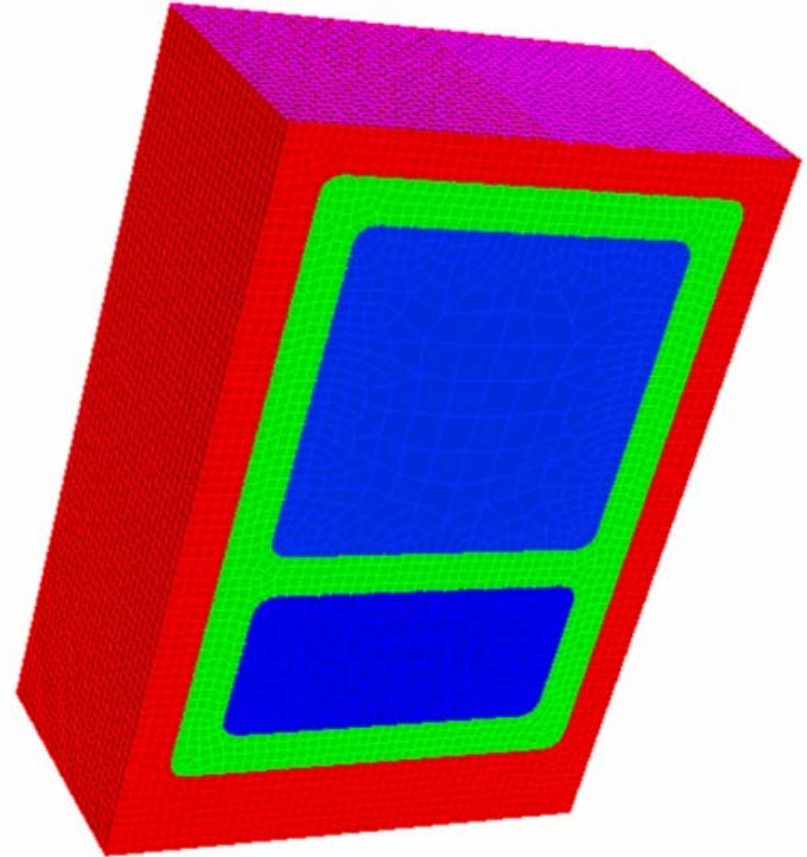


**FRF displays similar general response,
variations due to density variation**



Benchmark Validation: Model Validation

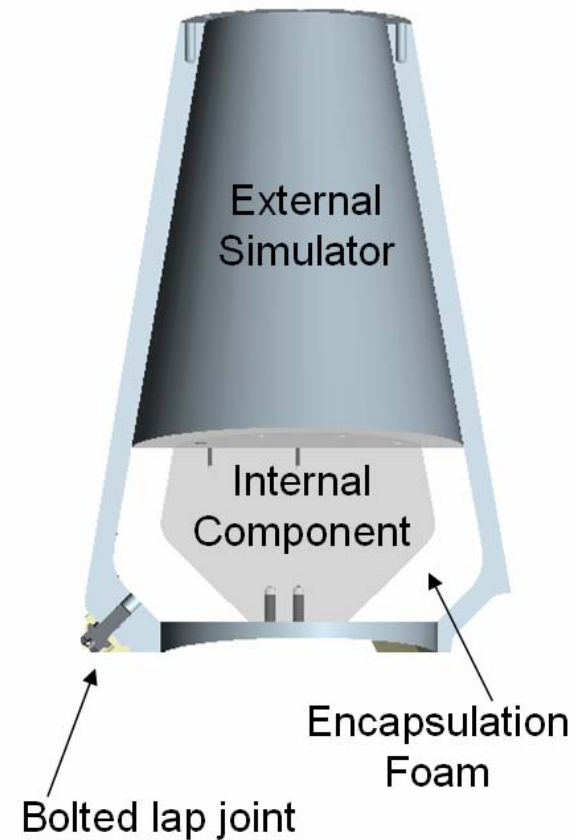
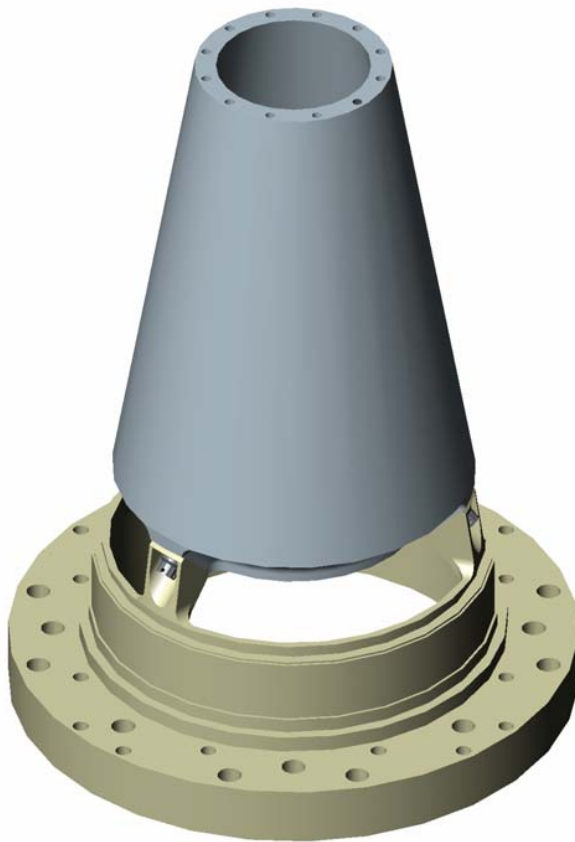
- Two separate model validation assessments
 - Free-free modal and analytical data
 - FRF-based windowed metric applied
 - 80% of predictions must contain experimental results
 - Shaker time-domain vibration data
- Model validated



Angel Urbina, Thomas L. Paez, Brian Rutherford, Chris O’Gorman, Terry Hinnerichs and Patrick Hunter, "**Validation of Mathematical Models: An Overview of the Process**", 2005 SEM Annual Conference, June 2005.



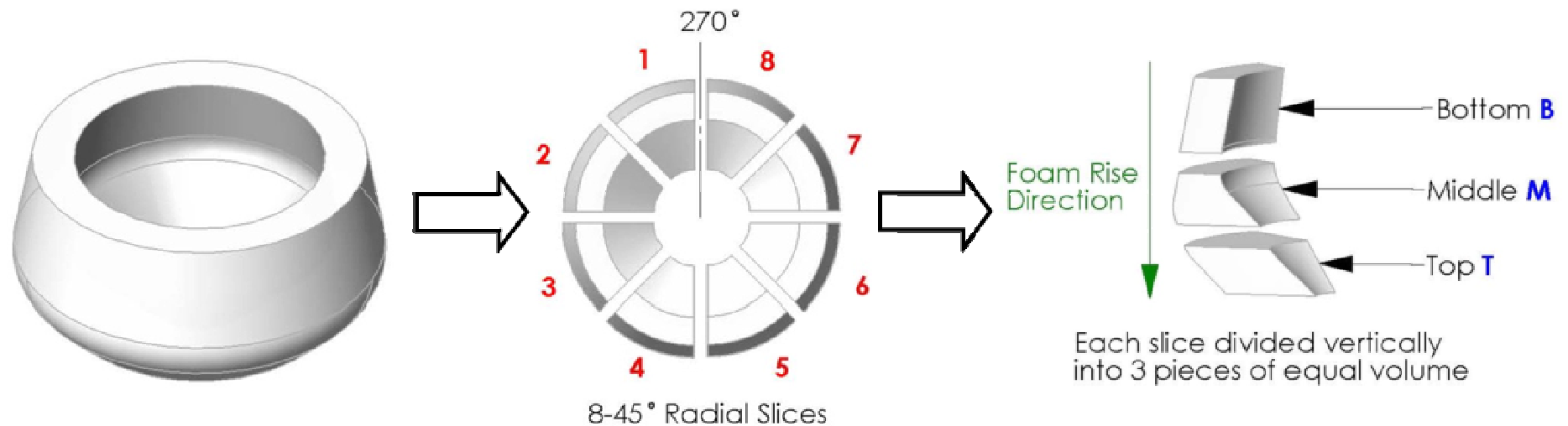
Low Fidelity Unit (LFU) Subsystem Validation



Merges two development efforts: foam & joint model



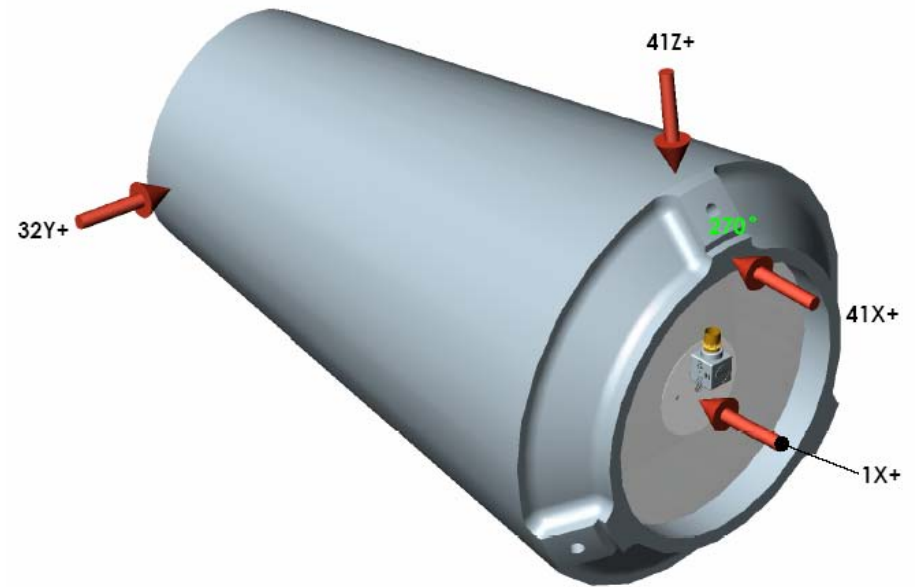
LFU Validation: Foam Development Study



Repeat density and gradient quantification:
Average density 21 lb/ft³, 19% gradient between sections



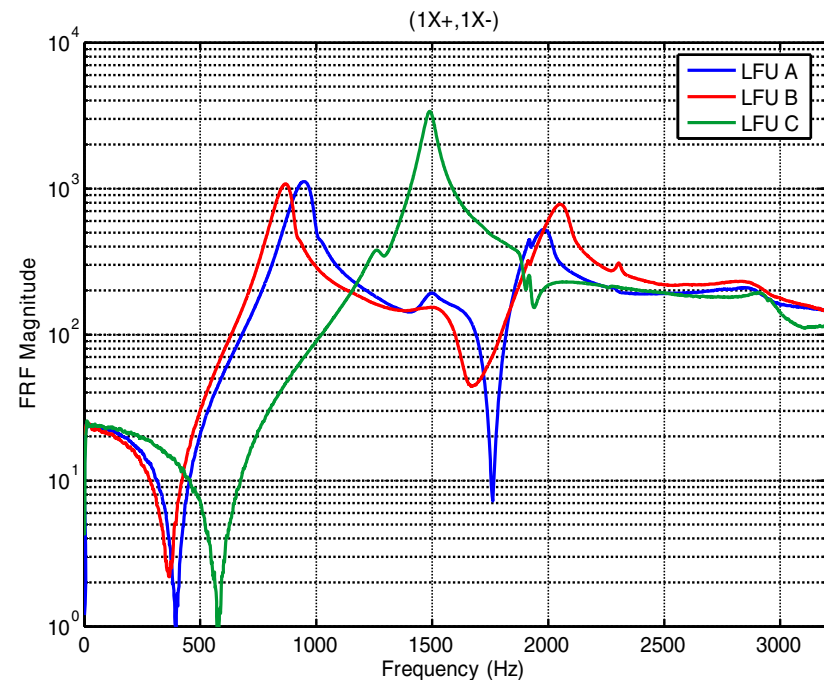
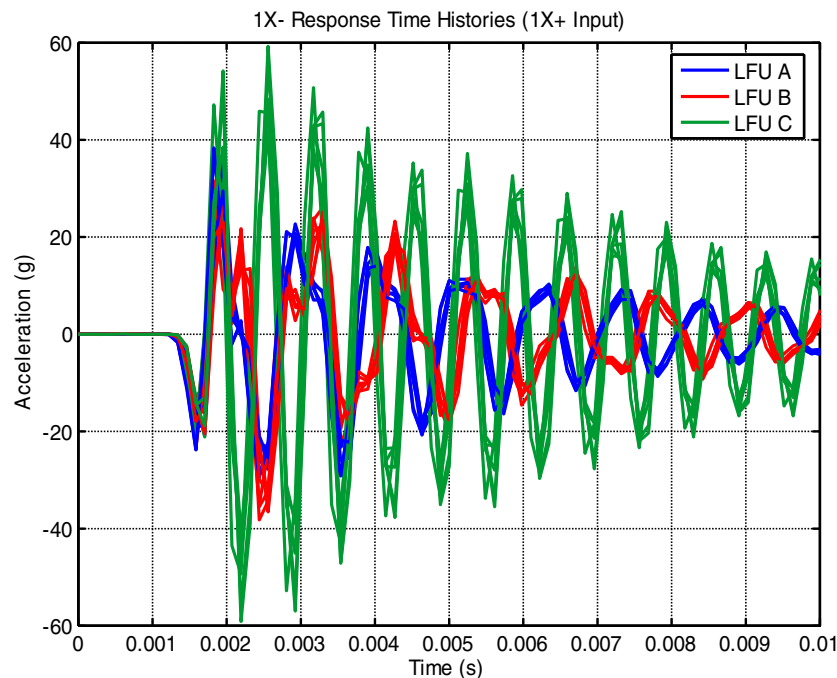
LFU Validation: Model Validation Data



**Free-free modal test:
internal & external, orthogonal input**



LFU Validation: Model Validation Data

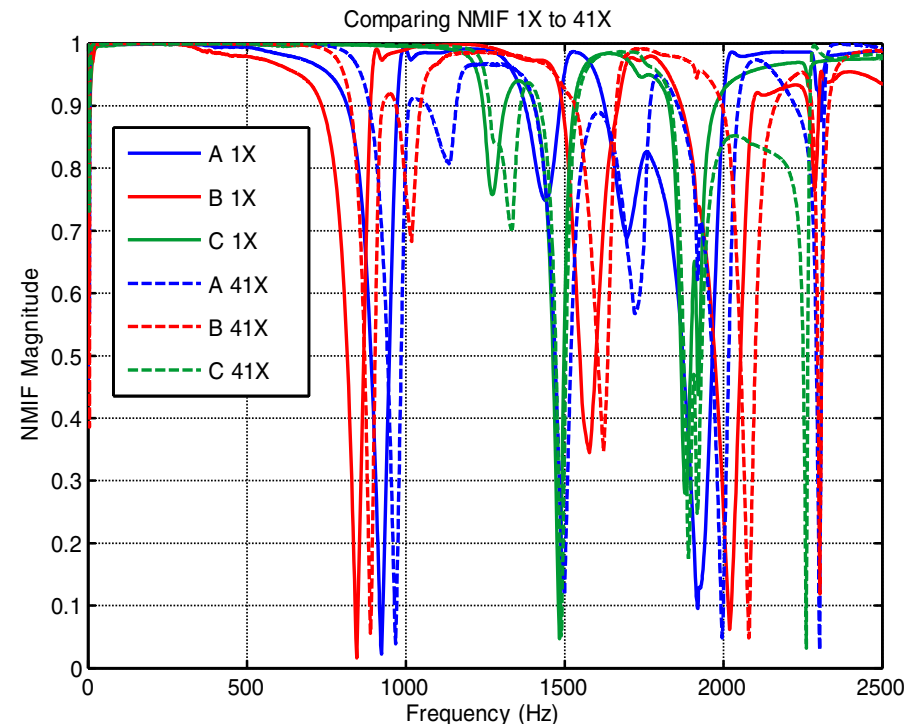


Time History & FRF: results differed between samples, nonlinearities present, inconsistent with Phase II repeatability



LFU Validation: Model Validation Data

- Normal Mode Indicator Function Calculated
 - Shift of A,B: indicates nonlinearity present
- Mode Shapes Calculated
 - A,B axial mode w/rocking
 - C more axial
- Force/Displacement measured for sample C
 - effective (B.O.E.) stiffness > experimental stiffness
- Density variation does not account for frequency shift



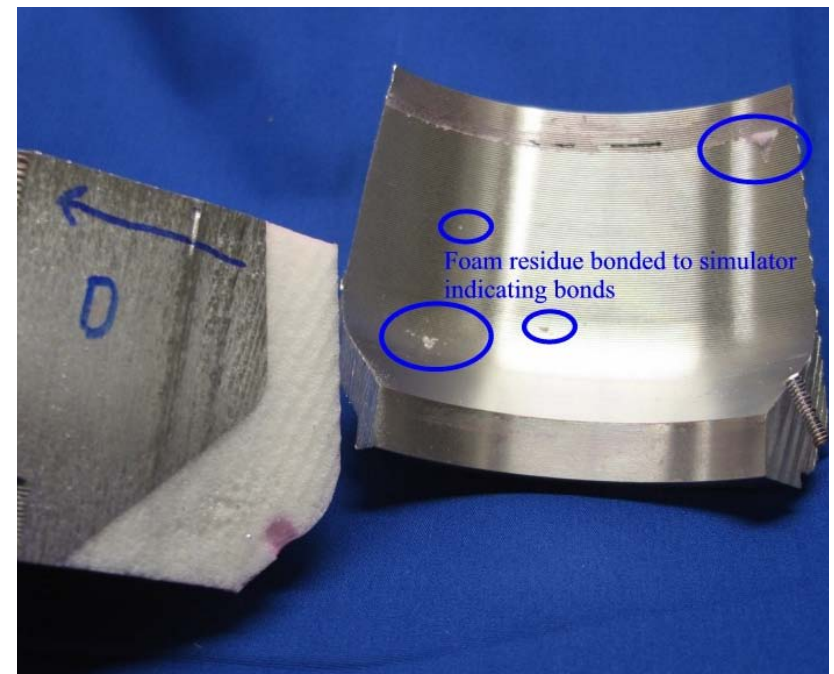
Solid – internal mass input

Dashed – external mass input



LFU Validation: Diagnostic Testing

- Two possible causes of behavior
 - Density variation
 - Interface bonding
- Diagnostic tests performed
 - NDE test, no results
 - Destructive test→
very little bonding observed
- Lack of bonding cause of soft, non-linear behavior





LFU Validation: New Samples

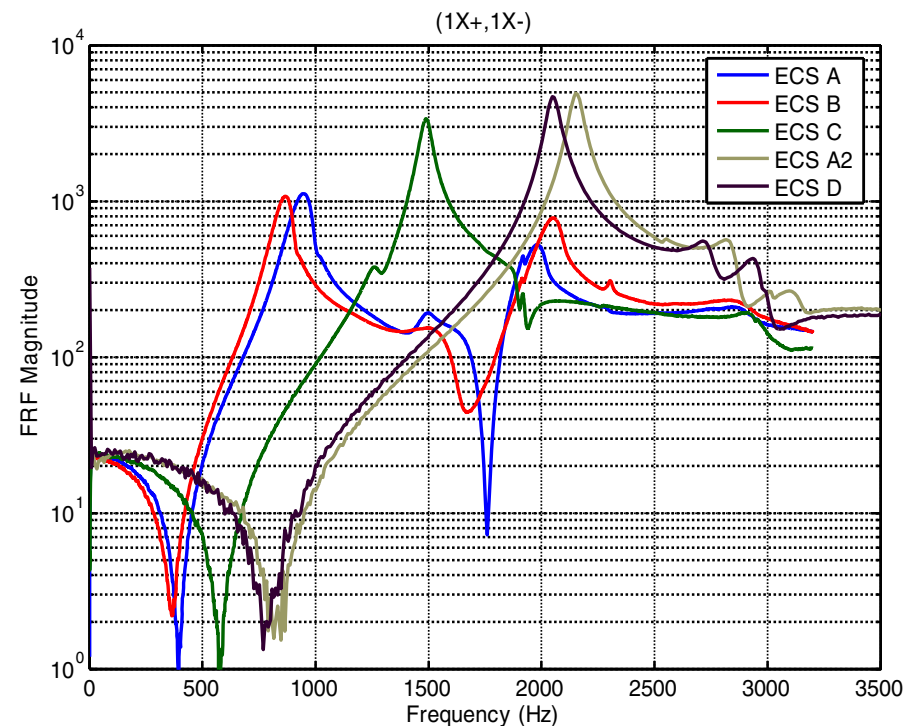
- LFU Foaming process reviewed
- Pre-foaming process included both grit blasting and Brulin®
- Two new validation samples created
- Parallel effort initiated to characterize non-bonding
- Time constraints required success-driven approach





LFU Validation: Model Valid. Data (revisited)

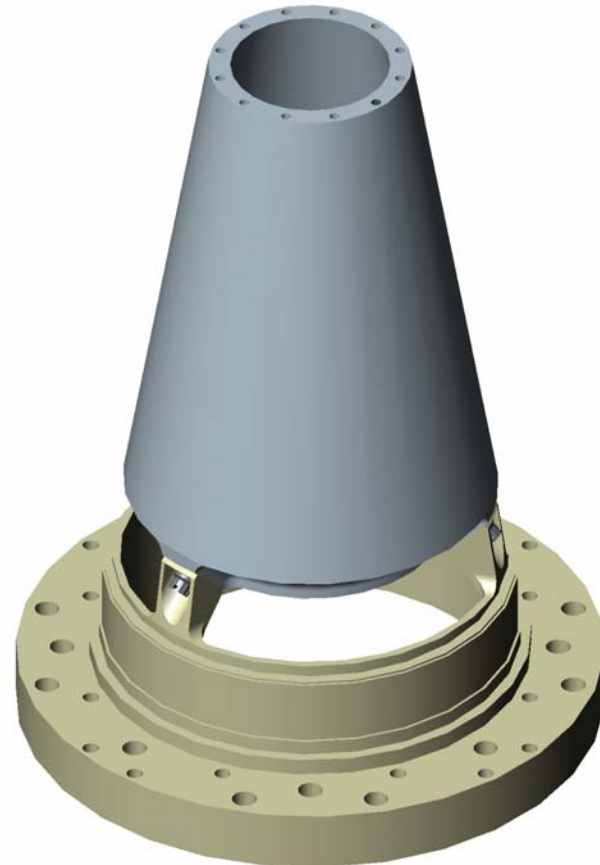
- Free-free modal test repeated
- FRF results for A2, D
 - more linear
 - increased stiffness
 - closer model agreement
- Pure axial motion mode shapes
- Complete set of data collected for validation





LFU Validation: Model Validation

- Validation metrics applied to experimental data
 - harmonic wavelet transform of impulse response function
 - windowed measure of FRF
 - SRS measure
- Validation agreed on 2/3
- Agreement information defines adequacy of model
- Details will be documented in future paper





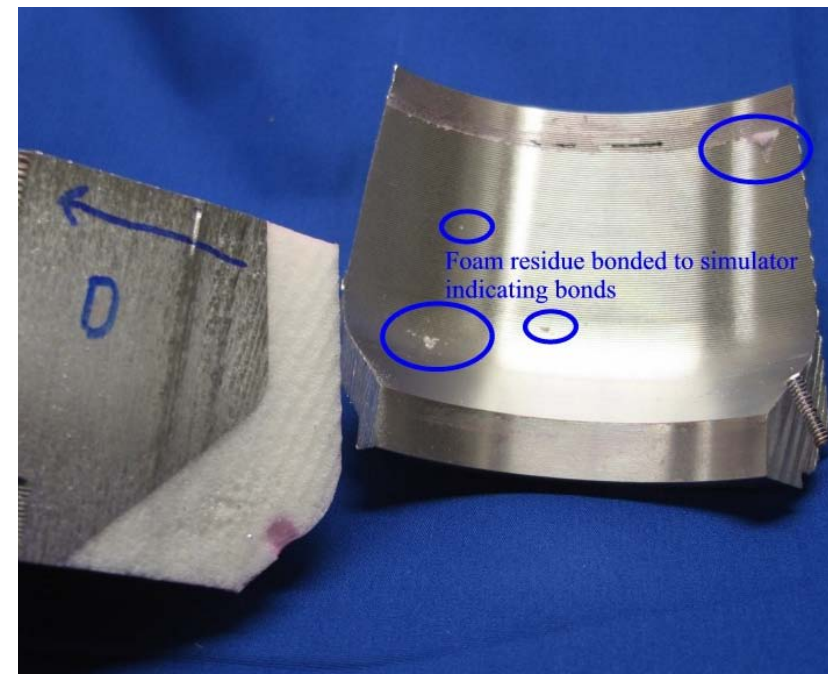
Summary

- **An FEA model of Experimental Hardware was developed, incorporating encapsulated components in a linear viscoelastic foam**
- **Validation performed at Material → Subsystem levels**
- **Inconsistent, non-linear behavior in subsystem tests resulted in a new foaming procedure with better results**
- **Triple-blind validation process was based on a series of foam/structure experiments with increasing complexity**
- **Acceptance information helps define the adequacy of the model for the intended application**



Summary: Lessons Learned

- Fully consider modeling assumptions
- Reassess at each level in validation process
- Previous experience indicated bonding would not be an issue
- Unclear why bonding did not occur in LFU
- Further investigation is being conducted



Model Assumptions may be violated (reality $\neq$ design)