

Contaminant Mixing at Pipe Joints: Comparison Between Laboratory Flow Experiments and Computational Fluid Dynamics Models

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Overview

- **Introduction**
- **Experimental Approach**
- **Modeling Approach**
- **Results**
- **Conclusions**

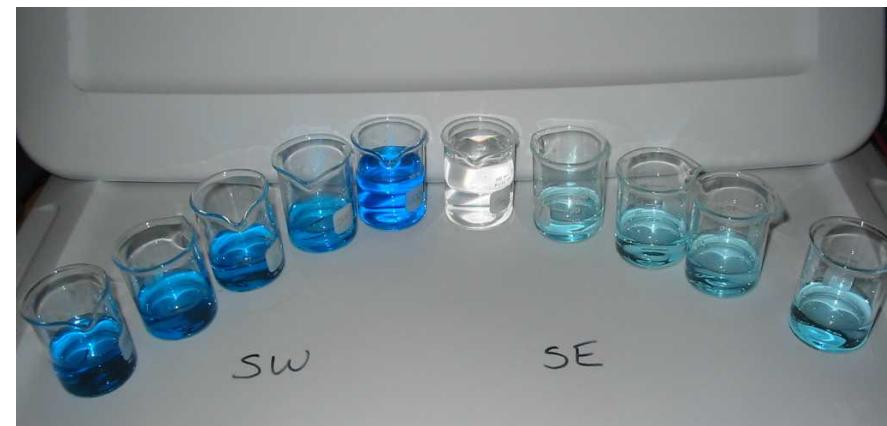
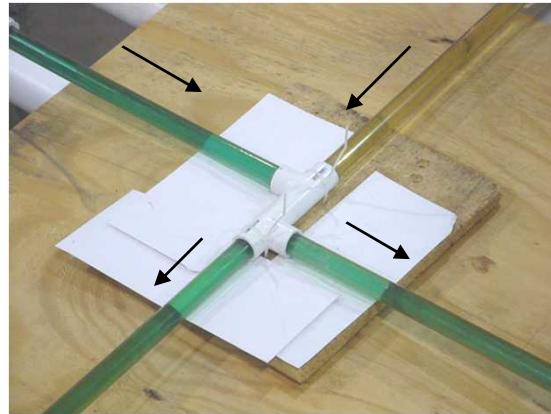


Introduction

- **Contaminant transport in water-distribution pipe networks is a growing concern**
 - Need to understand and predict contaminant movement
- **Need to understand how contaminants mix at pipe junctions**
 - Water quality
 - Interpretation of monitoring data
 - Mitigation of contamination events

Problem Statement

- Many water distribution models (e.g., EPANET) assume complete mixing at pipe junctions
- Flow in actual pipe joints yields incomplete mixing
 - Orear et al., 2005
 - van Bloemen Waanders et al., 2005

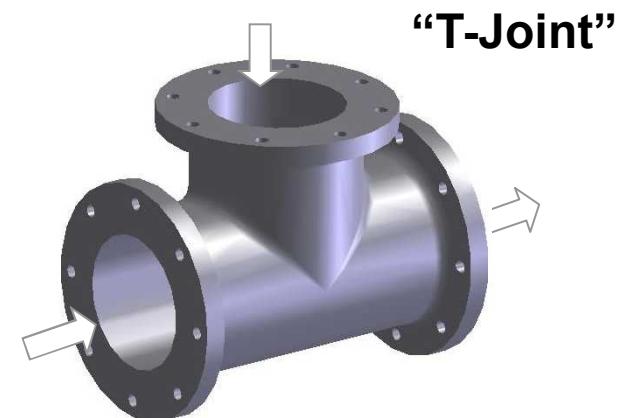
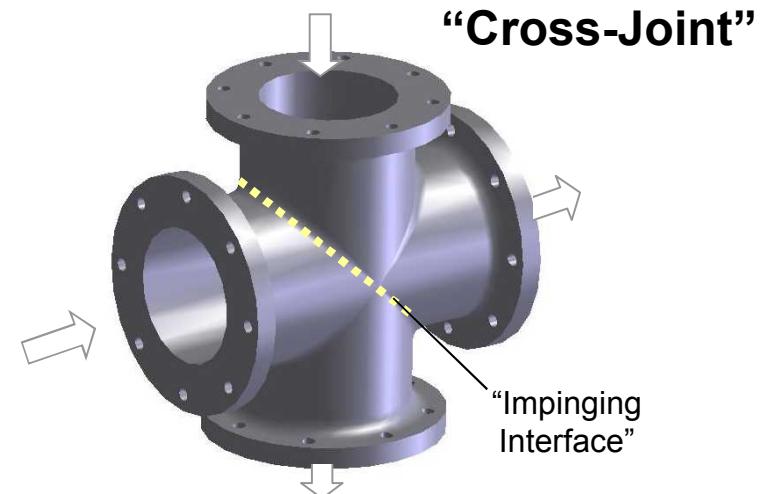


from Orear et al. (2005)



Objectives

- Conduct physical and numerical simulations of contaminant transport in pipe joints
- Understand impact of parameters and processes on mixing behavior
 - Different flow rates
 - Effective mass transfer at impinging interface
- Validate and calibrate models with data from single and multi-joint pipe configurations

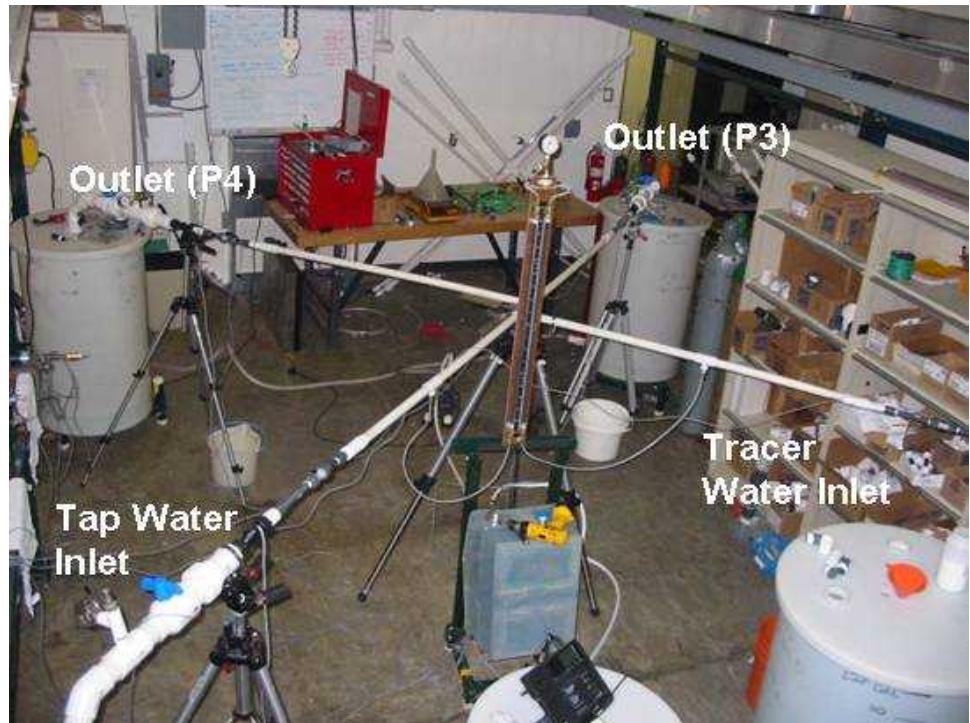
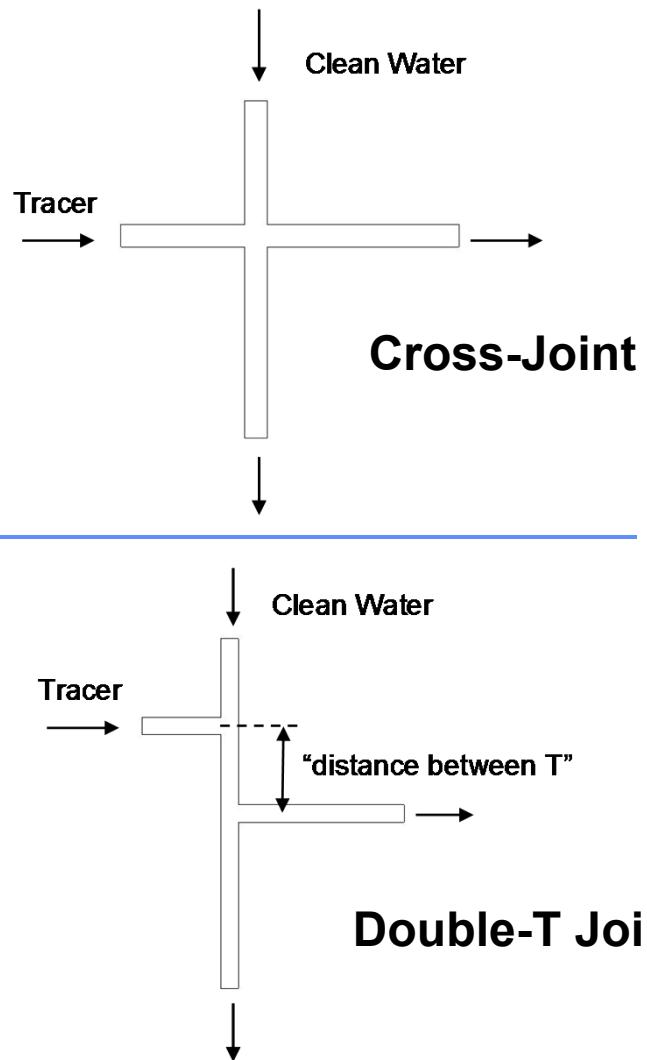




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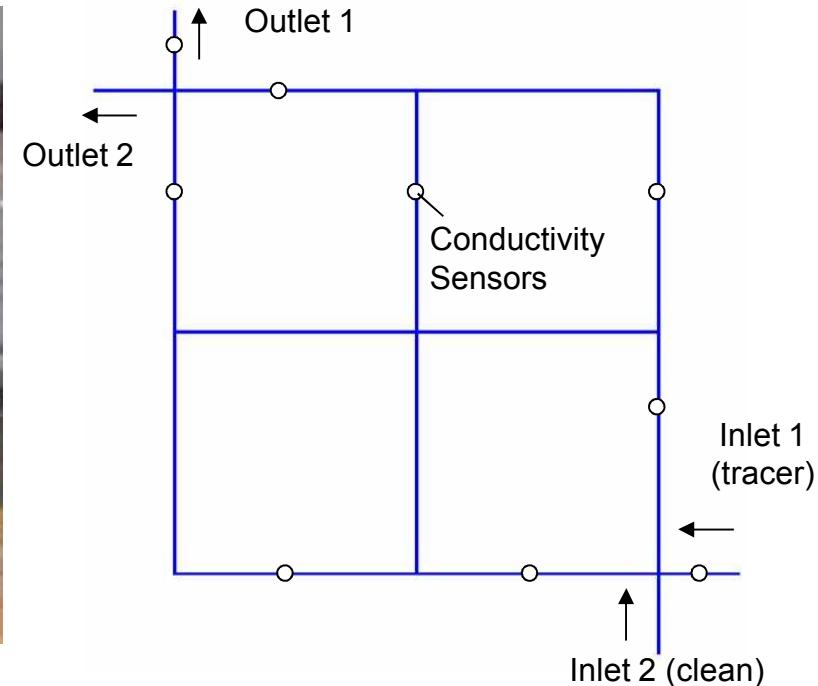
Single-Joint Tests



- Tracer consists of NaCl solution
- Tracer monitored continuously by electrical conductivity sensors
- Flow rate in each pipe was controlled
- Pipe diameters: 0.5", 1", 2"



Multi-Joint Tests (Small-Scale Network)



- 3x3 array of cross joints with 3-foot pipe lengths
- Flow rates at inlets and outlets controlled
- Pipe diameter: 0.5"

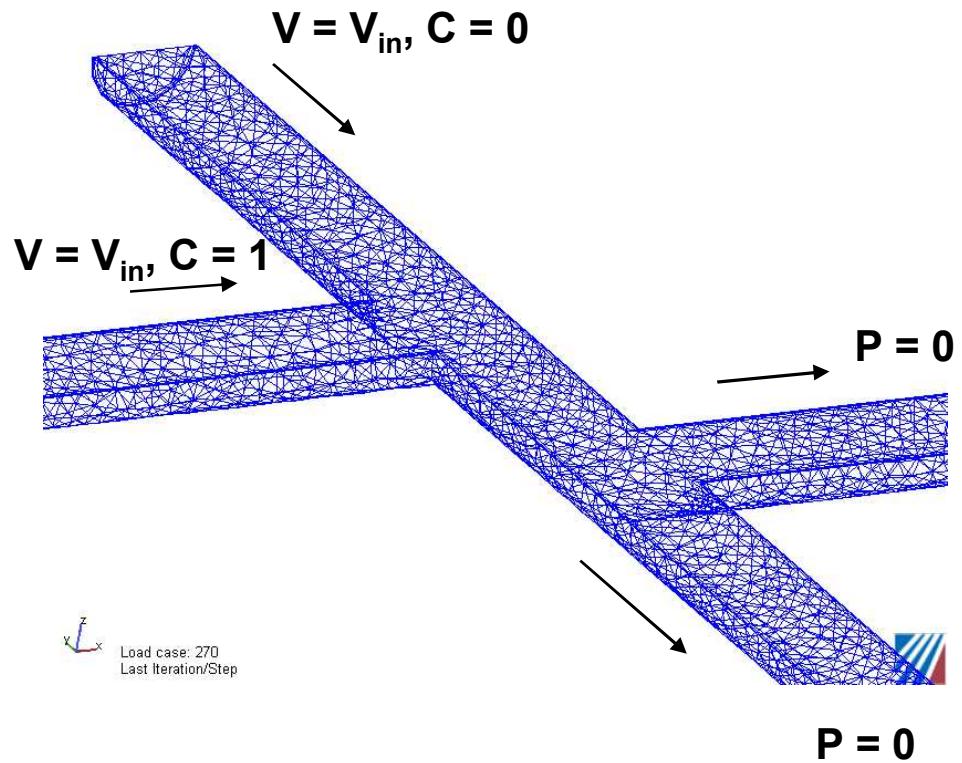


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Modeling Approach

- Finite-element computational fluid dynamics simulations (CFdesign®)
 - Mesh refinement: 50,000 to >1M elements
- K- ϵ turbulence model
 - Ran turbulent flow to convergence first
- Tracer simulation with normalized scalar concentration
 - Scalar diffusivity varied
 - $D = \text{eddy diffusivity} = \text{eddy viscosity}/Sc$
 - Turbulent Schmidt number, Sc , varied from 0.001 to 1.0





Single-Joint Simulations

All inlet and outlet flows approximately equal

Junction Configuration	Pipe Diameter	Reynolds Number	Velocity Boundary Conditions (V)	Turbulent Schmidt Number

*Experiments were run for this configuration



Multi-Joint Simulations

- Two simulations
 - Tracer inlet flow > clean-water inlet flow
 - Tracer inlet flow < clean-water inlet flow

Boundary Conditions				Reynolds Number	Turbulent Schmidt Number
Tracer Inlet Flow (Q_{tracer})	Clean Water Inlet Flow (Q_{clean})	Outlet 1 Flow ($Q_{out,1}$)	Outlet 2 Flow ($Q_{out,2}$)		
38 mL/s* (0.61 gpm)	31 mL/s (0.49 gpm) ($P = 0$ gage used as B.C.)	33 mL/s (0.52 gpm)	37 mL/s (0.58 gpm)	4,000 – 9,000	0.01, 0.001
28 mL/s** (0.44 gpm) ($P = 0$ gage used as B.C.)	50 mL/s (0.79 gpm)	32 mL/s (0.50 gpm)	46 mL/s (0.73 gpm)	7,000 – 11,000	0.01, 0.001

*Test period from 19-20 minutes in Orear et al. (2005)

**Test period from 8-9 minutes in Orear et al. (2005)

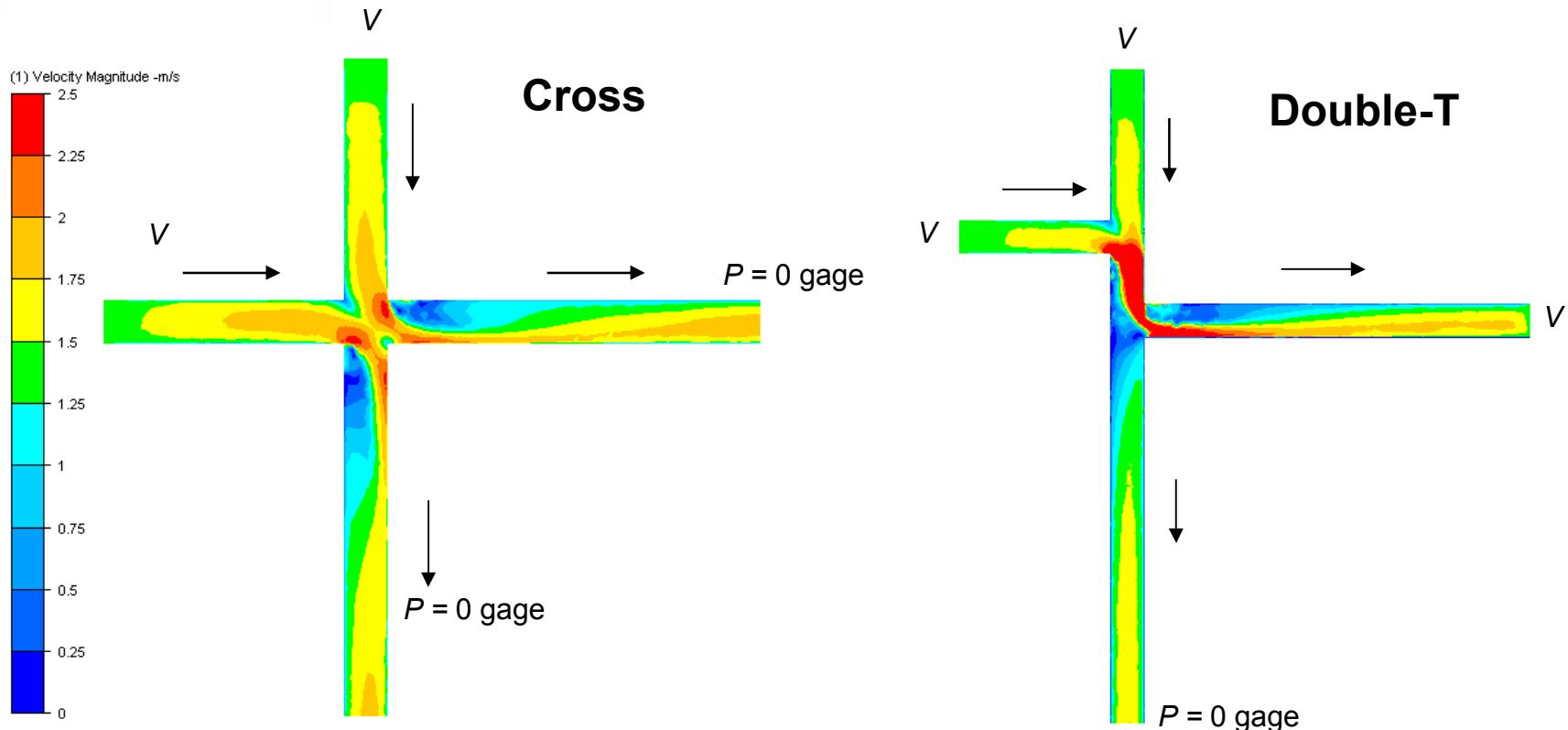


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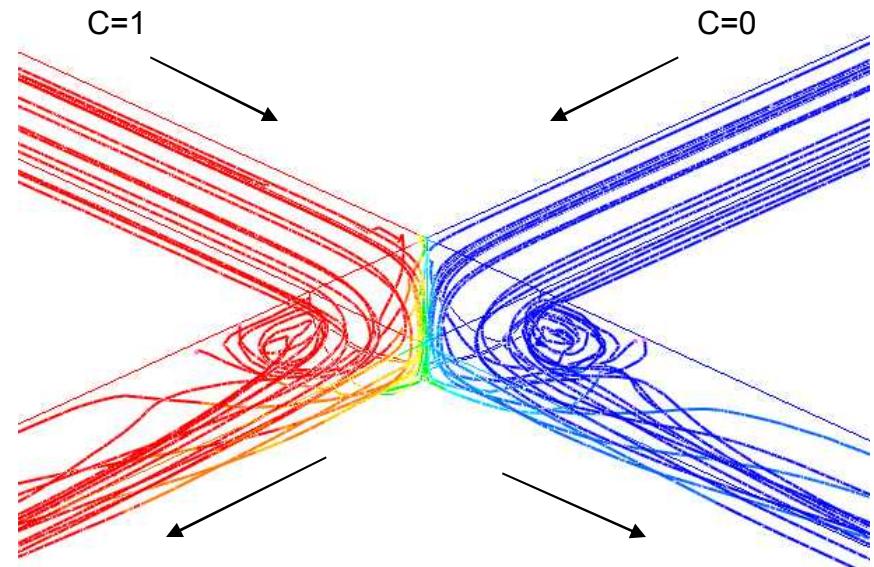
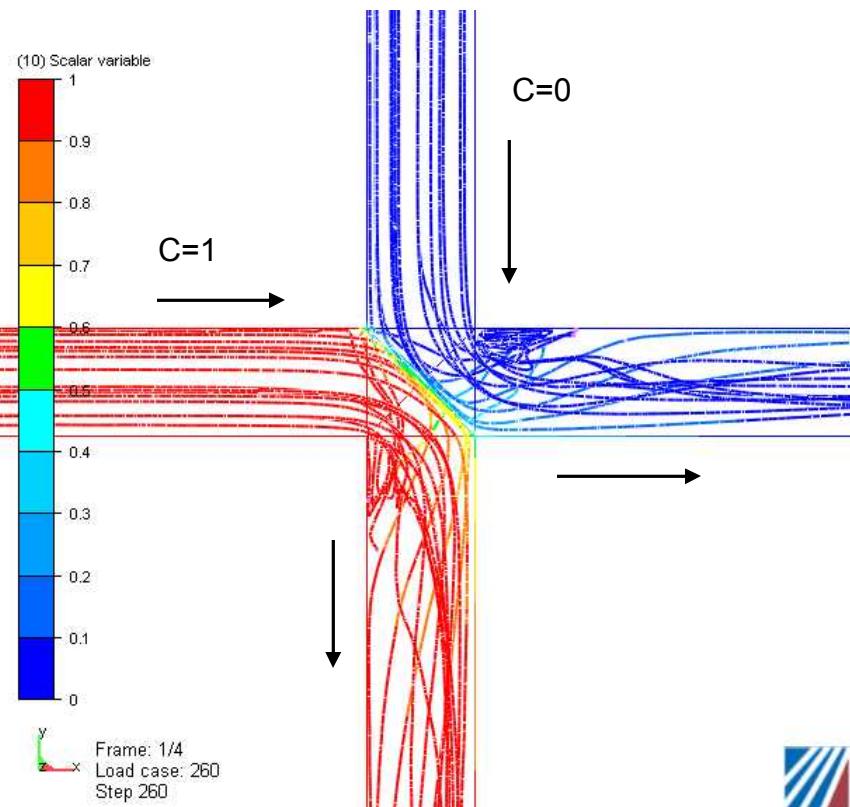
Simulated Velocity Profiles



- **Diameter: 0.5"**
- **Re = 20,000**
- **Spacing between double-T joints is 2.5 diameters**

Simulated Mixing

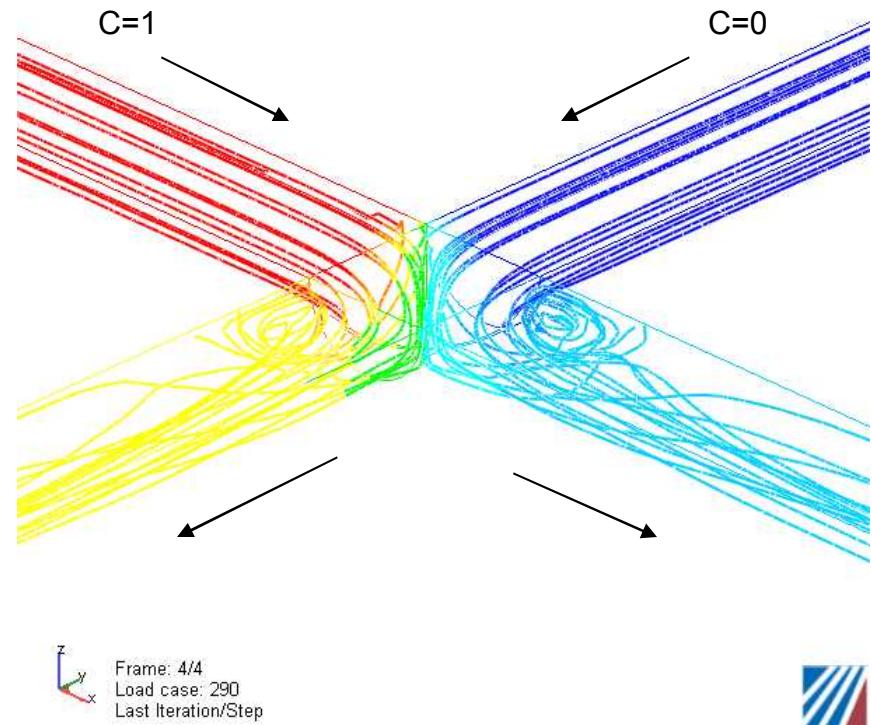
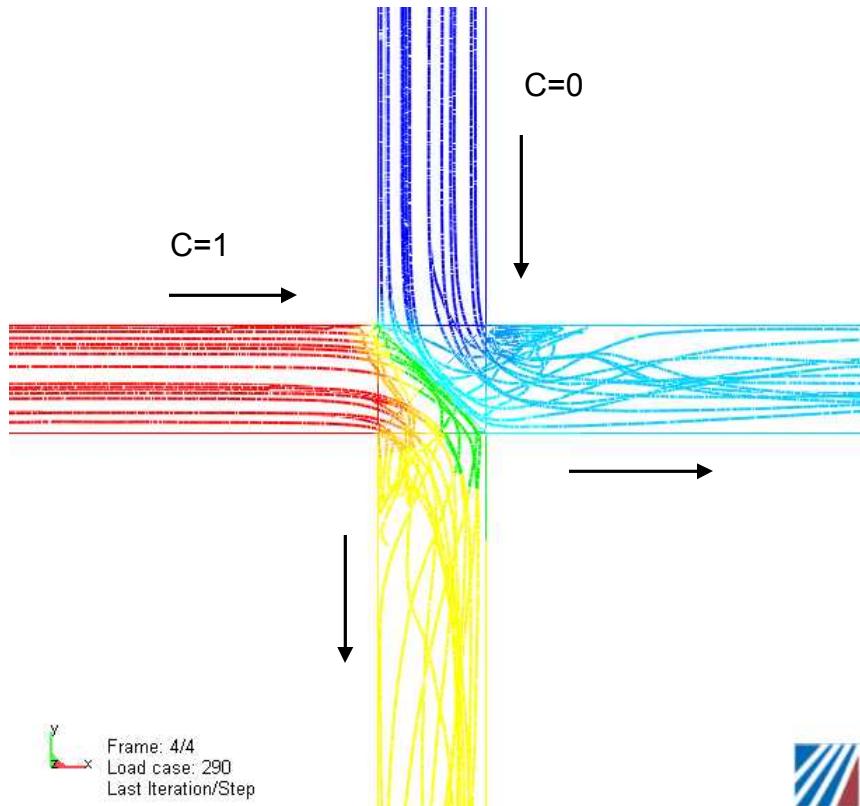
0.5" Cross Joint, $Re = 10K$, $Sc = 1$



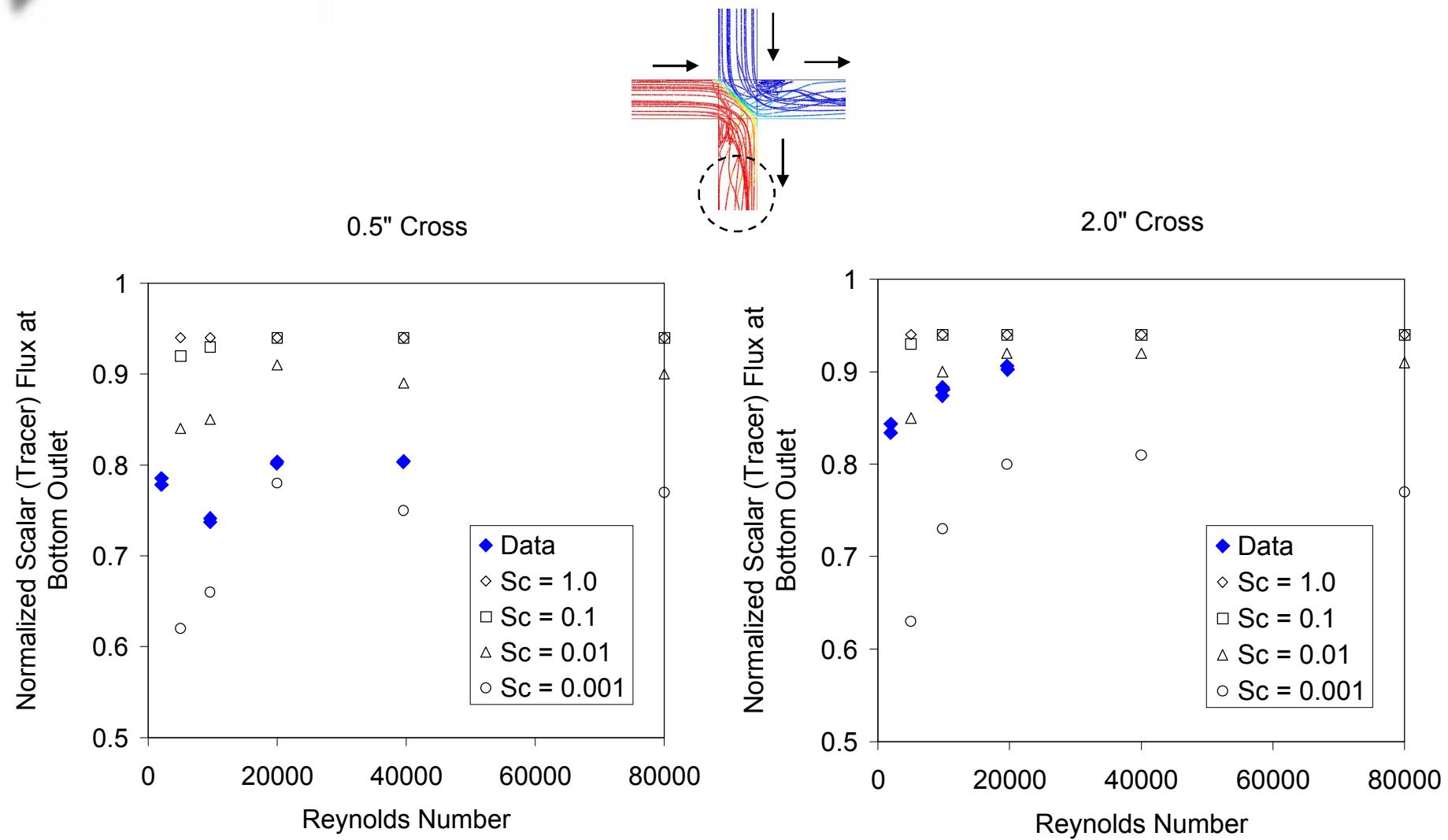


Simulated Mixing

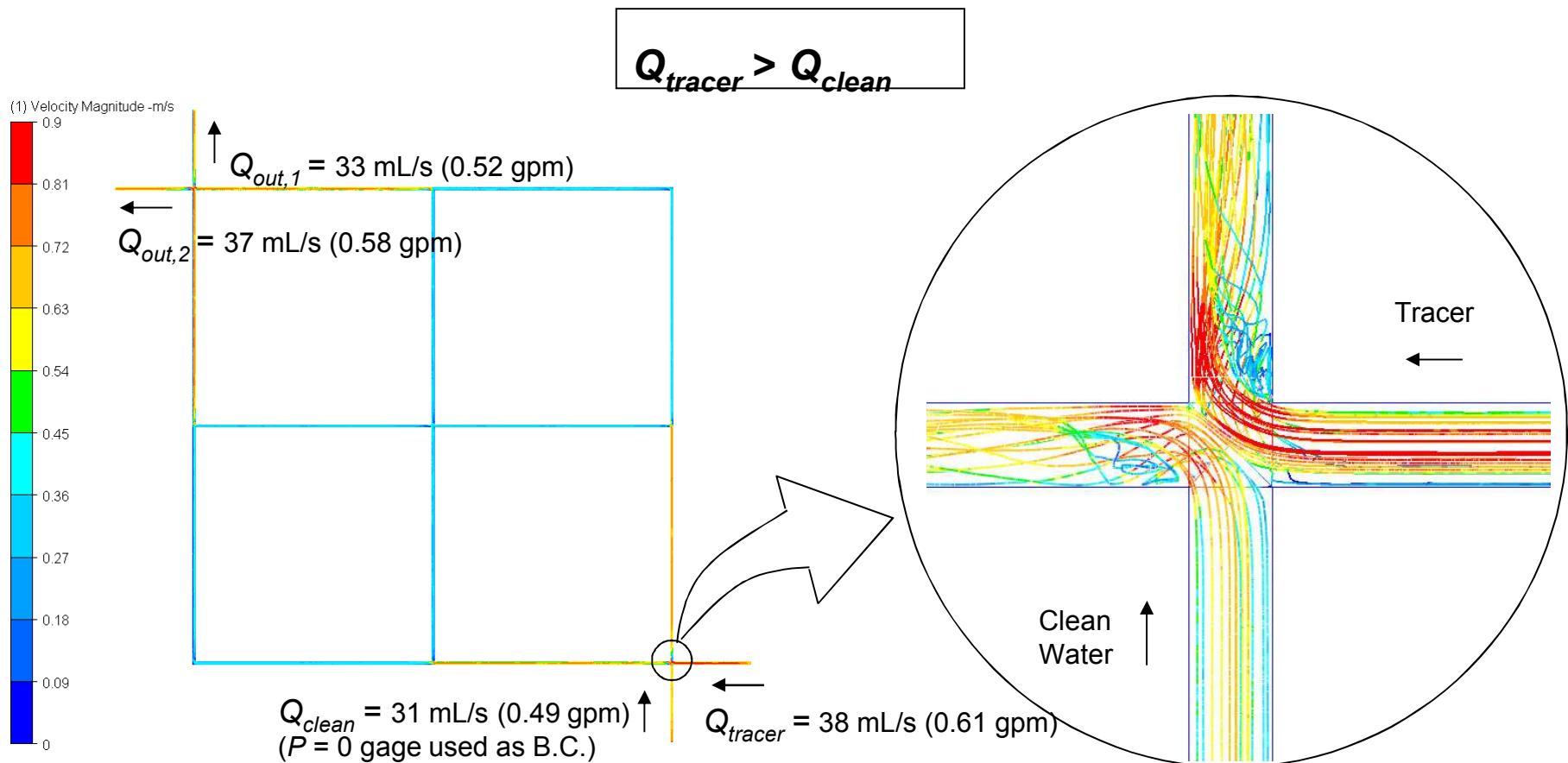
0.5" Cross Joint, $Re = 10K$, $Sc = 0.001$



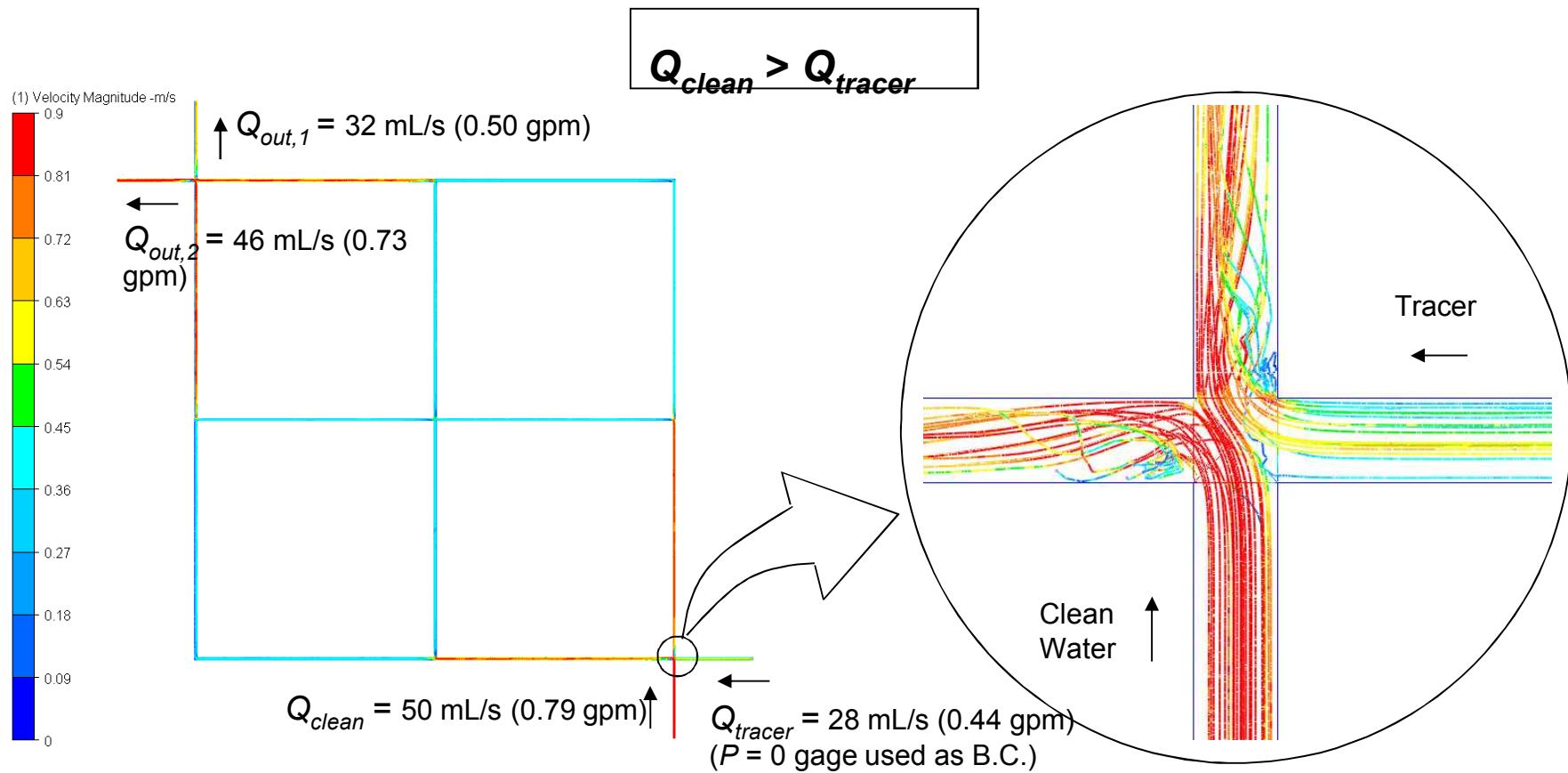
Single-Joint Results



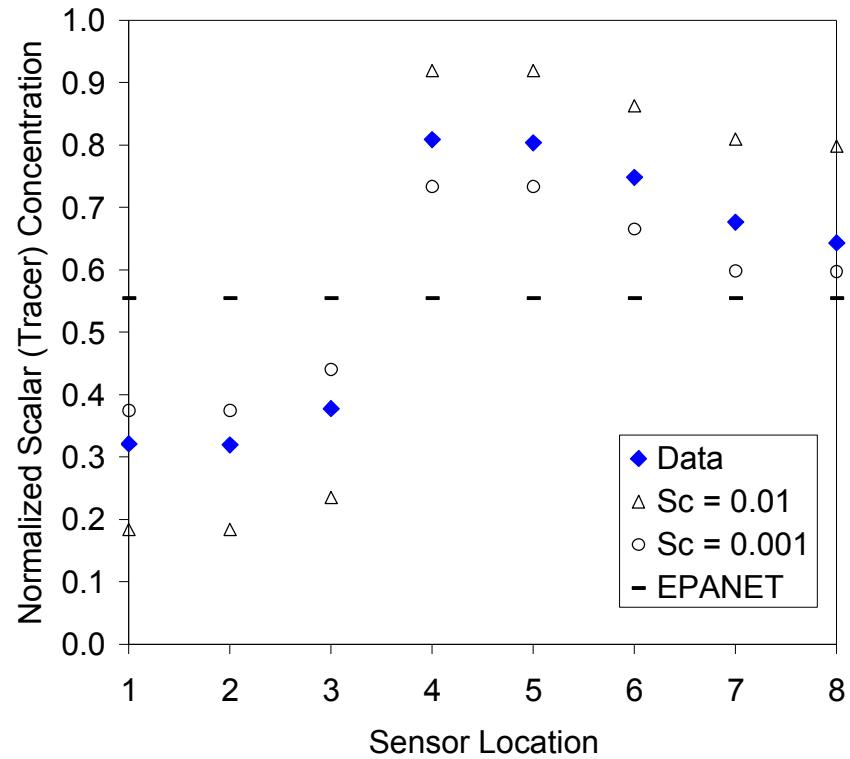
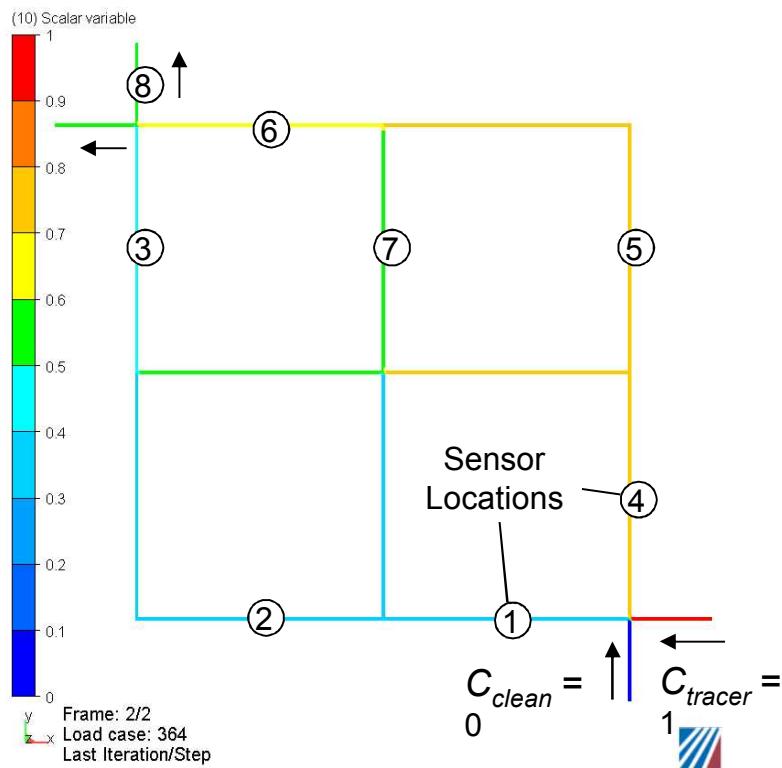
Network Hydraulic Results



Network Hydraulic Results

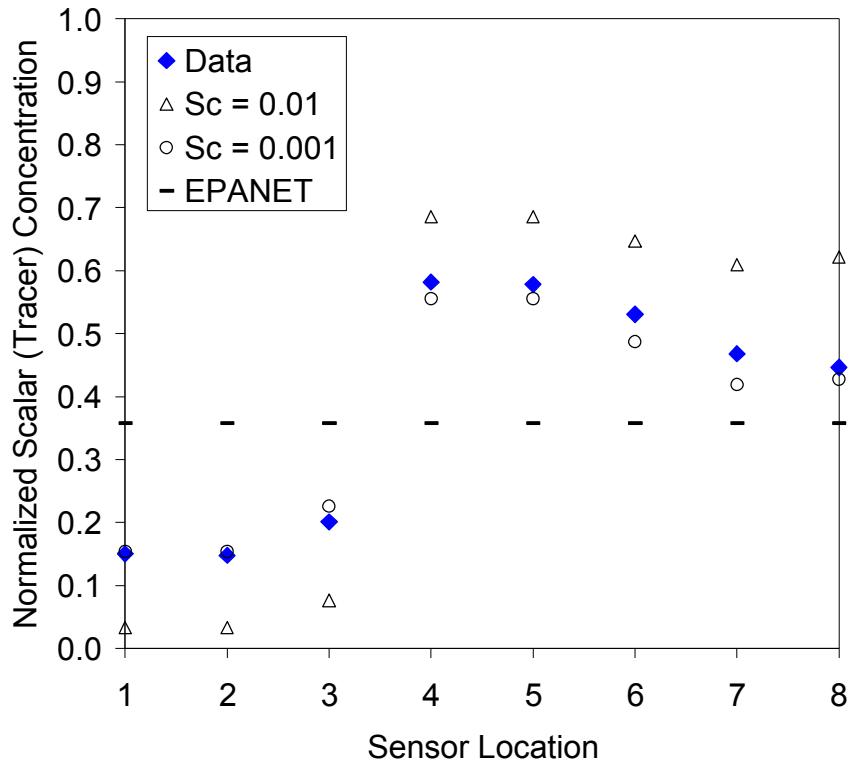
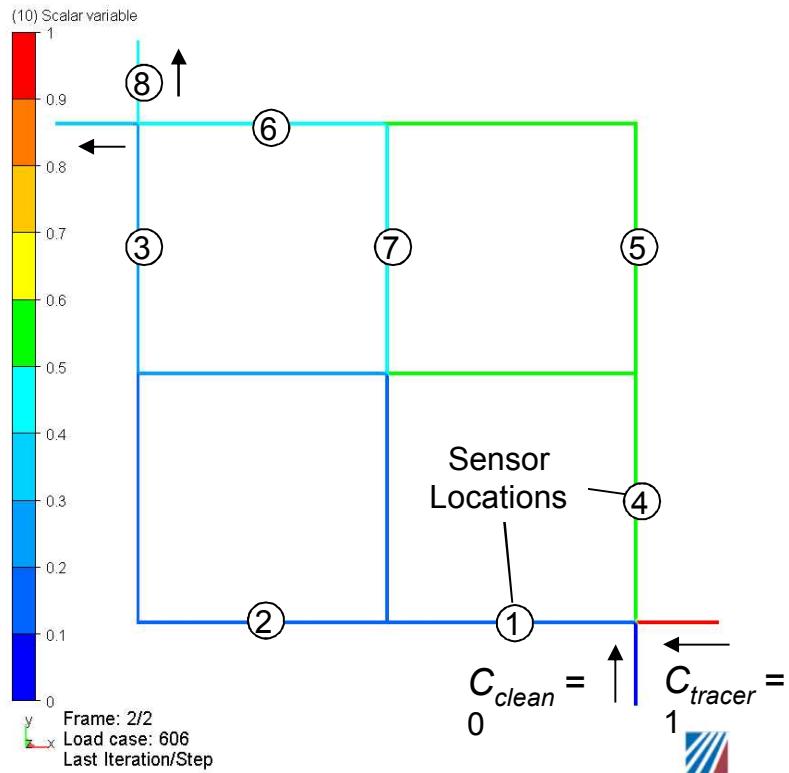


Network Tracer Results



Network Tracer Results

$$Q_{clean} > Q_{tracer}$$





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Conclusions

- Water flow and tracer transport were tested experimentally and simulated using CFD models of turbulent flow
- A turbulent Schmidt number (turbulent diffusivity) was calibrated using single-joint test results
 - $0.001 < Sc < 0.01$
- Mixing in cross joints decreased slightly as the velocity was increased for a fixed diameter pipe ($\sim 10,000 < Re < \sim 40,000$)
 - Increased momentum and reduced time of contact may dampen and offset the tendency for instabilities to increase mixing at the impinging interface at higher velocities



Conclusions (cont.)

- A small network with 3x3 array of cross joints was tested and simulated
 - Incomplete mixing resulted even after several junctions
 - Unequal inlet flow rates significantly affects mixing
 - Increased momentum from the higher flow-rate inlet allowed some fluid to cross over the junction into the opposite outlet pipe
 - Mixing is caused by both bulk flow (advection) and turbulent diffusion at impinging interface
 - Calibrated turbulent Schmidt numbers yielded good agreement between data and simulations



Next Steps

- **Continue physical and numerical simulations**
 - Evaluate mixing in more complex configurations and networks
 - Evaluate the effects of transient oscillations and storage on mixing in pipe networks



Backup Slides



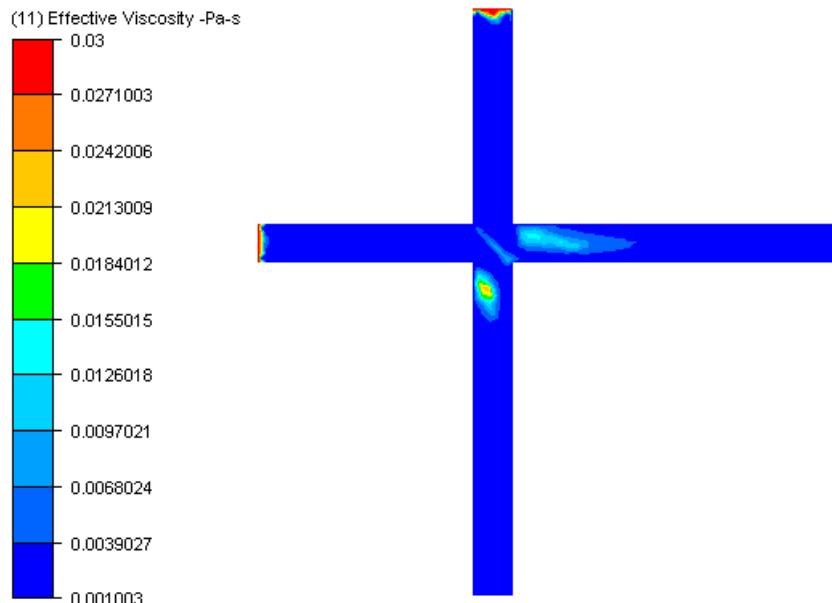
Mesh Refinement

Model Configuration	Element Size	Number of Elements
Single-Joint Cross 1.27 cm (0.5") diameter pipe	2.5 mm (pipe) 1.5 mm (junction)	46,352
Single-Joint Cross 5.08 cm (2") diameter pipe	10 mm (pipe) 6 mm (junction)	46,352
Single-Joint Double-T 1.27 cm (0.5") diameter pipe 2.5 diameter spacing between T-fittings	2.5 mm (pipe) 1.5 mm (junction)	56,093
Single-Joint Double-T 1.27 cm (0.5") diameter pipe 5 diameter spacing between T-fittings	2.5 mm (pipe) 1.5 mm (junction)	56,382
3x3 Network 1.27 cm (0.5") diameter pipe	2.5 mm (pipe) 1.5 mm (junction)	1,190,163

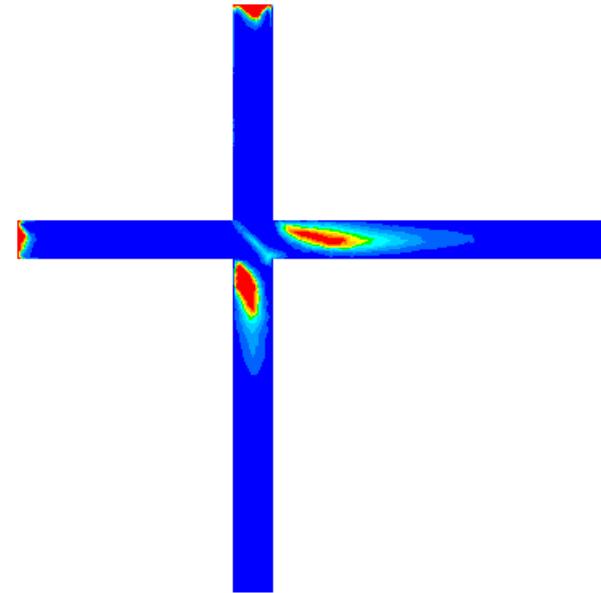


Simulated Eddy Viscosity

Re=5,000



Re=10,000



Simulated effective (eddy) viscosity [Pa-s] distribution for the 1.27 cm (0.5") diameter cross-joint configuration at two different Reynolds numbers: 5,000 (left) and 10,000 (right)